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CONTINUATION OF SPACE SHUTTLE
PROBABILISTIC RISK ASSESSMENT, PHASE 3
SAIC DOCUMENT NO. SAICNY95-02-25

PROBABILISTIC RISK ASSESSMENT
OF THE
SPACE SHUTTLE
A STUDY OF THE POTENTIAL OF
LOSING THE VEHICLE
DURING NOMINAL OPERATION
VOLUME IV: SYSTEM MODELS AND DATA ANALYSIS

PREPARED FOR
US NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
HEADQUARTERS OFFICE OF SPACE FLIGHT (CODE M)
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BY
SCIENCE APPLICATIONS INTERNATIONAL CORPORATION
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(NASA-CR-197811) PROBABILISTIC
RISK ASSESSMENT OF THE SPACE
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DURING NOMINAL OPERATION. VOLUME 4:
SYSTEM MODELS AND DATA ANALYSIS
(Science Applications International G3/16

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B. I. Space Shuttle Main
Engine



SSME/MPs Initiator Equivalent Flight Occurrences Evaluation

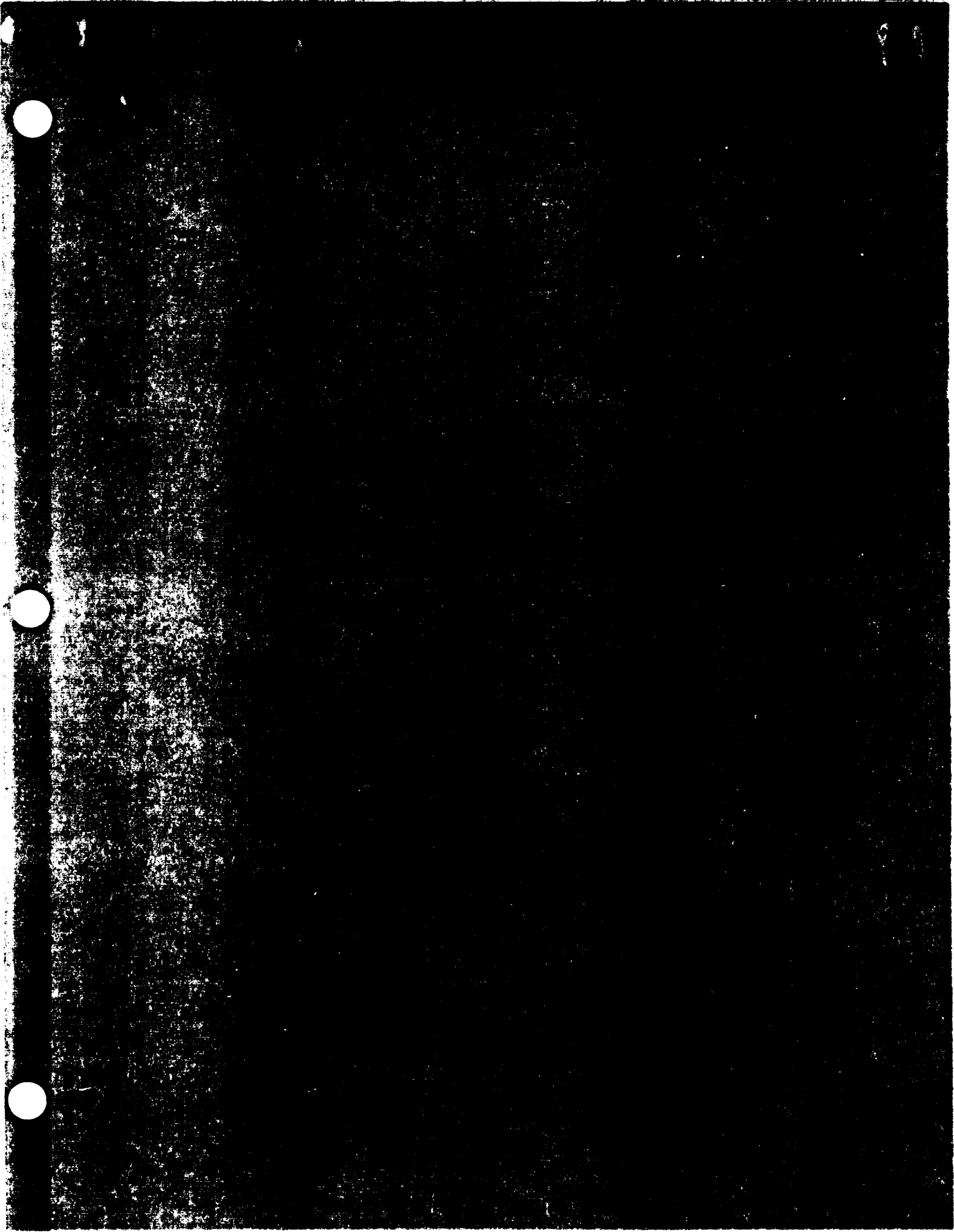
Record Type/ Source Study Initiator	Record/ Source ID	Date	System Element	Failure Description from Record	Analysis Comments	Engine #	Test/Flight	Redline Activation	Engine Configuration	Configuration Applicability	Event Priority Factor	Weighting Factor	Equivalent Flight Failure for Total Exposure Time
MSFC PRACA	A020946	24-Jul-88	SYSTEM	CROSS FEED GAIN BAD AT HIGH WLV POSITIONS	THROTTLE DOWN IN THRUST LIMIT *200F	0211	801.578	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FFLPH2	1	1	1	4.00
UCR	A015718	25-Jul-87	SYSTEM	HPOTP TURB TEMP EXCD RL	158H PRELIFT OFF RL - CHANGED TO 1000	0210	750.288	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FFLPH2	1	1	1	1
UCR	A016031	2-Sep-81	MINJ	SEVERE EROSION OF PRIMARIES FACE PLATES	MINJ BURJN OUT/REPLACED MINJ	0110	750.148	HPOTP TURBINE DISCHARGE TEMPERATURE	4 FFL	0.75	1	0.75	0.75
UCR	A013786	15-Jul-81	MINJ	SEVERE DAMAGE TO THE PRIMARIES FACE PLATES	MINJ BURJN OUT EXT DAM	2108	801.331	HPOTP TURBINE DISCHARGE TEMPERATURE	4 FFL	0.75	1	0.75	0.75
UCR	A017568	25-Jul-80	MINJ	RL CO. HPOT TURB DISC TEMP MAIN INJ	SOLE IN INJECTOR PORT/FAL	2004	802.186	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	0.5
SME/FP	Loss of Gross H2 Flow												
UCR	A011289	16-Apr-80	HPFTP	H2 FUEL TURB DISC TEMP VOTING LOGIC CO	TURNDOWN MAN COLLAPSED	2003	SF0901.8	HPFTP TURBINE DISCHARGE TEMPERATURE	2 MPFTA	0.25	1	0.25	0.25
UCR	A003243	10-Jul-78	HPFTP	EXTREME BULGING IN TURNDOWN MANIFOLD	BULGE IN TURBINE TURNDOWN MANIFOLD	0101	802.118	HPFTP TURBINE DISCHARGE TEMPERATURE	2 MPFTA	0.25	1	0.25	0.25
SME/EO	High Mixtures Ratio in Oxidizer Preburner												
UCR	A018563	26-Jan-81	SYSTEM	PREMATURE CUTOFF/OPOV POSITION	OPOV LIMIT RESET MCF	0007	750.119		2 MPFTA	0.25	1	0.25	0.25
MSFC PRACA	A06847	17-Jul-81	HYDRAULICS	ACT CHECK-OUT MODULE FAILURE	OPOV POSITION FAILURE		Field			1	0	0	
SME/FP	Loss of Fuel to Both Preburners												
UCR	A021548	2-Mar-88	FAM KI	H2 PREDICTION NOT PER WATER FLOW	OFF MAP/DUE TO BAD FLOWMETER CONSTANT	2107	802.465	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FFLPH2	1	1	1	6.25
UCR	A008918	11-Dec-86	SAW KI	PREMATURE CO. USED TURB TEMP FA	INCORRECT FLOWMETER CONSTANT	2028	802.348	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FFLPH2	1	1	1	1
UCR	A014574	24-Jul-86	SYSTEM	PREM. CO. HPOTP TURB. DISC TEMP	HIGH EFF HPFTP TURB/2 NO2 TUBE RUPT	2108	801.485	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FFLPH2	1	1	1	1
UCR	A008884	14-Apr-83	FAM KI	FAM CALIBRATION CONSTANT ESTIMATE LOW	HIGH INERTURE RATIO DUE TO KI	2011	802.308	HPOTP TURBINE DISCHARGE TEMPERATURE	4 FFL	0.75	1	0.75	0.75
UCR	A015978	5-Nov-80	NOZZLE	TURBINE 125 THRU 148 BLOWN FORWARD	NOZZLE TUBE RUPTURES	2003	SF1101.8	HPOTP TURBINE DISCHARGE TEMPERATURE	2 MPFTA	0.25	1	0.25	0.25
UCR	A016556	22-Sep-78	SYSTEM	CO-LOSS TURBINE TEMP EXCEEDED REDLINE	OVERSHOOT AT THROTTLE DOWN	0105	750.047	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	0.5
UCR	A018856	13-Jul-78	NOZZLE	NOZZLE TUBE RUPTURES-HPOT FA	TUBE RUPTURE (12) DOBBY DOORS	2004	802.182	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	0.5
UCR	A009345	22-May-79	NOZZLE	NUMEROUS TUBE LEAKS	TUBE LEAKS (13)	2004	802.158	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	0.5
UCR	A008488	14-May-79	NOZZLE	HPFT OVERTEMP REDLINE CUTOFF	NOZZLE STEERHORN FAILED	0201	750.041	HPFTP TURBINE DISCHARGE TEMPERATURE	2 MPFTA	0.25	1	0.25	0.25
UCR	A009316	10-May-79	NOZZLE	NOZZLE TUBE SPLITS - COOLANT LOSS	COLD WALL TUBE LEAKS (3)	2004	802.187	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	0.5
SME/TP	Failure to Maintain Proper Propellant Valve Position												
UCR	A018563	26-Jan-81	SYSTEM	PREMATURE CUTOFF/OPOV POSITION	OPOV LIMIT RESET MCF	0007	750.119		2 MPFTA	0.25	1	0.25	0.25
MSFC PRACA	A06847	17-Jul-81	HYDRAULICS	ACT CHECK-OUT MODULE FAILURE	OPOV POSITION FAILURE		Field			1	0	0	
SME/EO	HPFTP Coolant Line Overpressure												
MSFC PRACA	A08162	22-Apr-81	TURBOMCHNERY	COOLANT LINE PRESS HND ABNORMAL OSCIL	HPFTP COOLANT LINE OSCILLATIONS (SMALL OVERPRESSURE) - NO EFFECT SID		Field	HPFTP Coolant Line Pressure		1	0.1	0.1	0.40
MSFC PRACA	A08660	16-Oct-81	TURBOMCHNERY	COOLANT LINE PRESSURE INCREASED	COOLANT LINE PRESSURE LIMIT (115 PSI) EXCEEDED - 270 PSI MAXIMUM TO REDLINE SUI PHASE (IF SLUGGED)		Field	HPFTP Coolant Line Pressure		1	0.1	0.1	0.1
MSFC PRACA	A11878	28-Sep-84	TURBOMCHNERY	PREM. OSCILL OF HPFTP COOLANT LINE - FA	COOLANT LINE PRESSURE LIMIT EXCEEDED - SEE FA S15 26 E 4, 148 PSI MAXIMUM TO REDLINE SUI PHASE		Field	HPFTP Coolant Line Pressure		1	0.1	0.1	0.1
MSFC PRACA	A15403	25-Apr-88	TURBOMCHNERY	SPKED BELOW 300 PSD DURMO S15 S5 (FA	SPKED BELOW 300 PSD DURMO S15 S5 (FA		Field	HPFTP Coolant Line Pressure		1	0.1	0.1	0.1

SSME/MPs Initiator Equivalent Flight Occurrences Evaluation															
SMEST	Critical Structural Failure of SSME Component			NCA Nomenclature			Failure Description from Record			Analyst Comments	Type	Configuration Applicability	Event Possibility Factor	Weighting Factor	Equip. Flight Failure for Total Time
Record Type	Record #	Date	System Element	Initiator/Cause Description	NCA Part #	Failure Description from Record	Analyst Comments	Type	Configuration Applicability	Event Possibility Factor	Weighting Factor	Equip. Flight Failure for Total Time			
ANMCP8PRPMLPOTP				STRUCTURAL FAILURE OF LPOTP											
MSFC PRACA	A13505	1-Dec-86	TURBOMACHINERY	LPOTP UN 4306	RS007801-191	LPOTP UN 4306 HIGH BREAK AWAY IN VIOLATION OF OMRSD, ENGINE # 2012	LPOTP HIGH SHAFT TORQUE, BEARING DAMAGED	Field	1	0.02	0.02	0.06			
MSFC PRACA	A14010	1-Aug-87	TURBOMACHINERY	LPOTP UN 2028	RS007801-191	LPOTP UN 2028, HIGH BREAK AWAY TORQUE		Field	1	0.02	0.02				
MSFC PRACA	A14383	23-Nov-87	TURBOMACHINERY	LPOTP UN 2000	RS007801-191	LPOTP UN 2030 SHAFT SEIZED		Field	1	0.02	0.02				
ANMPS8PRPMPFB				HPFTP IMPELLER/DIFFUSER FAILURE								0.08			
MSFC PRACA	A08739	17-Oct-80	TURBOMACHINERY	RING, LOW PR ORRICE	RS007559-009		COOLANT LINER PRESSURE DROPPED AT C/O 4 SEC. HPFTP SPEED ROSE AT C/O (DAMAGE TO HPFTP, EXCESSIVE SHAFT TRAVEL, EXCESSIVE WEAR DUE TO IMBALANCE	Field	1	0.02	0.02				
MSFC PRACA	A08145	11-Apr-80	TURBOMACHINERY	IMPELLER	RS007556-013-25		EXCESSIVE WEAR, CRACKING, & RAISED MAT. IMPELLER CRACK	Field	1	0.02	0.02				
MSFC PRACA	A10076	27-May-82	TURBOMACHINERY	DIFFUSER	RS007532-091		HPFTP IMPACT DAMAGE ON PUMP RISE UNKNOWN CONTAMINATION - SEEMED TO HAVE NO EFFECT BUT SOUNDED SERIOUS	Field	1	0.02	0.02				
MSFC PRACA	A10203	10-Jul-82	TURBOMACHINERY	DIFFUSER	RS007527-061		HPFTP DIFFUSER NO 8 VANE DENTED BY IMPACT DAMAGE OF UNKNOWN CONTAMINATION - NO APPARENT EFFECT	Field	1	0.02	0.02	0.1			
ANM188PRPMPPTB				HPFTP TURBINE BLADE FAILURE											
MSFC PRACA	A14130	1-Aug-87	TURBOMACHINERY	HPFTP 1ST STG BLD8	R0019821-035	400790 HPFTP 1ST STAGE BLADE STOP FAILURE, ENGINE 2012		Field	1	0.02	0.02				
MSFC PRACA	A08076	27-Mar-80	TURBOMACHINERY	DISC 1ST STAGE ROTOR	RS007517-025	AU PLATE MISSING, CRACKS IN FRITREE ROOTS	CRACKS IN FRITREE ROOTS, HPFTP DISC FIRST STAGE ROTOR	Field	1	0.02	0.02				
MSFC PRACA	A08265	26-Jun-81	TURBOMACHINERY	BLADE 1ST STAGE	R0019821-013	CRACK IN FR TREE LOBBES, 1ST STAGE BLADE HPFTP, DISABY INSP, CANOGA	CRACK IN FIRST STAGE BLADES - SOME INFO ON CRACKS FROM 79-86	Field	1	0.02	0.02				
MSFC PRACA	A08461	21-Aug-81	TURBOMACHINERY	BLADE 1ST STAGE	R0019821-025	CRACK IN FR TREE LOBBES, 1ST STAGE BLADE HPFTP, DISABY INSP, CANOGA	CRACK IN FIRST STAGE BLADES - SOME INFO ON CRACKS FROM 79-86	Field	1	0.02	0.02				
MSFC PRACA	A02859	4-May-77	TURBOMACHINERY	HPFTP	RS007501-261	TIP BEARING VANE & SHROUD, EROSION		Field	1	0.02	0.02	0.08			
ANM100DPRPMPPOCD				HPOTP FAILURE DUE TO CAVITATION DAMAGE											
MSFC PRACA	A10062	1-May-82	TURBOMACHINERY	INLET VANE	RS007743-037		CAVITATION OF HPOTP - NO REDLINE, HIGHER THAN NORMAL HEAT LOSS	Field	1	0.02	0.02				
MSFC PRACA	A10069	26-May-82	TURBOMACHINERY	SEALS	RS007773-013		CAVITATION OF HPOTP - NO REDLINE, HIGHER THAN NORMAL HEAT LOSS	Field	1	0.02	0.02				
MSFC PRACA	A10073	29-May-82	TURBOMACHINERY	IMPELLER	RS007718-043		CAVITATION OF HPOTP - NO REDLINE, HIGHER THAN NORMAL HEAT LOSS	Field	1	0.02	0.02				
MSFC PRACA	A12023	19-Jan-85	TURBOMACHINERY	VANE, R.H.	RS007741-037		CAVITATION DAMAGE ON R.H. VANE, HPOTP	Field	1	0.02	0.02	0.06			
ANM088PRPMPPTB				HPOTP TURBINE BLADE FAILURE											
MSFC PRACA	A08530	19-Sep-81	TURBOMACHINERY	HPOTP UN 2018R3	RS007701-301	METAL PIECE LODGED IN 1ST STAGE NOZZLE		Field	1	0.02	0.02				
MSFC PRACA	A01035							Field	1	0.02	0.02				
MSFC PRACA	A12198	14-Apr-85	TURBOMACHINERY	TIP SEAL RETAINER	RS007813	TURBINE BLADE TIP SEAL GAP EXCEEDED SPEC., HPOTP UN 4106R1	HPOTP TIP SEAL RETAINER - GAP MEAS. EXCEEDED	Field	1	0.02	0.02				
ANM01LCPRPMPPTB				LOSS OF COOLANT TO HPOTP BEARINGS											
MSFC PRACA	A08751	22-Jun-79	TURBOMACHINERY	STRUT TURB DISCHARGE	RS007779-021		LET PARTIALLY OBSTRUCTED	Field	1	0.02	0.02				
MSFC PRACA	A12733	14-Feb-86	TURBOMACHINERY	ECCENTRIC RING	RS007879-005		ECCENTRIC RING FOUND CRUSHED POST STB-32	Field	1	0.02	0.02				
ANM188PRPMPPTB				HPFTP THRUST BALL FAILURE								0.02			
MSFC PRACA	A13928	3-Apr-87	TURBOMACHINERY	RING, ASSY OF	R0019213-001	IFA STB-37-E1, HPFTP 8008 THRUST BALL CRACKED POST R.T.	HPFTP THRUST BALL CRACKED POST STB-37 - NO EFFECT	Field	1	0.02	0.02	0.02			
ANM120DPRPMPONZ				HPOTP NOZZLE STRUCTURAL FAILURE											
MSFC PRACA	A11642	29-Jul-84	TURBOMACHINERY	NOZZLE, 2ND STAGE	R0016027-21	2ND STAGE NOZZLE CRACKS IN TURNING VANES, HPOTP UN 1800R		Field	1	0.02	0.02	0.06			
ANM188PRPMPPORR				HPOTP RETAINER RING FAILURE DUE TO LOSS OF BOLT PRELOAD											
MSFC PRACA	A10074	29-May-82	TURBOMACHINERY	WASHER	RS007873-003	CRACKED CUPWASHER, HPOTP, DISASSEMBLY	HPOTP CRACKED CUPWASHER, RECURRING PROBLEM AS PER REPORT BUT CONSEQUENCES UNKNOWN	Field	1	0.01	0.01				

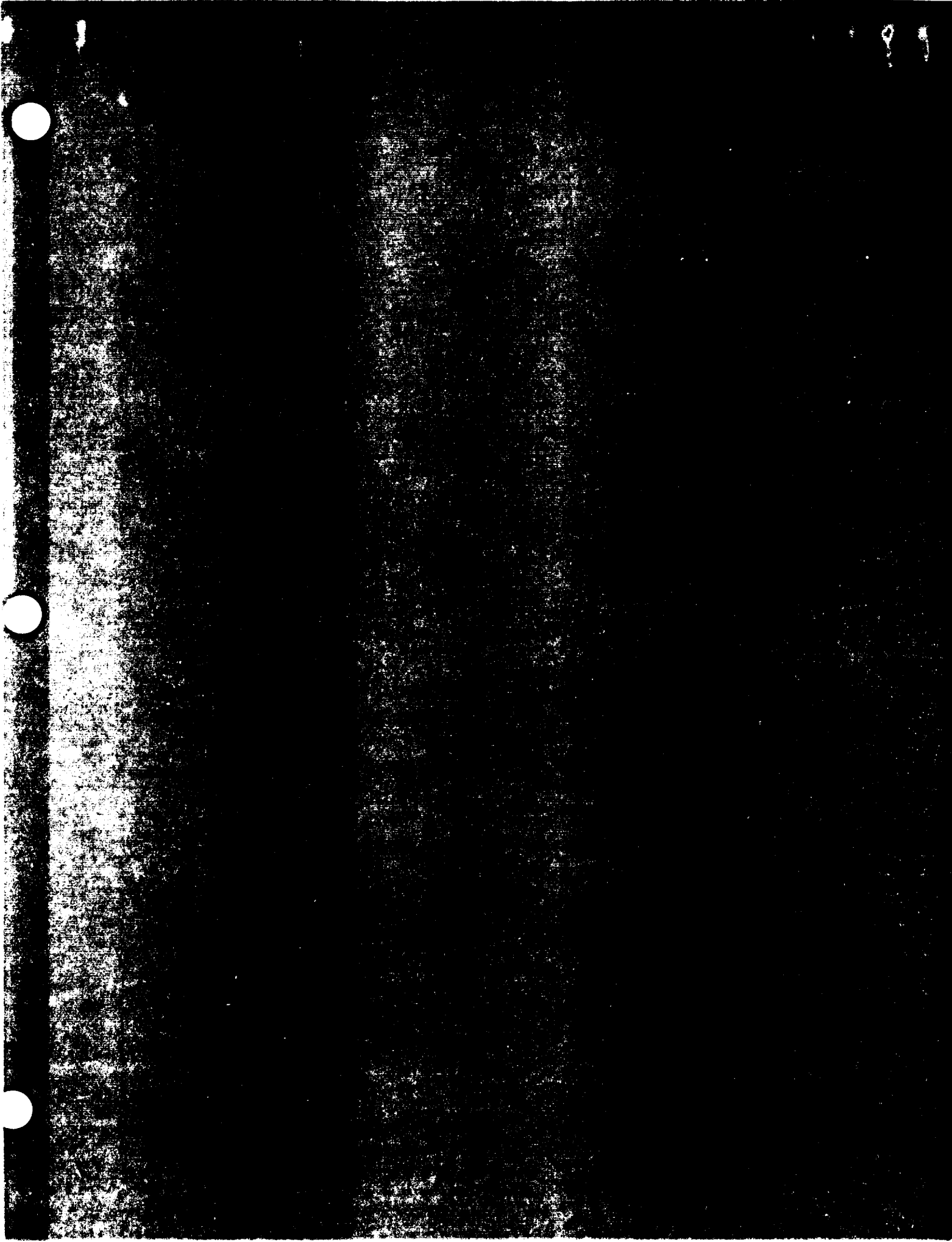
SSME/MPs Initiator Equivalent Flight Occurrences Evaluation												
Critical Structural Failure of SSME Component												
Record Type	Record #	Date	System Element	NCA Nomenclature	NCA Part #	Failure Description from Record	Analyst Comments	Type	Configuration Applicability	Event Possibility Factor	Weighting Factor	Est. Flight Failure or Total Time
MSFC PRACA	A10157	2-Jul-82	TURBOMCHNERY	CUPWASHER	RS007704-003	BROKEN CUPWASHER HPOTP DISASSEMBLY	HPOTP CRACKED CUPWASHERS. DEBRIS PEENS THE SURFACE OF THE MAIN IMPELLER OUTER SHROUD. RETAINERS RING AND SILVER SEAL AT THE PRESSURE SENSING ORifice AREA	Field	1	0.01	0.01	
MSFC PRACA	A10157	2-Jul-82	TURBOMCHNERY	CUPWASHER	RS007704-003	BROKEN CUPWASHER HPOTP DISASSEMBLY	HPOTP CRACKED CUPWASHERS. DEBRIS PEENS THE SURFACE OF THE MAIN IMPELLER OUTER SHROUD. RETAINERS RING AND SILVER SEAL AT THE PRESSURE SENSING ORifice AREA	Field	1	0.01	0.01	
MSFC PRACA	A12196	19-Apr-85	TURBOMCHNERY	CUPWASHERS	R032220-3	CUPWASHERS (2) ROTATED DURING HOT FIRE HPOTP UN 222R1, ENGINE 2022	3 ROTATED CUPWASHERS IN HPOTP	Field	1	0.01	0.01	
MSFC PRACA	A12197	19-Apr-85	TURBOMCHNERY	CUPWASHERS	R032220-3	CUPWASHERS (2) ROTATED DURING HOT FIRE HPOTP UN 418R1, ENGINE 2028	2 ROTATED CUPWASHERS	Field	1	0.01	0.01	0.18
MSFC PRACA	A11825	17-Dec-84	TURBOMCHNERY	TURBINE END #3 BRNG	RS007955-301	NO. 3 BEARING INNER RACE CRACK, HPOTP UN 810R1		Field	1	0.02	0.02	
MSFC PRACA	A05502	28-Aug-78	TURBOMCHNERY	HPOTP UN 0007R2	RS007701-271	SPALLED BALLS AND SURFACE DISTRESS/RACES	SPALLED BALLS & SURFACE DISTRESS OF RACES CAUSED SUB SYN VIB - MAYBE STRUCTURAL	Field	1	0.02	0.02	
MSFC PRACA	A05502	28-Aug-78	TURBOMCHNERY	HPOTP UN 0007R2	RS007701-271	SPALLED BALLS AND SURFACE DISTRESS/RACES	SPALLED BALLS & SURFACE DISTRESS OF RACES CAUSED SUB SYN VIB - MAYBE STRUCTURAL	Field	1	0.02	0.02	
MSFC PRACA	A05503	26-Aug-78	TURBOMCHNERY	HPOTP UN 0007R2	RS007701-271	SURFACE DISTRESS ON RACES		Field	1	0.02	0.02	
MSFC PRACA	A05344	3-Apr-79	TURBOMCHNERY	HPOTP UN 2404	33DRS007701-171	SPALLED BALLS AND GAGE DELAMINATION		Field	1	0.02	0.02	
MSFC PRACA	A11825	17-Dec-84	TURBOMCHNERY	TURBINE END #3 BRNG	RS007955-301	NO. 3 BEARING INNER RACE CRACK, HPOTP UN 810R1		Field	1	0.02	0.02	
MSFC PRACA	A11989	20-Jan-85	TURBOMCHNERY	BEARING #4	RS007955-301	CRACKS IN #4 TURBINE END BEARING RACE, HPOTP UN 810R1		Field	1	0.02	0.02	
MSFC PRACA	A14156	1-Aug-87	TURBOMCHNERY	HPOTP UN 4000R3	RS007701-531	HPOTP UN 4000R3 STRAIN GAGE DATA DISCREPANCY, BEARING WEAR		Field	1	0.02	0.02	
MSFC PRACA	A14782	23-Mar-88	TURBOMCHNERY	HPOTP UN 4000R2	RS007701-531	HPOTP UN 4000R2 BEARING GAGE FREQUENCIES		Field	1	0.02	0.02	
ANMHOEVRPMPHOEV			HPOTP EXCESSIVE VIBRATION									0.02
MSFC PRACA	A15189	12-Jan-89	TURBOMCHNERY	HPOTP	RS007701-581	HIGH SYNCHRONOUS VIBRATIONS ON HPOTP UN 8409, STS-44		Field	1	0.02	0.02	
ANMLSPRPMPM			IM LOX POST STRUCTURAL FAILURE									0.06
MSFC PRACA	A05915	16-Dec-78	COMBUSTION	MAIN INJECTOR	RS009122-391	SLIGHT LOW PORT EROSION		Field	1	0.02	0.02	
MSFC PRACA	A09789	22-Oct-80	COMBUSTION	RETAINER	RS009133-011	RETAINER BURNT/THRU & GALLING		Field	1	0.02	0.02	
MSFC PRACA	A09173	3-May-81	COMBUSTION	MAIN INJECTOR	RS009122-801	#8 RETAINER DAMAGE		Field	1	0.02	0.02	
ANMBESFRPMPMBE			BAFFLE ELEMENT INNER COPPER JACKET BURNT/THROUGH									0.02
MSFC PRACA	B0707A087C	7-Oct-80	COMBUSTION	BAFFLE ELEMENT	R0019527-091	INNER COPPER JACKET BURNT/THROUGH		Field	1	0.02	0.02	
ANMFAERPRPMPFASI			EXTERNAL RUPTURE OF FPB AS FLOX LINE									0.02
MSFC PRACA	A07144	29-Aug-79	ENGINE	ENGINE SYSTEM	RS007001-081	FPB AS FLOX LINE RUPTURED		Field	1	0.02	0.02	
ANMFFBFRPMPFBFP			FPB FACEPLATE FAILURE DUE TO EROSION									0.06
MSFC PRACA	A04877	18-Apr-78	COMBUSTION	FPB INJECTOR	RS009020-601	INJECTOR FACE EROSION		Field	1	0.02	0.02	
MSFC PRACA	A06846	25-Nov-81	COMBUSTION	FPB INJECTOR	RS009020-821	EROSION ON INJECTOR FACEPLATE		Field	1	0.02	0.02	
MSFC PRACA	A08817	28-Jan-82	COMBUSTION	FPB INJECTOR	RS009020-771	EROSION AND SLAG ON INJECTOR FACEPLATE		Field	1	0.02	0.02	

SSME/MPS Initiator Equivalent Flight Occurrences Evaluation

SSME/MPS Initiator Equivalent Flight Occurrences Evaluation		Nominal Ope		
Initiator ID	Cause ID	Description	Source	Equivalent Flight Failures for Total Exposure Time
SMEST		Structural Failure of SSME Components Leading to LOV		0.00
	ANMWSFRPMMCCMW	MCC MANIFOLD WELD FAILURE	MCC PRA	0.10
	ANMEDDBRPMDNCO	FAILURE IN EDNI LINER CLOSEOUT STRUCTURE	MCC PRA	0.07
	ANMHWCRPRPMMCCCHW	MCC HOT GAS WALL FAILURE DUE TO UNSTABLE CRACK GROWTH	MCC PRA	0.02
	ANMFRBTTPRPMFRI	FAILURE OF FLOW RECIRCULATION INHIBITOR	MCC PRA	0.02
	ANMCCCRPRPMMCCCC	FAILURE OF MCC COOLANT CHANNEL DUE TO UNSTABLE CRACK GROWTH	MCC PRA	0.00
	ANMBSFRPMMCCBP	MCC MULTIPLE BOLT FAILURE DUE TO INADEQUATE PRELOAD	MCC PRA	0.04
	ANMHMWFPRPMHGMWF	HGM TRANSFER TUBE WELD FAILURE	WELD STUDY	0.01
SMEHL		Hydraulic Lock-up Required	PRA APU Analysis	1.59
SMELP		Propellant Management System And/Or SSME Combustible Leakage	Lockheed PRA	0.32
SMELH		Helium System Leakage	Lockheed PRA	0.26
SMEPG		Failure To Provide Helium Pogo Charge	NPRD-3	0.24
SMEPV		Failure To Maintain Propellant Supply System Valve Positions	MPS F.R.D., NPRD91	
SMEDS		Simultaneous Dual SSME Shutdown	See Fault Tree in Next Section	
SMECD		Nominal MECO & Dump; No Mainstage Initiators	PRA Preliminary Results	



SSME/MPS Initiator Frequency Summary									
Initiator ID	Initiator Description	Total Exposure Time		Cluster Initiator Freq (per mission)	Mean # of Missions Between Occurrences	Percent of Non- nominal Initiators	Development	621491 sec	
		Equivalent Flight Occurrences for Total Exposure Time	One Engine Initiator Freq (per mission)					Nominal Operation Time	520 sec
SMEFO	Loss of MCC Pressure	4.00	3.35E-03	1.00E-02	100	25.87%	Event Tree 1		
SMEFH	Loss of Gross H2 Flow	0.50	4.18E-04	1.25E-03	797	3.24%	Event Tree 2		
SMEMO	High Mixture Ratio in Oxidizer Preburner	0.25	2.09E-04	6.27E-04	1594	1.62%	Event Tree 3		
SMEMF	High Mixture Ratio in Fuel Preburner	0.25	2.09E-04	6.27E-04	1594	1.62%	Event Tree 4		
SMEPB	Loss of Fuel to Both Preburners	6.25	5.23E-03	1.56E-02	64	40.34%	Event Tree 5		
SMEVP	Failure to Maintain Proper SSME Propellant Valve Position	0.25	2.09E-04	6.27E-04	1594	1.62%	Event Tree 6		
SMELO	HPFTP Coolant Liner Overpressure	0.40	3.35E-04	1.00E-03	898	2.59%	Event Tree 7		
SMEST	Critical Structural Failure of SSME Components	1.13	9.53E-04	2.85E-03	350	7.38%	Fault Trees-Page 55		
SMEHL	Hydraulic Lock-up Required	1.59	1.33E-03	4.00E-03	250	10.34%	Event Tree 8		
SMELP	Propellant Management System And/OR SSME Combustible Leakage	0.32	2.65E-04	7.96E-04	1256	2.06%	Fault Trees-Page 54		
SME LH	Helium System Leakage	0.26	2.15E-04	6.46E-04	1548	1.67%	Event Tree 9		
SMEPG	Failure To Provide Helium Pogo Charge	0.24	2.02E-04	6.05E-04	1653	1.56%	Event Tree 10		
SMEPV	Failure To Maintain Propellant Supply System Valve Positions	0.01		1.89E-05	52910	0.05%	Fault Trees-Page 65		
SMEDS	Simultaneous Dual SSME Shutdown	0.00		1.00E-05	100000	0.03%	Fault Trees-Page 53 Event Tree 11		
SMECD	Nominal MECO & Durrp. No Mainstage Initiators	376		9.43E-01	1,060		Event Tree 12		



TRANSFER	PROTECTIVE EVENT	MITIGATING EVENT	SEQ. PROB.	CLASS	SEQUENCE DESCRIPTION	#
HIGH MIXTURE RATIO IN OPB	HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEFO/SMEMO	OR	EH				
2.30E-05 SMEFO/SMEMO			2.30E-05	OK abort		1
			2.67E-11	LOV	MO/EH	2
			3.45E-09	LOV	MO/OR	3

HIGH MIXTURE RATIO IN OXIDIZER PREBURNER EVENT TREE 1A REV. 1

INITIATOR	PROTECTIVE EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#	TRANSFER TO
LOSS OF GROSS H2 FLOW	CONTROLLER INCREASES O2 FLOW TO FPB					
SMEFH	OF					
SMEFH		1.25E-03	TRANSFER		1	SMEMF EVENT TREE
	PAGE 9	1.25E-07	TRANSFER	FH/OF	2	SMEPB EVENT TREE

TRANSFER	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
HIGH MIXTURE RATIO IN FPB	HPFTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEFH/SMEMF	FR	EH				
1.25E-03 SMEFH/SMEMF	1.50E-04 PAGE 13	1.16E-06 PAGE 3	1.25E-03	OK abort		1
			1.45E-09	LOV	MF/EH	2
			1.88E-07	LOV	MF/FR	3

HIGH MIXTURE RATIO IN FUEL PREBURNER EVENT TREE 2A REV. 1

TRANSFER	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
LOSS OF FUEL TO BOTH PREBURNERS	HPFTP OR HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEFH/SMEPB	TR	EH				
1.25E-07 SMEFH/SMEPB			1.25E-07	OK abort		1
			1.45E-13	LOV	PB/EH	2
			2.81E-15	LOV	PB/TR	3

LOSS OF FUEL TO BOTH PREBURNERS EVENT TREE 2B REV. 1

INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
HIGH MIXT. RATIO IN OPB	HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEMO	OR	EH				
6.27E-04 SMEMO	1.50E-04 PAGE 13	1.16E-06 PAGE 3	6.27E-04	OK abort		1
			7.27E-10	LOV	MO/EH	2
			9.41E-08	LOV	MO/OR	3

HIGH MIXTURE RATIO IN OXIDIZER PREBURNER EVENT TREE 3 REV. 1

INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#	
HIGH MIXTURE RATIO IN FPB	HPFTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN					
SMEMF	FR	EH					
SMEMF	PAGE 13	PAGE 3	6.27E-04	OK abort		1	
			7.27E-10	LOV		MF/EH	2
			9.41E-08	LOV		MF/FR	3

HIGH MIXTURE RATIO IN FUEL PREBURNER EVENT TREE 4 REV. 1

INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
LOSS OF FUEL TO BOTH PREBURNERS	HPFTP OR HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
	TR	EH				
SMEPB			1.56E-02	OK abort		1
			1.81E-08	LOV	PB/EH	2
			3.51E-10	LOV	PB/TR	3

LOSS OF FUEL TO BOTH PREBURNERS EVENT TREE 5 REV. 1

INITIATOR	MITIGATING EVENTS		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#	TRANSFER TO
	FAIL-SAFE SERVO SWITCH WORKS	EMERGENCY PNEUMATIC SHUTDOWN					
SMEVP	HL	EP					
6.27E-04 SMEVP	2.10E-06 PAGE 8	1.41E-04 PAGE 5	6.27E-04 1.32E-09 1.86E-13	TRANSFER OK abort LOV		1 2 3	SMEHL EVENT TREE

TRANSFER	PROTECTIVE EVENT		MITIGATING EVENT	SYSTEM EVENTS		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
	BY-PASS VALVE FAILS TO MOVE	NO VALVE DRIFT		EMERGENCY PNEUMATIC SHUTDOWN	MAIN ENGINE CUT-OFF				
SMEVP/SMEHL	BL	ND	EP	ME	PM				
6.27E-04 SMEVP/SMEHL						5.02E-04	OK		1
						8.28E-11	LOV	HL/PM	2
						7.17E-08	LOV	HL/ME	3
						1.25E-04	OK abort		4
						1.77E-08	LOV	HL/ND/EP	5
						1.45E-09	LOV	HL/BL	

FAILURE TO PERFORM HYDRAULIC LOCK-UP EVENT TREE 6A REV. 1

1.65E-07
PAGE 40

1.43E-04
PAGE 21

.20
PAGE 38

1.41E-04
PAGE 5

2.32E-06
PAGE 6

INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
COOLANT LINER OVERPRESSURE.	REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
	OP	EH				
SMELO			1.00E-03	OK abort		1
SMELO			1.16E-09	LOV	LO/EH	2
			1.50E-07	LOV	LO/OP	3

COOLANT LINER OVERPRESSURE EVENT TREE 7 REV. 1

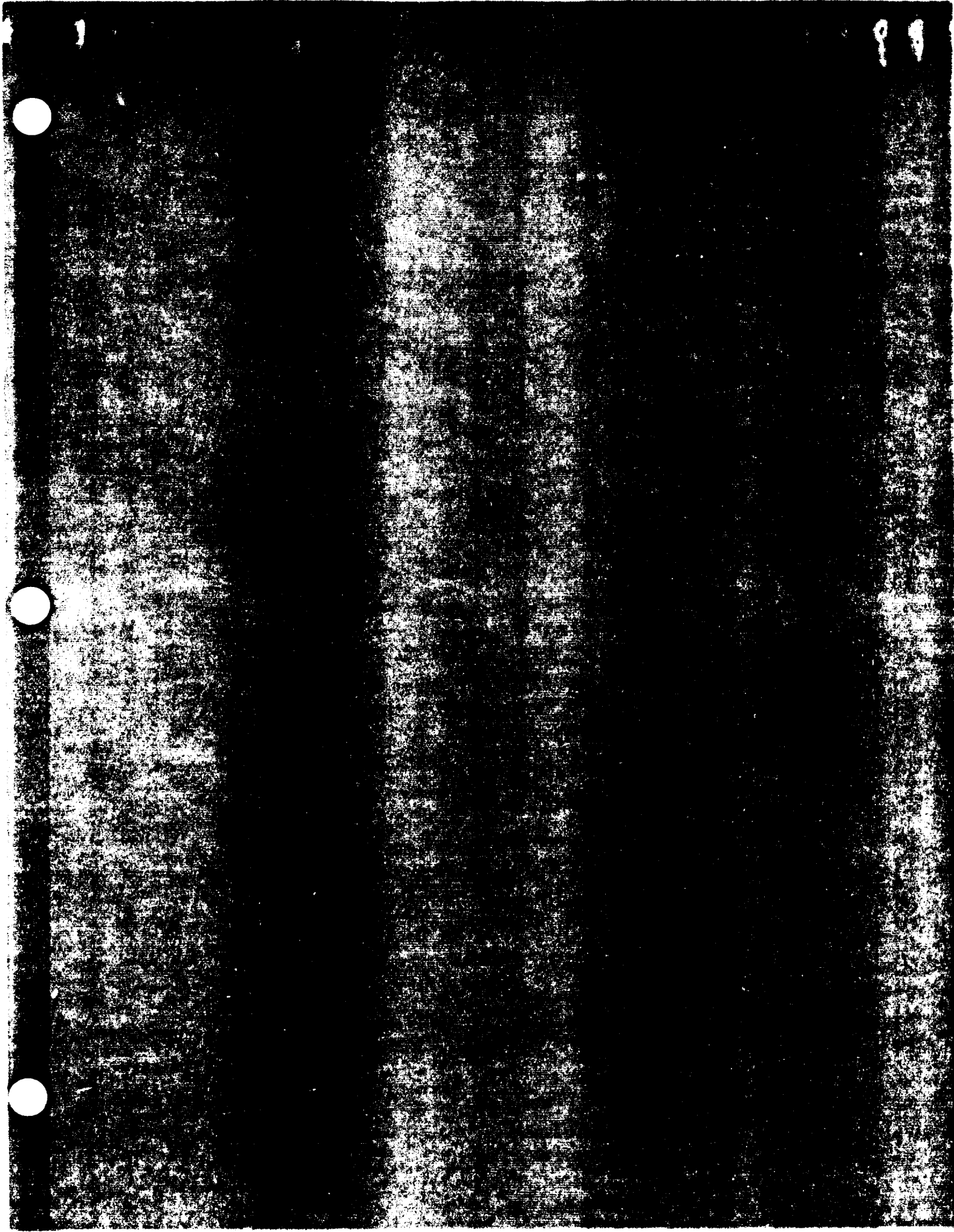
INITIATOR	PROTECTIVE EVENT		MITIGATING EVENT	SYSTEM EVENTS		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
	BY-PASS VALVE FAILS TO MOVE	NO VALVE DRIFT		EMERGENCY PNEUMATIC SHUTDOWN	MAIN ENGINE CUT-OFF				
SMEHL	BL	ND	EP	ME	PM				
SMEHL	PAGE 38		PAGE 5	PAGE 21	PAGE 40	3.20E-03	OK		1
	PAGE 6					5.28E-10	LOV	HL/PM	2
						4.58E-07	LOV	HL/ME	3
						8.00E-04	OK abort	HL/ND/EP	4
						1.13E-07	LOV	HL/BL	5
					9.28E-09	LOV			

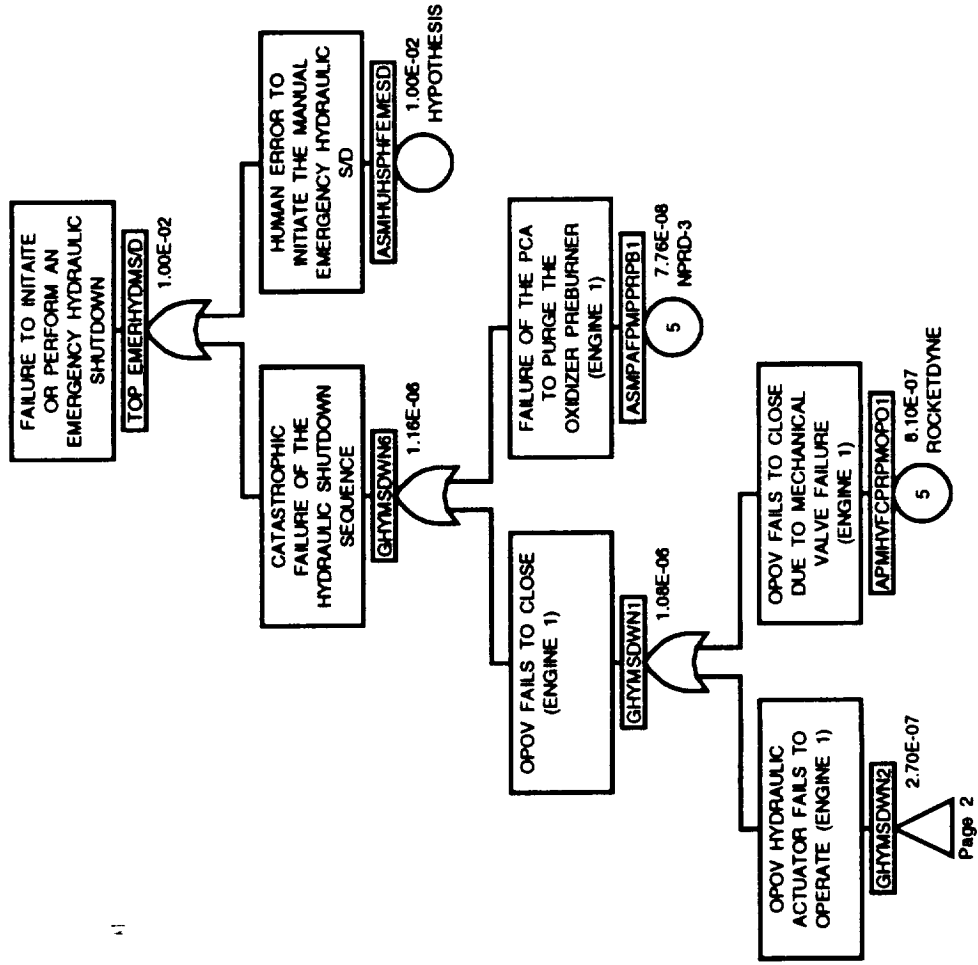
INITIATOR	MITIGATIVE EVENT		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
DUAL SSME PREMATURE SHUTDOWN	DUAL SSME PREMATURE S/D BEFORE LIFT-OFF	DUAL SSME PREMATURE S/D AFTER DROOP(109)				
SMEDS	BL	AC				
1.00E-05 SMEDS	1.0 BASIC EVENT	.65 BASIC EVENT	0.00E+00	OK abort		1
			3.54E-06	OK abort		2
			6.46E-06	LOV	DS/BL/AC	3

DUAL SSME PREMATURE SHUTDOWN EVENT TREE 11 REV. 1

INITIATOR	SYSTEM EVENT		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
	MECO PERFORMED	PROPELLANT DUMP PERFORMED				
NOMINAL MECO AND PROPELLANT DUMP REQUIRED						
SMECD	MN	PD				
.94 SMECD			9.43E-01	OK		1
			1.56E-07	LOV	CD/PD	2
			2.32E-06	LOV	CD/MN	3

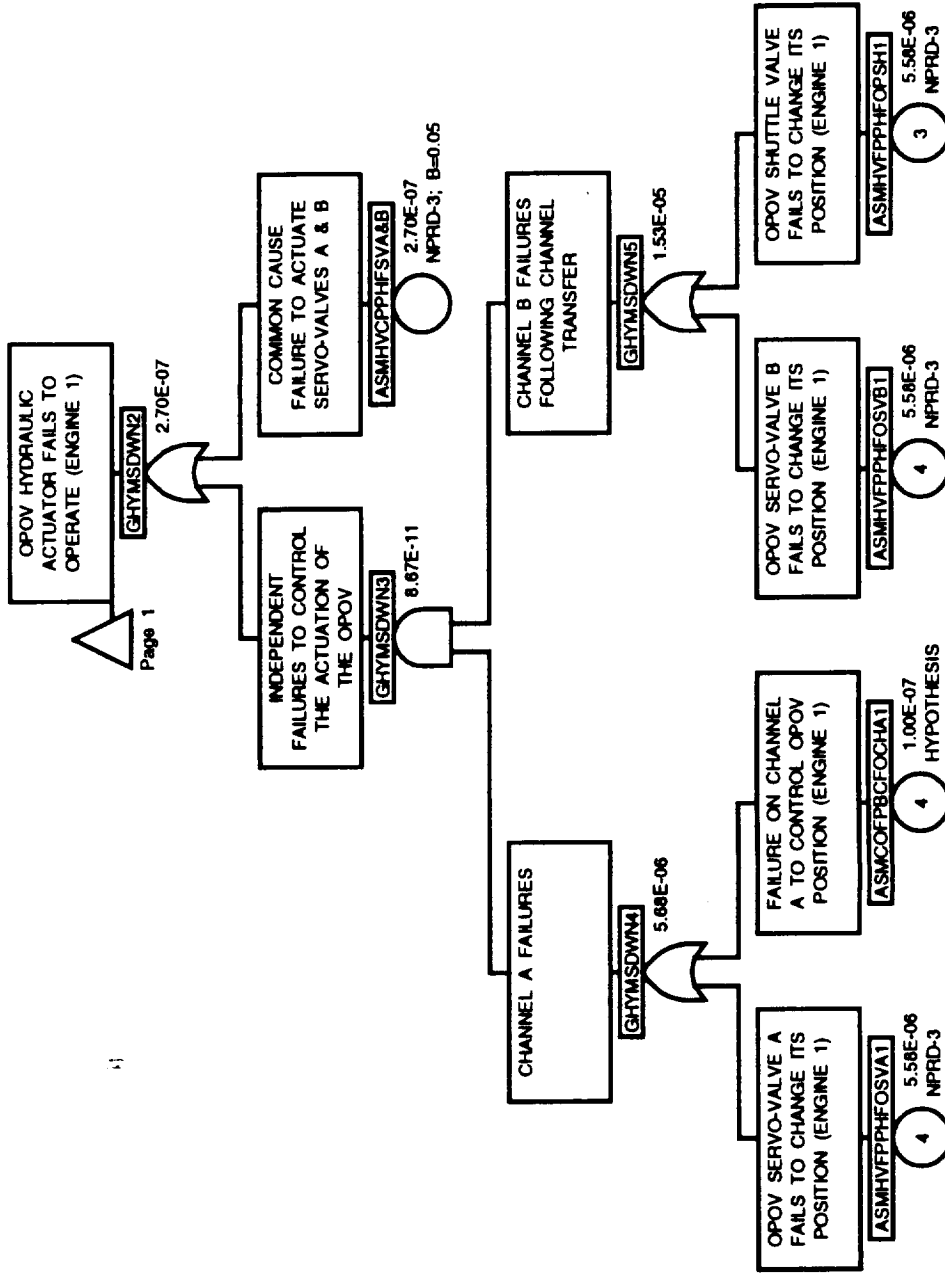
FAILURE TO PERFORM NOMINAL MECO & PROPELLANT DUMP EVENT TREE 12 REV. 1



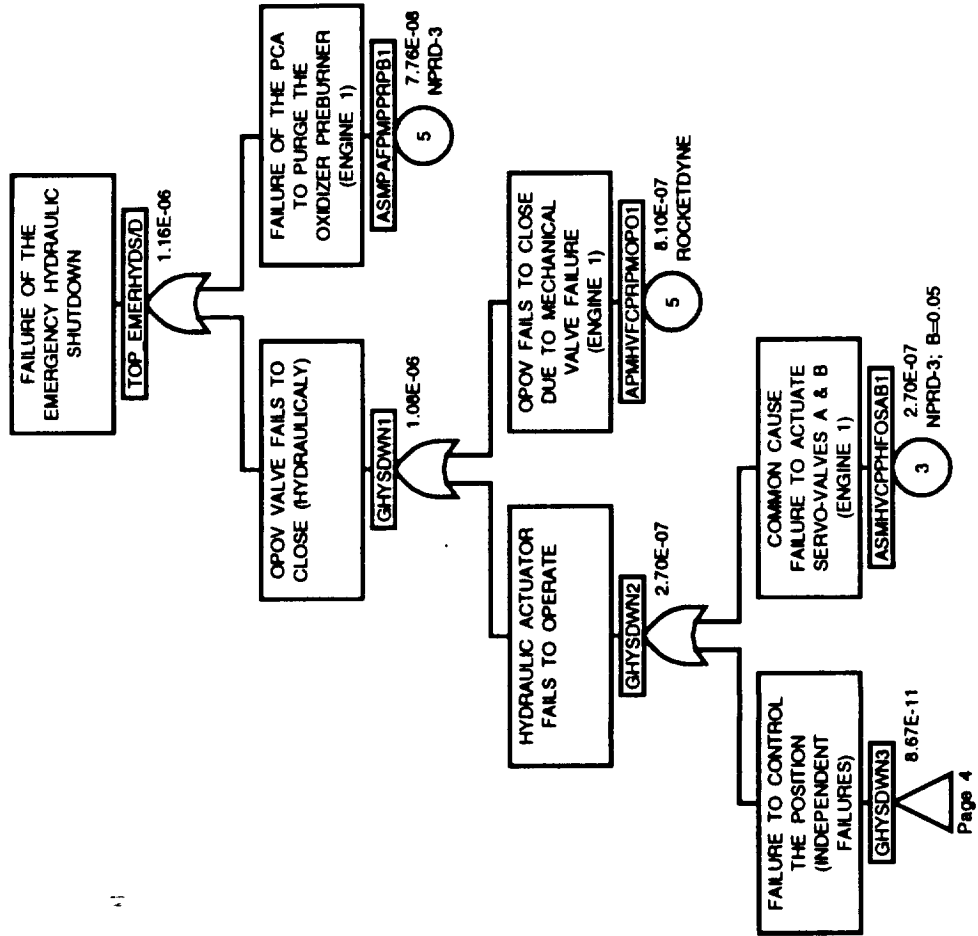


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Page 2

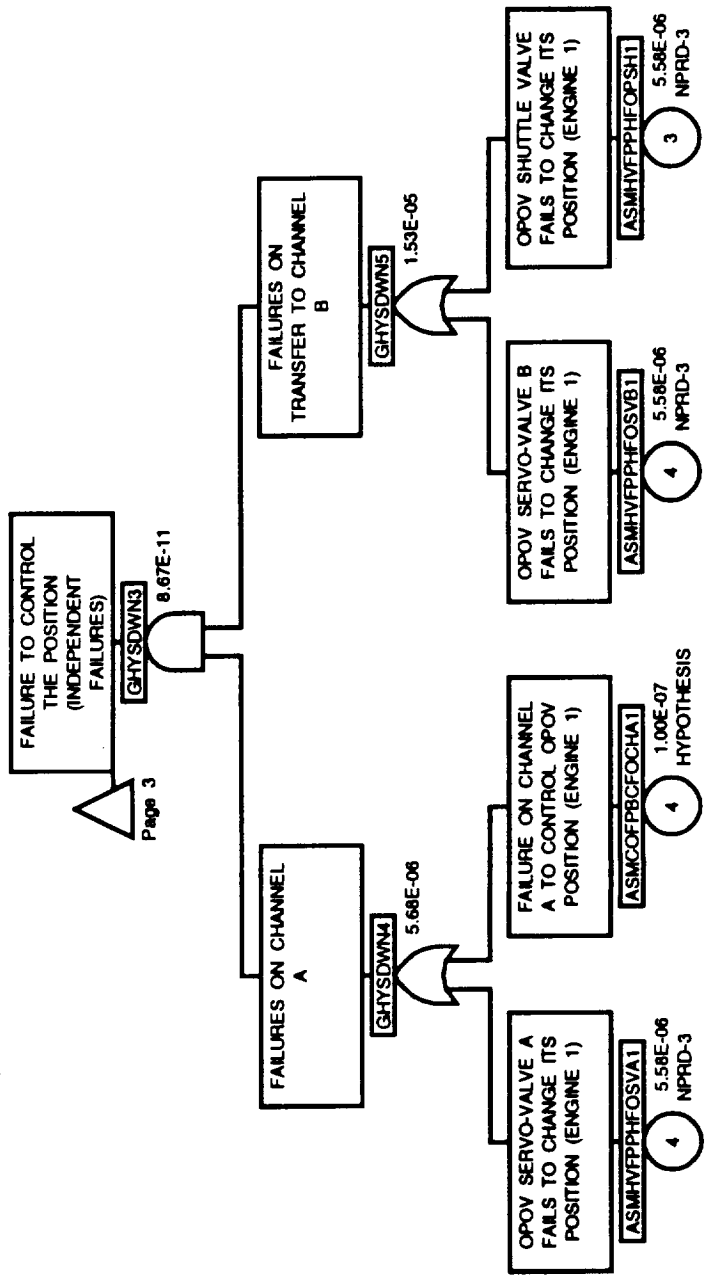


Page 1

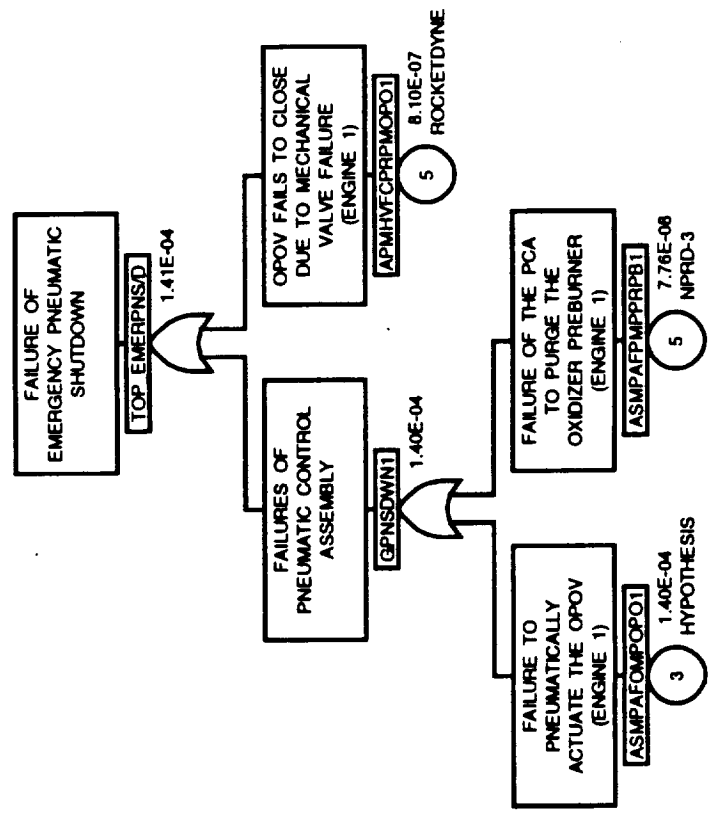


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Page 4



Page 3



BY-PASS VALVE FAILS
TO MOVE INTO LOCK-
UP POSITION

TOP FLBPVLUP

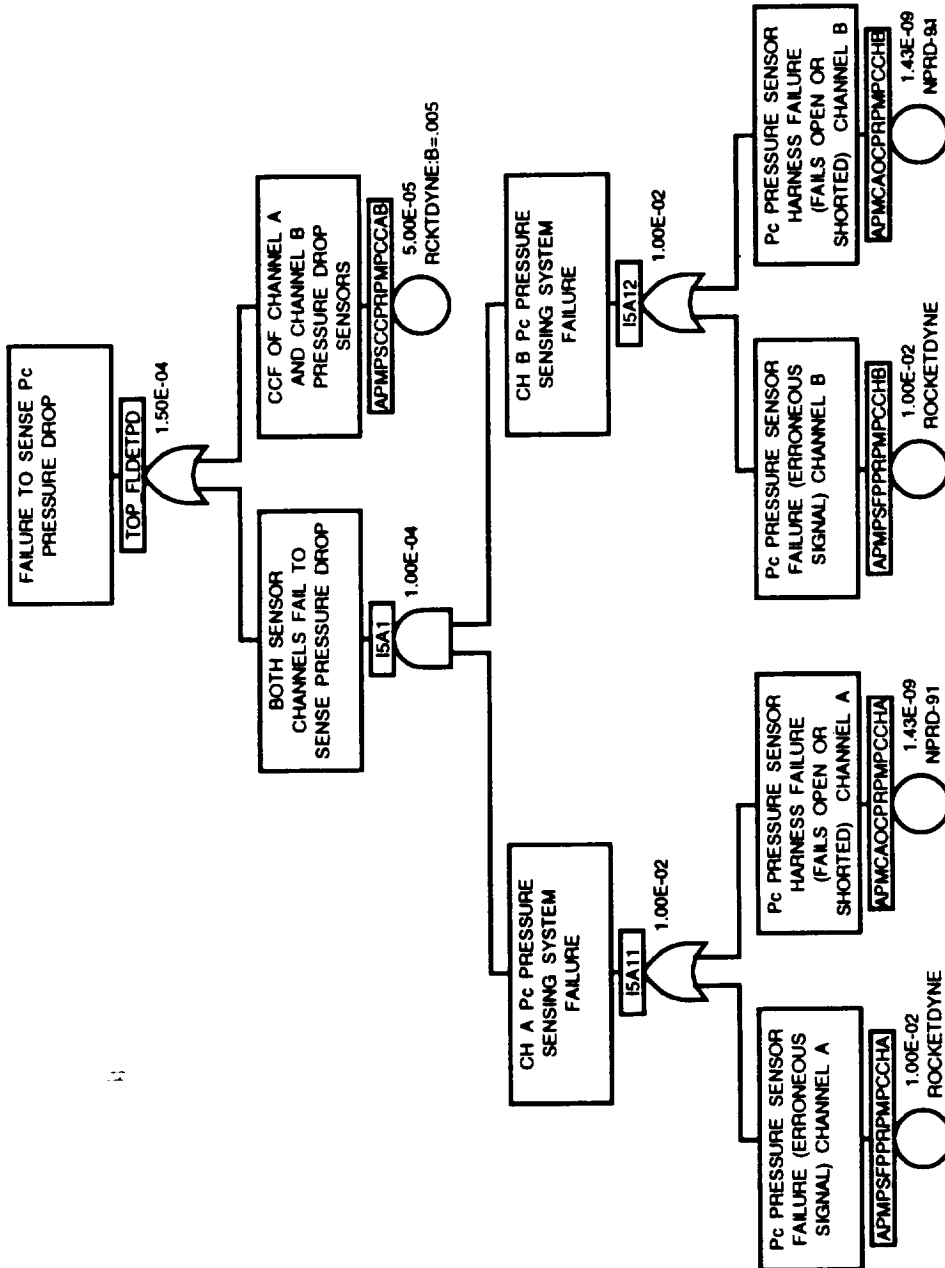
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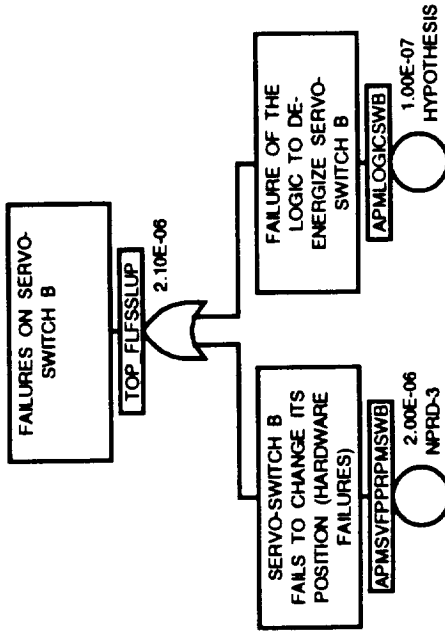
BY-PASS VALVE FAILS
TO CHANGE ITS
POSITION

