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# Manual for Automatic Generation of Finite Element Models of Spiral Bevel Gears in Mesh

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## ABSTRACT

The goal of this research is to develop computer programs that generate finite element models suitable for doing 3D contact analysis of faced milled spiral bevel gears in mesh. A pinion tooth and a gear tooth are created and put in mesh.

There are two programs:

1. Points.f
2. Pat.f

Points.f is based on the equation of meshing for spiral bevel gears. It uses machine tool settings to solve for an  $N \times M$  mesh of points on the four surfaces; pinion concave and convex, and gear concave and convex. Points.f creates the file POINTS.OUT, an ASCII file containing  $N \times M$  points for each surface. ( $N$  is the number of node points along the length of the tooth, and  $M$  is nodes on the height.)

Pat.f reads POINTS.OUT and creates the file t1.out. T1.out is a series of PATRAN input commands. In addition to the mesh density on the tooth face, additional user specified variables are the number of finite elements through the thickness, and the number of finite elements along the tooth full fillet. A full fillet is assumed to exist for both the pinion and gear.

This report is based on the theory presented in Army Research Laboratory Report ARL-TR-158 "Contact Stress Analysis of Spiral Bevel Gears Using Nonlinear Finite Element Static Analysis" by G.D. Bibel, A. Kumar and S. Reddy; and AVSCOM Technical Report 91-C-020 "A Method for Determining Spiral-Bevel Gear Tooth Geometry for Finite Element Analysis" by R. F. Handschuh and F. L. Litvin.

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## SUMMARY

The goal of this research is to develop computer programs that generate finite element models suitable for doing 3D contact analysis of faced milled spiral bevel gears in mesh. A pinion tooth and a gear tooth are created and put in mesh.

There are two programs:

1. Points.f
2. Pat.f

Points.f is based on the equation of meshing for spiral bevel gears. It uses machine tool settings to solve for an  $N \times M$  mesh of points on the four surfaces; pinion concave and convex, and gear concave and convex. Points.f creates the file POINTS.OUT, an ASCII file containing  $N \times M$  points for each surface. ( $N$  is the number of node points along the length of the tooth, and  $M$  is nodes on the height.)

NOTE: For Unix based systems, the program titles are case sensitive. All titles are lower case except POINTS.OUT.

Pat.f reads POINTS.OUT and creates the file t1.out. T1.out is a series of PATRAN input commands. In addition to the mesh density on the tooth face, additional user specified variables are the number of finite elements through the thickness, and the number of finite elements along the tooth full fillet. A full fillet is assumed to exist for both the pinion and gear.

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The following topics are covered in this report:

1. A description of the detailed procedure for generating a finite element model.
2. Instructions for inserting the data.
3. A numerical example of input and output.
4. A listing of the programs.
5. Sample plots.

Finite element analysis of spiral bevel gears can be used to determine contact stresses, bending stresses, stiffness for dynamic analysis, load sharing, contact area, and thermal gradients.

## PROCEDURE

1. Prepare the input data for points.f (described elsewhere in this report) for the pinion.
2. Compile and execute points.f
3. During the execution of points.f, the user is prompted for the desired N x M mesh.
4. Execution of points.f creates the file POINTS.OUT. This file will contain N x M points on the pinion concave surface and N x M points on the pinion convex surface. (2 x N x M total points)
5. Prepare the input data for model.f (described elsewhere in this report) for the pinion.
6. Compile and execute model.f.
7. During the execution of model.f, the user is prompted for the desired N x M mesh. These values must be the same used in step 3 above. The user is also prompted for the number of finite elements through the tooth thickness (this must be an even number), and the number of finite elements along the length of 1/2 of the full fillet. Trial and error may be required to obtain finite elements with appropriate aspect ratios.
8. Execution of model.f creates t1.out. This file is suitable for direct input into PATRAN ver 2.5.

**NOTE:** An 8 x 6 mesh is suggested as a practice mesh. Accuracy is affected with coarser meshes. (The increment is too large for the numerical solution)

### NUMERICAL EXAMPLE (SUMMARY)

A 8 x 6 mesh with 4 elements through the tooth thickness and 4 elements in the fillet region will be used as an example.

1. The input data is as shown in the section INPUT DATA: POINTS.F
2. Attachment 1 shows the output from points.f (i. e. the file POINTS.OUT). This file is the X, Y, and Z coordinates of the N x M mesh of points on the four surfaces.
3. The input data from the next step is as shown in the section INPUT DATA: PAT.F
4. Attachment 2 shows the output from Pat.f (i. e. the file t1.out.
5. Attachment 3 shows a typical PATRAN plot after reading t1.out.

INPUT DATA: Points.f

The input data for Points.f is as shown below. (The input data occurs inside of points.f) Each input variable is self explanatory or explained in detail in the reference reports.

The initial guess is very sensitive. The solution technique may converge on another surface if the initial guess is too far from the correct solution.

```

C
C
C
C
C
C-----
C-----
C
C          DESCRIPTION OF INPUT DATA
C-----
C
C          1) RADIUS OF CUTTER, INCHES           (R)
C          2) CRADLE ANGLE, DEGREES             (Q)
C          3) BLADE ANGLE, DEGREES              (PSI)
C          4) CRADLE TO CUTTER DISTANCE, INCHES (S)
C          5) RATIO OF ROLL                      (MCW)
C          6) MACHINE OFFSET, INCHES           (EM)
C          7) VECTOR SUM, INCHES               (LM)
C          8) DEDENDUM ANGLE, DEGREES          (DEDEN)
C          9) PITCH ANGLE, DEGREES             (MU)
C          10) ADDENDUM ANGLE, DEGREES         (ADDAN)
C          11) CLEARANCE, INCHES              (CL)
C          12) MEAN CONE DISTANCE, INCHES     (RL)
C          13) FACE WIDTH, INCHES             (FW)
C          14) INITIAL GUESS FOR SURFACE COORDINATE U ( U(1) )
C          15) INITIAL GUESS FOR SURFACE COORDINATE THETA ( THETA(1) )
C          16) INITIAL GUESS FOR ANGLE OF CRADLE, DEGREES ( PHIC(1) )
C-----
C          INSERT CONCAVE SIDE OF PINION DATA BELOW
C-----
C
C          R          = 2.96562137806
C          Q          = 63.9420304635 * PI/180.0
C          PSI        = 161.954330248 * PI/180.0
C          S          = 2.94780202969
C          MCW        = 0.30838512709

```

```

EM      = 0.154575896
LM      = 0.0384999977874
DEDEN   = 1.566666666 * pi/180
MU      = 18.43333333 * pi/180
ADDAN   = 3.88333334 * pi/180
CL      = 0.03
RL      = 3.191
FW      = 1.0
U(1)    = 9.59703
THETA(1) = 126.83544 * PI/180.0
PHIC(1) = -0.85813 * PI/180.0

```

C

```
ELSEIF (INT .EQ. 2) THEN
```

C-----

C

```
INSERT CONVEX SIDE OF PINION DATA BELOW
```

C-----

C

```

R      = 3.071306157
Q      = 53.9259945467 * PI/180.0
PSI    = 24.337423854 * PI/180.0
S      = 2.80104946
MCW    = 0.3220428536
EM     = -0.17426159493
LM     = -0.0518138227
DEDEN  = 1.566666666 * pi/180
MU     = 18.43333333 * pi/180
ADDAN  = 3.88333334 * pi/180
CL     = 0.03
RL     = 3.191
FW     = 1.0
U(1)   = 7.42534
THETA(1) = 124.43689 * PI/180.0
PHIC(1) = -11.38663 * PI/180.0

```

C

```
ELSEIF (INT .EQ. 3) THEN
```

C-----

C

```
INSERT CONCAVE SIDE OF GEAR DATA BELOW
```

C-----

C

```

R      = 3.0325
Q      = 59.2342023 * PI/180.0
PSI    = 158.0 * PI/180.0
S      = 2.85995004691
MCW    = 0.9508646
EM     = 0.0
LM     = 0.0
DEDEN  = 3.8833333333 * pi/180
MU     = 71.56666666 * pi/180
ADDAN  = 1.56666666 * pi/180
CL     = 0.0366
RL     = 3.191
FW     = 1.0
U(1)   = 8.12602
THETA(1) = 233.98994 * PI/180.0
PHIC(1) = -0.35063 * PI/180.0

```

C-----

C

C

C

C

C

```
ELSE
```

C

C-----

C

```
INSERT CONVEX SIDE OF GEAR DATA BELOW
```

C-----

R = 2.9675  
Q = 59.2342023 \* PI/180.0  
PSI = 22.0 \* PI/180.0  
S = 2.85995004691  
MCW = 0.9508646  
EM = 0.0  
LM = 0.0  
DEDEN = 3.8833333333 \* pi/180  
MU = 71.5666666 \* pi/180  
ADDAN = 1.5666666 \* pi/180  
CL = 0.0366  
RL = 3.191  
FW = 1.0  
U(1) = 7.89156  
THETA(1) = 234.95451 \* PI/180.0  
PHIC(1) = -12.3384 \* PI/180.0

INPUT DATA: Pat. f.

The input data for Model.f is as shown below. Some of the data is redundant with Points.f The new variables are as follows:

1. "ROTCON". ROTCON is the rotation of each convex surface required to obtain the desired top land thickness.

2. "ROTINT". ROTINT is the rotation of the pinion required to eliminate interference with the gear.

3. "ROGEAR". ROGEAR is the rotation of the gear required to place the gear in mesh with the pinion. For the general case, the gear tooth is rotated  $360/(\text{Number of gear teeth}) + 180$  degrees CW about the Z axis (the gear's axis of rotation).

```
-
C
C-----
C          DESCRIPTION OF INPUT DATA FOR PINION
C-----
C
C          1. DEPENDUM, DEGREES                (DEDEN)
C          2. PITCH ANGLE, DEGREES            (MU)
C          3. ROTATION OF CONVEX SURFACE TO
C              CREATE TOP LAND                (ROTCON)
C          4. ROTATION OF PINION TO ELIMINATE
C              INTERFERENCE                   (ROTINT)
C          5. PINION ID, INCHES                (RI)
C          6. CLEARANCE, INCHES               (CL)
C          7. NUMBER OF PINION TEETH          (NTPIN)
C-----
C
C-----
C          INPUT THE PINION DATA BELOW
C-----
C          DEDEN = 1.56666666 * PI/180.0
C          MU    = 18.43333333 * PI/180.0
C          ROTCON = 2.275
C          ROTINT = -3.56
C          RI    = 0.609375
C          CL    = 0.03
C          NTPIN = 12
C-----
```



OUTPUT FROM POINTS.F

X	Y	Z
0.7948185893337920	0.1518771876505158	2.565573009266192
0.8343433613077650	0.1745810495998836	2.552471190313917
0.8720324096583479	0.2042199804427480	2.539369371362535
0.9077908578945182	0.2394490290397444	2.526267552535221
0.9414155876464360	0.2795805696115394	2.513165735668416
0.9726798641190831	0.3241375989552031	2.500063936000037
0.8472371339193625	7.6106029221588933E-02	2.702284801203873
0.8913330776440134	9.5839030874127040E-02	2.688392059145086
0.9342070276559395	0.1231797235370555	2.674499317051919
0.9756155352323542	0.1566714188085960	2.660606575085474
1.015268047213935	0.1955944000191652	2.646713837702351
1.052870943839311	0.2394597732991732	2.632821147263364
0.8920544861387928	-8.7977041450044701E-03	2.838996593145300
0.9405003839933272	7.3083519719827627E-03	2.824312928070127
0.9884537411081434	3.1630276922439470E-02	2.809629262838540
1.035498881976111	6.2620579641409435E-02	2.794945597192247
1.081249167998568	9.9539397524525785E-02	2.780261940615036
1.125338129677023	0.1418941391352297	2.765578408798671
0.9279228340072788	-0.1023212288383641	2.975708385187462
0.9804198623141954	-9.0488151985839593E-02	2.960233797221159
1.033263802256655	-6.9914280082028490E-02	2.944759208992080
1.085845886896256	-4.2211242335634668E-02	2.929284618267694
1.137675976466795	-8.1252212097733256E-03	2.913810043739986
1.188306404191815	3.1855424697372125E-02	2.898335812878913
0.9534599334795802	-0.2037951651625605	3.112420178263912
1.009630926058035	-0.1968645393407975	3.096154666768726
1.067089798650322	-0.1807700720952332	3.079889156026669
1.125017872008955	-0.1571554097480132	3.063623637059750
1.182815359830648	-0.1267574497917443	3.047358144908540
1.239934504589937	-9.0054618527663610E-02	3.031093686081570
0.9672556523581568	-0.3123758786108948	3.249131977522822
1.026644599586983	-0.3109539641202601	3.232075536925217
1.088352545835276	-0.3000651176158047	3.215019104897882
1.151339425325948	-0.2813479710083238	3.197962650909841
1.214890364286590	-0.2555128377780433	3.180906240112322
1.278297192284771	-0.2230290530267571	3.163853372103641
0.9678796662918135	-0.4270252087603694	3.385843803228283
1.029951520163903	-0.4316883253646147	3.367996407956596
1.095449239626837	-0.4267184461595268	3.350149057378801
1.163106632451191	-0.4137081339625599	3.332301654167603
1.232086458109564	-0.3933218937462701	3.314454332645862
1.301293568935084	-0.3660335888044650	3.296621207705554
0.9538905193238456	-0.5464866609459378	3.522555720376076
1.018031477753651	-0.5577745718372567	3.503917280198983
1.086763175986946	-0.5594158588267257	3.485279016743563
1.158596913336253	-0.5529133643964257	3.466640634659134
1.232554428724539	-0.5388625992810234	3.448002511532153
1.306217203742137	-0.5177479993723693	3.429430372498238
0.7093463178422439	0.3893983454546772	2.565573009266191
0.7570852600711056	0.3917005187907718	2.552471190313766
0.8073029755824992	0.3878249981807325	2.539369371359211
0.8593909679113807	0.3779778338261695	2.526267552392368
0.9128138134481132	0.3622148457047225	2.513165733397398
0.9670614194895887	0.3405352495955354	2.500063914362740
0.7805547654008799	0.3381377633245926	2.702284801203850
0.8313192150683369	0.3355117554273983	2.688392059127966
0.8840811061706690	0.3260622820926806	2.674499317054876
0.9382129090097685	0.3100453874934890	2.660606574980783
0.9931445219848133	0.2875595701230784	2.646713832903523
1.048324166687691	0.2586450939788132	2.632821090805444
0.8483132970638206	0.2760491911215923	2.838996593141508
0.9015956233205106	0.2678053743188284	2.824312927885464
0.9562796868411379	0.2521317789571000	2.809629262692835
1.011723722807169	0.2293346362776858	2.794945597542682
1.067325789653079	0.1995595783460700	2.780261932355890
1.122494542284766	0.1628943693243237	2.765578267158041

