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National Aeronautics and Space Administration  
Lyndon B. Johnson Space Center  
Space Science Branch  
ATTN: Eric L. Christiansen  
Houston, TX 77058

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for research entitled

**DESIGN OF ORBITAL DEBRIS SHIELDS FOR OBLIQUE  
HYPERVELOCITY IMPACT**

(NASA-CR-195152) DESIGN OF ORBITAL  
DEBRIS SHIELDS FOR OBLIQUE  
HYPERVELOCITY IMPACT Final Report  
(Texas Univ.) 111 p

Submitted by

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## ABSTRACT

A new impact debris propagation code has been written to link CTH simulations of space debris shield perforation to the Lagrangian finite element code DYNA3D, for space structure wall impact simulations. This software (DC3D) simulates debris cloud evolution using a nonlinear elastic-plastic deformable particle dynamics model, and renders computationally tractable the supercomputer simulation of oblique impacts on Whipple shield protected structures. Comparison of three dimensional, oblique impact simulations with experimental data shows good agreement over a range of velocities of interest in the design of orbital debris shielding.

Source code developed during this research is provided on the enclosed floppy disk. An abstract based on the work described in this report has been submitted to the 1994 Hypervelocity Impact Symposium.

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## 1. Introduction

The design of the space station Freedom and similar structures for earth orbit must include provisions for the effects of hypervelocity impact, which may arise as a result of space debris or micrometeorite encounters. This problem can be expected to become increasingly important as longer duration space missions are launched, increasing the exposure time of orbiting systems. Such missions provide increased probability of impact damage while placing greater reliability demands on vehicles and structures. Existing light gas gun facilities used in the study of hypervelocity impact effects do not generally allow for tests at velocities above ten kilometers per second, suggesting the use of computer simulation methods for orbital debris shield design at those velocities.

The accomplishment of design goals for the space station and similar structures depends in part upon the development and verification of computationally tractable models capable of describing oblique hypervelocity impact effects at velocities beyond existing experimental capabilities. Experience to date has shown that the extreme CPU time and memory requirements of standard Eulerian hydrocodes (McGlaun et al., 1990) make their use in direct simulation of three dimensional impacts on space debris shields impractical, even given supercomputer resources. In addition, current Eulerian hydrocodes do not in general rigorously account for material history effects on the failure of space structures under impact debris loading. Conventional Lagrangian finite element codes (Goudreau and Hallquist, 1982), on the other hand, are not suitable for use in simulating the shield perforation portion of the impact problem. Mesh distortion effects greatly reduce the size of the time step used in the calculations, and mandate frequent rezoning. As a result of the preceding difficulties, the only general simulation technique demonstrated to date has involved the systematic linking of Eulerian hydrocodes (of shield perforation) to Lagrangian finite element models (of debris cloud evolution and debris impact on the protected structure). This approach has been developed and implemented by the principal investigator (Fahrenthold, 1993).

The development of particle-based debris cloud evolution models [e.g. Fritts et al. (1985), Trease et al. (1990), Monaghan (1988), and Trease (1988)], offers an opportunity to directly simulate complete three-dimensional debris impact problems on existing supercomputers. Particle-based methods address the previously discussed shortcomings of Eulerian and Lagrangian codes in two ways: (1) they effectively eliminate the mesh distortion problems of Lagrangian finite element codes, and (2) they greatly improve on the CPU time efficiency of Eulerian hydrocodes while allowing for accurate tracking of material history dependent effects such as plastic deformation. As an application which has severely taxed the capabilities of conventional Eulerian and Lagrangian computer codes, orbital debris shield design is well suited to capitalize on the strengths of new particle-based modeling techniques. Hence the research presented here has: (1) developed a debris cloud evolution code which links shield perforation and wall impact simulations, (2) conducted three dimensional, supercomputer based simulations of shield impact, debris cloud evolution, and wall impact problems, and (3) evaluated and validated the computer models using data from experiments conducted at NASA Johnson Space Center. This computer simulation methodology allows for the modeling of impacts at velocities beyond ten kilometers per second which are very difficult to duplicate in the laboratory.

## **2. Methodology**

The problem of hypervelocity impact on space structures has been an object of research since the 1950's, as reflected in the summary of Hypervelocity Impact Symposia presented during recent conferences in that series (e.g. Anderson, 1986). However both experimental and analytical research work has accelerated in recent years, with most recent NASA interest focused on debris effects on the space shuttle and planned space station. A significant data base exists for impacts at velocities below ten kilometers per second (Tower et al., 1987), including studies aimed specifically at NASA applications such as space shuttle windows (Schneider and Stilp, 1987) and debris shield



design (Yew and Kendrick, 1986). However difficulties with conducting experiments at higher velocities, relevant to both the space station and future programs, have limited the ability to evaluate new designs in a laboratory setting.

The preceding facts suggest a combined experimental and analytical approach to micrometeorite and debris shield design, using experimental data at velocities below ten kilometers per second to critique and verify computer models, which then provide a basis for higher velocity design calculations. The simulation work described here was conducted on a Cray Y-MP/864 supercomputer at the University of Texas System Center for High Performance Computing.

The principal investigator has made extensive use of existing supercomputer based Eulerian and Lagrangian hydrocodes to evaluate their use in orbital debris shield design. In general Eulerian codes are best suited to hypervelocity impact simulations where impact pressures are sufficiently large to render material strength effects generally unimportant. An Eulerian code is best used to predict initial debris cloud mass and distribution as a function of projectile material type and velocity, shield material type and geometry, and other parameters. The protected space structure must be designed to avoid spallation or fracture under the debris cloud impact. Since spallation and fracture processes are very stress and strain history dependent phenomena (Yew and Taylor, 1992, and Grady and Kipp, 1987), and since Lagrangian hydrocodes are best suited to trace stress and strain history in solid materials, a Lagrangian hydrocode model of debris cloud impact on the inner wall is most appropriate. The new modeling approach outlined here links both parts of the impact event using a new analysis methodology, significantly reducing computer resource requirements for oblique impact calculations.

### **3. Particle Dynamics Model**

#### **a. Introduction**

This section describes a new modeling approach combining Lagrangian bond graphs (Fahrenthold and Wargo, 1994) with a selected finite element discretization

scheme to allow for direct simulation of the dynamic evolution of debris particles arising from hypervelocity impact.

### b. Kinematics

The homogeneous deformation field associated with the finite element discretization employed here allows the position  $\mathbf{x}$  and velocity  $\mathbf{v}$  of any mass particle "P" in a particular element to be written in the form (Malvern, 1969)

$$\mathbf{x} = \mathbf{F}(t) (\mathbf{r} - \mathbf{r}_C) + \mathbf{c}(t) ; \quad \mathbf{v} = \dot{\mathbf{F}}(t) (\mathbf{r} - \mathbf{r}_C) + \dot{\mathbf{c}}(t) \quad (1a,b)$$

where  $\mathbf{c}(t)$  and  $\dot{\mathbf{c}}(t)$  are the position and velocity of the element center of mass "C",  $\mathbf{r}$  and  $\mathbf{r}_C$  are the position of P and C in the reference (initial undeformed) configuration of the body, and  $\mathbf{F}$  is the deformation gradient tensor. Note that since  $\mathbf{r}$  and  $\mathbf{r}_C$  in equations (1) are constants, the motion of any particle P in the element is determined by the motion of C and by the time dependent components of the second order tensor  $\mathbf{F}$ , related to the rate of deformation ( $\mathbf{D}$ ) and velocity gradient ( $\mathbf{L}$ ) tensors by

$$\mathbf{D} = (1/2) [\mathbf{L} + \mathbf{L}^T] ; \quad \mathbf{L} = \dot{\mathbf{F}}\mathbf{F}^{-1} \quad (2a,b)$$

where the superscripts "-1" and "T" denote the inverse and the transpose. In the special case where  $\mathbf{L}$  is the skew-symmetric tensor whose axial vector is the angular velocity, equation (1b) represents rigid body motion (Casey, 1983, and Fahrenthold and Wargo, 1991a and b).

### c. Kinetic energy

The homogeneous deformation kinematics of equations (1) allows the kinetic co-energy ( $T^*$ ) of a single element of fixed mass "m" and variable volume "V" to be expressed in the form

$$T^* = (1/2) \int_V \rho \mathbf{v} \cdot \mathbf{v} \, dV \quad (3a)$$

$$= (1/2) \left\{ \int_V \rho \dot{\mathbf{c}} \cdot \dot{\mathbf{c}} \, dV + \int_V \rho \dot{\mathbf{F}}(\mathbf{r} - \mathbf{r}_C) \cdot \dot{\mathbf{F}}(\mathbf{r} - \mathbf{r}_C) \, dV + 2\dot{\mathbf{c}} \cdot \dot{\mathbf{F}} \int_V \rho(\mathbf{r} - \mathbf{r}_C) \, dV \right\} \quad (3b)$$

$$= (1/2) [ m\dot{\mathbf{c}} \cdot \dot{\mathbf{c}} + \text{tr}(\dot{\mathbf{F}}^T \dot{\mathbf{F}} \mathbf{J}) ] \quad (3c)$$

where  $\rho$  is the density, "tr" is the trace operator,  $\mathbf{J}$  is an inertia tensor,

$$\mathbf{J} = \int_V \rho_0 (\mathbf{r} - \mathbf{r}_c) \otimes (\mathbf{r} - \mathbf{r}_c) dV_0 \quad (3d)$$

and conservation of mass requires

$$dm = \rho dV = \rho_0 dV_0 \quad (3e)$$

with  $\rho_0$  the density in the reference configuration. Note that the third term in equation (3b) is zero by definition of the center of mass. Since  $\mathbf{J}$  is a constant tensor defined in the reference configuration, the element momenta  $\mathbf{p}$  and  $\mathbf{H}$  are defined by

$$\mathbf{p} = \partial T^* / \partial \dot{\mathbf{c}} = m \dot{\mathbf{c}} ; \mathbf{H} = \partial T^* / \partial \dot{\mathbf{F}} = \dot{\mathbf{F}} \mathbf{J} \quad (4a,b)$$

Since the kinetic energy ( $T$ ) of the finite element is

$$T = \mathbf{p} \cdot \dot{\mathbf{c}} + \text{tr}(\mathbf{H}^T \dot{\mathbf{F}}) - T^* \quad (5a)$$

it follows that

$$T = (1/2) [ m^{-1} \mathbf{p} \cdot \mathbf{p} + \text{tr} \{ (\mathbf{H} \mathbf{J}^{-1})^T \mathbf{H} \} ] \quad (5b)$$

The preceding results demonstrate that kinetic energy storage in a single finite element may be modeled using the bond graph multiports shown in Figure 1. The kinetic energy function may be represented in the most familiar form by the introduction of a fourth order inertia tensor  $\mathbf{G}$ , defined by

$$\mathbf{G} \underset{\approx}{=} \frac{\partial^2 T^*}{\partial \dot{\mathbf{F}} \partial \dot{\mathbf{F}}} \quad (6a)$$

so that

$$T^* = (1/2) [ m \dot{\mathbf{c}} \cdot \dot{\mathbf{c}} + \dot{\mathbf{F}} : \mathbf{G} : \dot{\mathbf{F}} ] ; T = (1/2) [ m^{-1} \mathbf{p} \cdot \mathbf{p} + \mathbf{H} : \mathbf{G}^{-1} : \mathbf{H} ] \quad (6b,c)$$

Now the constitutive relation (4b) takes the form

$$\mathbf{H} = \mathbf{G} \dot{\mathbf{F}} \quad (6d)$$

#### d. Internal energy

The preceding discussion of inertia effects must be augmented by an RC network description of internal energy storage and energy dissipation in the material. Unlike the inertia multiports, the capacitance and resistance multiports required to model a particular material must be formulated for each material type. To illustrate this procedure, this section considers the large strain deformation of an elastic-viscoplastic material (Haupt,

1985). This case emphasizes the applicability of the bond graph modeling methodology described here to very complex engineering materials (Fahrenthold and Wu, 1988), and hence to system dynamics and impact dynamics problems of a very general nature. Note that the conventional assumptions of infinitesimal strain and linear stress-strain behavior, included in the vast majority of mechanical vibrations models, are not adopted here. Since the large strains and the relatively complex material response considered here often calls for special purpose finite element code development work, the example material selected demonstrates the simplicity of the proposed modeling methodology, as compared to conventional displacement-based finite element analysis.

Before formulating a stored energy function for an elastic-plastic material, it is appropriate to first define the system kinematics. A very general description of the large strain kinematics of elastic-plastic deformation is provided by a multiplicative decomposition of the deformation gradient tensor  $\mathbf{F}$  in the form (Haupt, 1985)

$$\mathbf{F} = \mathbf{F}^e \mathbf{F}^p ; \dot{\mathbf{F}} = \dot{\mathbf{F}}^e \mathbf{F}^p + \mathbf{F}^e \dot{\mathbf{F}}^p \quad (7a,b)$$

where  $\mathbf{F}^e$  describes the elastic deformation of the solid material from the unloaded plastically deformed configuration and  $\mathbf{F}^p$  relates the unloaded plastically deformed configuration of the material to the original undeformed reference configuration. Hence the rate of change of  $\mathbf{F}$  may be decomposed as in equation (7b) into a first term governing the rate of elastic energy storage and a second term governing the rate of plastic energy dissipation. In this case, the presence of both complex kinematics and energy dissipation effects highlights the value of bond graphs in nonlinear system modeling.

Since most elastic-plastic modeling work begins with a Helmholtz free energy function and then derives the internal energy, that procedure is followed here. The elastic-plastic kinematics just described are associated with a Helmholtz free energy density function of the form (Dashner, 1986)

$$\psi = \psi(\mathbf{F}^e, \mathbf{F}^p, \theta) \quad (7c)$$

Here  $\psi$  is assumed to take the conventional functional form (Bowen, 1989)

$$\psi = (1/\rho_\alpha) \{ (\lambda/2) \text{tr}(\mathbf{E}^e)^2 + \mu \text{tr}(\mathbf{E}^e)^2 - \beta(\theta - \theta_0) \text{tr}(\mathbf{E}^e) - [(c\rho_\alpha)/(2\theta_0)](\theta - \theta_0)^2 \} \quad (7d)$$

where  $\lambda$  and  $\mu$  are Lamé constants for an isotropic solid,  $c$  is the specific heat,  $\theta_0$  is a reference temperature,  $\rho_\alpha$  is the density in the unloaded plastically deformed configuration, and

$$\mathbf{E}^e = (1/2) [ \mathbf{F}^{eT} \mathbf{F}^e - \mathbf{I} ] ; \beta = k (3\lambda + 2\mu) ; \rho_0/\rho_\alpha = \det(\mathbf{F}^p) \quad (7e,f,g)$$

with "k" the thermal expansion coefficient and "det" the determinant operator. For an element of mass "m", this corresponds to a (conserved) internal energy function

$$U = m\psi + \theta S \quad (8a)$$

where  $S$  is the total entropy, defined by the thermodynamic identity

$$S = - \frac{\partial(m\psi)}{\partial\theta} = (m/\rho_\alpha) \{ c\rho_\alpha [ (\theta/\theta_0) - 1 ] + \beta \text{tr}(\mathbf{E}^e) \} \quad (8b)$$

Equations (7) and (8) may be combined to yield

$$U = (m/\rho_0) \det(\mathbf{F}^p) \{ \mu \text{tr}(\mathbf{E}^e)^2 + (\lambda/2) \text{tr}(\mathbf{E}^e)^2 + \beta\theta_0 \text{tr}(\mathbf{E}^e) \} + \\ [(cm\theta_0)/2] \{ [ 1 + S/(mc) - (\beta/(c\rho_0)) \det(\mathbf{F}^p) \text{tr}(\mathbf{E}^e) ]^2 - 1 \} \quad (8c)$$

The functional form for the internal energy

$$U = U(\mathbf{F}^e, \mathbf{F}^p, S) \quad (9a)$$

leads to the multiport capacitor shown in Figure 2, where in this case

$$\mathbf{K}^e = \frac{\partial U}{\partial \mathbf{F}^e} \Big|_{\mathbf{F}^p, S} = (m/\rho_\alpha) \mathbf{F}^e \{ [\lambda + ((\beta^2\theta_0)/(c\rho_\alpha))] \text{tr}(\mathbf{E}^e) \mathbf{I} + \\ 2\mu \mathbf{E}^e - [(\beta\theta_0 S)/(mc)] \mathbf{I} \} \quad (9b)$$

$$\mathbf{K}^p = \frac{\partial U}{\partial \mathbf{F}^p} \Big|_{\mathbf{F}^e, S} = (m/\rho_\alpha) \{ [(\lambda/2) + ((\beta^2\theta_0)/(c\rho_\alpha))] \text{tr}(\mathbf{E}^e)^2 + \\ \mu \text{tr}(\mathbf{E}^e)^2 - [(\beta\theta_0 S)/(mc)] \text{tr}(\mathbf{E}^e) \} \mathbf{F}^{p-T} \quad (9c)$$

$$\theta = \frac{\partial U}{\partial S} \Big|_{\mathbf{F}^e, \mathbf{F}^p} = \theta_0 \{ 1 + S/(mc) - [\beta/(c\rho_\alpha)] \text{tr}(\mathbf{E}^e) \} \quad (9d)$$

### e. Plastic deformation

The material description is completed by defining the plastic constitutive relations.

For simplicity, the rate form

$$\mathbf{K}^d = \eta (m/\rho_\alpha) \mathbf{L}^P ; \mathbf{L}^P = \dot{\mathbf{F}}^P \mathbf{F}^{P-1} \quad (10a,b)$$

is adopted here, with  $\eta$  a viscosity coefficient. The second order tensor  $\mathbf{K}^d$  (dimensionally an extensive chemical potential) is the effort power conjugate to  $\mathbf{L}^P$ .

A model for the elastic-viscoplastic material just defined is shown in Figure 2.

Note that a transformer with fourth order tensor modulus  $\mathbf{M}$ , defined by components

$$M_{ijrs} = \delta_{ir} F_{sj}^{P-1} \quad (11)$$

is introduced in order to conform to the fundamental kinematic relation (10b).

### f. Bond graph model

The bond graph structure of Figure 2 may be directly augmented with inertia multiports representing the kinetic energy contributions associated with  $\mathbf{p}$  and  $\mathbf{H}$ . Finally if the appropriate RC network model representing elastic-viscoplastic materials is introduced, the result is the complete element-level bond graph shown in Figure 3, representing the "ith" element of the system. Assuming adiabatic deformation, thermal energy is stored, as indicated by the thermomechanical coupling shown in Figure 3. Note that in Figure 3 transformers with moduli

$$M_{ijkl}^{e(i)} = \delta_{jl} F_{ik}^{e(i)-1} ; M_{ijkl}^{p(i)} = \delta_{ik} F_{lj}^{p(i)-1} \quad (12a,b)$$

are introduced in accordance with the kinematics of equations (7a and b).

### g. State equation derivation

The causally augmented bond graph of Figure 3 and the constitutive relations previously defined yield (Rosenberg and Karnopp, 1983) state equations for the "ith" element of the form:

$$\dot{\mathbf{p}}^{(i)} = \mathbf{0} \quad (13a)$$

$$\dot{\mathbf{H}}^{(i)} = - \mathbf{M}^{p(i)T} \mathbf{K}^{e(i)}(\mathbf{F}^{e(i)}, \mathbf{F}^{p(i)}, \mathbf{S}^{(i)}) \quad (13b)$$

$$\dot{\mathbf{F}}^e(i) = \underset{\approx}{\mathbf{M}}^{p(i)} \underset{\approx}{\mathbf{G}}^{(i)-1} \mathbf{H}^{(i)} - \{\rho_{\alpha}^{(i)}/(\eta m^{(i)})\} \underset{\approx}{\mathbf{M}}^{p(i)} \underset{\approx}{\mathbf{M}}^{e(i)-1} \underset{\approx}{\mathbf{M}}^{(i)-1} \mathbf{K}^d(i) \quad (13c)$$

$$\dot{\mathbf{F}}^p(i) = \{\rho_{\alpha}^{(i)}/(\eta m^{(i)})\} \underset{\approx}{\mathbf{M}}^{(i)-1} \mathbf{K}^d(i) \quad (13d)$$

$$\dot{\mathbf{S}}^{(i)} = [1/\theta^{(i)}(\mathbf{F}^e(i), \mathbf{F}^p(i), \mathbf{S}^{(i)})] \{\rho_{\alpha}^{(i)}/(\eta m^{(i)})\} \text{tr}\{ \mathbf{K}^d(i)^T \mathbf{K}^d(i) \} \quad (13e)$$

where

$$\mathbf{K}^d(i) = \underset{\approx}{\mathbf{M}}^{(i)-T} [ \underset{\approx}{\mathbf{M}}^{e(i)-T} \underset{\approx}{\mathbf{M}}^{p(i)T} \mathbf{K}^e(i)(\mathbf{F}^e(i), \mathbf{F}^p(i), \mathbf{S}^{(i)}) - \mathbf{K}^p(i)(\mathbf{F}^e(i), \mathbf{F}^p(i), \mathbf{S}^{(i)}) ] \quad (13f)$$

and the functions  $\mathbf{K}^e(i)$ ,  $\mathbf{K}^p(i)$ , and  $\theta^{(i)}$  are defined by equations (9). Note that

$$\mathbf{M}_{ijkl}^{e(i)-1} = \delta_{jl} F_{ik}^{e(i)} \quad ; \quad \mathbf{M}_{ijkl}^{p(i)} = \delta_{ik} F_{lj}^{p(i)-1} \quad ; \quad \mathbf{M}_{ijkl}^{(i)-1} = \delta_{ik} F_{lj}^{p(i)} \quad (14a,b,c)$$

Equations (13) are nonlinear equations in the state variables:  $\mathbf{p}^{(i)}$ ,  $\mathbf{H}^{(i)}$ ,  $\mathbf{F}^e(i)$ ,  $\mathbf{F}^p(i)$ , and  $\mathbf{S}^{(i)}$ .

#### h. Conclusion

The outlined modeling methodology may be implemented numerically, for a variety of internal energy functions and plasticity models, for use in engineering analysis and design. The source code listing at Appendix G represents an isothermal, variable compressibility implementation using the plasticity theory of Green and Naghdi (1971).

### 4. Comparison to Experiments

#### a. Introduction

Three dimensional simulation of hypervelocity impacts on space structures places extreme demands on even supercomputer resources. To reduce the computer time and memory requirements of oblique impact simulations, a three-dimensional, deformable particle dynamics model of the type just described has been coded and linked to an Eulerian hydrocode and a Lagrangian structural code, and applied in the simulation of oblique hypervelocity impacts on Whipple shield protected structures. Comparison of the results to experimental data shows good agreement at a computer time and memory cost much less than that associated with conventional hydrocode calculations.

This section describes evaluation of the preceding modeling approach using data from Whipple shield impact experiments conducted at NASA Johnson Space Center, including CPU time requirements for the simulation of representative oblique impact problems.