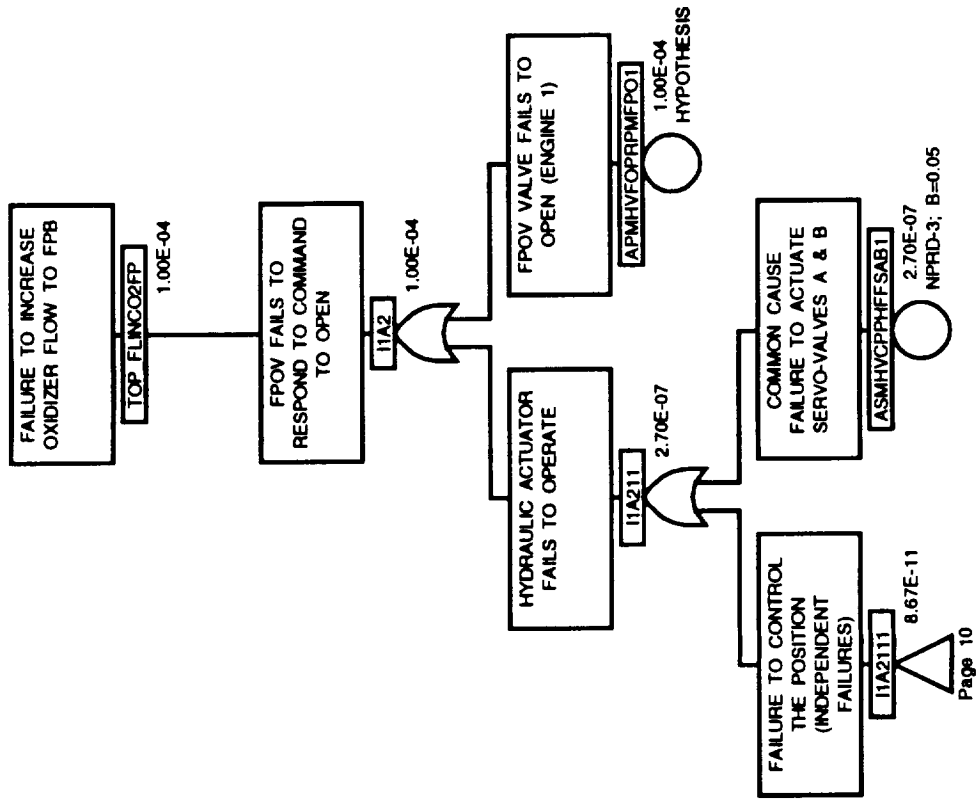
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NPRD-3



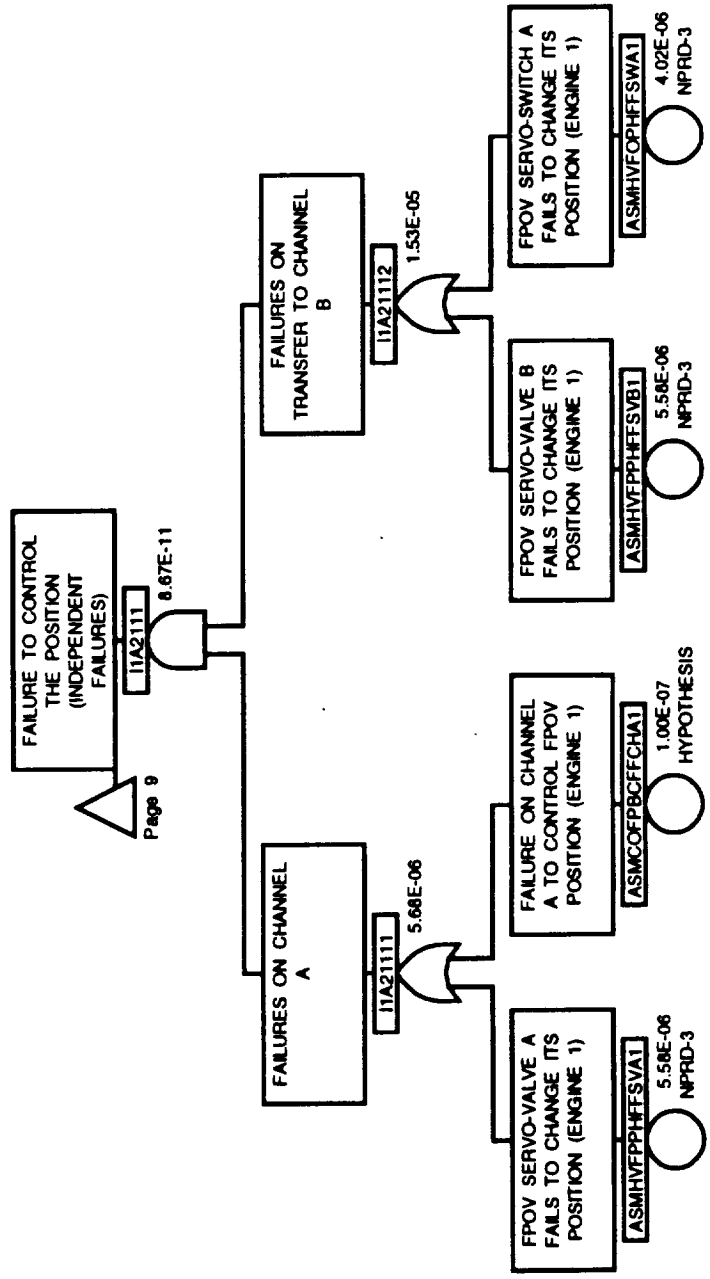




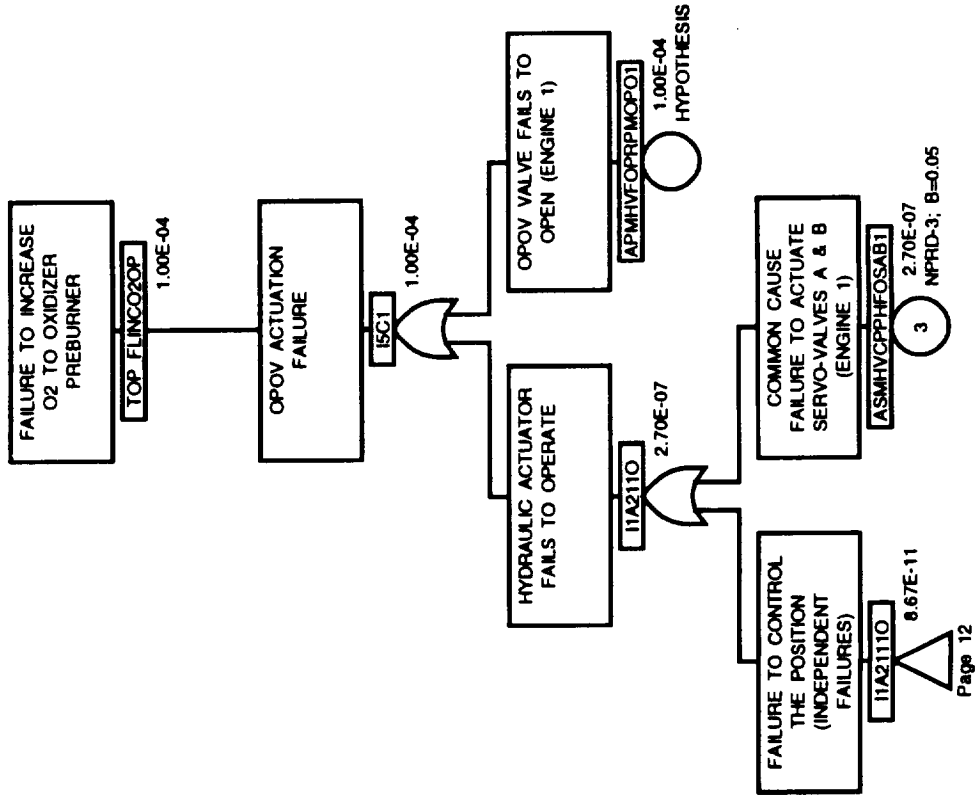
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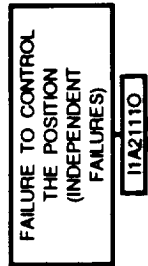
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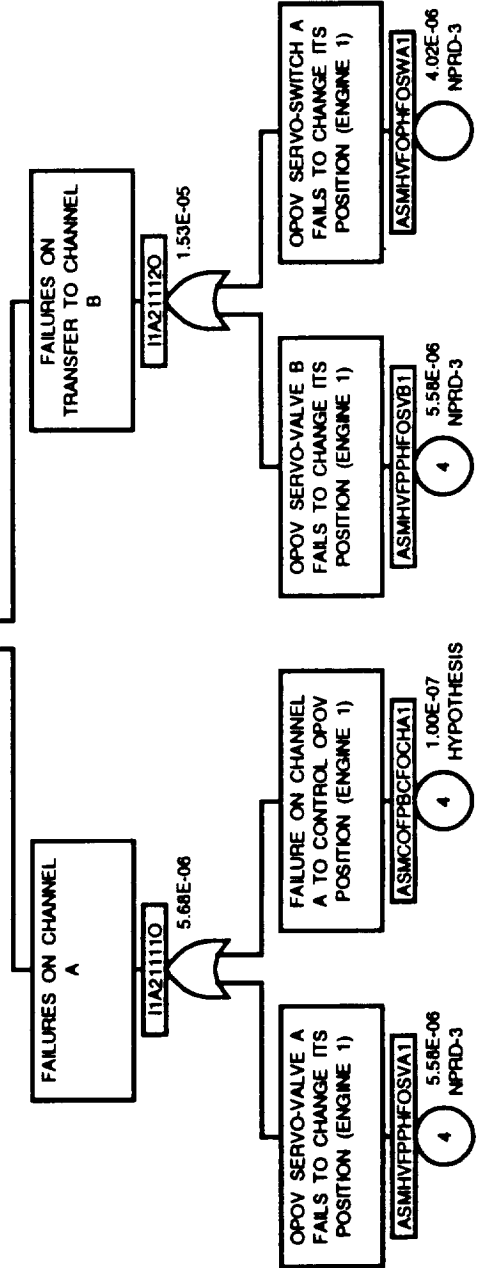


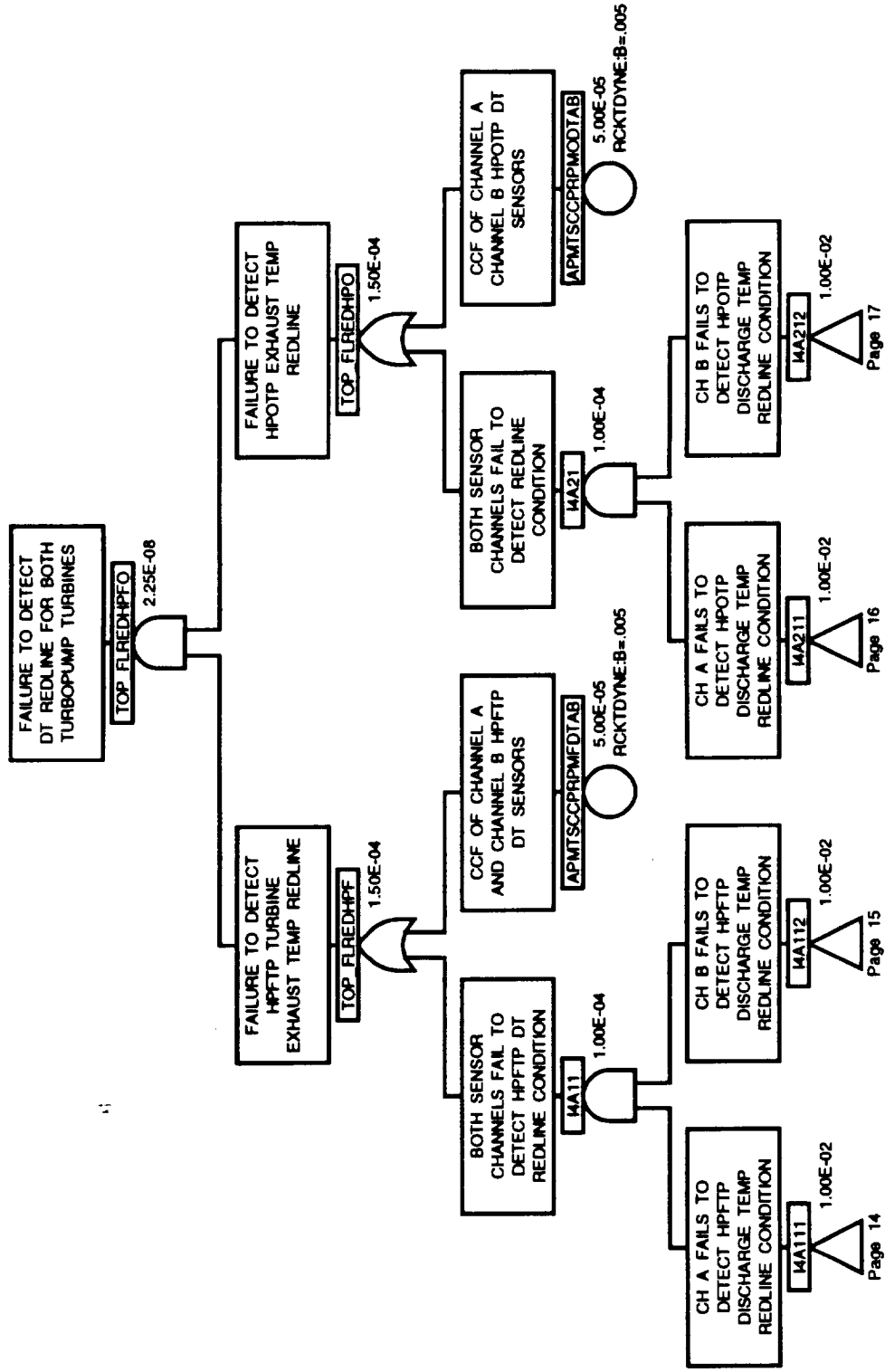
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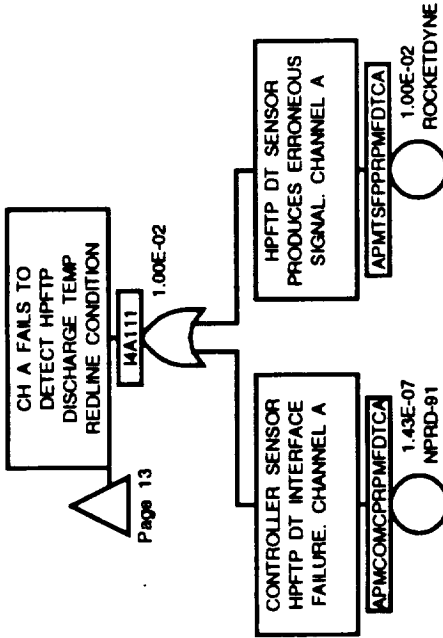


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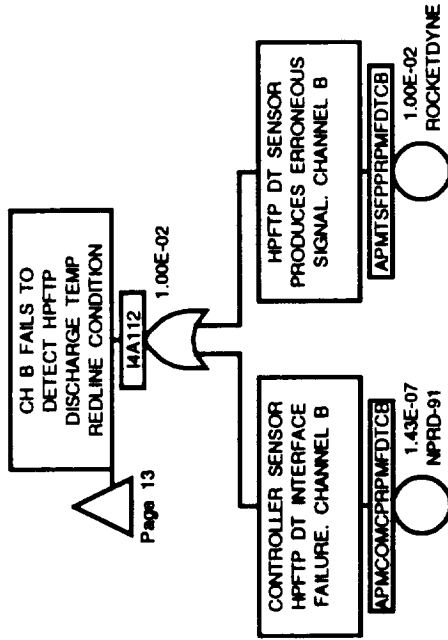




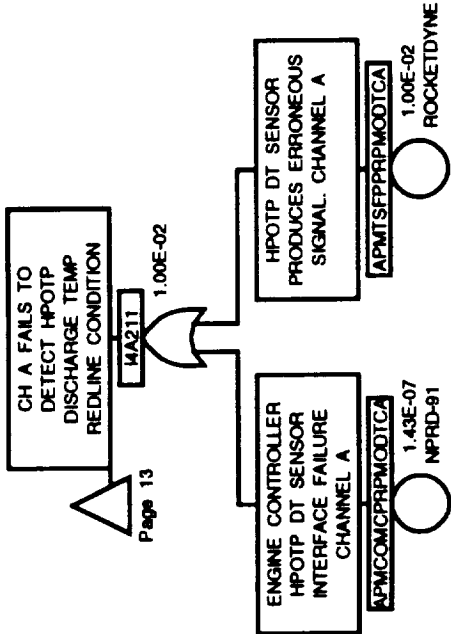
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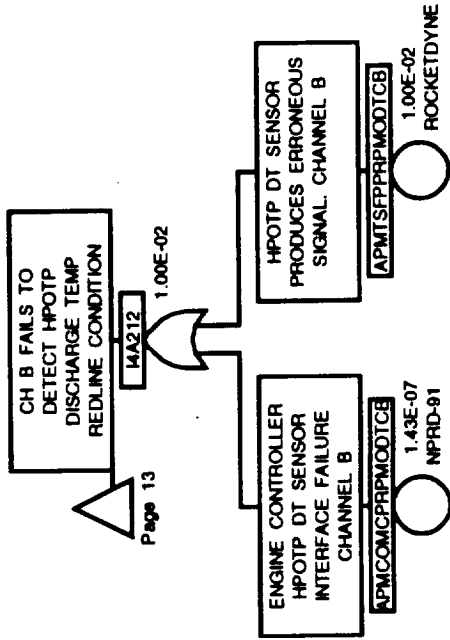
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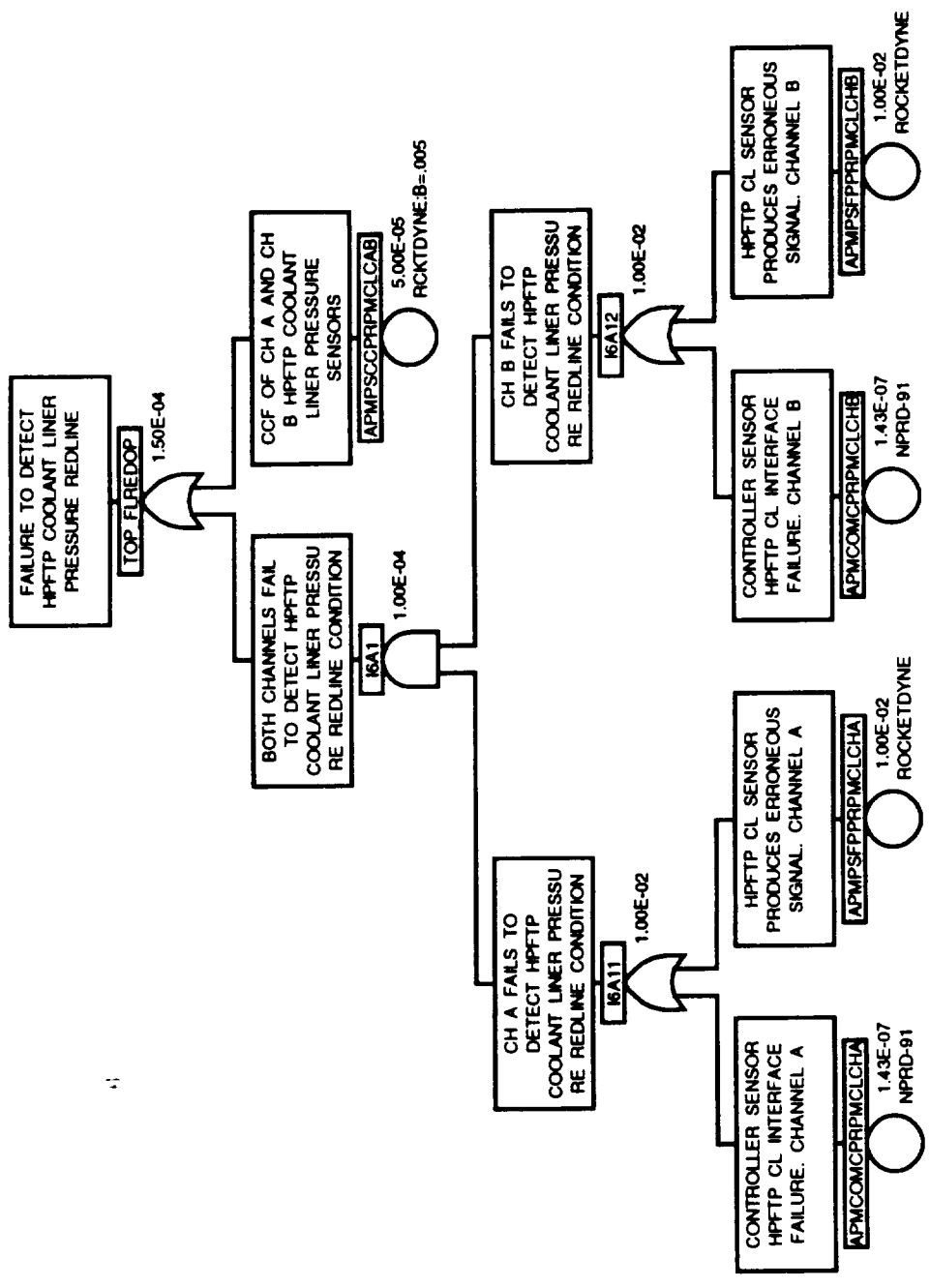
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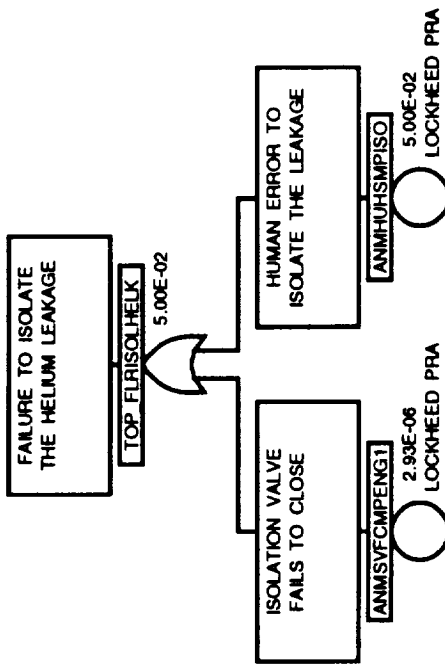


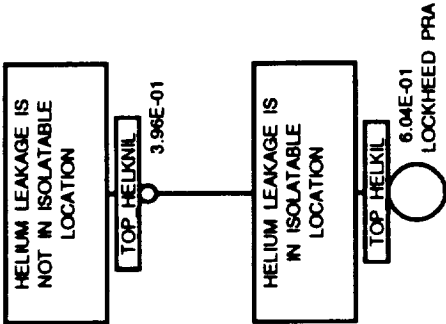
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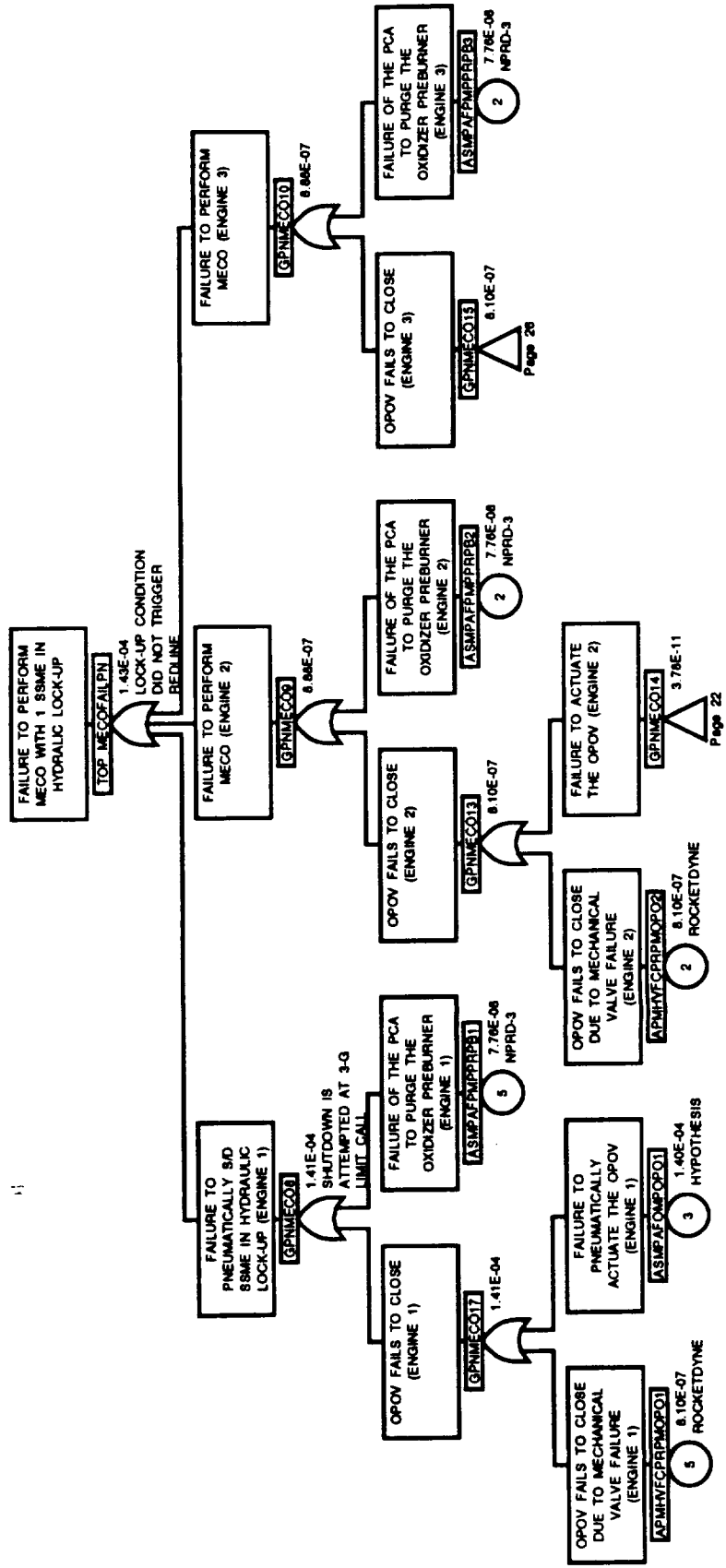


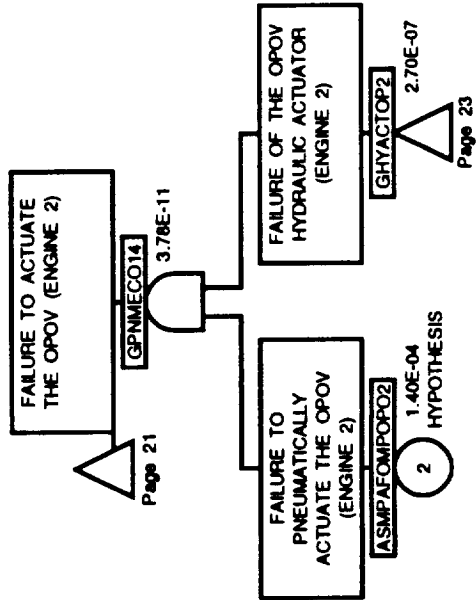
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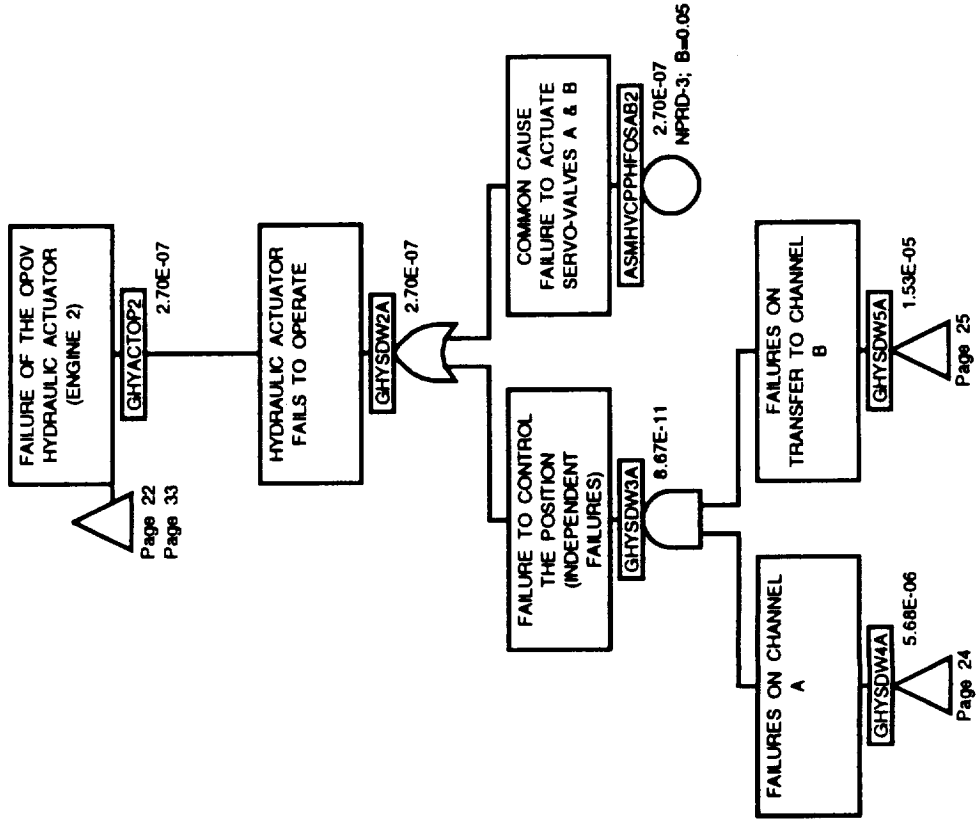


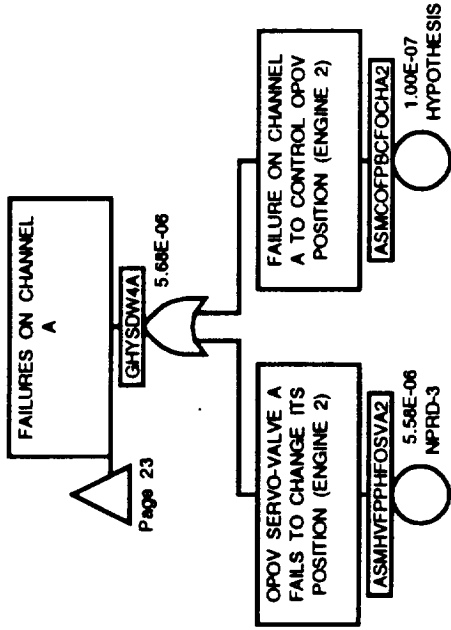




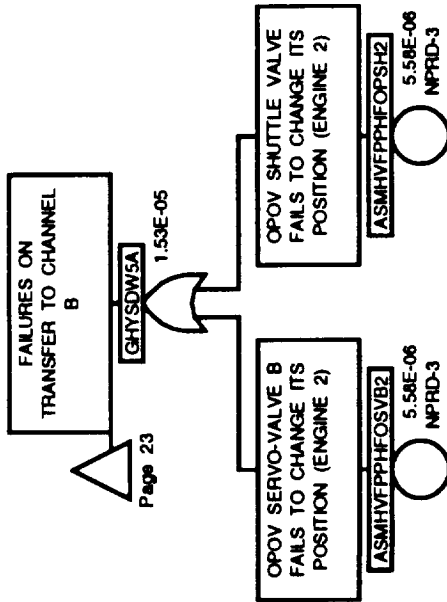




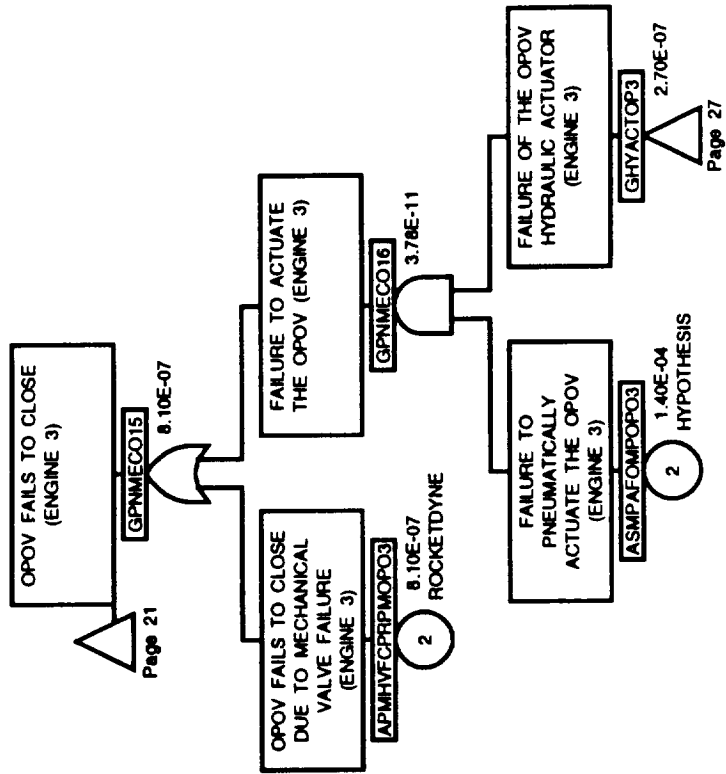


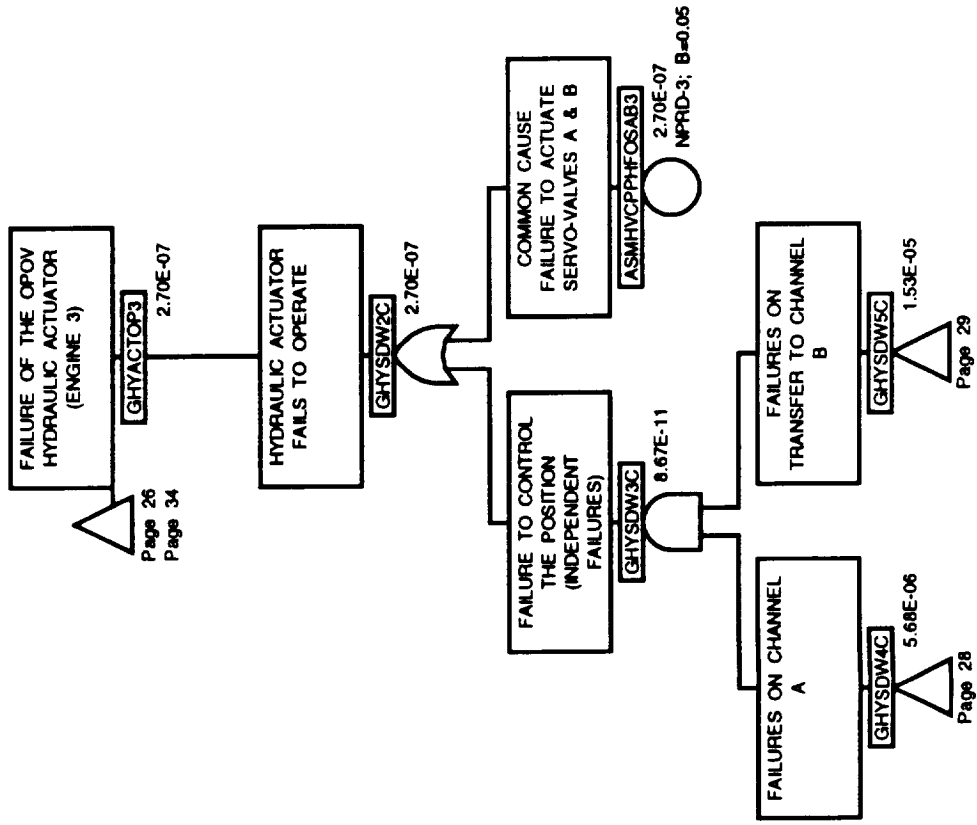


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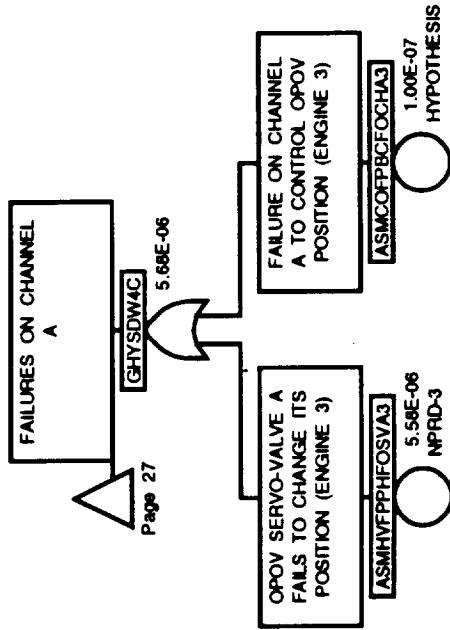


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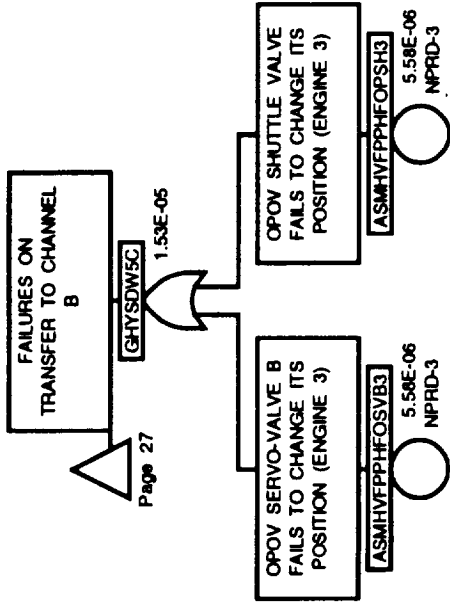




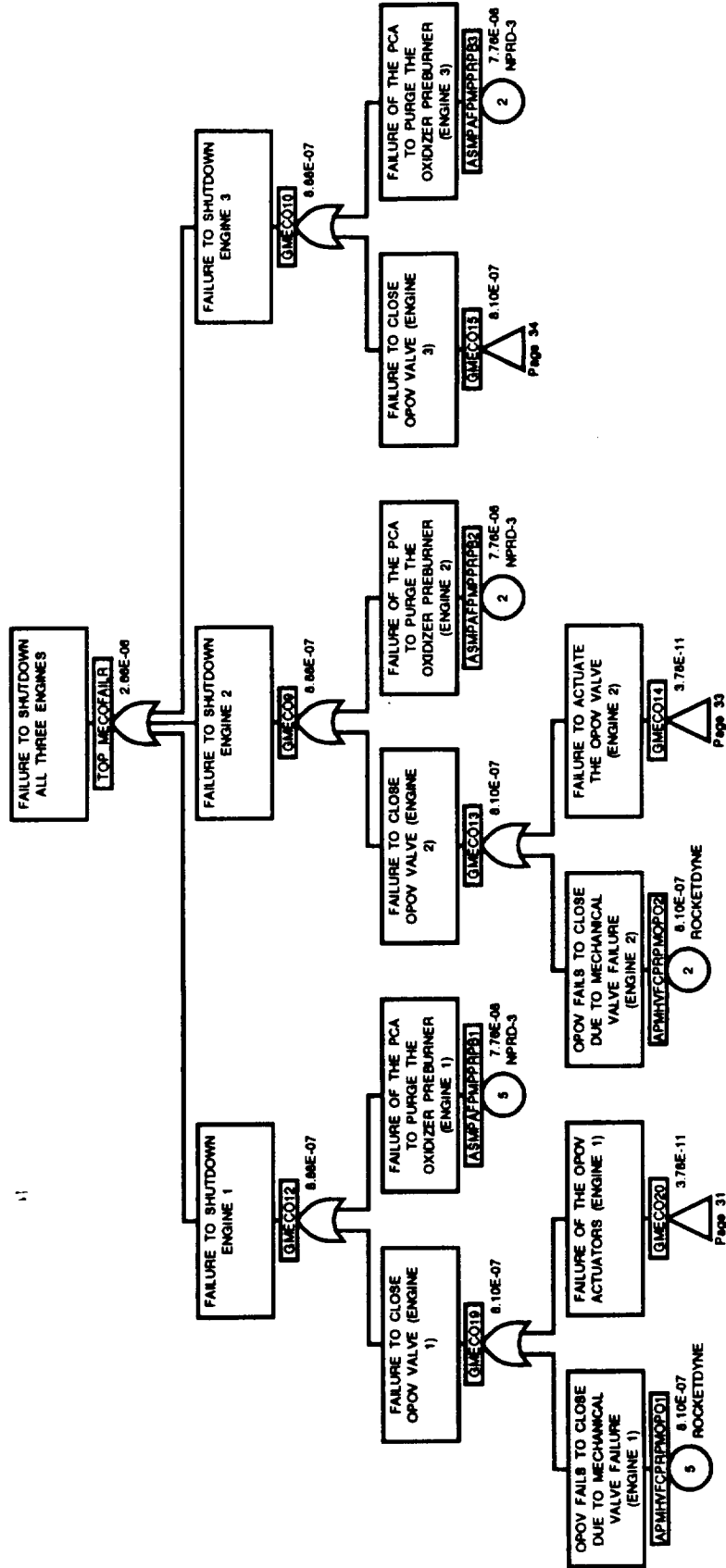
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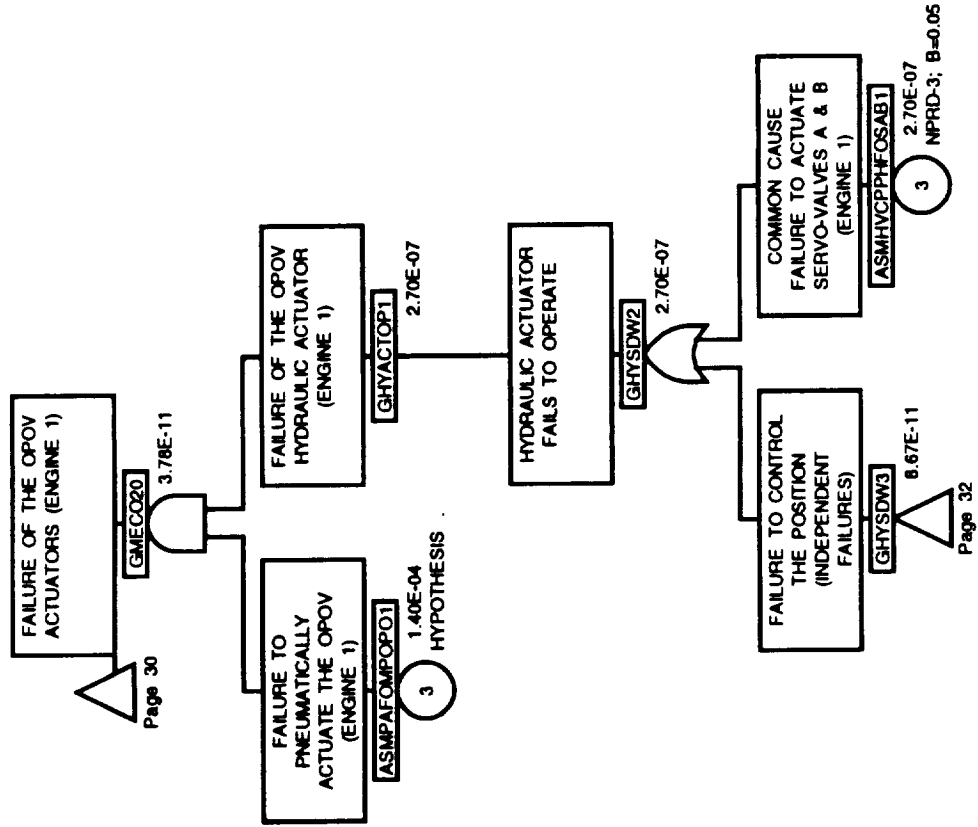


Page 27



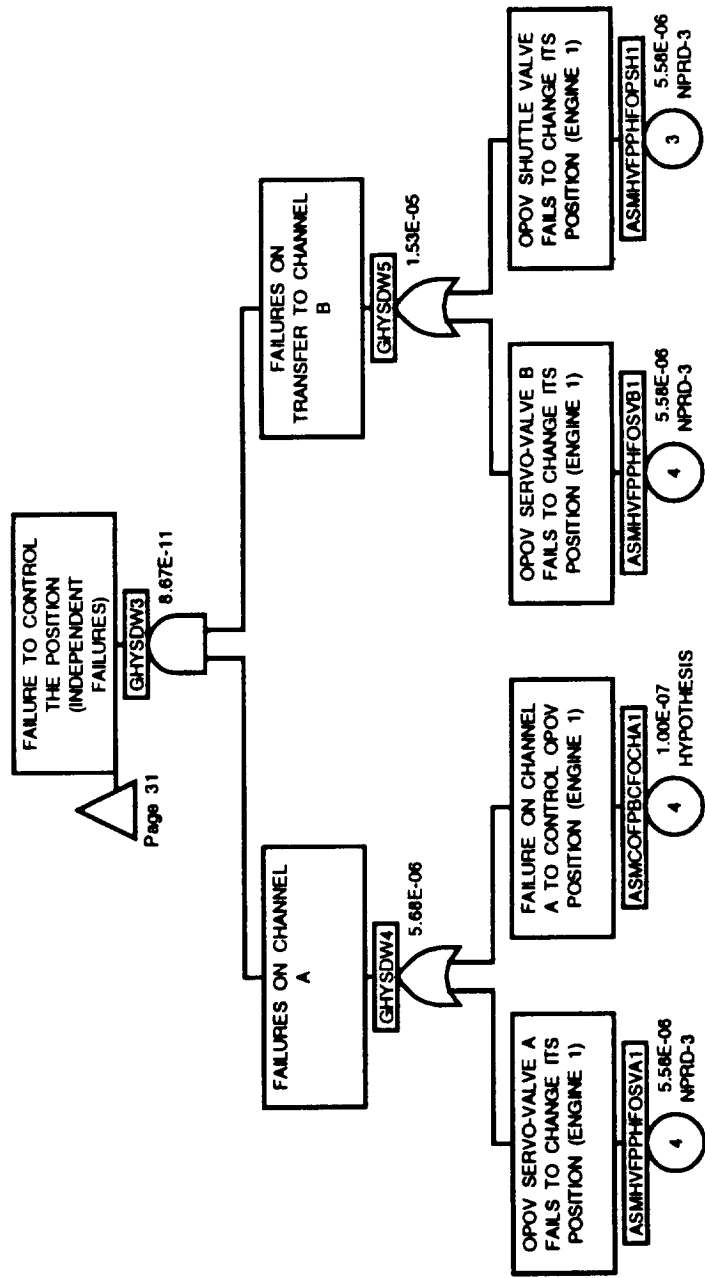
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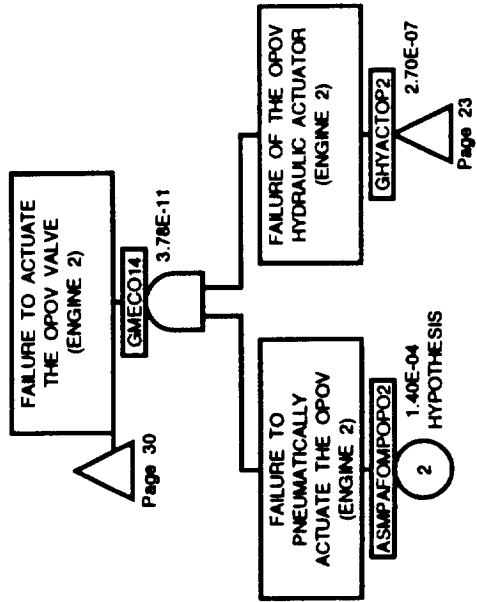


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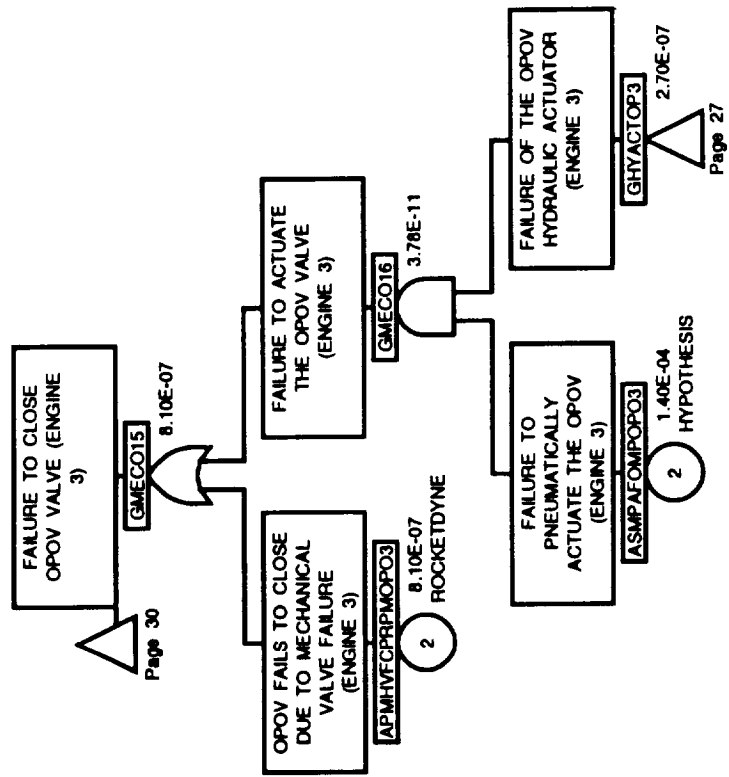
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Page 31

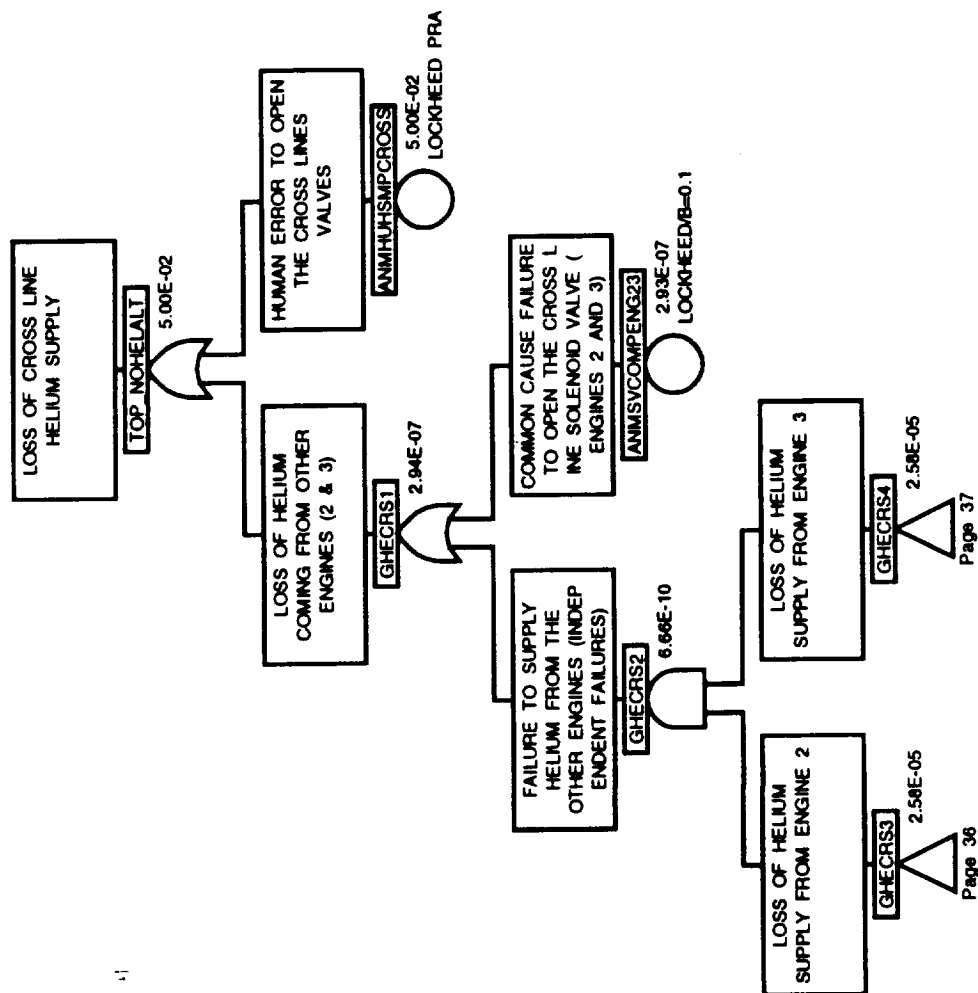


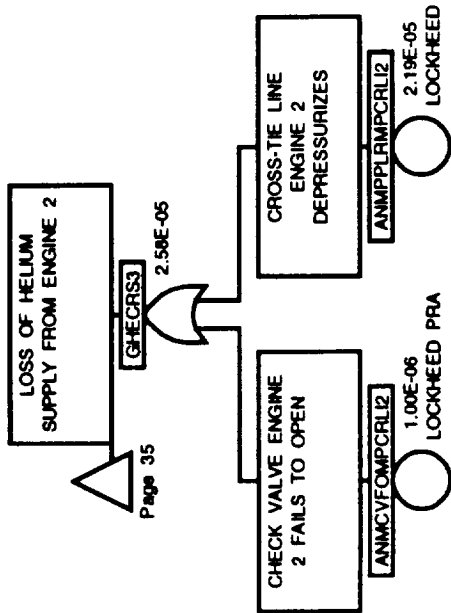
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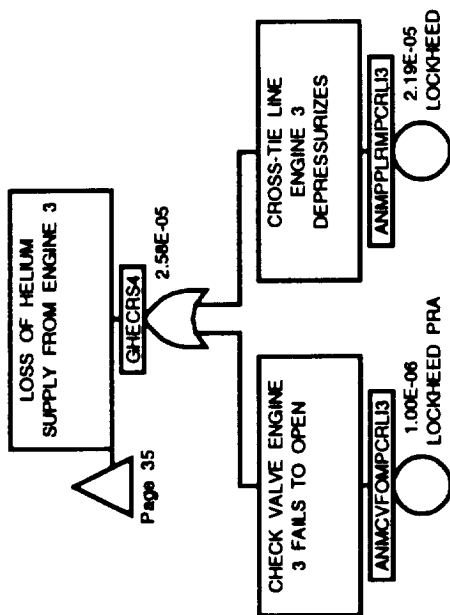
Page 30