0.9112000448284689	0.2030391581389535	2.975708385079163
0.9663724749316263	0.1885085186004414	2.960233796271262
1.022236225128360	0.1659976000986125	2.944759207797051
1.078139321839011	0.1358626773835785	2.929284619894748
1.133450935693196	9.8300989821880069E-02	2.913810031777249
1.187542779161388	5.3454488313127157E-02	2.898335443486139
0.9676895991379796	0.1191435063835695	3.112420177016817
1.023995422930553	9.7691650985565203E-02	3.096154663323241
1.080168552957352	6.7782050056511611E-02	3.079889150748298
1.135549961729417	2.9820889650890691E-02	3.063623641171534
1.189482972857256	-1.5938341746537521E-02	3.047358130942706
1.241305512978413	-6.9292504478944305E-02	3.031092619792399
1.016149494629492	2.4546941529382415E-02	3.249131968954469
1.072693870906420	-4.4094230428219916E-03	3.232075526708658
1.128170570501692	-4.2209828439173868E-02	3.215019087512731
1.181915774012974	-8.8397895323604203E-02	3.197962659109970
1.233250099226129	-0.1426588841462646	3.180906229149712
1.281481427875818	-0.2047210348378159	3.163849795972270
1.054836149594651	-8.0393756502517454E-02	3.385843760892120
1.110576450723173	-0.1173673033750138	3.367996381370604
1.164207315546032	-0.1634608596042426	3.350149009219072
1.215061572522443	-0.2181667004477261	3.332301668710605
1.262440437691158	-0.2811032336663852	3.314454324809642
1.305626160434559	-0.3519220612269351	3.296606971745099
1.081890093168536	-0.1951217417487592	3.522555552829777
1.135625698876967	-0.2405311921112059	3.503917217031341
1.186109140444834	-0.2952059400453120	3.485278897558544
1.232670689693987	-0.3585843827438959	3.466640659723548
1.274595758431425	-0.4302115809299476	3.448002414715995
1.311146184992092	-0.5096536842811183	3.429364146542768
2.474433967420987	-0.3395653327372070	0.9856358798469023
2.487839996829133	-0.3593061900500794	0.9465879479135923
2.500980732115327	-0.3799719362136913	0.9075400160259967
2.513847962185435	-0.4014972153625989	0.8684920851879474
2.526433333215689	-0.4238257450684864	0.8294441631803695
2.538728501263516	-0.4469082097766504	0.7903962834276070
2.615744367457404	-0.2713527297527838	1.039882343666109
2.630668874615893	-0.2921776971646133	0.9983126342013517
2.645336856855221	-0.3140021877370152	0.9567429270473953
2.659736900244837	-0.3367554455147062	0.9151732405016411
2.673857752554951	-0.3603767778219593	0.8736036480711737
2.687688379068866	-0.3848131384418187	0.8320343503411255
2.755122082966633	-0.1939252488334882	1.094128807487018
2.771646356120490	-0.2158264544757134	1.050037320781535
2.787926437149529	-0.2388005015425003	1.005945850025553
2.803947251406170	-0.2627715238015491	0.9618544915078790
2.819694200468521	-0.2876746263983043	0.9177635422435383
2.835153088849297	-0.3134531506865259	0.8736736400533243
2.892115805626759	-0.1070309492253978	1.148375271344924
2.910326750723583	-0.1300043557812005	1.101762007915943
2.928309186669705	-0.1541221288023844	1.055148803591732
2.946043871332245	-0.1793036410217184	1.008535978909207
2.963512305696952	-0.2054800085262900	0.9619243699325180
2.980696572015054	-0.2325910821084665	0.9153154443440815
3.026234802111897	-1.0397603116659048E-02	1.202621735548316
3.046226387571472	-3.4443711328922432E-02	1.153486695724431
3.066008199637873	-5.9703409974563026E-02	1.104351817871708
3.085556228980730	-8.6091707633022540E-02	1.055217942501711
3.104847356582463	-0.1135359377283138	1.006086988192335
3.123859380461631	-0.1419726571295392	0.9569616304362697
3.156942158964726	9.6270882267980528E-02	1.256868201705318
3.178817192398615	7.1146146344736038E-02	1.205211384146218
3.200503834343097	4.4741446463306910E-02	1.153554939872925
3.221972538278004	1.7145708246413704E-02	1.101900776270329
3.243194610216827	-1.1564815230486136E-02	1.050252743854398
3.264143329575414	-4.1323831199262528E-02	0.9986146558233269

3.283646305240354	0.2132989412203852	1.311114675992770
3.307518658058060	0.1870830974730224	1.256936072960456
3.331226092948566	0.1595243725147912	1.202758242897250
3.354732453389843	0.1307151794108270	1.148585121565755
3.378002211439905	0.1007351583096741	1.094423714581283
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HPAT,	12,2P,,	12,	17		

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 GRID, 201,, 0.604492/ 0.076986/ 2.565573  
 LINE, 25,ARC,5(0)/1/ 20.22185, 201  
 GRID, 203,, 0.609145/ 0.016728/ 2.702285  
 LINE, 26,ARC,5(0)/1/ 20.56433, 203  
 GRID, 205,, 0.607796/ -0.043834/ 2.838997  
 LINE, 27,ARC,5(0)/1/ 20.86543, 205  
 GRID, 207,, 0.600388/ -0.104272/ 2.975708  
 LINE, 28,ARC,5(0)/1/ 21.12931, 207  
 GRID, 209,, 0.586856/ -0.164129/ 3.112420  
 LINE, 29,ARC,5(0)/1/ 21.35904, 209  
 GRID, 211,, 0.567137/ -0.222920/ 3.249132  
 LINE, 30,ARC,5(0)/1/ 21.55671, 211  
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 LINE, 32,ARC,5(0)/1/ 21.85998, 215  
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 LINE, 49/ 50,BR,.5, 33  
 LINE, 34 ,ARC,0/0/0/0/0/1/ -9.778, 201  
 LINE, 81/ 82,BR,.5, 34  
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 LINE, 35,ARC, 0.84937/-0.04667/0/ 0.84937/-0.04667/1.0/ 170.56433, 7  
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 LINE, 41,ARC, 0.91651/-0.33260/0/ 0.91651/-0.33260/1.0/ 171.35904, 25  
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 LINE, 42 ,ARC,0/0/0/0/0/1/ -8.641, 209  
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 LINE, 102,ST,, 238, 240  
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 LINE, 118,ST,, 237, 239  
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 NAME,PI 1  
 SET,ACTIVE,NONE  
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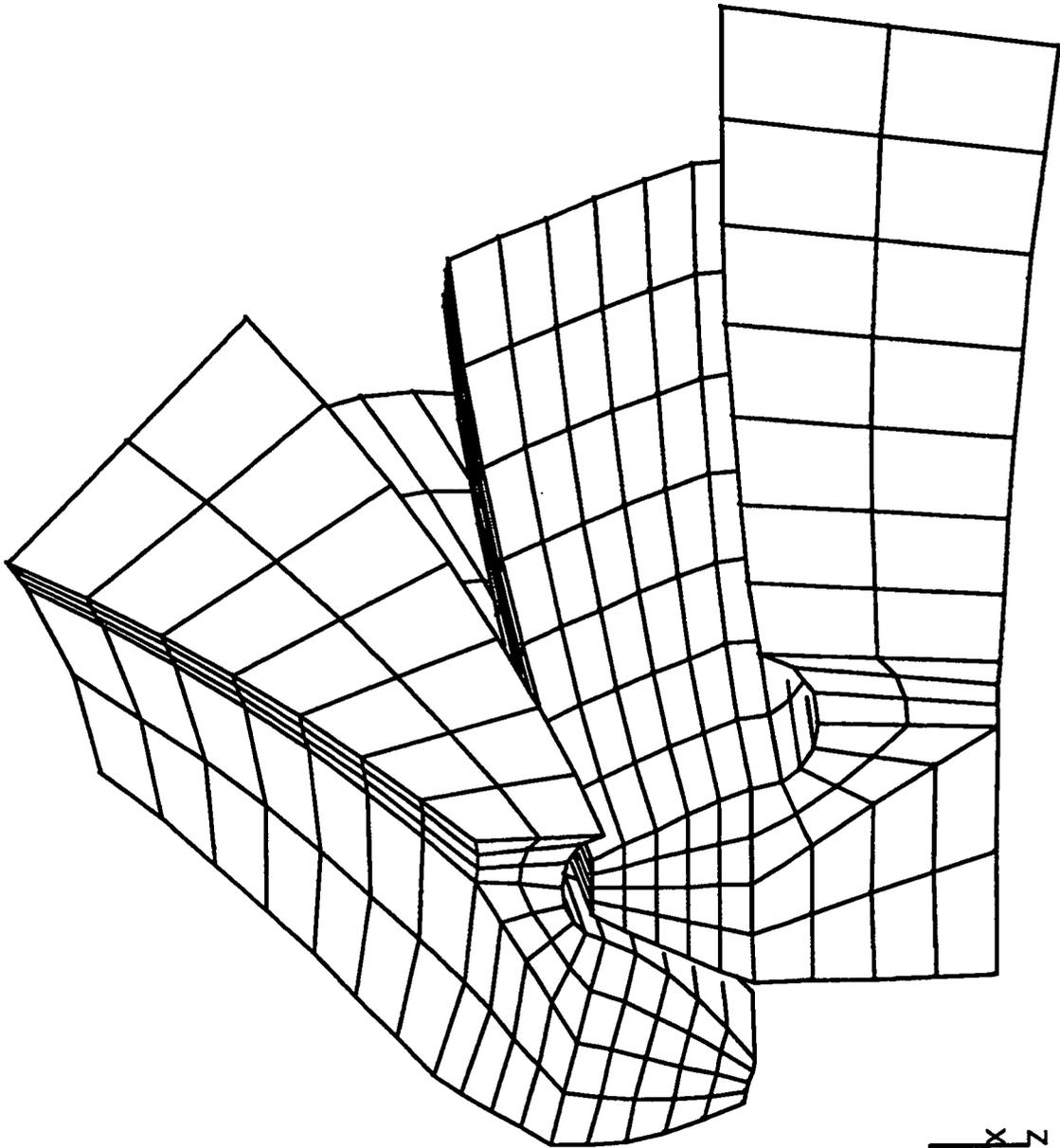
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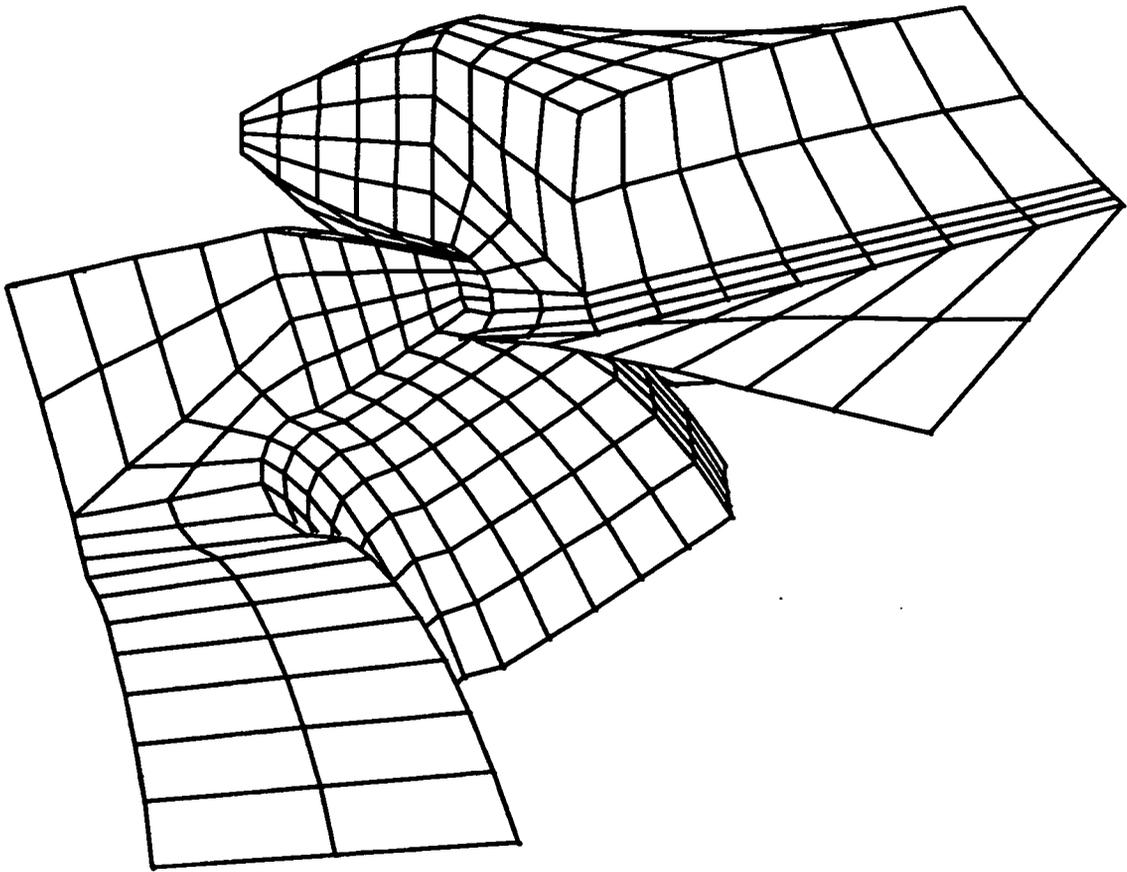
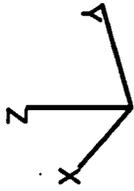
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 LINE, 161,ARC,0/0/0/-2.4908/-0.1849/ 0.985636/-175.880, 97  
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 LINE, 207 ,ARC,0/0/0/0/0/1/ 3.889, 263  
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 HPAT, 104 ,2P,, 118, 119  
 HPAT, 111 ,2P,, 126, 127  
 HPAT, 98 ,2P,, 111, 112  
 HPAT, 105 ,2P,, 119, 120  
 HPAT, 112 ,2P,, 127, 128  
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 SET,ACTIVE,NONE  
 NAME,PI 1,PL  
 MESH,H 1T 35,HEX,N,1/ 4/1/ 4/1  
 MESH,H 36T 49,HEX,N, 2/ 4/ 2/ 4/1  
 MESH,H 50T 56,HEX,N,3/ 2/3/ 2/1  
 NAME,PIN  
 SET,ACTIVE,NONE  
 NAME,GE 1,PLOT  
 MESH,H 57T 91,HEX,N,1/ 4/1/ 4/1  
 MESH,H 92T 105,HEX,N, 4/ 2/ 4/ 2/1  
 MESH,H 106T 112,HEX,N, 2/3/ 2/3/1