#### **b. Methodology**

The deformable particle dynamics model of debris cloud evolution is referred to here by the title DC3D. This numerical model is used in combination with the Eulerian hydrocode CTH (McGlaun et al., 1990) and the structural finite element code DYNA3D (Goudreau and Hallquist, 1982) as follows. An Eulerian simulation is first employed to model impact on the shield. Then post-processing of the velocity, mass density, and void space distribution data from the Eulerian simulation is used to establish the initial state of the elastic-plastic model of the debris cloud. Numerical integration of the particle dynamics model DC3D, using established system dynamics modeling techniques (Rosenberg and Karnopp, 1983) provides a thermodynamically rigorous yet computationally efficient basis for predictions of debris cloud evolution over the relatively large spaces which normally separate shields from the space structure which they protect. Output from the debris cloud evolution model then provides a basis for the simulation of impact on the wall plate, using DYNA3D. Input data for the wall impact simulation is generated automatically by DC3D, based on the final state of the debris cloud propagation model. By using a momentum deposition representation of the debris cloud loading on the wall plate (calculated from the DC3D results), meshing of each debris particle in DYNA3D can be avoided, yielding additional reductions in computer time and memory requirements.

#### **c. Oblique impact example**

The analysis procedure just discussed may be illustrated by considering an oblique impact simulation for a Whipple shield configuration. Specifically, consider the oblique (23 degree) impact of a 15/64 inch diameter aluminum (2017-T4) sphere, at 7.1 kilometers per second, on a 0.063 inch thick aluminum (7075-T6) shield, protecting a



0.125 inch thick aluminum (7075-T6) wall plate. The shield to wall plate spacing is 4.0 inches. Figure 4 shows the CTH simulation results for impact on the shield, at four microseconds after impact. (Note that due to symmetry, all of the figures discussed here depict only one-half of the physical system modeled.) The code DC3D was then employed to: (1) post-processes the CTH results to formulate a debris cloud model, (2) propagate the debris to the wall plate, and (3) generate a DYNA3D input file for use in modeling impact of the debris cloud on the wall plate. DC3D uses a variable step method for numerical integration of the first order state equations describing the elastic-plastic debris cloud dynamics, and commercial plotting routines for graphical representation of the simulation results. Figure 5 shows the predicted impact momentum distribution on the wall plate. Finally a DYNA3D simulation of the wall plate impact was conducted, using a momentum deposition approach to represent the effects of the debris. Figures 6 and 7 show front and rear views of the wall plate impact simulation, including extensive spallation observed in the experiment.

By making appropriate use of Eulerian and Lagrangian codes for those parts of the simulation where they are both accurate and computationally tractable, this approach does not suffer from the limiting assumptions of many previous attempts to model shield impact problems (e.g. Swift et al., 1983). In addition, that portion of the total impact simulation described by the debris cloud model incorporates arbitrarily nonuniform, three-dimensional velocity, density, and void space distributions not admitted by many simplified debris models published to date (Grady and Passman, 1990). In summary, the approach used here makes use of the known strengths of available codes while providing an essential improvement in computational efficiency for oblique impact simulation. Such an improvement is essential before computer codes can provide a practical analytical design tool.

The preceding example demonstrates the feasibility of the modeling approach. Its computational efficiency is such that computer resource requirements are relatively

modest, considering the three dimensional nature of the simulations. Typical CPU time requirements are listed in Table 1.

#### **d. Ballistic limit calculations**

Finally it is worthwhile to compare some hypervelocity impact simulation results with ballistic limit calculations based on published experimental research. Figure 8 depicts a typical Ballistic limit curve, and indicates the velocities and impact particle diameters used in the simulations. Figures 9 through 20 show results of the simulation of oblique Whipple shield impacts at 7 and 10 kilometers per second, using the debris propagation code and the general modeling methodology developed under this project. The cases represented are listed in Table 2.

Note that the simulations were conducted for particle diameters above and below the expected ballistic limits for the two velocities. The simulations are consistent with the ballistic limit curve data at 7 km/sec. At 10 km/sec, the simulations suggest slightly less wall damage than might be expected from the ballistic limit curve. Computer time requirements are very modest, considering the complexity of the problems.

### **5. Conclusion**

The outlined research has addressed fundamental problems relevant to the development of space vehicles and structures for a variety of missions. It makes use of state of the art supercomputer resources while applying the newest numerical modeling techniques, designed to make oblique impact simulations computationally tractable. It included numerical implementation of a nonlinear, elastic-plastic debris cloud dynamics model important to accurate shield impact calculations. The resulting simulation capability can provide an important adjunct to experimental work on space shield design for a variety of future missions. The outlined work has been coordinated directly with NASA JSC experimental research efforts, and the final source code has been provided to NASA. It is therefore suggested that the proposed research has addressed important objectives of the NASA Regional Universities Grant Program.

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**Table 1. Example Oblique Impact Simulations**

shield to wall spacing:	4.0-8.0 inches
shield thickness:	0.063-0.071 inches
wall thickness:	0.125-0.160 inches
impact velocity:	7.1-7.6 km/sec
impact obliquity:	23.0-58.4 degrees
impact mass:	0.202-0.376 grams
material:	aluminum

Simulation type	Computer system	Code	Memory	CPU time
shield impact	Cray Y-MP/864	CTH	< 64 MB	2.0-6.0 hrs
debris evolution	IBM RS/6000*	DC3D	< 16 MB	0.5-3.0 days
wall impact	Cray Y-MP/864	DYNA3D	< 64 MB	0.5-1.0 hrs

\*The CPU time range given is for a Model 320, a very low performance system.

**Table 2. Ballistic Limit Simulations**

bumper thickness	=	0.127 cm
wall thickness	=	0.3175 cm
impact obliquity	=	25 degrees
material	=	Al 6061-T6

(also see the ballistic limit plot in Figure 8)

<u>Simulation #</u>	<u>Impact velocity</u>	<u>Particle diameter</u>	<u>Figures</u>
7a	7 km/sec	0.575 cm	9 through 11
7b	7 km/sec	0.475 cm	12 through 14
10a	10 km/sec	0.530 cm	15 through 17
10b	10 km/sec	0.430 cm	18 through 20

CPU time requirements

bumper impact simulations (CTH):	1.80-2.11 CPU hrs, Cray YMP
debris transport calculations (DC3D):	3.34-5.67 CPU hrs, IBM RS/6000
wall impact calculations (DYNA3D):	0.27-0.28 CPU hrs, Cray YMP

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- Figure 19. DC3D simulation 10b results: areal density of the debris cloud momentum deposited on the wall plate.
- Figure 20. DYNA3D simulation 10b results: front surface of the wall plate.

Figure 1

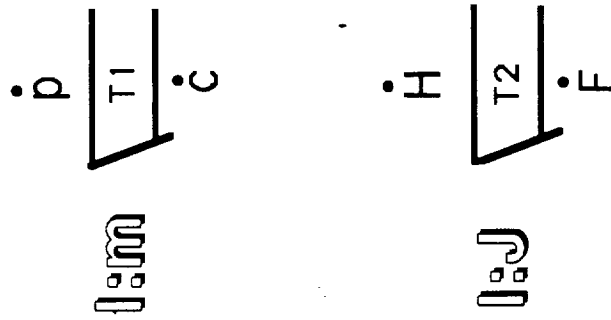




Figure 2

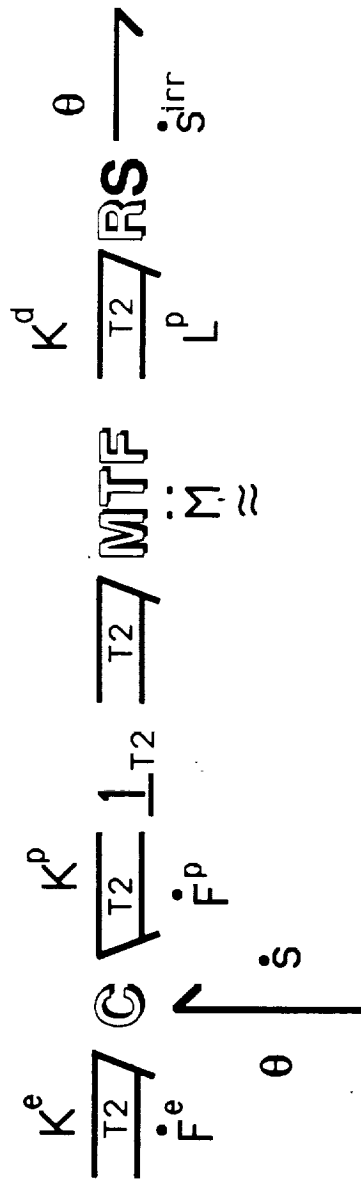
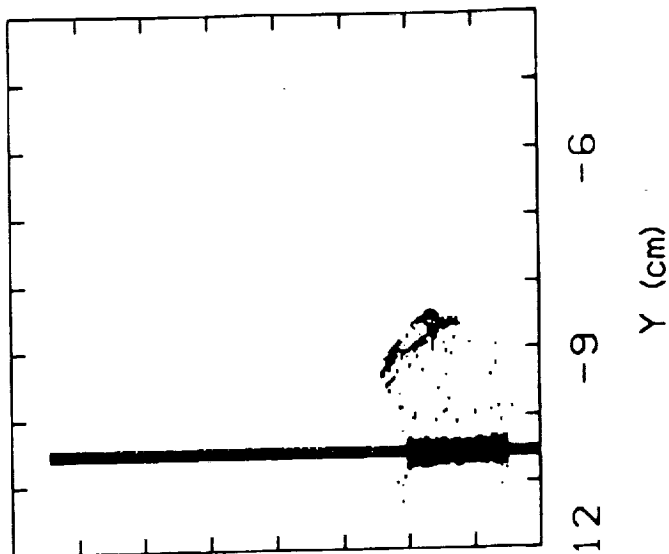
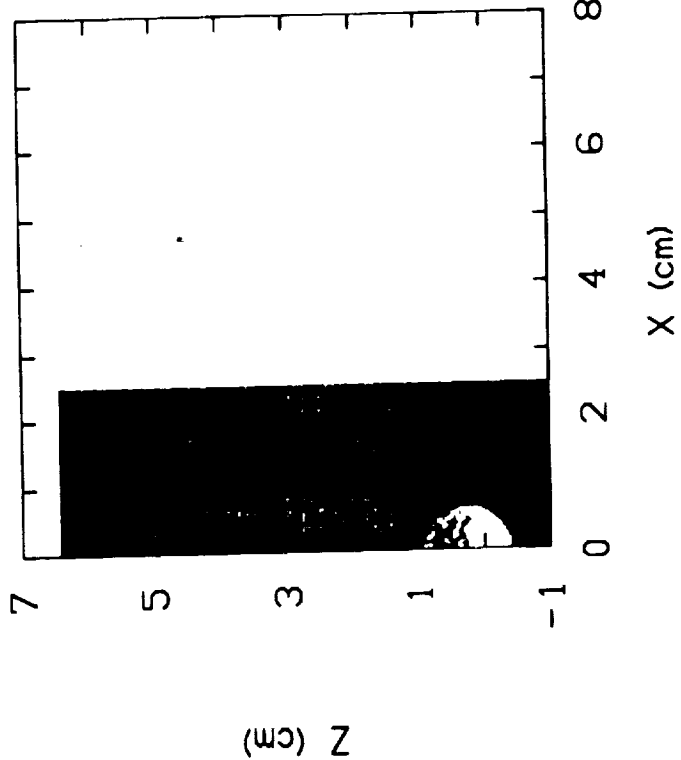
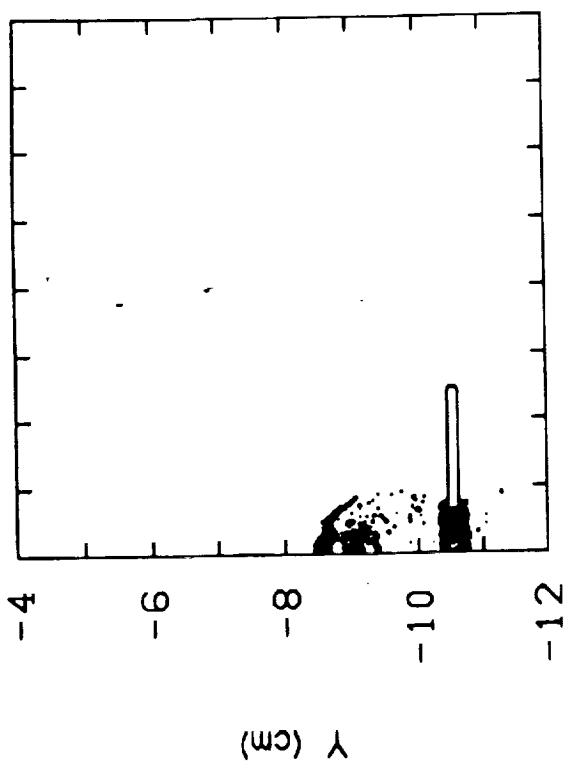




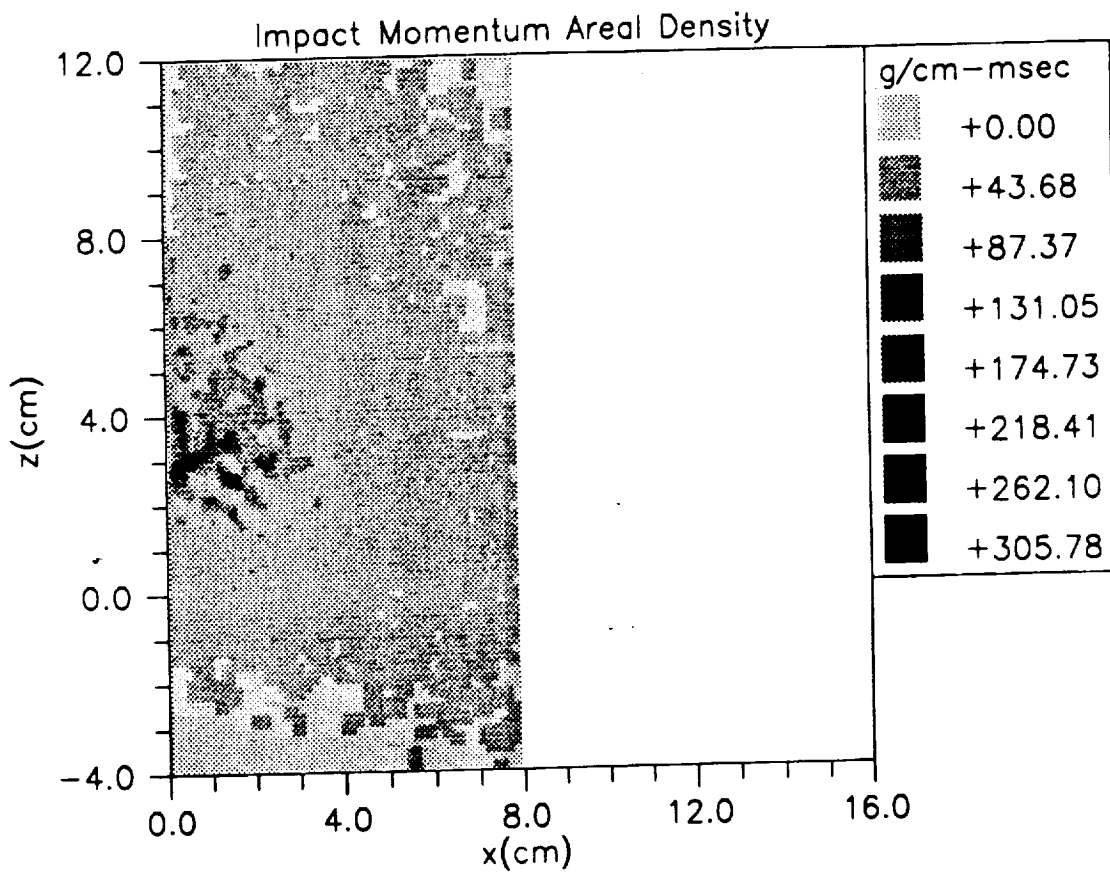
Figure 4

Time = 4.0160E-06  
Materials GTUDYV  
— 1 07/21/93  
— 2 10:02:33  
Block 1



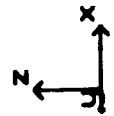
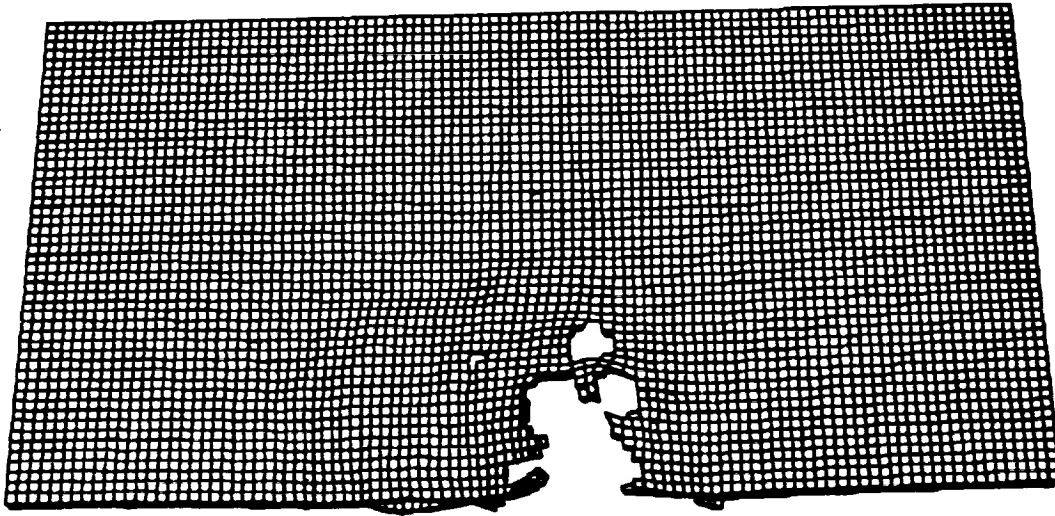
Oblique whipple shield impact (B324)

Figure 5



Debris Cloud Wall Impact Model  
time = 0.49974E+02

B324: front surface

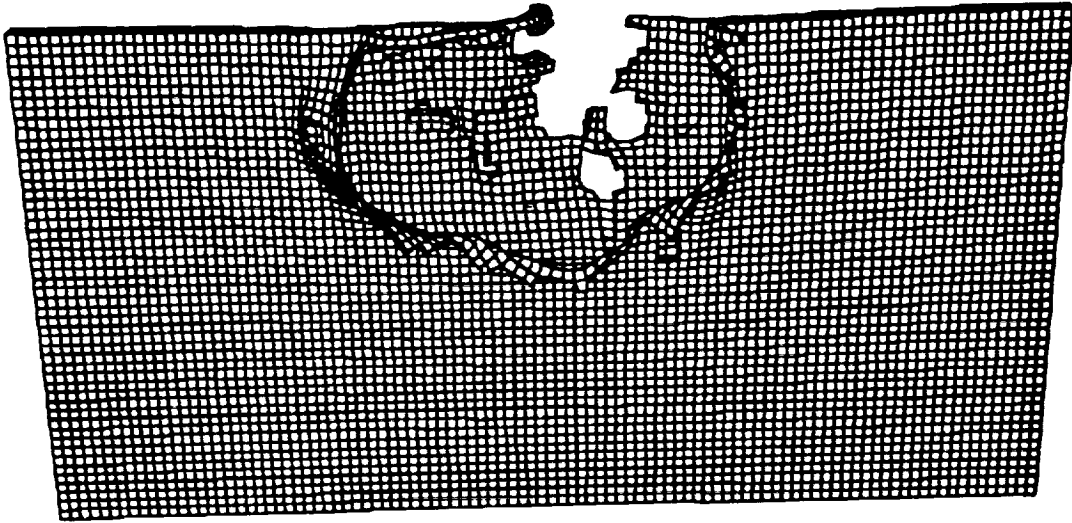


disp. scale factor = 0.100E+01 (default)

Figure 6

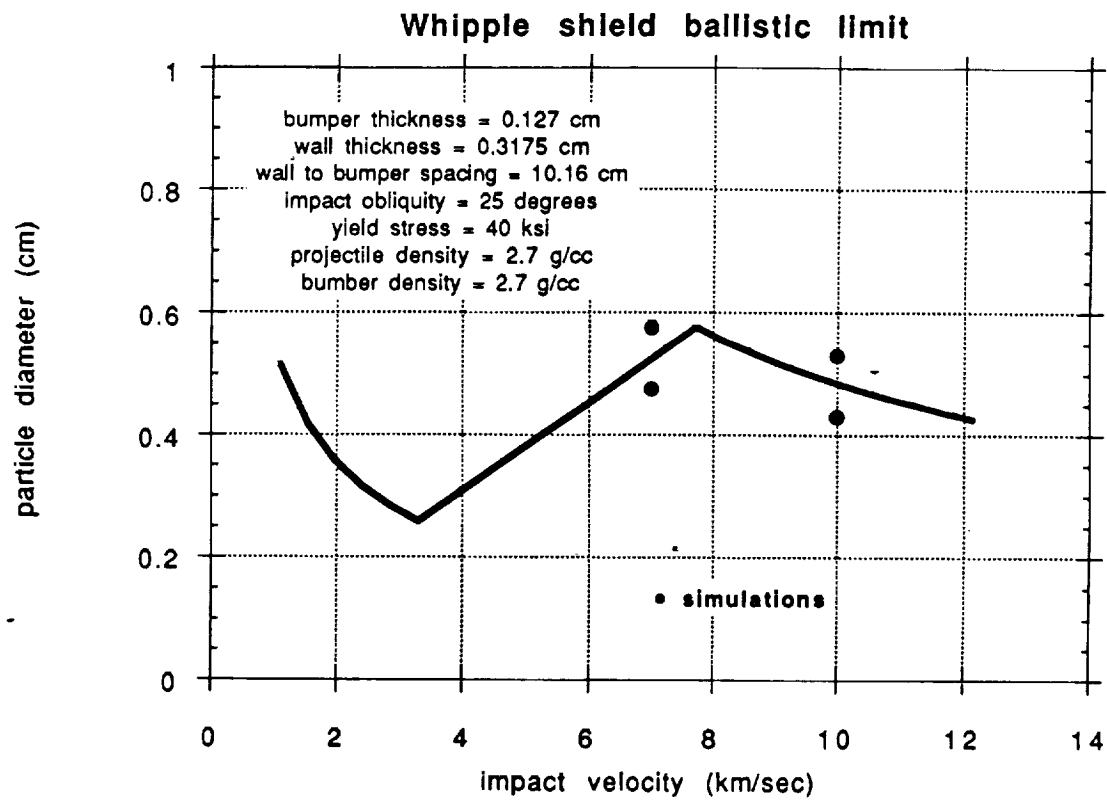
Debris Cloud Wall Impact Model  
time = 0.49974E+02