Page 27





Page 35



Page 35

NO VALVE DRIFT OR
DRIFT NOT CAUSING
REDLINE

TOP NOVLDRIFT

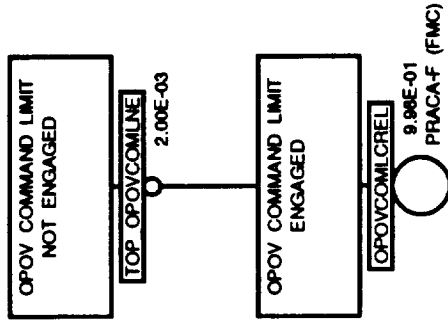
8.00E-01

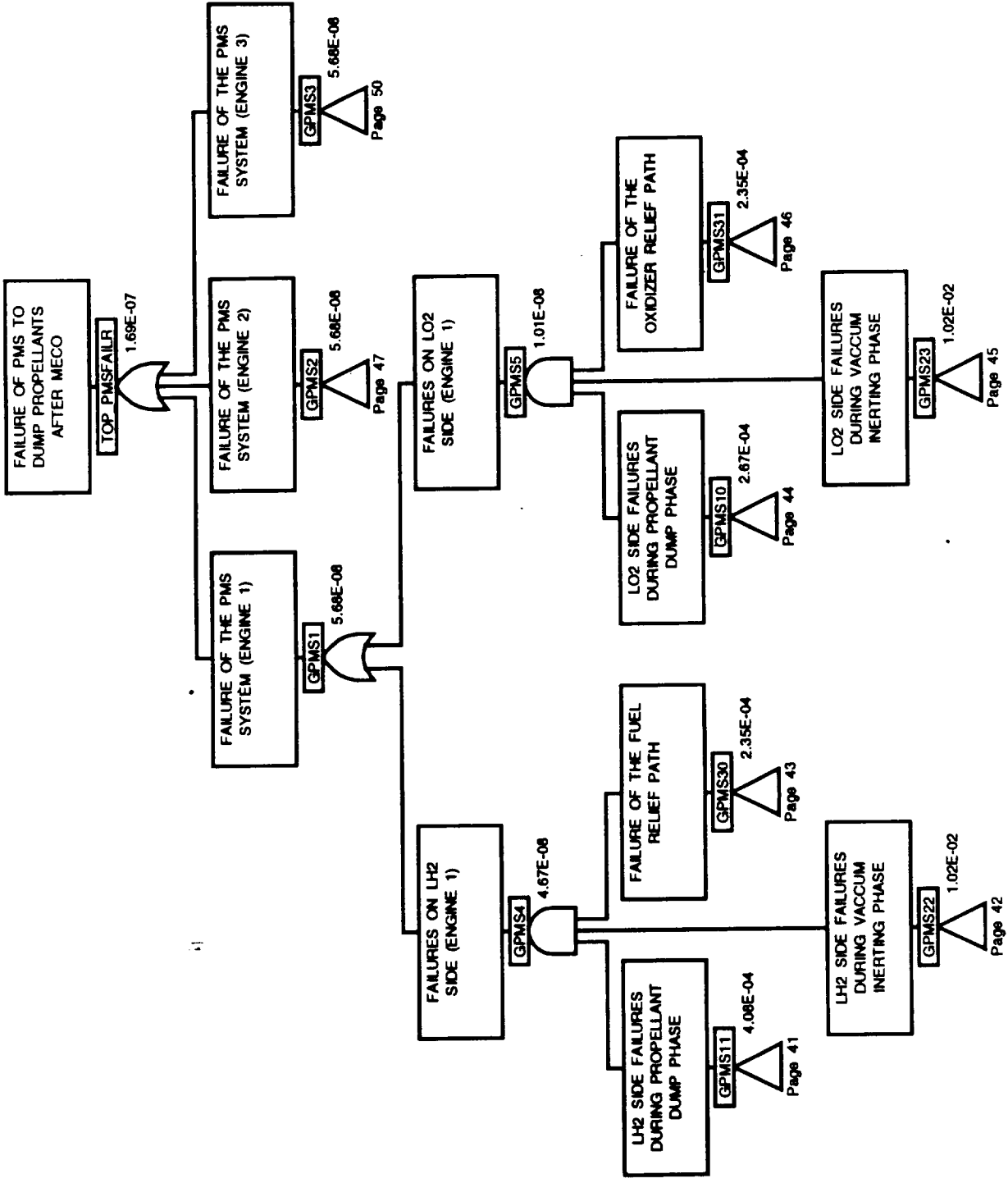
VALVE DRIFT AFTER
HYDRAULIC LOCKUP
CAUSES REDLINE

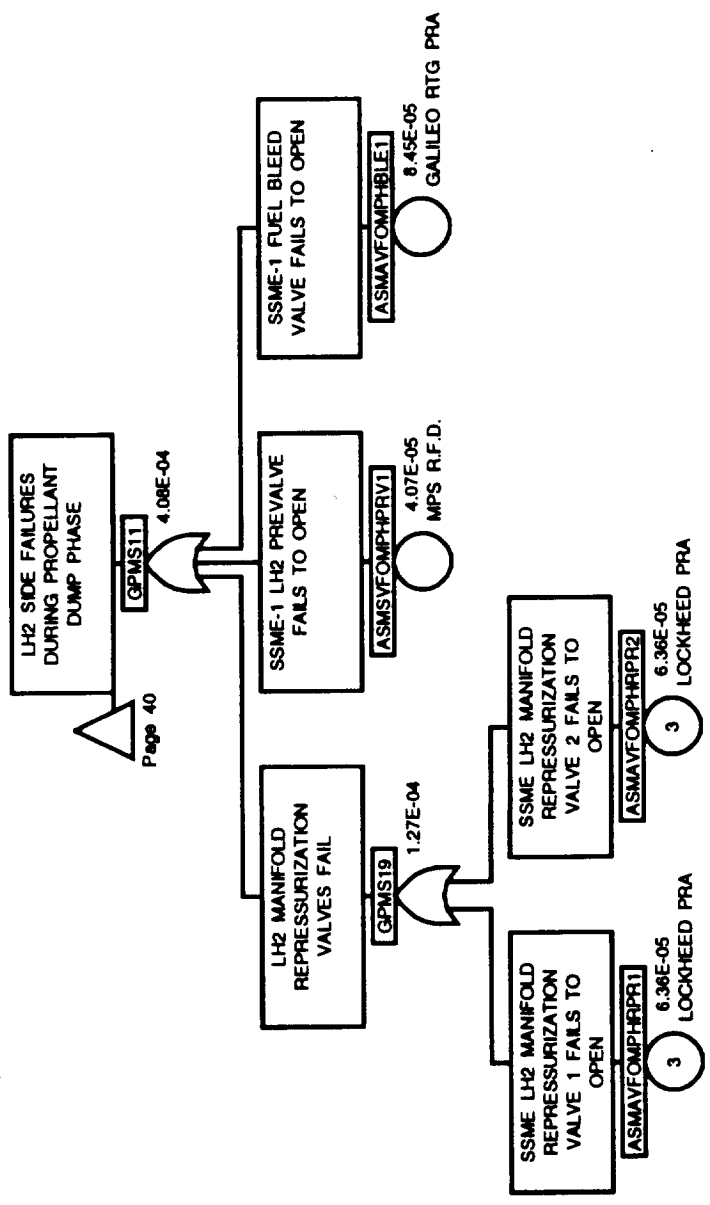
TOP VLDRIFT

2.00E-01

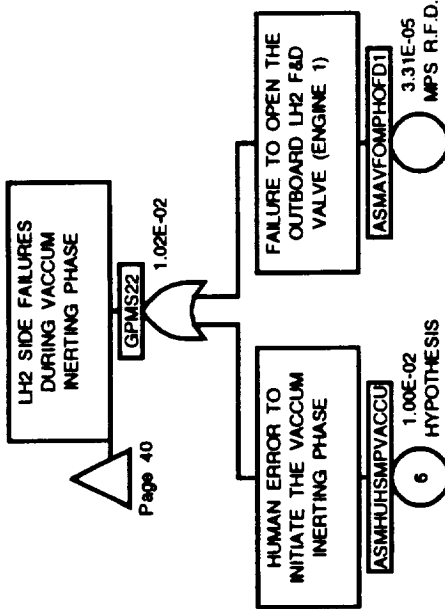
EXPERT OPINION



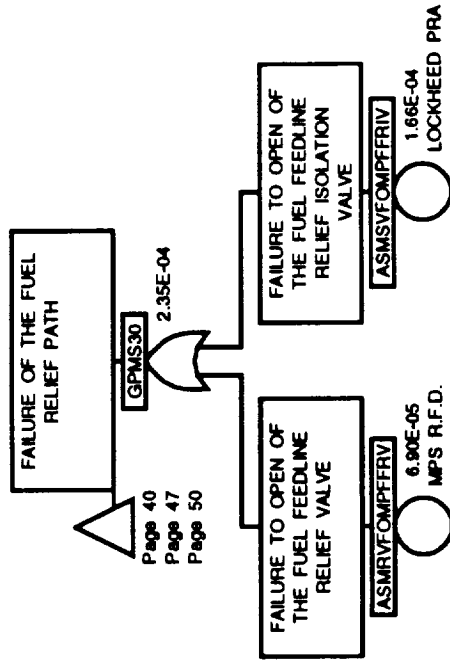


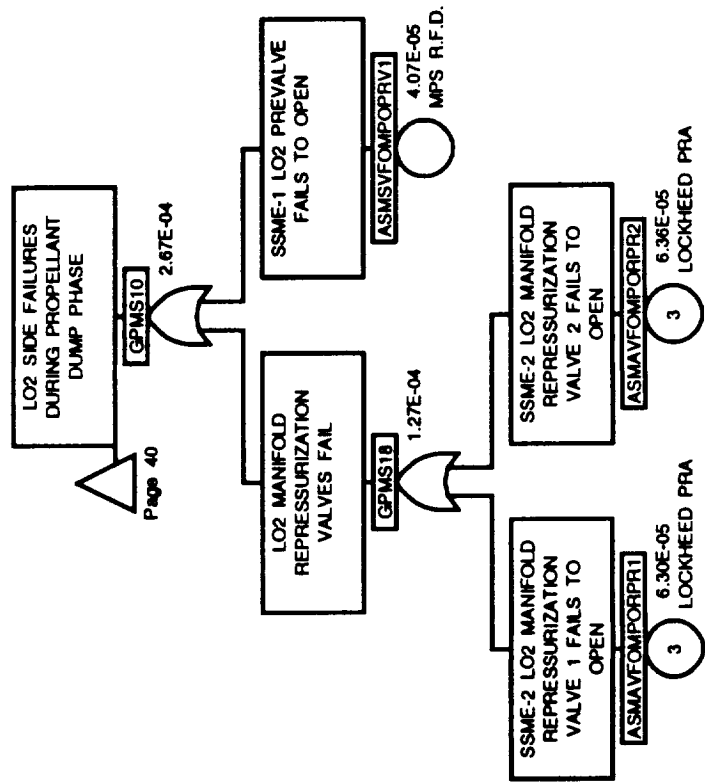


Page 40

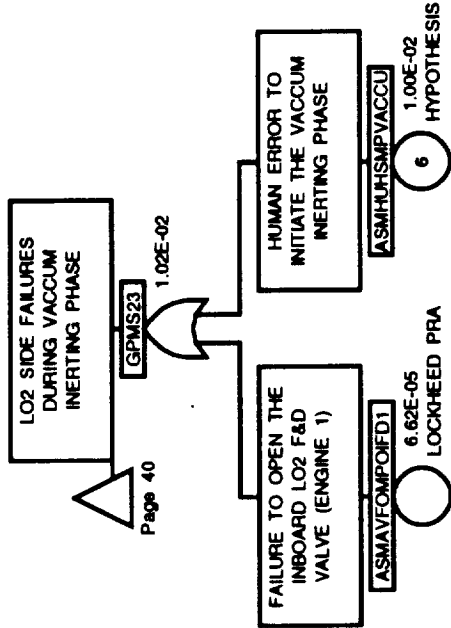


Page 40

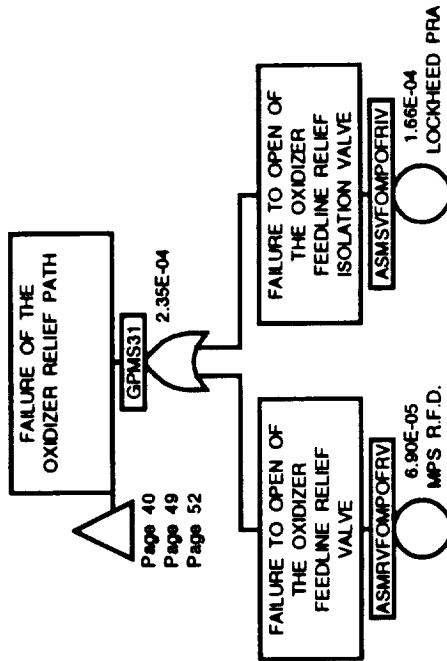




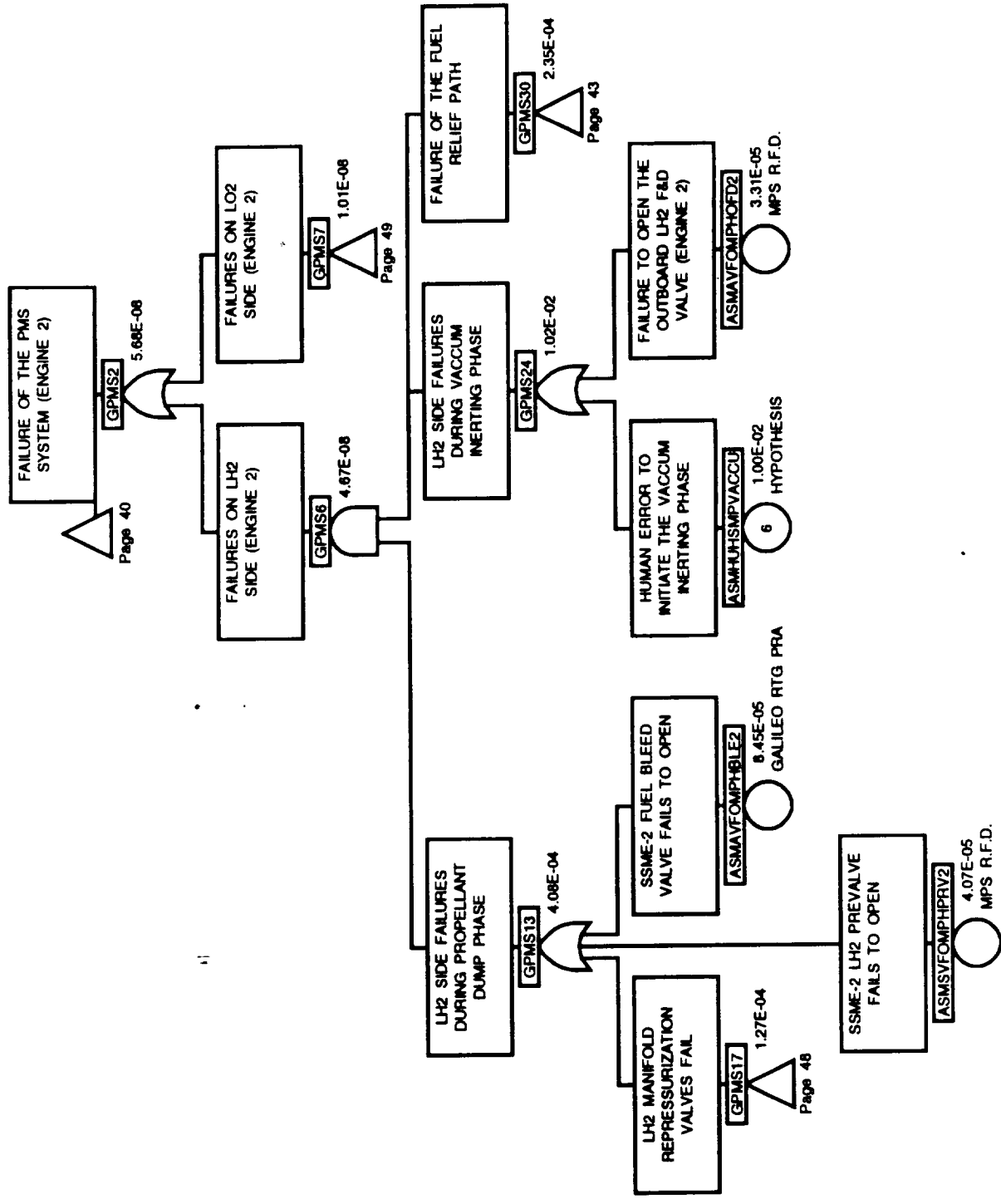
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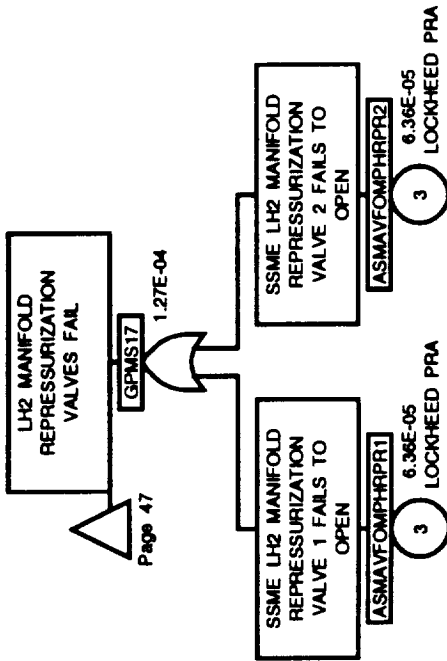


Page 40

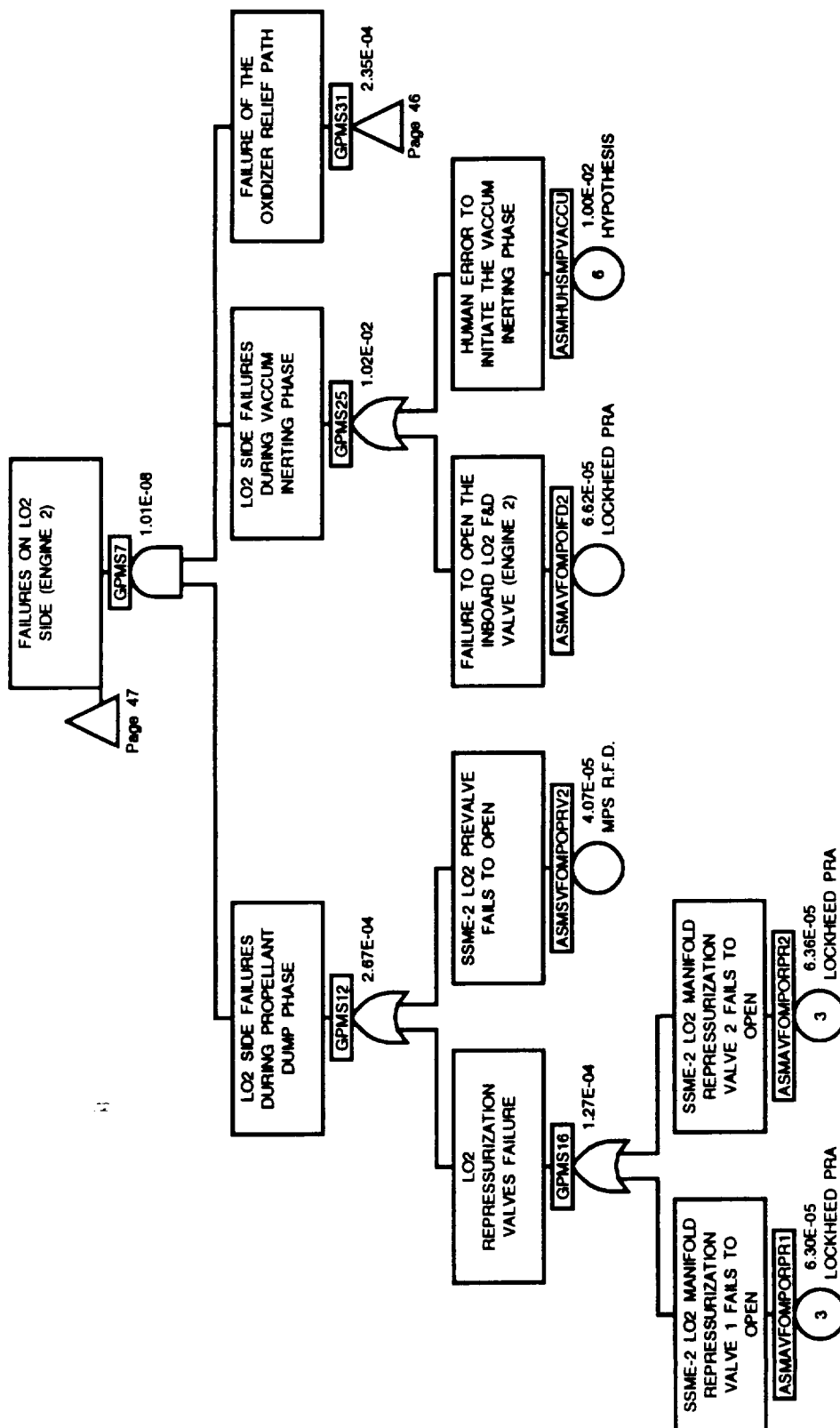


Page 40
Page 49
Page 52





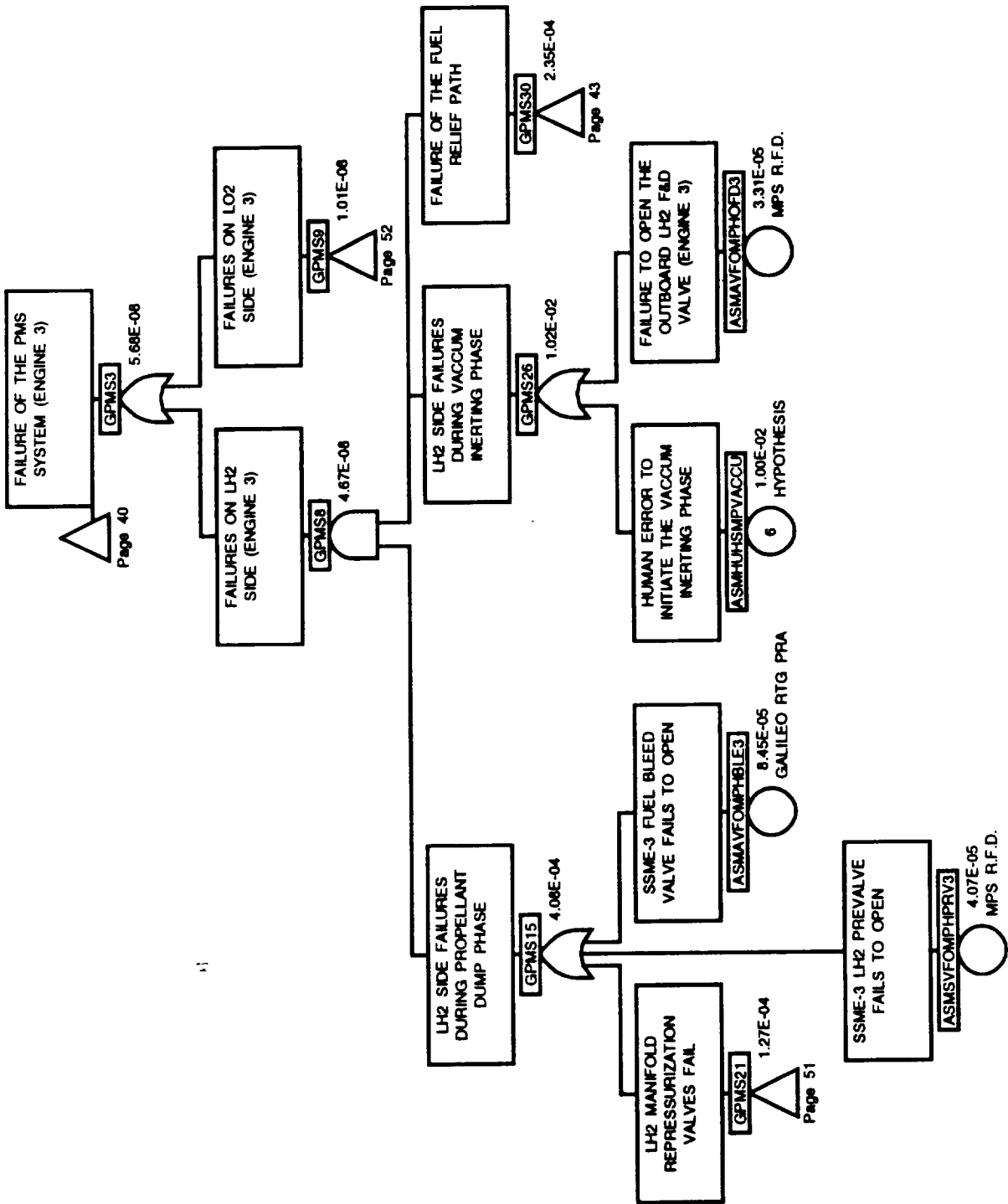
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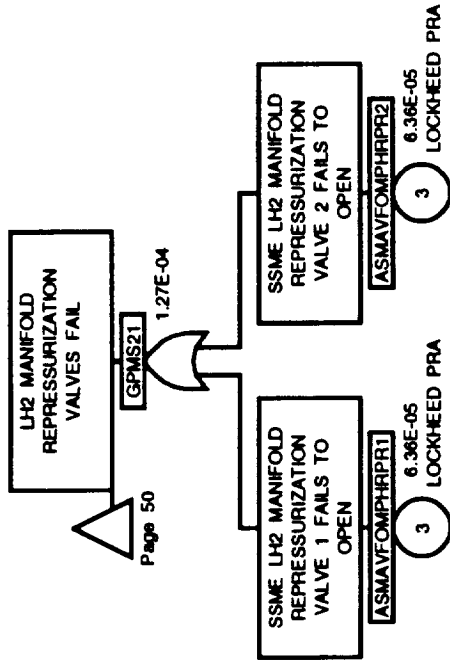


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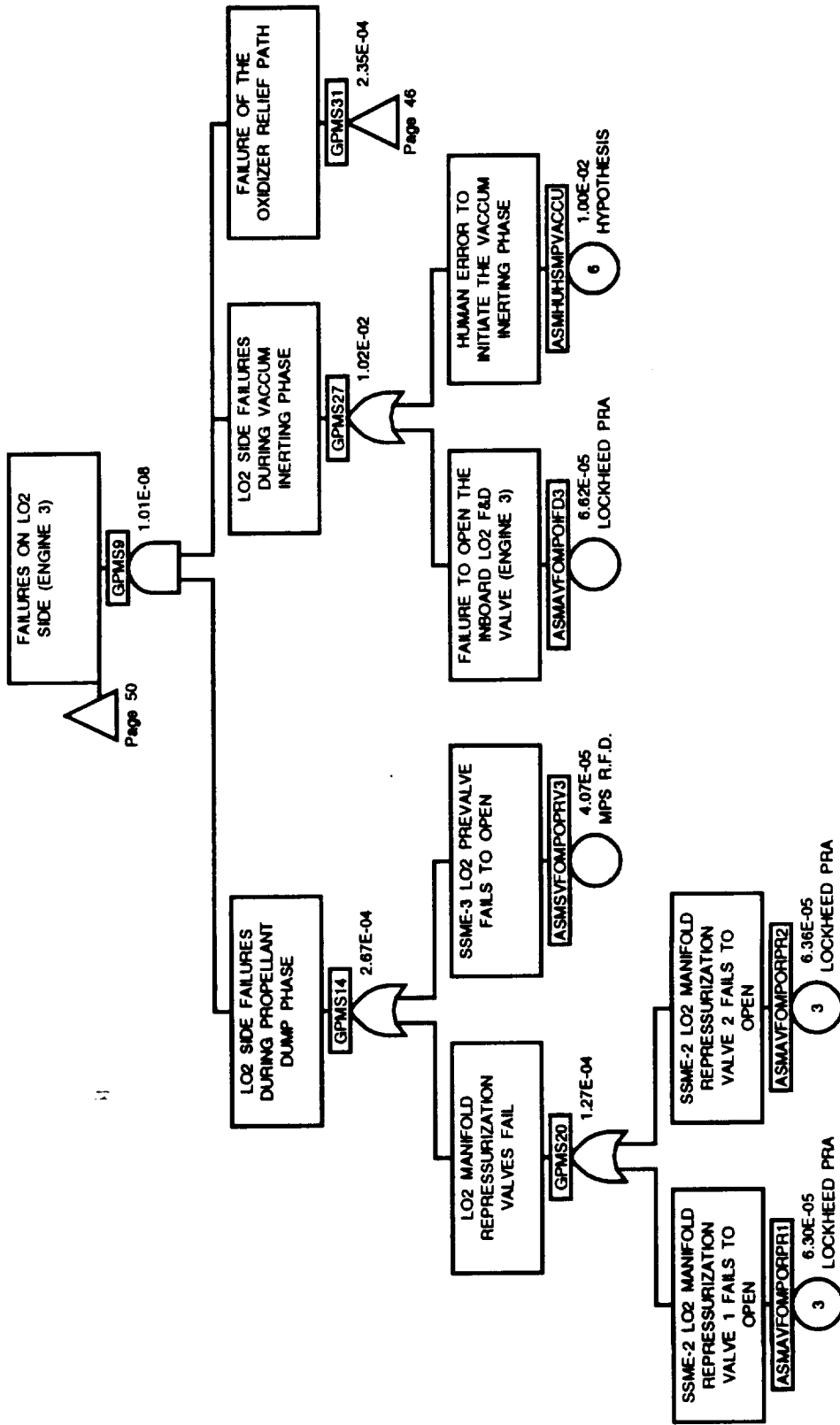
Page 47

Page 46



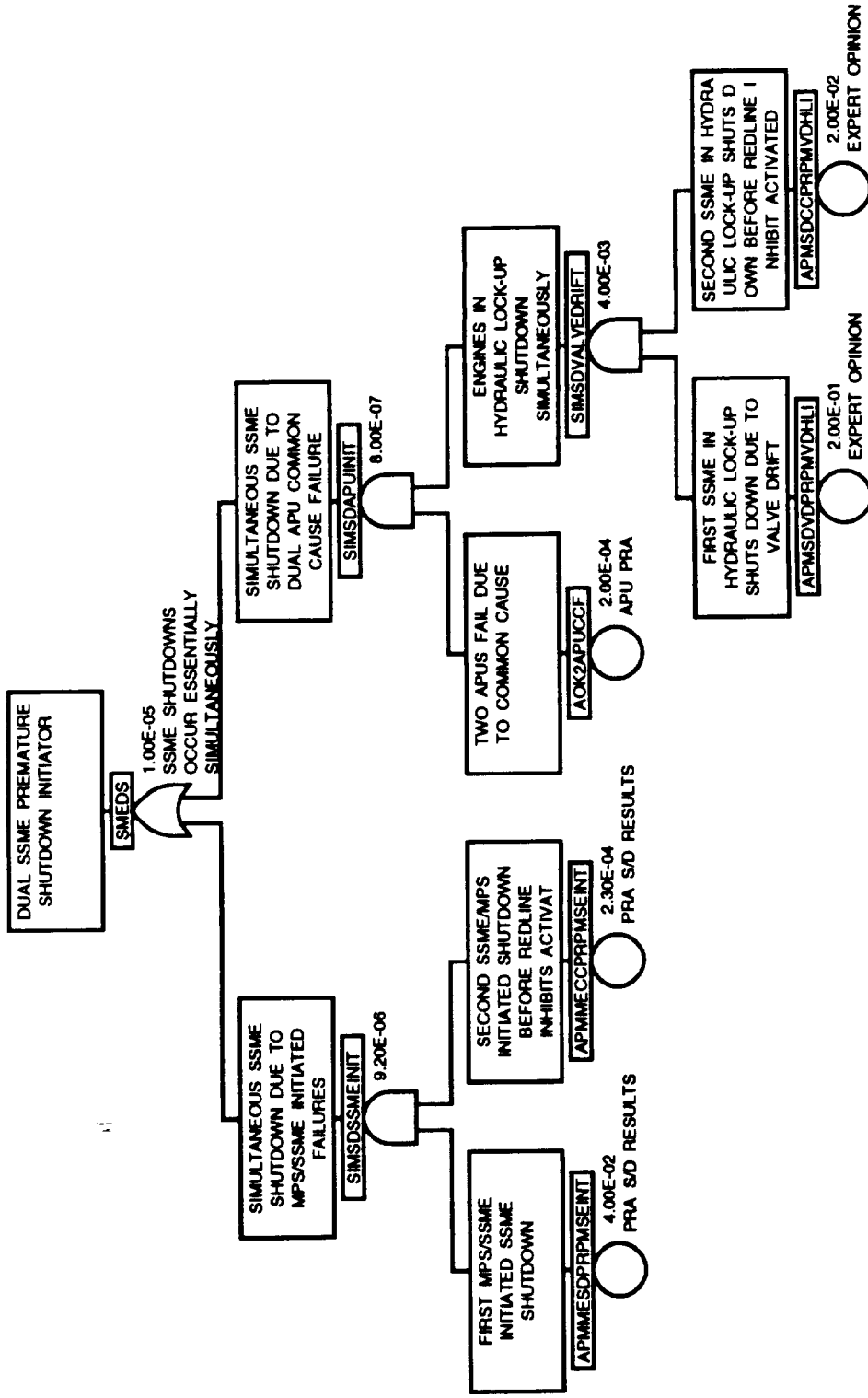


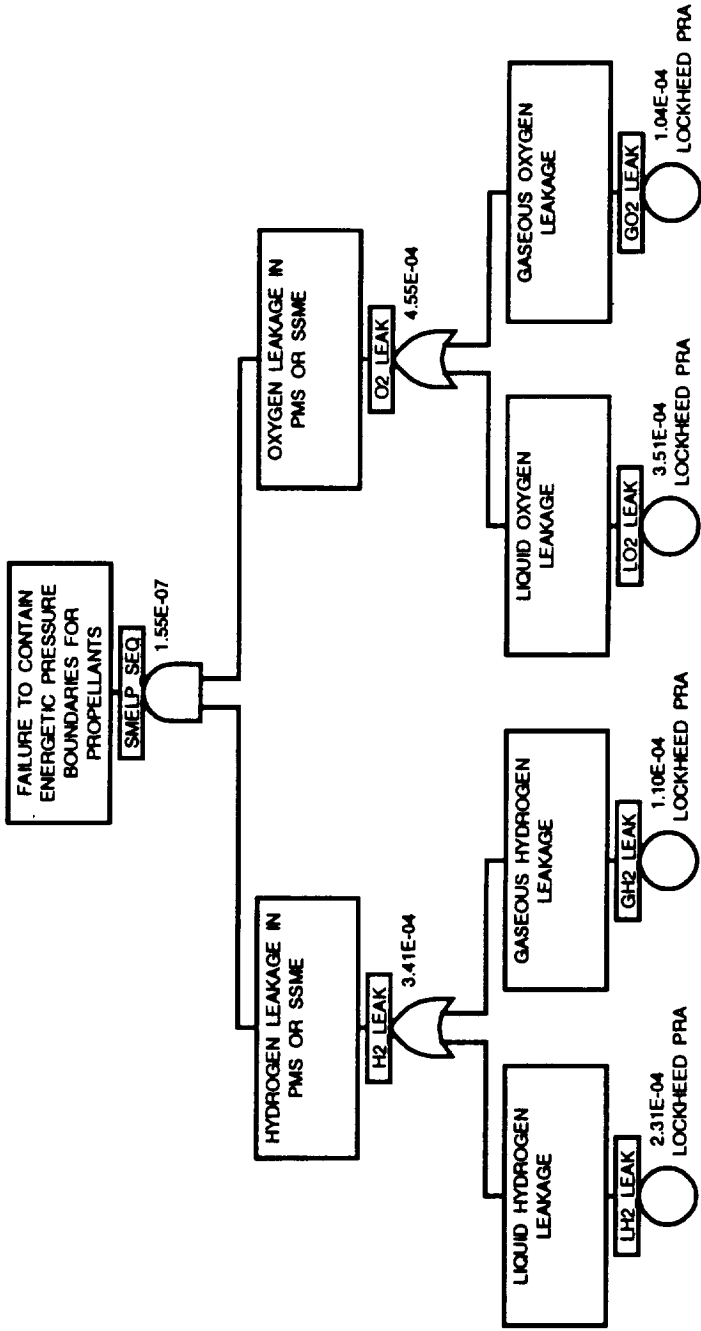
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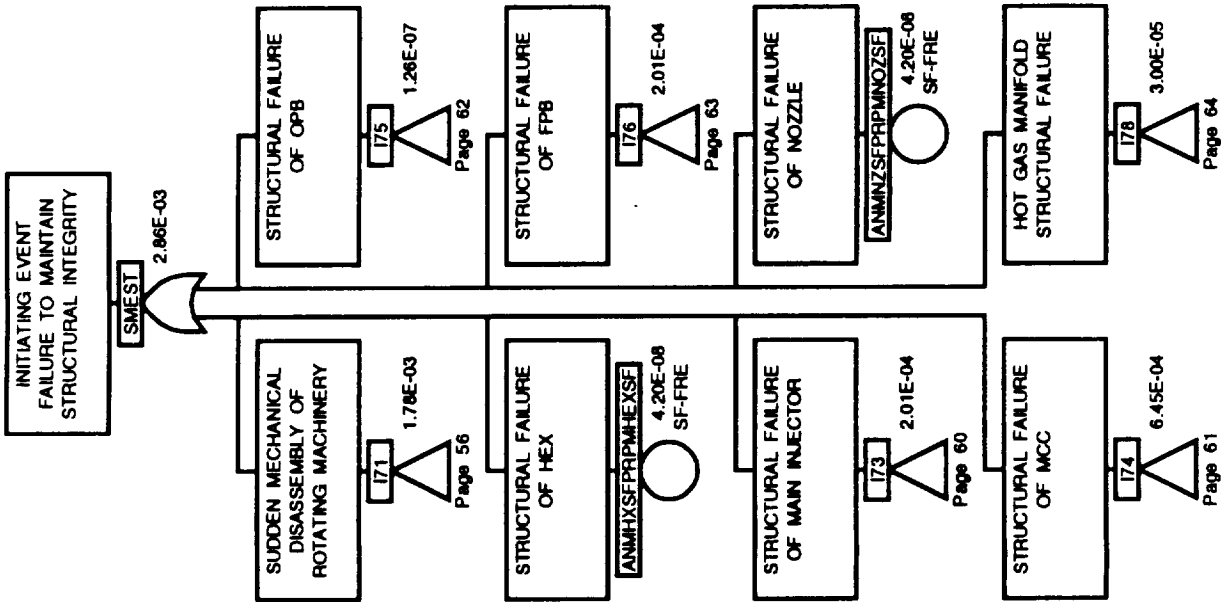


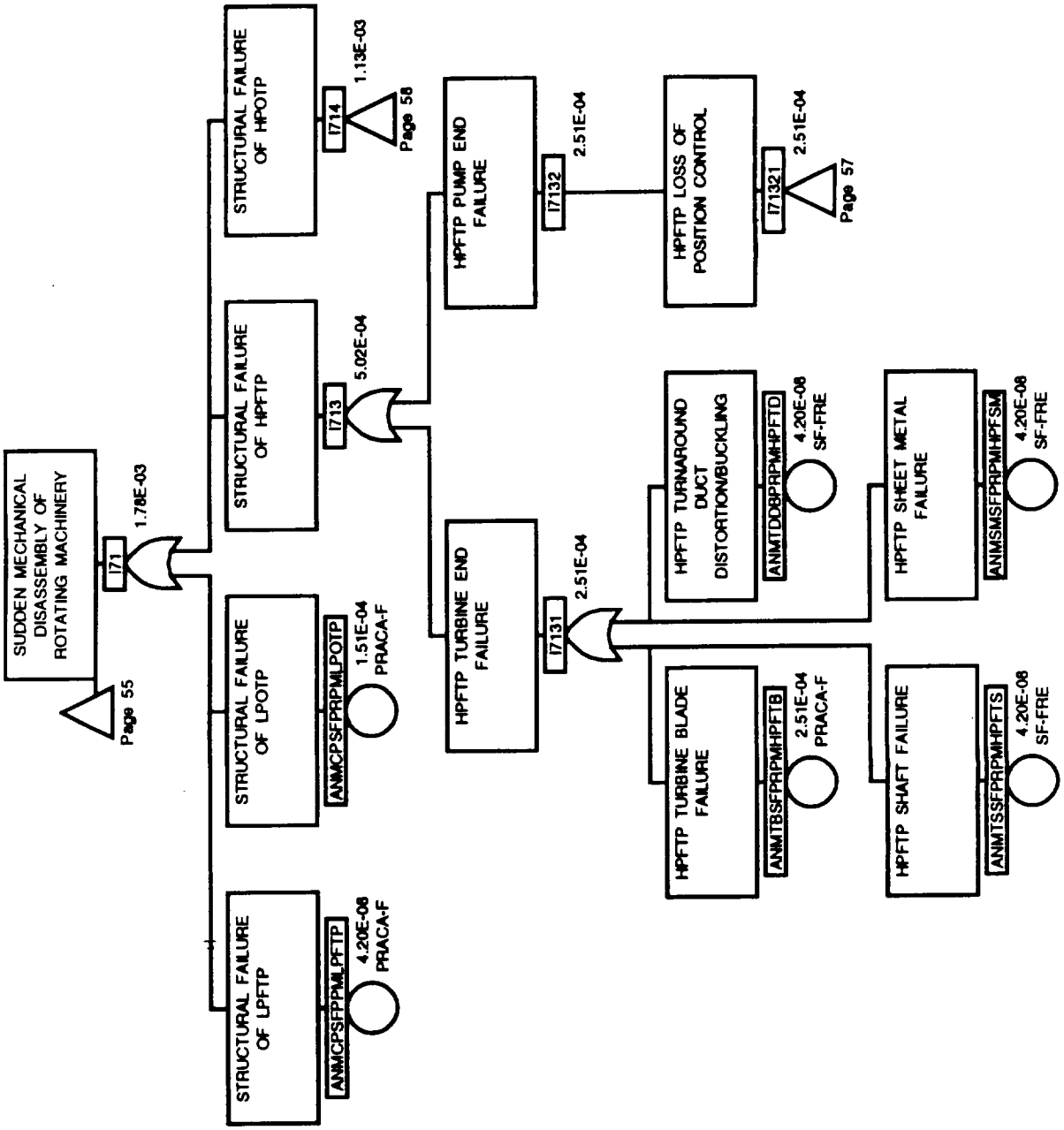
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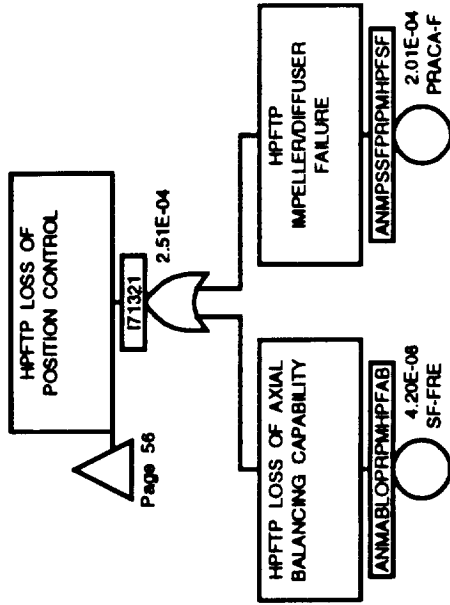
Page 46



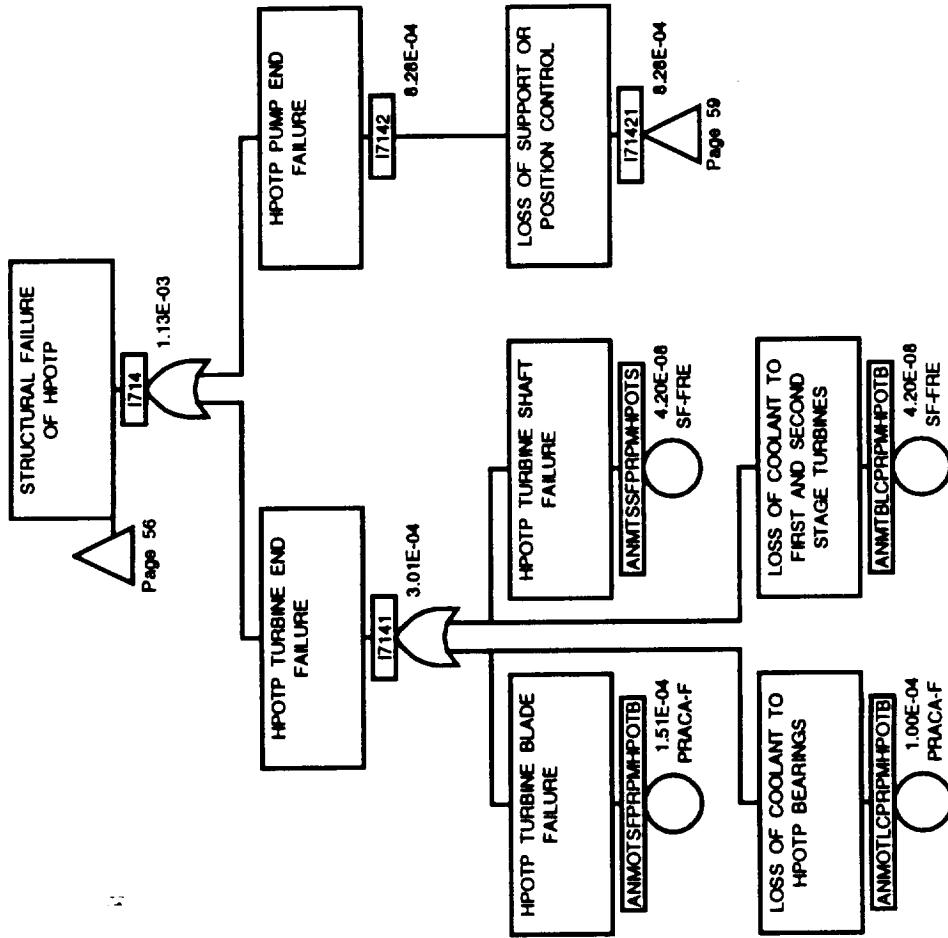






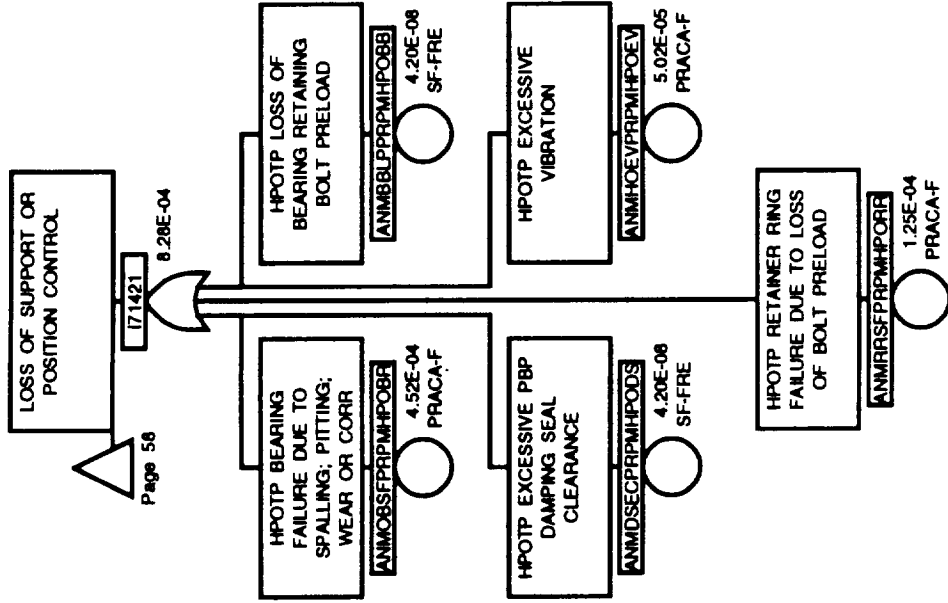


Page 56

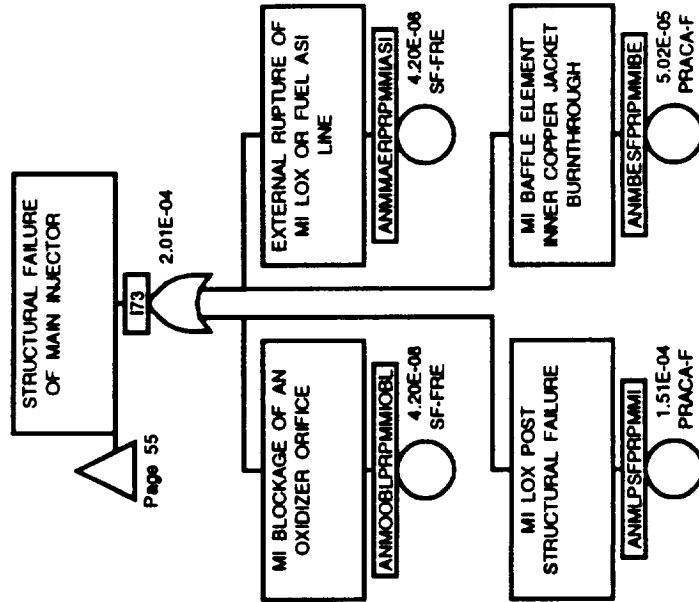


Page 56

Page 59

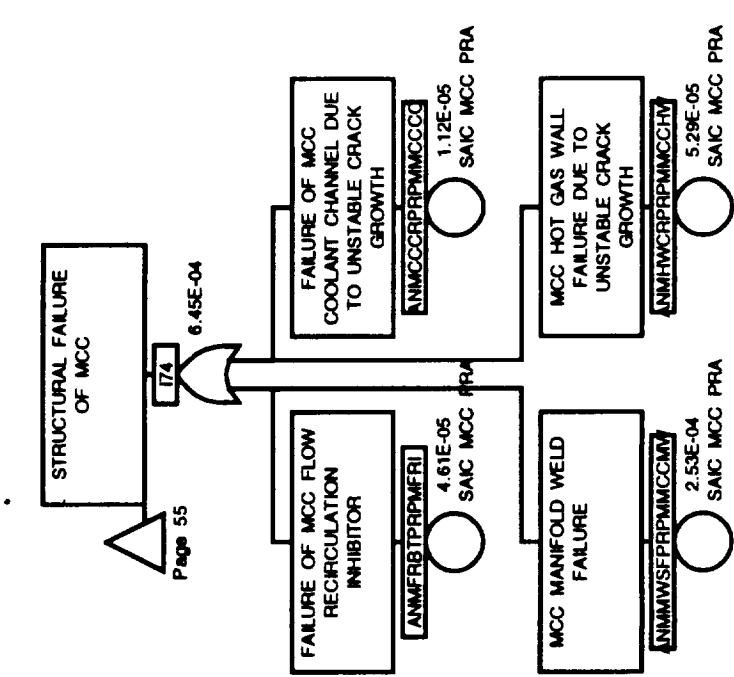


Page 56

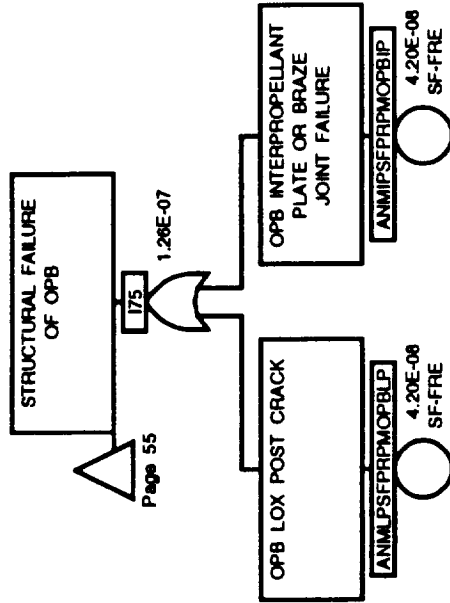


Page 55

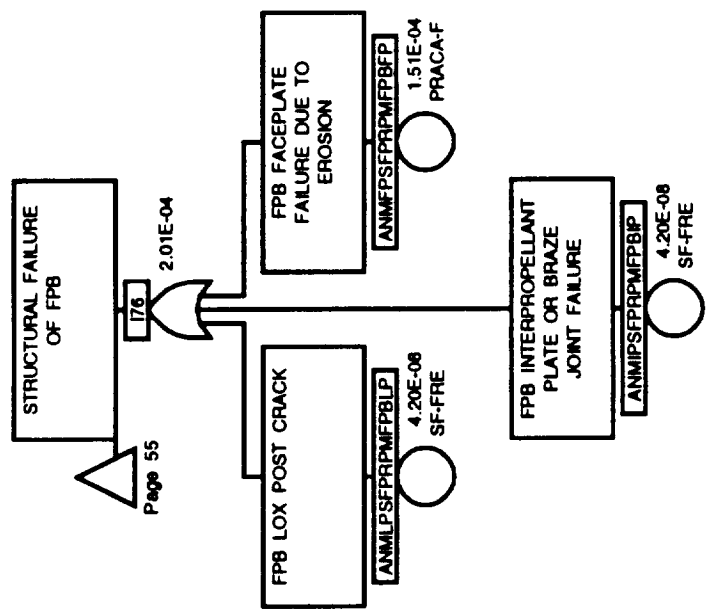
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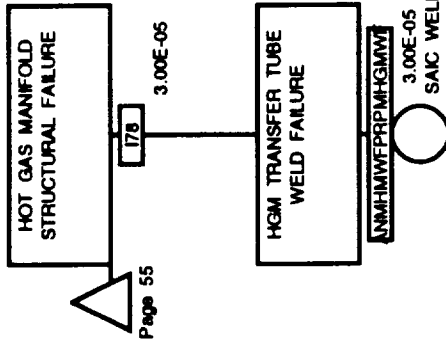
Page 55
174

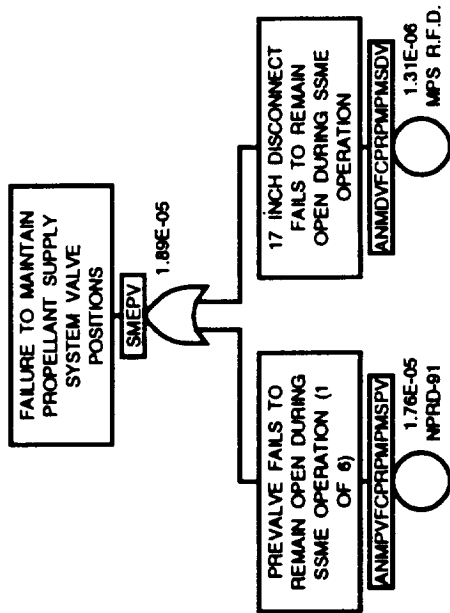


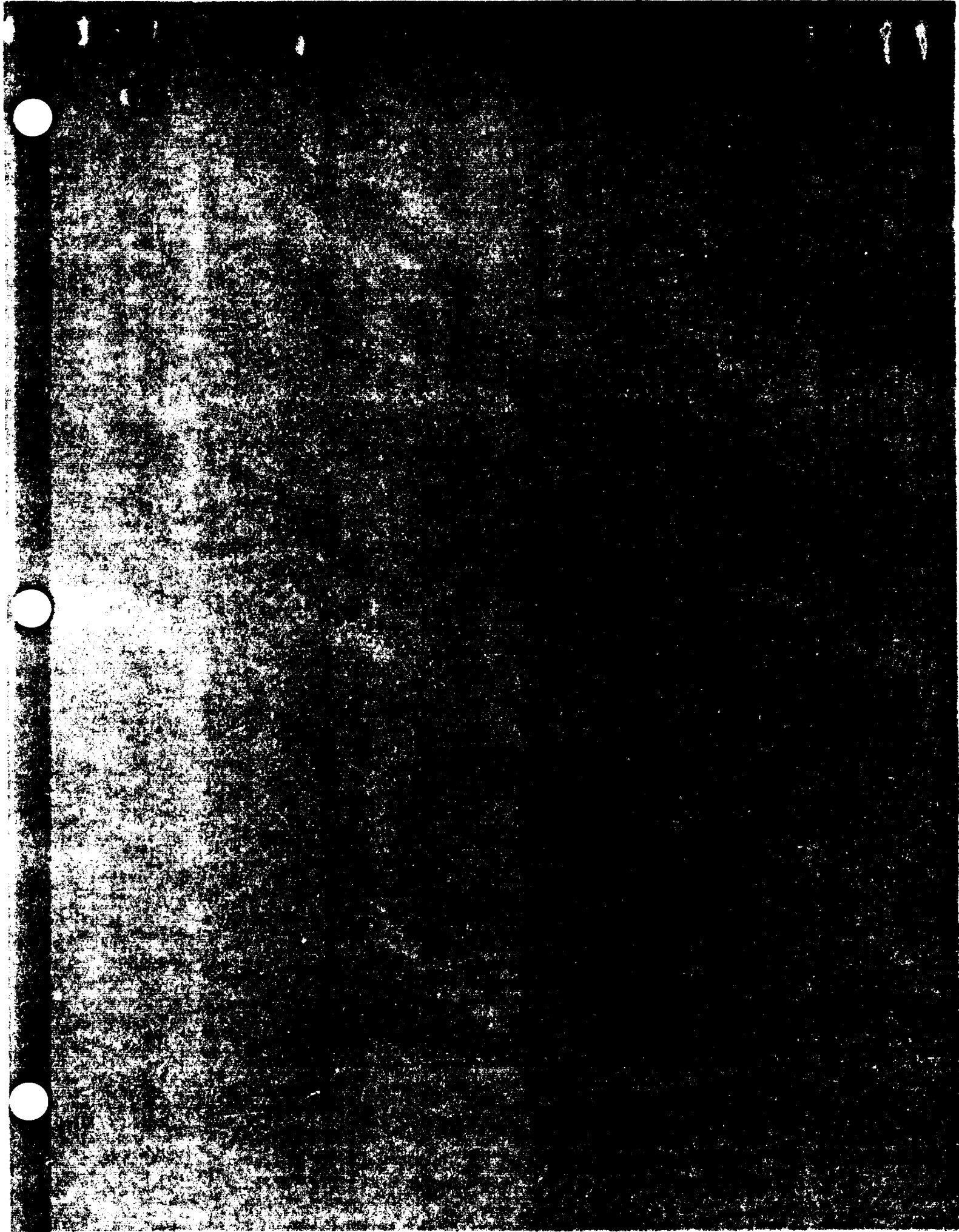
Page 55



Page 55







FUEL TURBINE TEMPERATURE REDLINE
SENSOR RELIABILITY ASSESSMENT

SENSOR FAILURE DATA - FUEL SIDE ONLY

PART NUMBER	7004-91	7013	TOTAL
TOTAL SECONDS	264,000	158,000	422,000
FAILURES	3	2	5

BOTH PART NUMBERS EXHIBIT THE SAME FAILURE RATE

MISSION RELIABILITY VALUES - SINGLE SENSOR (50%CONFIDENCE)

FAILURE (HIGH OR LOW)	0.993104
FAIL HIGH - DISQUALIFY	0.9943159
FAIL HIGH - VOTE FOR CUTOFF	0.9967419
FAIL LOW - DISQUALIFY	0.9979538

HISTORICAL SSME RELIABILITY DATA

SINGLE ENGINE - 104% MISSION	0.9924918
EXCEED FUEL TURBINE REDLINE	0.9984938

ERRONEOUS SHUTDOWN PROBABILITY

FIRST FAILURE HIGH OR LOW (1 OF 2)	0.0137444
SECOND FAILURE HIGH AND VOTE	0.0032581
COMBINED	4.478E-05
THREE ENGINE PROBABILITY	0.0001343
MTBF	7,440

LOSS OF PROTECTION PROBABILITY

FIRST FAILURE HIGH OR LOW (1 OF 2)	0.0137444
SECOND FAILURE - NO VOTE	0.0056841
COMBINED	7.812E-05
THREE ENGINE PROBABILITY	0.0002344
MTBF	4,270

REDLINE EXCEEDED PROBABILITY

SINGLE ENGINE	0.0015062
THREE ENGINE PROBABILITY	0.0045117
MTBF	220

REDLINE PROVIDES NEEDED PROTECTION

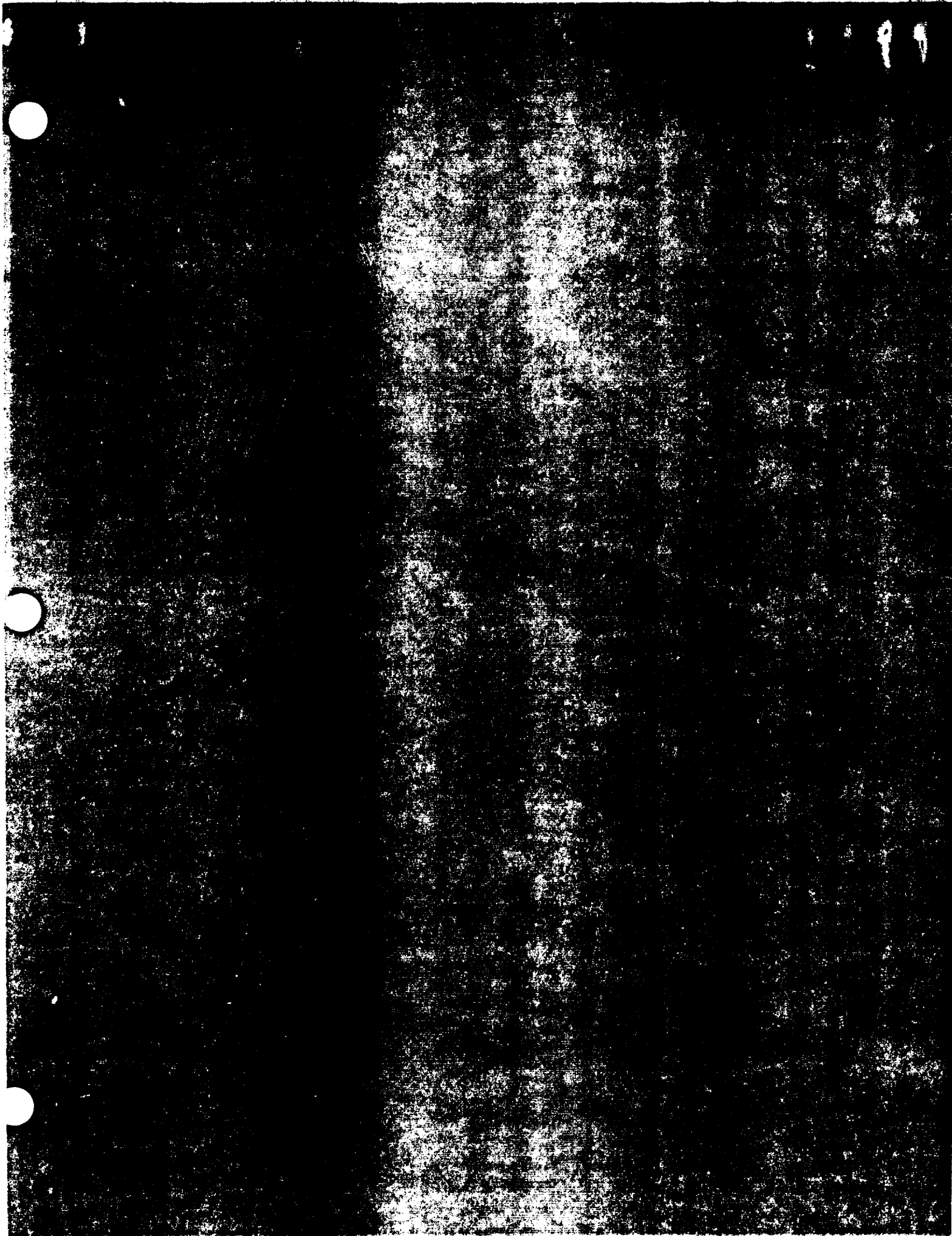
SAFE SHUT DOWN FOR 20 PERCENT OF HISTORICAL FAILURES	
EXPECTED NEED	1 IN 220 FLIGHTS
EXPECTED ERRONEOUS	1 IN 7,440 FLIGHTS
RATIO	34 TO 1

SENSOR CATASTROPHIC POTENTIAL

LOSS OF REDLINE	7.812E-05
ENGINE EXCEEDS REDLINE	0.0015062
COMBINED	1.177E-07
THREE ENGINE PROBABILITY	3.53E-07
MTBF	2,832,780