NAME, GEAR  
GR, 1T#, DEL  
NAME, PINION, RO, 4(0)/1/0/-90, PIN  
NAME, PINION, PL

TYPICAL FE MESH





```

C                                     POINTS.F
C-----
C      POINTS.F GENERATES N BY M POINTS FOR THE PINION & GEAR SURFACES
C      POINTS.OUT => N BY M POINTS
C      (MAIN PROGRAM)
C
C      COMMON/CONST/PI,R,Q,MU,DEDEN,PSI,S,MCW,LM,EM,INC
C      DIMENSION XYZ(4),U(51),THETA(51),PHIC(51),D(3,3),F(3),Y(3)
C      DIMENSION RBAR(50,50),ZBAR(50,50),X1(50,50),X2(50,50),X3(50,50)
C      DOUBLE PRECISION MU,A1,B1,C1,D1,E1,AA,BB,CC,RV,MCW,Q,PSI,PI
C      DOUBLE PRECISION THETA,D,F,Y,GAMMA,DEDEN,R,S,TAU,EM,LM,PHIC
C      DOUBLE PRECISION XYZ,U,INC,ZBAR,RBAR,X1,X2,X3,LV,ADDAN,CL,RL,FW
C      INTEGER N1,N2,N3,M,UU,T,INT,BBB,CCC,SS
C
C      WRITE(*,(''PLEASE ENTER THE GRID PATTERN REQUIRED.''/
C      *''FOR EXAMPLE: FOR A 7X8 PATTERN, ENTER 7 AND RETURN''/
C      *''THEN ENTER 8 '''))
C
C      READ(*,*)BBB
C      READ(*,*)CCC
C
C      PI    = 4.0 * ATAN(1.0)
C      INC   = 0.1
C      N1    = 11
C      N2    = 3
C      N3    = 4
C
C      DO 5 INT = 1,4
C
C      IF (INT .EQ. 1) THEN
C
C
C
C-----
C      DESCRIPTION OF INPUT DATA
C-----
C
C      1) RADIUS OF CUTTER, INCHES           (R)
C      2) CRADLE ANGLE, DEGREES             (Q)
C      3) BLADE ANGLE, DEGREES              (PSI)
C      4) CRADLE TO CUTTER DISTANCE, INCHES (S)
C      5) RATIO OF ROLL                      (MCW)
C      6) MACHINE OFFSET, INCHES           (EM)
C      7) VECTOR SUM, INCHES               (LM)
C      8) DEDENDUM ANGLE, DEGREES           (DEDEN)
C      9) PITCH ANGLE, DEGREES             (MU)
C      10) ADDENDUM ANGLE, DEGREES          (ADDAN)
C      11) CLEARANCE, INCHES                (CL)
C      12) MEAN CONE DISTANCE, INCHES      (RL)
C      13) FACE WIDTH, INCHES              (FW)
C      14) INITIAL GUESS FOR SURFACE COORDINATE U ( U(1) )
C      15) INITIAL GUESS FOR SURFACE COORDINATE THETA ( THETA(1) )
C      16) INITIAL GUESS FOR ANGLE OF CRADLE, DEGREES ( PHIC(1) )
C-----
C      INSERT CONCAVE SIDE OF PINION DATA BELOW
C-----
C
C      R    = 2.96562137806
C      Q    = 63.9420304635 * PI/180.0
C      PSI  = 161.954330248 * PI/180.0
C      S    = 2.94780202969
C      MCW  = 0.30838512709

```

```

EM      = 0.154575896
LM      = 0.0384999977874
DEDEN   = 1.56666666 * pi/180
MU      = 18.4333333 * pi/180
ADDAN   = 3.8833334 * pi/180
CL      = 0.03
RL      = 3.191
FW      = 1.0
U(1)    = 9.59703
THETA(1) = 126.83544 * PI/180.0
PHIC(1) = -0.85813 * PI/180.0

```

C

```
ELSEIF (INT .EQ. 2) THEN
```

```

-----
C-----
C      INSERT CONVEX SIDE OF PINION DATA BELOW
C-----
C

```

```

R      = 3.071306157
Q      = 53.9259945467 * PI/180.0
PSI    = 24.337423854 * PI/180.0
S      = 2.80104946
MCW    = 0.3220428536
EM     = -0.17426159493
LM     = -0.0518138227
DEDEN  = 1.56666666 * pi/180
MU     = 18.4333333 * pi/180
ADDAN  = 3.8833334 * pi/180
CL     = 0.03
RL     = 3.191
FW     = 1.0
U(1)   = 7.42534
THETA(1) = 124.43689 * PI/180.0
PHIC(1) = -11.38663 * PI/180.0

```

C

```
ELSEIF (INT .EQ. 3) THEN
```

```

-----
C-----
C      INSERT CONCAVE SIDE OF GEAR DATA BELOW
C-----
C

```

```

R      = 3.0325
Q      = 59.2342023 * PI/180.0
PSI    = 158.0 * PI/180.0
S      = 2.85995004691
MCW    = 0.9508646
EM     = 0.0
LM     = 0.0
DEDEN  = 3.8833333333 * pi/180
MU     = 71.5666666 * pi/180
ADDAN  = 1.5666666 * pi/180
CL     = 0.0366
RL     = 3.191
FW     = 1.0
U(1)   = 8.12602
THETA(1) = 233.98994 * PI/180.0
PHIC(1) = -0.35063 * PI/180.0

```

```

-----
C-----
C
C
C
C
C

```

```
ELSE
```

```

-----
C-----
C      INSERT CONVEX SIDE OF GEAR DATA BELOW
C-----
C

```

```

C
R      = 2.9675
Q      = 59.2342023 * PI/180.0
PSI    = 22.0 * PI/180.0
S      = 2.85995004691
MCW    = 0.9508646
EM     = 0.0
LM     = 0.0
DEDEN  = 3.8833333333 * pi/180
MU     = 71.5666666 * pi/180
ADDAN  = 1.5666666 * pi/180
CL     = 0.0366
RL     = 3.191
FW     = 1.0
U(1)   = 7.89156
THETA(1) = 234.95451 * PI/180.0
PHIC(1) = -12.3384 * PI/180.0
ENDIF

C
OPEN(UNIT=900,FILE='POINTS.OUT',STATUS='UNKNOWN')

C
DO 10 UU = 1, BBB
DO 20 T = 1, CCC

C
CALL STEPZR(ZBAR,RBAR,UU,T,int,BBB,CCC,deden,mu,addan,cl,rl,fw)

C
SS = BBB - 1
DO 100 M = 1, SS

C
CALL DIFF(U,THETA,PHIC,M,D,N1,N2,UU,T,ZBAR,RBAR,INT)

C
IF ((INT .EQ. 1).OR.(INT .EQ. 2)) THEN
    TAU = (THETA(M)) - Q + (PHIC(M))
    GAMMA = MU - DEDEN

C
ELSEIF ((INT .EQ. 3).OR.(INT .EQ. 4)) THEN
    TAU = (THETA(M)) + Q - (PHIC(M))
    GAMMA = MU - DEDEN
ENDIF

C
C (THE FIRST EQUATION. (EQUATION OF MESHING FOR LEFT HAND PINION))
C
1 A1 = ((U(M))-R*(COS(PSI)*COS(PSI)/SIN(PSI)))
   *COS(GAMMA)*SIN(TAU)
B1 = S*(MCW-SIN(GAMMA))*COS(PSI)*SIN(THETA(M))
C1 = S*COS(GAMMA)*SIN(PSI)*SIN(Q-(PHIC(M)))
D1 = EM*(COS(GAMMA)*SIN(PSI)+SIN(GAMMA)*COS(PSI)*COS(TAU))
E1 = LM*SIN(GAMMA)*COS(PSI)*SIN(TAU)
IF ((INT .EQ. 1).OR.(INT .EQ. 2)) THEN
    LV = A1 + B1 - C1 + D1 - E1
    AA = LV
ELSEIF ((INT .EQ. 3).OR.(INT .EQ. 4)) THEN
    RV = A1 + B1 + C1 - D1 - E1
    AA = RV
ENDIF

C
C (THE SECOND EQUATION. ZW - Z = 0)
C
CALL TRANSF(U,THETA,PHIC,M,XYZ,N3,N1,INT)

C
BB = XYZ(3) - ZBAR(UU,T)

C
C (THE THIRD EQUATION. R - SQRT( X*X + Y*Y ) = 0)
C
CC = RBAR(UU,T) - SQRT(XYZ(1)*XYZ(1) + XYZ(2)*XYZ(2))

```

```

      F(1) = -AA
      F(2) = -BB
      F(3) = -CC
C
      CALL GAUSS(D,F,Y,N2)
C
      U(M+1) = U(M) + Y(1)
      THETA(M+1) = THETA(M) + Y(2)
      PHIC(M+1) = PHIC(M) + Y(3)
100  CONTINUE
C
      X1(UU,T) = XYZ(1)
      X2(UU,T) = XYZ(2)
      X3(UU,T) = XYZ(3)
C
      WRITE(900,*)X1(UU,T),X2(UU,T),X3(UU,T)
C
20  CONTINUE
10  CONTINUE
C
5  CONTINUE
   CLOSE(900,STATUS='KEEP')
C
   STOP
   END
C
   SUBROUTINE DIFF(X1,X2,X3,M,D,N1,N2,UU,T,ZBAR,RBAR,INT)
C
C   (THE VARIABLES X1,X2,X3; LOCAL TO THIS PROCEDURE; REPRESENT
C   U, THETA AND PHIC. )
C
   COMMON/CONST/PI,R,Q,MU,DEDEN,PSI,S,MCW,LM,EM,INC
   DIMENSION X1(N1),X2(N1),X3(N1),A(5,3),B(5,3),C(5,3),RVAL(5,3)
   DIMENSION XX1(51),XX2(51),XX3(51),D(N2,N2),XYZ(4),ZBAR(50,50)
   DIMENSION RBAR(50,50),LVAL(5,3)
   INTEGER I,J,L,UU,T
   DOUBLE PRECISION RVAL,A,B,C,K,H1,H2,H3,TAU,GAMMA,A1,B1,C1,D1
   DOUBLE PRECISION MU,DEDEN,PI,LM,MCW,X1,X2,X3,XX1,XX2,XX3,D
   DOUBLE PRECISION E1,INC,R,PSI,XYZ,EM,Q,S,ZBAR,RBAR,LVAL
C
C   (H1,H2,H3 ARE THE INCREMENTS ADDED TO THE)
C   (VAR X1,X2,X3 DURING THE NUMERICAL DIFF. )
C   (A1,B1,C1,D1,E1 INTERMEDIATE VALUES FOR EQU. OF MESHING)
C
   DO 201 I = 1,5
      L = I - 3
      K = L/2.0
C
C   (K IS THE MULTIPLIER ON THE INCREMENT "INC".)
C
      DO 205 J = 1,3
C
         IF (J .EQ. 1) THEN
            H1 = INC
            H2 = 0.
            H3 = 0.
         ELSE IF (J .EQ. 2) THEN
            H1 = 0.
            H2 = INC
            H3 = 0.
         ELSE
            H1 = 0.
            H2 = 0.
            H3 = INC
         ENDIF
C