B324: rear surface



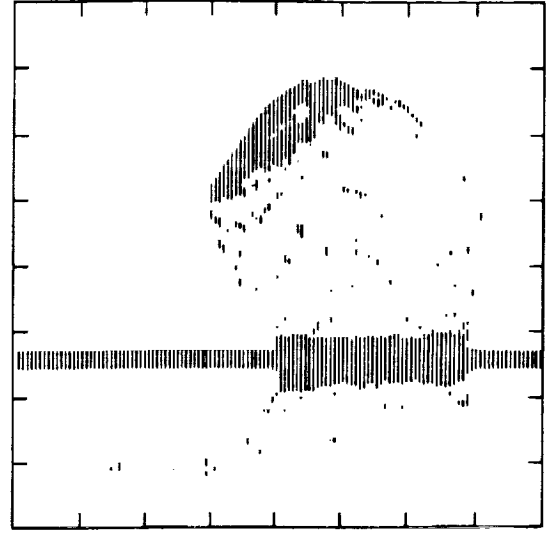
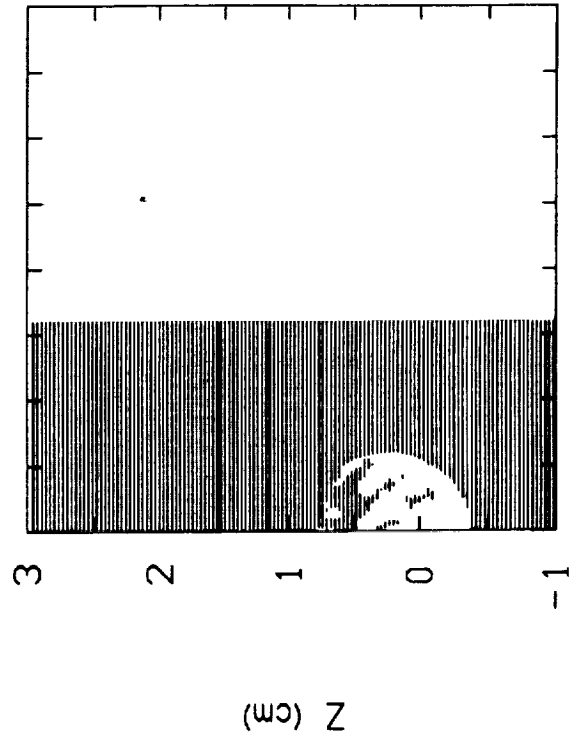
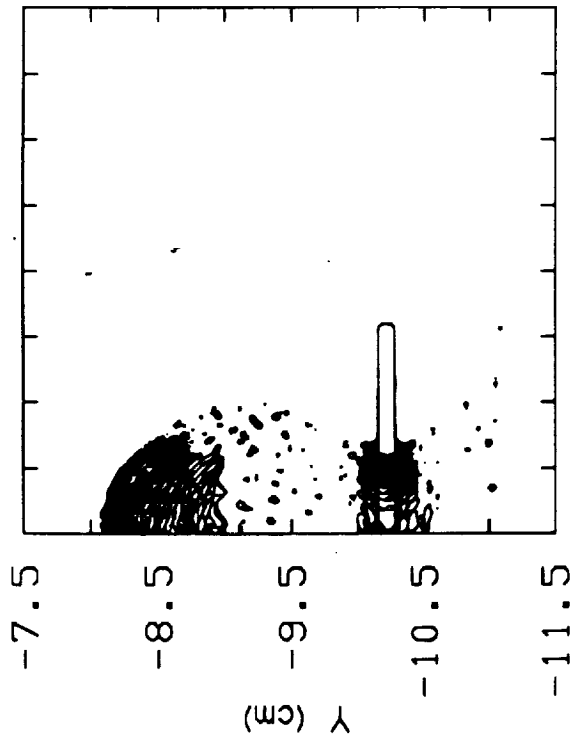
disp. scale factor = 0.100E+01 (default)

Figure 7



Time = 4.0090E-06

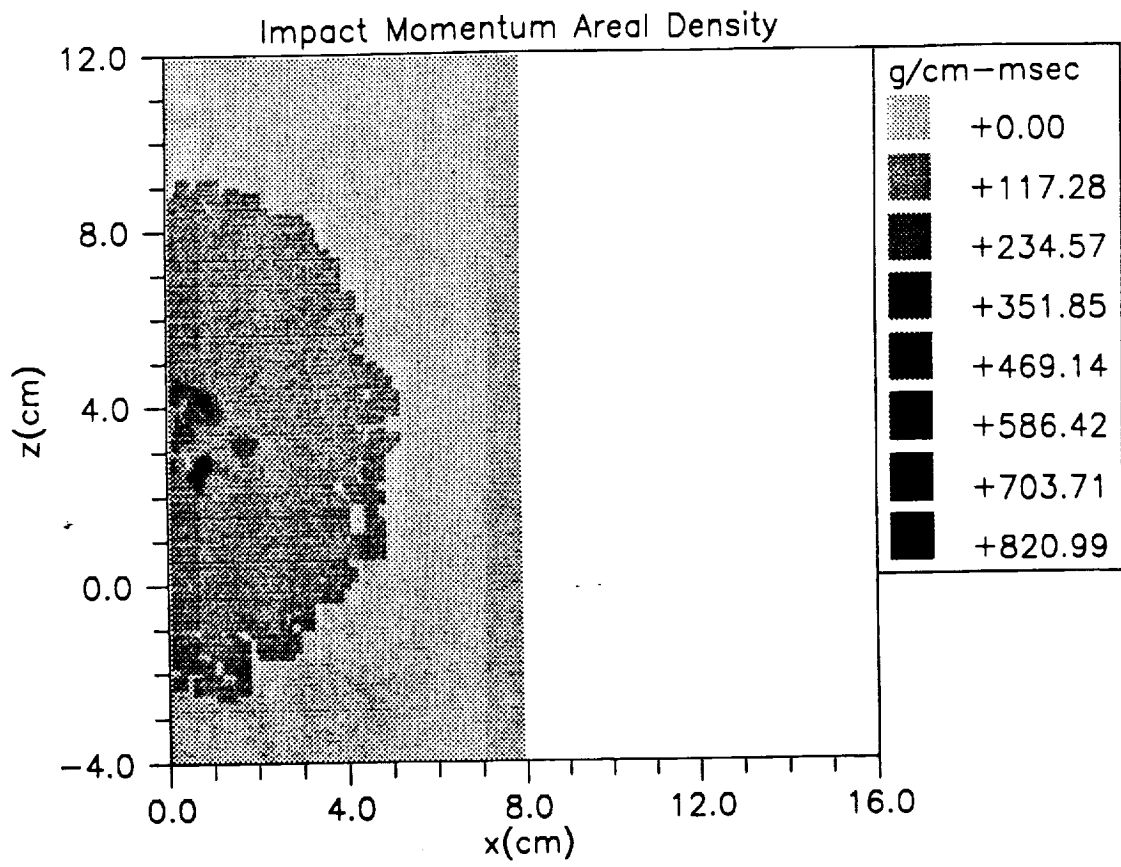
Materials K1SECN  
 — 1 11/28/93  
 20:33:27  
 Block 1



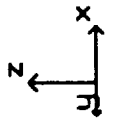
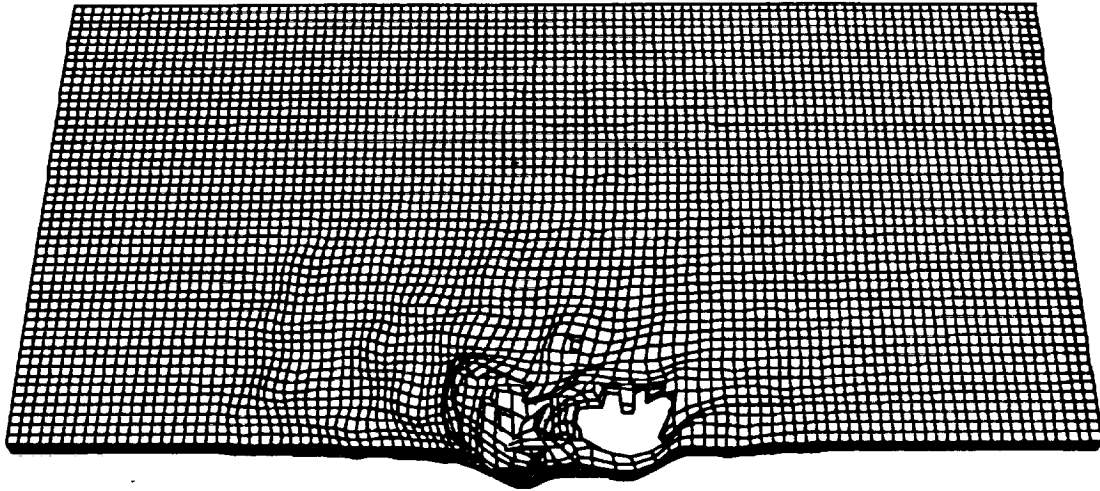
Oblique whipple shield impact (7a)



Figure 10

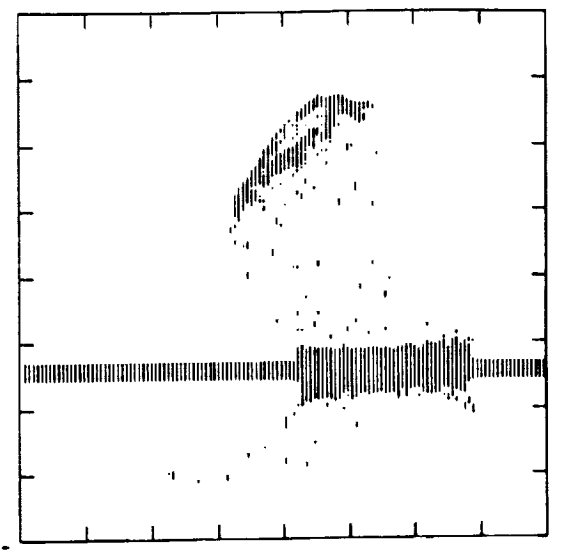
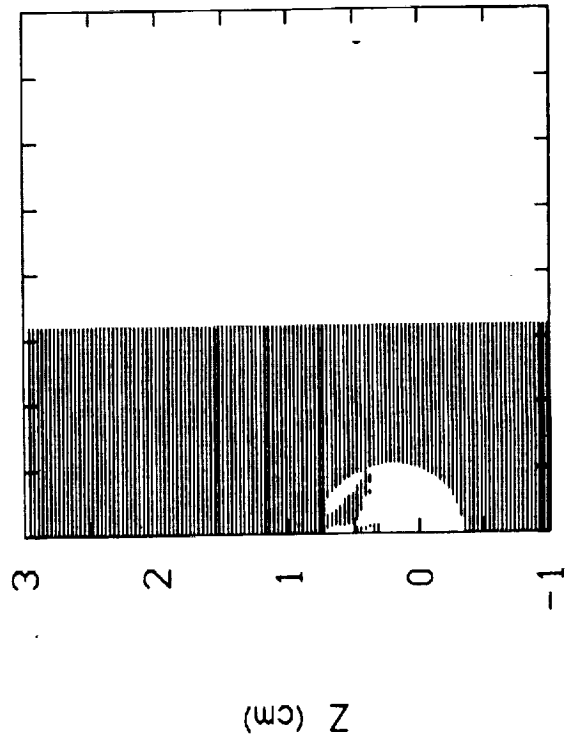
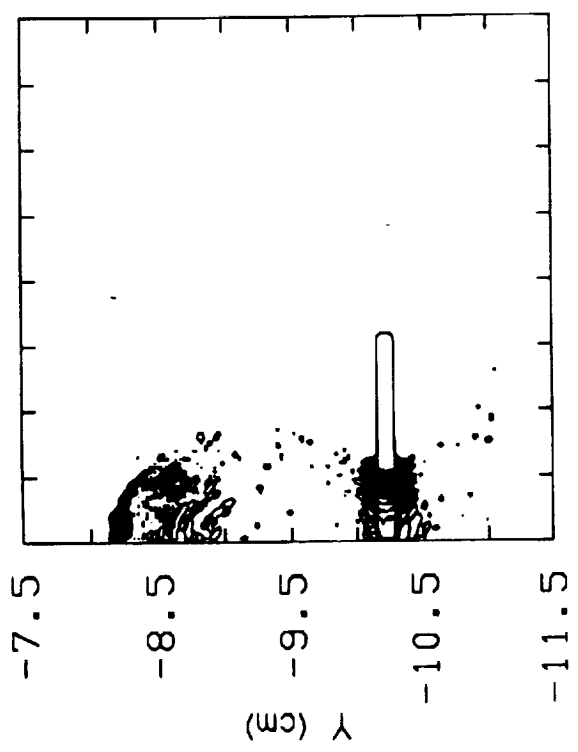


Debris Cloud Wall Impact Model  
time = 0.99799E+01



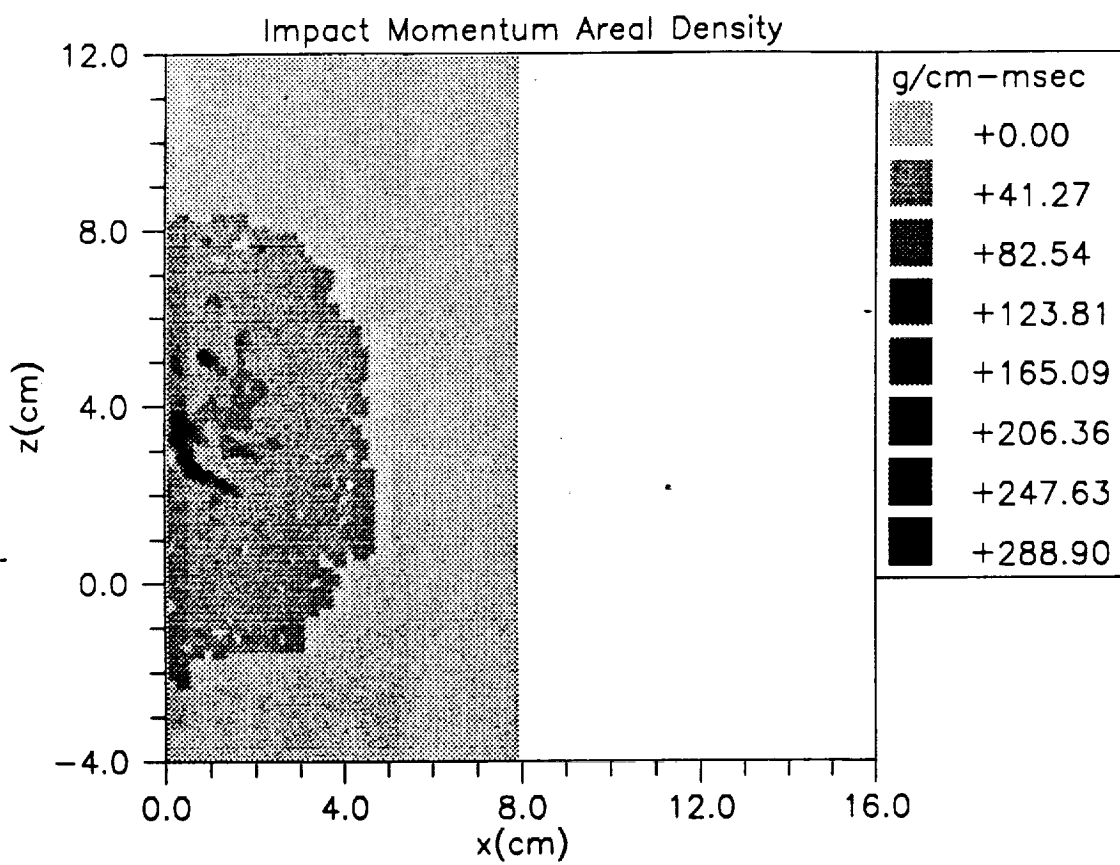
disp. scale factor = 0.100E+01 (default)

Time = 4.0059E-06  
Materials K1QCUH  
— 1 11/28/93  
18:36:31  
Block 1

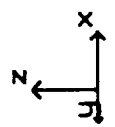
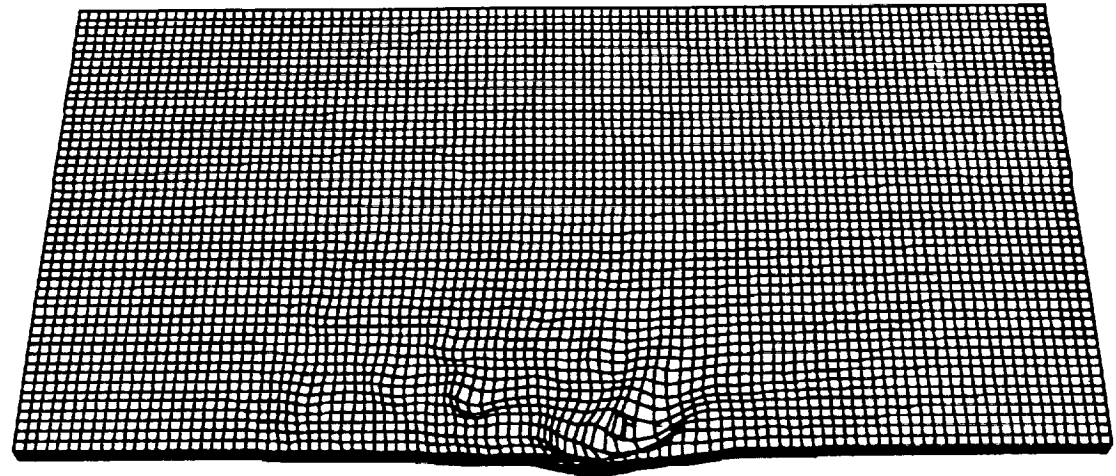


Oblique whipple shield impact (7b)

Figure 13

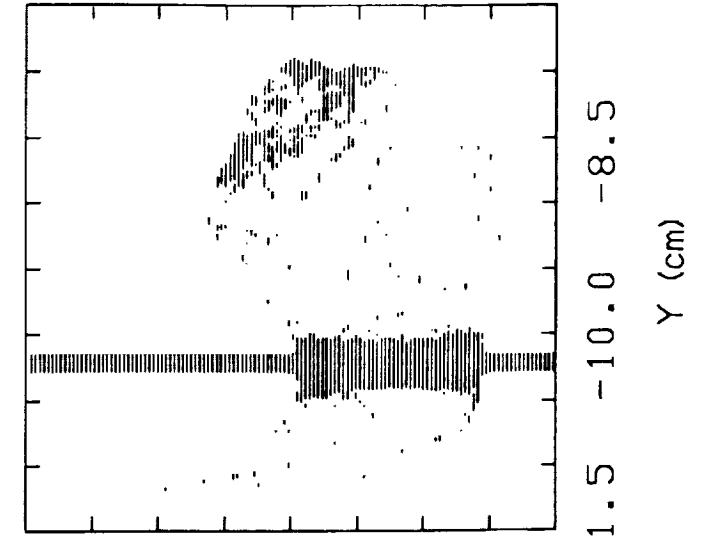
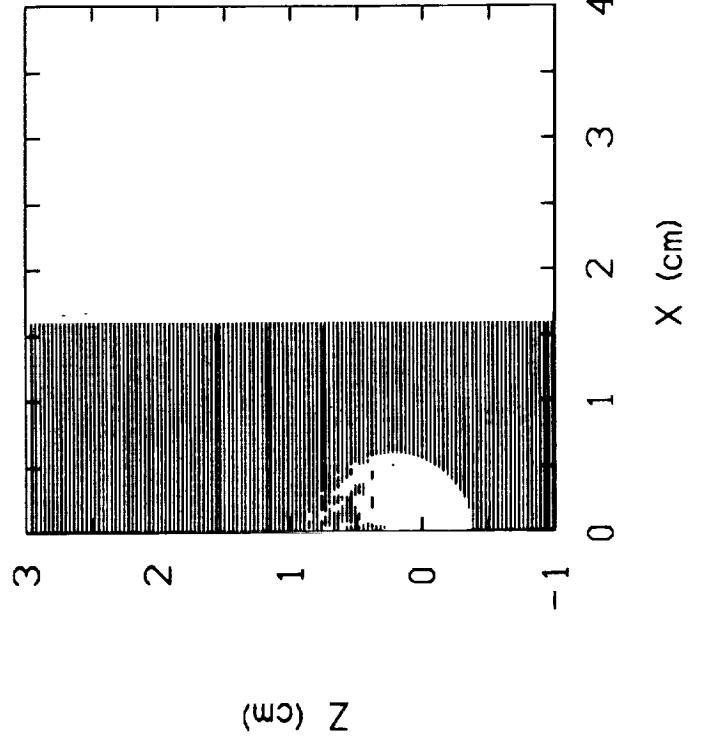
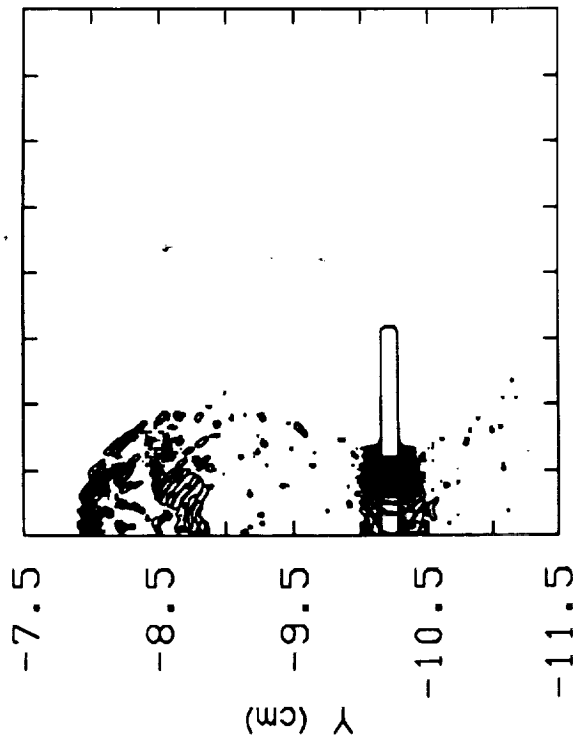