ERRONEOUS SHUTDOWN (3 ENGINES)	0.0001343
SECOND ENGINE SHUTDOWN	0.0075082
COMBINED	1.009E-06
MTBF	991,450

UNABLE TO ASSESS ORBITER ABORT RISK



CUTOFF CODES

CODE	ID	DESCRIPTION
CADS	1	COMMAND AND DATA SIMULATOR COMMAND (SIMULATES ORBITER COMPUTER)
CADS ELU	2	CADS - ELECTRONIC LOCKUP
CADS FTD	3	CADS - HPFTP TURBINE DISCHARGE TEMPERATURE REDLINE LOST
CONT	4	ENGINE CONTROLLER INITIATED
CONT FD	5	CONTROLLER - FUEL DENSITY (OBSOLETE)
CONT IEA	6	CONTROLLER - INPUT ELECTRONICS CHANNEL A
ENG RDY	7	LOSS OF ENGINE READY
F SPD IC	8	HPFTP SPEED IGNITION CONFIRM
F TD T	9	HPFTP TURBINE DISCHARGE TEMPERATURE
F TD T E	10	HPFTP TURBINE DISCHARGE TEMPERATURE - ERRONEOUS
F TI T	11	HPFTP TURBINE INLET TEMPERATURE (OBSOLETE)
FAC	12	FACILITY INITIATED CUTOFF (NOT AN ENGINE PROBLEM)
FAC E	13	FACILITY INITIATED CUTOFF - ERRONEOUS
H2O PR	14	FACILITY WATER PRESSURE
HEX DP	15	HEAT EXCHANGER DELTA PRESSURE (OBSOLETE)
HEX PR	16	HEAT EXCHANGER PRESSURE (OBSOLETE)
HEX PR E	17	HEAT EXCHANGER PRESSURE - ERRONEOUS
HF ACC	18	HPFTP ACCELEROMETERS
HF ACC A	19	HPFTP ACCELEROMETERS - AXIAL (OBSOLETE)
HF ACC E	20	HPFTP ACCELEROMETERS - ERRONEOUS
HF ACC N	21	HPFTP ACCELEROMETERS - NON STANDARD MONITOR (OBSOLETE)
HF SPD	22	HPFTP SPEED (OBSOLETE)
HGM	23	HOT GAS MANIFOLD DELTA PRESSURE
HO ACC	24	HPOTP ACCELEROMETERS
HO ACC A	25	HPOTP ACCELEROMETERS - AXIAL (OBSOLETE)
HO ACC C	26	HPOTP ACCELEROMETERS - CROSSFEED FROM HPFTP
HO ACC E	27	HPOTP ACCELEROMETERS - ERRONEOUS
HO ACC N	28	HPOTP ACCELEROMETERS - NON STANDARD MONITOR (OBSOLETE)
HO BRG T	29	HPOTP BEARING COOLANT TEMPERATURE
HO SPD	30	HPOTP SPEED (OBSOLETE)
HO SPD E	31	HPOTP - ERRONEOUS
INJ ACC	32	MAIN INJECTOR ACCELEROMETERS
LF ACC	33	LPFTP ACCELEROMETERS
LF ACC E	34	LPFTP ACCELEROMETERS - ERRONEOUS
LO ACC E	35	LPOTP ACCELEROMETERS - ERRONEOUS
LOX T E	36	HPOTP LOX DISCHARGE TEMP RISE - ERRONEOUS (OBSOLETE)
LPF TURB	37	LPFTP TURBINE INLET PRESSURE (OBSOLETE)
MCC	38	MCC LINER CAVITY PRESSURE
MCC ACC E	39	MAIN COMBUSTION CHAMBER ACCELEROMETERS - ERRONEOUS
MCC PC	40	MAIN CHAMBER PRESSURE
MCF ACT	41	MAJOR COMPONENT FAIL REPORT - ACTUATOR
MCF CL	42	MCF - COMMAND LIMIT
MCF DCU	43	MCF - DIGITAL COMPUTER UNIT
MCF FD	44	MCF - FUEL DENSITY
MCF FTD	45	MCF - HPFTP TURBINE DISCHARGE TEMPERATURE
MCF FM	46	MCF - FUEL FLOWMETER
MCF OTD	47	MCF - HPOTP TURBINE DISCHARGE TEMPERATURE
MCF PC	48	MCF - MAIN CHAMBER PRESSURE
MOV ACC	49	MAIN OXIDIZER VALVE ACCELEROMETER (OBSOLETE)
O DR DP	50	HPOTP PRIMARY OXIDIZER SEAL DRAIN DELTA PRESSURE (OBSOLETE)
O DR P	51	HPOTP PRIMARY OXIDIZER SEAL DRAIN PRESSURE (OBSOLETE)
O DR P E	52	HPOTP PRIMARY OXIDIZER SEAL DRAIN PRESSURE - ERRONEOUS
O DR T	53	HPOTP PRIMARY OXIDIZER SEAL DRAIN TEMPERATURE (OBSOLETE)
O IS PRG	54	HPOTP INTERMEDIATE SEAL PURGE PRESSURE
O ISCP	55	HPOTP INTERMEDIATE SEAL CAVITY DELTA PRESSURE (OBSOLETE)
O ISCP	56	HPOTP INTERMEDIATE SEAL CAVITY PRESSURE (OBSOLETE)
O ISCP E	57	HPOTP INTERMEDIATE SEAL CAVITY PRESSURE ERRONEOUS
O TD T	58	HPOTP TURBINE DISCHARGE TEMPERATURE
O TD T E	59	HPOTP TURBINE DISCHARGE TEMPERATURE - ERRONEOUS
O TI T	60	HPOTP TURBINE INLET TEMPERATURE (OBSOLETE)
O TI T E	61	HPOTP TURBINE INLET TEMPERATURE - ERRONEOUS (OBSOLETE)
OBS	62	MANUAL CUTOFF BY OBSERVER
OBS E	63	ERRONEOUS OBSERVER CUTOFF
OBS FIRE	64	OBSERVER CUTOFF - FIRE
PB PG IC	65	PREBURNER PURGE IGNITION CONFIRM
PB PRG	66	PREBURNER PURGE FAILED ON
PBP PR	67	PREBURNER PUMP DISCHARGE PRESSURE (OBSOLETE)
PC IC H	68	CHAMBER PRESSURE IGNITION CONFIRM - HIGH
PC IC L	69	CHAMBER PRESSURE IGNITION CONFIRM - LOW
PC MS	70	CHAMBER PRESSURE MAINSTAGE
PH/T	71	POWERHEAD AREA ENVIRONMENT TEMPERATURE
PIF	72	LOW FUEL INLET PRESSURE (FACILITY)
PIO	73	LOW OXIDIZER INLET PRESSURE (FACILITY)
SATS	74	SHUTTLE AVIONICS TEST SET (CLUSTER GROUND TEST ORBITER COMPUTER SIMULATC
TH BNG	75	HPFTP THRUST BEARING SPEED (OBSOLETE)
TH BNG E	76	HPFTP THRUST BEARING SPEED - SENSOR MALFUNCTION (OBSOLETE)
VEH	77	VEHICLE (ORBITER) COMMAND

TEST NUMBER	ENGINE NUMBER	REGULINE	COMP	MAJOR IACID	DATE	COMMENT	DURATION	POWER LEVEL	FAILURE MODE FROM ICS	UCR	COMPLETION	CPTOP ID	DISCREPANCY/NOTABLE
ASIS68-C	2032	MCF O/D	SYSTEM		18-Aug-91	CHANNEL A HPOIP TEMP EXCEEDED 1560	3.72	100				47	
901-674	2032	MCF FD	CCV		06-Nov-91	HIGH I/P/T DISCHARGE PRESSURE	4.72	95	FAILED TO INSTALL CCV COUPLING	A03126715	FPL/PH2	44	Case Open
902-245	2107	O/T D	F/M R		02-MAR-89	OFF M/R DUE TO BAD FLOWMETER CONST	447.40	109	KI PREDICTION NOT PER WATER FLOW	A02153815	FPL/PH2	58	Random Human Event
901-578	0211	O/T D	SYSTEM		28-JUL-88	THROTTLE DOWN IN THRUST LIMIT +200%	596.40	109	CROSS FEED GAIN BAD AT HIGH VIB POSITIONS	A02066465	FPL/PH2	54	
902-228	2106	C/ADS F/D	OPB		01-JUL-87	HPOIP BELOWS BURNTURBINE L/U	204.12	104	BOTH F/T D DESUAL LOW TEMP C/ADS S/D	A01842515	FPL/PH2	3	Sensor Failure
750-288	0210	O/T D	SYSTEM		25-JUN-87	1560 PREFLIGHT R/L - CHANGED TO 1660	18.21	108	HPOIP TURB TEMP EXCD R/L	A01571815	FPL/PH2	58	
902-386	2026	O/T D	SAW/R		11-Dec-86	INCORRECT FLOWMETER CONSTANT	4.80	104	PREMATURE C/O - OVID TURB TEMP R/L	A00891815	FPL/PH2	58	
STSS1F-A	2023	F/D T/E	SENSOR		29-JUL-85	BOTH F/T D SENSORS FAILED	349.75	104	HD-SENSOR DISQUALIFIED	A00676214	FPL	10	Sensor Failure
901-485	2108	O/T D	SYSTEM		24-JUL-85	HIGH STAGE HPOIP/RR72 NOZ TUBE RUPIT	28.53	109	PREM C/O: HPOIP TURB DISC. TEMP	A01487415	FPL/PH2	58	
750-245	2308	HF ACC	HP/TP		23-AUG-84	FIRST STAGE HPOIP/RR72 NOZ TUBE RUPIT	25.61	109	PREM C/O BY HPT/RADIAL ACCELS	A01709115	FPL/PH2	18	FASCOS Not Active
901-421	2010	HF ACC	HP/TP		25-SEP-83	CAVITATION/KEEP NSS BELOW 7350	148.49	104	R/L CUTOFF DUE TO EXCV VIBRATION	A01259314	FPL	18	FASCOS Not Active
901-412	2018	MCF O/D	F/M R		21-MAY-83	OFF M/R HPOIP CHAN B TEMP MCF	5.22	100	F/M CALIBRATION CONSTANT ESTIMATE LOW	A01337014	FPL	47	OR Cutoff
902-309	2011	O/T D	F/M R		14-APR-83	HIGH MIXTURE RATIO DUE TO R	4.95	100	F/M CALIBRATION CONSTANT ESTIMATE LOW	A00668414	FPL	58	
902-292	2010	O/T D	SYSTEM		09-AUG-82	OVERSHOOT DURING THROTTLE	146.02	111	HPOIP TURB DIS TEMP: F/M CONST	A00832114	FPL	47	OR Cutoff
901-376	2014	MCF CL	F/M R		10-11-82	OPV COMMAND LIMIT	5.12	98	OPV COMMAND LIMIT - F/M CONST HIGH(PHEN)	A01594214	FPL	58	No Effect SW
901-356	0107	HO ACC	HPOIP		25-JUN-82	SUB SYNC VIBRATION UN 2011R1	37.16	111	SUB SYNC VIB - #2 & #4 BALL WEAR	A01357114	FPL	24	111% PL
750-151	0110	MCF O/D	SYSTEM		04-DEC-81	HPOIP TD LOW/DELAYED OPB IGN	3.61	20	LOW HPOIP TEMP ENG BAL NOT CHANGE	A01603414	FPL	47	OR Cutoff
901-347	0107	OBS	F/M R		30-NOV-81	OPB C/O HPOIP TEMP LOW - F/M	95.40	100	OPB C/O HPOIP TURB DIS TEMP LOW: F/M CONS	A01757414	FPL	62	Manual Cutoff
901-340	0107	F/D T	HP/TP		15-OCT-81	HP/TP V/A DUCT S/M BULGED	405.50	109	FAC HPT TURB R/L TURB AROUND DUCT FAIL	A01830514	FPL	9	Facility R/L
750-148	0110	O/T D	M/R U		02-SEP-81	M/R U BURN OUT/REPLACED M/R U	16.00	105	SEVERE DAMAGE TO THE PRIM/SEC F PLATES	A01603114	FPL	58	
901-331	2108	O/T D	M/R U		15-JUL-81	M/R U BURN OUT EXT DAM	233.14	100	SEVERE DAMAGE TO THE PRIM/SEC F PLATES	A01374514	FPL	58	
750-119	0007	MCF CL	SYSTEM		28-JUN-81	OPV LIMIT RESET MCF	5.25	100	PREMATURE CUTOFF: OPV POSITION	A01856312	MPTA	42	Delayed Ignition
750-107	0007	MCF O/D	SYSTEM		13-NOV-80	LOW LOX TURB TEMP DELAYED OPB	3.64	20	IMPROPER PWR BED UP DURING START SEQ	A01856212	MPTA	47	Delayed Ignition
SP1101-B	2003	F/D T	NOZZLE		03-NOV-80	NOZZLE TUBE RUPTURES	19.50	100	TUBES 125 THRU 126 BLOWN INWARD	A01557812	MPTA	9	
902-198	2004	O/T D	M/R U		23-11-80	HOLE IN LOX POST FAIL	8.53	102	R/L C/O - HPOIP TURB DISC TEMP MAIN RU	A01756613	FMCF	58	
SP6901-B	2003	O/T D	HP/TP		15-APR-80	TURBINE IN/LOX POST FAIL	4.72	100	M R FUEL TURB DISC TEMP YOUNG LOGIC C/O	A01124912	MPTA	9	
SP4701-C	0006	O/T D	SYSTEM		01-FEB-80	OPB DELAY/OVERSHOOT	4.61	100	PREMATURE C/O: HPOIP DISC TEMP EXCEEDED RL	A01113912	MPTA	58	Delayed Ignition
SP6033-C	0006	O/RCP	HPOIP		04-NOV-79	SECONDARY TURBINE SEAL FAILURE	8.69	100	AMCERMET SEALS CHANGED TO CARBON	A01099412	MPTA	56	Obsolete Redline
750-047	0105	O/T D	SYSTEM		22-SEP-79	OVERSHOOT AT THROTTLE DOWN	10.43	95	C/O: LOX TURBINE TEMP EXCEEDED REDLINE	A01855313	FMCF	58	
901-25	0007	O/RCP	HPOIP		12-AUG-79	M/C C/NO SW CALV PR HIGH	6.48	100	FAILED MAPPING RING - C/E/RUBBING	A01407512	MPTA	56	Obsolete Redline
901-246	2007	PCLMS	SYSTEM		12-JUL-79	OPB RUPITURE (12) DOGGY DOORS	4.45	100	NOZZLE TUBE RUPTURES: HPOIP R/L	A01895313	FMCF	70	Delayed Ignition
902-162	2004	O/T D	NOZZLE		22-MAY-79	TUBE LEAKS (13)	27.67	100	NUMEROUS TUBE LEAKS	A00934613	FMCF	58	
750-041	0201	F/D T	NOZZLE	YES	14-MAY-79	NOZZLE SHEERHORN FAILED	4.32	100	HP/TP OVERTEMP REDLINE CUTOFF	A00946612	MPTA	9	
902-157	2004	O/T D	NOZZLE		10-MAY-79	COLD SW/TUBE LEAKS (3)	90.50	100	NOZZLE TUBE SPLITS - COOLANT LOSS	A00931613	FMCF	58	FASCOS Not Active
902-145	2002	HF ACC	HP/TP		08-DEC-78	HIGH SW/TUBE HPT UN 2103R2	68.61	100	#21 TEST IN A ROW - PUMP REMOVED	A01797612	MPTA	18	FASCOS Not Active
902-144	2002	HO ACC C	HP/TP		04-DEC-78	HPF CROSS FEED /CHANGED PROFILE	36.29	70	TEST CUT BY HPOIP TURBINE RADIAL ACCEL	A01797112	MPTA	26	FASCOS Not Active
901-216	0005	O/T D	SYSTEM		03-DEC-78	HPF CROSS FEED /CHANGE R/L	3.57	20	TEST CUT BY HPOIP TURBINE RADIAL ACCEL	A01796812	MPTA	26	Damaged HPOIP
902-127	2002	HO ACC A	HPOIP		17-OCT-78	LOW TURB EFF-CHANGED M/R	4.88	90	DAMAGED HPOIP TURBINE FROM ENG. 0006 (MOV)	A00926912	MPTA	58	Damaged HPOIP
901-190	0005	IF ACC	LPTP		05-SEP-78	PREM ACCLS (AXIAL)	117.55	100	SHOW DELAY TAKE - BASED REDLINE	A01914412	MPTA	25	FASCOS Not Active
902-118	0101	LOX TE	SENSOR		28-AUG-78	DELETE FUEL VENT	137.83	100	HIGH I/P/T VIB (NOISE) - MISUNDERSTOOD	A01917112	MPTA	33	FASCOS Not Active
902-116	0101	HO ACC	HPOIP		13-AUG-78	CHA CONN FELT OFF - CH B SENSOR FAIL	240.39	100	OPEN CIRCUIT BRG #1 (RISE RATE REDLINE)	A01913612	MPTA	36	Sensor Failure
902-114	0101	HO ACC C	HP/TP		10-JUL-78	BULGE IN TURBINE TURB MANIFOLD	6.84	92	EXTREME BULGING IN TURB AROUND MANIFOLD	A00328312	MPTA	9	
902-111	0101	HO ACC	HPOIP		29-JUN-78	TURBINE SEAL FAILURE HPOIP 0005	10.85	92	SUB SYNC VIB - PUMP BRG CAGE FAIL	A01865312	MPTA	24	FASCOS Not Active
901-183	0005	HF ACC	M/R U		24-JUN-78	HPB ACCCL	281.03	100	BASED PRP REDLINE	A01924312	MPTA	24	FASCOS Not Active
901-178	0005	F/D T	HP/TP		05-JUL-78	M/R U BURN THROUGH/REPLACE P/H	51.00	100	HP/TP RADIAL CUTOFF UN 0103R8	A01920112	MPTA	24	FASCOS Not Active
901-176	0005	CONF EA	SENSOR		02-JUL-78	TURB S/L RUBBED SHAFT - CHANGE PROFILE	7.82	100	PR PUMP RADIAL ACCEL REDLINE CUTOFF	A00329912	MPTA	24	FASCOS Not Active
901-173	0005	F/D T	HP/TP		13-MAY-78	PRESS LOX YANK TO 105 PSI	4.27	100	START DAMAGE BY PROV D/S SEAL(BELVILLE)	A01878512	MPTA	9	Facility Redlined
901-167	0002	HO ACC	HP/TP		08-MAY-78	CHB LOX FLOW/DCAUA P/ELECT	32.03	100	TEMP SENSOR SHORT SATURATED MIXR SHUTDOWN	A01900912	MPTA	9	Sensor Failure
901-164	0002	HO ACC	HP/TP		31-MAR-78	M/R U BURN THROUGH/REPLACED ENG	201.73	92	MAIN INJECTOR HPT R/L	A01871011	PRE MPTA	9	PRE MPTA
901-163	0002	HO ACC	HP/TP		21-MAR-78	NOZZLE TUBE SPLITS/REPAIRED	10.71	100	HP/TP DISCHARGE TEMP REDLINE CUTOFF	A01874211	PRE MPTA	9	PRE MPTA
901-162	0002	HO ACC	HP/TP		17-MAR-78	NOZZLE TUBE SPLITS /CAVITATION	210.97	93	HP/TP RADIAL ACCEL REDLINE CUTOFF	A01863811	PRE MPTA	18	PRE MPTA
901-161	0002	HO ACC	HP/TP		21-FEB-78	OLD START SEQ EARLY OPB PRIME	6.08	91	HPOIP TURBINE DAMAGED BY START TEMP SPIKE	A00917711	PRE MPTA	58	PRE MPTA
901-160	0002	HO ACC	HP/TP		21-FEB-78	OLD START SEQ EARLY OPB PRIME	3.57	50	HPOIP SYNCHRONOUS WITH HOUSING RESONANCE	A00817611	PRE MPTA	24	PRE MPTA
902-101	2002	CONF	CONT		15-FEB-78	DELAYED R/L	11.32	100	HP/TP RADIAL ACCEL REDLINE CUTOFF	A00819111	PRE MPTA	18	PRE MPTA
902-101	2002	HO ACC	HP/TP		14-FEB-78	LIMIT P/L & OPEN FUEL REPR-CAV	4.25	100	HP/TP RADIAL ACCEL REDLINE CUTOFF	A00861711	PRE MPTA	18	PRE MPTA
902-101	2002	HO ACC C	HP/TP		09-FEB-78	TURBINE RADIAL G S CHANGE R/L	4.04	90	HPOIP SYNCHRONOUS WITH HOUSING RESONANCE	A00861711	PRE MPTA	24	PRE MPTA
902-1	2002	HO ACC C	HP/TP		02-FEB-78	PNEUMATIC S/D DCAUA HALT	26.64	90	PWR OSC - SINGLE POINT FAILURE	A00516712	MPTA	4	Controller Filtered
902-1	2002	HO ACC C	HP/TP		02-FEB-78	CROSS FEED FROM HP/TP	2.89	20	HP/TP INTERSTAGE SEAL RUB	A00327112	MPTA	26	FASCOS Not Active

Table with columns: TRF, 50000, 51000, 52000, 53000, 54000, 55000, 56000, 57000, 58000, 59000, 60000, 61000, 62000, 63000, 64000, 65000, 66000, 67000, 68000, 69000, 70000, 71000, 72000, 73000, 74000, 75000, 76000, 77000, 78000, 79000, 80000, 81000, 82000, 83000, 84000, 85000, 86000, 87000, 88000, 89000, 90000, 91000, 92000, 93000, 94000, 95000, 96000, 97000, 98000, 99000, 100000. Columns include TRF, 50000, 51000, 52000, 53000, 54000, 55000, 56000, 57000, 58000, 59000, 60000, 61000, 62000, 63000, 64000, 65000, 66000, 67000, 68000, 69000, 70000, 71000, 72000, 73000, 74000, 75000, 76000, 77000, 78000, 79000, 80000, 81000, 82000, 83000, 84000, 85000, 86000, 87000, 88000, 89000, 90000, 91000, 92000, 93000, 94000, 95000, 96000, 97000, 98000, 99000, 100000.

SOME FRICTION CUT-OFFS (Duration > 2.4 seconds)

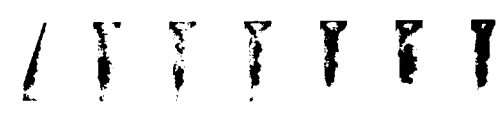
TEST NUMBER	ENGINE	ENGINE	MAJOR	DATE	COMMENT	DURATION	POWER	FAILURE	UCR	COUNT	DESCRIPTION
		TYPE	TEST ID			MIN	LEVEL	MODE	NO.	PERCENT	REASON
901.051	0001	F 111		22-Apr-76	HPF TURB INT R/L	10.32	75	HPFT TURBINE INLET TEMP REDLINE	A003359	11	PRE MPFA
901.046	0001	HF ACC A		02-Apr-76	EXCESSIVE AXIAL VIBRATION	6.27	61		A001428	19	PRE MPFA
901.044	0001	TH BNG		12-Mar-76	HPFTP BNG SPD	45.18	55	THRUST BEARINGS WELDED TO HPFT SHAFT	A001422	75	PRE MPFA
901.041	0001	O 111		05-Mar-76	OPB O/T	3.84	50		A001413	60	PRE MPFA
901.040	0001	HGM		02-Mar-76	HGM LINER DELTA-P R/L	3.39	50		A001410	23	PRE MPFA
901.039	0001	O 111		27-Feb-76	OPB OVERTEMP	2.88	20		A001408	60	PRE MPFA
901.035	0001	HGM		24-Jan-76	HGM GHTG P	3.16	20	HGM LINER DELTA-P R/L - LATE LOX POWER	A007597	23	PRE MPFA
901.033	0001	TH BNG		19-Jan-76	HPFTP BNG SPEED	2.86	20		NO UCR	75	PRE MPFA
901.032	0001	TH BNG		16-Jan-76	HPFTP BNG SPEED	2.76	20		NO UCR	75	PRE MPFA
901.031	0001	TH BNG		15-Jan-76	HPFTP BNG SPEED	2.73	20		NO UCR	75	PRE MPFA
901.023	0001	HF ACC A		12-Nov-75	HPFTP AX & RAD ACCLS	2.99	20	HPFT AXIAL ACCEL REDLINE EXCEEDED	A007555	19	PRE MPFA
901.022	0001	HF ACC A		07-Nov-75	EXCESSIVE AXIAL VIBRATION	2.76	20	HPFT AXIAL ACCEL REDLINE EXCEEDED	A007552	19	PRE MPFA

Catastrophic Failures in Entire SSME History

TEST NUMBER	ENGINE	COMP	DATE	COMMENT	DURATION	POWER LEVEL	FAILURE MODE FROM DCR	DCR	CONFIGURATION
904.044	0212	HPOTP	23-Jun-89	HPOTP #2 BEARING FAILURE	1270.72	96	BEARING WEAR WITH OPERATING TIME	A023129	5 FPL/PH2
902.471	2206	DUCT-LPF	02-Jun-89	LPF DUCT BELLOW TIE BROKE	147.68	104	FLEX JOINT TRIPOD FATIGUE - SMALL RADIUS	A008935	5 FPL/PH2
750.285	0210	NOZLE	21-May-87	FEED LINE CRACK AT STOP WELD	224.00	109	LEAK IN NO. 3 DOWNCOMMER	A015716	5 FPL/PH2
750.259	2308	MCC	27-Mar-85	DISCH MAN RUPTURE - EXT DAM	101.56	109	PREM C/O. HPFTP ACCELS	A015713	5 FPL/PH2
901.468	0207	FPB	04-Feb-85	CRACK AT F-13 FLANGE-eng retired	203.86	109	CRACK STARTED IN BOSS TO MAN. WELD	A014585	5 FPL/PH2
901.436	0108	HPFTP	14-Feb-84	CUNT LNR PR-MAJOR DAMAGE	611.06	109	EXTENSIVE TURB DAMAGE (RLCO)	A013338	5 FPL/PH2
750.175	2208	DUCT	27-Aug-82	HPO DUCT RUPTURE - ULTRASONIC F/M	116.08	111	PREM C/O P/B BOOST PUMP ACCELS	A011506	4 FPL
750.160	0110	FPB-ICE	12-Feb-82	H2O FROM EDM/EXT DAMAGE (CG1B)	3.16	20	TURB DIS TEMP. WATER IN ENG. EDM OPER	A016045	4 FPL
902.249	0204	HPFTP	21-Sep-81	TURB BL FAIL/VOLUTE RUPTURE/EXT DAM	450.57	109	PREM C/O HPFT TURB BLADE FAILURE	A018288	4 FPL
SF1001-C	0006	FPB	12-Jul-80	HOLE BURNED IN FPB	106.52	102	OBSERVER PREMATURE CUT DUE TO FIRE	A015391	2 MPTA
SF0601-A	2002	MFV	02-Jul-79	MFV BODY FAILURE	18.49	100	VALVE CAP TO BODY BOLTS BROKEN	A009437	2 MPTA
901.225	2001	MOV	27-Dec-78	MOV FRETTING-FIRE-EXT DAM	255.63	100	MOV FIRE - HPFT R/L	A010816	2 MPTA
901.136	0004	HPOTP	08-Sep-77	HPOTP BNG FAILURE - EXT DAM	300.22	90	CUTOFF DUE TO HPOT FIRE OPOVA FID 34-0	A005350	1 PRE MPTA
901.133	0004	FPB	27-Aug-77	HOLE IN FPB BODY	48.21	90	HOLE BURNT THRU FPB BODY OF POWERHEAD	A005072	1 PRE MPTA
901.110	0003	HPOTP	24-Mar-77	HPOTP FIRE EXT DAM	74.07	75	SEVERE INTERNAL FIRE DAMAGE	A005353	1 PRE MPTA



B.2. Integrated Solid
Rocket Booster

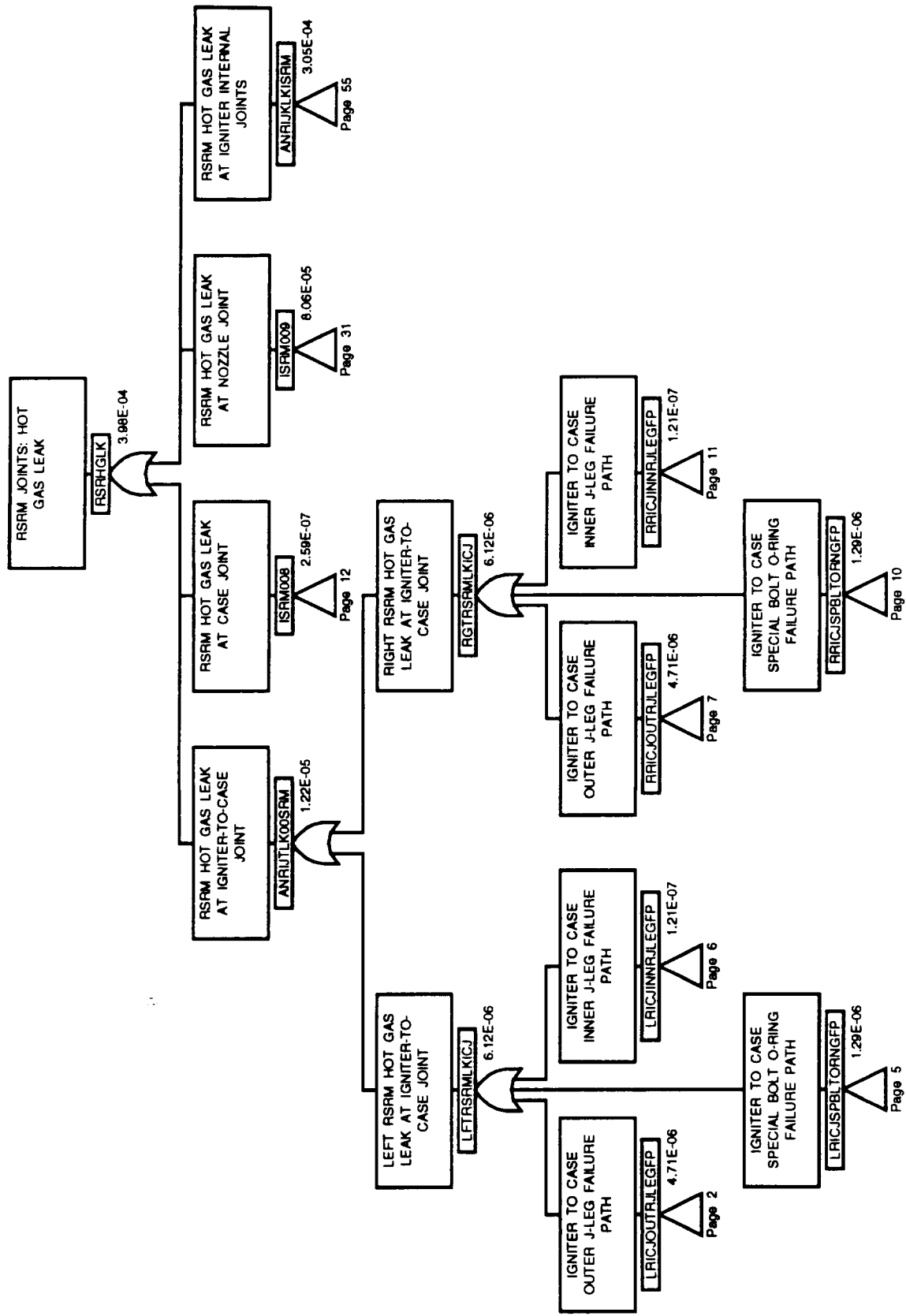


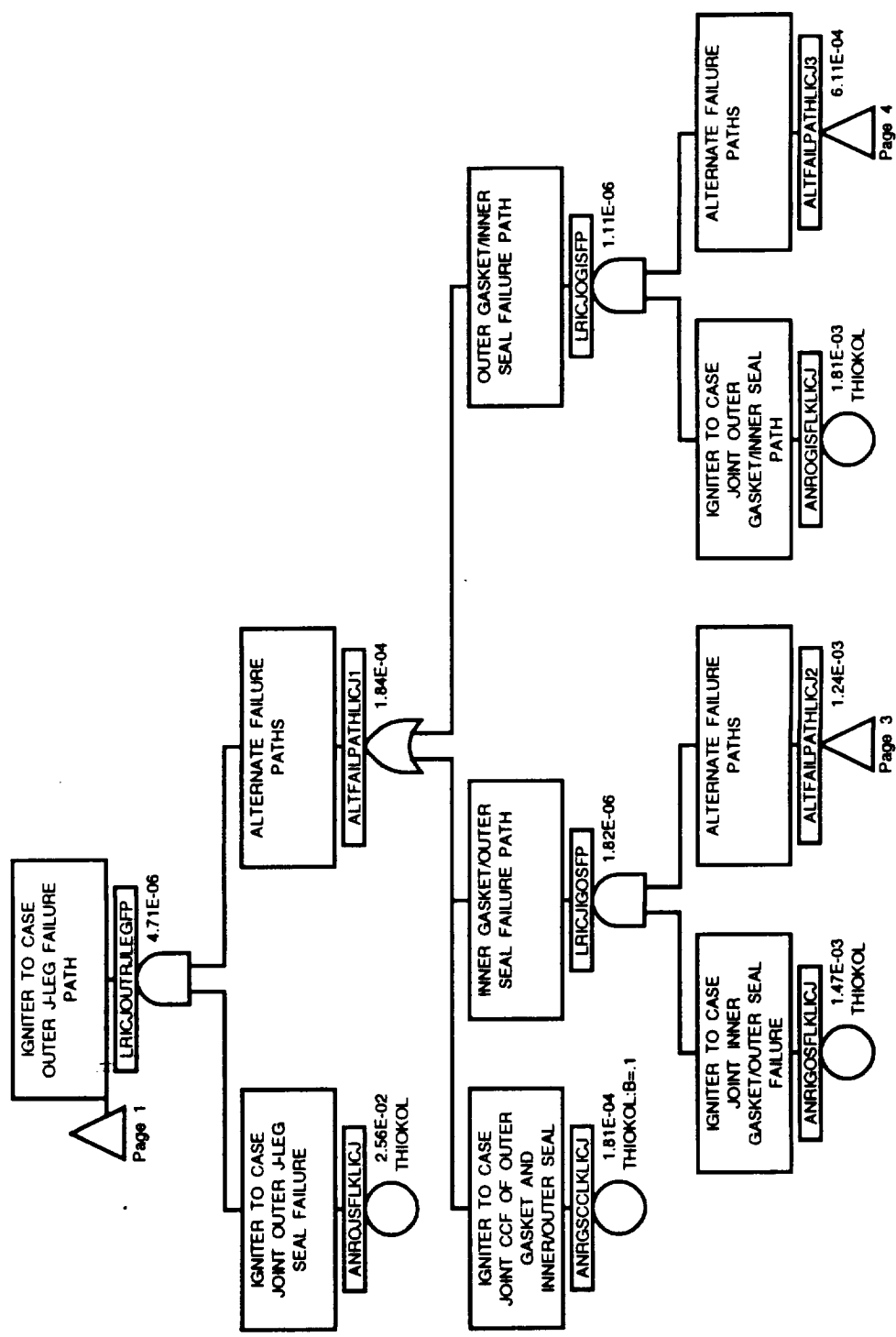
ISRB Initiator Frequency Summary						
Initiator ID	Initiator Description	One Motor Initiator Freq (per mission)	Pair Initiator Freq (per mission)	Mean # of Missions Between Occurrences	Percent of Non-nominal Initiators	Development
RSRHGLK	RSRM JOINTS: HOT GAS LEAK	1.99E-04	3.98E-04	2513	31.59%	Fault Trees-Page 1
RSRZRUP	RSRM NOZZLE RUPTURE	4.45E-05	8.90E-05	11236	7.06%	Fault Trees-Page 64
RSRPVRUP	RSRM PRESSURE VESSEL RUPTURE	3.61E-05	7.22E-05	13850	5.73%	Fault Trees-Page 65
RSRWRTHR	RSRM WRONG THRUST	5.00E-09	1.00E-08	100000000	0.00%	Fault Trees-Page 66
SRBNOHLDN	SRB NO. LATE, OR IMPROPER HOLDDOWN RELEASE	1.29E-04	2.58E-04	3876	20.48%	Fault Trees-Page 68
SRBNOIGN	NO OR LATE IGNITION OF 1 SRB/RSRM	1.11E-04	2.22E-04	4505	17.62%	Fault Trees-Page 82
SRBNOSEP	SRB FAILS TO SEPARATE	6.95E-05	1.39E-04	7194	11.03%	Fault Trees-Page 87
SRBPREMHD	SRB HOLDDOWN: PREMATURE RELEASE	8.00E-07	1.60E-06	625000	0.13%	Fault Trees-Page 190
SRBRECPREM	SRB RECOVERY DEVICE: PREMATURE RELEASE	3.00E-06	6.00E-06	166667	0.48%	Fault Trees-Page 191
SRBSTR	SRB STRUCTURAL FAILURES	5.00E-07	1.00E-06	1000000	0.08%	Fault Trees-Page 192
SRBTV	SRB THRUST VECTOR CONTROL SYSTEM FAILURE	3.57E-05	7.13E-05	14025	5.66%	Fault Trees-Page 193

82

ISRB Hypothesis Descriptions

- Hypothesis-1 The analyst made an educated estimate of the anticipated frequency of the event in question. This was deemed necessary when there was insufficient data to support a statistical analysis. The estimation was made after conferring with experts on reliability of the sub-component based on their respective experience.
- Hypothesis-2 Insufficient data to support a statistical analysis was available for the NASA Standard Initiators (NSIs) and NASA Standard Detonators (NSDs) however the components were found to be similar in both design and function as the Confined Detonating Fuses (CDFs). However due to additional elements in the NSI and NSD assemblies they were assumed to be 2-3 times more prone to fail than the CDF.
- Hypothesis-3 The data available for the Pyrotechnic Initiator Controllers (PICs) indicates that they are extremely reliable components however the fact that no actual failures have occurred makes the estimation of their failure rate difficult. As a conservative assumption, their failure rate was assumed to be on the same order of magnitude as the CDFs.
- Hypothesis-4 The ISRB use pyrogenic igniters for which a limited amount of failure data exists. For this reason the analyst made a conservative assumption based on the data available and conversations with USBI personnel.
- Hypothesis-5 This estimate concerned the possibility of an explosive device detonating without any external influences; an extremely rare event. A conservative estimate was made which considered such an event to be 10 times less likely than an explosive device (CDF) failing to detonate on command.
- Hypothesis-6 The Booster Separation Motors (BSMs) have a limited amount of failure related data however it was agreed (USBI & MSFC) that the failure modes were approximately an order of magnitude (10 times) more likely than an explosive device (CDF) failing to detonate.





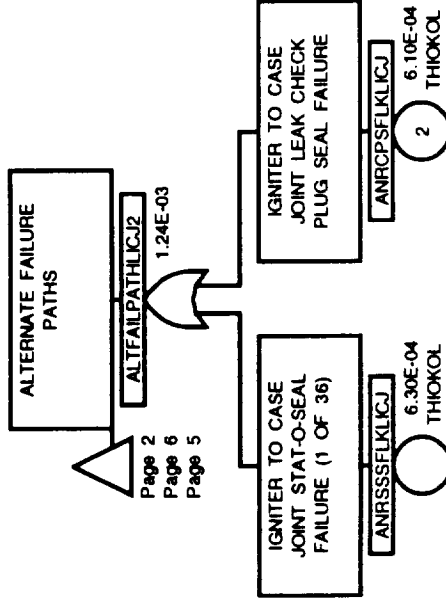
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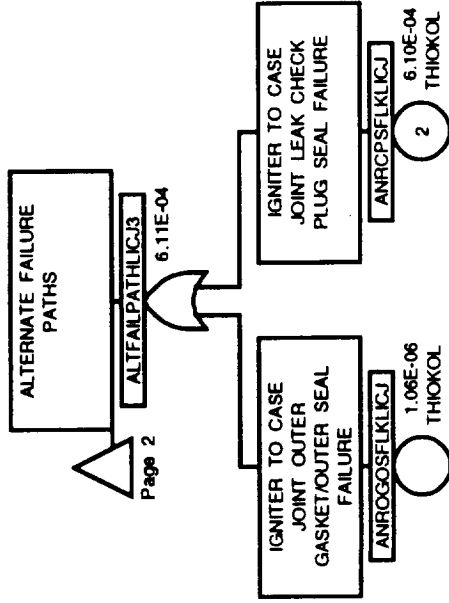


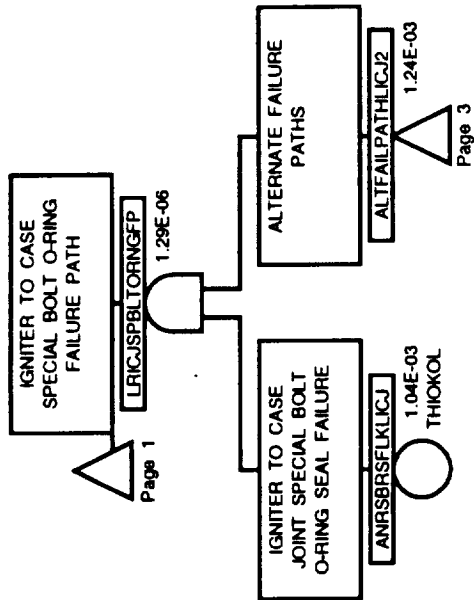
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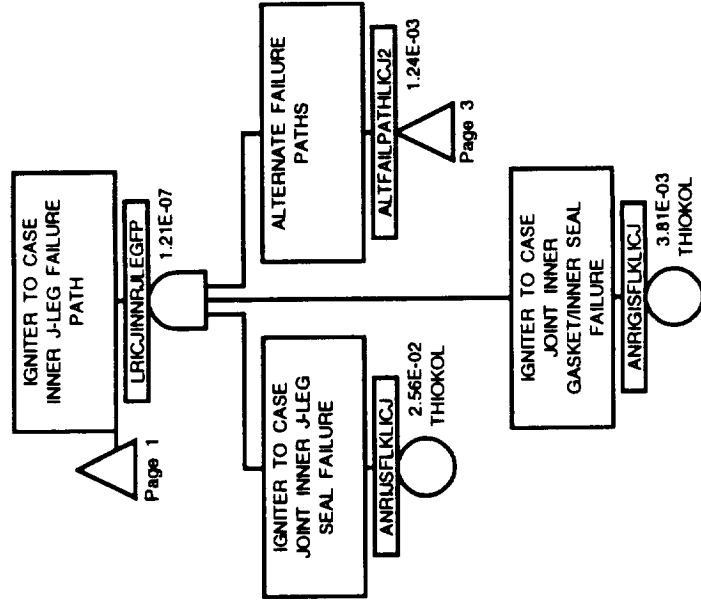


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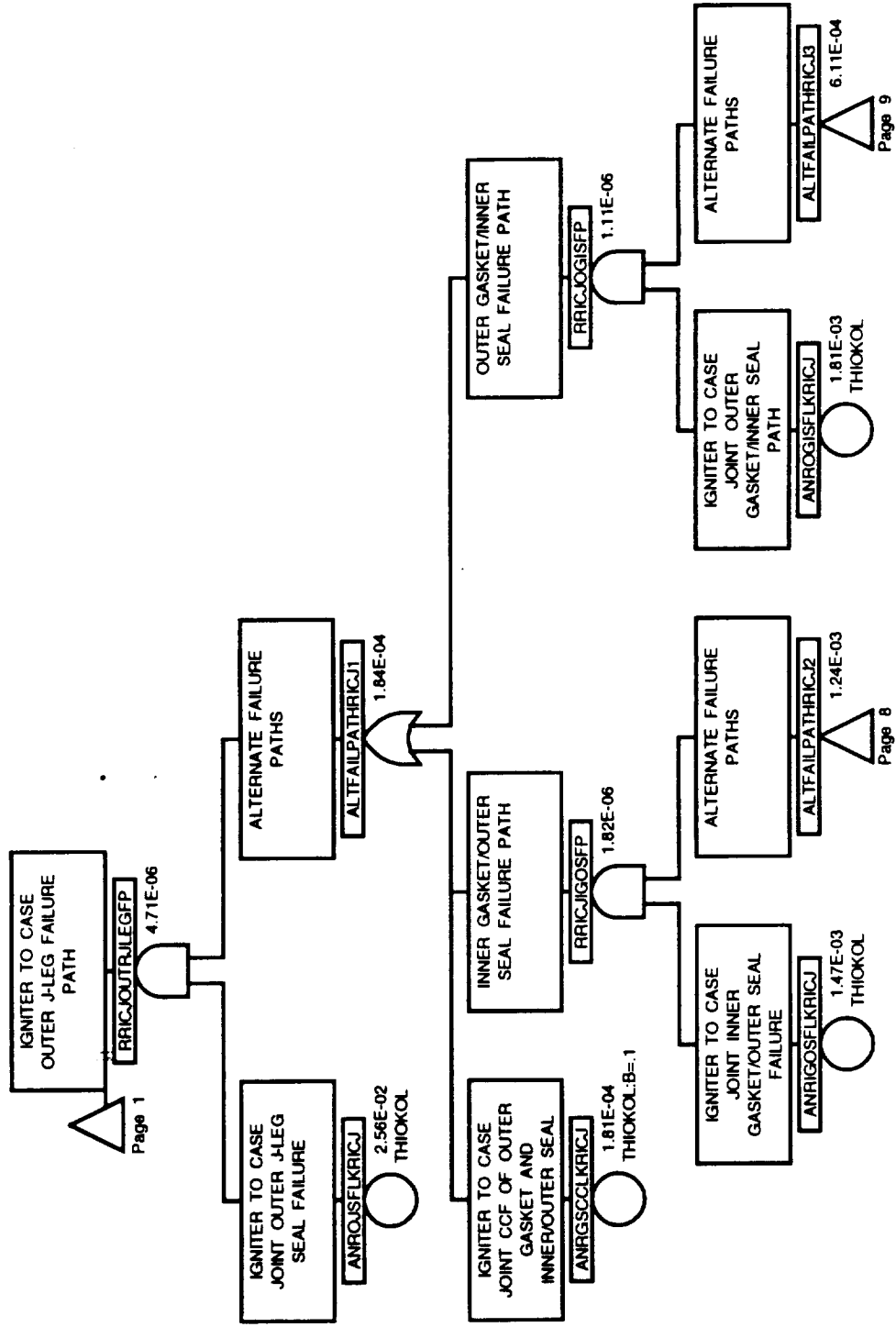






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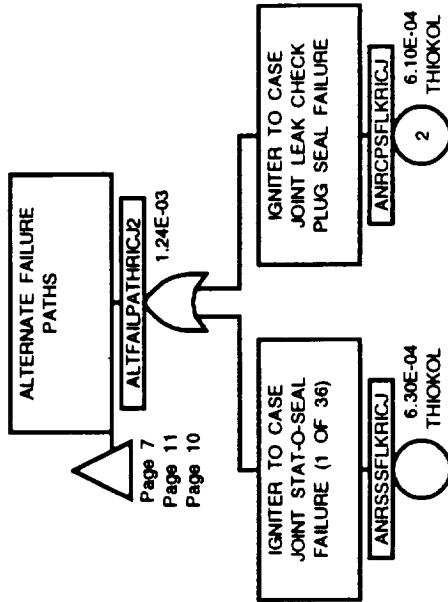
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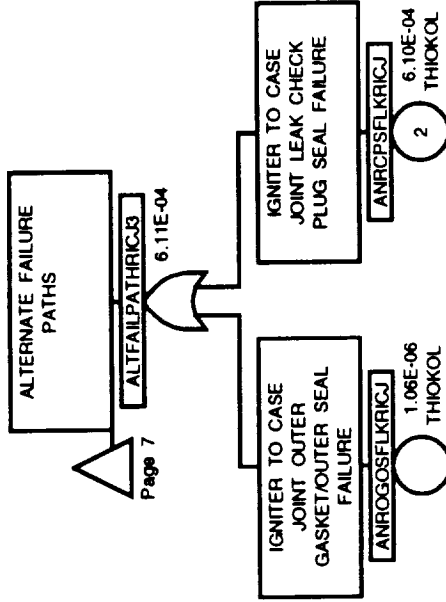


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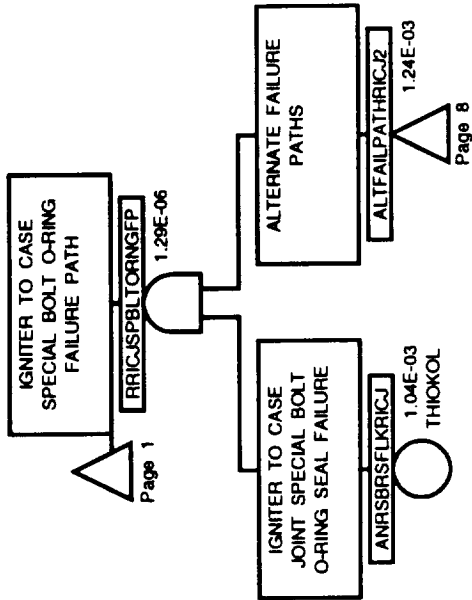
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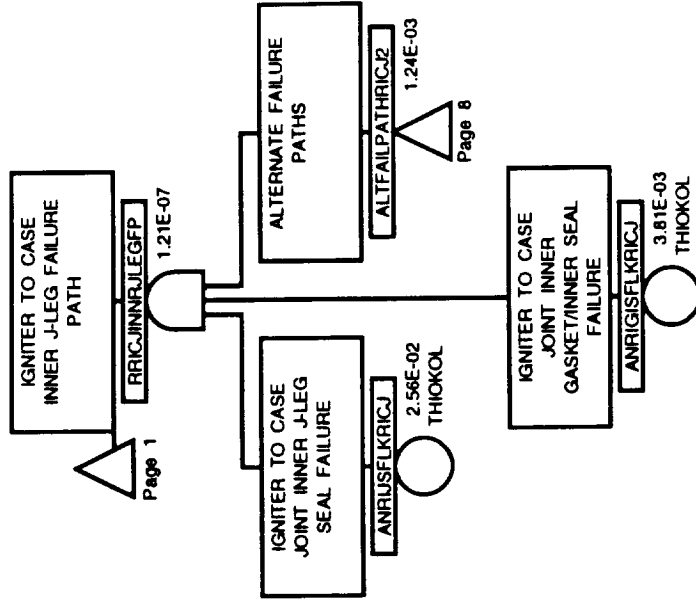
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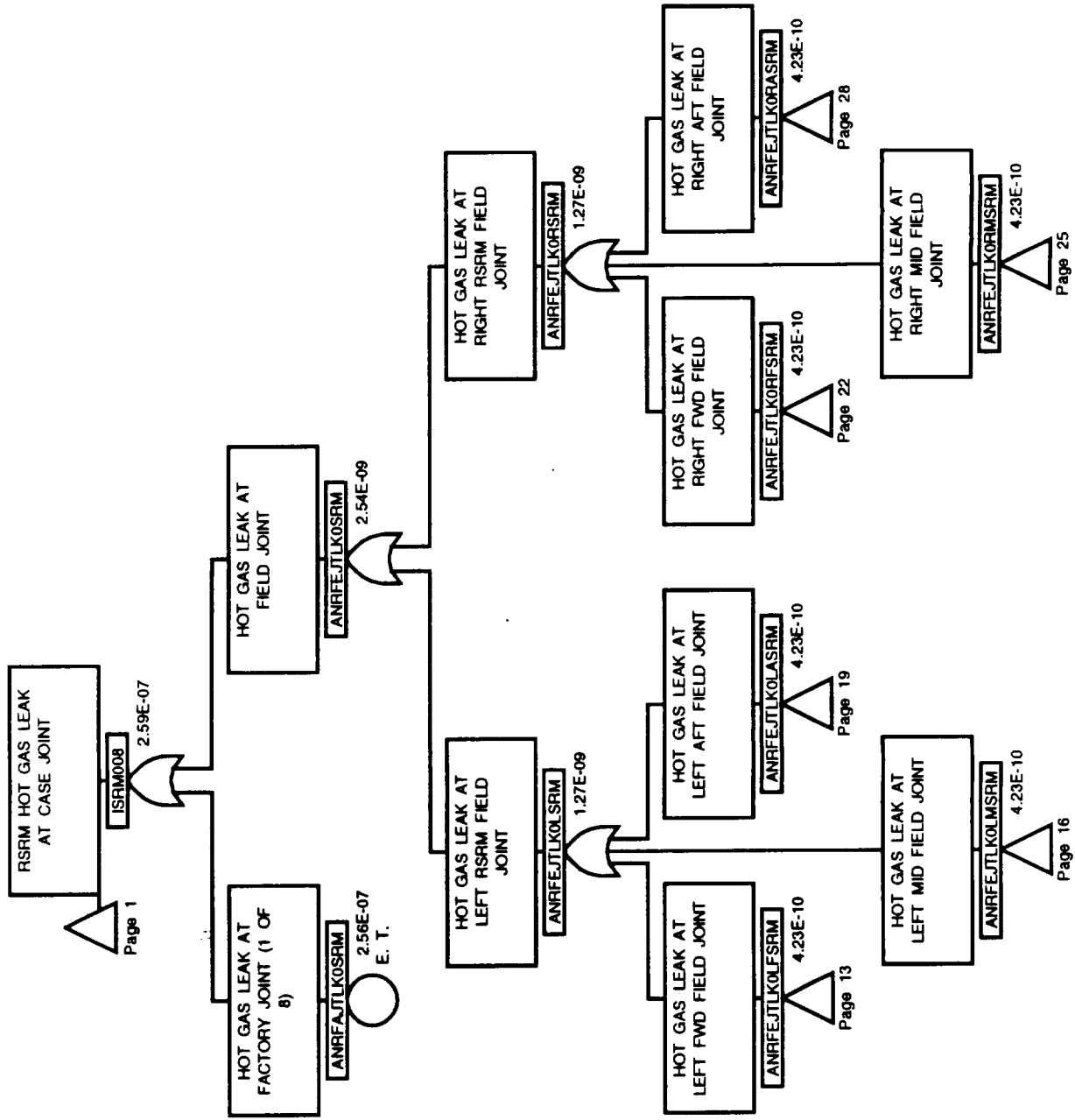


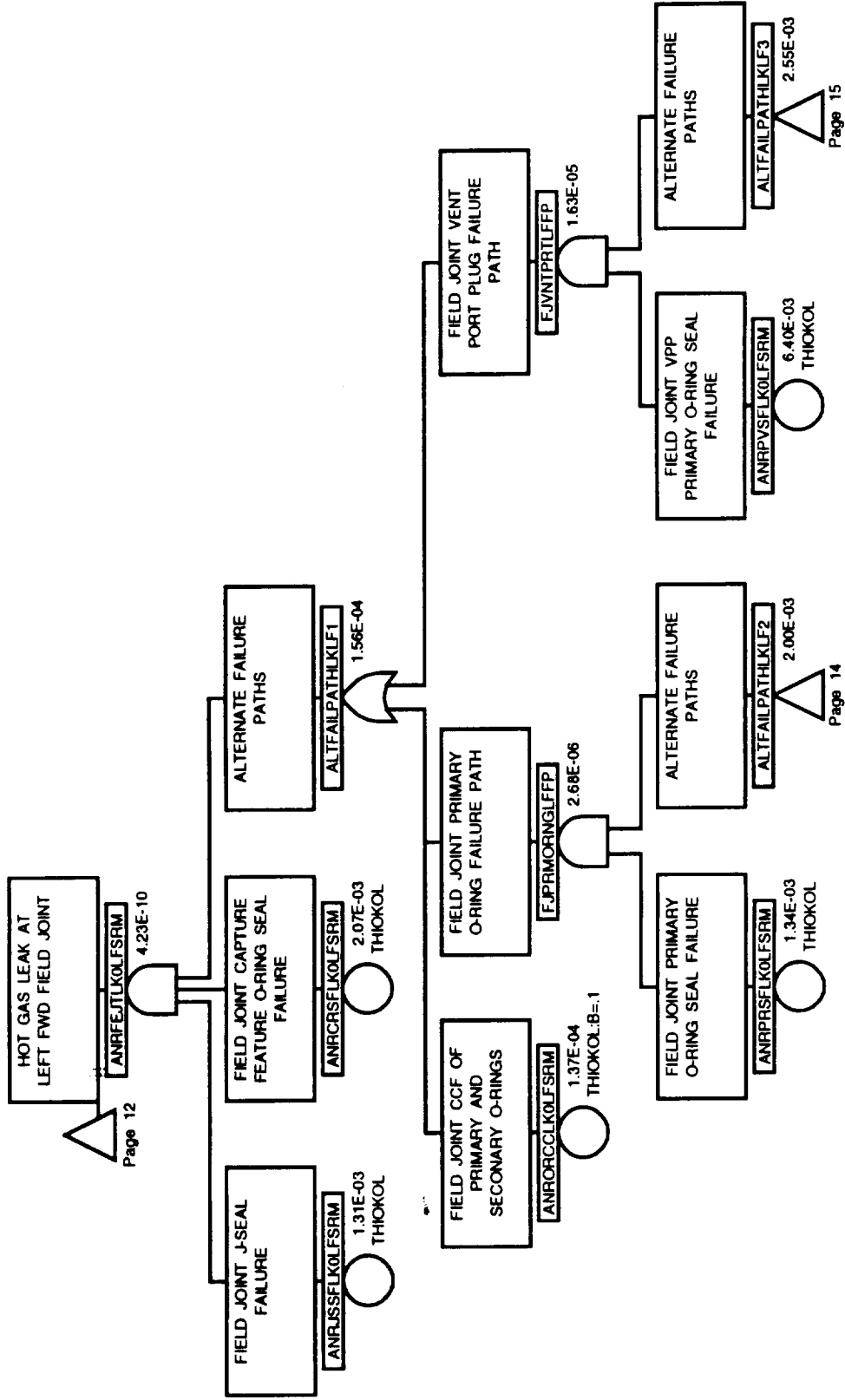


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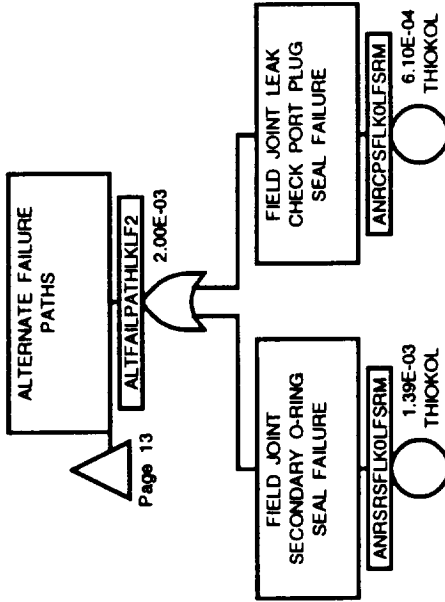




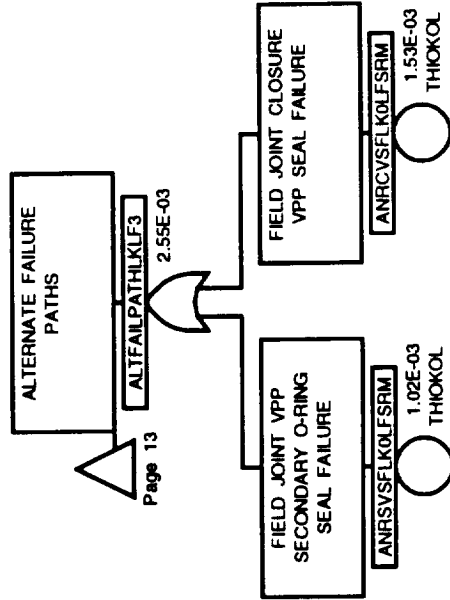
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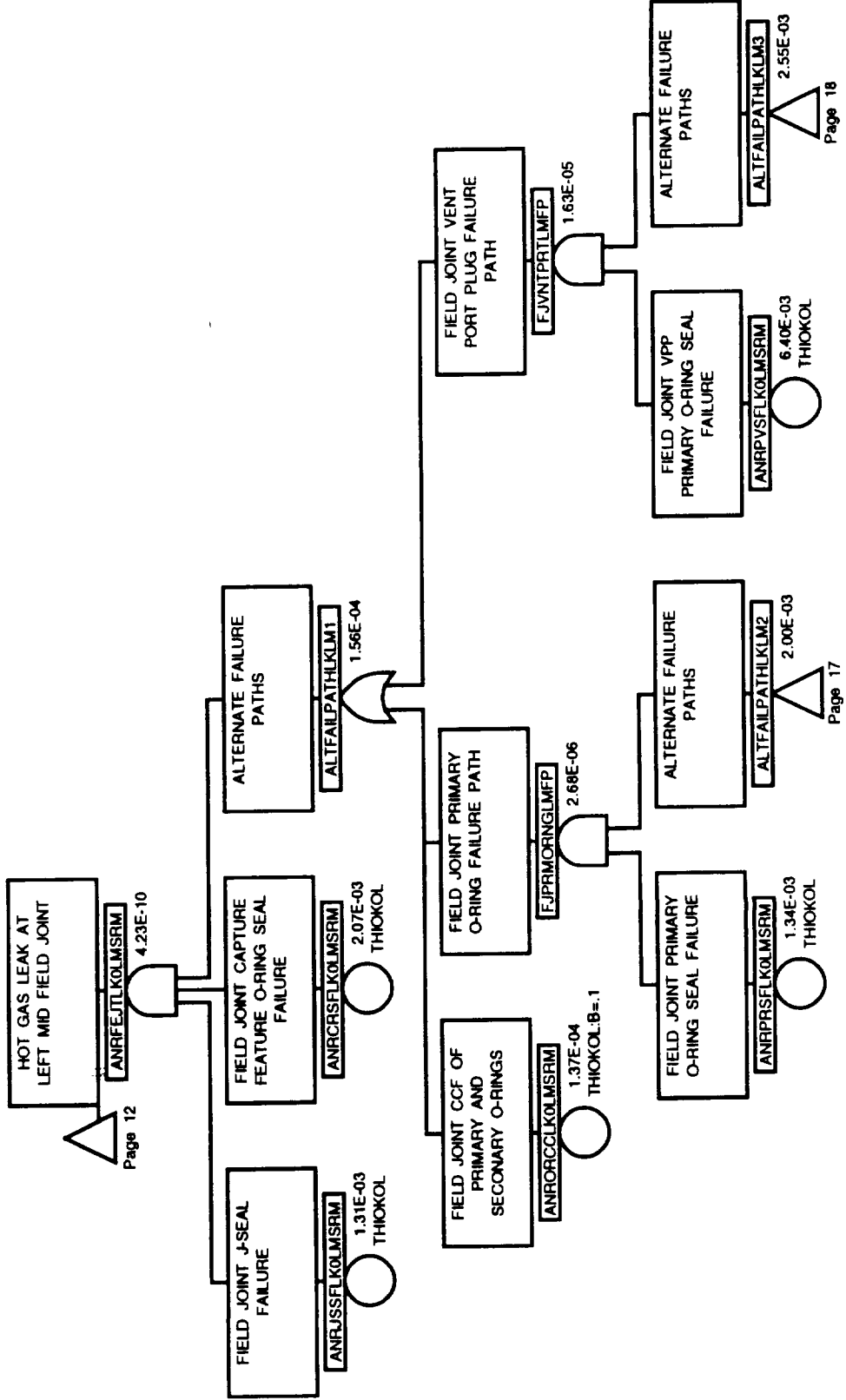
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Page 13