```

```

C      (* INSERT THE THREE EQUATIONS TO BE DIFFERENTIATED HERE *)
C      ( ADD K*H1, K*H2, K*H3 TO EACH VARIABLE X1,X2,X3 )
C
      IF ((INT .EQ. 1).OR.(INT .EQ. 2)) THEN
          TAU = (X2(M)+K*H2) - Q + (X3(M)+K*H3)
          GAMMA = MU - DEDEN
      ELSEIF ((INT .EQ. 3).OR.(INT .EQ. 4)) THEN
          TAU = (X2(M)+K*H2) + Q - (X3(M)+K*H3)
          GAMMA = MU - DEDEN
      ENDIF
C
C      (THE FIRST EQUATION. (EQUATION OF MESHING FOR LEFT HAND PINION))
C
      A1 = ((X1(M)+K*H1)-R*(COS(PSI)*COS(PSI)/SIN(PSI)))
      *COS(GAMMA)*SIN(TAU)
      B1 = S*(MCW-SIN(GAMMA))*COS(PSI)*SIN(X2(M)+K*H2)
      C1 = S*COS(GAMMA)*SIN(PSI)*SIN(Q-(X3(M)+K*H3))
      D1 = EM*(COS(GAMMA)*SIN(PSI) + SIN(GAMMA)*COS(PSI)*COS(TAU))
      E1 = LM*SIN(GAMMA)*COS(PSI)*SIN(TAU)
      IF ((INT .EQ. 1).OR.(INT .EQ. 2)) THEN
          LVAL(I,J) = A1 + B1 - C1 + D1 - E1
          A(I,J) = LVAL(I,J)
      ELSEIF ((INT .EQ. 3).OR.(INT .EQ. 4)) THEN
          RVAL(I,J) = A1 + B1 + C1 - D1 - E1
          A(I,J) = RVAL(I,J)
      ENDIF
C
C      (THE SECOND EQUATION. ZW - Z = 0)
C
      XX1(M) = X1(M) + K*H1
      XX2(M) = X2(M) + K*H2
      XX3(M) = X3(M) + K*H3
C
      CALL TRANSF(XX1, XX2, XX3,M,XYZ,N3,N1,INT)
C
      B(I,J) = XYZ(3) - ZBAR(UU,T)
C
C      (THE THIRD EQUATION. R - SQRT(X*X + Y*Y) = 0)
C
      C(I,J) = RBAR(UU,T) - SQRT(XYZ(1)*XYZ(1) + XYZ(2)*XYZ(2))
205      CONTINUE
C
201      CONTINUE
C
      DO 210 I = 1,3
          D(1,I) = -(A(5,I) - 8*A(4,I) - A(1,I) + 8*A(2,I))/(6*INC)
          D(2,I) = -(B(5,I) - 8*B(4,I) - B(1,I) + 8*B(2,I))/(6*INC)
          D(3,I) = -(C(5,I) - 8*C(4,I) - C(1,I) + 8*C(2,I))/(6*INC)
210      CONTINUE
C
      RETURN
      END
C
C
      SUBROUTINE TRANSF( X1,X2,X3,M,XYZ,N3,N1,INT)
C
      COMMON/CONST/PI,R,Q,MU,DEDEN,PSI,S,MCW,LM,EM,INC
      DIMENSION X1(N1),X2(N1),X3(N1),A(4),REST1(4,4)
      DIMENSION REST2(4,4),REST3(4,4),REST4(4,4),MSC(4,4),MMS(4,4)
      DIMENSION MPM(4,4),MAP(4,4),MWA(4,4),XYZ(N3)
      DOUBLE PRECISION INC,PI,MCW,Q,LM,MU,PSI,MSC,MMS,MPM,MAP,MWA
      DOUBLE PRECISION REST1,REST2,REST3,REST4,DEDEN,S,R,EM,PHIW
      DOUBLE PRECISION X1,X2,X3,A,XYZ
      INTEGER I,J,K
C
      DO 300 I = 1,4

```

```

C
DO 310 J = 1,4
    REST1(I,J)=0
    REST2(I,J)=0
    REST3(I,J)=0
    REST4(I,J)=0
    MSC(I,J)=0
    MMS(I,J)=0
    MPM(I,J)=0
    MAP(I,J)=0
    MWA(I,J)=0
310 CONTINUE
C
300 CONTINUE
C
        PHIW = X3(M)/MCW
C
C      ( THE COORDINATE TRANSFORMATIONS )
C
IF ((INT .EQ. 1).OR.(INT .EQ. 2)) THEN
    MSC(1,1) = 1.0
    MSC(2,2) = COS(Q)
    MSC(2,3) = -SIN(Q)
    MSC(2,4) = -S*SIN(Q)
    MSC(3,2) = +SIN(Q)
    MSC(3,3) = COS(Q)
    MSC(3,4) = S*COS(Q)
    MSC(4,4) = 1.0
C
    MPM(1,1) = COS(DEDEN)
    MPM(1,3) = -SIN(DEDEN)
    MPM(1,4) = -LM*SIN(DEDEN)
    MPM(2,2) = 1.0
    MPM(2,4) = +EM
    MPM(3,1) = SIN(DEDEN)
    MPM(3,3) = COS(DEDEN)
    MPM(3,4) = LM*COS(DEDEN)
    MPM(4,4) = 1.0
C
    MMS(1,1) = 1.0
    MMS(2,2) = COS(X3(M))
    MMS(2,3) = +SIN(X3(M))
    MMS(3,2) = -SIN(X3(M))
    MMS(3,3) = COS(X3(M))
    MMS(4,4) = 1.0
C
    MAP(1,1) = COS(MU)
    MAP(1,3) = SIN(MU)
    MAP(2,2) = 1.0
    MAP(3,1) = -SIN(MU)
    MAP(3,3) = COS(MU)
    MAP(4,4) = 1.0
C
    MWA(1,1) = COS(PHIW)
    MWA(1,2) = +SIN(PHIW)
    MWA(2,1) = -SIN(PHIW)
    MWA(2,2) = COS(PHIW)
    MWA(3,3) = 1.0
    MWA(4,4) = 1.0
C
ELSEIF ((INT .EQ. 3).OR.(INT .EQ. 4)) THEN
C
    MSC(1,1) = 1.0
    MSC(2,2) = COS(Q)
    MSC(2,3) = +SIN(Q)
    MSC(2,4) = +S*SIN(Q)

```

```

MSC(3,2) = -SIN(Q)
MSC(3,3) = COS(Q)
MSC(3,4) = S*COS(Q)
MSC(4,4) = 1.0
C
MPM(1,1) = COS(DEDEN)
MPM(1,3) = -SIN(DEDEN)
MPM(1,4) = -LM*SIN(DEDEN)
MPM(2,2) = 1.0
MPM(2,4) = -EM
MPM(3,1) = SIN(DEDEN)
MPM(3,3) = COS(DEDEN)
MPM(3,4) = LM*COS(DEDEN)
MPM(4,4) = 1.0
C
MMS(1,1) = 1.0
MMS(2,2) = COS(X3(M))
MMS(2,3) = -SIN(X3(M))
MMS(3,2) = +SIN(X3(M))
MMS(3,3) = COS(X3(M))
MMS(4,4) = 1.0
C
MAP(1,1) = COS(MU)
MAP(1,3) = SIN(MU)
MAP(2,2) = 1.0
MAP(3,1) = -SIN(MU)
MAP(3,3) = COS(MU)
MAP(4,4) = 1.0
C
MWA(1,1) = COS(PHIW)
MWA(1,2) = -SIN(PHIW)
MWA(2,1) = +SIN(PHIW)
MWA(2,2) = COS(PHIW)
MWA(3,3) = 1.0
MWA(4,4) = 1.0
C
ENDIF
C
C
C
C
( THE MATRIX MULTIPLICATIONS )
DO 320 I = 1,4
  DO 325 J = 1,4
    DO 330 K = 1,4
      REST1(I,J) = REST1(I,J) + MMS(I,K)*MSC(K,J)
    CONTINUE
  CONTINUE
CONTINUE
330
325
320
C
DO 335 I = 1,4
  DO 340 J = 1,4
    DO 345 K = 1,4
      REST2(I,J) = REST2(I,J) + MPM(I,K)*REST1(K,J)
    CONTINUE
  CONTINUE
CONTINUE
345
340
335
C
DO 350 I = 1,4
  DO 355 J = 1,4
    DO 360 K = 1,4
      REST3(I,J) = REST3(I,J) + MAP(I,K)*REST2(K,J)
    CONTINUE
  CONTINUE
CONTINUE
360
355
350
C
DO 365 I = 1,4
  DO 370 J = 1,4

```

```

          DO 375 K = 1,4
          REST4(I,J) = REST4(I,J) + MWA(I,K)*REST3(K,J)
375      CONTINUE
370      CONTINUE
365      CONTINUE
C
      DO 380 I = 1,4
      XYZ(I) = 0
380      CONTINUE
C
          A(1) = R*COS(PHI)/SIN(PHI)-X1(M)*COS(PHI)
          A(2) = X1(M)*SIN(PHI)*SIN(X2(M))
          A(3) = X1(M)*SIN(PHI)*COS(X2(M))
          A(4) = 1.0
C
      DO 385 K = 1,4
      DO 390 I = 1,4
      XYZ(K) = XYZ(K) + REST4(K,I)*A(I)
390      CONTINUE
385      CONTINUE
C
      RETURN
      END
C
C
      SUBROUTINE GAUSS(D,F,Y,N2)
C
      DIMENSION D(N2,N2),F(N2),Y(N2)
      DOUBLE PRECISION PIVOT,MULT,TOP,D,F,Y
      INTEGER I,J,K,N
C
      N = 3
C
      DO 400 J = 1,N-1
      PIVOT = D(J,J)
C
      DO 410 I = J+1,N
      MULT = D(I,J)/PIVOT
C
          DO 420 K = J+1,N
          D(I,K) = D(I,K) - MULT * D(J,K)
          F(I) = F(I) - MULT * F(J)
420      CONTINUE
C
410      CONTINUE
C
          Y(N) = F(N)/D(N,N)
      DO 430 I = N-1,1,-1
      TOP = F(I)
      DO 440 K = I+1,N
      TOP = TOP - D(I,K) * Y(K)
          Y(I) = TOP/D(I,I)
440      CONTINUE
C
430      CONTINUE
C
400      CONTINUE
C
      RETURN
      END
C
C
      Subroutine stepzr(zbar,rbar,uu,t,int,bbb,ccc,deden,mu,addan
* ,cl,rl,fw)
C
      DIMENSION ZBAR(50,50),RBAR(50,50)

```

```

DOUBLE PRECISION ZPITCH,ZROOT1,ZM1,ZMX,ZINC1,ZM, RM,G,G9,Z,R
DOUBLE PRECISION ZBAR,RBAR,DEDEN,ADDAN,MU,CL,RL,FW
INTEGER DZ1,DR1,UU,T,BBB,CCC
PI      = 4.0*ATAN(1.0)

```

C

```

ZPITCH = RL - FW/2.0
ZROOT1 = ZPITCH * COS(DEDEN)
ZM1     = ZROOT1 * COS(MU - DEDEN)
ZMX     = (ZROOT1 + FW) * COS(MU - DEDEN)
ZINC1   = (ZMX - ZM1)/(BBB - 1)
Z       = 0.
R       = 0.

```

C

```

DZ1     = (UU - 1)
ZM      = ZM1 + DZ1*ZINC1 - CL * SIN(MU -DEDEN)
RM      = ZM * TAN(MU - DEDEN) + CL/COS(MU - DEDEN)
G       = ZM * TAN(ADDAN + DEDEN)/COS(MU - DEDEN) - CL
G9      = G/(ccc - 1)

```

C

C

```

dr1 = (T-1)
Zbar(uu,t) = zm - dr1*g9*sin(mu-deden)
rbar(uu,t) = rm + dr1*g9*cos(mu-deden)

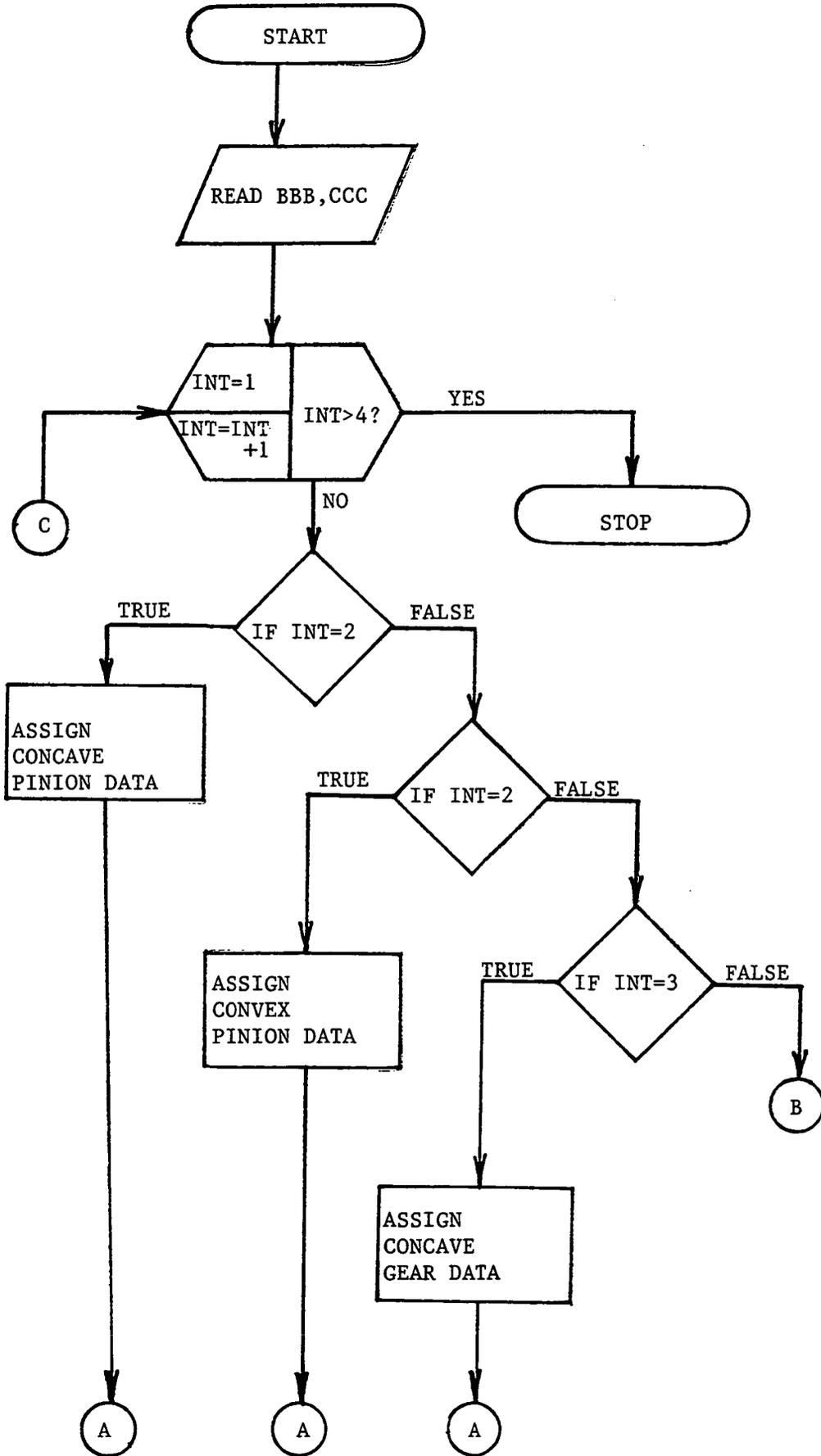
```