Debris Cloud Wall Impact Model  
time = 0.99984E+01



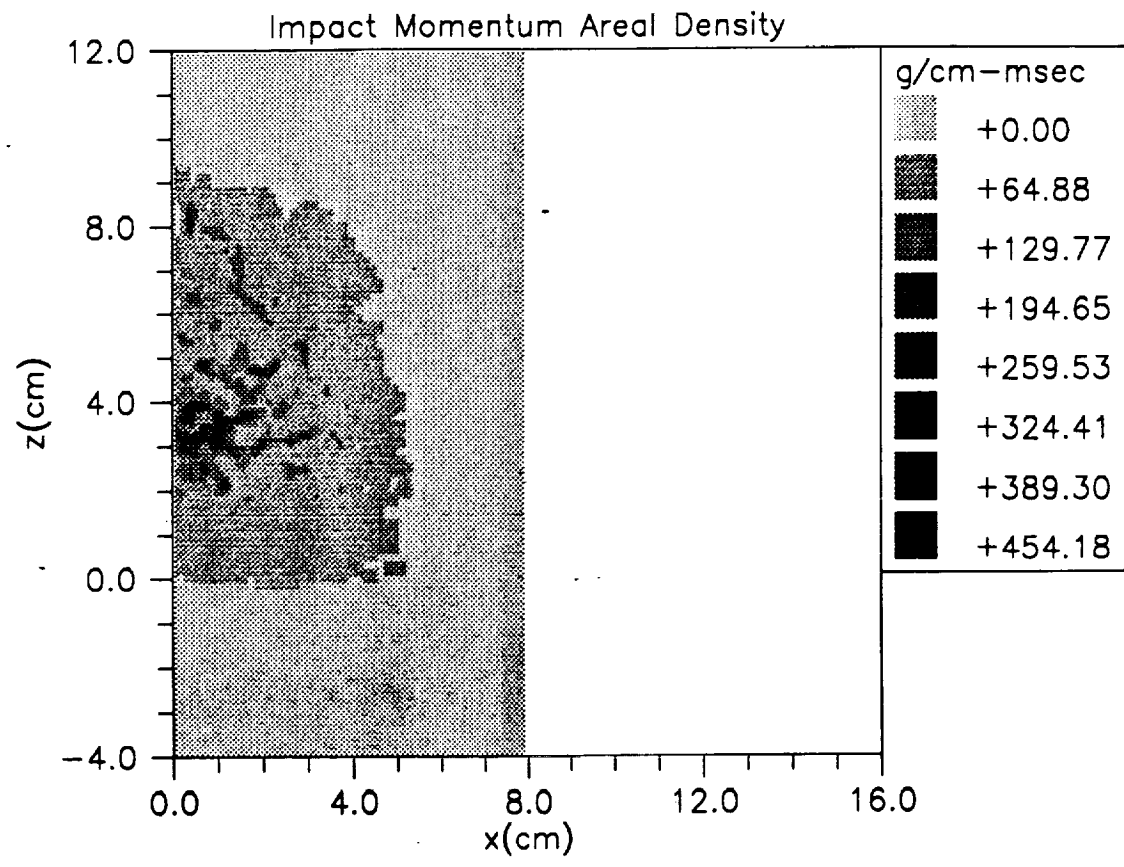
disp. scale factor = 0.100E+01 (default)

Time = 3.0073E-06  
Materials K1WEUG  
— 1 11/29/93  
01:06:27  
Block 1

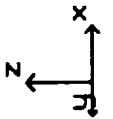
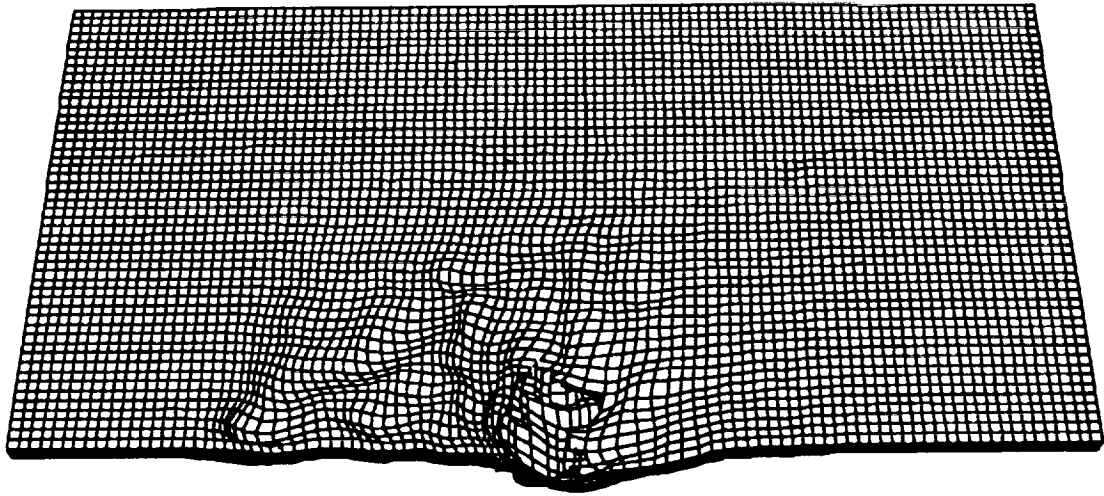


Oblique whipple shield impact (10a)

Figure 16



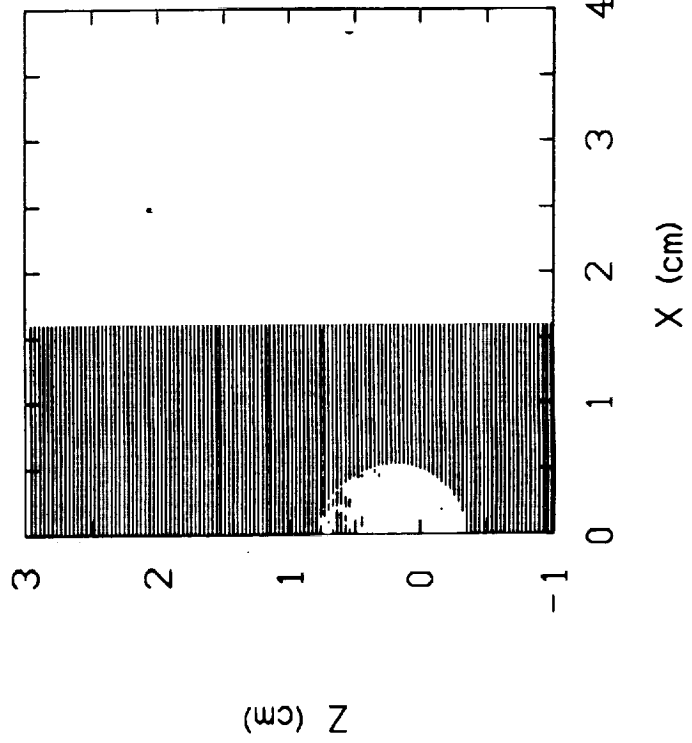
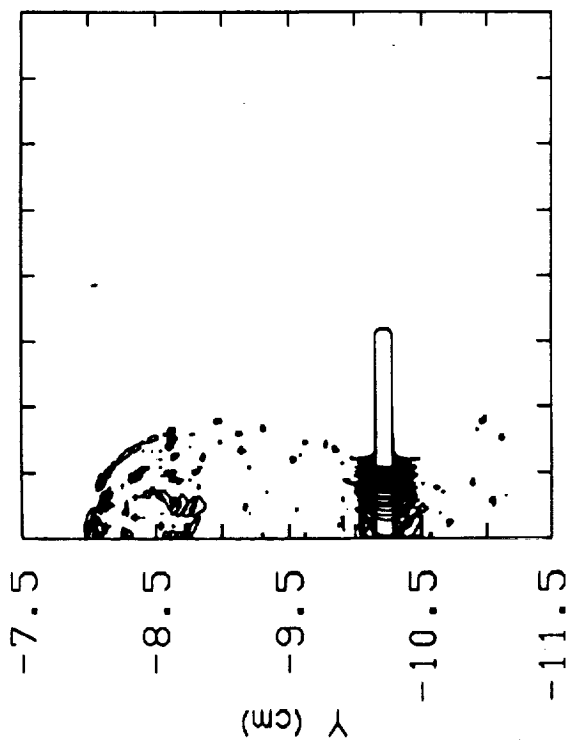
Debris Cloud Wall Impact Model  
time = 0.99761E+01



disp. scale factor = 0.100E+01 (default)

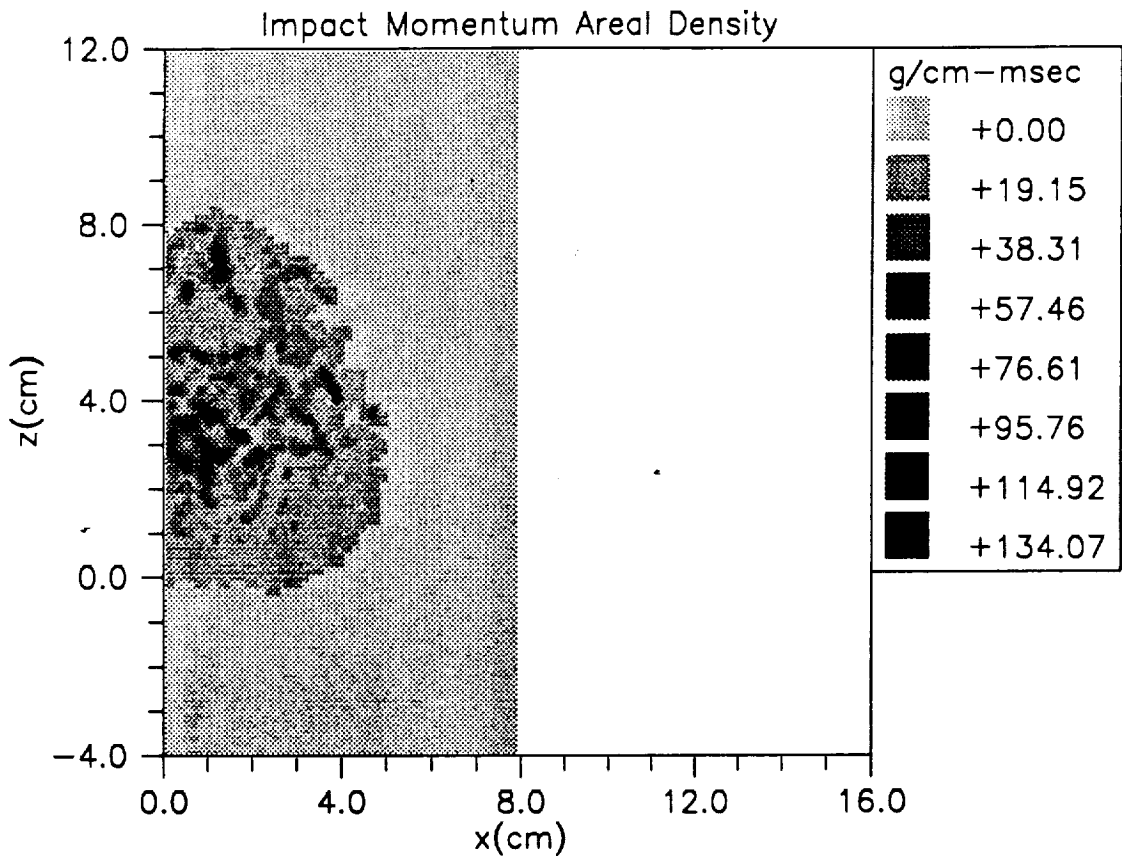


Time = 3.0032E-06  
Materials K1WEUP  
— 1 11/29/93  
00:54:04  
Block 1

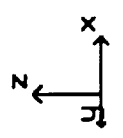
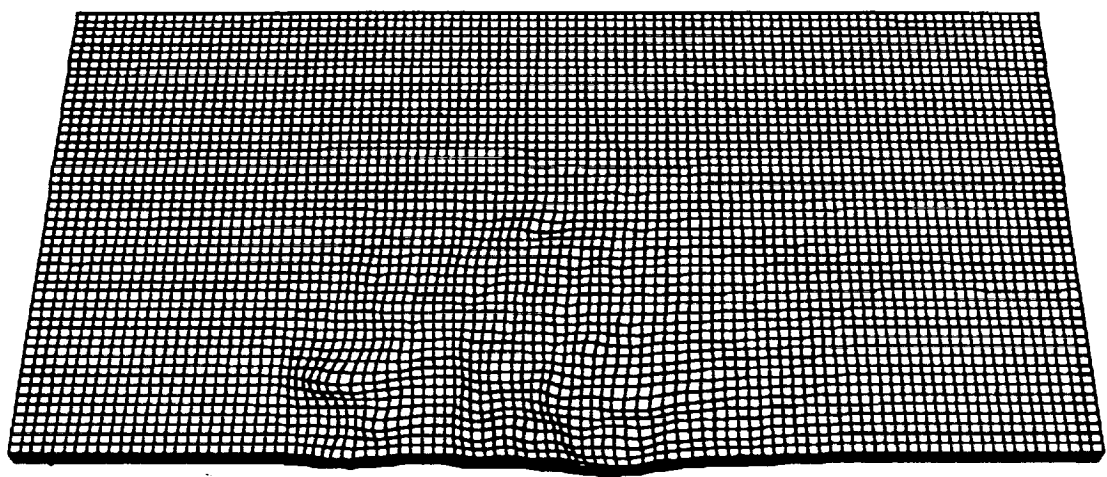


Oblique whipple shield impact (10b)

Figure 19



Debris Cloud Wall Impact Model  
time = 0.99903E+01



disp. scale factor = 0.100E+01 (default)

**APPENDIX A**

**Example Input File (CTH simulation)**

```

*****
*
*eor* cgenin
*
*****
*
*   cthgen input
*
*****
*
*   Title record
*
Oblique whipple shield impact (7a)
*
*****
*
*   control records
*
control
  ep
* rump
endc
*
*****
*
*   edit records
*
edit
  block 1
    expanded
  endb
ende
*
*****
*
*   mesh records
*
mesh
  block 1 geom=3dr type=e
    x0 0.0
      x1 n=50 w=1.5875 rat=1.
    endx
    y0 -11.5
      y1 n=125 w=3.96875 rat=1.
    endy
    z0 -1.000
      z1 n=125 w=3.96875 rat=1.
    endz
    xact = 0.0      1.00
    yact = -11.5   -10.40
    zact = -0.50   1.00
  endb
endm
*
*****
*
*   material insertion records
*

```

```

insertion of material
*
  block 1
*
  package projectile
  material 1
  numsub 49
  velocities xvel 0.0 yvel 6.3441545e5 zvel 2.9583278e5
  insert sphere
  center 0.0 -10.5745 0.0
  r      0.2875
  endi
  endp
*
  package shield
  material 1
  numsub 49
  velocities xvel 0. yvel 0. zvel 0.
  insert box
  x1 0.0 y1 -10.287 z1 -1.00 x2 1.5875 y2 -10.16 z2 2.96875
  endi
  endp
*
  endb
*
endi
*
*****
*
* eos records
*
* eos num 2
eos
  mat1 mgrun eos=6061-t6_al
* mat1 mgrun eos=2024-t4_al
* mat2 mgrun eos=7075-t6_al
*
* aneos1 -1 'Aluminum library' lib=6 type=4 rhug=-1. thug=-1.
*
ende
*
*****
*
* material strength records
*
epdata
* matep 1 jfrac=7
* matep 2 jfrac=8
  matep 1 st=6061-t6_aluminum
* matep 1 st=2024-t4_aluminum
* matep 2 st=7075-t6_aluminum
* matep 1 st=user r0=1.0
* matep 2 st=user r0=1.0
  mix = 5
ende
*
*****
*

```

```
endinput
*
* end of cthgen input
*
*****
*
*eor* cthin
*
*****
*
*   cth input
*
*****
*
*   Title record
*
Oblique whipple shield impact (7a)
*
*****
*
*   control records
*
restart
  nu = 1
endr
*
control
  tst = 1.0e-6
  nsc = 5000
  cpshift = 60.
* mmp
endc
*
convect
  convection = 1
endc
*
*****
*
*   time step records
*
mindt
  time = 0.   dt = 1.e-12
endn
*
maxdt
  time=0.      dt=0.5e-10
  time=3.e-10 dt=1.
endx
*
*****
*
*   tracer records
*
tracer
* add 0.0 -10.528 0.0
* add 0.0 -10.368 0.0
* add 0.0 -10.287 0.0
```

```

* add 0.0 -9.368
* add 0.0 -0.127
* add 0.0 -9.368 to 1.0 -9.368 n 3
* add 0.0 -0.127 to 1.0 -0.127 n 9
endt
*
*****
*
* edit records
*
edit
  shortt
    time=0.    dtf=5.e-6
    time=1.e-5 dtf=1.e-5
    time=1.e-4 dtf=1.e-4
  ends
  longt
    time=0.    dtf=5.e-6
    time=1.e-5 dtf=1.e-5
    time=1.e-4 dtf=1.e-4
  endl
  plott
    time=0.    dtf=0.5e-6
    time=15.0e-6 dtf=1.0e-6
    time=30.0e-6 dtf=2.0e-6
  endp
  histt
    time = 0.  dtf = 1.e-8
*   htracer1
*   htracer2
*   htracer3
*   bxyz 1 0.0 -8.01 0.0
*   bxyz 1 0.2 -8.01 0.0
*   bxyz 1 0.4 -8.01 0.0
*   bxyz 1 0.6 -8.01 0.0
*   bxyz 1 0.8 -8.01 0.0
*   bxyz 1 1.0 -8.01 0.0
  endh
ende
*
*
* boundary condition records
*
boundary
  bhydro
    block 1
      bxb=0 bxt=1 byb=1 byt=1 bzb=1 bzt=1
    endb
  endh
endb
*
* end of cth input
*
*****
*
*eor* hisinp
*
*****

```



```
*
* hisplt input
*
*****
*
bottom=off
plot time cpu          v2=dt          v3=etot
*plot time pressure.1 v2=pressure.2 v3=pressure.3
*plot time yvelocity.1 v2=yvelocity.2 v3=yvelocity.3
*plot time zvelocity.1 v2=zvelocity.2 v3=zvelocity.3
*plot time pressure.4 v2=pressure.5 v3=pressure.6
*plot time pressure.7 v2=pressure.8 v3=pressure.9
*
* end of hisplt input
*
*****
*
*eor* pltinp
*
*****
*
* cthplt input
*
*****
*
units cgsk
bottom=off
*
*color table = 6
*color material = 16 112
*color nmaterial = 31 127
*3dplot
*tcolor = 6
*
*3dline, mat=0
3dortho, mat=0
*
*2dfix x=0.0
*2dplot if tracer dots=density=3.0
-*
* end of cthplt input
*
*****
```

**APPENDIX B**

**Example Input File (CTH simulation restart)**

```
*****
*
*eor* cgenin
*
*****
*
*   cthgen input
*
*****
*
*   Title record
*
Oblique whipple shield impact (7a)
*
*****
*
*   control records
*
control
  ep
* mmp
endc
*
*****
*
*   edit records
*
edit
  block 1
    expanded
  endb
ende
*
*****
*
*   mesh records
*
mesh
  block 1 geom=3dr type=e
    x0 0.0
      x1 n=50 w=1.5875 rat=1.
    endx
    y0 -11.5
      y1 n=125 w=3.96875 rat=1.
    endy
    z0 -1.000
      z1 n=125 w=3.96875 rat=1.
    endz
    xact = 0.0 1.00
    yact = -11.5 -10.40
    zact = -0.50 1.00
  endb
endm
*
*****
*
*   material insertion records
*
```

```

insertion of material
*
  block 1
*
  package projectile
  material 1
  numsub 49
  velocities xvel 0.0 yvel 6.3441545e5 zvel 2.9583278e5
  insert sphere
    center 0.0 -10.5745 0.0
    r      0.2875
  endi
  endp
*
  package shield
  material 1
  numsub 49
  velocities xvel 0. yvel 0. zvel 0.
  insert box
    x1 0.0 y1 -10.287 z1 -1.00 x2 1.5875 y2 -10.16 z2 2.96875
  endi
  endp
*
  endb
*
endi
*
*****
*
* eos records
*
* eos num 2
eos
  mat1 mgrun eos=6061-t6_al
* mat1 mgrun eos=2024-t4_al
* mat2 mgrun eos=7075-t6_al
*
* aneos1 -1 'Aluminum library' lib=6 type=4 rhug=-1. thug=-1.
*
ende
*
*****
*
* material strength records
*
epdata
* matep 1 jfrac=7
* matep 2 jfrac=8
  matep 1 st=6061-t6_aluminum
* matep 1 st=2024-t4_aluminum
* matep 2 st=7075-t6_aluminum
* matep 1 st=user r0=1.0
* matep 2 st=user r0=1.0
  mix = 5
ende
*
*****
*

```

```
endinput
*
* end of cthgen input
*
*****
*
*eor* cthin
*
*****
*
*   cth input
*
*****
*
*   Title record
*
Oblique whipple shield impact (7a)
*
*****
*
*   control records
*
restart
  newfile
  nu = 3
endr
*
control
  tst = 4.0e-6
  nsc = 5000
  cpshift = 60.
* mmp
endc
*
convect
  convection = 1
endc
*
*****
*
*   time step records
*
mindt
  time = 0.  dt = 1.e-12
endn
*
maxdt
  time=0.      dt=0.5e-10
  time=3.e-10 dt=1.
endx
*
*****
*
*   tracer records
*
tracer
* add 0.0 -10.528 0.0
* add 0.0 -10.368 0.0
```

```

* add 0.0 -10.287 0.0
* add 0.0 -9.368
* add 0.0 -0.127
* add 0.0 -9.368 to 1.0 -9.368 n 3
* add 0.0 -0.127 to 1.0 -0.127 n 9
endt
*
*****
*
* edit records
*
edit
  shortt
    time=0.      dtf=5.e-6
    time=1.e-5  dtf=1.e-5
    time=1.e-4  dtf=1.e-4
  ends
  longt
    time=0.      dtf=5.e-6
    time=1.e-5  dtf=1.e-5
    time=1.e-4  dtf=1.e-4
  endl
  plott
    time=0.      dtf=1.5e-6
    time=15.0e-6 dtf=1.0e-6
    time=30.0e-6 dtf=2.0e-6
  endp
  histt
    time = 0.  dtf = 1.e-8
*   htracer1
*   htracer2
*   htracer3
*   bxyz 1 0.0 -8.01 0.0
*   bxyz 1 0.2 -8.01 0.0
*   bxyz 1 0.4 -8.01 0.0
*   bxyz 1 0.6 -8.01 0.0
*   bxyz 1 0.8 -8.01 0.0
*   bxyz 1 1.0 -8.01 0.0
  endh
.ende
*
*
* boundary condition records
*
boundary
  bhydro
    block 1
      bxb=0 bxt=1 byb=1 byt=1 bzb=1 bzt=1
    endb
  endh
endb
*
* end of cth input
*
*****
*
*eor* hisinp
*

```

```
*****
*
* hisplt input
*
*****
*
bottom=off
plot time cpu          v2=dt          v3=etot
*plot time pressure.1 v2=pressure.2 v3=pressure.3
*plot time yvelocity.1 v2=yvelocity.2 v3=yvelocity.3
*plot time zvelocity.1 v2=zvelocity.2 v3=zvelocity.3
*plot time pressure.4 v2=pressure.5 v3=pressure.6
*plot time pressure.7 v2=pressure.8 v3=pressure.9
*
* end of hisplt input
*
*****
*
*eor* pltinp
*
*****
*
* cthplt input
*
*****
*
units cgsk
bottom=off
*
*color table = 6
*color material = 16 112
*color nmaterial = 31 127
*3dplot
*tcolor = 6
*
*3dline, mat=0
3dortho, mat=0
*
*2dfix x=0.0
*2dplot if tracer dots=density=3.0
*
* end of cthplt input
*
*****
```