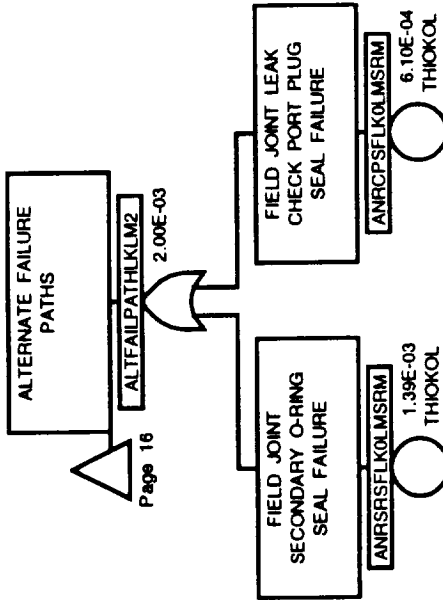
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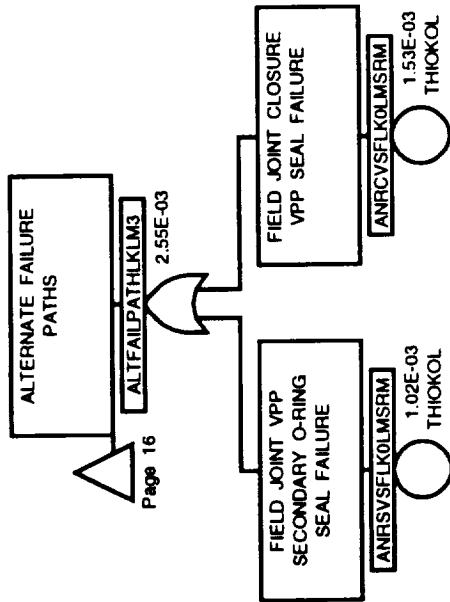
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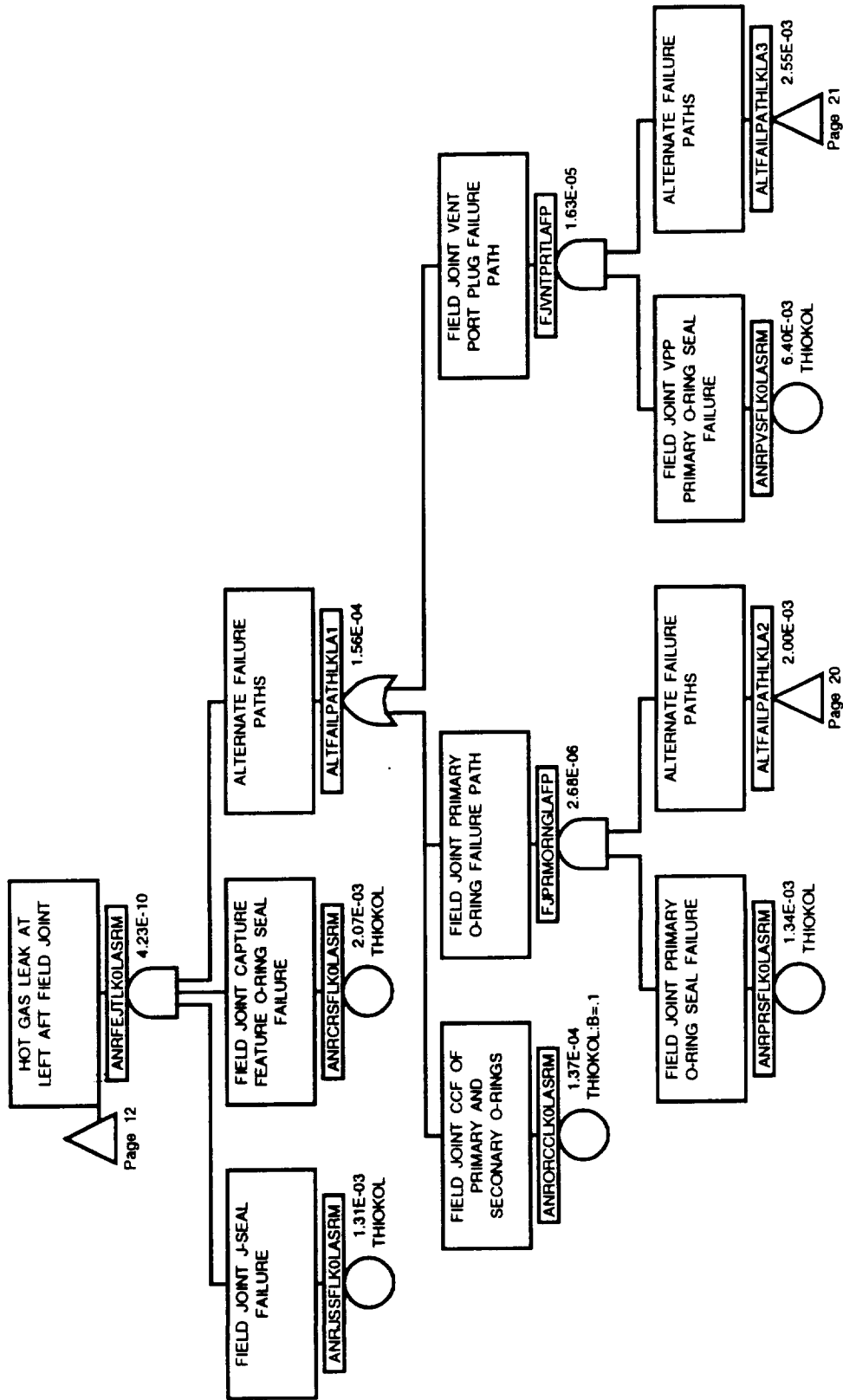
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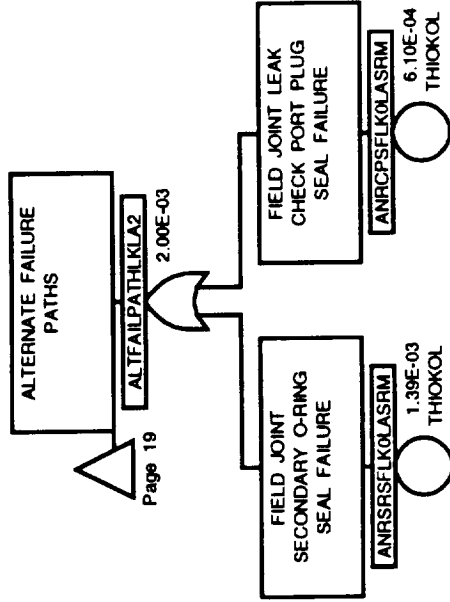
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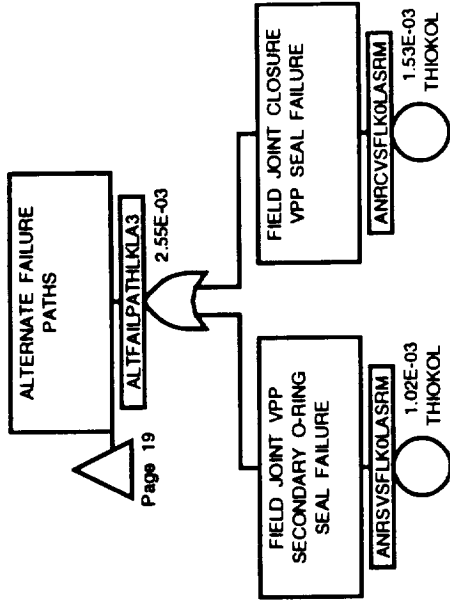


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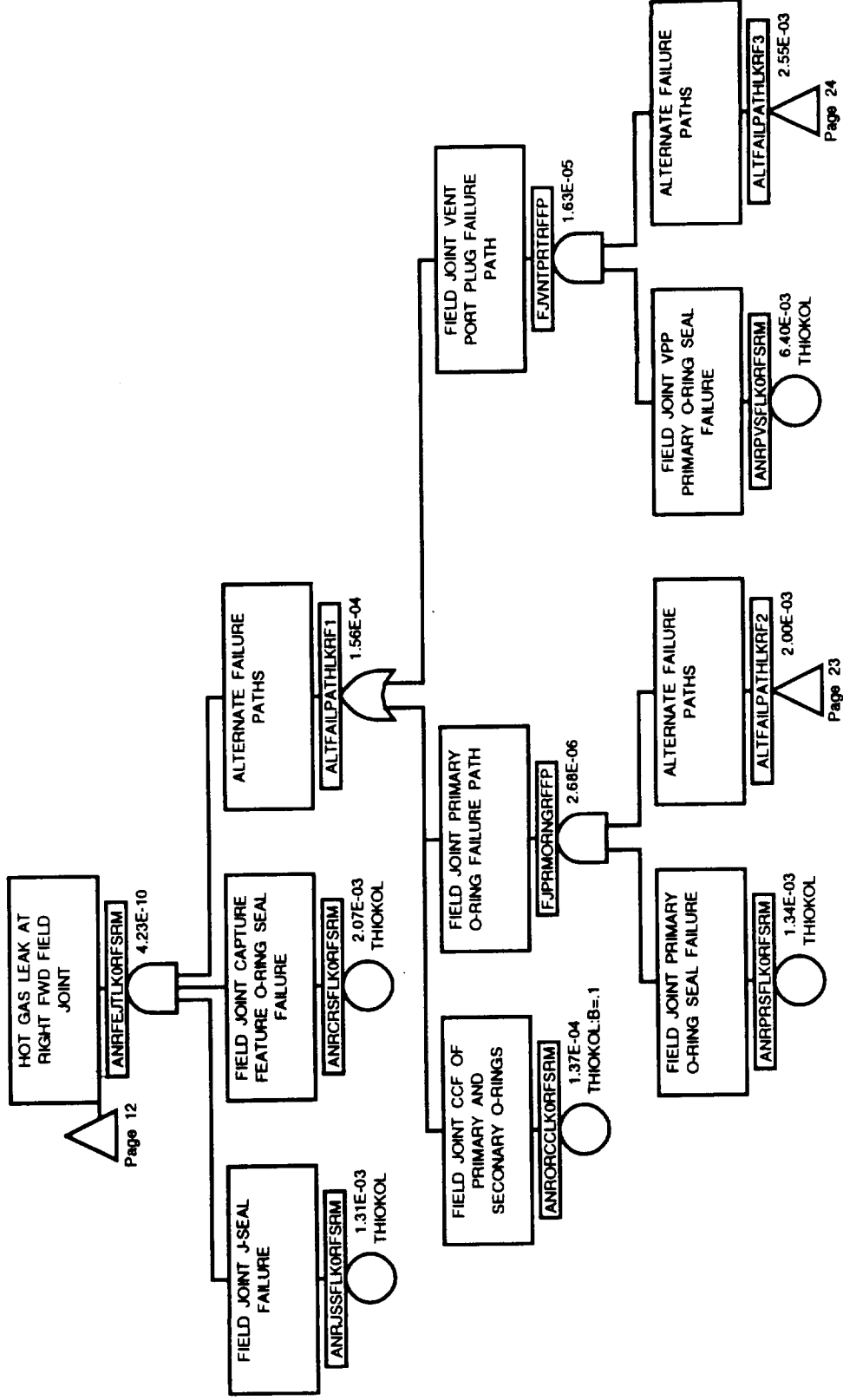
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Page 21





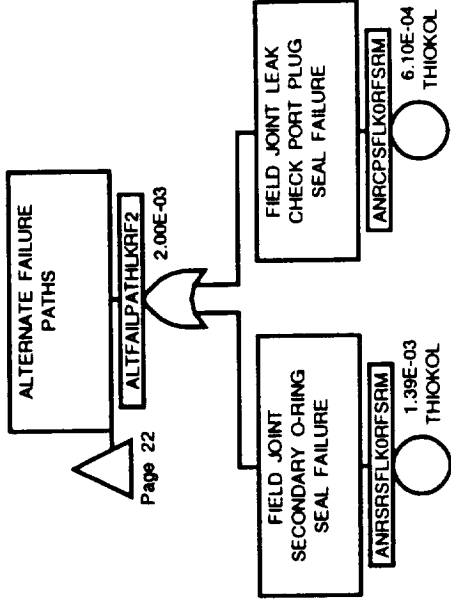
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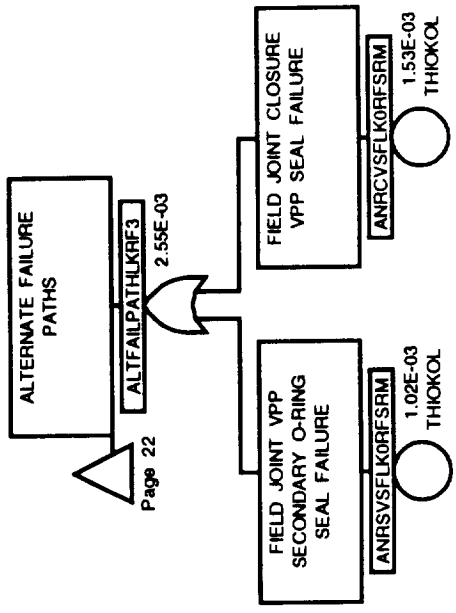
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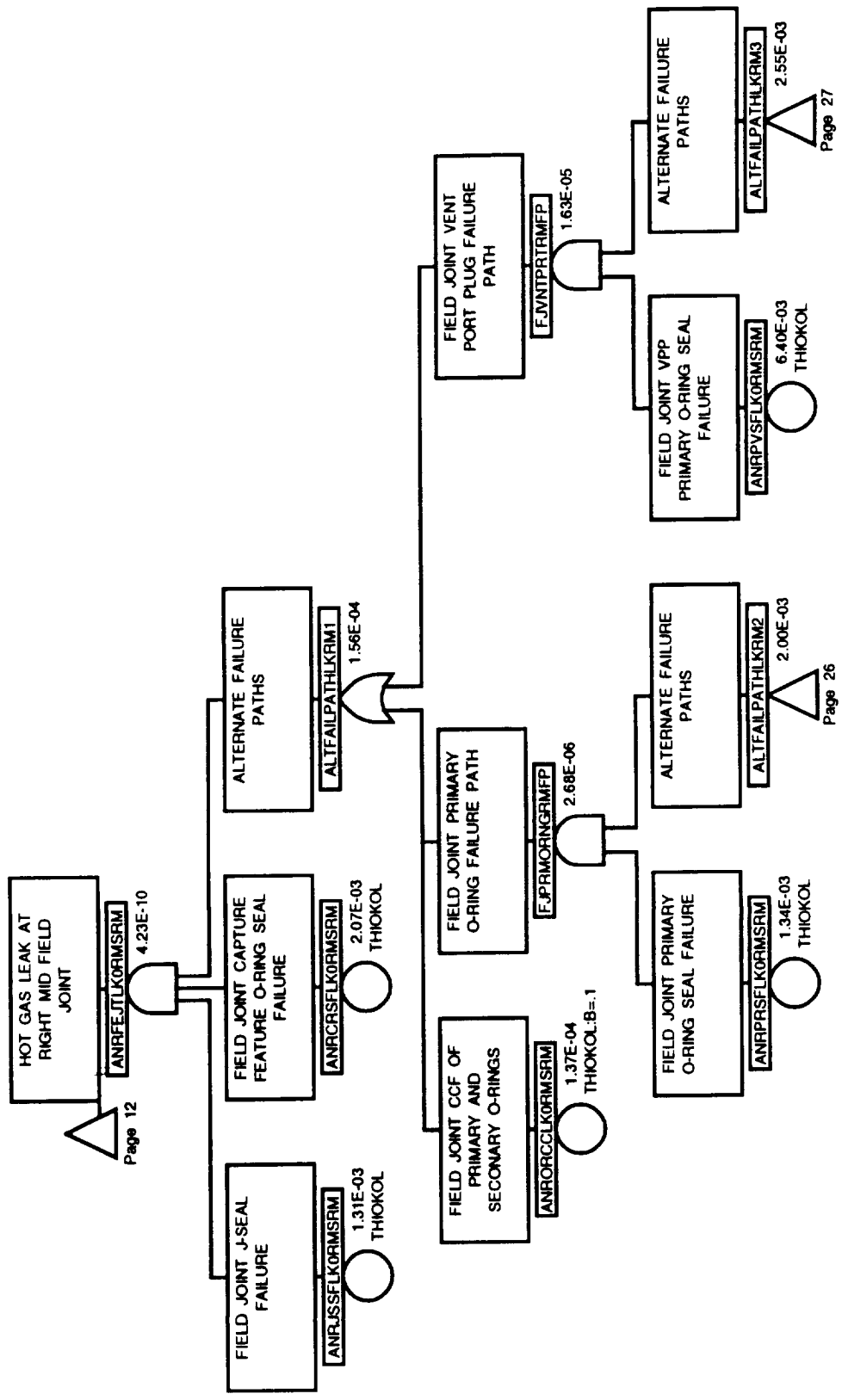
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Page 22



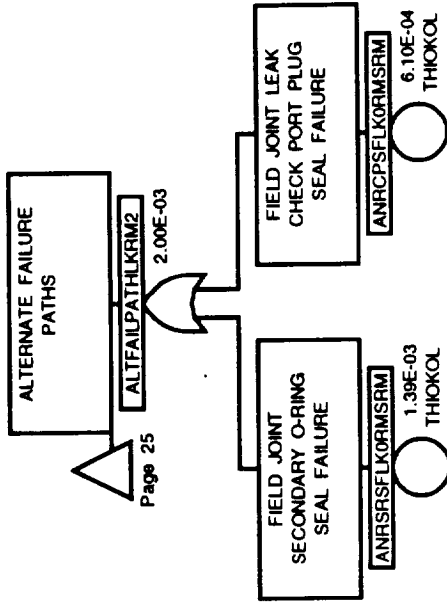
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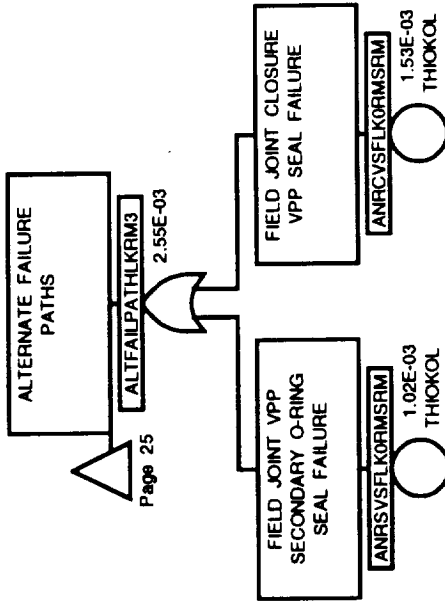
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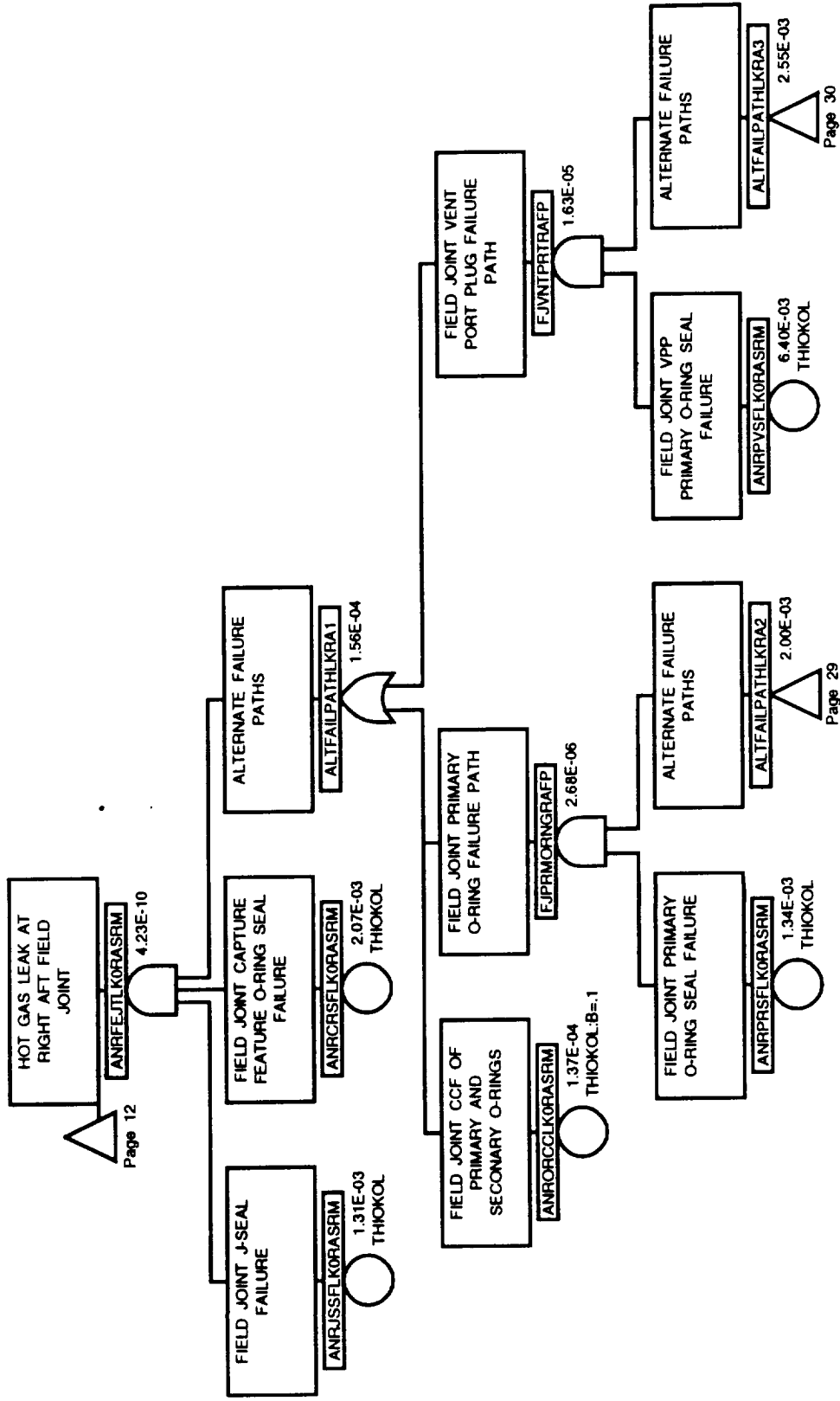
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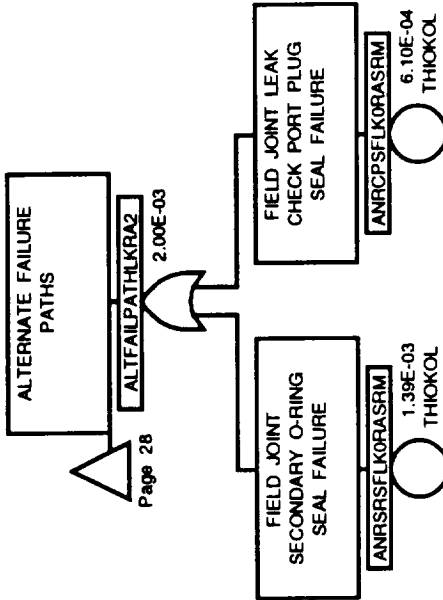
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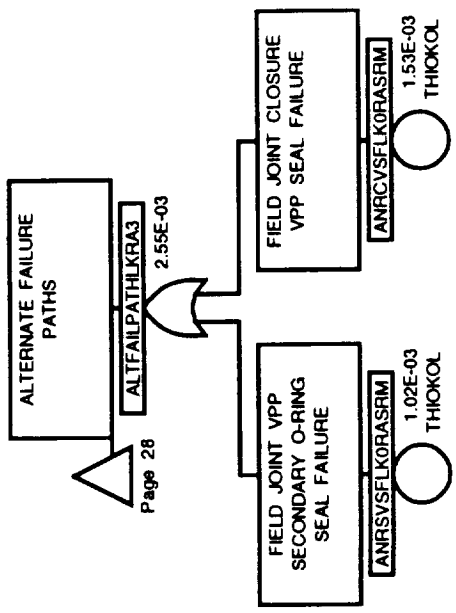
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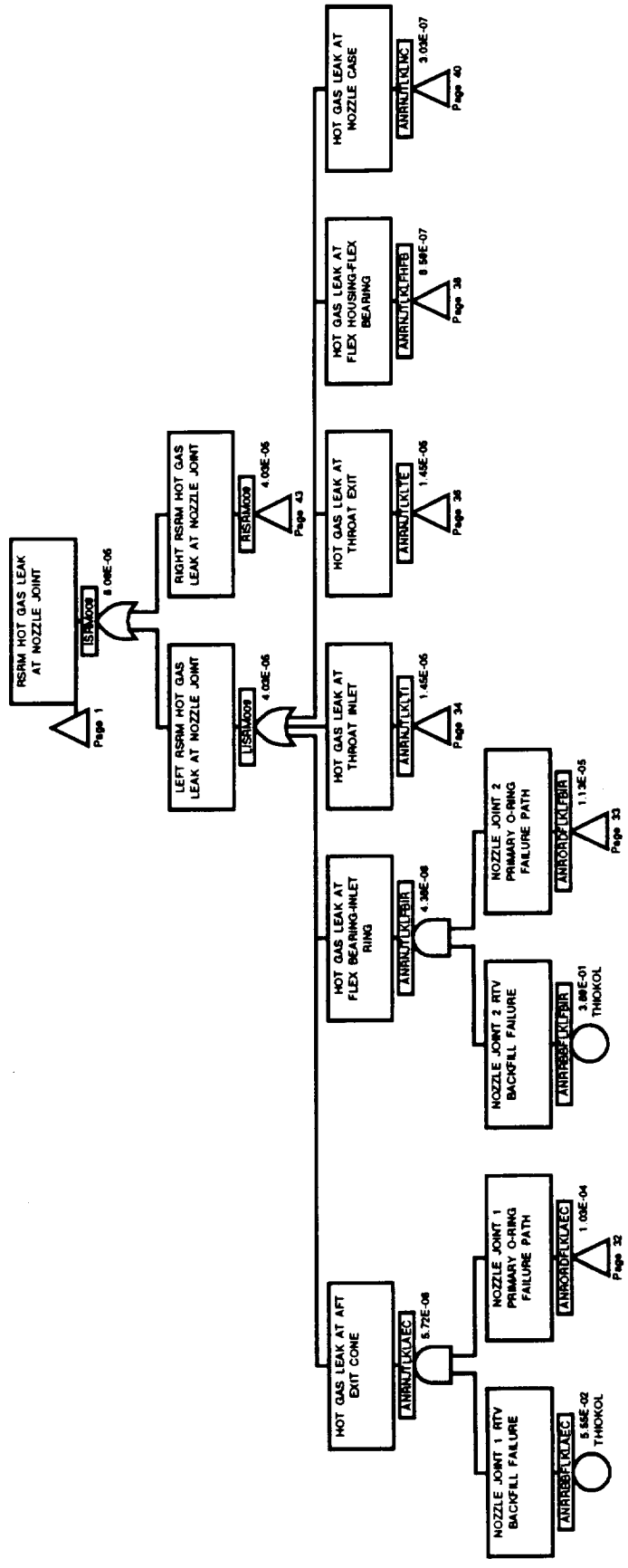
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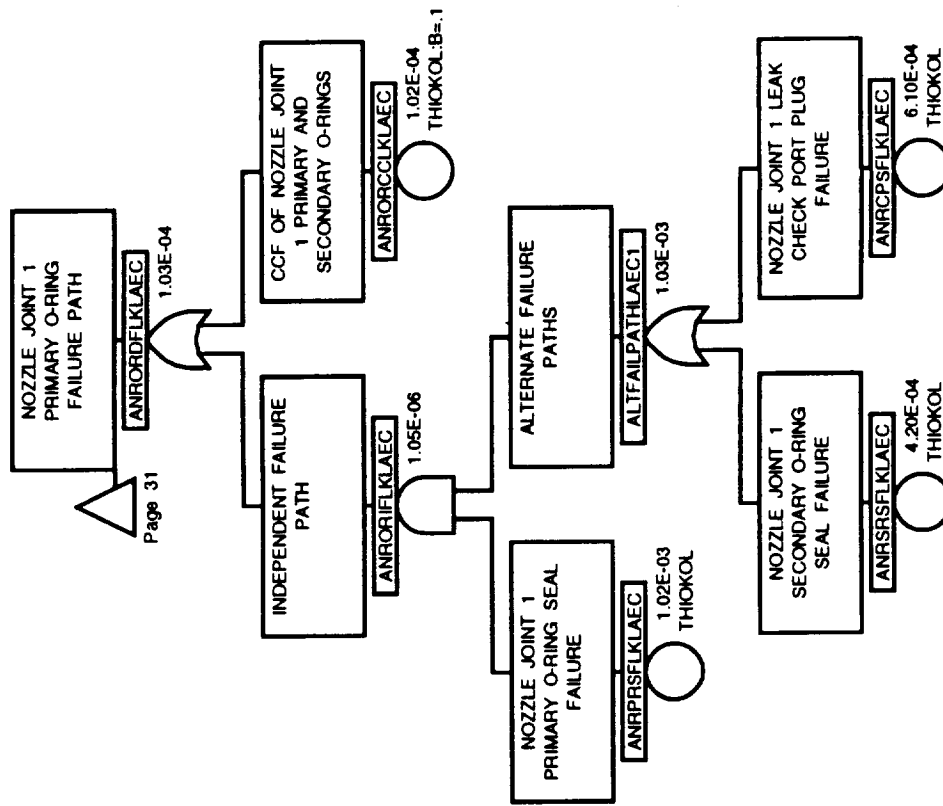


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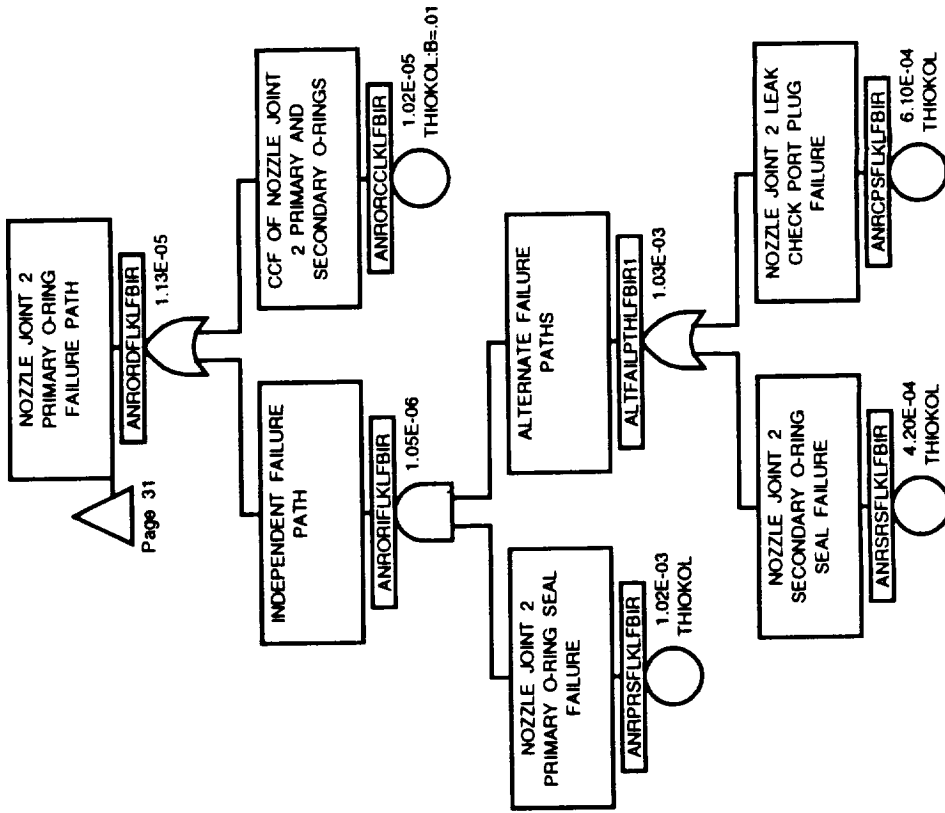


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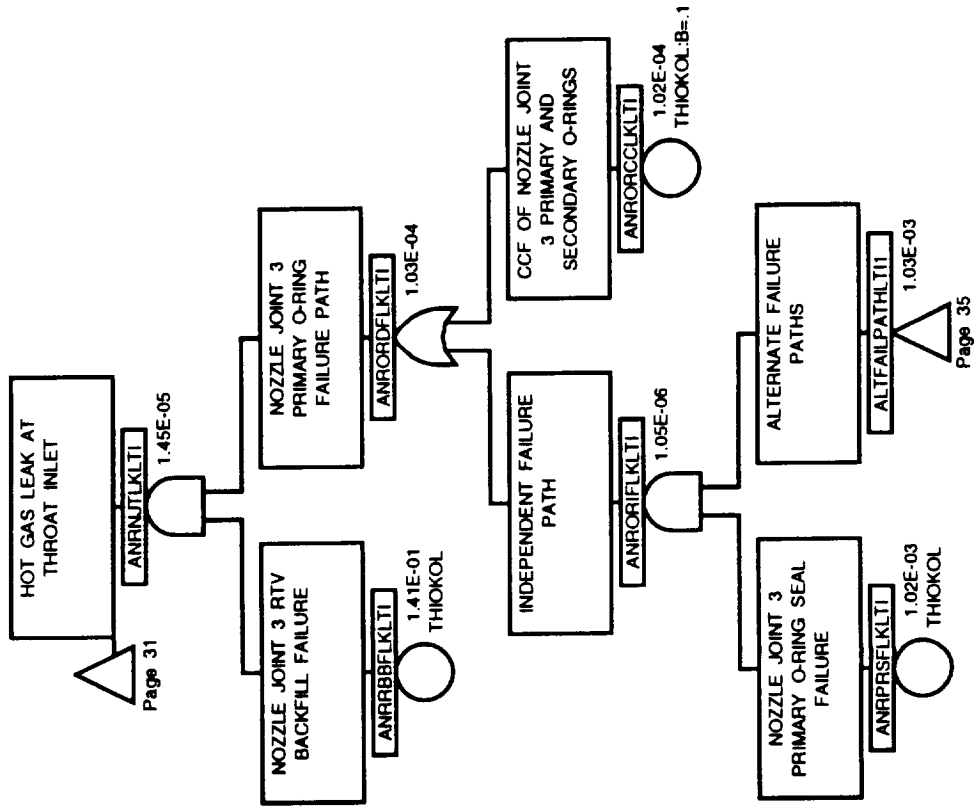


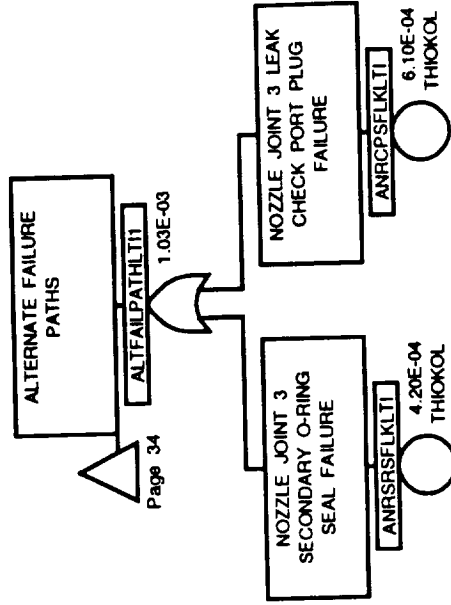


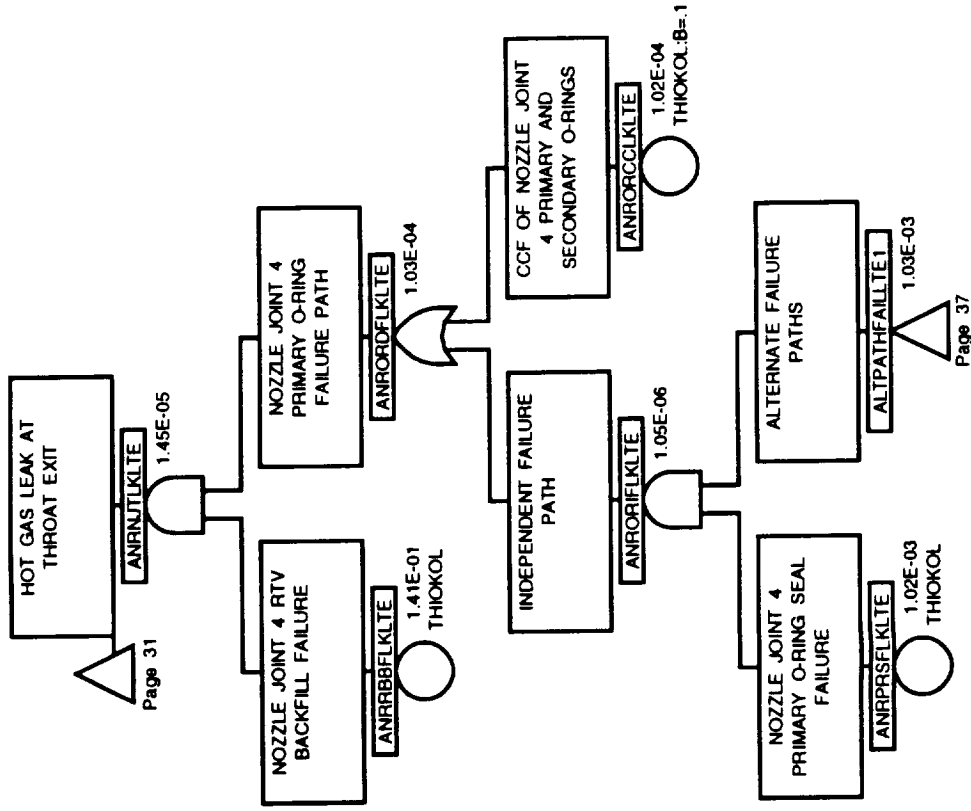
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Page 31

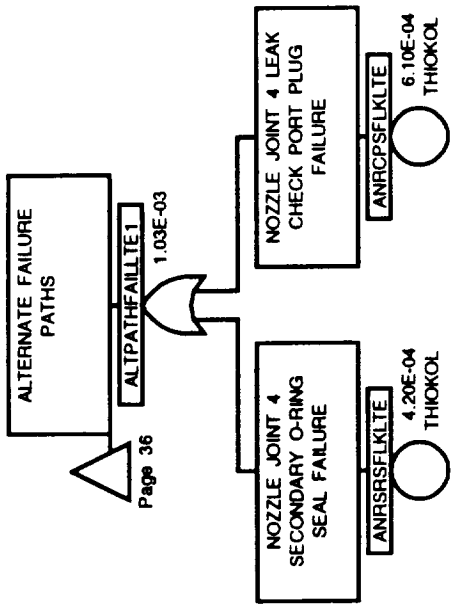




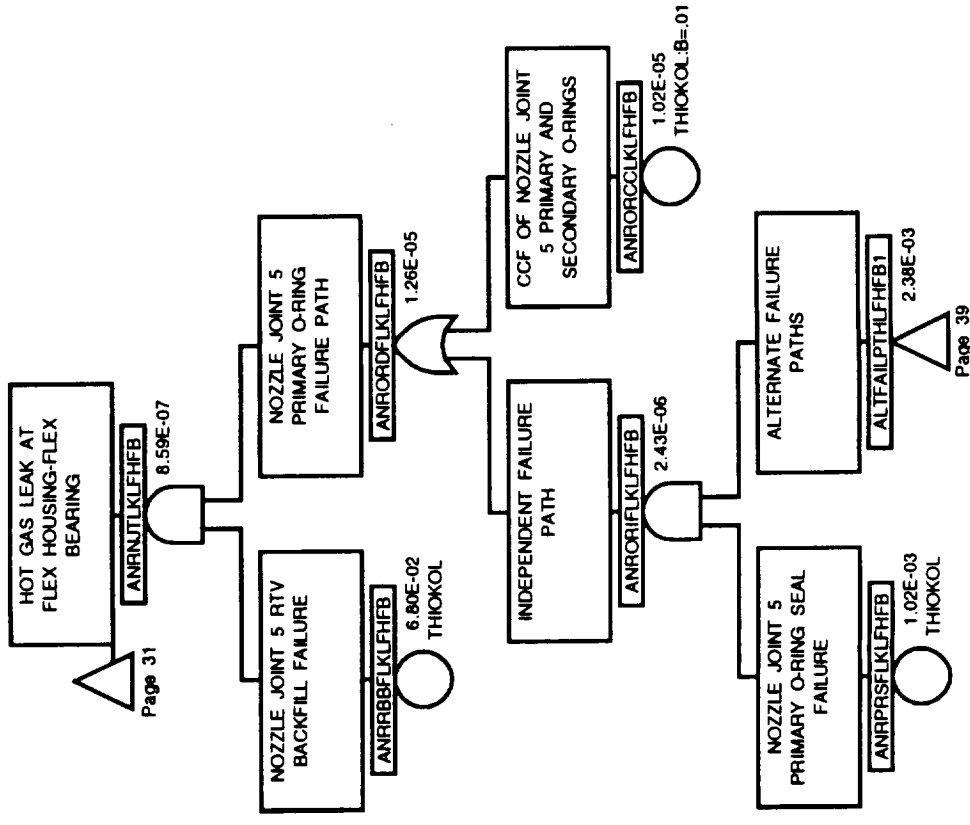


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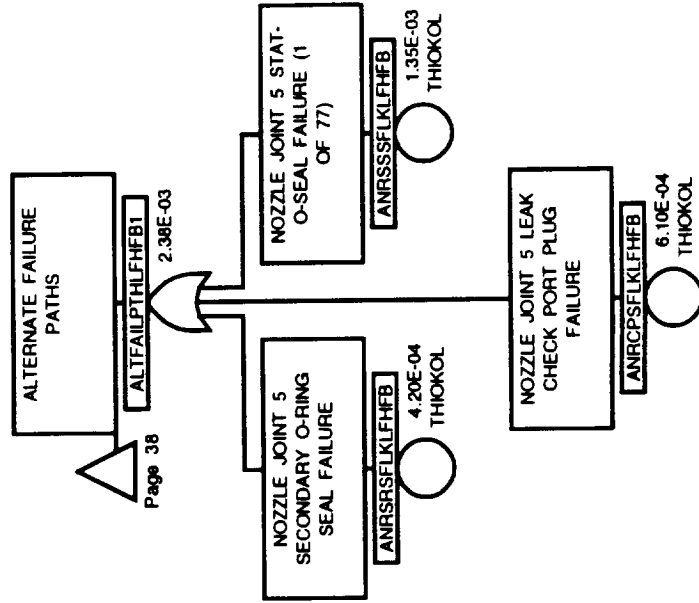


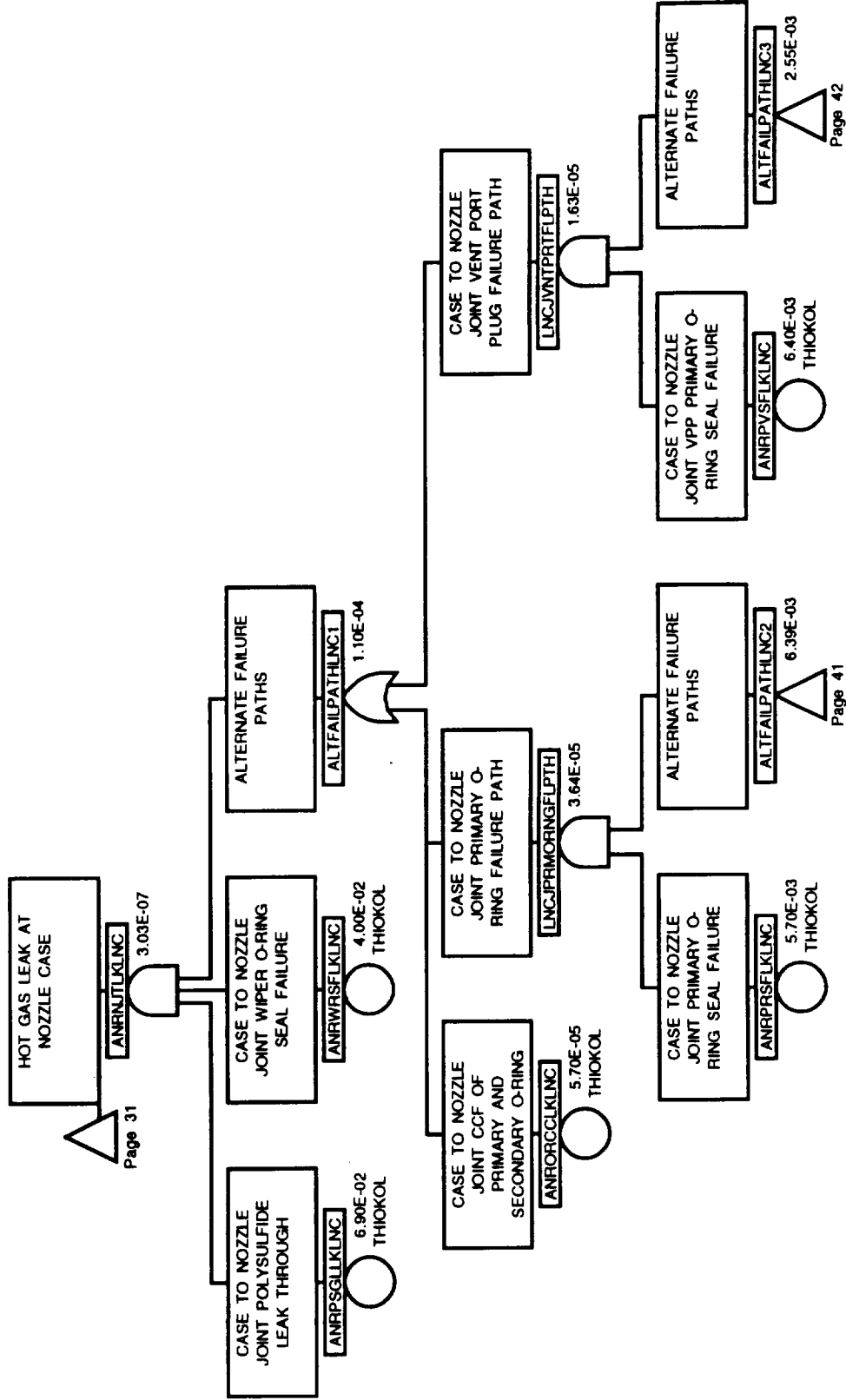
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Page 31

Page 39

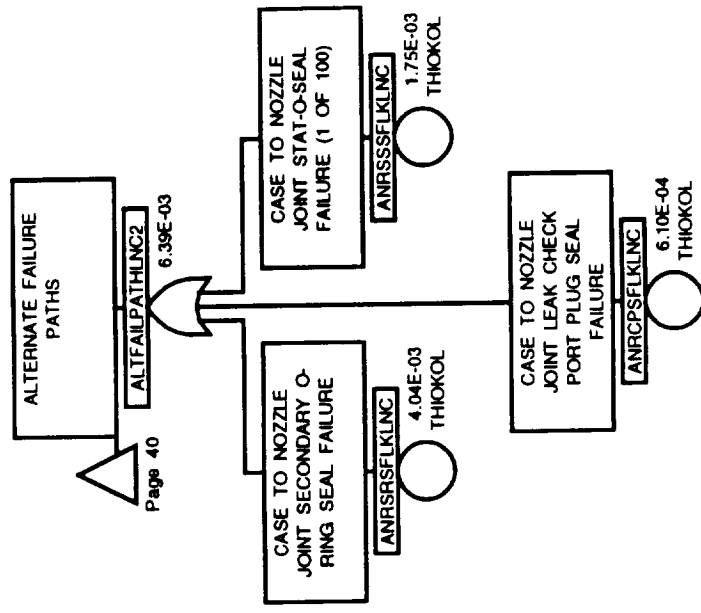




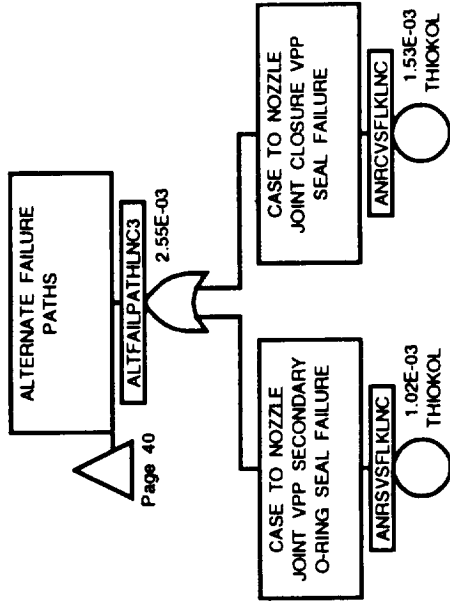
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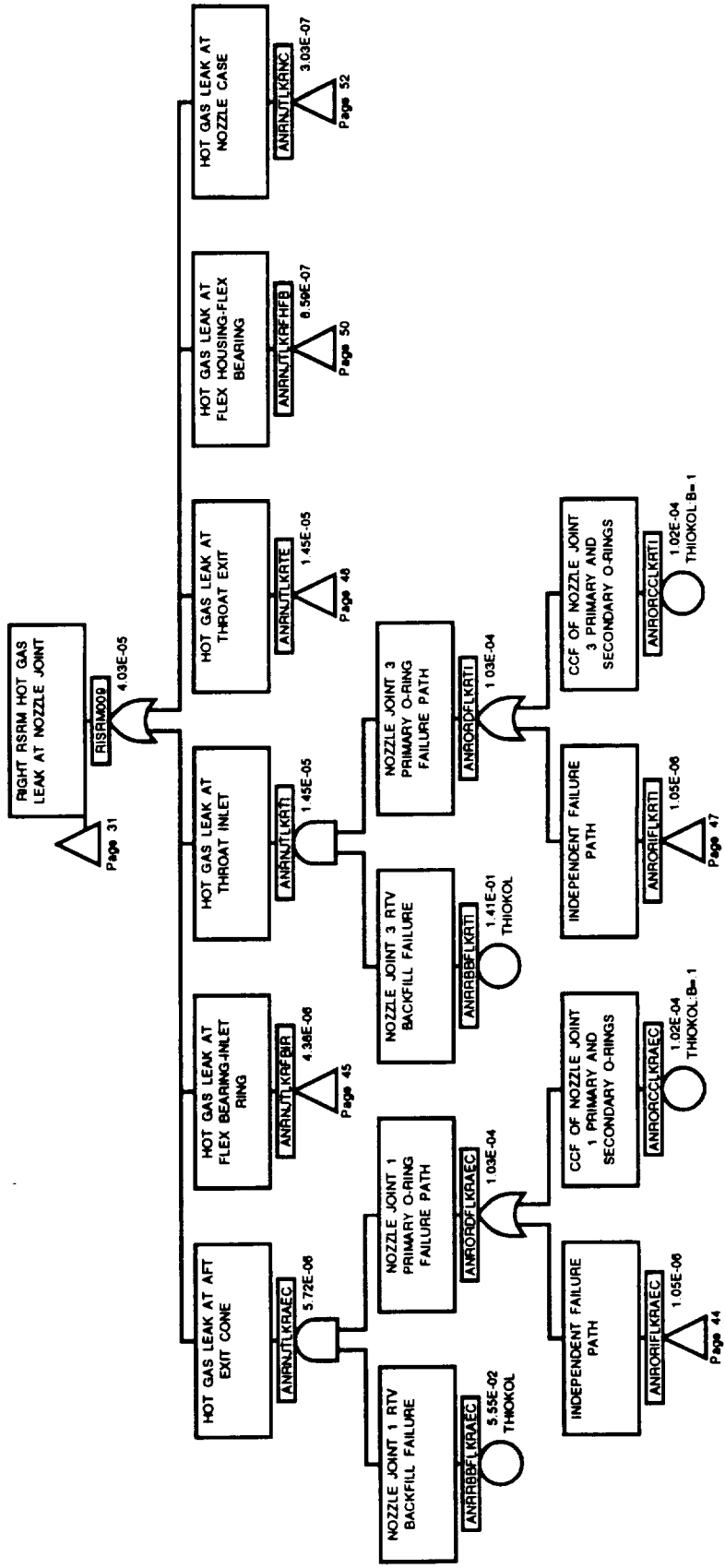
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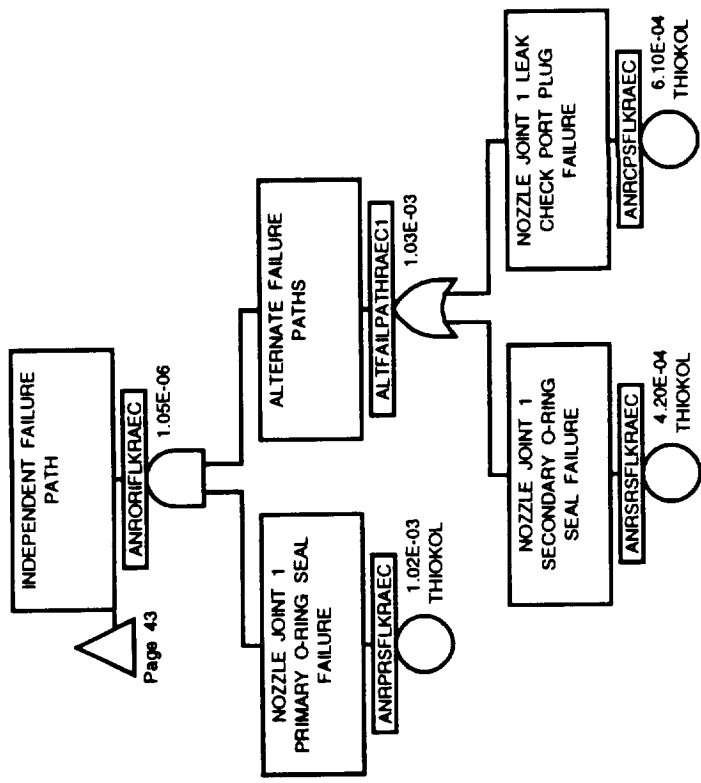
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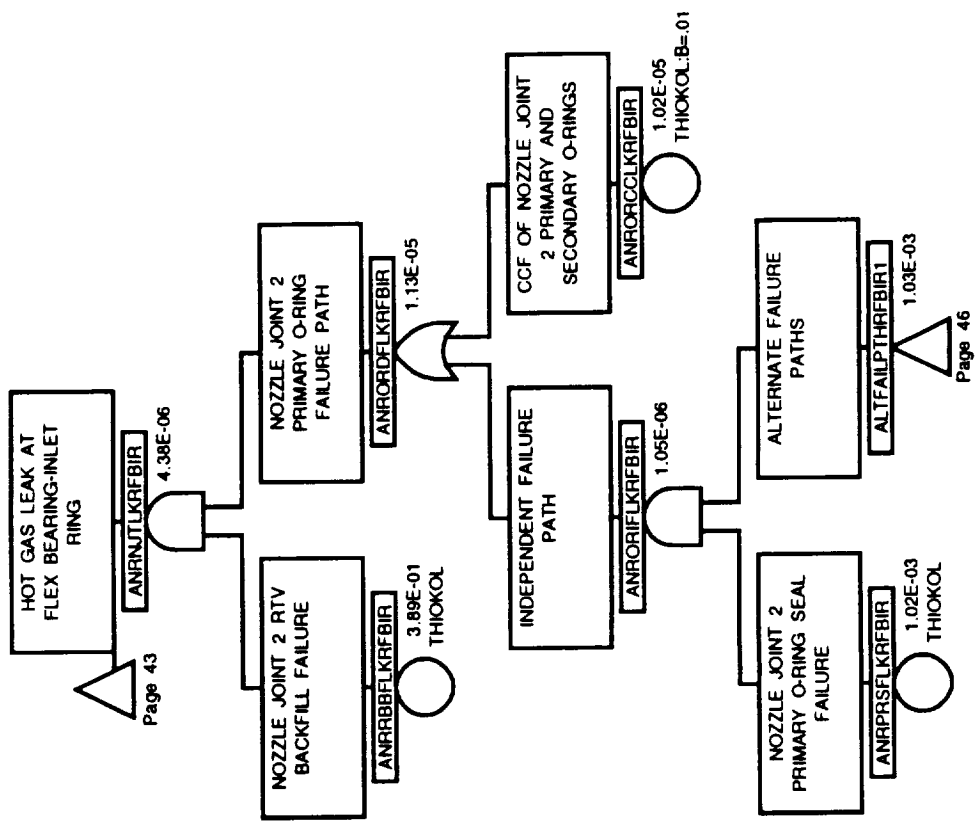
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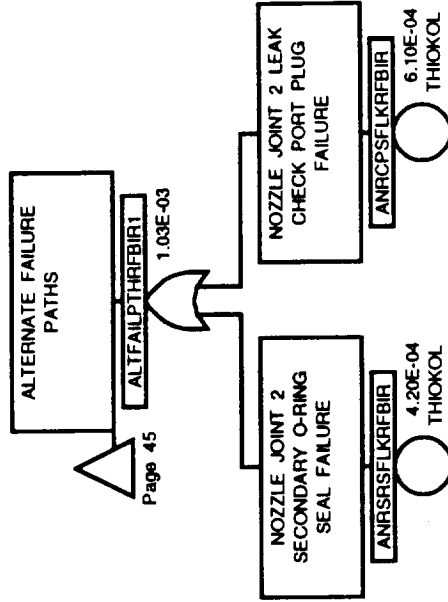


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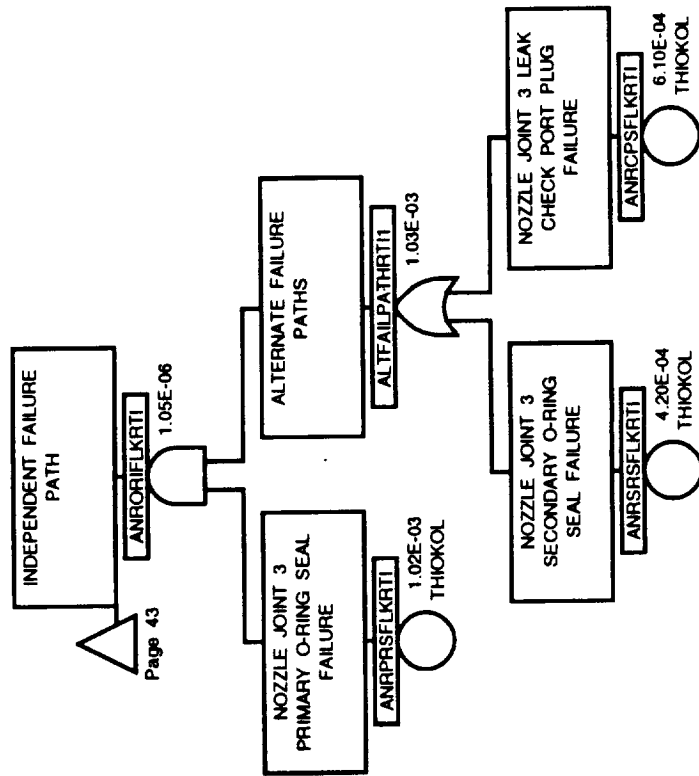