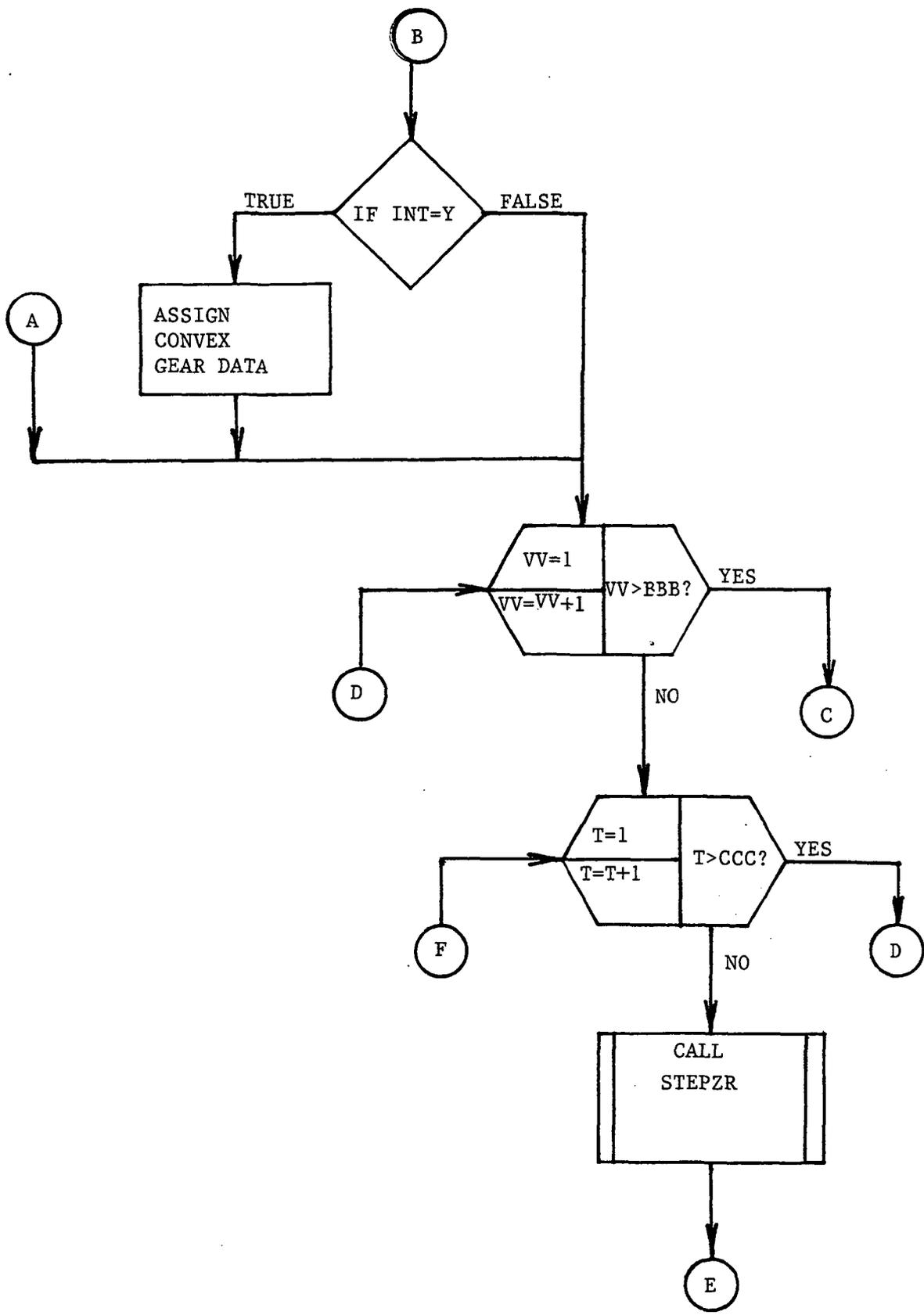
```

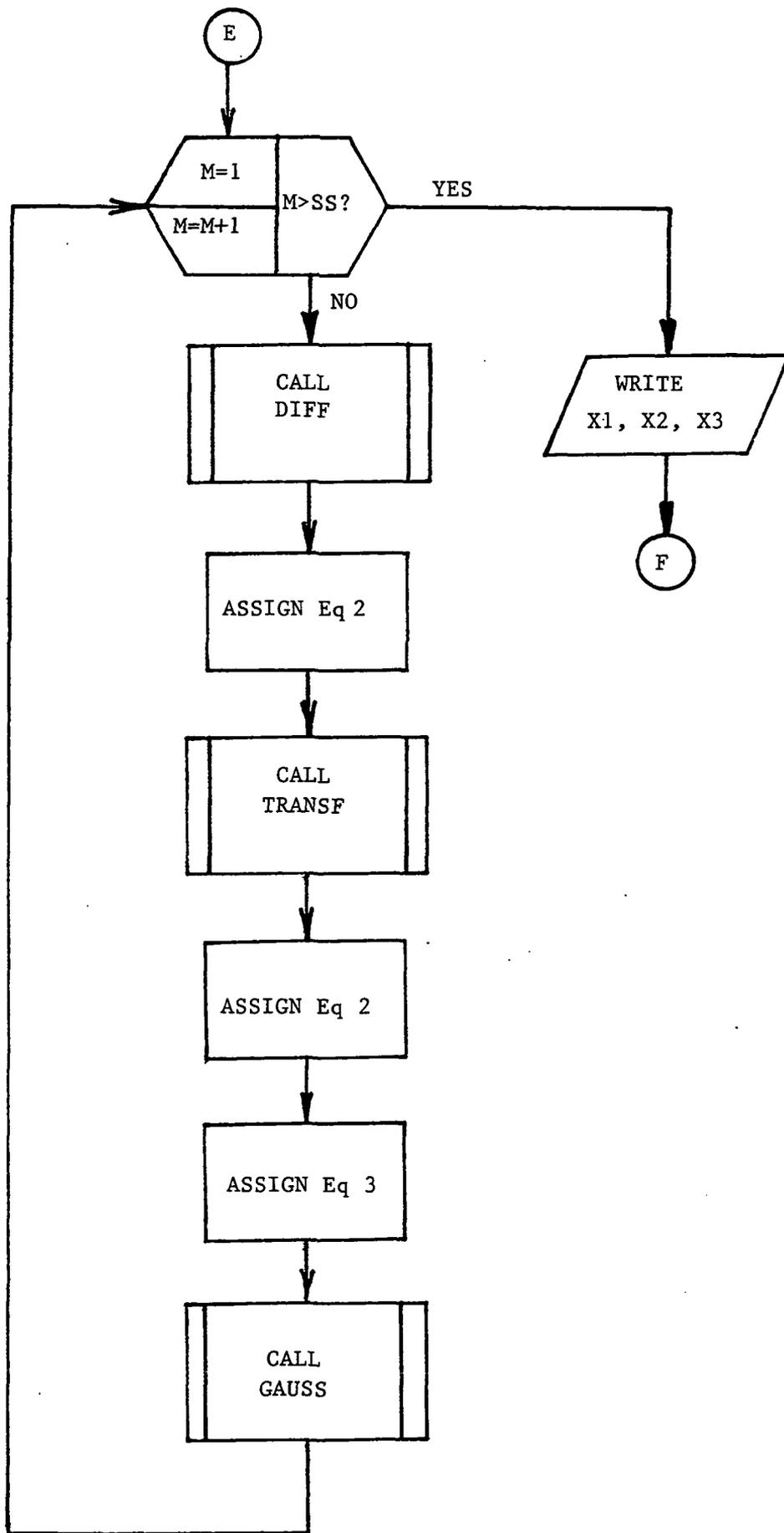
RETURN
END

```

FLOWCHART: POINTS : F







## FLOWCHART: POINTS.F (DISCUSSION)

There are 4 loops in the main program.

Loop 1: loops one through four to read data for the four surfaces.

Loop 2: loops one through BBB, where BBB is the number of points across the face of the tooth surface.

Loop 3: loops one through CCC, where CCC is the number of points along the length of the tooth height.

Loop 4: The final loop iterates to solve the three equations used to identify a point on the surface.

### Subroutines:

1. STEPZR. This subroutine steps Z and R as the solution "marches" across the tooth face.
2. DIFF. This subroutine performs the numerical differentiation of the three equations (to form the Jacobian).
3. TRANSF. Subroutine that performs the matrix multiplication for the five coordinate transformations.
4. GAUSS. Uses gauss elimination to solve the Jacobian matrix.

```

C                                     PAT. F
C-----C
C      THIS PROGRAM GIVES THE N * M GRID PATRAN INPUT FILE FOR      C
C      THE GENERATION OF SPIRAL BEVEL GEAR TOOTH SURFACE WITH FILLET  C
C-----C
C      READS POINTS.OUT AND GIVES T1.OUT
C      T1.OUT => INPUT FILE FOR PATRAN
C
C      (MAIN PROGRAM)
C
COMMON/UNITS/NF1,NF2
DIMENSION X1(45,45),X2(45,45),X3(45,45)
DIMENSION X1R(45,45),X2R(45,45),XX(8000),ZZ(8000),YY(8000)
DOUBLE PRECISION ri,cl,r1,r2,mu,deden,rogear
DOUBLE PRECISION X1,X2,X3,X1R,X2R,XX,YY,ZZ,rotcon,rotint
INTEGER UU,T,INT,NF1,NF2,NF3,JI,BB,CC
INTEGER NUMBER,FILL,NTPIN,NTGE

C      PI      = 4.0*ATAN(1.0)
C
NF1 = 900
NF2 = 1000
NF3 = 1001

C      OPEN(UNIT=NF1,FILE='t1.out',STATUS='UNKNOWN')
C      OPEN(UNIT=NF2,FILE='t2.out',STATUS='UNKNOWN')
C      OPEN(UNIT=NF3,FILE='POINTS.OUT',STATUS='OLD')

C      WRITE(*,('PLEASE ENTER THE REQUIRED GRID PATTERN.'/
C      *'FOR EXAMPLE : FOR A 8X7 PATTERN ENTER 8 AND THEN 7 >'))
C      READ(*,*)BB
C      READ(*,*)cc
C      write(*,*)'ENTER NUMBER OF ELEMENTS THROUGH THE THICKNESS'
C      READ(*,*) number
C      WRITE(*,*)'ENTER THE NUMBER OF ELEMENTS IN THE FILLET'
C      READ(*,*)FILL
C      DO 5 INT = 1,4
C      IF ((INT .EQ. 1).OR.(INT .EQ. 2)) THEN

C-----C
C      DESCRIPTION OF INPUT DATA FOR PINION
C-----C
C
C      1. DEDENDUM, DEGREES          (DEDEN)
C      2. PITCH ANGLE, DEGREES      (MU)
C      3. ROTATION OF CONVEX SURFACE TO
C      CREATE TOP LAND              (ROTCON)
C      4. ROTATION OF PINION TO ELIMINATE
C      INTERFERENCE                 (ROTINT)
C      5. PINION ID, INCHES         (RI)
C      6. CLEARANCE, INCHES        (CL)
C      7. NUMBER OF PINION TEETH    (NTPIN)
C-----C
C
C      INPUT THE PINION DATA BELOW
C-----C
C      DEDEN = 1.56666666 * PI/180.0
C      MU    = 18.4333333 * PI/180.0
C      ROTCON = 2.275
C      ROTINT = -3.56
C      RI    = 0.609375
C      CL    = 0.03
C      NTPIN = 12
C-----C