## APPENDIX C

### Example Input File (DC3D)



```

* dc3d input file
*
*      itype      jtype
*          2          1
*      il          i2
*          2          33
*      j1          j2
*      64          112
*      k1          k2
*      17          80
*
*      xlow      delta x
*          0.0      0.031750
*      ylow      delta y
*      -11.5000      0.031750
*      zlow      delta z
*      -1.0000      0.031750
*      tcut      tmin      dencut
*          25.0      0.0      0.01
*      idmax      jdmax      kdmax      idmaxn      jdmaxn      kdmaxn
*          51          5      101      51          5      101
*      xmin      xmax      xminn      xmaxn
*          0.0      8.00      0.0      4.00
*      ymin      ymax      yminn      ymaxn
*          0.0      0.3175      0.0      0.3175
*      zmin      zmax      zminn      zmaxn
*          -4.00      12.00      2.0      10.0
*      vmu      vlamb      denref      eta
*          0.259      0.503      2.703      1.0e-3
*      zeta      eps      ymxref
*          1.0e-9      1.0e-6      1.0e-6
*      mdfactor
*          1.0

```

**APPENDIX D**

**Example Input File Header (DYNA3D)**

Debris Cloud Wall Impact Model

88 large

```
2      25763      20001
0      0      0      0      0      0      0      0
                                e20.0
0
100.0e-01      -2.e+4      50.e-01      1.0e-18
0
0
0
1      13      2.703
e-p w/failure
0.276 2.900e-03 3.88e-03 1.500e-0 -12.e+33
7.20e-1
```

0 0 1619

```
2      1      1.0
elastic
1.0
0.3
```

**APPENDIX E**

**Plotting Routine Source Code (DCMPLT)**

```
c   program dcmlpt
c
c   dimension x(500),y(500),z(500),
1  zz(500,500),cval(10)
c
c   external grctr,efspplt
c   external grctr,egsgl,efspplt
c
c   open(1,file='dcpost.plt')
c   open(2,file='dc3din')
c   open(9,file='dcmlpt.out')
c
c   do 11 i=1,500
c   x(i)=0.0
c   y(i)=0.0
c   z(i)=0.0
c 11 continue
c
c   scale=1.0e+6
c   scale=1.0e+3
c
c   jmax=1
c   kmax=1
c   zmax=0.0
c
c   do 10 i=1,500000
c   read(1,101,end=98) j,k,xx,yy,pmag
101 format(2i6,3e15.3)
c   x(j)=xx
c   y(k)=yy
c   zz(j,k)=pmag*scale
c   if(zz(j,k).gt.zmax) zmax=zz(j,k)
c   if(j.gt.jmax) jmax=j
c   if(k.gt.kmax) kmax=k
c 10 continue
c
c 98 dummy=1.0
c
c   iunit=0
c   ldzz=500
c   iopt=1+2+4
c   iopt=2+8
c   ncv=8
c
c   cval(1)=1.0e-33
c   cval(2)=zmax
c
c   call grctr(jmax,kmax,x,y,zz,ldzz,iopt,ncv,cval)
c   call egsgl('!contour_plot use$', 'dcmlpt.d1$')
c   call egsgl('.1 use$', 'dcmlpt.d2$')
c   call egsgl('.1 viewport$', 0.1,0.9,0.1,0.9)
c   call efspplt(iunit, ' ')
c
c   stop
c   end
```

**APPENDIX F**

**Post-processor Source Code (DCPOST)**

```

      program dcpst
c
c**** program dcpst
c
      dimension iflg(100000),px(100000),py(100000),pz(100000),
1 jnew(100000)
      dimension xcen(500),zcen(500),emom(500,500)
c
      character*8 ch0,ch1,ch2,ch3,ch4,ch5,ch6,ch7,ch8,ch9
c
      open(1,file='dc3din')
      open(12,file='dc3d.dyn')
      open(61,file='dc3d.mom')
c
      open(13,file='dcbase')
c
      open(21,file='dcpst.out')
      open(22,file='dcpst.plt')
c
c      time=1.0
c      time=0.0
c
c      factor=0.75
c      factor=1.0
c
      read(1,110) itype,jtype
110 format(///2i10)
      read(1,111) i1,i2,j1,j2,k1,k2
111 format(/2i10)
      read(1,112) xlow,deltx,ylow,deltz,zlow,deltz
112 format(/2e15.6)
      read(1,113) tcut
113 format(/e15.3)
      read(1,114) idmax,jdmax,kdmax,idmaxn,jdmaxn,kdmaxn
114 format(/6i10)
      read(1,115) xdmn,xdmax,xdmnn,xdmaxn,
1 ydmn,ydmax,ydmnn,ydmaxn,
2 zdmn,zdmax,zdmnn,zdmaxn
115 format(/4e15.3)
      read(1,116) factor
116 format(/////e15.3)
c
      ncnt=idmax*jdmax*kdmax+(idmax-1)*(jdmax-1)*(kdmax-1)+
1      8+1+5
c
      if(jtype.ne.1) go to 777
      if(jtype.eq.0) go to 777
c
      do 14 i=1,ncnt
      read(12,202) ch0,ch1,ch2,ch3,ch4,ch5,ch6,ch7,ch8,ch9
202 format(10a8)
c
      if(jtype.eq.3) go to 14
c
      write(21,203) ch0,ch1,ch2,ch3,ch4,ch5,ch6,ch7,ch8,ch9
203 format(10a8)
      14 continue
c
      777 dummy=1.0

```

```

c
do 10 j=1,100000
  iflg(j)=0
  px(j)=0.0
  py(j)=0.0
  pz(j)=0.0
10 continue
c
do 11 i=1,500000
c
read(12,102,end=75) j,dpx,dpy,dpz
read(61,102,end=75) j,dpx,dpy,dpz
102 format(i8,3e10.3)
  iflg(j)=1
  px(j)=px(j)+dpx*factor
  py(j)=py(j)+dpy*factor
  pz(j)=pz(j)+dpz*factor
11 continue
c
75 dummy=1.0
c
ridmax=idmax
rkdmax=kdmax
deldx=(xmax-xmin)/(ridmax-1.0)
deldz=(zmax-zmin)/(rkdmax-1.0)
ridmaxn=idmaxn
rkdmaxn=kdmaxn
deldxn=(xmaxn-xminn)/(ridmaxn-1.0)
deldzn=(zmaxn-zminn)/(rkdmaxn-1.0)
c
do 710 k=1,kdmax-1
do 711 i=1,idmax-1
  rk=k
  ri=i
  zcen(k)=zmin+deldz/2.0+(rk-1.0)*deldz
  xcen(i)=xmin+deldx/2.0+(ri-1.0)*deldx
  emom(i,k)=0.0
c
  jelem=i+(idmax-1)*(k-1)
  jenew(jelem)=0
  if(xcen(i).lt.xminn) go to 711
  if(xcen(i).gt.xmaxn) go to 711
  if(zcen(k).lt.zminn) go to 711
  if(zcen(k).gt.zmaxn) go to 711
  inew=int((xcen(i)-xminn)/deldxn)+1
  knew=int((zcen(k)-zminn)/deldzn)+1
  jenew(jelem)=inew+(idmaxn-1)*(knew-1)
c
711 continue
710 continue
c
do 12 j=1,100000
c
jout=j
if(jtype.eq.3) jout=jenew(j)
if(jout.eq.0) go to 12
c
if(iflg(j).eq.0) go to 12
write(21,201) jout,px(j),py(j),pz(j),time

```



```
201 format (i8,4e10.3)
c
  if(jtype.eq.3) go to 12
c
  iel=mod(j,idmax-1)
  kel=j/(idmax-1)+1
  pmag=(px(j)**2+py(j)**2+pz(j)**2)**0.5
  emom(iel,kel)=pmag/(deldx*deldz)
c  emom(iel,kel)=pmag
c  riel=iel
c  rkel=kel
c  xi=xdmin+deldx+(riel-1.0)*deldx
c  zi=zdmin+deldz+(rkel-1.0)*deldz
c  write(22,212) iel,kel,xi,zi,pmag,time
c 212 format (2i6,4e15.3)
c
  12 continue
c
  if(jtype.eq.3) go to 99
c
  do 721 k=1,kdmax-1
  do 722 i=1,idmax-1
  write(22,213) i,k,xcen(i),zcen(k),emom(i,k)
213 format (2i6,3e15.5)
722 continue
721 continue
c
  99 dummy=2.0
c
  stop
  end
```

**APPENDIX G**

**Analysis Source Code (DC3D)**

```

      program dc3d
c
c**** program dc3d
c
      common/atype/itype, jtype
      common/mesh/i1, i2, j1, j2, k1, k2, deltx, delty, deltz,
1 xlow, ylow, zlow
      common/walldat/ywall, tcut, tmin, dencut,
1 idmax, jdmax, kdmax, xmin, xmax, ymin, ymax, zmin, zmax
      common/walnew/idmaxn, jdmaxn, kdmaxn,
1 xminn, xmaxn, yminn, ymaxn, zminn, zmaxn
      common/props/den, denref, rmass, vmu, vlamb, eta, zeta, phi, rj(3, 3)
      common/intpar/epsint, ymxref
c
      open(1, file='dc3din')
c
      open(7, file='pltdat/dc3d.plt1')
      open(8, file='pltdat/dc3d.plt2')
      open(4, file='dc3d.cth')
      open(9, file='dc3d.dyn')
c
      open(61, file='dc3d.mom')
c
      open(10, file='dc3d.dbg')
c
      read(1, 110) itype, jtype
110 format(///2i10)
      read(1, 111) i1, i2, j1, j2, k1, k2
111 format(/2i10)
      read(1, 112) xlow, deltx, ylow, delty, zlow, deltz
112 format(/2e15.6)
      read(1, 113) tcut, tmin, dencut
113 format(/3e15.3)
      read(1, 114) idmax, jdmax, kdmax, idmaxn, jdmaxn, kdmaxn
114 format(/6i10)
      read(1, 115)  xmin, xmax, xminn, xmaxn,
1             ymin, ymax, yminn, ymaxn,
2             zmin, zmax, zminn, zmaxn
115 format(/4e15.3)
      read(1, 116) vmu, vlamb, denref, eta
116 format(/4e15.3)
      read(1, 117) zeta, epsint, ymxref
117 format(/3e15.3)
c
      ywall=ydmin
c
c      call rdavs
c
c      if(itype.eq.2) call dyngen
      if(itype.eq.2.and.jtype.eq.1) call dyngen
      if(itype.eq.2.and.jtype.eq.2) call dyngen
      if(itype.eq.2.and.jtype.eq.3) call dyngen
      if(jtype.eq.2) go to 99
      if(jtype.eq.3) go to 99
c
      call rdavs
c
      ifst=2

```

```

        jfst=2
        kfst=2
c
c        ilast=2
c        jlast=2
c        klast=2
c
        ilast=i2-i1
        jlast=j2-j1
        klast=k2-k1
c
        lfst=1
        llast=5
c
        do 10 i=ifst,ilast
        do 11 j=jfst,jlast
        do 12 k=kfst,klast
        do 13 l=lfst,llast
        call dcelem(i,j,k,l)
13 continue
12 continue
11 continue
10 continue
c
99 dummy=1.0
c
        stop
        end
c
        subroutine dyngen
c
c**** subroutine dyngen
c
        common/atype/itype,jtype
        common/walnew/idmaxn,jdmaxn,kdmaxn,
1 xdminn,xdmaxn,ydminn,ydmaxn,zdminn,zdmaxn
        common/walnat/ywall,tcut,tmin,dencut,
1 idmax,jdmax,kdmax,xdmin,xdmax,ydmin,ydmax,zdmin,zdmax
c
        dimension x(8),y(8),z(8),xn(501),yn(501),zn(501)
c
        if(jtype.ne.3) go to 88
        idmax=idmaxn
        jdmax=jdmaxn
        kdmax=kdmaxn
        xdmin=xdminn
        ydmin=ydminn
        zdmin=zdminn
        xdmax=xdmaxn
        ydmax=ydmaxn
        zdmax=zdmaxn
88 dummy=1.0
c
        ridmax=idmax
        delx=(xdmax-xdmin)/(ridmax-1.0)
        rjdmax=jdmax
        dely=(ydmax-ydmin)/(rjdmax-1.0)
        rkdmax=kdmax

```

```

delz=(zdmax-zdmin)/(rkdmax-1.0)
c
do 10 i=1,idmax
  ri=i
  xn(i)=(ri-1.0)*delx
10 continue
c
do 11 j=1,jdmax
  rj=j
  yn(j)=(rj-1.0)*dely
11 continue
c
do 12 k=1,kdmax
  rk=k
  zn(k)=(rk-1.0)*delz
12 continue
c
define the nodes
c
c
c
c
nconst=0
c
do 20 j=1,jdmax
do 21 k=1,kdmax
do 22 i=1,idmax
c
nconst=0
if(i.eq.1)      nconst=1
c
go to 761
c
if(i.eq.idmax) nconst=4
if(k.eq.1)     nconst=5
if(k.eq.kdmax) nconst=5
if(i.eq.1.and.k.eq.1)      nconst=7
if(i.eq.1.and.k.eq.kdmax) nconst=7
if(i.eq.idmax.and.k.eq.1)  nconst=7
if(i.eq.idmax.and.k.eq.kdmax) nconst=7
c
761 dummy=1.0
c
nnode=i+idmax*(k-1)+idmax*kdmax*(j-1)
write(9,101) nnode,nconst,xn(i),yn(j),zn(k)
c 101 format (i5,i5,3e20.8)
101 format (i8,i5,3e20.8)
22 continue
21 continue
20 continue
c
nconst=0
c
x(1)=xdmin
y(1)=ydmin-1.0
z(1)=zdmin
x(2)=xdmin+1.0
y(2)=ydmin-1.0
z(2)=zdmin
x(3)=xdmin+1.0
y(3)=ydmin-1.0

```

```

z(3)=zdmin+1.0
x(4)=xdmin
y(4)=ydmin-1.0
z(4)=zdmin+1.0
x(5)=xdmin
y(5)=ydmin-2.0
z(5)=zdmin
x(6)=xdmin+1.0
y(6)=ydmin-2.0
z(6)=zdmin
x(7)=xdmin+1.0
y(7)=ydmin-2.0
z(7)=zdmin+1.0
x(8)=xdmin
y(8)=ydmin-2.0
z(8)=zdmin+1.0
c
do 40 l=1,8
nnode=idmax+idmax*(kdmax-1)+idmax*kdmax*(jdmax-1)+1
write(9,103) nnode,nconst,x(l),y(l),z(l)
c 103 format(i5,i5,3e20.8)
103 format(i8,i5,3e20.8)
40 continue
c
c define the elements
c
nmat=1
ngen=0
c
do 30 j=1,jdmax-1
do 31 k=1,kdmax-1
do 32 i=1,idmax-1
nelem=i+(idmax-1)*(k-1)+(idmax-1)*(kdmax-1)*(j-1)
n1=i+idmax*(k-1)+idmax*kdmax*(j-1)
n2=n1+1
n3=n2+idmax
n4=n3-1
n5=n1+idmax*kdmax
n6=n5+1
n7=n6+idmax
n8=n7-1
c write(9,102) nelem,nmat,ngen,n5,n6,n7,n8,n1,n2,n3,n4
c 102 format(11i5)
write(9,102) nelem,nmat,n5,n6,n7,n8,n1,n2,n3,n4
102 format(i8,i5,8i8)
32 continue
31 continue
30 continue
c
nmat=2
c
nelem=idmax-1+(idmax-1)*(kdmax-1-1)+
1 (idmax-1)*(kdmax-1)*(jdmax-1-1)+1
n1=idmax+idmax*(kdmax-1)+idmax*kdmax*(jdmax-1)+1
n2=n1+1
n3=n1+2
n4=n1+3
n5=n1+4

```

```

        n6=n1+5
        n7=n1+6
        n8=n1+7
c       write(9,104) nelelem,nmat,ngene,n1,n2,n3,n4,n5,n6,n7,n8
c 104 format(11i5)
        write(9,104) nelelem,nmat,n1,n2,n3,n4,n5,n6,n7,n8
104 format(i8,i5,8i8)
c
c       write(9,110)
c 110 format('      1      1      11',/, '      1      0',/, '      1')
c       idmp1=idmax+1
c       idmp2=idmax+2
c       write(9,111) idmp2,idmp1,n4,n3,n2,n1
c 111 format('      1      0      1      2',2i5,
c      1      /, '      1      0',4i5)
c
c       write(9,110)
110 format('      1      1      11',/, '      1      0',/, '      1')
c       idmp1=idmax+1
c       idmp2=idmax+2
c       write(9,111) idmp2,idmp1,n4,n3,n2,n1
111 format('      1      1      2',2i8,
c      1      /, '      1',4i8)
c
c       return
c       end
c
c       subroutine rdavs
c
c**** subroutine rdavs
c
c       common/mesh/i1,i2,j1,j2,k1,k2,deltx,dely,deltz,
c      1 xlow,ylow,zlow
c
c       common/cthdath/ velx(75,75,75),vely(75,75,75),
c      1 velz(75,75,75),pres(75,75,75),temp(75,75,75),
c      2 gama(75,75,75),spen(75,75,75),vmas(75,75,75),
c      3 vphi(75,75,75),cspd(75,75,75)
c
c       common/cthxyz/xcth(100),ycth(100),zcth(100)
c
c       common/velling/vfx(75,75,75),vfy(75,75,75),vfx(75,75,75)
c
c       character*1 chdum
c
c       open(2,file='avsout')
c       open(3,file='avschk')
c
c       calculate the nodal coordinates
c
c       do 20 i=i1,i2
c         vi=i
c         xcth(i-i1+1)=xlow+(vi-1.0)*deltx-deltx
20 continue
c
c       do 21 j=j1,j2
c         vj=j
c         ycth(j-j1+1)=ylow+(vj-1.0)*dely-dely

```

```

21 continue
c
  do 22 k=k1,k2
    vk=k
    zcth(k-k1+1)=zlow+(vk-1.0)*deltz-deltz
22 continue
c
  read in the mesh data
c
  do 400 idum=1,27
    read(2,901) chdum
901 format(a1)
400 continue
c
  do 10 k=1,k2-k1+1
    do 11 j=1,j2-j1+1
      do 12 i=1,i2-i1+1
        read(2,902) velx(i,j,k),vely(i,j,k),velz(i,j,k),
1 pres(i,j,k),temp(i,j,k),gama(i,j,k),spen(i,j,k)
        read(2,902) vmas(i,j,k),vphi(i,j,k),
1 cspd(i,j,k)
c
  unit conversion factors
c
  velx(i,j,k)=velx(i,j,k)/1.0e+6
  vely(i,j,k)=vely(i,j,k)/1.0e+6
  velz(i,j,k)=velz(i,j,k)/1.0e+6
  pres(i,j,k)=pres(i,j,k)/1.0e+12
c
902 format(7e11.3)
12 continue
11 continue
10 continue
c
  do 30 k=1,k2-k1+1
    do 31 j=1,j2-j1+1
      do 32 i=1,i2-i1+1
c
        write(3,903) velx(i,j,k),vely(i,j,k),velz(i,j,k),
c 1 pres(i,j,k),temp(i,j,k),gama(i,j,k),spen(i,j,k)
c
        write(3,903) vmas(i,j,k),vphi(i,j,k),cspd(i,j,k),
c 1 xcth(i),ycth(j),zcth(k)
c 903 format(7e11.3)
32 continue
31 continue
30 continue
c
  calculate the nodal velocities
c
  do 40 k=2,k2-k1+1
    do 41 j=2,j2-j1+1
      do 42 i=2,i2-i1+1
        wta=vmas(i,j,k-1)
        wtb=vmas(i,j-1,k-1)
        wtc=vmas(i,j-1,k)
        wtd=vmas(i,j,k)
        va=velx(i,j,k-1)
        vb=velx(i,j-1,k-1)
        vc=velx(i,j-1,k)

```



```

      vd=velx(i,j,k)
      if(wta+wtb+wtc+wtd.gt.0.0) then
        vfx(i,j,k)=(wta*va+wtb*vb+wtc*vc+wtd*vd)/
1          (wta+wtb+wtc+wtd)
      else
        vfx(i,j,k)=0.0
      endif
c
c   write(10,910) wta,wtb,wtc,wtd,va,vb,vc,vd
c 910 format(8e10.2)
c
      wta=vmas(i-1,j,k-1)
      wtb=vmas(i,j,k-1)
      wtc=vmas(i,j,k)
      wtd=vmas(i-1,j,k)
      va=vely(i-1,j,k-1)
      vb=vely(i,j,k-1)
      vc=vely(i,j,k)
      vd=vely(i-1,j,k)
      if(wta+wtb+wtc+wtd.gt.0.0) then
        vfy(i,j,k)=(wta*va+wtb*vb+wtc*vc+wtd*vd)/
1          (wta+wtb+wtc+wtd)
      else
        vfy(i,j,k)=0.0
      endif
c
c   write(10,911) wta,wtb,wtc,wtd,va,vb,vc,vd
c 911 format(8e10.2)
c
      wta=vmas(i,j,k)
      wtb=vmas(i,j-1,k)
      wtc=vmas(i-1,j-1,k)
      wtd=vmas(i-1,j,k)
      va=velz(i,j,k)
      vb=velz(i,j-1,k)
      vc=velz(i-1,j-1,k)
      vd=velz(i-1,j,k)
      if(wta+wtb+wtc+wtd.gt.0.0) then
        vfx(i,j,k)=(wta*va+wtb*vb+wtc*vc+wtd*vd)/
1          (wta+wtb+wtc+wtd)
      else
        vfx(i,j,k)=0.0
      endif
c
c   write(10,912) wta,wtb,wtc,wtd,va,vb,vc,vd
c 912 format(8e10.2)
c
      42 continue
      41 continue
      40 continue
c
      return
      end
c
      subroutine dcelem(ii,jj,kk,ll)
c
c**** subroutine dcelem
c

```

```

common/atype/itype, jtype
common/walldat/ywall, tcut, tmin, dencut,
1 idmax, jdmax, kdmax, xmin, xmax, ymin, ymax, zmin, zmax
common/props/den, denref, rmass, vmu, vlamb, eta, zeta, phi, rj(3,3)
common/ndata/x1(3), x2(3), x3(3), x4(3),
1          v1(3), v2(3), v3(3), v4(3), xc(3)
c
c   dimension h(3,3), f(3,3), e(3,3), ep(3,3), p(3),
1 y(33), yt(33,101)
c   dimension param(50), time(101)
c
c   external fcn
c
c   call eldata(ii, jj, kk, ll)
c
c   rden=den/denref
c   if(rden.gt.1000.0) go to 99
c   if(rden.lt.0.01) go to 99
c   if(phi.gt.0.999) go to 99
c
c   denblk=(1.-phi)*den/denref
c   if(denblk.lt.0.01) go to 99
c   if(denblk.lt.dencut) go to 99
c
c   call nddata(ii, jj, kk, ll)
c
c   call jcalc(den, x1, x2, x3, x4, xc, rj)
c   call jcalc(x1, x2, x3, x4, xc, rj)
c
c   call initlz(h, f, ep, p)
c
c   write(10,558) rmass
c 558 format(/, 'inertia tensor ( mass = ', e11.3, ' )', /)
c
c   do 555 io=1,3
c   do 556 jo=1,3
c   write(10,557) rj(io,jo)
c 557 format(e20.8)
c   556 continue
c 555 continue
c
c   set the state vector
c
c   do 10 i=1,3
c   do 11 j=1,3
c   y(3*(i-1)+j) = h(i,j)
c   y(3*(i-1)+j+9) = f(i,j)
c   y(3*(i-1)+j+18) = ep(i,j)
c   write(10,1000) h(i,j), f(i,j), ep(i,j)
c1000 format(3e15.4)
c   11 continue
c   10 continue
c
c   do 12 i=1,3
c   y(i+27)= p(i)
c   y(i+30)=xc(i)
c   write(10,1001) p(i), xc(i)
c1001 format(2e15.4)