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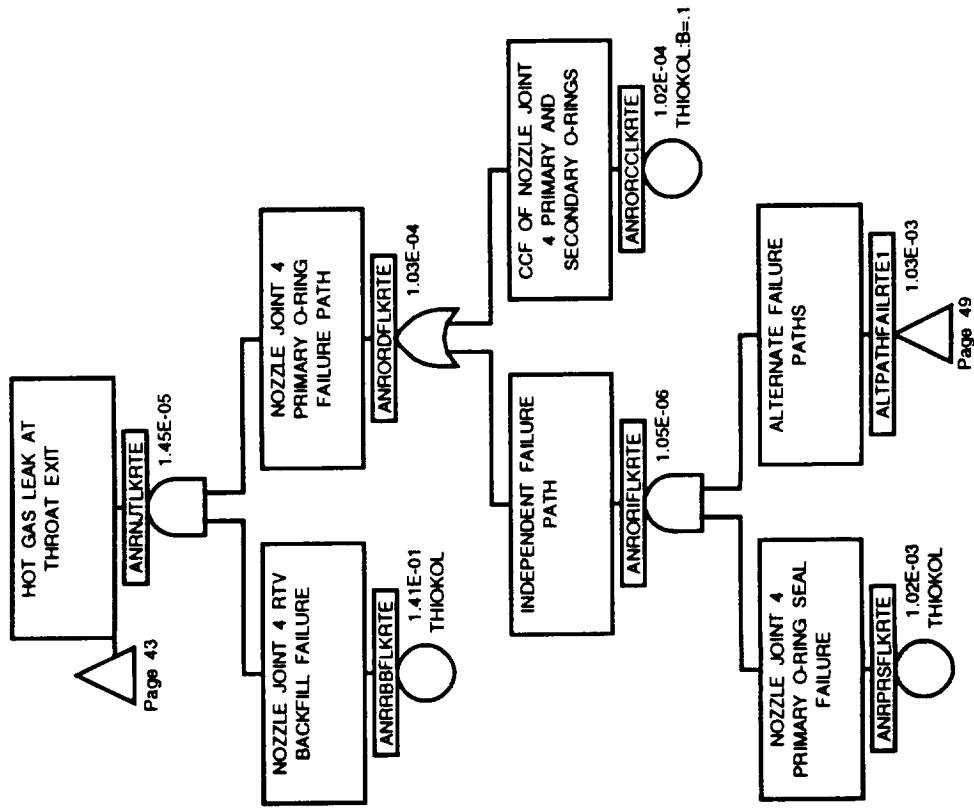
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Page 45

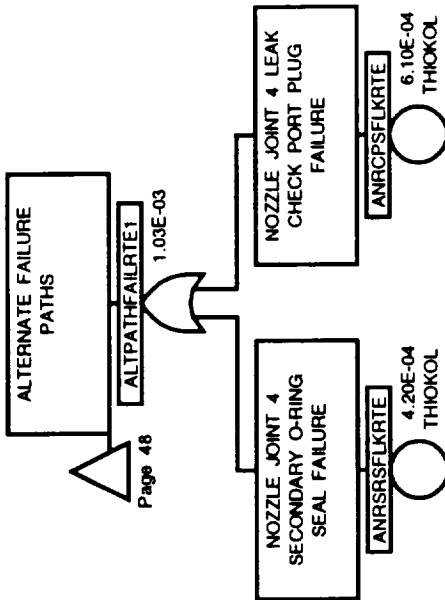


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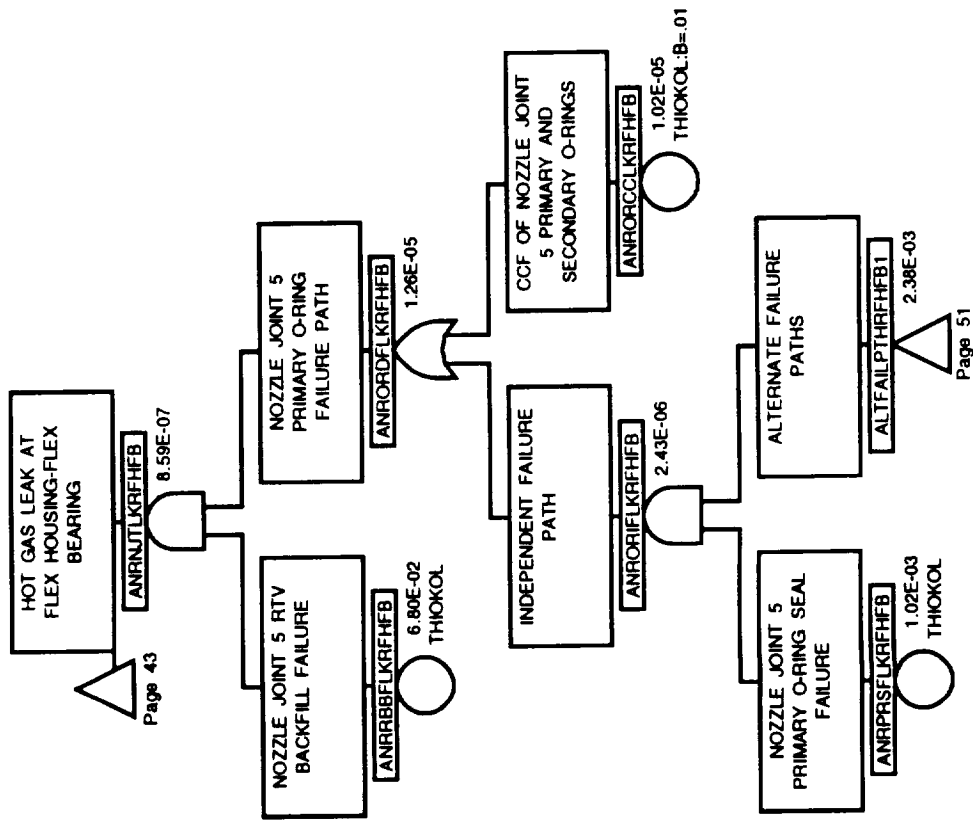


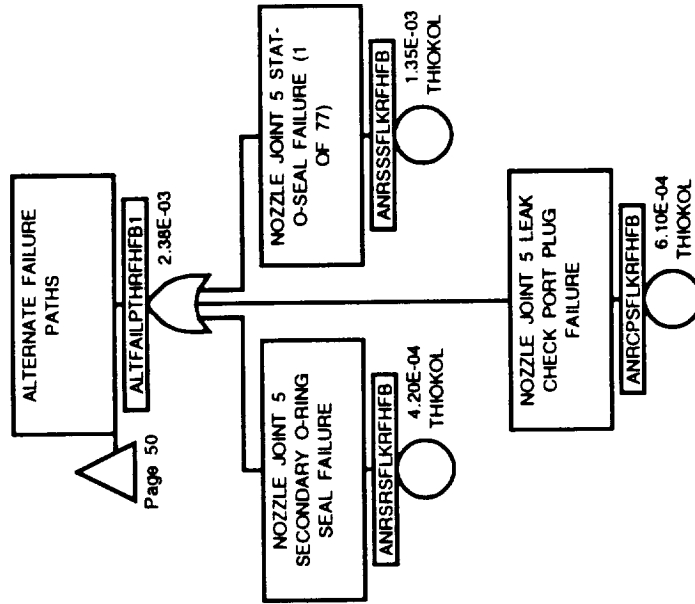
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Page 49

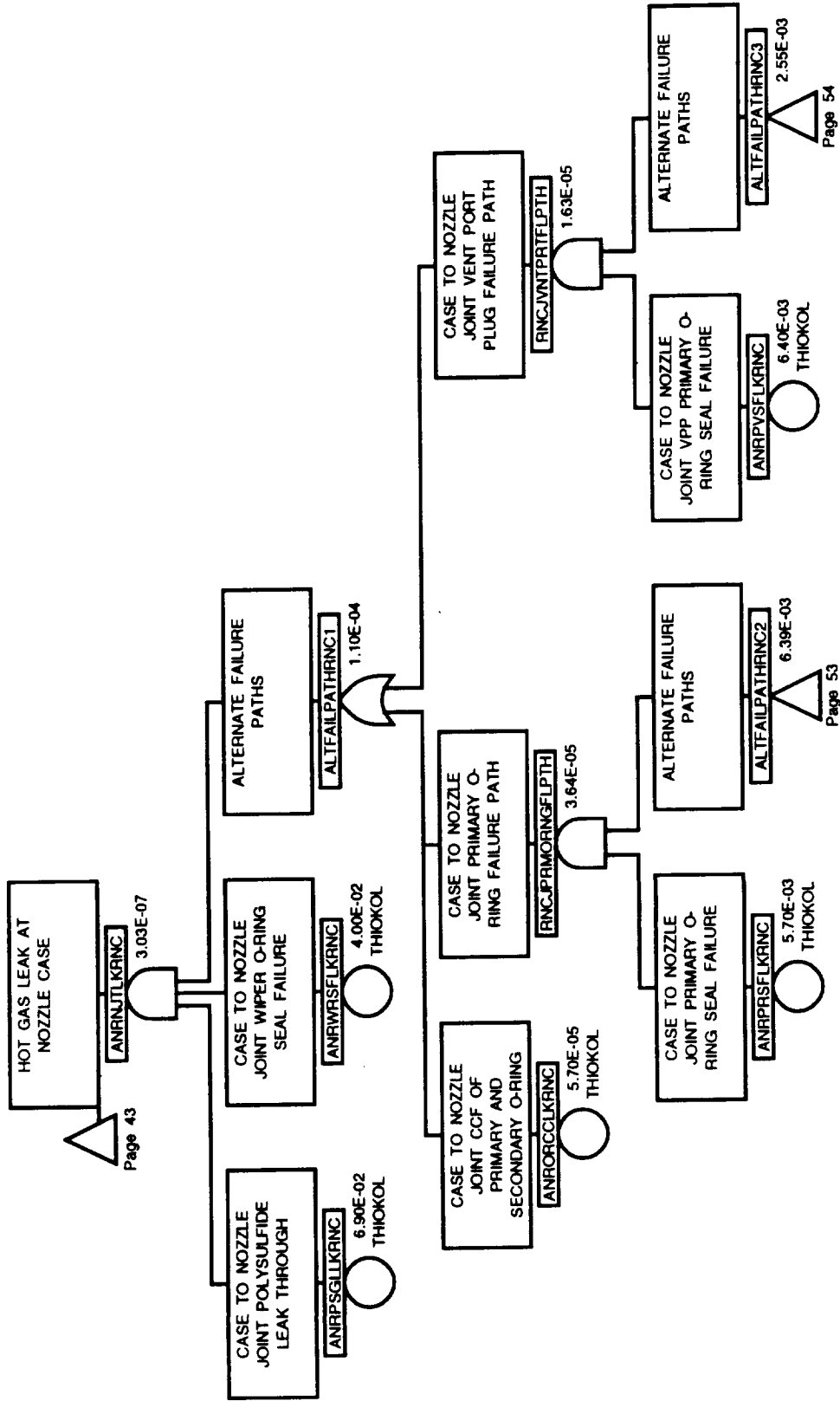


Page 48





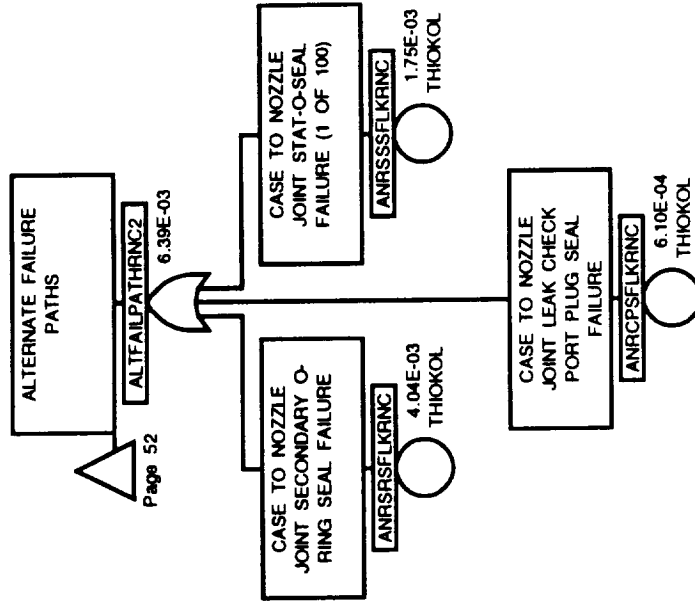
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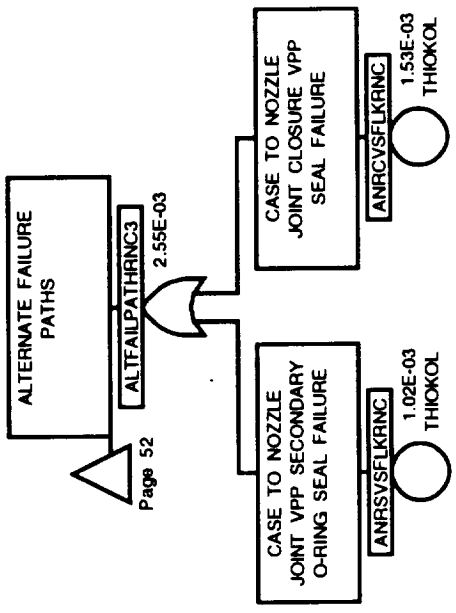
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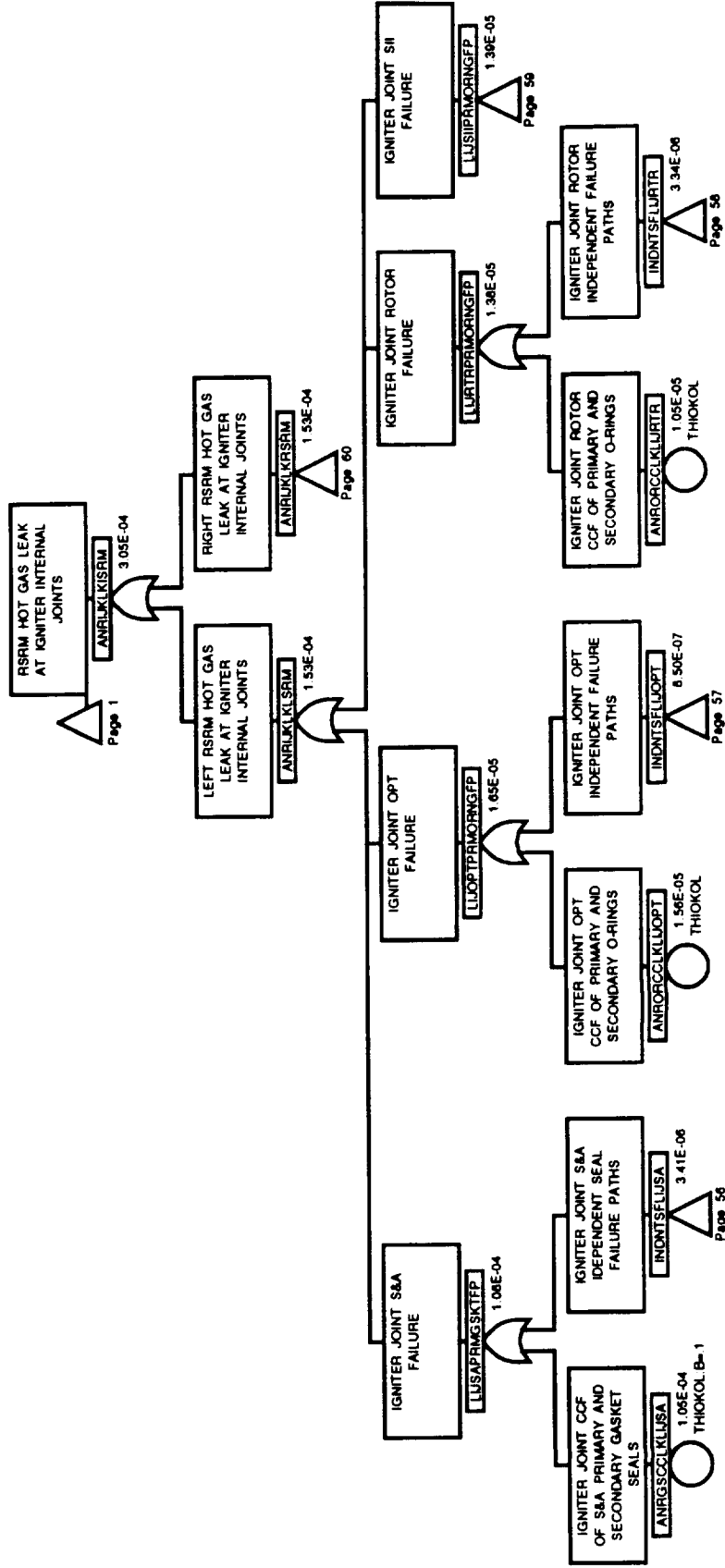
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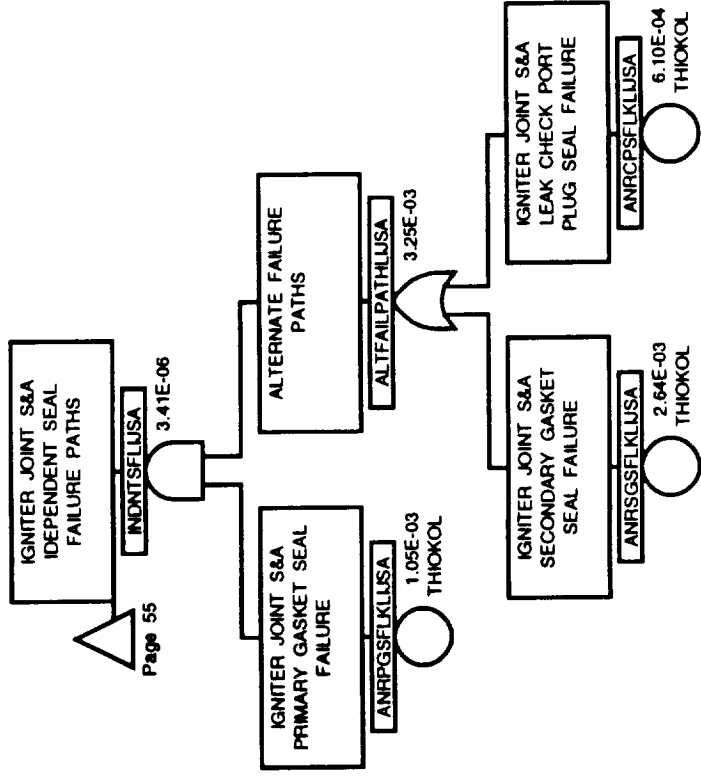


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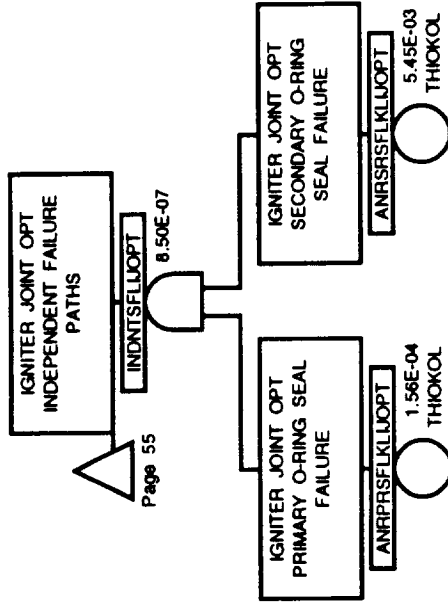


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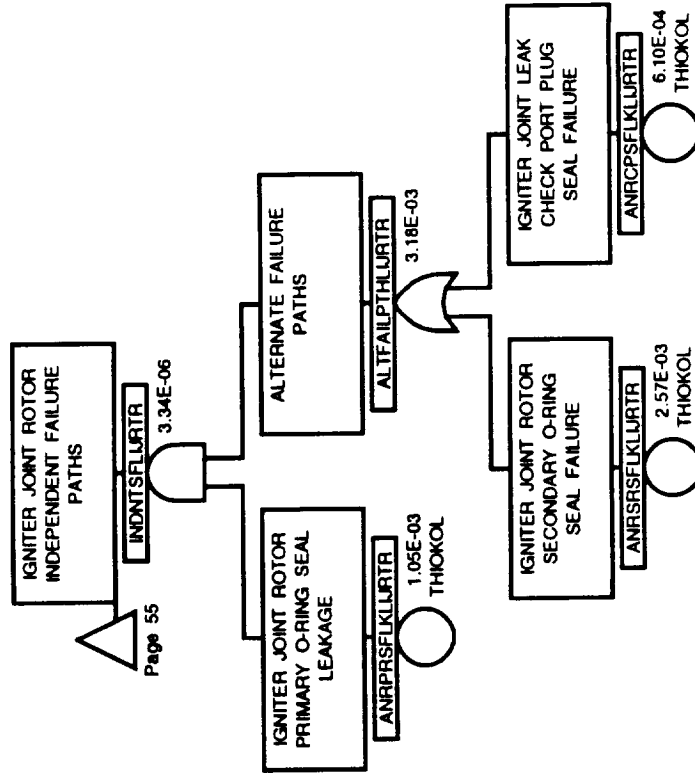




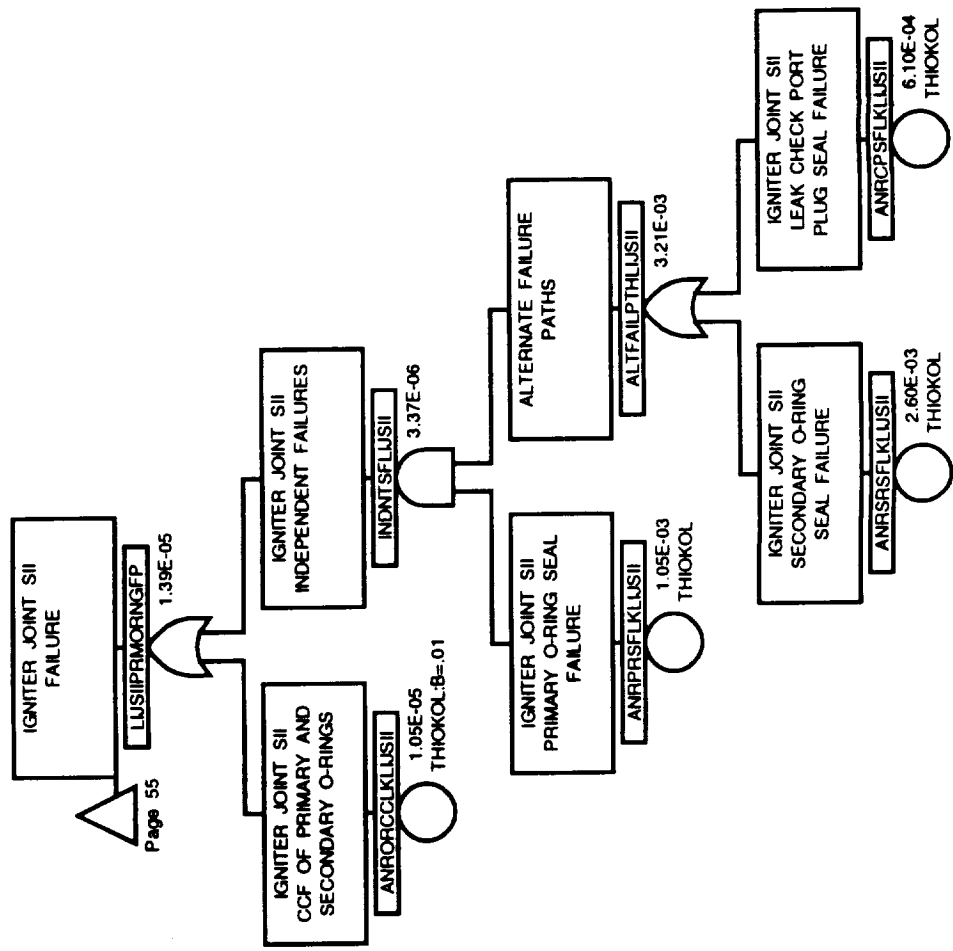
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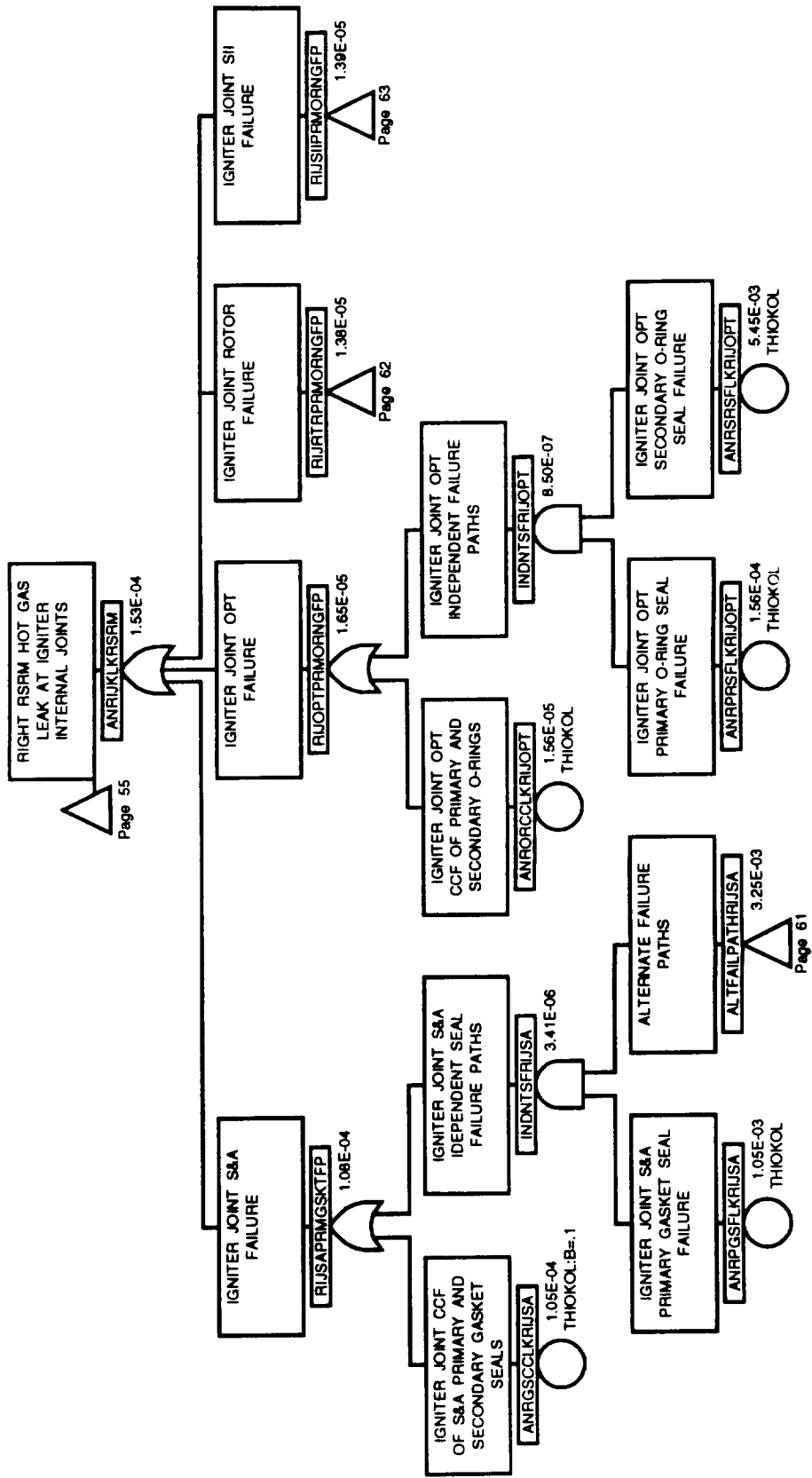
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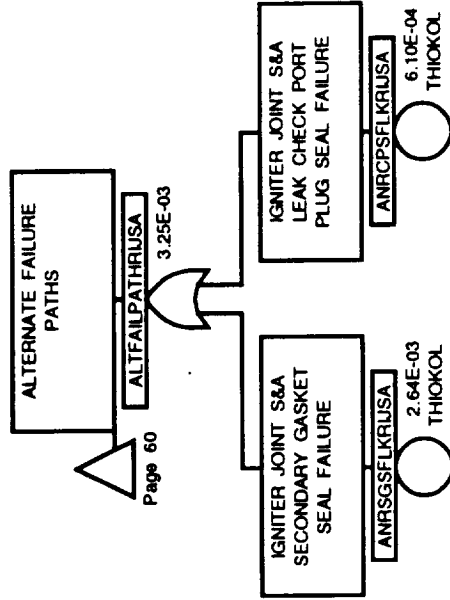


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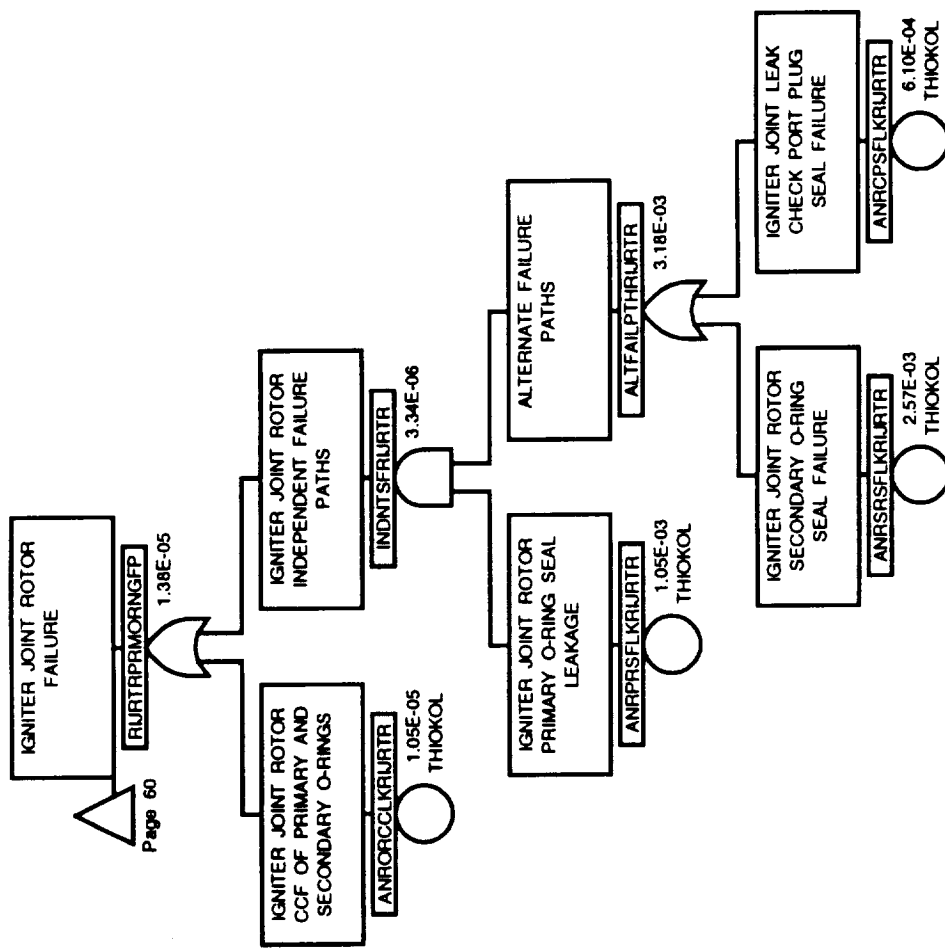


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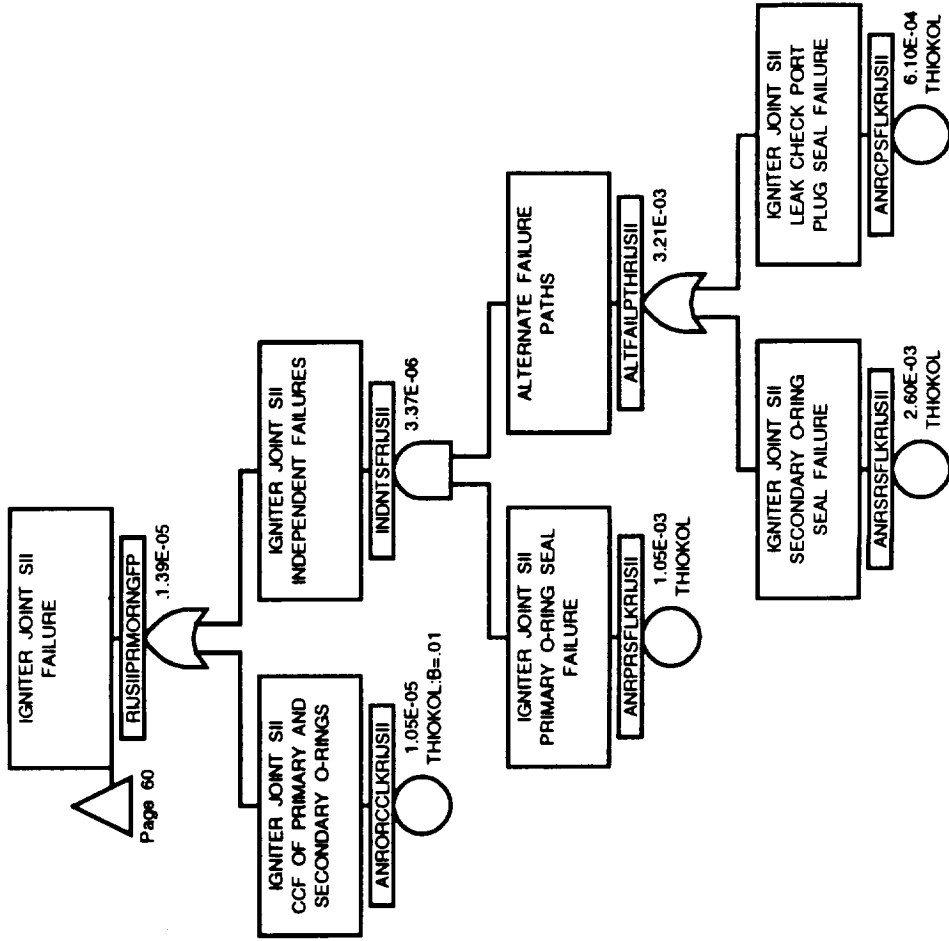




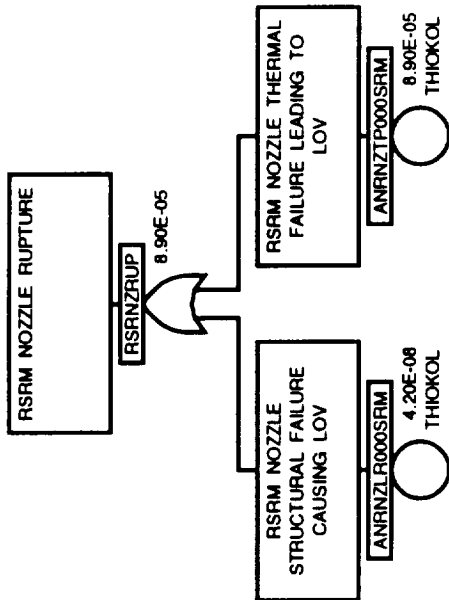
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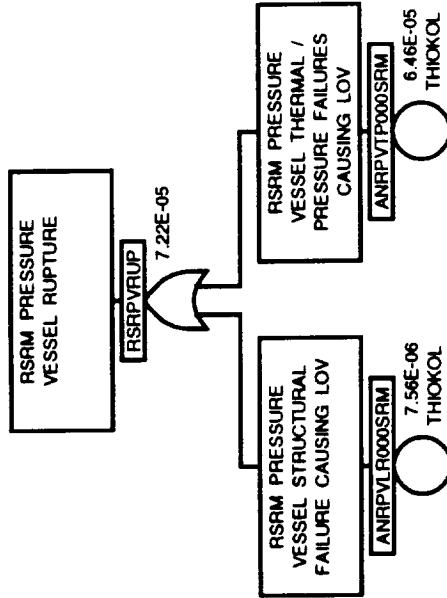


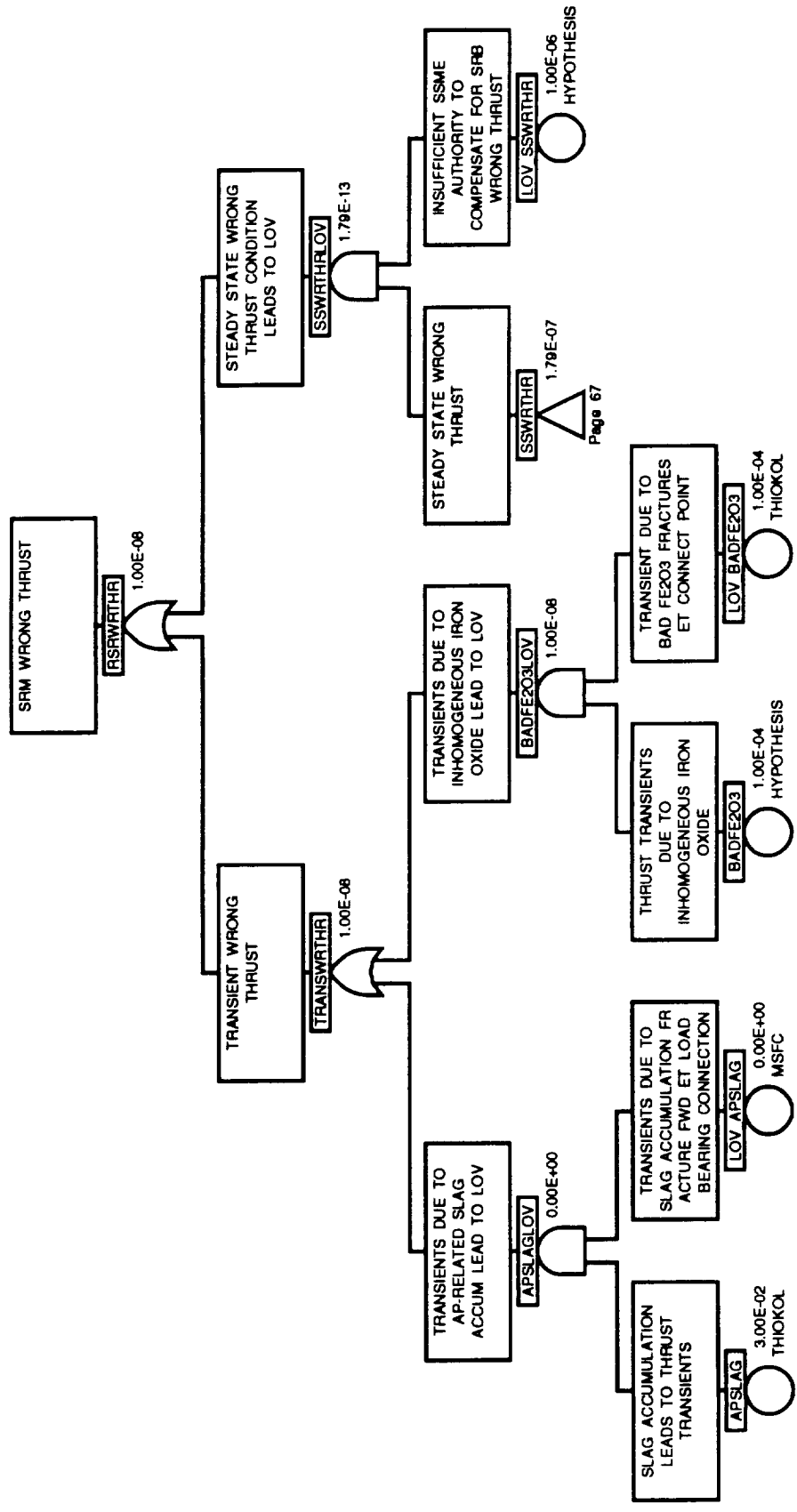
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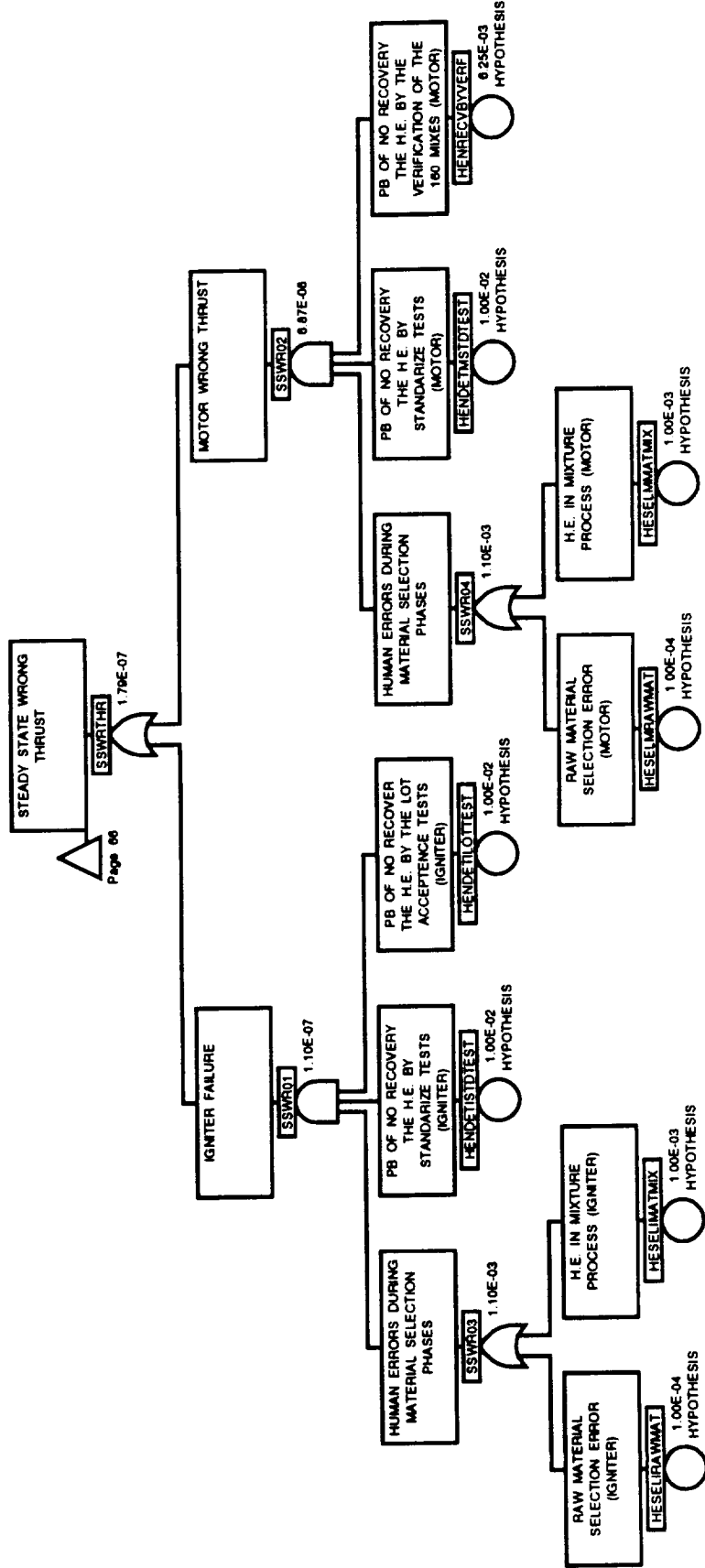
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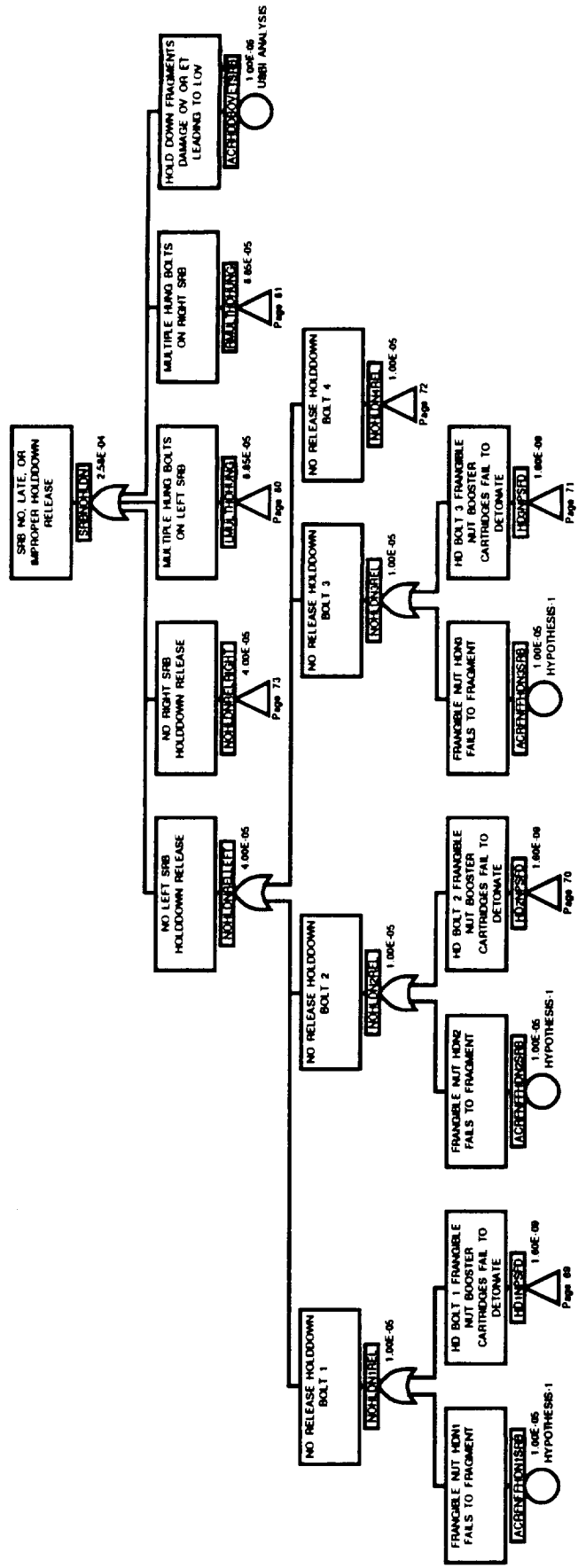


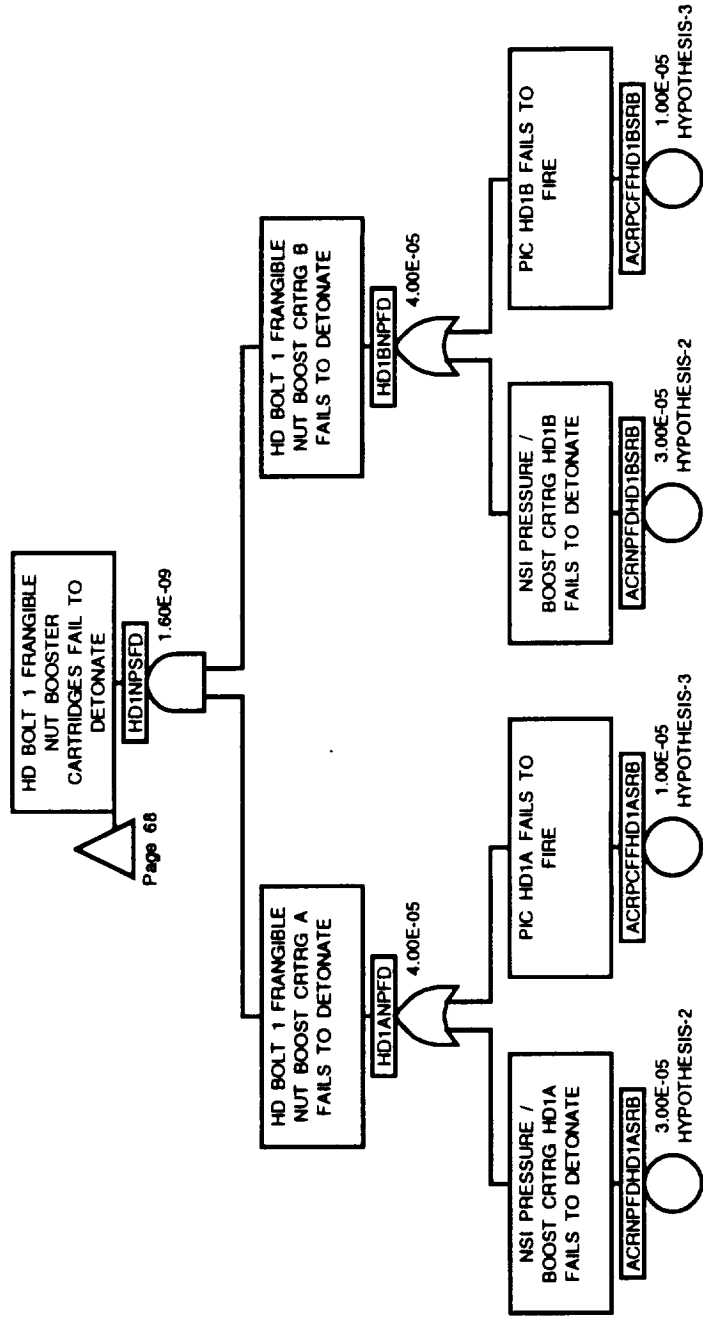


Page 67

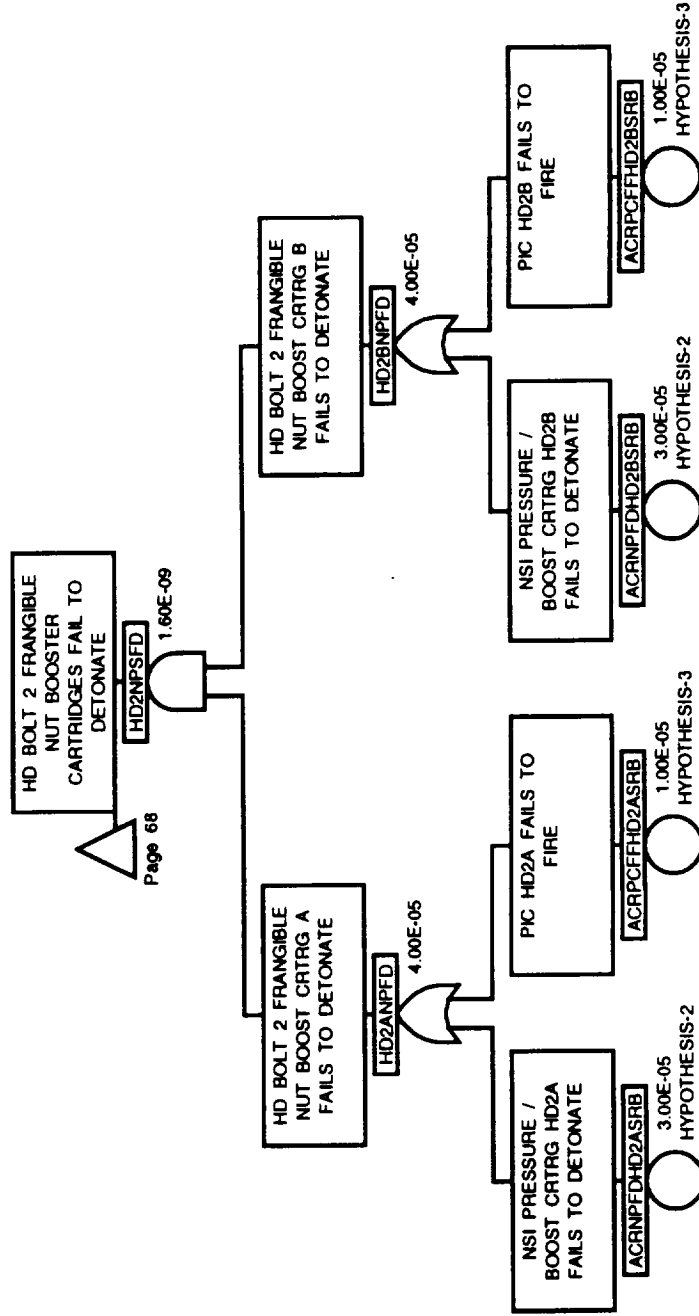


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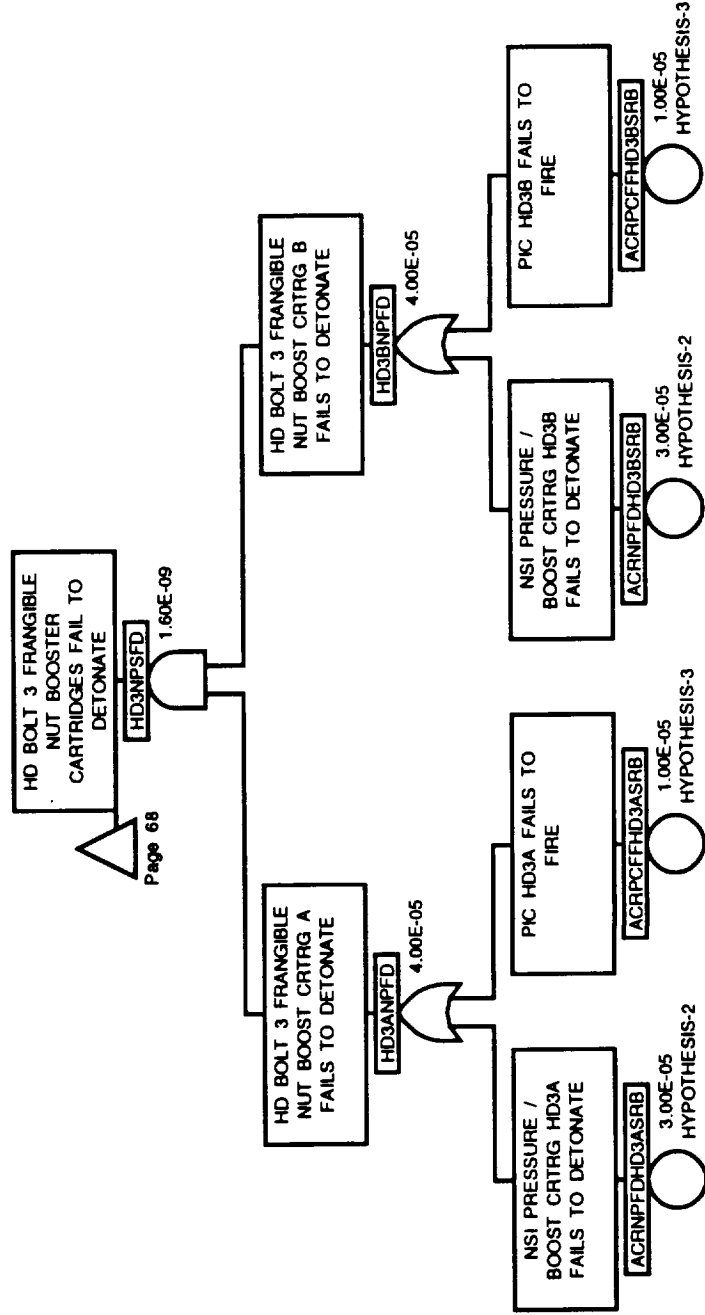