```

```

C
C
C
ELSEIF ((INT .EQ. 3).OR.(INT .EQ. 4)) THEN
C
C
C-----
C      DESCRIPTION OF INPUT DATA FOR THE GEAR
C-----
C
C      1. DEDENDUM, DEGREES                (DEDEN)
C      2. PITCH ANGEL, DEGREES            (MU)
C      3. ROTATION OF CONVEX SURFACE TO
C          CREATE TOP LAND                (ROTCON)
C      4. ROTATION OF GEAR TO PUT IN MESH  (ROGEAR)
C      5. CLEARANCE, INCHES               (CL)
C      6. ID OF GEAR BASE                 (R1)
C      7. OD OF GEAR BASE                 (R2)
C      8. NUMBER OF GEAR TEETH            (NTGE)
C-----
C
C-----
C      INPUT THE GEAR DATA BELOW
C-----
C          DEDEN = 3.883333333 * PI/180.0
C          MU    = 71.56666666 * PI/180.0
C          ROTCON = -8.49
C          ROGEAR = 190.0
C          CL    = 0.0366
C          R1    = 2.375
C          R2    = 3.250
C          NTGE  = 36
C-----
C
C
C
C
C
C
C      ENDIF
C
C      IF (int.EQ.1) THEN
C          WRITE(NF1,*) 'SET,LABEL,OFF'
C          WRITE(NF1,*) 'VI'
C          WRITE(NF1,*) '1'
C          WRITE(NF1,*) '120,0,120'
C      ENDIF
C
C      JI = 1
C
C      DO 10 UU = 1,BB
C      DO 20 T = 1,cc
C
C          READ(NF3,*)X1(UU,T),X2(UU,T),X3(UU,T)
C
C          IF ((INT .EQ. 2).OR.(INT .EQ. 4)) THEN
C              CALL ROTATE(X1(UU,T),X2(UU,T),X1R(UU,T),X2R(UU,T),INT,
C * rotcon)
C          ENDIF
C
C          CALL ALLIGN(X1(UU,T),X2(UU,T),X1R(UU,T),X2R(UU,T),INT,
C * rotint,rogear)
C
C          CALL GRID(UU,T,INT,X1,X2,X3,X1R,X2R,XX,YY,ZZ,bb,cc)
C
C          JI = JI + 1

```

```

C
20 CONTINUE
10 CONTINUE
5 CONTINUE
C
DO 6 int = 1,4
C
IF ((INT .EQ. 2).OR.(INT .EQ. 4)) THEN
CALL LINE(INT,bb,cc)
SS = INT
CALL PATCH(SS,bb,cc)
CALL HPAT(INT,bb,cc)
CALL FILLET(XX,YY,ZZ,INT,bb,cc,ri,cl,r1,r2,mu,deden,
* ntpin,ntge)
ENDIF
C
6 CONTINUE
C
CALL MODEL(bb,cc,number,fill)
CLOSE(NF3,STATUS='KEEP')
CLOSE(NF2,STATUS='KEEP')
CLOSE(NF1,STATUS='KEEP')
C
STOP
END
C
C
SUBROUTINE ROTATE(X1,X2,X1R,X2R,INT,rotcon)
C
COMMON/UNITS/NF1,NF2
DOUBLE PRECISION PI,Q,A,X1,X2,X1R,X2R,rotcon
DIMENSION A(2,2)
C
ROTATION OF PINION AND GEAR CONVEX SIDES BY Q DEG. TO CREATE TOP LAND
C
PI = 4.0 * ATAN(1.0)
IF ((INT .EQ. 1).OR.(INT .EQ. 2)) THEN
Q = rotcon*PI/180.0
ELSEIF ((INT .EQ. 3).OR.(INT .EQ. 4)) THEN
Q = rotcon*PI/180.0
ENDIF
A(1,1) = COS(Q)
A(2,1) = -SIN(Q)
A(1,2) = SIN(Q)
A(2,2) = COS(Q)
C
X1R = X1*A(1,1)+X2*A(2,1)
X2R = X1*A(1,2)+X2*A(2,2)
C
RETURN
END
C
C
SUBROUTINE ALLIGN(X1,X2,X1R,X2R,INT,rotint,rogear)
C
TO ALLIGN THE PINION ABOVE THE GEAR AND CALCULATE GAPS
C
COMMON/UNITS/NF1,NF2
DOUBLE PRECISION X1,X2,X1R,X2R,X11,X22,X11R,X22R
DOUBLE PRECISION Q,PI,X18,Y18,X18R,Y18R,rotint,rogear.
C
PI = 4.0 * ATAN(1.0)
C
ROTATION OF THE PINION BY -3.56 DEG. ABOUT Z-AXIS
C
Q =rotint*PI/180.0

```

```

IF (INT.EQ.1) THEN
  X11 = X1*COS(Q)-X2*SIN(Q)
  X22 = X1*SIN(Q)+X2*COS(Q)
  X1 = X11
  X2 = X22
ELSEIF (INT.EQ.2) THEN
  X11R = X1R*COS(Q)-X2R*SIN(Q)
  X22R = X1R*SIN(Q)+X2R*COS(Q)
  X1R = X11R
  X2R = X22R
ENDIF

```

C

```

Q = -30.0*PI/180.0
IF (INT.EQ.1) THEN
  X30 = X1*COS(Q)-X2*SIN(Q)
  Y30 = X1*SIN(Q)+X2*COS(Q)
ELSEIF (INT.EQ.2) THEN
  X30R = X1R*COS(Q)-X2R*SIN(Q)
  Y30R = X1R*SIN(Q)+X2R*COS(Q)
ENDIF

```

C

C

C

ROTATION OF THE GEAR BY 190 DEG. ABOUT Z-AXIS

```

Q = rogear*PI/180.0
IF (INT.EQ.3) THEN
  X18 = X1*COS(Q)-X2*SIN(Q)
  Y18 = X1*SIN(Q)+X2*COS(Q)
  X1 = X18
  X2 = Y18
ELSEIF (INT.EQ.4) THEN
  X18R = X1R*COS(Q)-X2R*SIN(Q)
  Y18R = X1R*SIN(Q)+X2R*COS(Q)
  X1R = X18R
  X2R = Y18R
ENDIF

```

C

C

```

RETURN
END

```

C

C

C

SUBROUTINE GRID(UU,T,INT,X1,X2,X3,X1R,X2R,XX,YY,ZZ,BB,cc)

C

```

COMMON/UNITS/NF1,NF2
INTEGER NN,UU,T,BB,cc
DOUBLE PRECISION X1(45,45),X2(45,45),X3(45,45)
DOUBLE PRECISION X1R(45,45),X2R(45,45)
DOUBLE PRECISION XX(8000),YY(8000),ZZ(8000)
IF (INT .EQ. 1) THEN
  NN = (UU - 1) * cc + T
ELSEIF (INT .EQ. 2) THEN
  NN = (UU - 1) * cc + T + (BB*cc)
ELSEIF (INT .EQ. 3) THEN
  NN = (UU - 1) * cc + T + 2*(BB*cc)
ELSEIF (INT .EQ. 4) THEN
  NN = (UU - 1) * cc + T + 3*(BB*cc)
ENDIF

```

C

```

IF ((INT .EQ. 1).OR.(INT .EQ. 3)) THEN
  XX(NN) = X1(UU,T)
  YY(NN) = X2(UU,T)
  ZZ(NN) = X3(UU,T)
ELSEIF ((INT .EQ. 2).OR.(INT .EQ. 4)) THEN
  XX(NN) = X1R(UU,T)
  YY(NN) = X2R(UU,T)
  ZZ(NN) = X3(UU,T)

```

```

        ENDIF
C
        WRITE(NF1,111)'GRID',',',',',NN,',',',',XX(NN),',',',',YY(NN),',',',',ZZ(NN)
111  FORMAT(A4,A1,I4,A2,F10.6,A1,F10.6,A1,F10.6)
C
        RETURN
        END
C
        SUBROUTINE LINE(INT,bb,cc)
C
        COMMON/UNITS/NF1,NF2
        INTEGER L,M,N,K,bb,cc
C
        DO 600 L = 1, BB
            K = L
        IF (INT .EQ. 2) THEN
            M = (L-1) * cc + 1
            n = m+bb*cc
        ELSEIF (INT .EQ. 4) THEN
            K = L + BB*16
            m = (L - 1) *cc + (2*bb*cc + 1)
            n = M + bb*cc
        ENDIF
            N = M + BB*cc
        WRITE(NF1,610)'LINE',',',',',K,',',',',ST',',',',',M,',',',',N
        WRITE(nf1,611)'LINE',',',k+bb+L-1,',',',',k+bb+L,',',',',BR,.5,',',k
610  FORMAT(a4,a1,i4,a1,2a2,i4,a1,i4)
611  FORMAT(a5,i3,a1,i3,a1,a6,i4)
600  CONTINUE
C
        RETURN
        END
C
        SUBROUTINE PATCH(SS,bb,cc)
C
        COMMON/UNITS/NF1,NF2
        INTEGER I,II,J,JJ,K,L,M,bb,cc
C
        JJ = (cc-1)*BB
        DO 700 I = 1,JJ
C
        IF (SS .EQ. 2) THEN
            J = INT((I-1)/(cc-1)) + I
            II = I
        ELSEIF (SS .EQ. 4) THEN
            j = int((I-1)/(cc-1)) + I + 2*(bb*cc)
            II = jj + I + 3*bb
        ENDIF
            K = J + 1
            L = K + BB*cc
            M = L - 1
        WRITE(NF1,710)'PATCH',',',',',II,',',',',QUAD',',',',',J,',',',',K,',',',',L,',',',',M
710  FORMAT(A5,A1,I4,A1,A5,A2,I4,A1,I4,A1,I4,A1,I4)
700  CONTINUE
C
        RETURN
        END
        SUBROUTINE HPAT (int,bb,cc)
C
        COMMON/units/nf1,nf2
        INTEGER i,j,bb,cc
C
        jj = (bb-1)*(cc-1)
        Do 800 I = 1,jj
        If(int .eq. 2) then
            k = i

```



```

JJ = (I-1)*cc + 1
KK = (I-1)*cc + BB*cc + 1
J = I + BB
IF (ABS(Y(JJ)).LE.1.0E-5)GOTO 141
MM(I) = ATAN(Y(JJ)/X(JJ))
IF (X(JJ).LT.0.0.AND.Y(JJ).LT.0.0)MM(I) = MM(I) + PI
IF (X(JJ).LT.0.0.AND.Y(JJ).GT.0.0)MM(I) = MM(I) + PI
GOTO 142
141 CONTINUE
MM(I) = 0.0
IF (Z(JJ).LT.0.0)MM(I) = PI
142 CONTINUE
IF (ABS(Y(KK)).LT.1.E-5)GOTO 143
PP(J) = ATAN(Y(KK)/X(KK))
IF (X(KK).LT.0.0.AND.Y(KK).LT.0.0)PP(J) = PP(J) + PI
IF (X(KK).LT.0.0.AND.Y(KK).GT.0.0)PP(J) = PP(J) + PI
GOTO 140
143 CONTINUE
PP(J) = 0.0
IF (X(KK).LT.0.0)PP(J) = PI
140 GOTO 155
C
ELSEIF(INT.EQ.4)THEN
JJ = (I-1)*cc + 2*(BB*cc)+1
KK = (I-1)*cc + 3*(BB*cc)+1
J = I + 2*(BB*cc) + BB
IF (ABS(Y(JJ)).LE.1.0E-5)GOTO 151
MM(I) = ATAN(Y(JJ)/X(JJ))
IF (X(JJ).LT.0.0.AND.Y(JJ).LT.0.0)MM(I) = MM(I) + PI
IF (X(JJ).LT.0.0.AND.Y(JJ).GT.0.0)MM(I) = MM(I) + PI
GOTO 152
151 CONTINUE
MM(I) = 0.0
IF (X(JJ).LT.0.0)MM(I) = PI
152 CONTINUE
IF (ABS(Y(KK)).LT.1.E-5)GOTO 153
PP(J) = ATAN(Y(KK)/X(KK))
IF (X(KK).LT.0.0.AND.Y(KK).LT.0.0)PP(J) = PP(J) + PI
IF (X(KK).LT.0.0.AND.Y(KK).GT.0.0)PP(J) = PP(J) + PI
GOTO 150
153 CONTINUE
PP(J) = 0.0
IF (X(KK).LT.0.0)PP(J) = PI
150 GOTO 155
ENDIF
155 CONTINUE
C
C
C FOR INNER GEAR BLANK RADIUS GRIDS & ARC LOCATIONS
C
IF(INT.EQ.4)THEN
DELTA = (R2-R1)/(BB-1)
RBAR = R1
ENDIF
C
DO 910 I = 1, BB
J = I + BB
G = GR + 1 + (I-1)*2
C
IF(INT.EQ.2)THEN
JJ = (I-1)*cc + 1
K = I + 2*BB
XR = RI*COS(MM(I))
YR = RI*SIN(MM(I))
ZR = Z(JJ)
DELTA(I) = ((PP(J)-MM(I))*180./PI)
WRITE(nf1,915)'GRID,',G+bb',',',',',XR,'/',YR,'/',ZR

```

```

911 WRITE(nf1,911)'LINE,',k+bb,',ARC,5(0)/1/',delta(i),',',g+bb
    FORMAT(a5,i3,a12,f10.5,a1,i4)

```

C

```

ELSEIF(INT.EQ.4)THEN
  JJ = (I-1)*cc + 2*(BB*cc)+1
  J  = I + 2*(BB*cc)+BB
  K  = I + (cc-1)*BB
  RBAR = R1 + (I-1)*DELR
  RX(I) = RBAR*COS(MM(I))
  RY(I) = RBAR*SIN(MM(I))
  RICC = SQRT(X(JJ)*X(JJ)+Y(JJ)*Y(JJ))
  RZ(I) = Z(JJ) + (RICC-RBAR)/TAN(PI/2.-(MU-DEDED))
  DELTA(I) = (PP(J)-MM(I))*180./PI
  WRITE(nf1,915)'GRID,',G+2*bb,',',RX(i),',',Ry(i),',',Rz(i)
WRITE(nf1,920)'LINE,',19*bb+i,',ARC,5(0)/1.0/',delta(i),',',g+2*bb
  ENDIF
915 FORMAT(A5,I4,A2,F10.6,A1,F10.6,A1,F10.6)
920 FORMAT(A5,I4,A20,F10.4,A2,I4)
910 CONTINUE
925 CONTINUE