```

```

12 continue
c
c   set up and call the integration routine
c
c   ido=1
c   neq=33
c   tol=1.0e-6
c
c   do 20 i=1,50
c   param(i)=0.0
20 continue
c
c   param(1)=1.0e-6
c   param(3)=1.0e-3
c   param(4)=100000
c   param(9)=1.0e-1
c   param(10)=3
c   param(12)=2
c
c   do 32 i=1,neq
c   yt(i,1)=y(i)
32 continue
c
c   iend=2
c   iend=1
c   riend=iend
c
c   tarr=1.0e+33
c   vceny=p(2)/rmass
c   avceny=abs(vceny)
c   if(avceny.gt.0.0)
1 tarr=abs((ywall-y(32))/vceny)
c   if(itype.eq.2.and.tarr.gt.tcut) go to 99
c   if(itype.eq.2.and.tarr.lt.tmin) go to 99
c   if(tarr.gt.tcut) go to 99
c   if(tarr.ge.tcut) go to 99
c   if(tarr.lt.tmin) go to 99
c
c   if(ii.ne.3) go to 99
c   if(jj.ne.38) go to 99
c   if(kk.ne.44) go to 99
c
c   delt=tarr/riend
c   if(itype.eq.2) delt=tarr/riend
c   if(itype.eq.1) delt=0.2
c
c   t=0.0
c   time(1)=0.0
c
c   do 30 i=1,iend
c
c   ri=i
c   t=(ri-1.0)*delt
c   tend=t+delt
c
c   call ivprk(ido,neq,fcn,t,tend,tol,param,y)
c   call ivpbs(ido,neq,fcn,t,tend,tol,param,y)
c   call ivpag(ido,neq,fcn,fcnj,aaa,t,tend,tol,param,y)

```

```

c
c   call ifdcrk(ido,neq,t,tend,tol,param,y)
c   call ivdcrk(ido,neq,t,tend,tol,param,y)
c
c   write(10,101) tarr,t,tend,y(32)
c 101 format(5e15.3)
c
c   do 31 j=1,neq
c     yt(j,i+1)=y(j)
c 31 continue
c
c     t=tend
c     time(i+1)=tend
c
c 30 continue
c
c   write cth input data
c
c     if(itype.eq.1)
c 1 call cthout(ii,jj,kk,ll,y)
c     if(itype.eq.2)
c 1 call dynout(ii,jj,kk,ll,y,tarr)
c
c     ido=3
c   call ivprk(ido,neq,fcn,t,tend,tol,param,y)
c   call ivpbs(ido,neq,fcn,t,tend,tol,param,y)
c   call ivpag(ido,neq,fcn,fcnj,aaa,t,tend,tol,param,y)
c
c   call prtout(iend,time,yt)
c
c   go to 99
c
c   write(7,501) ii,jj,kk,ll,yt(31,1),yt(32,1),yt(33,1)
c   write(8,501) ii,jj,kk,ll,
c 1 yt(31,iend+1),yt(32,iend+1),yt(33,iend+1)
c 501 format(4i6,3e15.4)
c
c 99 return
c   end
c
c   subroutine dynout(ip,jp,kp,lp,y,tarr)
c
c**** subroutine dynout
c
c   common/props/den,denref,rmass,vmu,vlamb,eta,zeta,phi,rj(3,3)
c   common/ndata/x1(3),x2(3),x3(3),x4(3),
c 1     v1(3),v2(3),v3(3),v4(3),xc(3)
c   common/walldat/ywall,tcut,tmin,dencut,
c 1 idmax,jdmax,kdmax,xdmin,xdmax,ydmin,ydmax,zdmin,zdmax
c
c   dimension y(33),f(3,3),xt1(3),xt2(3),xt3(3),xt4(3),xt5(3),
c 1 ptc(3),id(5),jd(5),kd(5)
c
c   cl=(denref/den)**(-1./3.)
c
c   do 10 i=1,3
c   do 11 j=1,3
c     f(i,j)=y(3*(i-1)+j+9)

```

```

c      write(4,101) i,j,f(i,j)
c 101 format(i5,i5,e15.6)
      11 continue
      10 continue
c
c      call detcal(f,detf)
c      denout=denref/detf
c
c      momentum enhancement
c
c      ridmax=idmax
c      rjdmax=jdmax
c      rkdmax=kdmax
c      tmass=denref*((xdmax-xdmin)/(ridmax-1.0))*
1 ((ydmax-ydmin)/(rjdmax-1.0))*((zdmax-zdmin)/(rkdmax-1.0))
c      enhmom=((tmass+rmass)/rmass)**0.5
c      enhmom=1.0
c
c      do 12 i=1,3
c      ptc(i)=enhmom*y(27+i)/5.0
12 continue
c
c      do 20 i=1,3
c      xt1(i)=0.0
c      xt2(i)=0.0
c      xt3(i)=0.0
c      xt4(i)=0.0
c      xt5(i)=0.0
20 continue
c
c      do 23 i=1,3
c      do 21 j=1,3
c      xt1(i)=xt1(i)+c1*f(i,j)*(x1(j)-xc(j))
c      xt2(i)=xt2(i)+c1*f(i,j)*(x2(j)-xc(j))
c      xt3(i)=xt3(i)+c1*f(i,j)*(x3(j)-xc(j))
c      xt4(i)=xt4(i)+c1*f(i,j)*(x4(j)-xc(j))
21 continue
23 continue
c
c      do 22 i=1,3
c      xt1(i)=xt1(i)+y(30+i)
c      xt2(i)=xt2(i)+y(30+i)
c      xt3(i)=xt3(i)+y(30+i)
c      xt4(i)=xt4(i)+y(30+i)
c      xt5(i)=y(30+i)
22 continue
c
c      calculate the element numbers
c
c      nelmax=(idmax-1)*(jdmax-1)*(kdmax-1)
c
c      ridmax=idmax
c      delx=(xdmax-xdmin)/(ridmax-1.0)
c      rjdmax=jdmax
c      dely=(ydmax-ydmin)/(rjdmax-1.0)
c      rkdmax=kdmax
c      delz=(zdmax-zdmin)/(rkdmax-1.0)
c

```

```

id(1)=int((xt1(1)-xdmin)/delx)+1
kd(1)=int((xt1(3)-zdmin)/delz)+1
id(2)=int((xt2(1)-xdmin)/delx)+1
kd(2)=int((xt2(3)-zdmin)/delz)+1
id(3)=int((xt3(1)-xdmin)/delx)+1
kd(3)=int((xt3(3)-zdmin)/delz)+1
id(4)=int((xt4(1)-xdmin)/delx)+1
kd(4)=int((xt4(3)-zdmin)/delz)+1
id(5)=int((xt5(1)-xdmin)/delx)+1
kd(5)=int((xt5(3)-zdmin)/delz)+1
c
c   write(9,501) ip,jp,kp,lp
c 501 format(4i5)
c
c   do 303 ic=1,5
c   ia=id(ic)
c   if(ia.gt.idmax-1) go to 303
c   if(ia.lt.1) go to 303
c   ka=kd(ic)
c   if(ka.gt.kdmax-1) go to 303
c   if(ka.lt.1) go to 303
c   nelem=ia+(idmax-1)*(ka-1)
c   write(9,503) nelem,ptc(1),ptc(2),ptc(3),tarr
c 503 format(i5,4e10.3)
c   503 format(i8,4e10.3)
c   303 continue
c
c   go to 301
c
c   write(9,506) xt1(1),xt1(2),xt1(3)
c 506 format(3e20.8)
c   write(9,507) xt2(1),xt2(2),xt2(3)
c 507 format(3e20.8)
c   write(9,508) xt3(1),xt3(2),xt3(3)
c 508 format(3e20.8)
c   write(9,598) xt4(1),xt4(2),xt4(3)
c 598 format(3e20.8)
c   write(9,597) xt5(1),xt5(2),xt5(3)
c 597 format(3e20.8)
c
c 301 dummy=1.0
c
c   return
c   end
c
c   subroutine cthout(ip,jp,kp,lp,y)
c
c**** subroutine cthout
c
c   common/props/den,denref,rmass,vmu,vlamb,eta,zeta,phi,rj(3,3)
c   common/ndata/x1(3),x2(3),x3(3),x4(3),
c 1          v1(3),v2(3),v3(3),v4(3),xc(3)
c
c   dimension y(33),f(3,3),xt1(3),xt2(3),xt3(3),xt4(3),vtc(3)
c
c   nummat=1
c   numsub=49

```

```

c
c   c1=(denref/den)**(1./3.)
c   c2=(1.-phi)**(1./3.)
c   c3=c2/c1
c
c   do 10 i=1,3
c   do 11 j=1,3
c   f(i,j)=y(3*(i-1)+j+9)
c   write(4,101) i,j,f(i,j)
c 101 format(i5,i5,e15.6)
c   11 continue
c   10 continue
c
c   call detcal(f,detf)
c   denout=denref/detf
c
c   do 12 i=1,3
c   vtc(i)=1.0e+6*y(27+i)/rmass
c 12 continue
c
c   do 20 i=1,3
c   xt1(i)=0.0
c   xt2(i)=0.0
c   xt3(i)=0.0
c   xt4(i)=0.0
c   write(4,102) x1(i),x2(i),x4(i),x4(i),xc(i)
c 102 format(5e15.6)
c   20 continue
c
c   do 23 i=1,3
c   do 21 j=1,3
c   xt1(i)=xt1(i)+c3*f(i,j)*(x1(j)-xc(j))
c   xt2(i)=xt2(i)+c3*f(i,j)*(x2(j)-xc(j))
c   xt3(i)=xt3(i)+c3*f(i,j)*(x3(j)-xc(j))
c   xt4(i)=xt4(i)+c3*f(i,j)*(x4(j)-xc(j))
c 21 continue
c 23 continue
c
c   go to 301
c
c
c   do 22 i=1,3
c   xt1(i)=xt1(i)+y(30+i)
c   xt2(i)=xt2(i)+y(30+i)
c   xt3(i)=xt3(i)+y(30+i)
c   xt4(i)=xt4(i)+y(30+i)
c 22 continue
c
c 301 dummy=1.0
c
c   write(4,501) ip,jp,kp,lp
c 501 format(5x,'package ',i3,',',i3,',',i3,',',i3)
c   write(4,502) nummat,numsub
c 502 format(7x,'material ',i3,'/7x,'numsub ',i3)
c   write(4,532) denout
c 532 format(7x,'density = ',e20.8)
c   write(4,503) vtc(1)
c 503 format(7x,'xvel = ',e20.8)
c   write(4,504) vtc(2)

```

```

504 format (7x, 'yvel = ', e20.8)
write (4, 594) vtc (3)
594 format (7x, 'zvel = ', e20.8)
write (4, 505)
505 format (7x, 'insert pyramid')
write (4, 506) xt1 (1), xt1 (2), xt1 (3)
506 format (9x, 'point = ', e15.6, ', ', e15.6, ', ', e15.6)
write (4, 507) xt2 (1), xt2 (2), xt2 (3)
507 format (9x, 'point = ', e15.6, ', ', e15.6, ', ', e15.6)
write (4, 508) xt3 (1), xt3 (2), xt3 (3)
508 format (9x, 'point = ', e15.6, ', ', e15.6, ', ', e15.6)
write (4, 598) xt4 (1), xt4 (2), xt4 (3)
598 format (9x, 'vertex = ', e15.6, ', ', e15.6, ', ', e15.6)
write (4, 509)
509 format (7x, 'endinsert')
write (4, 591)
591 format (5x, 'endpackage')
c
return
end
c
subroutine prtout (iend, time, yt)
c
c**** subroutine prtout
c
dimension yt (33, 101)
c
dimension time (101), out (18, 101), f (3, 3), e (3, 3), ep (3, 3),
1 c (3, 3)
c
print output
c
open (9, file='pltdat/dc3d.out')
c
open (11, file='pltdat/h11.plt')
open (12, file='pltdat/h12.plt')
open (13, file='pltdat/h13.plt')
open (14, file='pltdat/h21.plt')
open (15, file='pltdat/h22.plt')
open (16, file='pltdat/h23.plt')
open (17, file='pltdat/h31.plt')
open (18, file='pltdat/h32.plt')
open (19, file='pltdat/h33.plt')
c
open (20, file='pltdat/f11.plt')
open (21, file='pltdat/f12.plt')
open (22, file='pltdat/f13.plt')
open (23, file='pltdat/f21.plt')
open (24, file='pltdat/f22.plt')
open (25, file='pltdat/f23.plt')
open (26, file='pltdat/f31.plt')
open (27, file='pltdat/f32.plt')
open (28, file='pltdat/f33.plt')
c
open (29, file='pltdat/ep11.plt')
open (30, file='pltdat/ep12.plt')
open (31, file='pltdat/ep13.plt')
open (32, file='pltdat/ep21.plt')

```



```

open(33, file='pltdat/ep22.plt')
open(34, file='pltdat/ep23.plt')
open(35, file='pltdat/ep31.plt')
open(36, file='pltdat/ep32.plt')
open(37, file='pltdat/ep33.plt')
c
open(38, file='pltdat/p1.plt')
open(39, file='pltdat/p2.plt')
open(40, file='pltdat/p3.plt')
c
open(41, file='pltdat/xcl.plt')
open(42, file='pltdat/xcl.plt')
open(43, file='pltdat/xcl.plt')
c
open(44, file='pltdat/detf.plt')
open(45, file='pltdat/ile.plt')
open(46, file='pltdat/j2e.plt')
open(47, file='pltdat/ilep.plt')
open(48, file='pltdat/j2ep.plt')
open(49, file='pltdat/detc.plt')
open(50, file='pltdat/out7.plt')
open(51, file='pltdat/out8.plt')
open(52, file='pltdat/out9.plt')
c
c print out the states
c
c do 80 i=1,iend+1
c write(9,111) (yt(j,i),j=1,33)
c 111 format(11e15.6)
c 80 continue
c
c calculate output variables
c
c do 60 i=1,18
c do 61 j=1,iend+1
c out(i,j)=0.0
61 continue
60 continue
c
c do 610 i=1,iend+1
c
c do 611 j=1,3
c do 612 k=1,3
c f(j,k) =yt(3*(j-1)+k+9,i)
c ep(j,k)=yt(3*(j-1)+k+18,i)
612 continue
611 continue
c
c call detcal(f,detval)
c call ecalc(f,e)
c
c do 614 j=1,3
c do 615 k=1,3
c if(j.eq.k) then
c deljk=1.0
c else
c deljk=0.0
c endif

```

```

        c(j,k)=deljk+2.0*e(j,k)
615 continue
614 continue
c
    call detcal(c,detc)
c
    out(1,i)=detval
    out(2,i)=(1./3.)*(e(1,1)+e(2,2)+e(3,3))
    out(4,i)=(1./3.)*(ep(1,1)+ep(2,2)+ep(3,3))
    out(6,i)=detc
c
610 continue
c
    do 52 j=1,9
        j1=j
        j2=j+9
        j3=j+18
        k1=j+10
        k2=j+19
        k3=j+28
        do 51 i=1,iend+1
            write(k1,112) time(i),yt(j1,i)
            write(k2,112) time(i),yt(j2,i)
            write(k3,112) time(i),yt(j3,i)
112 format(2e20.8)
        51 continue
        52 continue
c
    do 53 j=1,3
        j1=j+27
        j2=j+30
        k1=j+37
        k2=j+40
        do 54 i=1,iend+1
            write(k1,102) time(i),yt(j1,i)
            write(k2,102) time(i),yt(j2,i)
102 format(2e20.8)
        54 continue
        53 continue
c
    do 55 j=1,9
        jj=j+43
        do 56 i=1,iend+1
            write(jj,113) time(i),out(j,i)
113 format(2e20.8)
        56 continue
        55 continue
c
c
c    do 50 i=1,iend+1
c    out1(i)=yt(19,i)+yt(23,i)+yt(27,i)
c    out2(i)=abs(yt(19,i)-yt(23,i))
c    out3(i)=abs(yt(23,i)-yt(27,i))
c    out4(i)=abs(yt(19,i)-yt(27,i))
c    write(11,101) time(i),out1(i),out2(i),out3(i),out4(i)
c 101 format(5e15.6)
c 50 continue
c
    return

```

```

end
c
c      subroutine detcal(a,deta)
c
c**** subroutine detcal
c
c      dimension a(3,3)
c
c      deta=a(1,1)*(a(2,2)*a(3,3)-a(3,2)*a(2,3))-
1      a(1,2)*(a(2,1)*a(3,3)-a(2,3)*a(3,1))+
2      a(1,3)*(a(2,1)*a(3,2)-a(3,1)*a(2,2))
c
c      return
c      end
c
c      subroutine eldata(ii,jj,kk,ll)
c
c**** subroutine eldata
c
c      common/props/den,denref,rmass,vmu,vlamb,eta,zeta,phi,rj(3,3)
c
c      common/mesh/i1,i2,j1,j2,k1,k2,deltx,delty,deltz,
1 xlow,ylow,zlow
c
c      common/cthdatt/ velx(75,75,75),vely(75,75,75),
1 velz(75,75,75),pres(75,75,75),temp(75,75,75),
2 gama(75,75,75),spen(75,75,75),vmas(75,75,75),
3 vphi(75,75,75),cspd(75,75,75)
c
c      rmass=vmas(ii,jj,kk)
c
c      den=gama(ii,jj,kk)
c      phi=vphi(ii,jj,kk)
c
c      denref=2.7
c      dmge=0.0
c      vmu  =(1.-dmge)*1.0
c      vlamb=(1.-dmge)*1.0
c      eta=1.0
c
c      write(10,100) velx(ii,jj,kk),vely(ii,jj,kk),velz(ii,jj,kk),
c      1 pres(ii,jj,kk),temp(ii,jj,kk),gama(ii,jj,kk),spen(ii,jj,kk),
c      2 vmas(ii,jj,kk),vphi(ii,jj,kk),cspd(ii,jj,kk)
c 100 format(/7e11.3,/3e11.3,/)
c
c      return
c      end
c
c      subroutine nddata(ii,jj,kk,ll)
c
c**** subroutine nddata
c
c      common/ndata/x1(3),x2(3),x3(3),x4(3),
1      v1(3),v2(3),v3(3),v4(3),xc(3)
c
c      common/mesh/i1,i2,j1,j2,k1,k2,deltx,delty,deltz,
1 xlow,ylow,zlow
c

```

```

common/cthdatt/ velx(75,75,75),vely(75,75,75),
1 velz(75,75,75),pres(75,75,75),temp(75,75,75),
2 gama(75,75,75),spen(75,75,75),vmas(75,75,75),
3 vphi(75,75,75),cspd(75,75,75)
c
common/cthxyz/xcth(100),ycth(100),zcth(100)
c
common/velling/vfx(75,75,75),vfy(75,75,75),vfv(75,75,75)
c
c
c set cell coordinates
c
xn1=xcth(ii)
xn2=xcth(ii+1)
xn3=xcth(ii+1)
xn4=xcth(ii)
xn5=xcth(ii)
xn6=xcth(ii+1)
xn7=xcth(ii+1)
xn8=xcth(ii)
c
yn1=ycth(jj)
yn2=ycth(jj)
yn3=ycth(jj+1)
yn4=ycth(jj+1)
yn5=ycth(jj)
yn6=ycth(jj)
yn7=ycth(jj+1)
yn8=ycth(jj+1)
c
zn1=zcth(kk)
zn2=zcth(kk)
zn3=zcth(kk)
zn4=zcth(kk)
zn5=zcth(kk+1)
zn6=zcth(kk+1)
zn7=zcth(kk+1)
zn8=zcth(kk+1)
c
c
c set element coordinates
c
c
c go to (301,302,303,304,305) 11
c
301 x1(1)=xn1
x1(2)=yn1
x1(3)=zn1
x2(1)=xn2
x2(2)=yn2
x2(3)=zn2
x3(1)=xn4
x3(2)=yn4
x3(3)=zn4
x4(1)=xn5
x4(2)=yn5
x4(3)=zn5
go to 306
c
302 x1(1)=xn3
x1(2)=yn3

```

```
x1 (3) =zn3
x2 (1) =xn4
x2 (2) =yn4
x2 (3) =zn4
x3 (1) =xn2
x3 (2) =yn2
x3 (3) =zn2
x4 (1) =xn7
x4 (2) =yn7
x4 (3) =zn7
go to 306
```

c

```
303 x1 (1) =xn4
x1 (2) =yn4
x1 (3) =zn4
x2 (1) =xn2
x2 (2) =yn2
x2 (3) =zn2
x3 (1) =xn7
x3 (2) =yn7
x3 (3) =zn7
x4 (1) =xn5
x4 (2) =yn5
x4 (3) =zn5
go to 306
```

c

```
304 x1 (1) =xn8
x1 (2) =yn8
x1 (3) =zn8
x2 (1) =xn5
x2 (2) =yn5
x2 (3) =zn5
x3 (1) =xn7
x3 (2) =yn7
x3 (3) =zn7
x4 (1) =xn4
x4 (2) =yn4
x4 (3) =zn4
go to 306
```

c

```
305 x1 (1) =xn6
x1 (2) =yn6
x1 (3) =zn6
x2 (1) =xn7
x2 (2) =yn7
x2 (3) =zn7
x3 (1) =xn5
x3 (2) =yn5
x3 (3) =zn5
x4 (1) =xn2
x4 (2) =yn2
x4 (3) =zn2
go to 306
```

c

```
306 dummy=1.0
```

c

c

```
set cell velocities
```

c

```

vxnl=vfx(ii,jj,kk)
vxn2=vfx(ii+1,jj,kk)
vxn3=vfx(ii+1,jj+1,kk)
vxn4=vfx(ii,jj+1,kk)
vxn5=vfx(ii,jj,kk+1)
vxn6=vfx(ii+1,jj,kk+1)
vxn7=vfx(ii,jj+1,kk+1)
vxn8=vfx(ii+1,jj+1,kk+1)
c
vyn1=vfy(ii,jj,kk)
vyn2=vfy(ii+1,jj,kk)
vyn3=vfy(ii+1,jj+1,kk)
vyn4=vfy(ii,jj+1,kk)
vyn5=vfy(ii,jj,kk+1)
vyn6=vfy(ii+1,jj,kk+1)
vyn7=vfy(ii,jj+1,kk+1)
vyn8=vfy(ii+1,jj+1,kk+1)
c
vzn1=vfz(ii,jj,kk)
vzn2=vfz(ii+1,jj,kk)
vzn3=vfz(ii+1,jj+1,kk)
vzn4=vfz(ii,jj+1,kk)
vzn5=vfz(ii,jj,kk+1)
vzn6=vfz(ii+1,jj,kk+1)
vzn7=vfz(ii,jj+1,kk+1)
vzn8=vfz(ii+1,jj+1,kk+1)
c
c set nodal velocities
c
c go to (331,332,333,334,335) 11
c
331 v1(1)=vxnl
v1(2)=vyn1
v1(3)=vzn1
v2(1)=vxn2
v2(2)=vyn2
v2(3)=vzn2
v3(1)=vxn4
v3(2)=vyn4
v3(3)=vzn4
v4(1)=vxn5
v4(2)=vyn5
v4(3)=vzn5
go to 336
c
332 v1(1)=vxn3
v1(2)=vyn3
v1(3)=vzn3
v2(1)=vxn4
v2(2)=vyn4
v2(3)=vzn4
v3(1)=vxn2
v3(2)=vyn2
v3(3)=vzn2
v4(1)=vxn7
v4(2)=vyn7
v4(3)=vzn7
go to 336