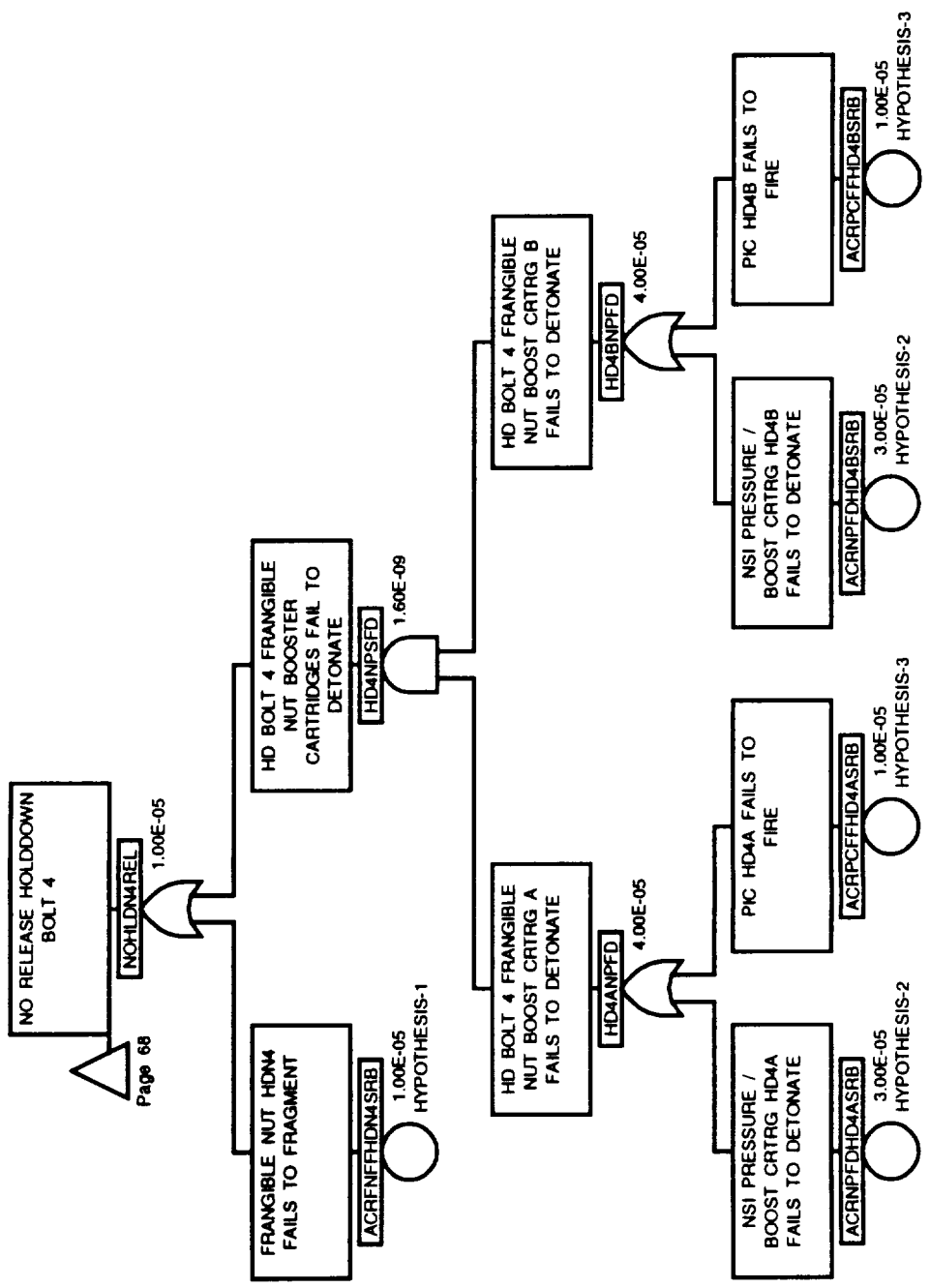
Page 68



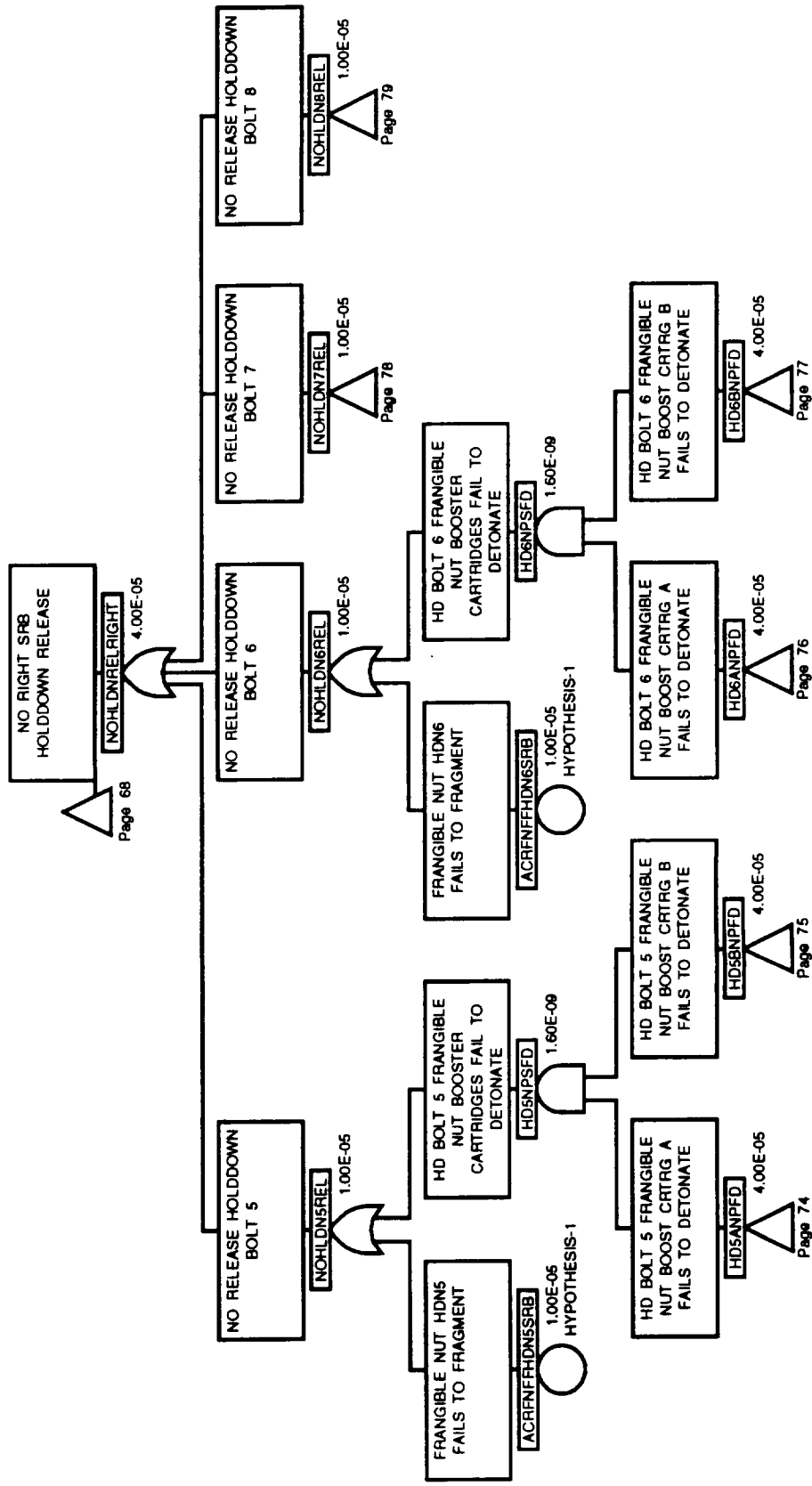
Page 68

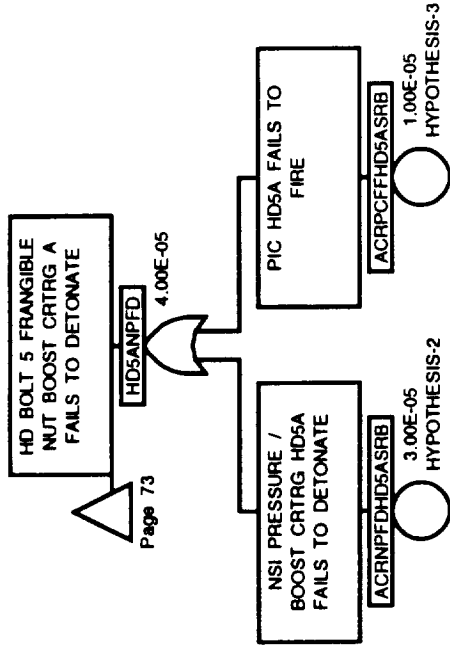


Page 68

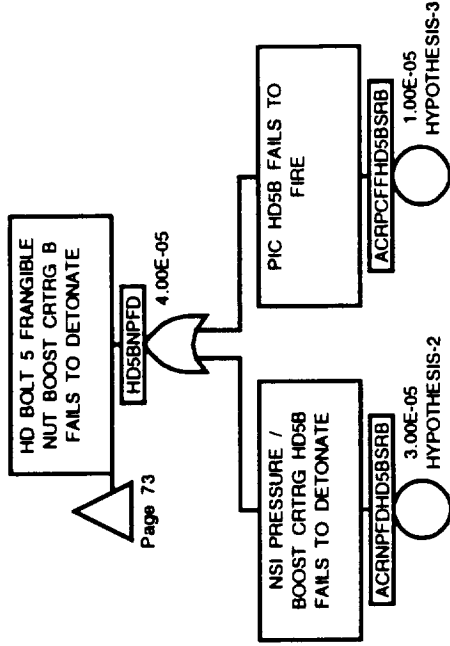


Page 68

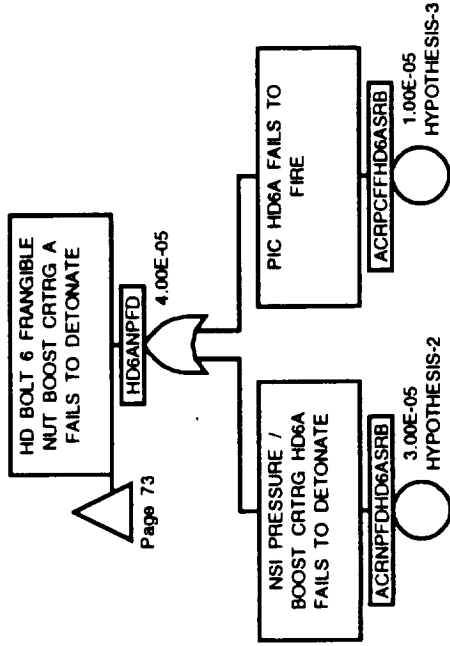




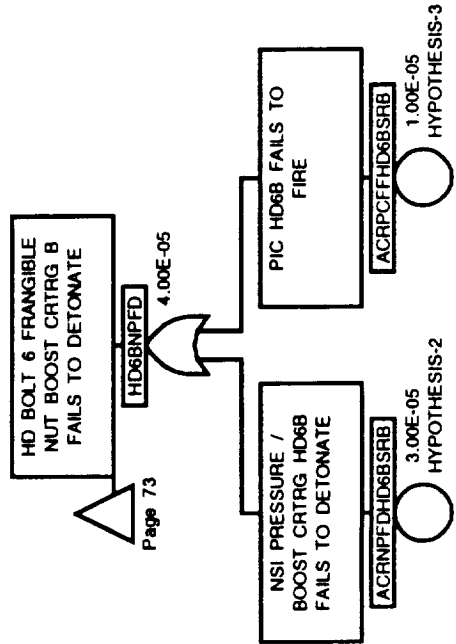
Page 73



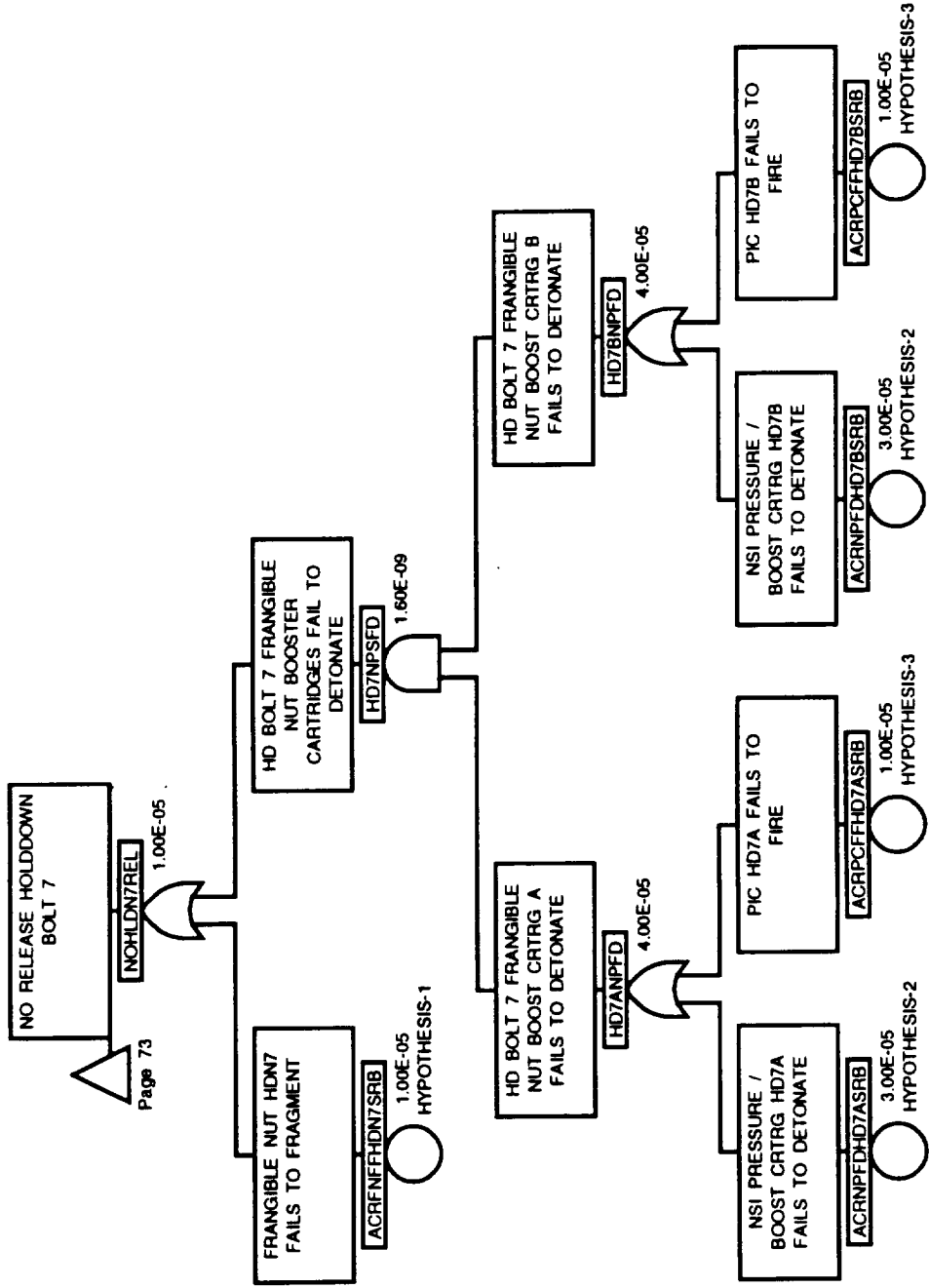
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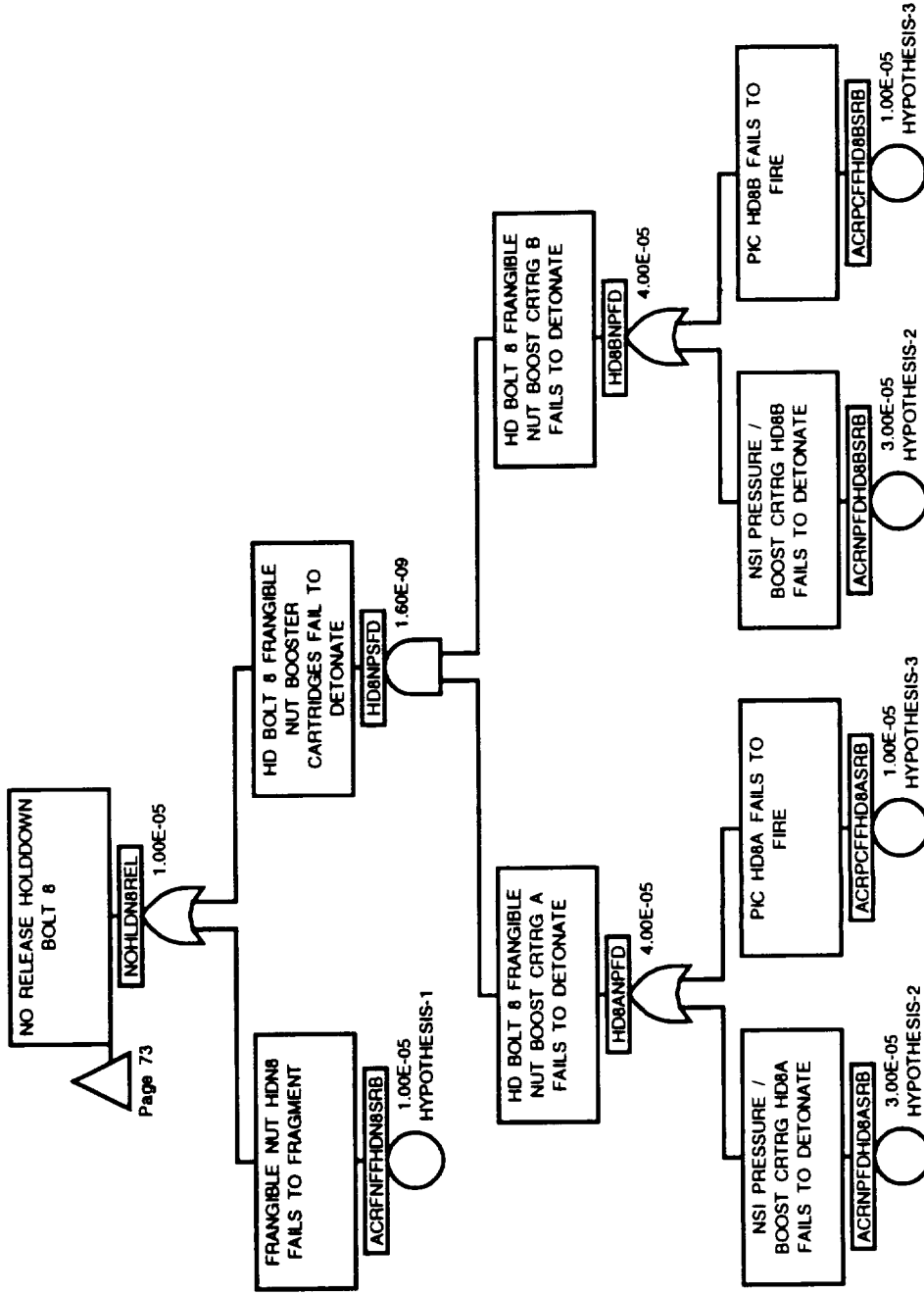
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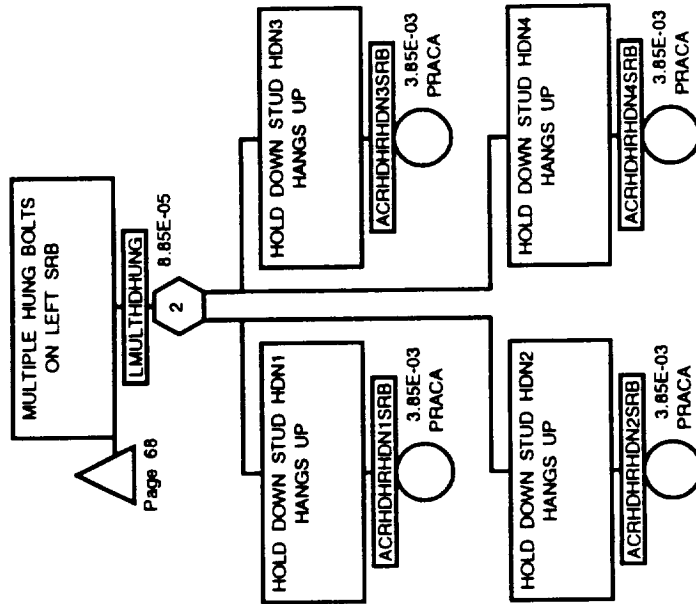
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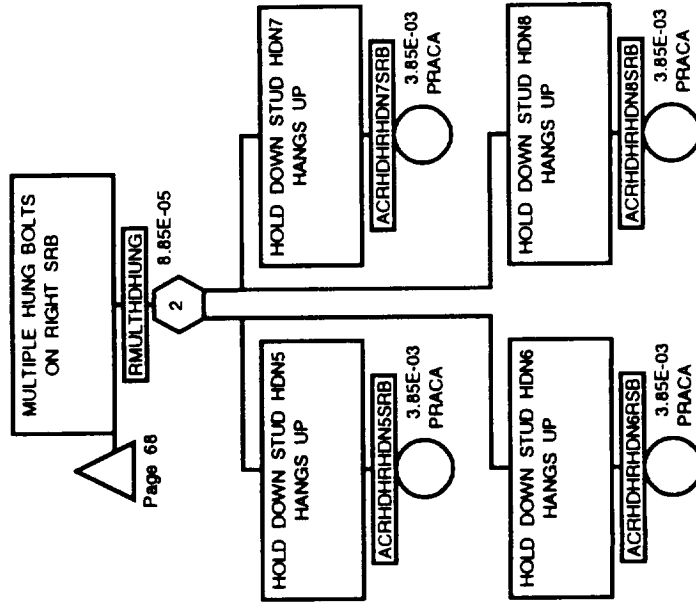
Page 73



Page 73



Page 68



Page 68

8.85E-05

2

MULTIPLE HUNG BOLTS ON RIGHT SRB

RMULTIHUNG

HOLD DOWN STUD HDN5 HANGS UP

ACRHDHHDN5SRB

3.85E-03 PRACA

HOLD DOWN STUD HDN6 HANGS UP

ACRHDHHDN6SRB

3.85E-03 PRACA

HOLD DOWN STUD HDN7 HANGS UP

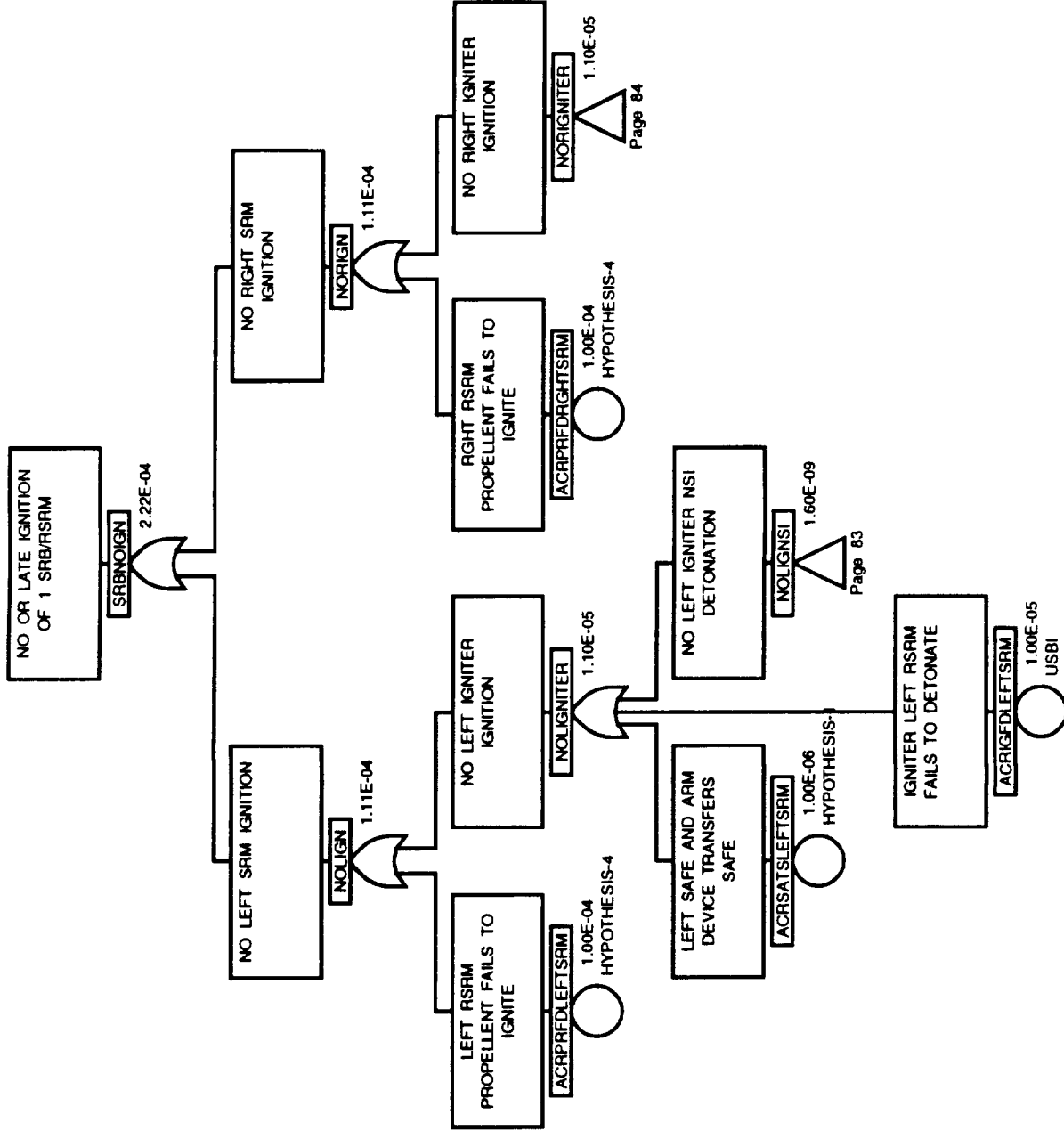
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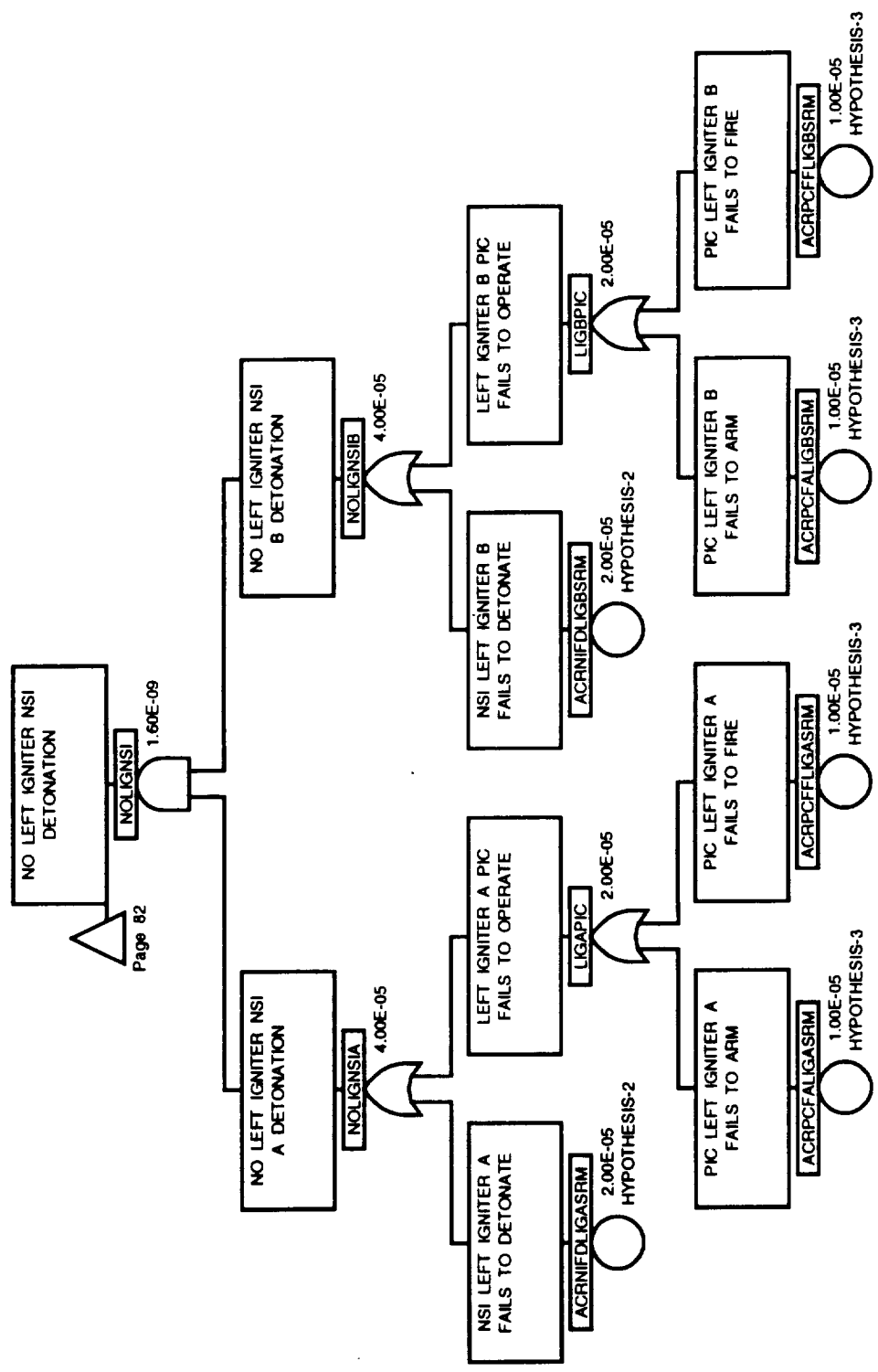
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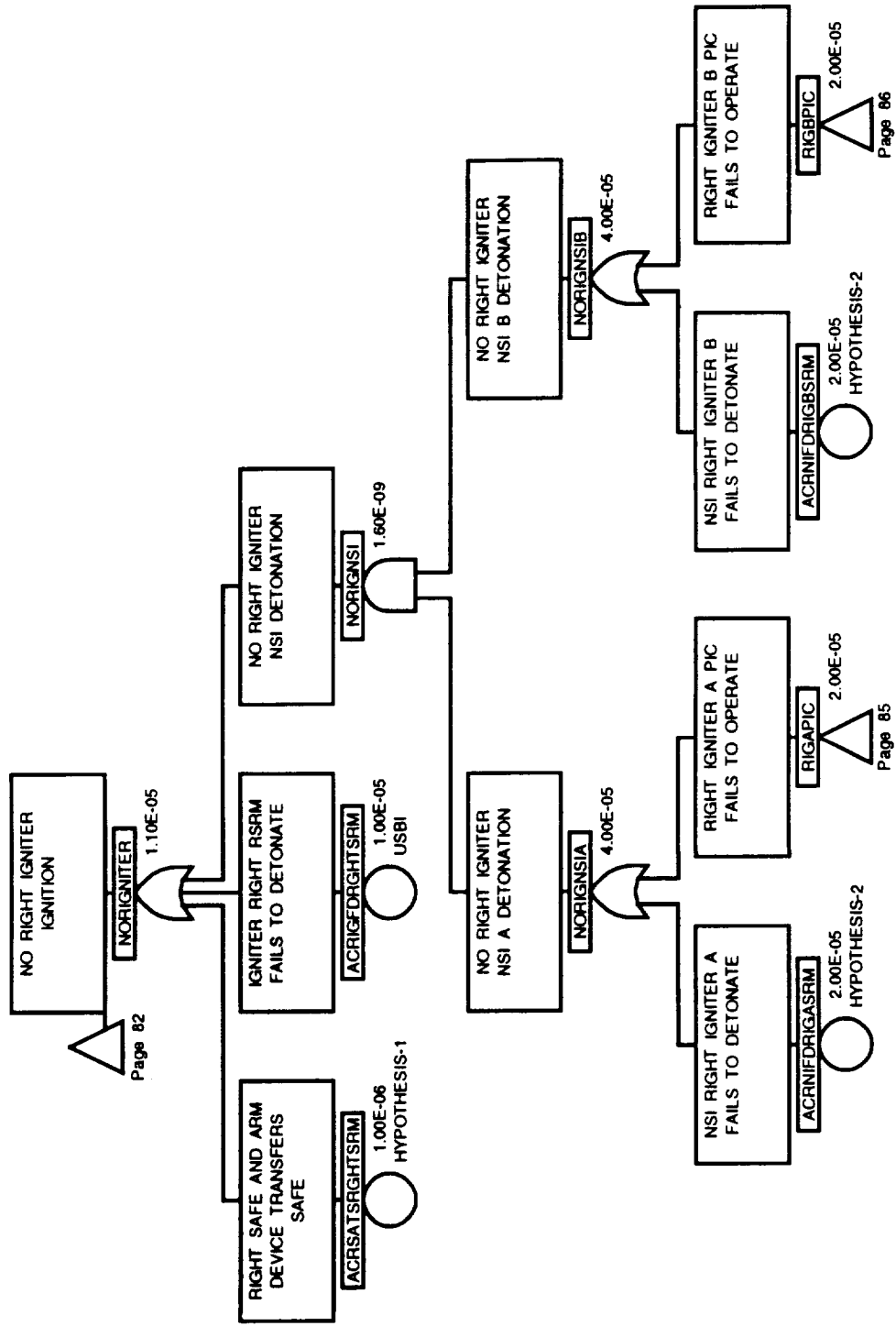
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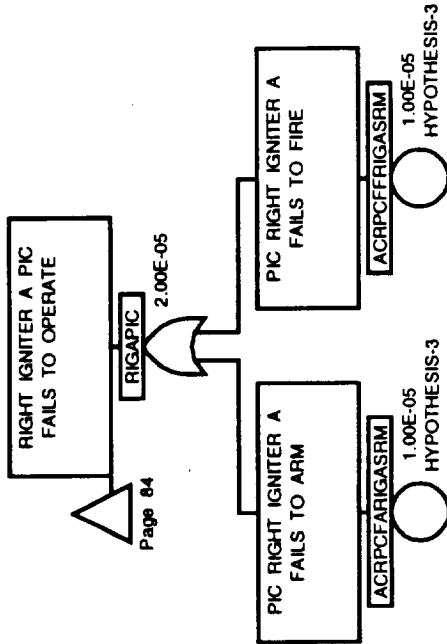
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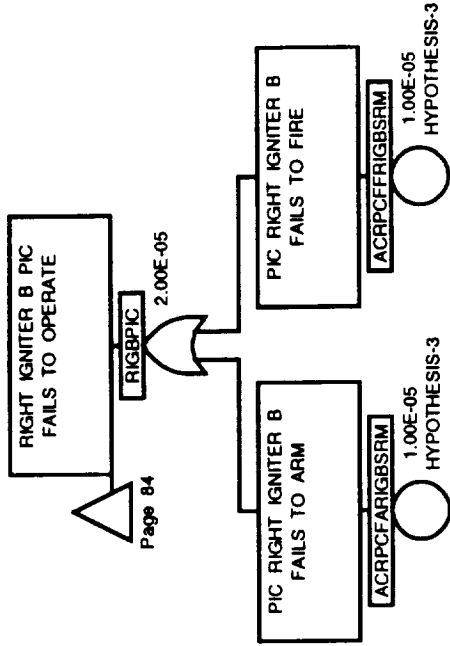
Page 82

Page 85

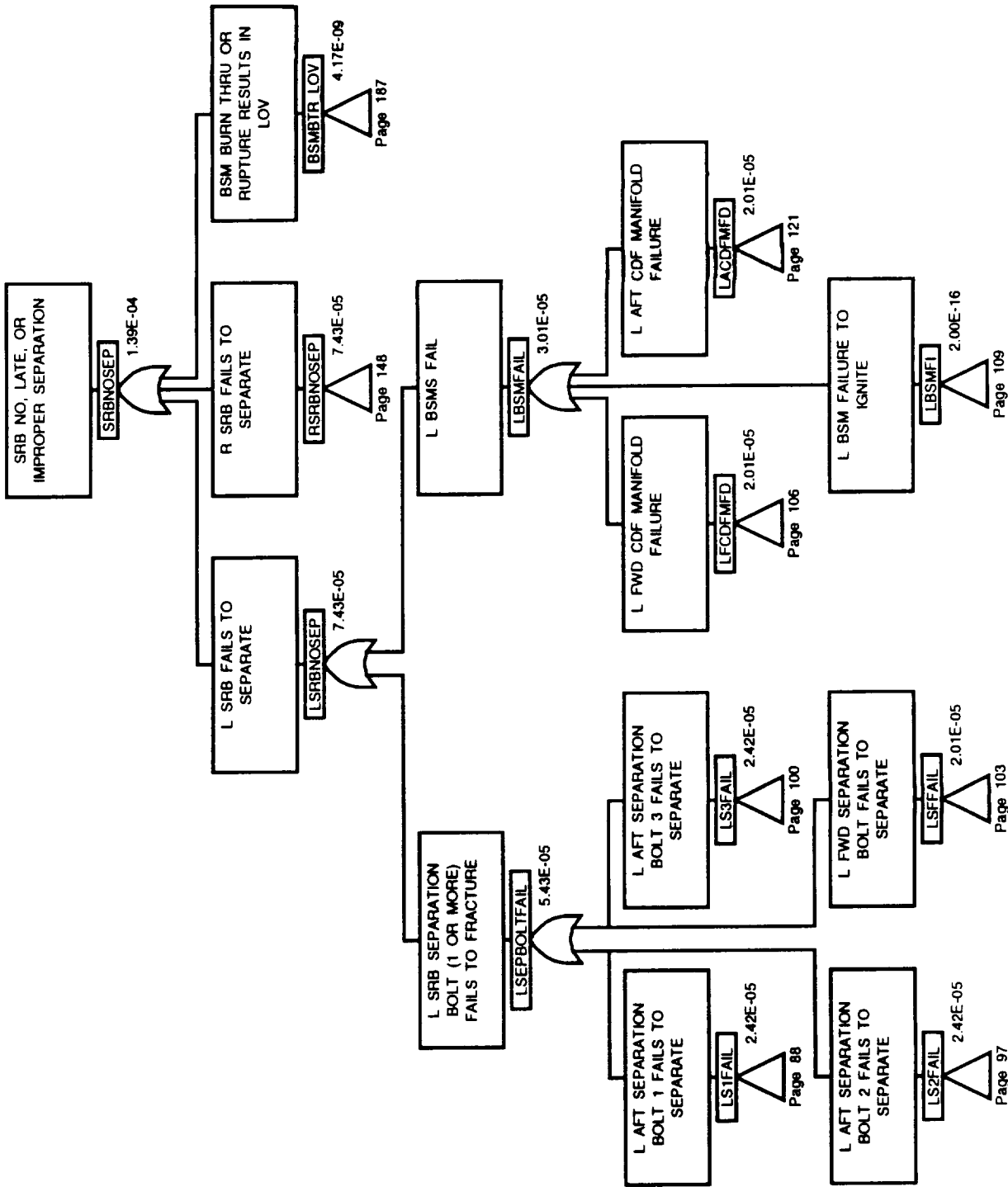
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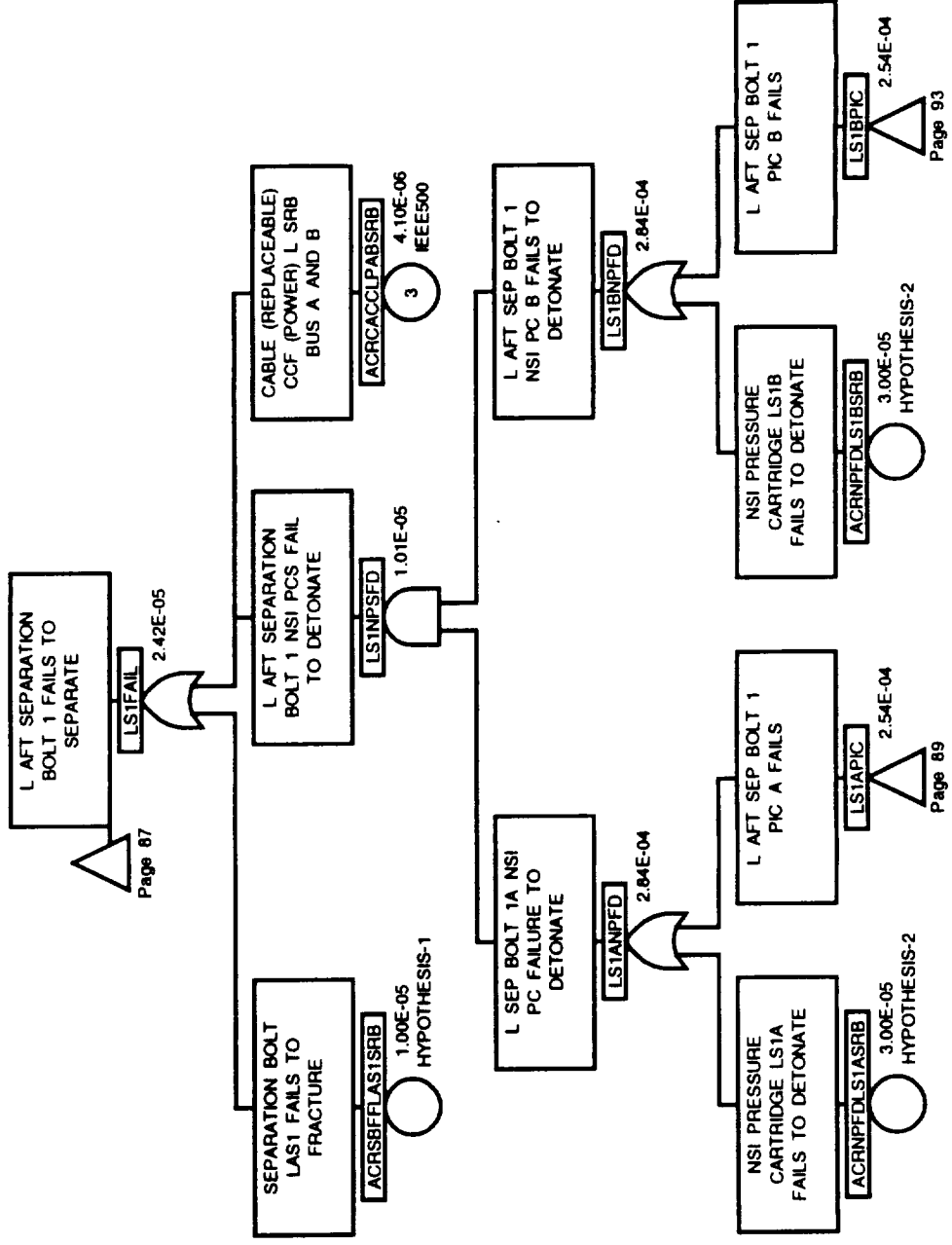