```

C

C

C

TO MAKE HYPAT FROM GEAR BLANK INSIDE RADIUS TO TOOTH BOTTOM

```

IF(INT.EQ.2)THEN
  GR = 4*BB*cc
  PA = 2*BB*cc - BB
  LI = 3*BB
  HP = 2*(cc-1)*(bb-1) + (BB-1)
  ntp = ntpin
ELSEIF(INT.EQ.4)THEN
  GR = 4*BB*cc + 6*BB
  PA = 2*BB*cc + BB
  LI = BB*cc
  HP = 2*(cc-1)*(bb-1) + 3*(BB-1)
  ntp = ntge
ENDIF
NT = FLOAT(NTP)

```

C

C

```

DO 930 I = 1, BB
  LI = LI + i
IF(INT.EQ.2)THEN
  Li1 = 4*bb + 2*i
  Li2 = 4*bb*cc + bb + (2*i-1)
  Li3 = 10*bb+(2*i-1)
  Li4 = 10*bb+2*i
  Li5 = Li1
  Li6 = 12*bb+i
  Li7 = 4*bb*cc + 3*bb +(4*i-2)
  Li8 = 4*bb*cc +3*bb +4*i
  LI9 = 13*bb+i
  Li10 = bb*cc+cc*i-(cc-1)
  Li11 = 4*bb*cc+bb+(2*i)
  Li12 = 14*bb+i
  LI13 = 4*bb*cc +3*bb +(4*i-3)
  Li14 = 4*bb*cc +3*bb +(4*i-1)
  LI15 = 15*bb+i
  Li16 = 3*bb+i
  Li17 = 10*bb+(2*i-1)
  II = (I-1)*cc + 1
  DELA = ABS(DELTA(I)*PI/180.)
  ROT = (2.* PI / NT - DELA)/2.
  VEC = SQRT(X(II)*X(II)+Y(II)*Y(II))
  ETA = ACOS(1.-(CL/VEC)**2.)
  XRHO = VEC*COS(MM(I)-ROT)

```

```

        YRHO = VEC*SIN(MM(I)-ROT)
        ANG = ((PI-2.*ROT)*180.)/ PI
        W4 = 8*bb + i
        w5 = 4*bb*cc + i
        W6 = 4*bb*cc + 3*bb + 4*i
        WRITE(nf1,929)'LINE,',4*bb+(2*i-1),',ARC,',xrho,'/',yrho,'/0/',
*      xrho,'/',yrho,'/1.0/',ang,',',ii
        WRITE(nf1,933)'LINE,',6*bb+(2*i-1),',/',6*bb+2*i,',BR,.5,',
*      4*bb+(2*i-1)

933  FORMAT (a5,i4,a1,i4,a7,i4)

929  FORMAT(a5,i4,a5,f8.5,a1,f8.5,a3,f8.5,a1,f8.5,a5,f11.5,a1,i4)
934  FORMAT(a5,i4,a3,a2,i4,a1,i4)
      ELSE
        Li1 = 25*bb+(2*i-1)
        Li2 = 4*cc*bb + 8*bb + (2*i - 1)
        Li3 = 27*bb + 2*i
        Li4 = 27*bb + 2*i + 1
        LI5 = 25*bb+(2*i-1)
        Li6 = 29*bb + 1 + i
        Li7 = 4*bb*cc + 10*bb + (4*i -2)
        Li8 = 4*bb*cc +10*bb + 4*i
        Li9 = 30*bb + 1 + i
        Li10 = 3*cc*bb + (cc*i - cc+1)
        Li11 = 4*bb*cc + 8*bb + 2*i
        LI12 = 31*bb + 1 + i
        Li13 = 4*bb*cc + 10*bb + (4*i - 3)
        Li14 = 4*bb*cc + 10*bb + (4*i - 1)
        Li15 = 32*bb + 1 + i
        li16 = 19*bb + i
        Li17 = 27*bb + 2*i
        II = (I-1)*cc + 2*(BB*cc)+1
        DELA = ABS(DELTA(I)*PI/180.)
        ROT = (2.* PI / NT - DELA)/2.
        VEC = SQRT(X(II)*X(II)+Y(II)*Y(II))
        XRHO = VEC*COS(MM(I)+ROT)
        YRHO = VEC*SIN(MM(I)+ROT)
        ANG = -((PI-2.*ROT)*180.)/ PI
        WRITE(NF1,931)'LINE,',20*bb+i,',ARC,',',0/0/0/',XRHO,'/',
*      YRHO,'/',Z(II),',/',ANG,',',II
        w1 = 22*bb + (2*i-1)
        w2 = w1 +1
        w3 = 20*bb+i
        w4 = 24*bb + i
        w5 = 4*bb*cc + 7*bb + i
        w6 = 4*bb*cc + 10*bb + 4*i
        WRITE(nf1,933)'LINE,',w1,'/',w2,',BR,.5,',w3
931  FORMAT(A5,I4,A5,A6,F7.4,A1,F7.4,A1,F10.6,A1,F8.3,A1,I4)
      ENDIF
        IF(INT.EQ.2)ROTAT = -(2 * ROT * 180./PI)
        IF(INT.EQ.4)ROTAT = (2 * ROT * 180./PI)
        IF(I.EQ.1)GR = GR + 1
        IF(I.GT.1)GR = GR + 2
        Write(nf1,932)'LINE,',LI1, ',ARC,0/0/0/0/0/1/',ROTAT,',',LI2
        write(nf1,936)'LINE,',LI3, ',/',LI4, ',BR,.5,',LI5
        write(nf1,934)'LINE,',w4,',ST',',',w5,',',w6
        write(nf1,937)'LINE,',LI6,',ST',',',LI7,',',LI8
        write(nf1,937)'LINE,',LI9,',ST',',',LI10,',',LI11
        write(nf1,937)'LINE,',LI12,',ST',',',LI13,',',LI14
        write(nf1,938)'LI,',Li15,',MER,',',Li16,'/',Li17
938  format(a3,i4,a6,i4,a1,i4)
937  format(a5,i4,a3,a2,i4,a1,i4)
936  format(a5,i4,a1,i4,a7,i4)
932  FORMAT(A5,I4,A18,F8.3,A1,I4)
930  CONTINUE

```

C  
C  
C  
C

CONNECT LINES ON TOP OF FILLET/ROOT RADIUS &  
GEAR BLANK INSIDE RADIUS

```
DO 940 I = 1,bb
  IF(INT.EQ.2) then
    pppa = bb*cc-bb
    pa1 = bb+2*i
    pa2 = 13*bb+i
    pa3 = 15*bb+i
    pa4 = 8*bb+i
    pa5 = bb+(2*i-1)
    pa6 = 8*bb+i
    pa7 = 12*bb+i
    pa8 = 6*bb+(2*i-1)
    pa9 = 10*bb+(2*i)
    pa10 = 14*bb+i
    pa11 = 6*bb+2*i
    pa12 = 12*bb+i
  elseif(int.eq.4)then
    Pppa = 2*bb*(cc-1) + 3*bb
    pa1 = 30*bb + 1 + i
    pa2 = 17*bb + 2*i
    Pa3 = 24*bb + i
    Pa4 = 32*bb + 1 + i
    Pa5 = pa3
    Pa6 = pa2 - 1
    Pa7 = 22*bb + 2*i -1
    pa8 = 29*bb + 1 + i
    pa9 = pa8
    pa10 = pa7 + 1
    Pa11 = 31*bb + i + 1
    pa12 = 27*bb + 2*i + 1
  endif
  write(nf1,941)'PA,',1*PPPA+i,',EDGE,,,pa1,/',pa2,/',pa3,/',pa4
  write(nf1,941)'PA,',1*PPPA+bb+i,',EDGE,,,pa5,/',pa6,/',pa7,/',pa8
  write(nf1,941)'PA,',1*pppa+2*bb+i,',EDGE,,,pa9,/',pa10,/',pa11,
  * '/',pa12
941  format(a3,i4,a7,i4,a1,i4,a1,i4,a1,i4)
940  CONTINUE
```

C  
C  
C

CONNECT PATCHES IN BETWEEN TEETH TO MAKE HYPERPATCHES

```
do 945 i = 1,(bb-1)
  If (int.eq.2) then
    hp1 = bb*(cc-1) + i
    hp2 = hp1 + 1
    hp3 = hp1 + bb
    hp4 = hp3 + 1
    hp5 = hp3 + bb
    hp6 = hp5 + 1
  hh1 = (bb-1)*(cc-1)+i
  hh2 = hh1 + (bb-1)
  hh3 = hh2 + (bb-1)
  ELSEIF (INT .EQ. 4) THEN
    hp1 = 2*bb*(cc-1) + 3*bb + i
    hp2 = hp1 + 1
    hp3 = hp1 + bb
    hp4 = hp3 + 1
    hp5 = hp3 + bb
    hp6 = hp5 + 1
    hh1 = 2*(bb-1)*(cc-1) + 3*(bb-1) + i
    hh2 = hh1 + bb-1
    hh3 = hh2 + bb-1
  ENDIF
  write(nf1,913)'HPAT,',hh1,',2P,,,hp1,',',hp2
```

```

          write(nf1,913)'HPAT','hh2','2P','','hp3','','hp4
          write(nf1,913)'HPAT','hh3','2P','','hp5','','hp6
913  format(a5,i4,a6,i4,a1,i4)
945  CONTINUE
          IF(INT.EQ.2)GO TO 980
C
980  CONTINUE
          IF (INT.EQ.2) THEN
              WRITE(NF1,*)'SET,LINES,0'
              WRITE(NF1,*)'NAME,PI 1'
              WRITE(NF1,*)'SET,ACTIVE,NONE'
          ELSEIF(INT.EQ.4) THEN
              WRITE(NF1,*)'SET,LINES,0'
              WRITE(NF1,*)'NAME,GE 1'
              write(nf1,*)'SET,ACTIVE,NONE'
          ENDIF
C
          RETURN
          END
C
C
C
          SUBROUTINE MODEL(BB,cc,number,fill)
C
          COMMON/UNITS/NF1,NF2
          INTEGER I,J,K,L,numb
          INTEGER I1,I2,J1,J2,K1,K2,L1,L2,bb,cc
C
          WRITE(NF1,*)'NAME,GE 1,PLOT'
C
          to generate the whole gear use this do loop
          DO 901 I = 1,35
              L = I + 1
C
          WRITE(NF1,905)'NAME','','GE',L','','RO','','5(0)/1/10','','GE',I
C 905  FORMAT(A6,A2,I2,A1,A2,A1,A10,A2,I2)
C 901  CONTINUE
              WRITE(NF1,*)'NAME,GEAR'
              write(nf1,*)'NAME,PI 1,PL'
              WRITE(NF1,*)'PA,1T#,DEL'
C
              I1 = 1
              I2 = (BB-1)*(cc-1)
              j1 = i2 + 1
              j2 = i2 + 2*(bb-1)
              numb = number/2
C
              write(nf1,917)'MESH,H',i1,'T',i2,'HEX,N,1/',number
              *,'/1/',number,'/1'
              write(nf1,918)'MESH,H',j1,'T',j2,'HEX,N',numb,'/',
              * fill,'/',numb,'/',fill,'/1'
              write(nf1,919)'MESH,H',j2+1,'T',j2+bb-1,'HEX,N','','3',
              * '/',numb,'/3/',numb,'/1'
          919  format(a6,i4,a1,i4,a7,a1,a1,i4,a3,i4,a2)
          917  format(a6,i4,a1,i4,a9,i4,a3,i4,a2)
          918  format(a6,i4,a1,i4,a7,i4,a1,i4,a1,i4,a1,i4,a2)
              write(nf1,*)'NAME,PIN'
              WRITE(NF1,*)'SET,ACTIVE,NONE'
              WRITE(NF1,*)'NAME,GE 1,PLOT'
C
              K1 = (bb-1)*(cc-1) + 3*(bb-1) + 1
              K2 = K1 + (bb-1) *(cc-1) - 1
              JJ1 = K2 + 1
              jj2 = k2 + 2*(bb-1)
              numb = number/2
C
              write(nf1,917)'MESH,H',K1,'T',K2,'HEX,N,1/',number
              *,'/1/',number,'/1'