```

```
c
333 v1(1)=vxn4
    v1(2)=vyn4
    v1(3)=vzn4
    v2(1)=vxn2
    v2(2)=vyn2
    v2(3)=vzn2
    v3(1)=vxn7
    v3(2)=vyn7
    v3(3)=vzn7
    v4(1)=vxn5
    v4(2)=vyn5
    v4(3)=vzn5
    go to 336

c
334 v1(1)=vxn8
    v1(2)=vyn8
    v1(3)=vzn8
    v2(1)=vxn5
    v2(2)=vyn5
    v2(3)=vzn5
    v3(1)=vxn7
    v3(2)=vyn7
    v3(3)=vzn7
    v4(1)=vxn4
    v4(2)=vyn4
    v4(3)=vzn4
    go to 336

c
335 v1(1)=vxn6
    v1(2)=vyn6
    v1(3)=vzn6
    v2(1)=vxn7
    v2(2)=vyn7
    v2(3)=vzn7
    v3(1)=vxn5
    v3(2)=vyn5
    v3(3)=vzn5
    v4(1)=vxn2
    v4(2)=vyn2
    v4(3)=vzn2
    go to 336

c
336 dummy=2.0

c
c   set initial coordinates
c
c   go to 337
c
    x1(1)=0.0
    x1(2)=0.0
    x1(3)=0.0
    x2(1)=1.0
    x2(2)=0.0
    x2(3)=0.0
    x3(1)=0.5
    x3(2)=sqrt(0.75)
    x3(3)=0.0
```

```

x4(1)=0.5
x4(2)=sqrt(0.75)/3.
x4(3)=1.0
c
c   set initial velocities
c
v1(1)=1.0
v1(2)=0.0
v1(3)=0.0
v2(1)=0.0
v2(2)=0.0
v2(3)=0.0
v3(1)=0.0
v3(2)=0.0
v3(3)=0.0
v4(1)=0.0
v4(2)=0.0
v4(3)=0.0
c
c 337 dummy=3.0
c
c   do 350 ip=1,3
c   write(10,340) x1(ip),x2(ip),x3(ip),x4(ip)
c 340 format(4e15.3)
c   350 continue
c   write(10,341)
c 341 format(' ')
c   do 352 ip=1,3
c   write(10,342) v1(ip),v2(ip),v3(ip),v4(ip)
c 342 format(4e15.3)
c   352 continue
c
c 337 dummy=3.0
c
c   return
c   end
c
c   subroutine initlz(h,f,ep,p)
c
c**** subrouitne initlz
c
c   common/props/den,denref,rmass,vmu,vlamb,eta,zeta,phi,rj(3,3)
c   common/ndata/x1(3),x2(3),x3(3),x4(3),
1      v1(3),v2(3),v3(3),v4(3),xc(3)
c
c
c   dimension h(3,3),f(3,3),ep(3,3),p(3)
c
c   set initial conditions
c
f(1,1)=1.0
f(1,2)=0.0
f(1,3)=0.0
f(2,1)=0.0
f(2,2)=1.0
f(2,3)=0.0
f(3,1)=0.0
f(3,2)=0.0

```



```

      f(3,3)=1.0
c
      detf=denref/den
c
      f(1,1)=detf**(1./3.)
      f(2,2)=detf**(1./3.)
      f(3,3)=detf**(1./3.)
c
      detf=f(1,1)*(f(2,2)*f(3,3)-f(3,2)*f(2,3))-
c 1      f(1,2)*(f(2,1)*f(3,3)-f(2,3)*f(3,1))+
c 2      f(1,3)*(f(2,1)*f(3,2)-f(3,1)*f(2,2))
c
      den=denref/detf
c
      write(10,103) den
c 103 format (e20.8)
c
      ep(1,1)=0.0
      ep(1,2)=0.0
      ep(1,3)=0.0
      ep(2,1)=0.0
      ep(2,2)=0.0
      ep(2,3)=0.0
      ep(3,1)=0.0
      ep(3,2)=0.0
      ep(3,3)=0.0
c
      h(1,1)=0.0
      h(1,2)=0.0
      h(1,3)=0.0
      h(2,1)=0.0
      h(2,2)=0.0
      h(2,3)=0.0
      h(3,1)=0.0
      h(3,2)=0.0
      h(3,3)=0.0
c
      p(1)=0.0
      p(2)=0.0
      p(3)=0.0
c
      call ivcalc(h,p)
c
      xc(1)=0.5
      xc(2)=sqrt(0.75)/3.
      xc(3)=1.0/4.0
c
      return
      end
c
      subroutine fcn(neq,t,y,yprime)
c
c**** subroutine fcn
c
      common/props/den,denref,rmass,vmu,vlamb,eta,zeta,phi,rj(3,3)
      common/ndata/x1(3),x2(3),x3(3),x4(3),
c 1      v1(3),v2(3),v3(3),v4(3),xc(3)
c

```

```

      dimension y(33),yprime(33)
c
      dimension h(3,3),f(3,3),fi(3,3),e(3,3),ep(3,3),p(3),
1 rji(3,3),rm(3,3,3,3),rk(3,3),rkp(3,3),c(3,3),ci(3,3),
2 vg(3,3),dd(3,3),rn(3,3,3,3),vkv(3,3),xct(3)
c
      dimension hd(3,3),fd(3,3),ed(3,3),epd(3,3),pd(3),xcd(3)
c
c      define variables
c
      do 10 i=1,3
      do 11 j=1,3
      h(i,j) = y(3*(i-1)+j)
      f(i,j) = y(3*(i-1)+j+9)
      ep(i,j)= y(3*(i-1)+j+18)
11 continue
10 continue
c
      do 13 i=1,3
      do 14 j=1,3
      c(i,j)=0.0
      do 15 ia=1,3
      c(i,j)=c(i,j)+f(ia,i)*f(ia,j)
15 continue
14 continue
13 continue
c
      ninv=3
      ldc=3
      ldcinv=3
c
      call linrg(ninv,c,ldc,ci,ldcinv)
      iflag=1
      call matv03(iflag,ninv,c,ci)
c
      do 12 i=1,3
      p(i) = y(i+27)
      xct(i)= y(i+30)
12 continue
c
      call ecalc(f,e)
c
      write(10,104)
c 104 format('subroutine fcn')
c
      call jcalc(den,x1,x2,x3,x4,rj)
c
      write(10,105)
c 105 format('subroutine fcn jcalc')
c
      do 201 ii=1,3
      do 202 jj=1,3
      write(10,102) rj(ii,jj)
c 102 format(e20.8)
c 202 continue
c 201 continue
c
      call jinv(rj,rji)

```

```

c
c   calculate transformer modulus
c
  do 20 i=1,3
  do 21 j=1,3
  do 22 ia=1,3
  do 23 ib=1,3
  if(i.eq.ib) then
    delib=1.0
  else
    delib=0.0
  endif
  if(j.eq.ib) then
    deljb=1.0
  else
    deljb=0.0
  endif
  rm(i,j,ia,ib)=0.5*(delib*f(ia,j)+f(ia,i)*deljb)
23 continue
22 continue
21 continue
20 continue
c
  do 30 i=1,3
  do 31 j=1,3
  if(i.eq.j) then
    delij=1.0
  else
    delij=0.0
  endif
c
  rk(i,j)=(rmass/denref)*(2.*vmu*(e(i,j)-ep(i,j))+
1 delij*vlamb*((e(1,1)+e(2,2)+e(3,3))-
c 2 (ep(1,1)+ep(2,2)+ep(3,3))))
c   rkp(i,j)=-rk(i,j)
c
  call detcal(f,rvl)
  rk(i,j)= (rmass/((1.-phi)*denref))*2.*vmu*((e(i,j)-
1 (1./3.)*delij*(e(1,1)+e(2,2)+e(3,3)))-ep(i,j))
2 -(rmass/((1.-phi)*denref))*(vlamb+(2./3.)*vmu)*(1./rvl-1.)
3 *(1./rvl)*ci(i,j)
  rkp(i,j)=- (rmass/((1.-phi)*denref))*2.*vmu*((e(i,j)-
1 (1./3.)*delij*(e(1,1)+e(2,2)+e(3,3)))-ep(i,j))
c
31 continue
30 continue
c
  do 50 i=1,3
  do 51 j=1,3
  fd(i,j)=0.0
  do 52 ia=1,3
  fd(i,j)=fd(i,j)+h(i,ia)*rji(ia,j)
52 continue
51 continue
50 continue
c
  ninv=3
  ldf=3

```

```

        ldfinv=3
c
c    call linrg(ninv,f,ldf,fi,ldfinv)
        iflag=2
        call matv03(iflag,ninv,f,fi)
c
        do 300 i=1,3
        do 301 j=1,3
        vg(i,j)=0.0
        do 302 ia=1,3
        vg(i,j)=vg(i,j)+fd(i,ia)*fi(ia,j)
302 continue
301 continue
300 continue
c
        do 303 i=1,3
        do 304 j=1,3
        dd(i,j)=0.5*(vg(i,j)+vg(j,i))
304 continue
303 continue
c
c    calculate transformer modulus
c
        do 220 i=1,3
        do 221 j=1,3
        do 222 ia=1,3
        do 223 ib=1,3
        if(i.eq.ib) then
            delib=1.0
        else
            delib=0.0
        endif
        if(j.eq.ib) then
            deljb=1.0
        else
            deljb=0.0
        endif
        rn(i,j,ib,ia)=0.5*(delib*fi(ia,j)+fi(ia,i)*deljb)
223 continue
222 continue
221 continue
220 continue
c
c    zeta=1.0
        call detcal(f,rvl)
c
        do 231 i=1,3
        do 232 j=1,3
        vkv(i,j)=0.0
        do 233 ia=1,3
        do 234 ib=1,3
        if(ia.eq.ib) then
            delab=1.0
        else
            delab=0.0
        endif
c    vkv(i,j)=vkv(i,j)+zeta*rn(ia,ib,i,j)*dd(ia,ib)
        vkv(i,j)=vkv(i,j)+zeta*(rmas*rvl/((1.-phi)*denref))

```

```

      1 *rn(ia,ib,i,j)*
c     1 delab*(1./3.)*(dd(1,1)+dd(2,2)+dd(3,3))
c     2 delab*(1./3.)*amin1(0.0,dd(1,1)+dd(2,2)+dd(3,3))
      2 dd(ia,ib)
      3 *(0.5*(dd(1,1)**2+dd(1,2)**2+dd(1,3)**2+
      4         dd(2,1)**2+dd(2,2)**2+dd(2,3)**2+
      5         dd(3,1)**2+dd(3,2)**2+dd(3,3)**2))**2
234 continue
233 continue
232 continue
231 continue
c
      do 40 i=1,3
      do 41 j=1,3
      hd(i,j)=0.0
      do 42 ia=1,3
      do 43 ib=1,3
      hd(i,j)=hd(i,j)-rm(ia,ib,i,j)*rk(ia,ib)
43 continue
42 continue
      hd(i,j)=hd(i,j)-vkv(i,j)
41 continue
40 continue
c
      do 60 i=1,3
      do 61 j=1,3
      epd(i,j)=-(1./eta)*rkp(i,j)
61 continue
60 continue
c
      do 70 i=1,3
      pd(i)=0.0
      xcd(i)=(1./rmass)*p(i)
70 continue
c
c     set the vector yprime
c
      do 80 i=1,3
      do 81 j=1,3
      yprime(3*(i-1)+j) = hd(i,j)
      yprime(3*(i-1)+j+9) = fd(i,j)
      yprime(3*(i-1)+j+18) = epd(i,j)
81 continue
80 continue
c
      do 82 i=1,3
      yprime(i+27)=pd(i)
      yprime(i+30)=xcd(i)
82 continue
c
      do 201 ii=1,3
      do 202 jj=1,3
c     write(10,102) f(ii,jj),fd(ii,jj),h(ii,jj),hd(ii,jj)
c 102 format(5e15.3)
202 continue
201 continue
c
      return

```

```

end
c
subroutine ecalc(f,e)
c
c**** subroutine ecalc
c
dimension f(3,3),e(3,3),c(3,3)
c
calculate e
c
do 10 i=1,3
do 11 j=1,3
c
e(i,j)=0.0
c(i,j)=0.0
if(i.eq.j) then
delij=1.0
else
delij=0.0
endif
c
do 12 ia=1,3
c(i,j)=c(i,j)+f(ia,i)*f(ia,j)
12 continue
c
e(i,j)=0.50*(c(i,j)-delij)
c
11 continue
10 continue
c
return
end
c
subroutine jinv(z,zi)
c
c**** subroutine jinv
c
inverts the symmetric 3x3 matrix z
c
dimension z(3,3),zi(3,3)
c
z1=z(1,1)
z2=z(2,2)
z3=z(3,3)
z4=z(1,2)
z5=z(2,3)
z6=z(1,3)
c
det=z1*(z2*z3-z5*z5)-z4*(z4*z3-z5*z6)+z6*(z4*z5-z2*z6)
c
zi(1,1)=+(1./det)*(z2*z3-z5*z5)
zi(2,1)=- (1./det)*(z4*z3-z5*z6)
zi(3,1)=+(1./det)*(z4*z5-z2*z6)
zi(1,2)=- (1./det)*(z4*z3-z5*z6)
zi(2,2)=+(1./det)*(z1*z3-z6*z6)
zi(3,2)=- (1./det)*(z1*z5-z4*z6)
zi(1,3)=+(1./det)*(z4*z5-z2*z6)
zi(2,3)=- (1./det)*(z1*z5-z4*z6)

```

```

      zi(3,3)=+(1./det)*(z1*z2-z4*z4)
c
      return
      end
c
      subroutine jref(g,rjp)
c
c**** subroutine jref
c
      common/props/den,denref,rmass,vmu,vlamb,eta,zeta,phi,rj(3,3)
      common/rdata/xx1(3),xx2(3),xx3(3),xx4(3),xxc(3),vref
c
      dimension g(3,3),rjp(3,3)
c
      detg=g(1,1)*(g(2,2)*g(3,3)-g(3,2)*g(2,3))-
1      g(1,2)*(g(2,1)*g(3,3)-g(2,3)*g(3,1))+
2      g(1,3)*(g(2,1)*g(3,2)-g(3,1)*g(2,2))
c
      rmass=(1.0-phi)*den*vref*detg
      rmass=abs((1.0-phi)*den*vref*detg)
c
      calculate the reference inertia tensor
c
      h1 = sqrt((xx1(1)-xxc(1))**2+(xx1(2)-
1      xxc(2))**2+(xx1(3)-xxc(3))**2)
      h2 = sqrt((xx2(1)-xxc(1))**2+(xx2(2)-
1      xxc(2))**2+(xx2(3)-xxc(3))**2)
      h3 = sqrt((xx3(1)-xxc(1))**2+(xx3(2)-
1      xxc(2))**2+(xx3(3)-xxc(3))**2)
      h4 = sqrt((xx4(1)-xxc(1))**2+(xx4(2)-
1      xxc(2))**2+(xx4(3)-xxc(3))**2)
c
      ep11 = (xx1(1)-xxc(1))/h1
      ep12 = (xx1(2)-xxc(2))/h1
      ep13 = (xx1(3)-xxc(3))/h1
c
      ep21 = (xx2(1)-xxc(1))/h2
      ep22 = (xx2(2)-xxc(2))/h2
      ep23 = (xx2(3)-xxc(3))/h2
c
      ep31 = (xx3(1)-xxc(1))/h3
      ep32 = (xx3(2)-xxc(2))/h3
      ep33 = (xx3(3)-xxc(3))/h3
c
      ep41 = (xx4(1)-xxc(1))/h4
      ep42 = (xx4(2)-xxc(2))/h4
      ep43 = (xx4(3)-xxc(3))/h4
c
      rjp11=(rmass/20.)*((h1**2)*ep11*ep11+(h2**2)*ep21*ep21
1      +(h3**2)*ep31*ep31+(h4**2)*ep41*ep41)
      rjp12=(rmass/20.)*((h1**2)*ep11*ep12+(h2**2)*ep21*ep22
1      +(h3**2)*ep31*ep32+(h4**2)*ep41*ep42)
      rjp13=(rmass/20.)*((h1**2)*ep11*ep13+(h2**2)*ep21*ep23
1      +(h3**2)*ep31*ep33+(h4**2)*ep41*ep43)
c
      rjp21=(rmass/20.)*((h1**2)*ep12*ep11+(h2**2)*ep22*ep21
1      +(h3**2)*ep32*ep31+(h4**2)*ep42*ep41)
      rjp22=(rmass/20.)*((h1**2)*ep12*ep12+(h2**2)*ep22*ep22

```

```

1 +(h3**2)*ep32*ep32+(h4**2)*ep42*ep42)
rjp23=(rmass/20.)*(h1**2)*ep12*ep13+(h2**2)*ep22*ep23
1 +(h3**2)*ep32*ep33+(h4**2)*ep42*ep43)
c
rjp31=(rmass/20.)*(h1**2)*ep13*ep11+(h2**2)*ep23*ep21
1 +(h3**2)*ep33*ep31+(h4**2)*ep43*ep41)
rjp32=(rmass/20.)*(h1**2)*ep13*ep12+(h2**2)*ep23*ep22
1 +(h3**2)*ep33*ep32+(h4**2)*ep43*ep42)
rjp33=(rmass/20.)*(h1**2)*ep13*ep13+(h2**2)*ep23*ep23
1 +(h3**2)*ep33*ep33+(h4**2)*ep43*ep43)
c
rjp(1,1)=rjp11
rjp(1,2)=rjp12
rjp(1,3)=rjp13
rjp(2,1)=rjp21
rjp(2,2)=rjp22
rjp(2,3)=rjp23
rjp(3,1)=rjp31
rjp(3,2)=rjp32
rjp(3,3)=rjp33
c
return
end
c
subroutine jcalc(x1,x2,x3,x4,xc,rj)
c
subroutine jcalc(den,x1,x2,x3,x4,xc,rj)
c
c**** subroutine jcalc
c
common/rdata/xx1(3),xx2(3),xx3(3),xx4(3),xxc(3),vref
c
dimension x1(3),x2(3),x3(3),x4(3),rj(3,3),
1 rjp(3,3),a(12,12),b(12),s(12),ainv(12,12),
2 g(3,3),ginv(3,3),xc(3),aml(12,12),am2(12,12)
c
c set the reference tetrahedron
c
xx1(1)=0.0
xx1(2)=0.0
xx1(3)=0.0
xx2(1)=1.0
xx2(2)=0.0
xx2(3)=0.0
xx3(1)=0.5
xx3(2)=sqrt(0.75)
xx3(3)=0.0
xx4(1)=0.5
xx4(2)=sqrt(0.75)/3.
xx4(3)=1.0
c
xxc(1)=0.5
xxc(2)=sqrt(0.75)/3.
xxc(3)=1.0/4.0
c
vref=(1./3.)*(1./2.)*sqrt(0.75)
c
c set the right hand side vector
c

```



```

b(1) =x1(1)
b(2) =x1(2)
b(3) =x1(3)
b(4) =x2(1)
b(5) =x2(2)
b(6) =x2(3)
b(7) =x3(1)
b(8) =x3(2)
b(9) =x3(3)
b(10)=x4(1)
b(11)=x4(2)
b(12)=x4(3)

```

c  
c  
c

```
set the coefficient matrix
```

```

a(1,1) =xx1(1)-xxc(1)
a(1,2) =xx1(2)-xxc(2)
a(1,3) =xx1(3)-xxc(3)
a(1,4) =0.0
a(1,5) =0.0
a(1,6) =0.0
a(1,7) =0.0
a(1,8) =0.0
a(1,9) =0.0
a(1,10)=1.0
a(1,11)=0.0
a(1,12)=0.0

```

c

```

a(2,1) =0.0
a(2,2) =0.0
a(2,3) =0.0
a(2,4) =xx1(1)-xxc(1)
a(2,5) =xx1(2)-xxc(2)
a(2,6) =xx1(3)-xxc(3)
a(2,7) =0.0
a(2,8) =0.0
a(2,9) =0.0
a(2,10)=0.0
a(2,11)=1.0
a(2,12)=0.0

```

c

```

a(3,1) =0.0
a(3,2) =0.0
a(3,3) =0.0
a(3,4) =0.0
a(3,5) =0.0
a(3,6) =0.0
a(3,7) =xx1(1)-xxc(1)
a(3,8) =xx1(2)-xxc(2)
a(3,9) =xx1(3)-xxc(3)
a(3,10)=0.0
a(3,11)=0.0
a(3,12)=1.0

```

c

```

a(4,1) =xx2(1)-xxc(1)
a(4,2) =xx2(2)-xxc(2)
a(4,3) =xx2(3)-xxc(3)
a(4,4) =0.0