```

```

        write(nf1,918) 'MESH,H',jj1,'T',jj2,'HEX,N',fill,'/',
* numb,'/',fill,'/',numb,'/1'
        write(nf1,921) 'MESH,H',jj2+1,'T',jj2+bb-1,'HEX,N',
* numb,'/','3','/',numb,'/','3','/1'

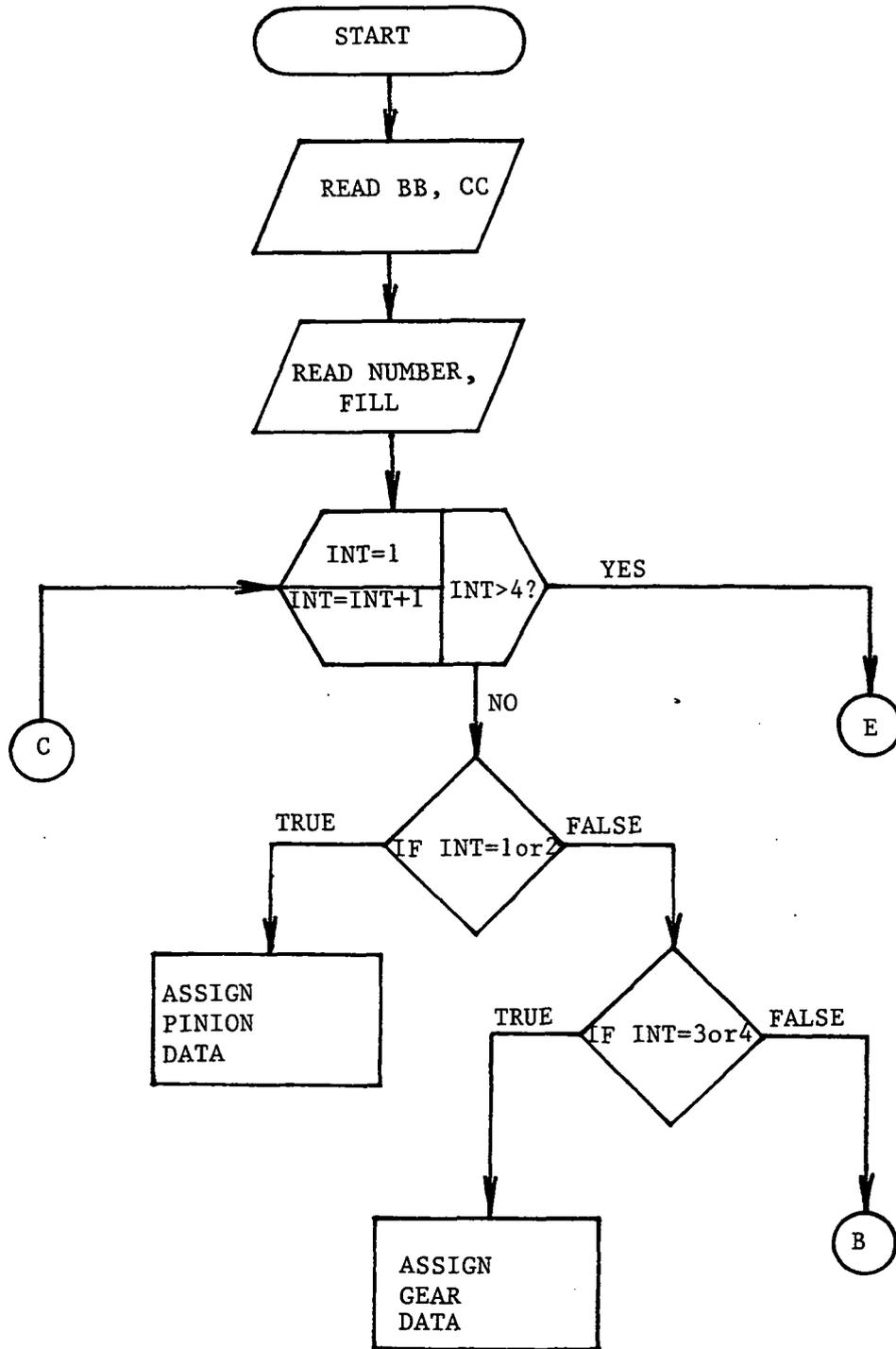
```

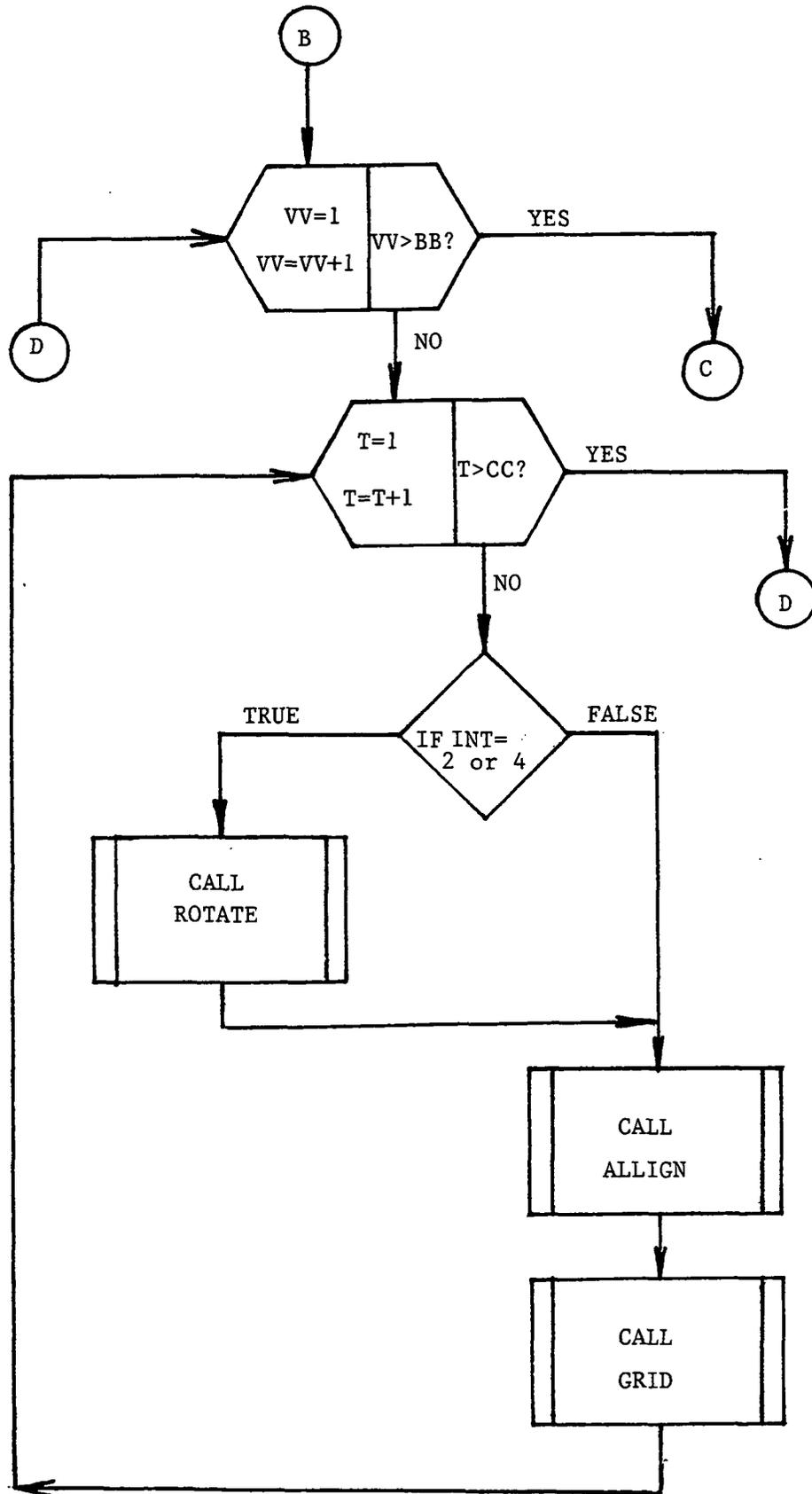
```

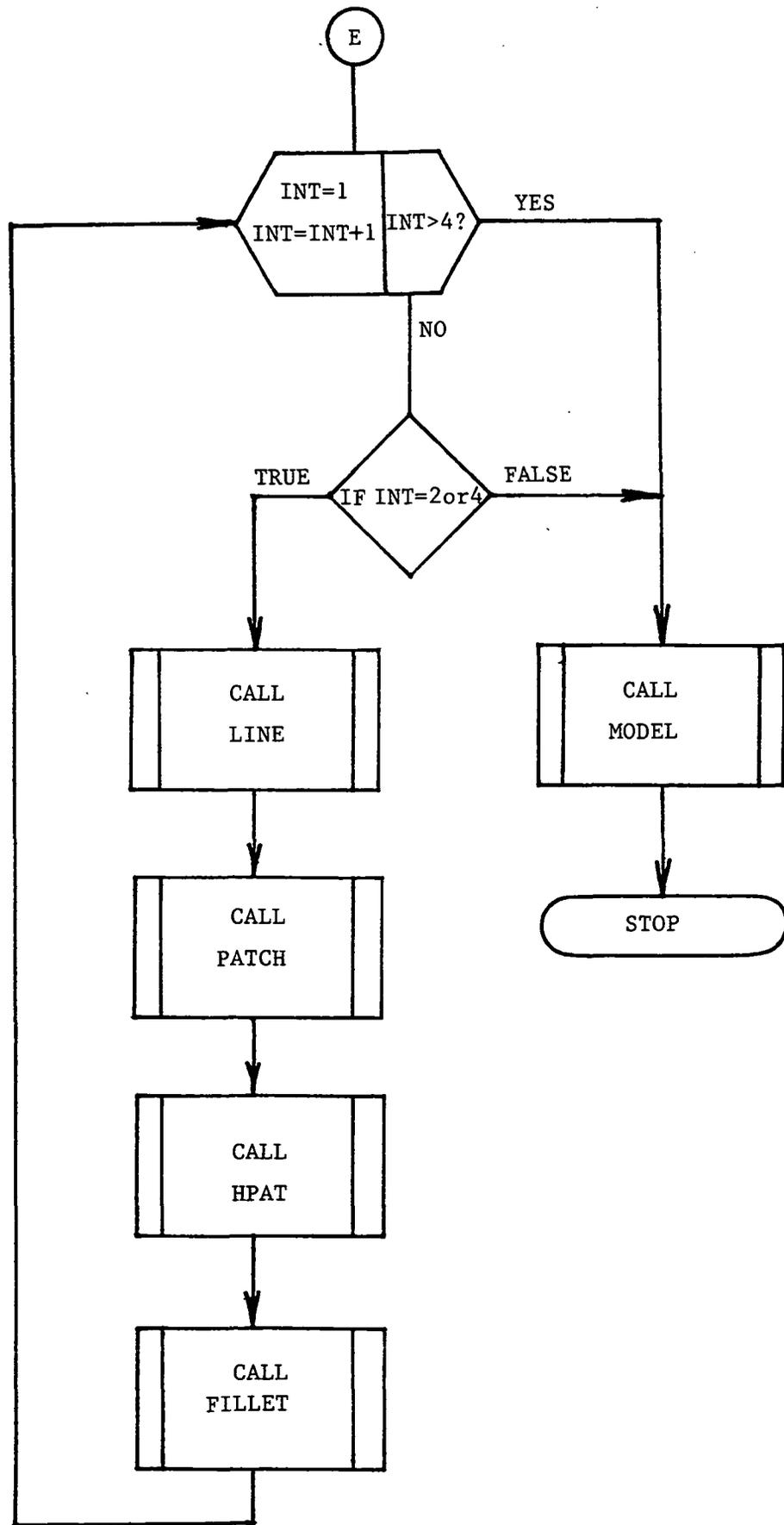
921     FORMAT(a6,i4,a1,i4,a7,i4,a1,a1,a1,i4,a1,a1,a2)
        K1 = (BB-1)*(cc-1) + 1
        K2 = 2*(BB-1)*(cc-1)
        L1 = 2*(bb-1)*cc + 1
        L2 = 2*(BB-1)*cc + 2*(bb-1)
C      to generate the whole pinion use this do loop
C      DO 902 J = 1,11
C          K = J + 1
C      WRITE(NF1,906) 'NAME','PI',K,',','RO',',',',',3(0)/1/0/0/30,'
C      *      ',PI',J
C 906     FORMAT(A6,A2,I2,A1,A2,A1,A14,A2,I2)
C 902     CONTINUE
C          WRITE(NF1,*) 'NAME,PINION1'
C
C          WRITE(NF1,*) 'NAME,GEAR'
C          WRITE(NF1,*) 'GR,1T#,DEL'
C          WRITE(NF1,*) 'NAME,PINION,RO,4(0)/1/0/-90,PIN'
C          write(nf1,*) 'NAME,PINION,PL'
C      Return
C      END

```

FLOWCHART: PAT. F.







## FLOWCHART: PAT.F (DISCUSSION)

There are four loops in the main program.

Loop 1: Loops one through four to read data for the four surfaces.

Loop 2: Loops one through BB, where BB is the number of points across the face of the tooth surface.

Loop 3: Loops one through CC, where CC is the number of points along the height of the tooth.

Loop 4: The final loop creates the lines, patches, hyper-patches, fillet and meshes the model for one gear tooth and one pinion tooth.

### Subroutines:

1. ROTATE: Rotates the pinion and gear convex sides by Q degrees to create top land.
2. ALLIGN: Aligns the pinion in mesh with the gear.
3. GRID: Creates PATRAN commands for the grids.
4. LINE: Creates PATRAN commands for the lines.
5. PATCH: Creates PATRAN commands for the patches.
6. HPAT: Creates PATRAN commands for the hyper-patches.
7. FILLET: Creates PATRAN commands to creat the fillet.
8. MODEL: Creates PATRAN commands to mesh the model.

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13. ABSTRACT (Maximum 200 words)  The goal of this research is to develop computer programs that generate finite element models suitable for doing 3D contact analysis of faced milled spiral bevel gears in mesh. A pinion tooth and a gear tooth are created and put in mesh. There are two programs: Points.f and Pat.f to perform the analysis. Points.f is based on the equation of meshing for spiral bevel gears. It uses machine tool settings to solve for an N x M mesh of points on the four surfaces, pinion concave and convex, and gear concave and convex. Points.f creates the file POINTS.OUT, an ASCII file containing N x M points for each surface. (N is the number of node points along the length of the tooth, and M is nodes along the height.) Pat.f reads POINTS.OUT and creates the file t1.out. T1.out is a series of PATRAN input commands. In addition to the mesh density on the tooth face, additional user specified variables are the number of finite elements through the thickness, and the number of finite elements along the tooth full fillet. A full fillet is assumed to exist for both the pinion and gear.				
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