```

a(4,5) =0.0  
 a(4,6) =0.0  
 a(4,7) =0.0  
 a(4,8) =0.0  
 a(4,9) =0.0  
 a(4,10)=1.0  
 a(4,11)=0.0  
 a(4,12)=0.0

c

a(5,1) =0.0  
 a(5,2) =0.0  
 a(5,3) =0.0  
 a(5,4) =xx2(1)-xxc(1)  
 a(5,5) =xx2(2)-xxc(2)  
 a(5,6) =xx2(3)-xxc(3)  
 a(5,7) =0.0  
 a(5,8) =0.0  
 a(5,9) =0.0  
 a(5,10)=0.0  
 a(5,11)=1.0  
 a(5,12)=0.0

c

a(6,1) =0.0  
 a(6,2) =0.0  
 a(6,3) =0.0  
 a(6,4) =0.0  
 a(6,5) =0.0  
 a(6,6) =0.0  
 a(6,7) =xx2(1)-xxc(1)  
 a(6,8) =xx2(2)-xxc(2)  
 a(6,9) =xx2(3)-xxc(3)  
 a(6,10)=0.0  
 a(6,11)=0.0  
 a(6,12)=1.0

c

a(7,1) =xx3(1)-xxc(1)  
 a(7,2) =xx3(2)-xxc(2)  
 a(7,3) =xx3(3)-xxc(3)  
 a(7,4) =0.0  
 a(7,5) =0.0  
 a(7,6) =0.0  
 a(7,7) =0.0  
 a(7,8) =0.0  
 a(7,9) =0.0  
 a(7,10)=1.0  
 a(7,11)=0.0  
 a(7,12)=0.0

c

a(8,1) =0.0  
 a(8,2) =0.0  
 a(8,3) =0.0  
 a(8,4) =xx3(1)-xxc(1)  
 a(8,5) =xx3(2)-xxc(2)  
 a(8,6) =xx3(3)-xxc(3)  
 a(8,7) =0.0  
 a(8,8) =0.0  
 a(8,9) =0.0  
 a(8,10)=0.0

```

a(8,11)=1.0
a(8,12)=0.0
c
a(9,1) =0.0
a(9,2) =0.0
a(9,3) =0.0
a(9,4) =0.0
a(9,5) =0.0
a(9,6) =0.0
a(9,7) =xx3(1)-xxc(1)
a(9,8) =xx3(2)-xxc(2)
a(9,9) =xx3(3)-xxc(3)
a(9,10)=0.0
a(9,11)=0.0
a(9,12)=1.0
c
a(10,1) =xx4(1)-xxc(1)
a(10,2) =xx4(2)-xxc(2)
a(10,3) =xx4(3)-xxc(3)
a(10,4) =0.0
a(10,5) =0.0
a(10,6) =0.0
a(10,7) =0.0
a(10,8) =0.0
a(10,9) =0.0
a(10,10)=1.0
a(10,11)=0.0
a(10,12)=0.0
c
a(11,1) =0.0
a(11,2) =0.0
a(11,3) =0.0
a(11,4) =xx4(1)-xxc(1)
a(11,5) =xx4(2)-xxc(2)
a(11,6) =xx4(3)-xxc(3)
a(11,7) =0.0
a(11,8) =0.0
a(11,9) =0.0
a(11,10)=0.0
a(11,11)=1.0
a(11,12)=0.0
c
a(12,1) =0.0
a(12,2) =0.0
a(12,3) =0.0
a(12,4) =0.0
a(12,5) =0.0
a(12,6) =0.0
a(12,7) =xx4(1)-xxc(1)
a(12,8) =xx4(2)-xxc(2)
a(12,9) =xx4(3)-xxc(3)
a(12,10)=0.0
a(12,11)=0.0
a(12,12)=1.0
c
c
c
call inverse solver
ninv=12

```

```
        lda=12
        ldainv=12
c
c      write(10,106)
c 106 format('sub jcalc before solver')
c
c      do 108 iii=1,12
c      do 109 jjj=1,12
c      write(10,110) a(iii,jjj)
c 110 format(e20.8)
c 109 continue
c 108 continue
c
c      call linrg(ninv,a,lda,ainv,ldainv)
c      iflag=3
c      call matv12(iflag,ninv,a,ainv)
c      call amod1(a,am1)
c      call matinv(ninv,am1,am2)
c      call amod2(am2,ainv)
c
c      write(10,107)
c 107 format('sub jcalc after solver')
c
c      calculate the solution vector
c
c      do 10 i=1,12
c      s(i)=0.0
c      do 11 j=1,12
c      s(i)=s(i)+ainv(i,j)*b(j)
c 11 continue
c      write(4,876) i,b(i),s(i)
c 876 format(1x,i5,2e15.3)
c 10 continue
c
c      set the tensor g
c
c      g(1,1)=s(1)
c      g(1,2)=s(2)
c      g(1,3)=s(3)
c      g(2,1)=s(4)
c      g(2,2)=s(5)
c      g(2,3)=s(6)
c      g(3,1)=s(7)
c      g(3,2)=s(8)
c      g(3,3)=s(9)
c
c      xc(1)=s(10)
c      xc(2)=s(11)
c      xc(3)=s(12)
c
c      invert the tensor g
c
c      call inverse solver
c
c      ninv=3
c      ldg=3
c      ldginv=3
c
```

```

c      call linrg(ninv,g,ldg,ginv,ldginv)
c      iflag=4
c      call matv03(iflag,ninv,g,ginv)
c
c      call jref(g,rjp)
c
c      calculate the inertia tensor
c
c      do 20 i=1,3
c      do 21 j=1,3
c      rj(i,j)=0.0
c      do 22 ia=1,3
c      do 23 ib=1,3
c      rj(i,j)=rj(i,j)+ginv(ia,i)*rjp(ia,ib)*ginv(ib,j)
23 continue
22 continue
21 continue
20 continue
c
c      return
c      end
c
c
c      subroutine ivcalc(h,p)
c
c**** subroutine ivcalc
c
c      common/props/den,denref,rmass,vmu,vlamb,eta,zeta,phi,rj(3,3)
c      common/rdata/xx1(3),xx2(3),xx3(3),xx4(3),xxc(3),vref
c      common/ndata/x1(3),x2(3),x3(3),x4(3),
1      v1(3),v2(3),v3(3),v4(3),xc(3)
c
c      dimension a(12,12),b(12),s(12),ainv(12,12),
1      g(3,3),h(3,3),p(3),am1(12,12),am2(12,12)
c
c      set the right hand side vector
c
c      b(1) =v1(1)
c      b(2) =v1(2)
c      b(3) =v1(3)
c      b(4) =v2(1)
c      b(5) =v2(2)
c      b(6) =v2(3)
c      b(7) =v3(1)
c      b(8) =v3(2)
c      b(9) =v3(3)
c      b(10)=v4(1)
c      b(11)=v4(2)
c      b(12)=v4(3)
c
c
c      set the coefficient matrix
c
c      a(1,1) =x1(1)-xc(1)
c      a(1,2) =x1(2)-xc(2)
c      a(1,3) =x1(3)-xc(3)
c      a(1,4) =0.0
c      a(1,5) =0.0
c      a(1,6) =0.0

```

a(1,7) =0.0  
a(1,8) =0.0  
a(1,9) =0.0  
a(1,10)=1.0  
a(1,11)=0.0  
a(1,12)=0.0

c

a(2,1) =0.0  
a(2,2) =0.0  
a(2,3) =0.0  
a(2,4) =x1(1)-xc(1)  
a(2,5) =x1(2)-xc(2)  
a(2,6) =x1(3)-xc(3)  
a(2,7) =0.0  
a(2,8) =0.0  
a(2,9) =0.0  
a(2,10)=0.0  
a(2,11)=1.0  
a(2,12)=0.0

c

a(3,1) =0.0  
a(3,2) =0.0  
a(3,3) =0.0  
a(3,4) =0.0  
a(3,5) =0.0  
a(3,6) =0.0  
a(3,7) =x1(1)-xc(1)  
a(3,8) =x1(2)-xc(2)  
a(3,9) =x1(3)-xc(3)  
a(3,10)=0.0  
a(3,11)=0.0  
a(3,12)=1.0

c

a(4,1) =x2(1)-xc(1)  
a(4,2) =x2(2)-xc(2)  
a(4,3) =x2(3)-xc(3)  
a(4,4) =0.0  
a(4,5) =0.0  
a(4,6) =0.0  
a(4,7) =0.0  
a(4,8) =0.0  
a(4,9) =0.0  
a(4,10)=1.0  
a(4,11)=0.0  
a(4,12)=0.0

c

a(5,1) =0.0  
a(5,2) =0.0  
a(5,3) =0.0  
a(5,4) =x2(1)-xc(1)  
a(5,5) =x2(2)-xc(2)  
a(5,6) =x2(3)-xc(3)  
a(5,7) =0.0  
a(5,8) =0.0  
a(5,9) =0.0  
a(5,10)=0.0  
a(5,11)=1.0  
a(5,12)=0.0

c

```
a(6,1) =0.0
a(6,2) =0.0
a(6,3) =0.0
a(6,4) =0.0
a(6,5) =0.0
a(6,6) =0.0
a(6,7) =x2(1)-xc(1)
a(6,8) =x2(2)-xc(2)
a(6,9) =x2(3)-xc(3)
a(6,10)=0.0
a(6,11)=0.0
a(6,12)=1.0
```

c

```
a(7,1) =x3(1)-xc(1)
a(7,2) =x3(2)-xc(2)
a(7,3) =x3(3)-xc(3)
a(7,4) =0.0
a(7,5) =0.0
a(7,6) =0.0
a(7,7) =0.0
a(7,8) =0.0
a(7,9) =0.0
a(7,10)=1.0
a(7,11)=0.0
a(7,12)=0.0
```

c

```
a(8,1) =0.0
a(8,2) =0.0
a(8,3) =0.0
a(8,4) =x3(1)-xc(1)
a(8,5) =x3(2)-xc(2)
a(8,6) =x3(3)-xc(3)
a(8,7) =0.0
a(8,8) =0.0
a(8,9) =0.0
a(8,10)=0.0
a(8,11)=1.0
a(8,12)=0.0
```

c

```
a(9,1) =0.0
a(9,2) =0.0
a(9,3) =0.0
a(9,4) =0.0
a(9,5) =0.0
a(9,6) =0.0
a(9,7) =x3(1)-xc(1)
a(9,8) =x3(2)-xc(2)
a(9,9) =x3(3)-xc(3)
a(9,10)=0.0
a(9,11)=0.0
a(9,12)=1.0
```

c

```
a(10,1) =x4(1)-xc(1)
a(10,2) =x4(2)-xc(2)
a(10,3) =x4(3)-xc(3)
a(10,4) =0.0
a(10,5) =0.0
```

```

a(10,6) =0.0
a(10,7) =0.0
a(10,8) =0.0
a(10,9) =0.0
a(10,10)=1.0
a(10,11)=0.0
a(10,12)=0.0
c
a(11,1) =0.0
a(11,2) =0.0
a(11,3) =0.0
a(11,4) =x4(1)-xc(1)
a(11,5) =x4(2)-xc(2)
a(11,6) =x4(3)-xc(3)
a(11,7) =0.0
a(11,8) =0.0
a(11,9) =0.0
a(11,10)=0.0
a(11,11)=1.0
a(11,12)=0.0
c
a(12,1) =0.0
a(12,2) =0.0
a(12,3) =0.0
a(12,4) =0.0
a(12,5) =0.0
a(12,6) =0.0
a(12,7) =x4(1)-xc(1)
a(12,8) =x4(2)-xc(2)
a(12,9) =x4(3)-xc(3)
a(12,10)=0.0
a(12,11)=0.0
a(12,12)=1.0
c
c call inverse solver
c
c ninv=12
c lda=12
c ldainv=12
-c
c write(10,106)
c 106 format('sub jcalc before solver')
c
c do 108 iii=1,12
c do 109 jjj=1,12
c write(10,110) a(iii, jjj)
c 110 format(e20.8)
c 109 continue
c 108 continue
c
c call linrg(ninv,a,lda,ainv,ldainv)
c iflag=5
c call matv12(iflag,ninv,a,ainv)
c call amod1(a,am1)
c call matinv(ninv,am1,am2)
c call amod2(am2,ainv)
c
c write(10,107)

```



```

c 107 format('sub jcalc after solver')
c
c   calculate the solution vector
c
      do 10 i=1,12
        s(i)=0.0
        do 11 j=1,12
          s(i)=s(i)+ainv(i,j)*b(j)
11      continue
10     continue

c
c   set the tensor g
c
      const=(denref/den)**(1./3.)
c
      g(1,1)=s(1)*const
      g(1,2)=s(2)*const
      g(1,3)=s(3)*const
      g(2,1)=s(4)*const
      g(2,2)=s(5)*const
      g(2,3)=s(6)*const
      g(3,1)=s(7)*const
      g(3,2)=s(8)*const
      g(3,3)=s(9)*const
c
      p(1)=s(10)*rmass
      p(2)=s(11)*rmass
      p(3)=s(12)*rmass
c
c   calculate the tensor h
c
      do 20 i=1,3
        do 21 j=1,3
          h(i,j)=0.0
          do 22 ia=1,3
            h(i,j)=h(i,j)+g(i,ia)*rj(ia,j)
22      continue
21      continue
20      continue

c
      return
      end
c
      subroutine ifdcrk(ido,neq,t,tend,tol,param,y)
c
      dimension y(33),yprime(33),param(50)
      dimension f1(33),f2(33),f3(33),f4(33),y1(33),y2(33),y3(33),
1 y4(33)
c
c   external fcn
c
      nstep=1000
      rnstep=nstep
      delt=(tend-t)/rnstep
c
      do 10 i=1,nstep
c
      ri=i

```

```

t1=t+(ri-1.0)*delt
t2=t1+delt/2.0
t3=t1+delt/2.0
t4=t1+delt
c
do 21 j=1,neq
y1(j)=y(j)
21 continue
c
call fcn(neq,t1,y1,f1)
c
do 22 j=1,neq
y2(j)=y(j)+(delt/2.0)*f1(j)
22 continue
c
call fcn(neq,t2,y2,f2)
c
do 23 j=1,neq
y3(j)=y(j)+(delt/2.0)*f2(j)
23 continue
c
call fcn(neq,t3,y3,f3)
c
do 24 j=1,neq
y4(j)=y(j)+delt*f3(j)
24 continue
c
call fcn(neq,t4,y4,f4)
c
do 30 j=1,neq
y(j)=y(j)+(delt/6.0)*(f1(j)+2.0*f2(j)+2.0*f3(j)+f4(j))
30 continue
c
10 continue
c
return
end
c
subroutine ivdcrk(ido,neq,tbeg,tend,tol,param,y)
c
common/intpar/epsint,ymxref
c
dimension y(33),yw(33),ymax(33),param(50),err(33)
dimension f1(33),f2(33),f3(33),f4(33),y1(33),y2(33),y3(33),
1 y4(33)
c
eps=1.0e-6
ymxref=1.0e-6
c
eps=epsint
c
delmin=1.0e-24
nstep=1000000
c
rnstep=nstep
delt=(tend-tbeg)/rnstep
c
delmin=delt/10.0
c

```

```

do 11 i=1,neq
  ymax(i)=amax1(ymxref,abs(y(i)))
11 continue
c
  t=tbeg
c
100 t1=t
  if(t+delt.gt.tend) delt=tend-t
  t2=t+delt/2.0
  t3=t+delt
c
  do 91 i=1,neq
    y1(i)=y(i)
  91 continue
c
  call rkstep(ido,neq,t1,t3,tol,param,y1,y2)
  call rkstep(ido,neq,t1,t2,tol,param,y1,y3)
  call rkstep(ido,neq,t2,t3,tol,param,y3,y4)
c
  errmax=0.0
  do 12 i=1,neq
    err(i)=abs(y4(i)-y2(i))/(eps*ymax(i))
    errmax=amax1(errmax,err(i))
  12 continue
c
  if(errmax.le.0.0) delt=2.0*delt
  if(errmax.gt.1.0) go to 101
  if(errmax.gt.0.0) delt=0.99*delt*errmax**(-1.0/5.0)
c
  do 21 i=1,neq
    y(i)=y4(i)
    ymax(i)=amax1(ymax(i),abs(y(i)))
  21 continue
c
  t=t3
  if(t.ge.tend) go to 99
  if(delt.lt.delmin) go to 98
  go to 100
c
-101 delt=delt/2.0
  if(delt.lt.delmin) go to 98
  go to 100
c
  98 ido=98
  write(10,110) ido,t,delt
  110 format(1x,i5,2e15.3)
c 110 format(1x,'time step less than minimum, ido =',i5)
  return
c
  99 ido=99
  write(10,120) ido,t,delt
c 120 format(1x,i5,2e15.3)
  return
c
  end
c
  subroutine rkstep(ido,neq,tbeg,tend,tol,param,y,yout)
c

```

```

dimension y(33),param(50),yout(33)
dimension f1(33),f2(33),f3(33),f4(33),y1(33),y2(33),y3(33),
1 y4(33)
c
delt=tend-tbeg
t1=tbeg
t2=t1+delt/2.0
t3=t1+delt/2.0
t4=t1+delt
c
do 21 j=1,neq
y1(j)=y(j)
21 continue
c
call fcn(neq,t1,y1,f1)
c
do 22 j=1,neq
y2(j)=y(j)+(delt/2.0)*f1(j)
22 continue
c
call fcn(neq,t2,y2,f2)
c
do 23 j=1,neq
y3(j)=y(j)+(delt/2.0)*f2(j)
23 continue
c
call fcn(neq,t3,y3,f3)
c
do 24 j=1,neq
y4(j)=y(j)+delt*f3(j)
24 continue
c
call fcn(neq,t4,y4,f4)
c
do 30 j=1,neq
yout(j)=y(j)+(delt/6.0)*(f1(j)+2.0*f2(j)+2.0*f3(j)+f4(j))
30 continue
c
return
end
c
subroutine matv12(iflag,n,rm,rmi)
c
gauss-jordon elimination
c
dimension rm(12,12),rmw(12,12),rmi(12,12),chk(12,12),
1 v(12),vw(12),itrak(12)
c
open(1,file='gauss.inp')
open(2,file='gauss.out')
c
write(10,101) n
c 101 format(/'n =',i5)
c
do 40 i=1,n
c do 41 j=1,n
c write(10,422) rm(i,j)
c 422 format(e15.3)

```

```

c 41 continue
c 40 continue
c
c   do 42 i=1,n
c   read(1,423) v(i)
c 423 format(e15.3)
c   vw(i)=v(i)
c 42 continue
c
c   do 20 i=1,n
c   itrak(i)=i
c   do 21 j=1,n
c   rmw(i,j)=rm(i,j)
c   chk(i,j)=0.0
c   rmi(i,j)=0.0
c   if(i.eq.j) rmi(i,j)=1.0
21 continue
20 continue
c
c   do 10 i=1,n
c
c   isav=i
c   pmag=abs(rmw(i,i))
c   do 301 irow=i,n
c   tmpnum=abs(rmw(irow,i))
c   if(tmpnum.gt.pmag) isav=irow
301 continue
c   itrak(i)=isav
c   do 302 jcol=1,n
c   hold=rmw(i,jcol)
c   rmw(i,jcol)=rmw(isav,jcol)
c   rmw(isav,jcol)=hold
c   hold=rmi(i,jcol)
c   rmi(i,jcol)=rmi(isav,jcol)
c   rmi(isav,jcol)=hold
302 continue
c
c   pivot=rmw(i,i)
c   vw(i)=vw(i)/pivot
c
c   do 11 jj=1,n
c   rmi(i,jj)=rmi(i,jj)/pivot
c   rmw(i,jj)=rmw(i,jj)/pivot
11 continue
c
c   do 12 k=1,n
c   if(k.eq.i) go to 12
c   scale=rmw(k,i)
c   vw(k)=vw(k)-scale*vw(i)
c   do 13 j=1,n
c   rmi(k,j)=rmi(k,j)-scale*rmi(i,j)
c   rmw(k,j)=rmw(k,j)-scale*rmw(i,j)
13 continue
12 continue
c
c 10 continue
c
c   go to 99

```

```

c
  chksum=0.0
  do 50 i=1,n
  do 51 j=1,n
  do 52 k=1,n
  chk(i,j)=chk(i,j)+rm(i,k)*rmi(k,j)
52 continue
  if(i.eq.j) chk(i,j)=chk(i,j)-1.0
  chksum=chksum+chk(i,j)**2
51 continue
50 continue
c
  if(iflag.ne.4) go to 99
  ichk=0
  if(chksum.ge.1.0e-12) ichk=-999
  write(4,222) ichk,iflag,n,chksum
222 format(1x,3i5,e15.3)
c
  do 30 i=1,n
  do 31 j=1,n
  write(4,223) i,j,rm(i,j),rmw(i,j),rmi(i,j),chk(i,j)
223 format(1x,2i5,4e15.3)
  31 continue
  30 continue
c
  99 dummy=1.0
c
c
c  do 44 i=1,n
c  write(2,223) i,v(i),vw(i)
c 223 format(1x,i5,2e15.3)
c  44 continue
c
  return
  end
c
  subroutine matv03(iflag,n,rm,rmi)
c
c  gauss-jordan elimination
c
  dimension rm(3,3),rmw(3,3),rmi(3,3),chk(3,3),
1 v(3),vw(3),itrak(3)
c
c  open(1,file='gauss.inp')
c  open(2,file='gauss.out')
c
c  write(10,101) n
c 101 format('/n =',i5)
c
c  do 40 i=1,n
c  do 41 j=1,n
c  write(10,422) rm(i,j)
c 422 format(e15.3)
c  41 continue
c  40 continue
c
c  do 42 i=1,n
c  read(1,423) v(i)
c 423 format(e15.3)

```

```

c   vw(i)=v(i)
c 42 continue
c
c   do 20 i=1,n
c   itrak(i)=i
c   do 21 j=1,n
c   rmw(i,j)=rm(i,j)
c   chk(i,j)=0.0
c   rmi(i,j)=0.0
c   if(i.eq.j) rmi(i,j)=1.0
21 continue
20 continue
c
c   do 10 i=1,n
c
c   isav=i
c   pmag=abs(rmw(i,i))
c   do 301 irow=i,n
c   tmpnum=abs(rmw(irow,i))
c   if(tmpnum.gt.pmag) isav=irow
301 continue
c   itrak(i)=isav
c   do 302 jcol=1,n
c   hold=rmw(i,jcol)
c   rmw(i,jcol)=rmw(isav,jcol)
c   rmw(isav,jcol)=hold
c   hold=rmi(i,jcol)
c   rmi(i,jcol)=rmi(isav,jcol)
c   rmi(isav,jcol)=hold
302 continue
c
c   pivot=rmw(i,i)
c   vw(i)=vw(i)/pivot
c
c   do 11 jj=1,n
c   rmi(i,jj)=rmi(i,jj)/pivot
c   rmw(i,jj)=rmw(i,jj)/pivot
11 continue
c
c   do 12 k=1,n
c   if(k.eq.i) go to 12
c   scale=rmw(k,i)
c   vw(k)=vw(k)-scale*vw(i)
c   do 13 j=1,n
c   rmi(k,j)=rmi(k,j)-scale*rmi(i,j)
c   rmw(k,j)=rmw(k,j)-scale*rmw(i,j)
13 continue
12 continue
c
10 continue
c
c   go to 99
c
c   chksum=0.0
c   do 50 i=1,n
c   do 51 j=1,n
c   do 52 k=1,n
c   chk(i,j)=chk(i,j)+rm(i,k)*rmi(k,j)

```

```
52 continue
   if(i.eq.j) chk(i,j)=chk(i,j)-1.0
   chksum=chksum+chk(i,j)**2
51 continue
50 continue
c
   if(iflag.ne.4) go to 99
   ichk=0
   if(chksum.ge.1.0e-12) ichk=-999
   write(4,222) ichk,iflag,n,chksum
222 format(1x,3i5,e15.3)
c
   do 30 i=1,n
   do 31 j=1,n
   write(4,223) i,j,rm(i,j),rmw(i,j),rmi(i,j),chk(i,j)
223 format(1x,2i5,4e15.3)
   31 continue
   30 continue
c
   99 dummy=1.0
c
c   do 44 i=1,n
c   write(2,223) i,v(i),vw(i)
c 223 format(1x,i5,2e15.3)
c 44 continue
c
   return
   end
```