Page 84



Page 84

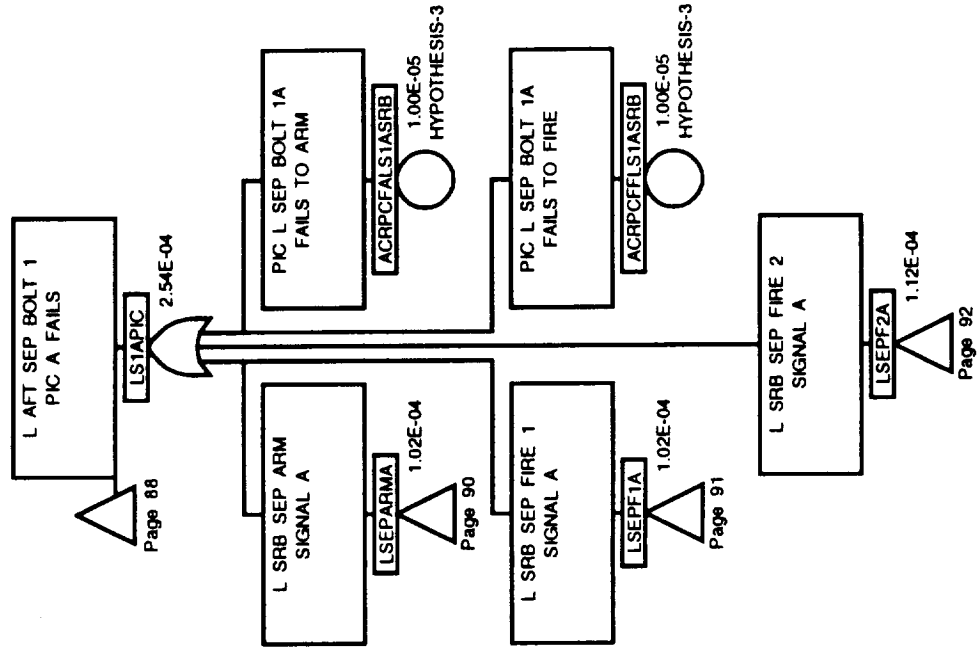


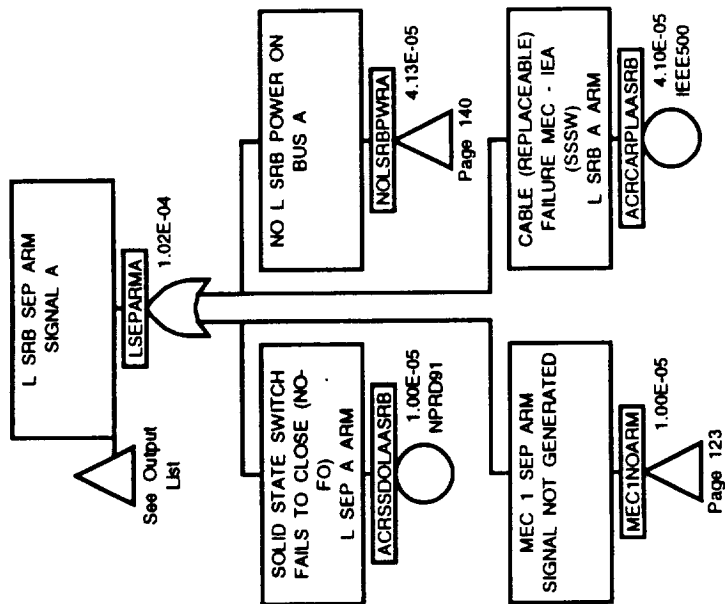


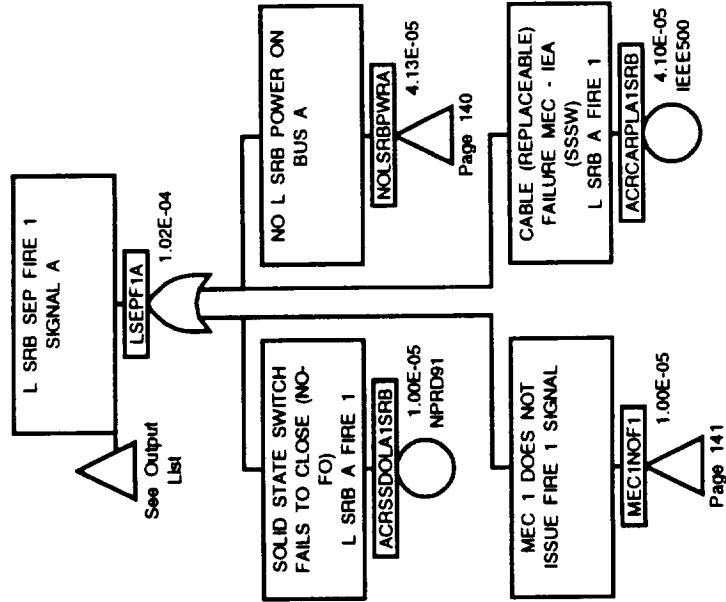
Page 87

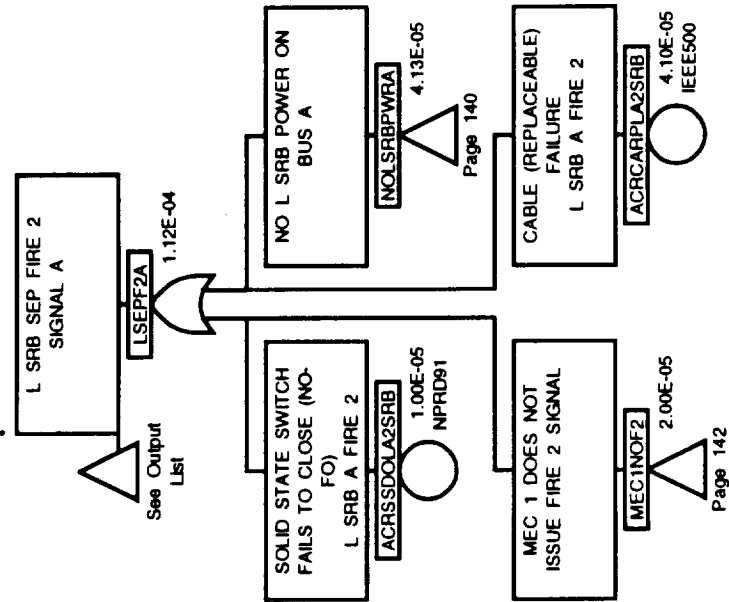
Page 89

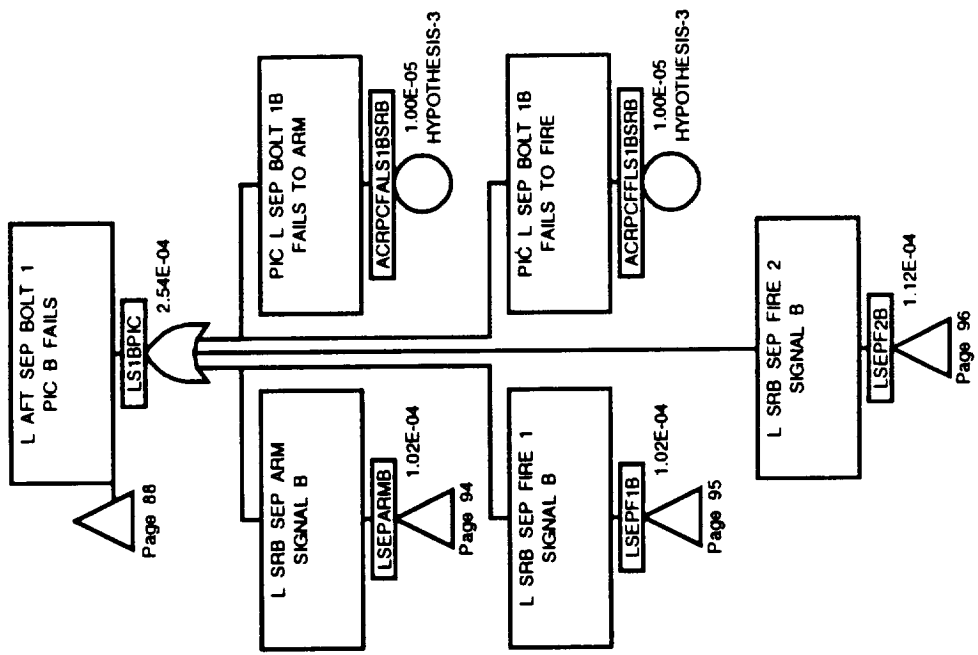
Page 93

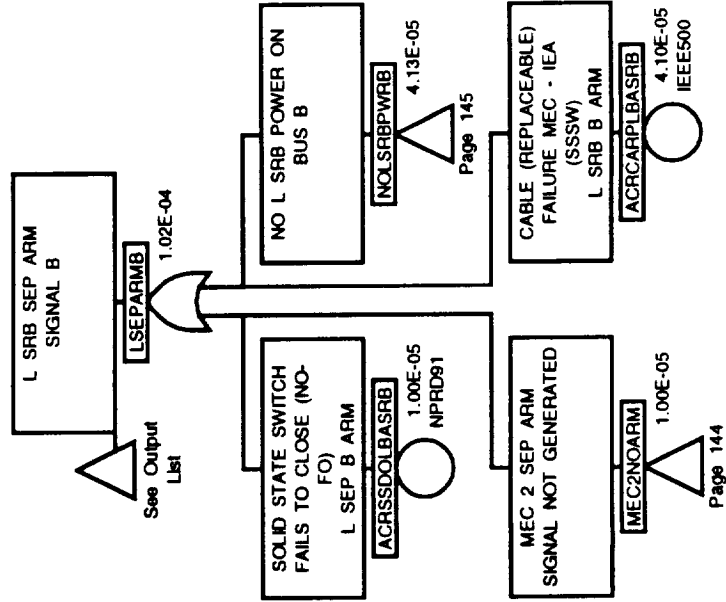


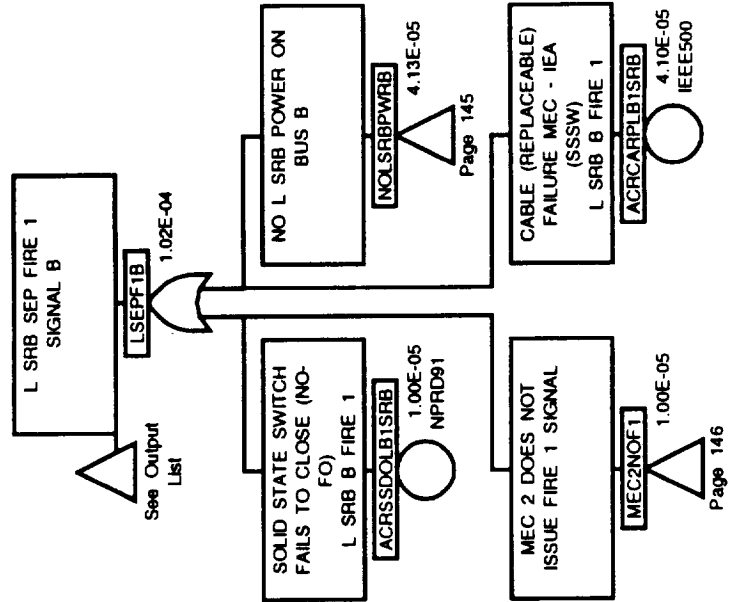


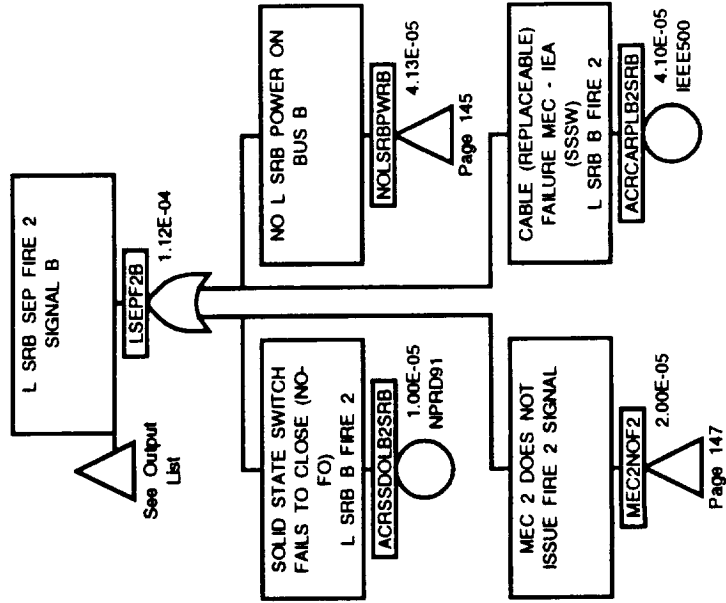


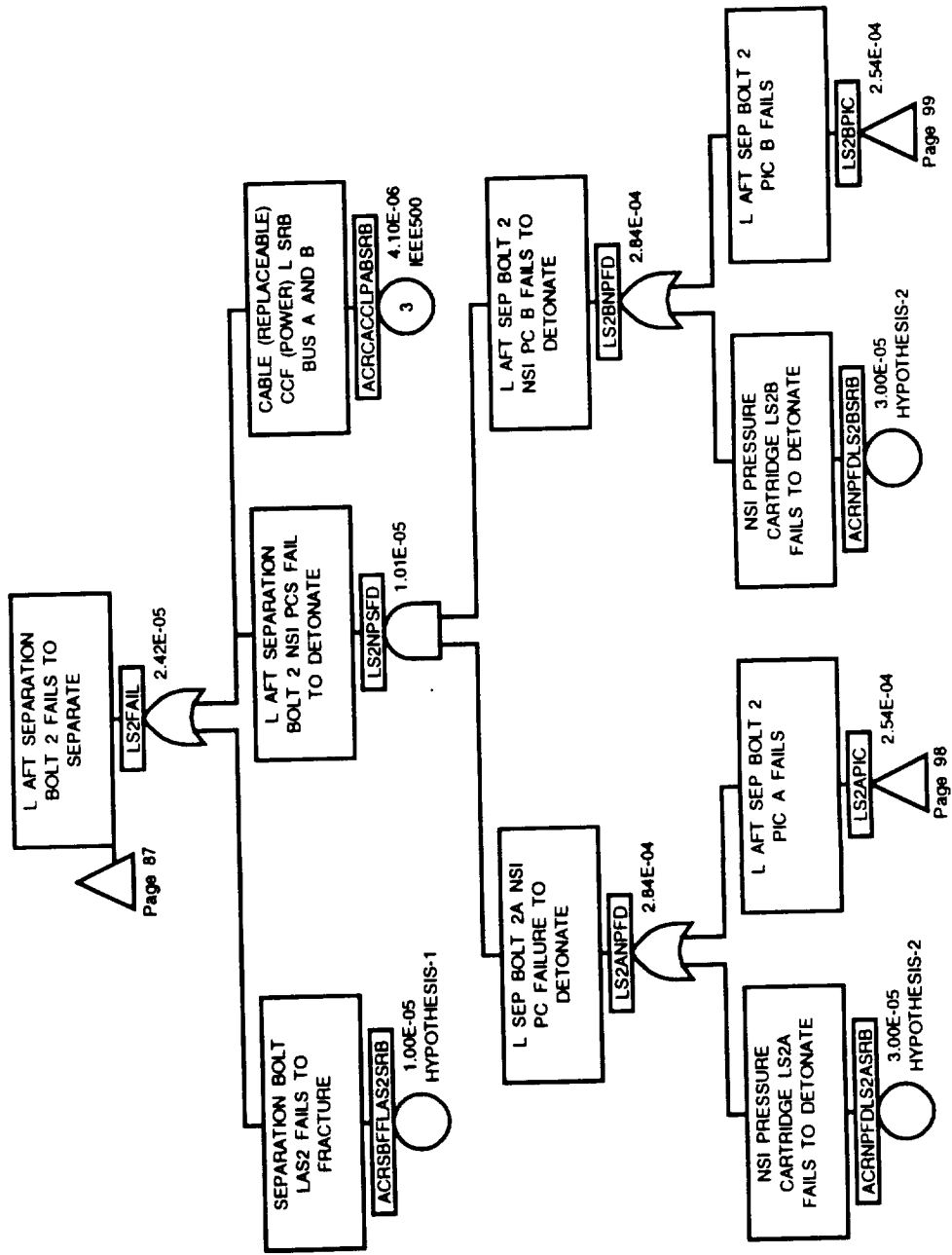








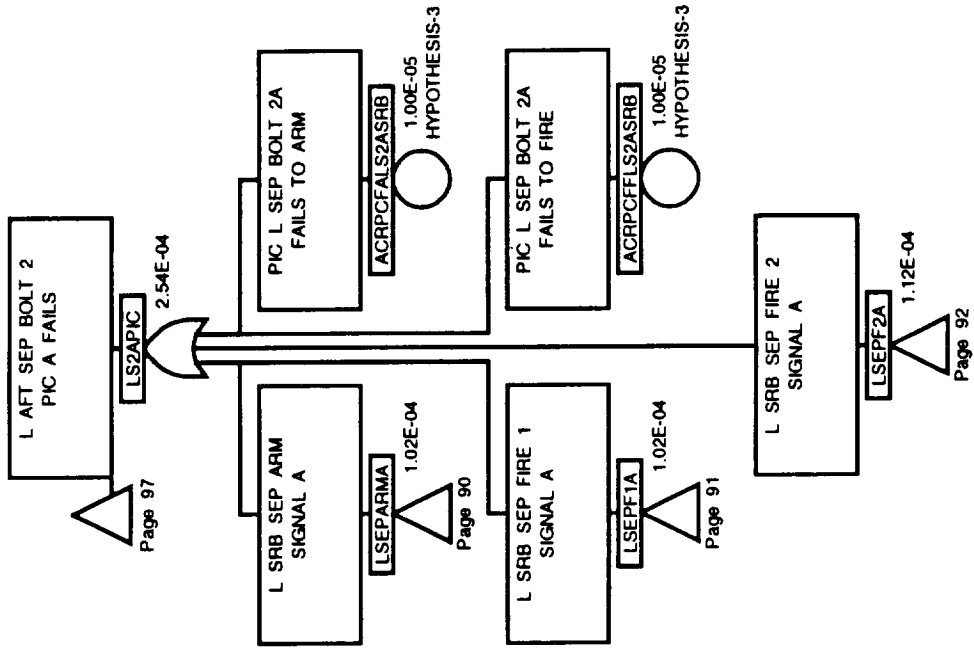


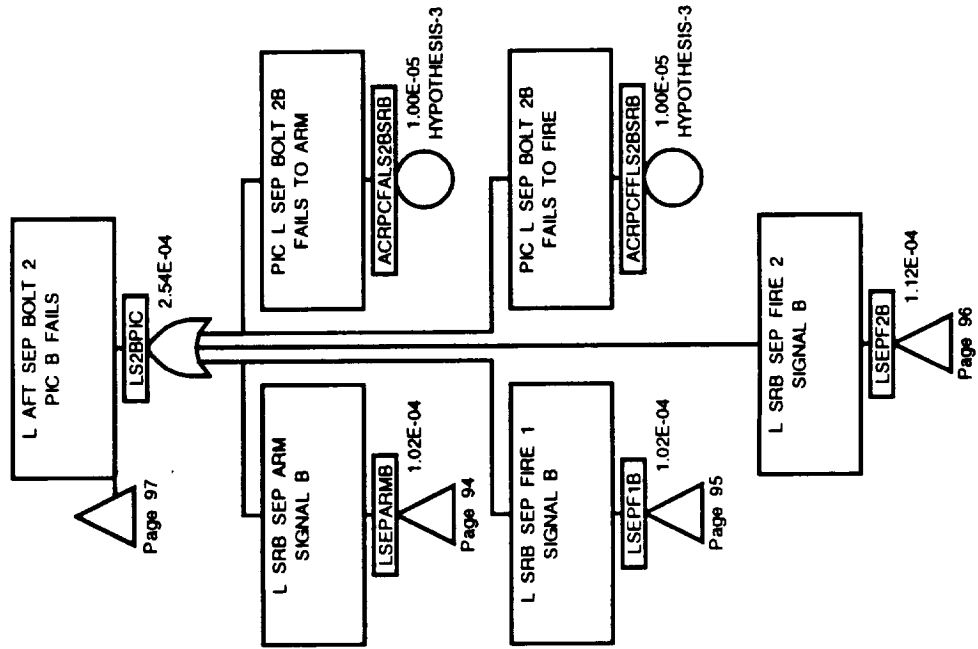


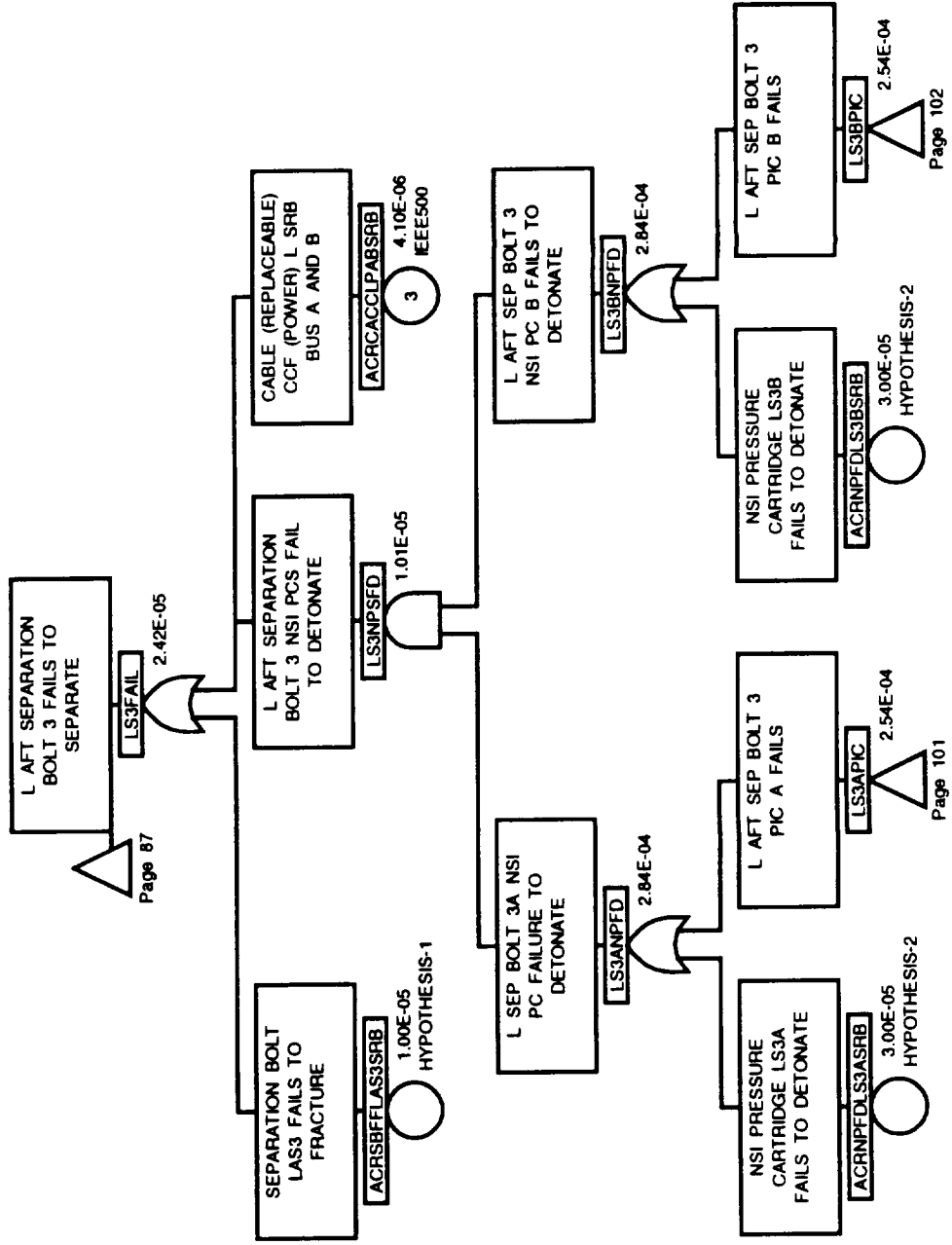
Page 87

Page 99

Page 98



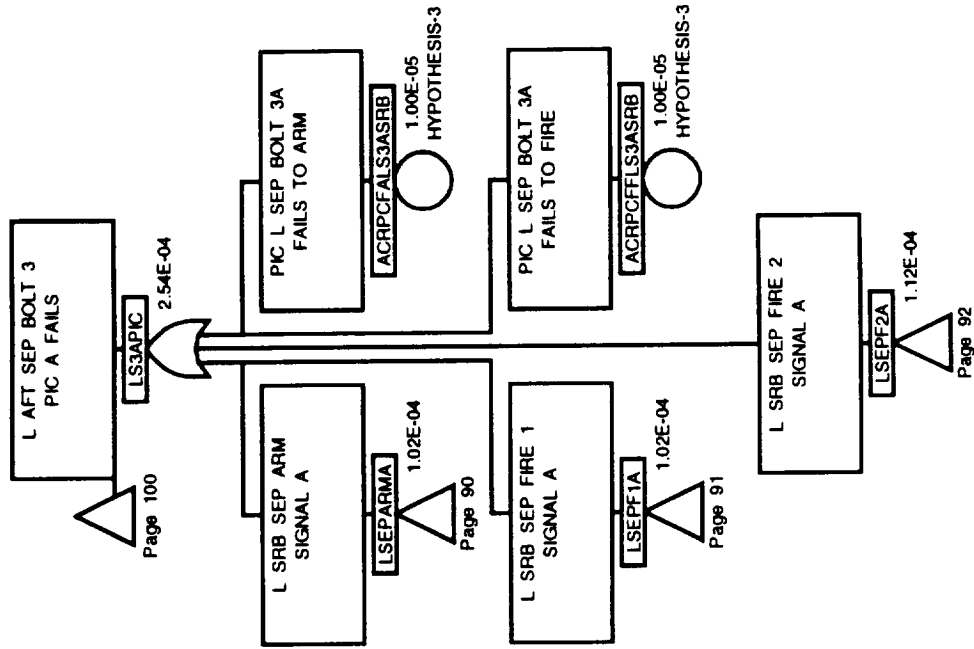


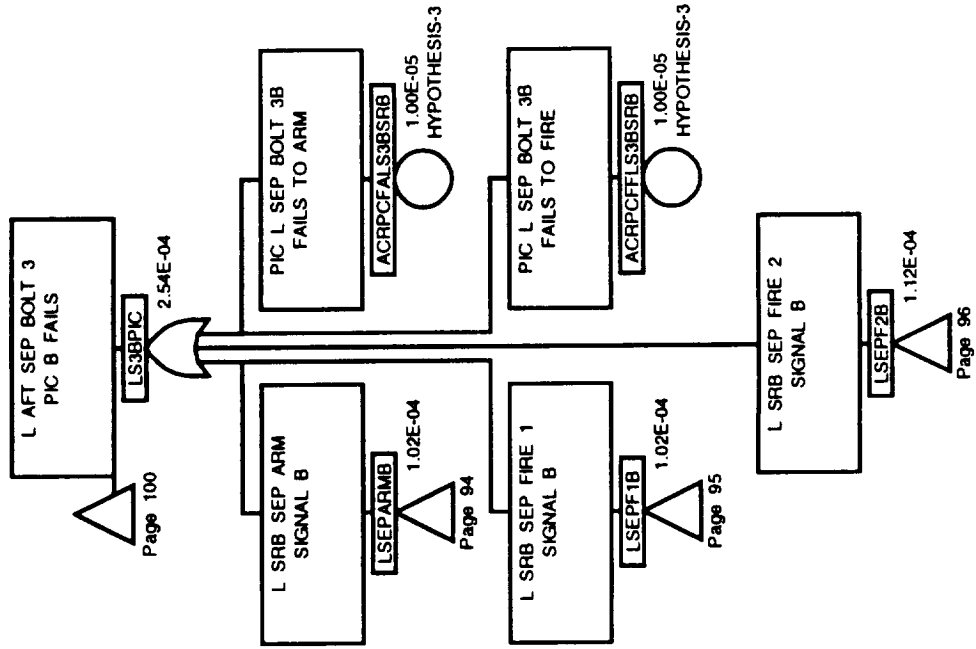


Page 87

Page 101

Page 102



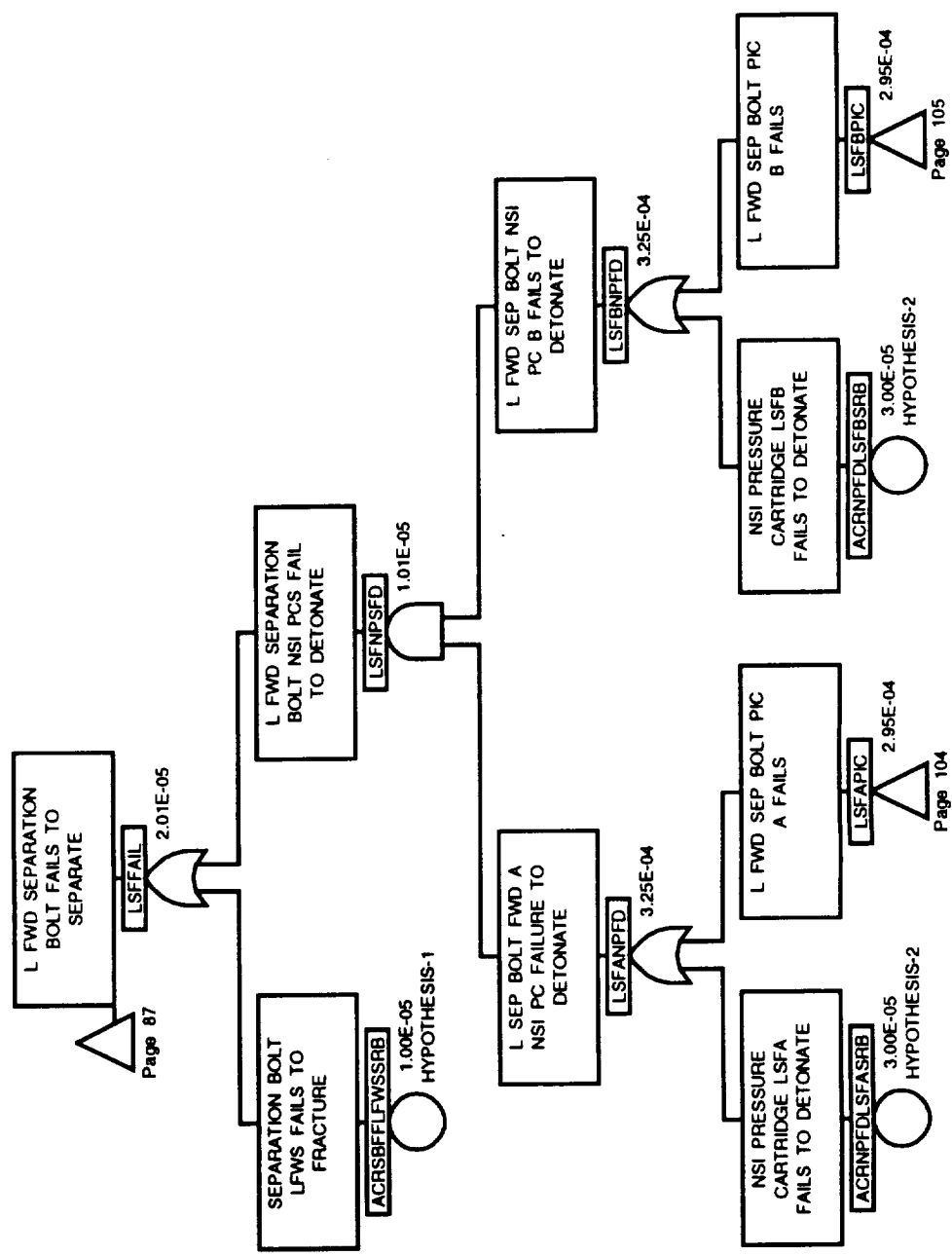


Page 100

Page 94

Page 95

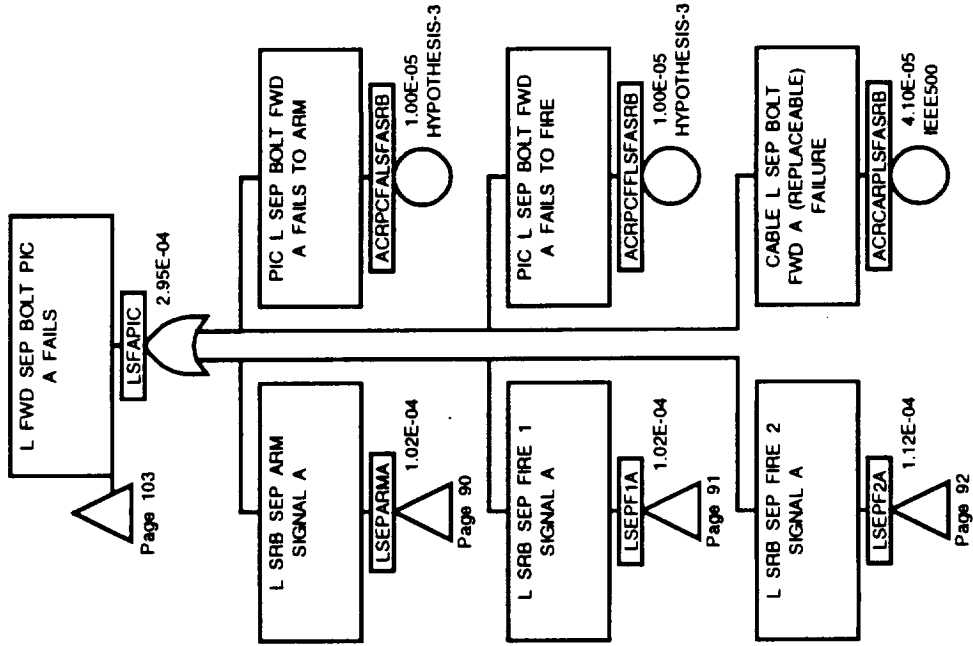
Page 96

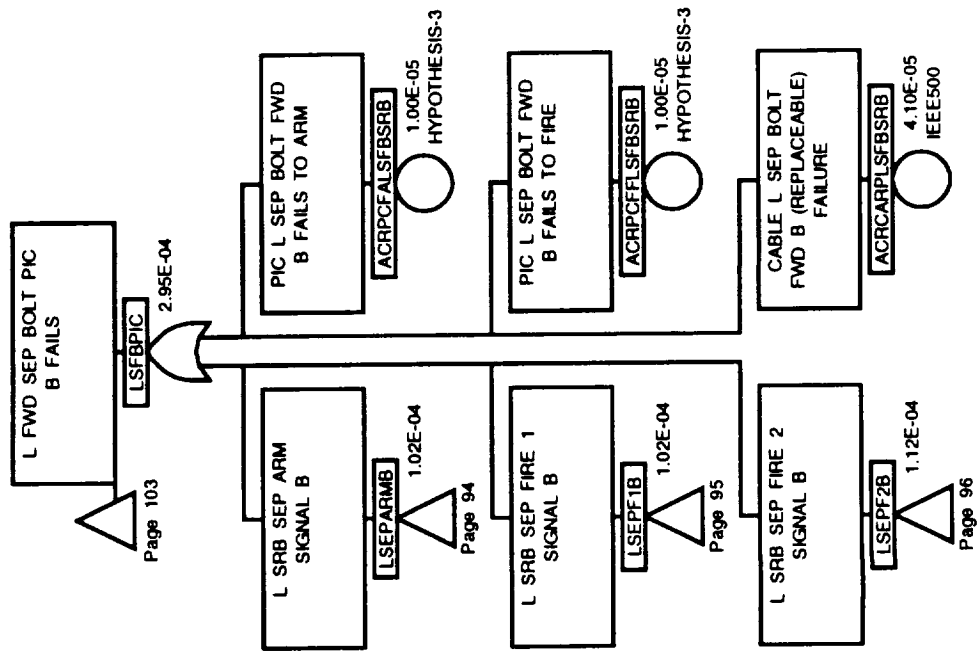


Page 87

Page 104

Page 105



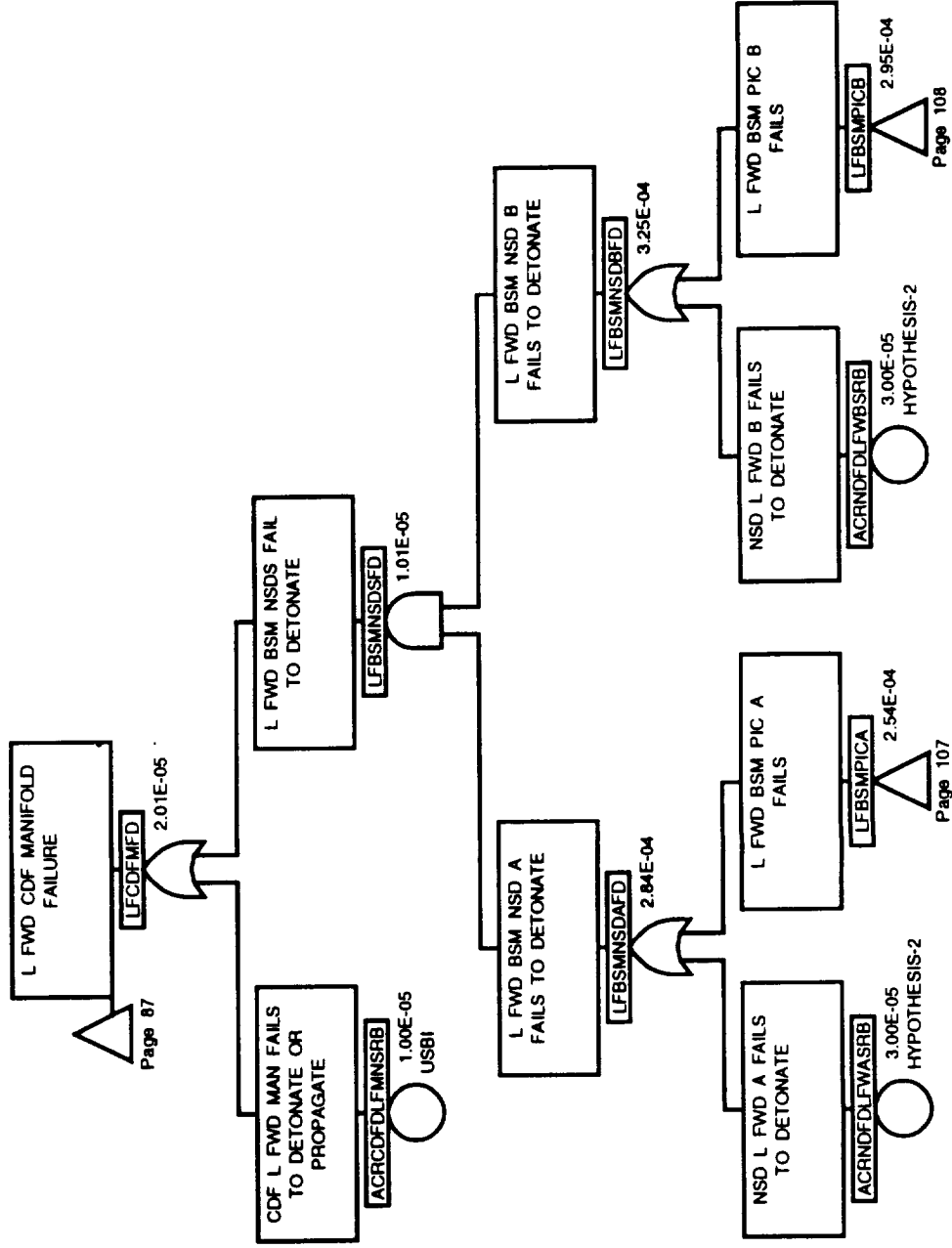


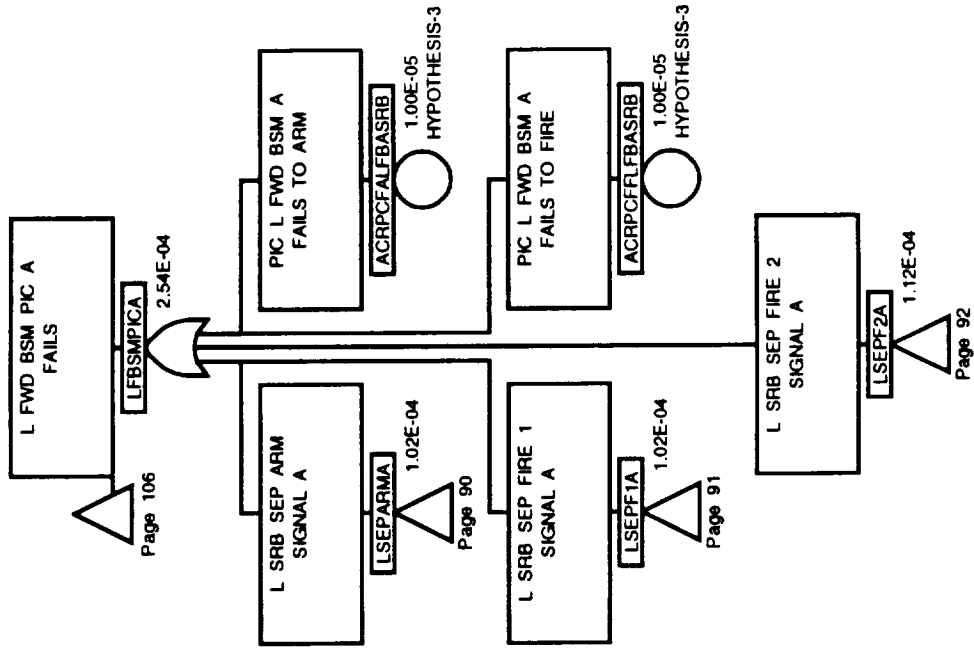
Page 103

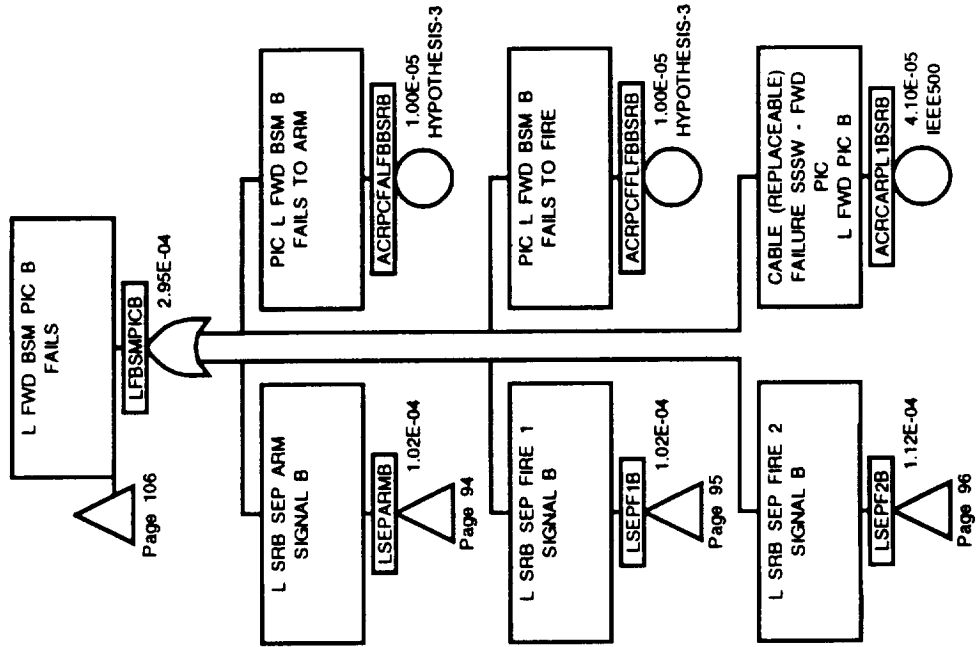
Page 94

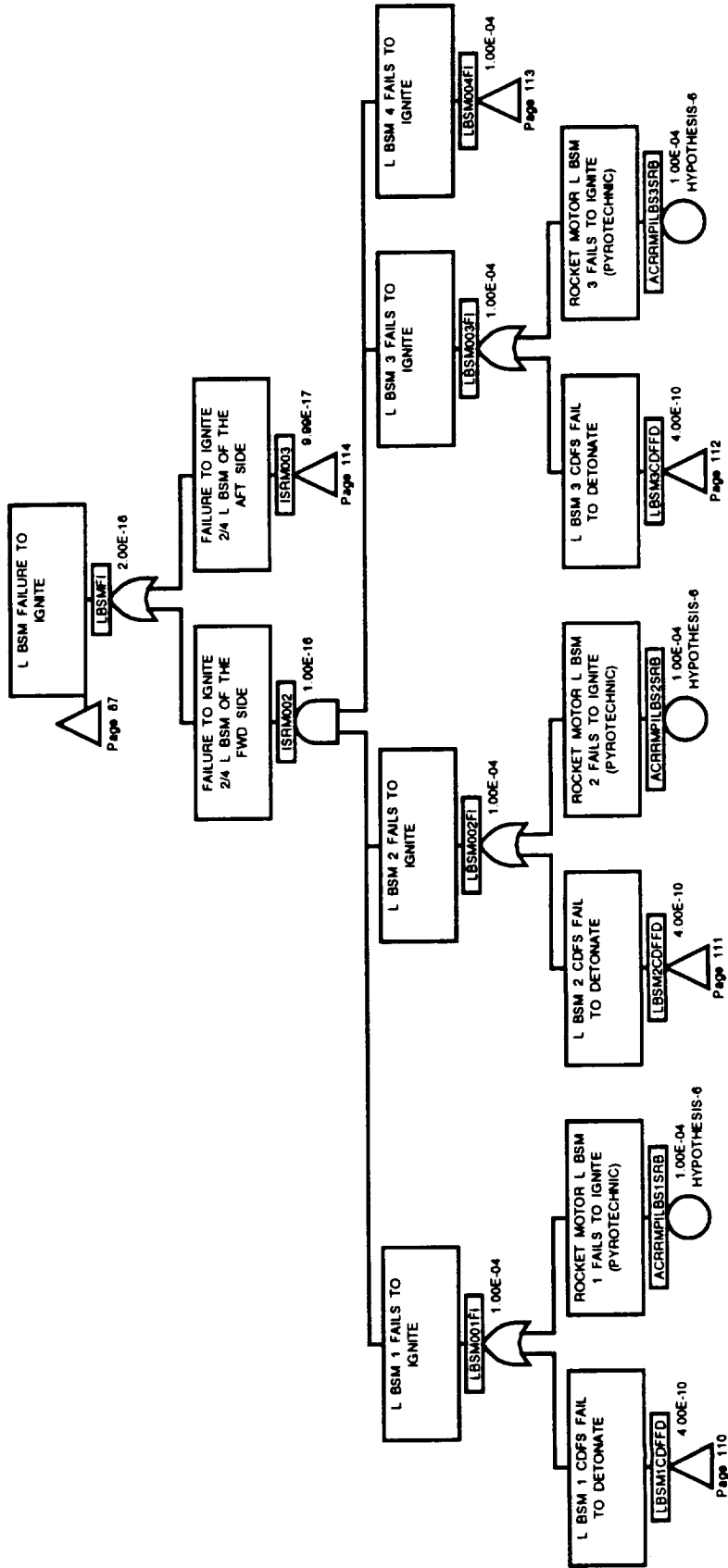
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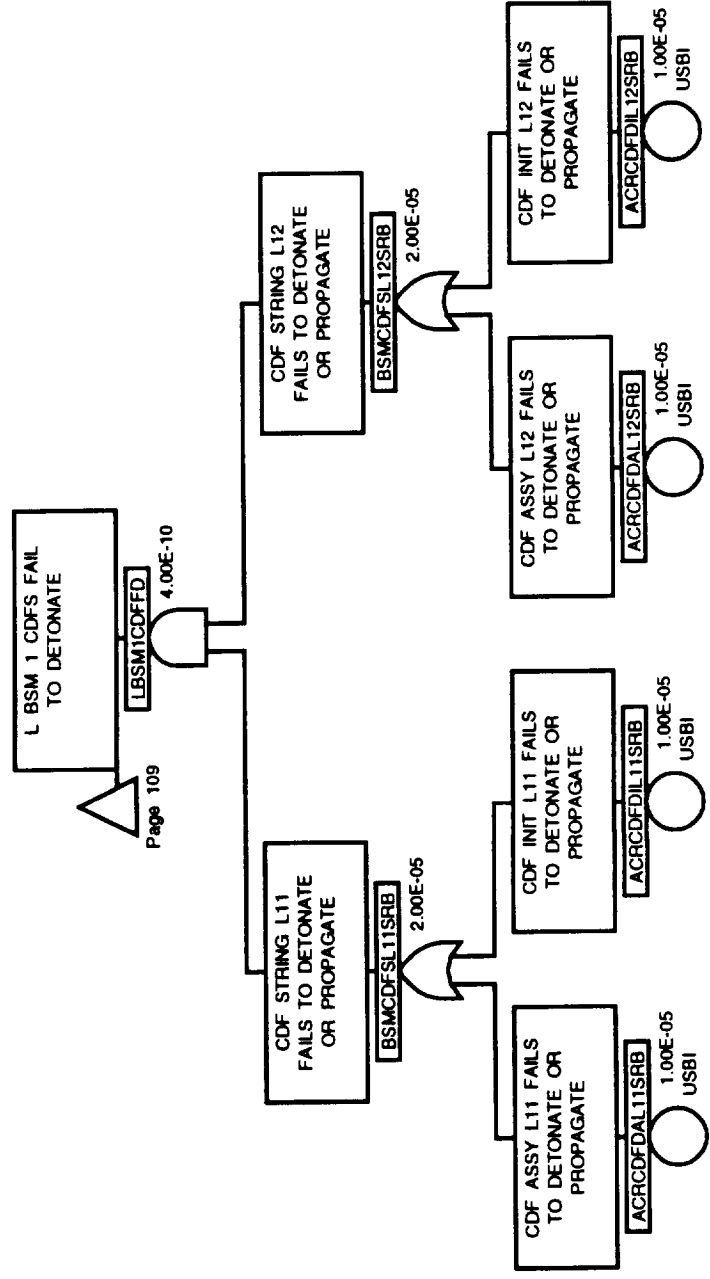
Page 96



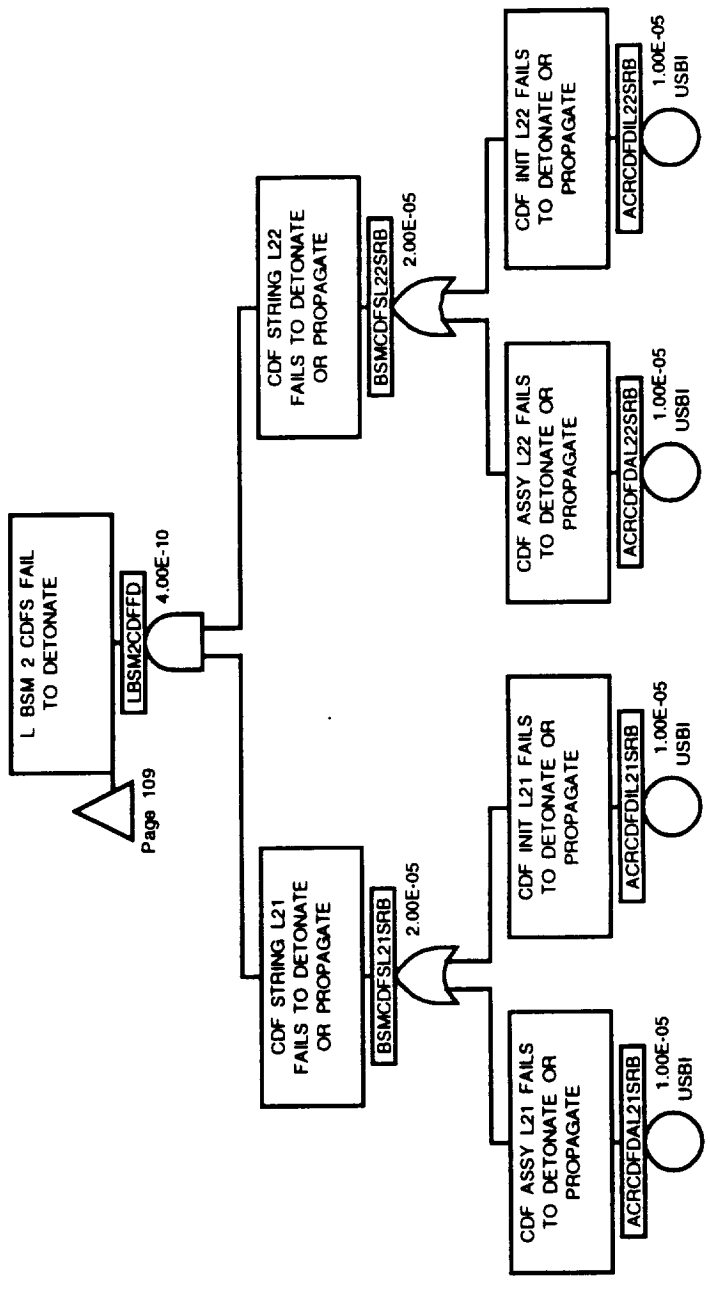




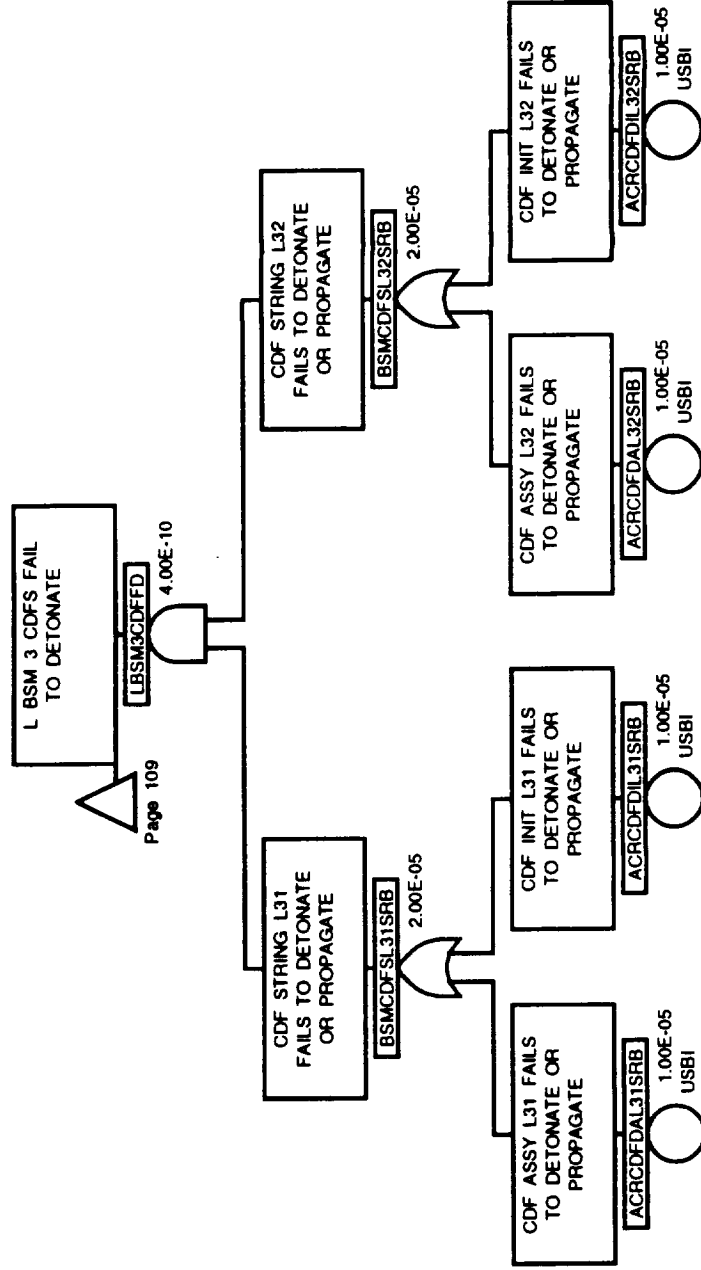




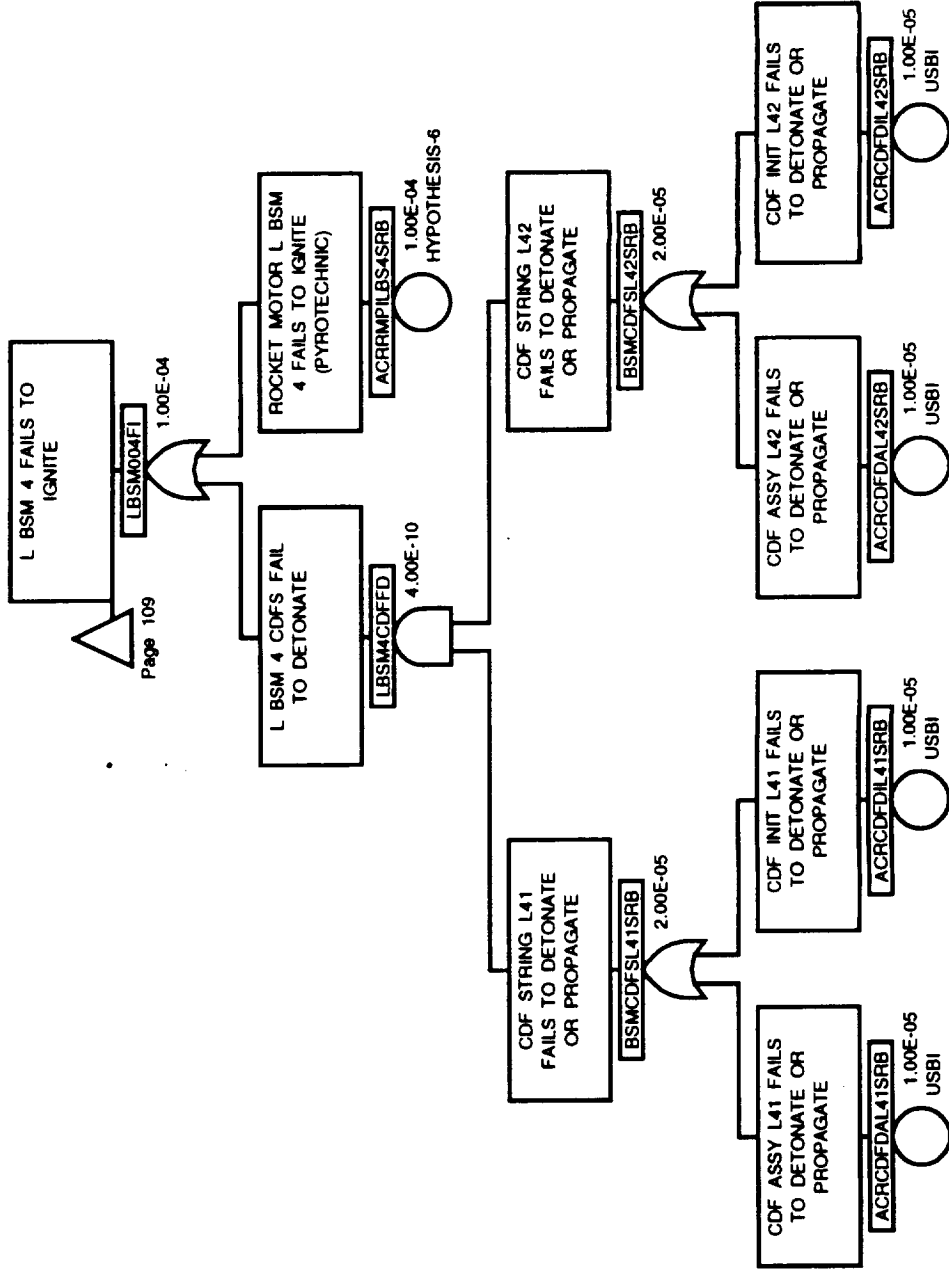
Page 109



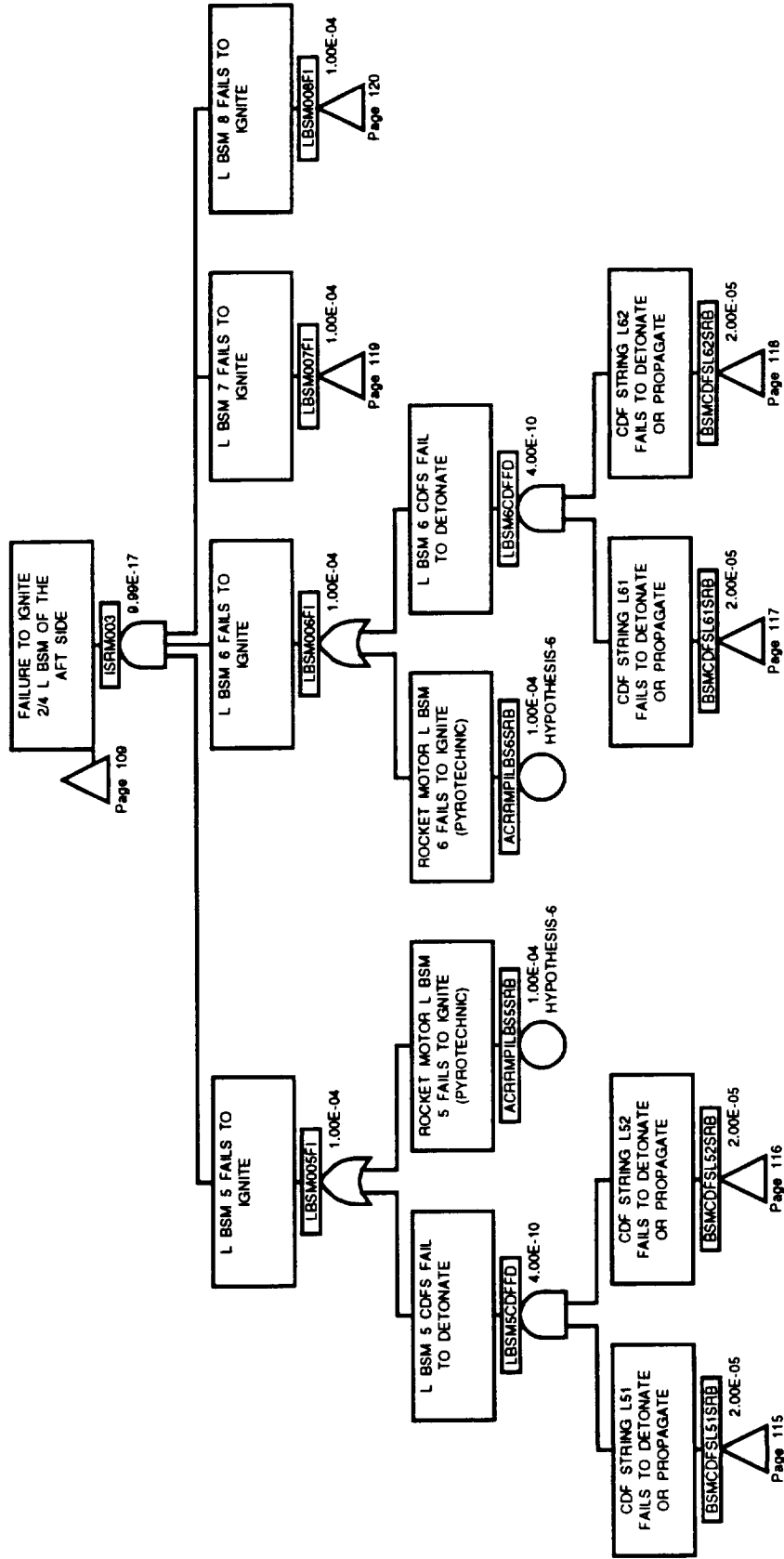
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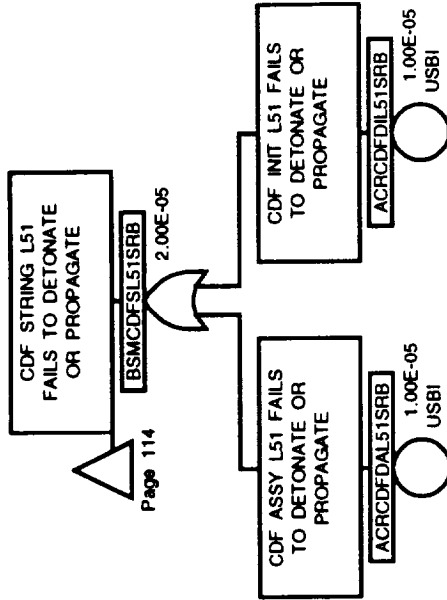


Page 109

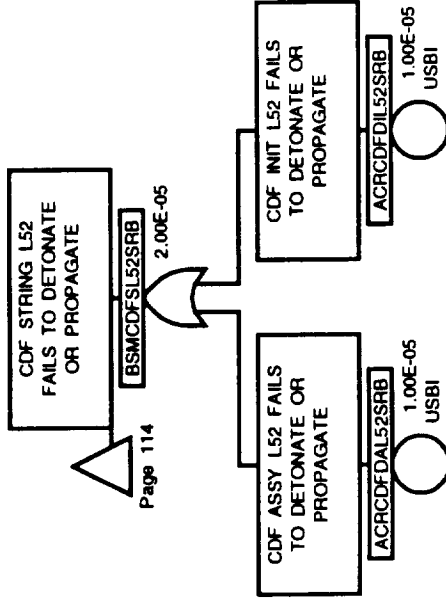


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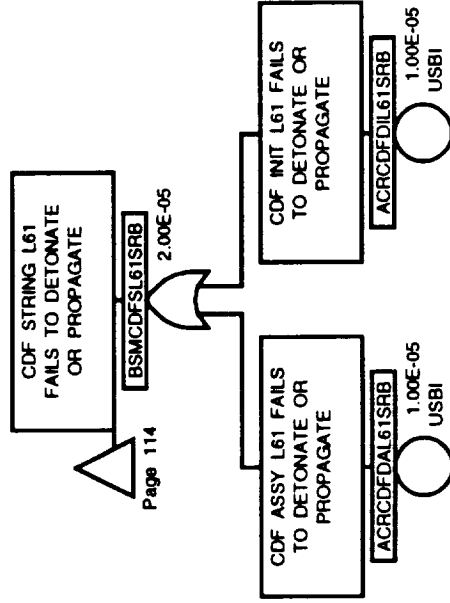




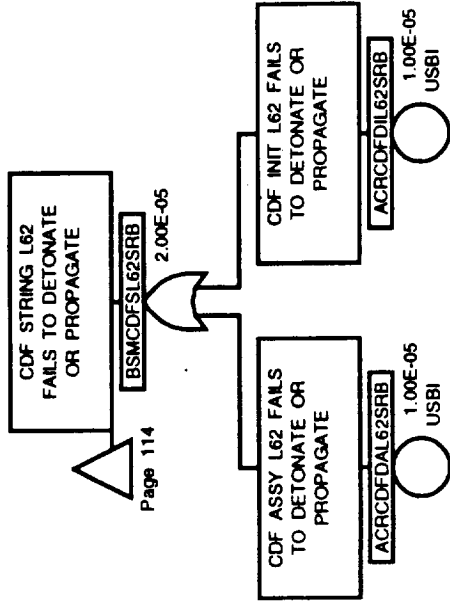
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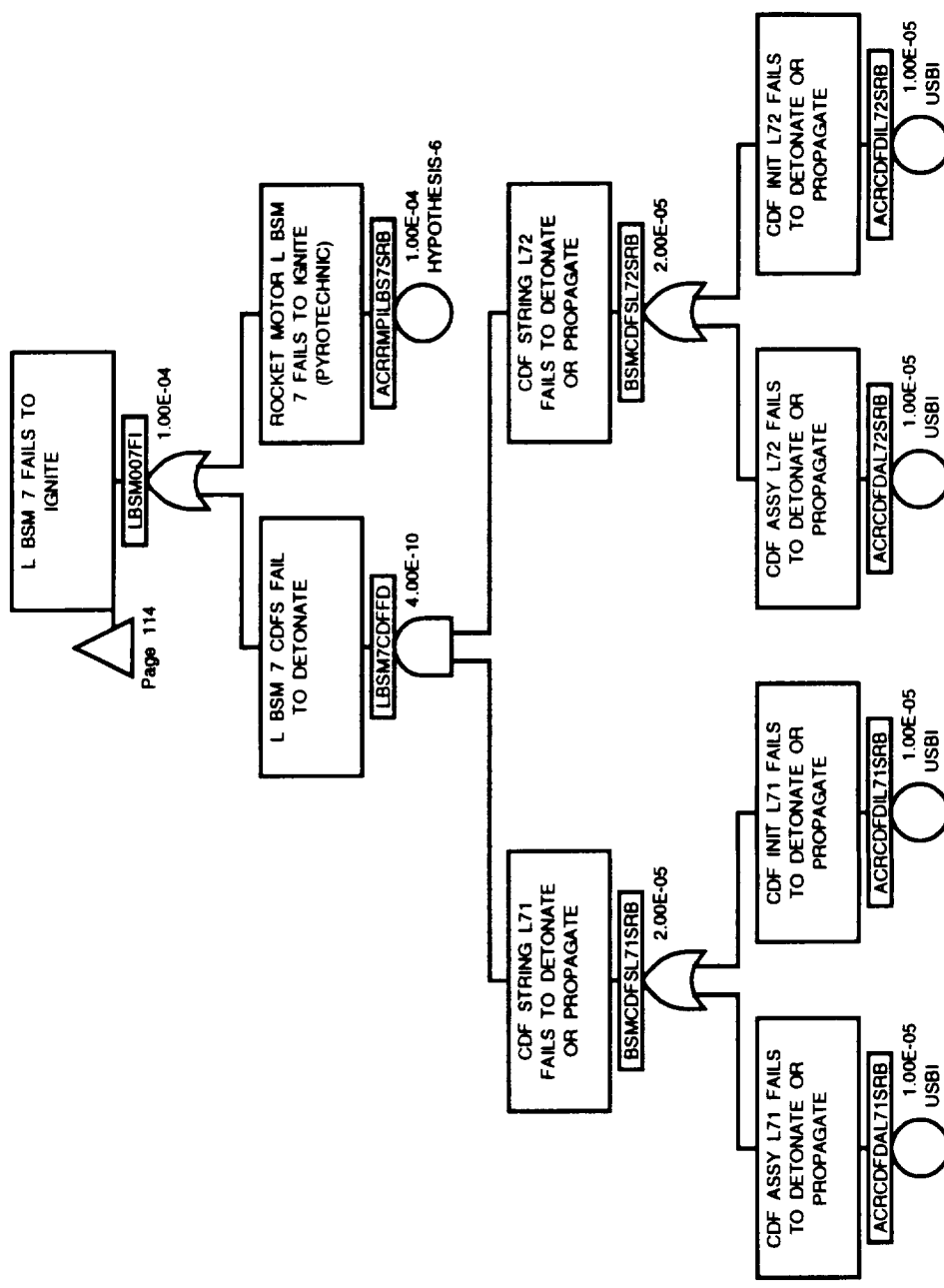
Page 114



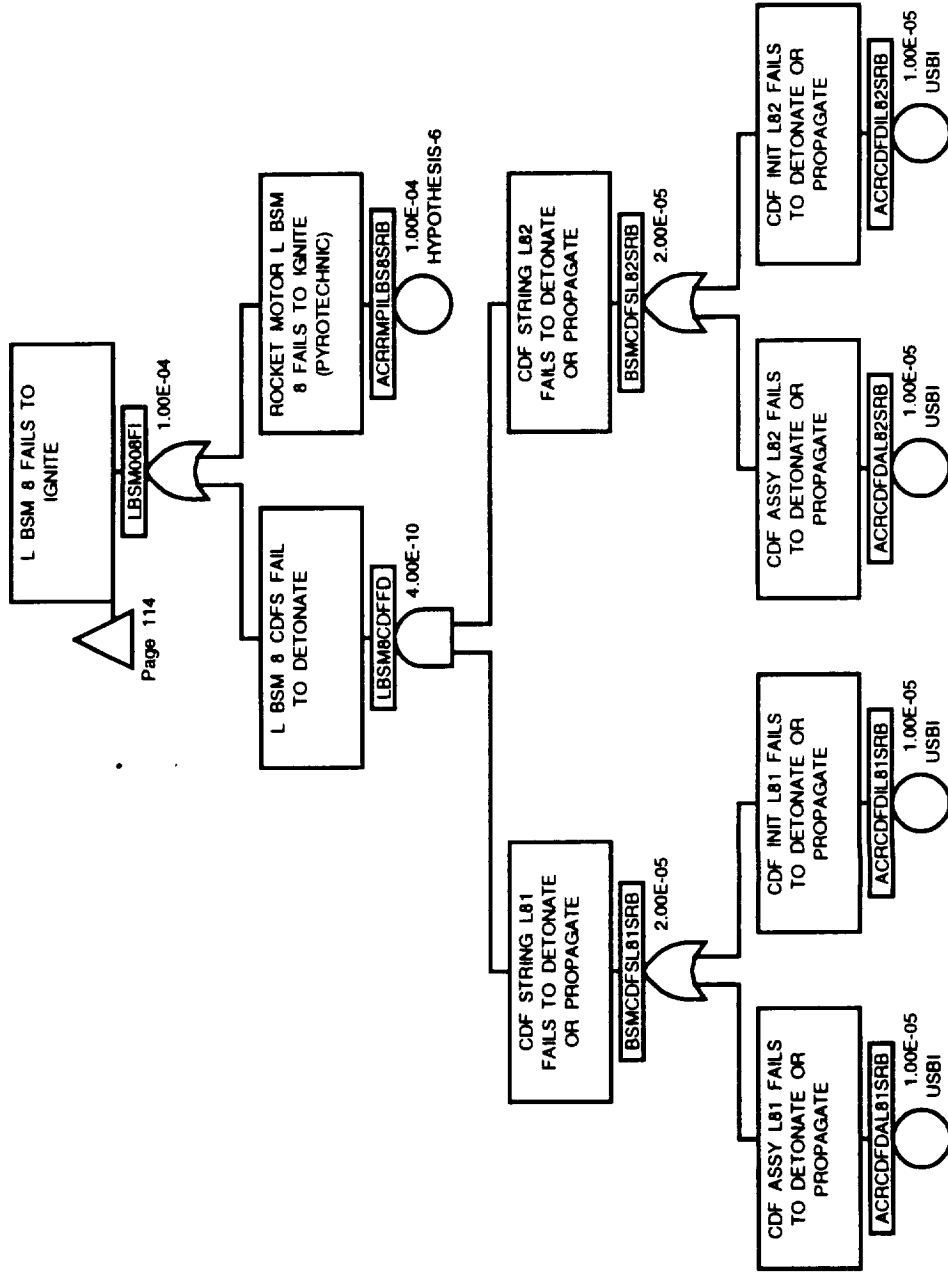
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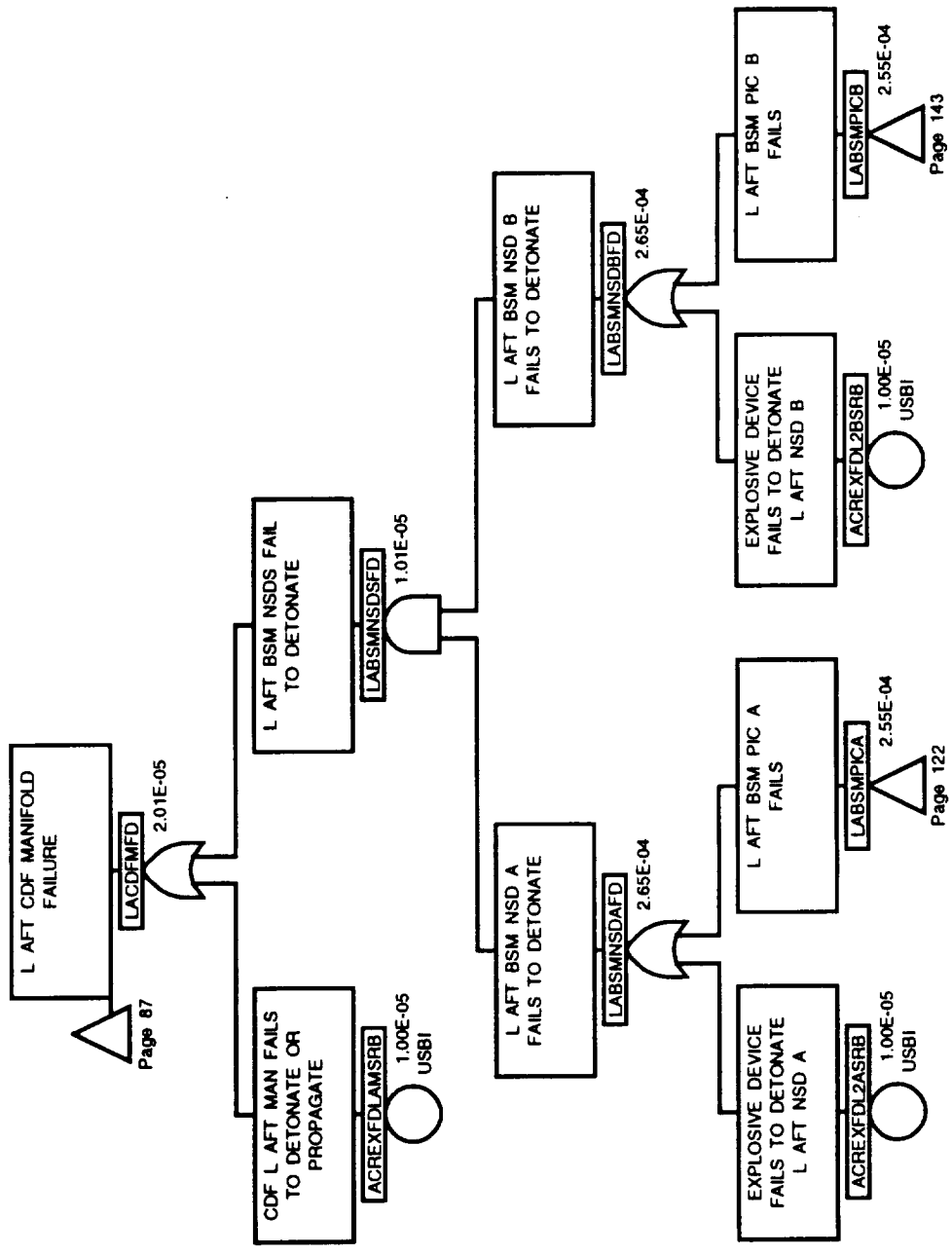


Page 114



Page 114

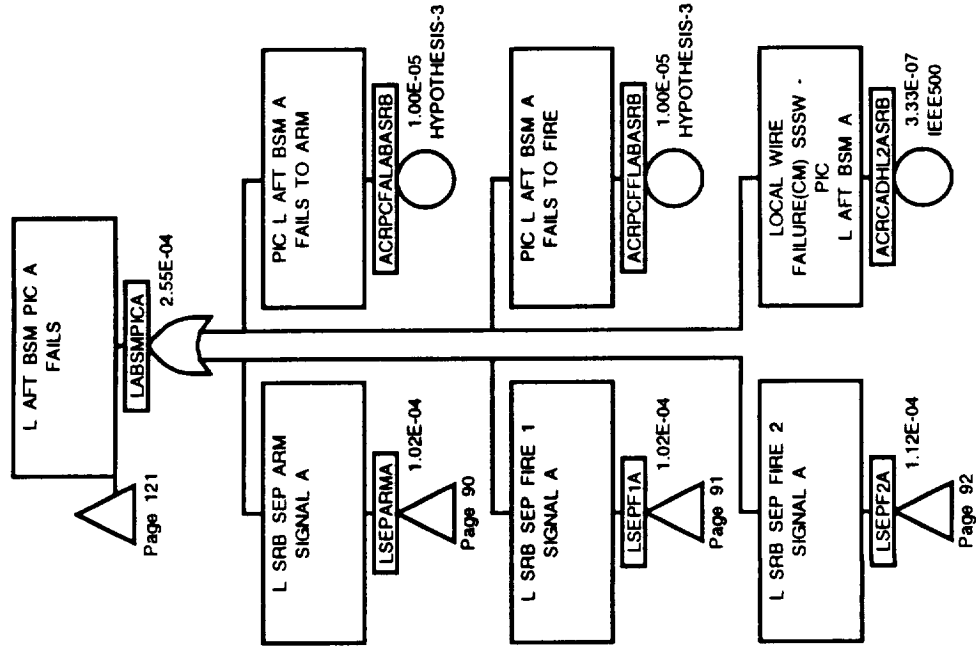


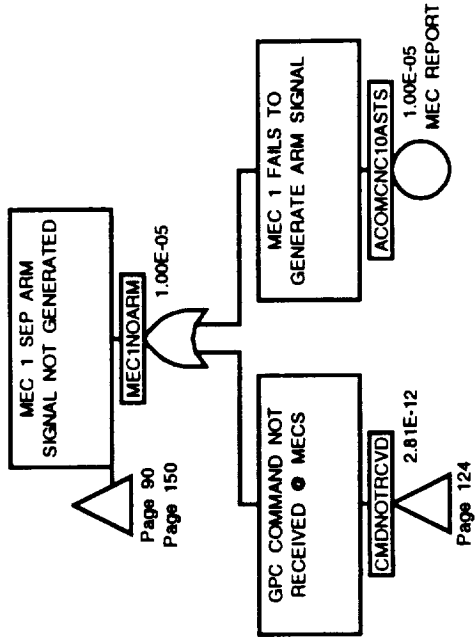


Page 87

Page 122

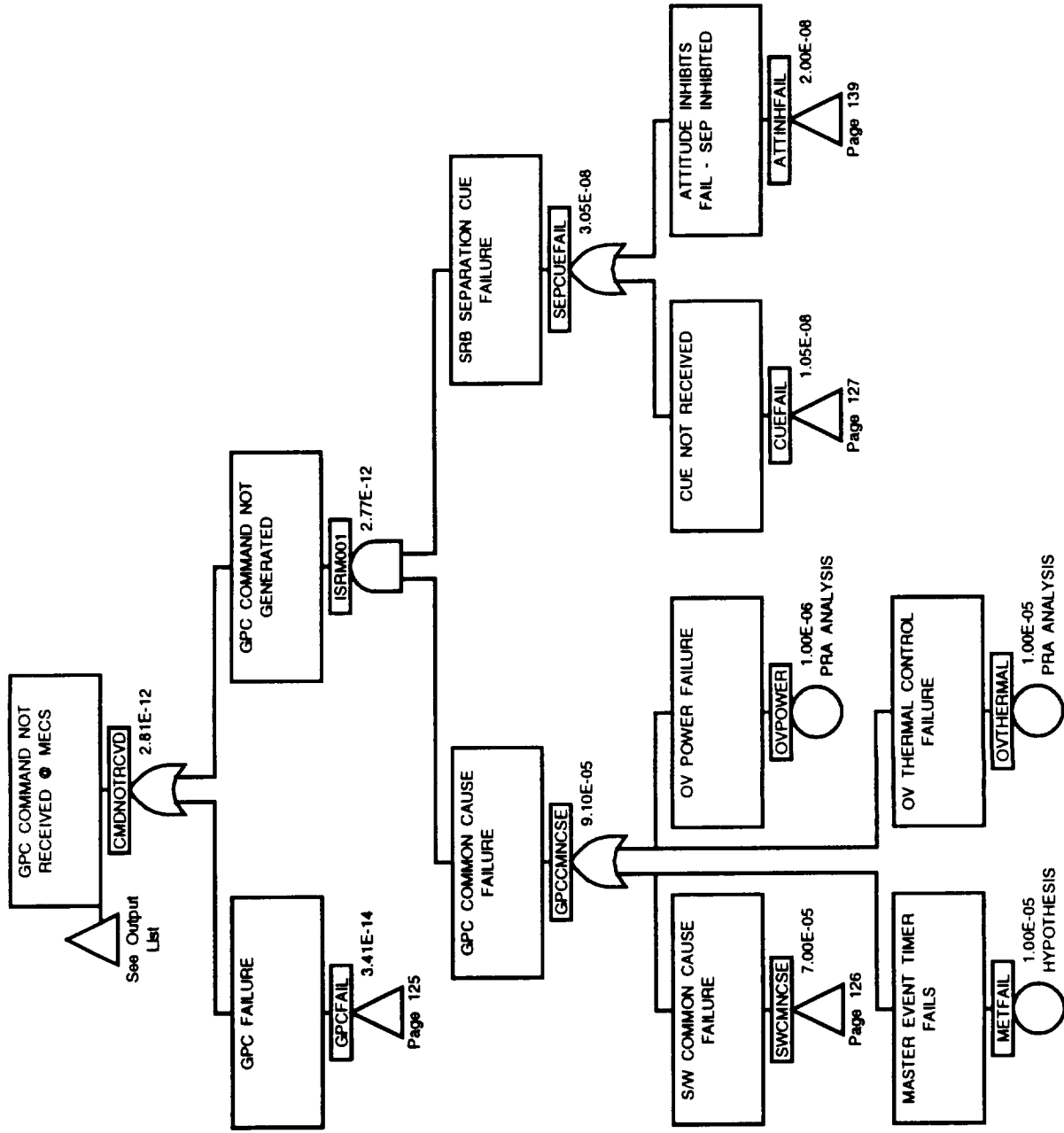
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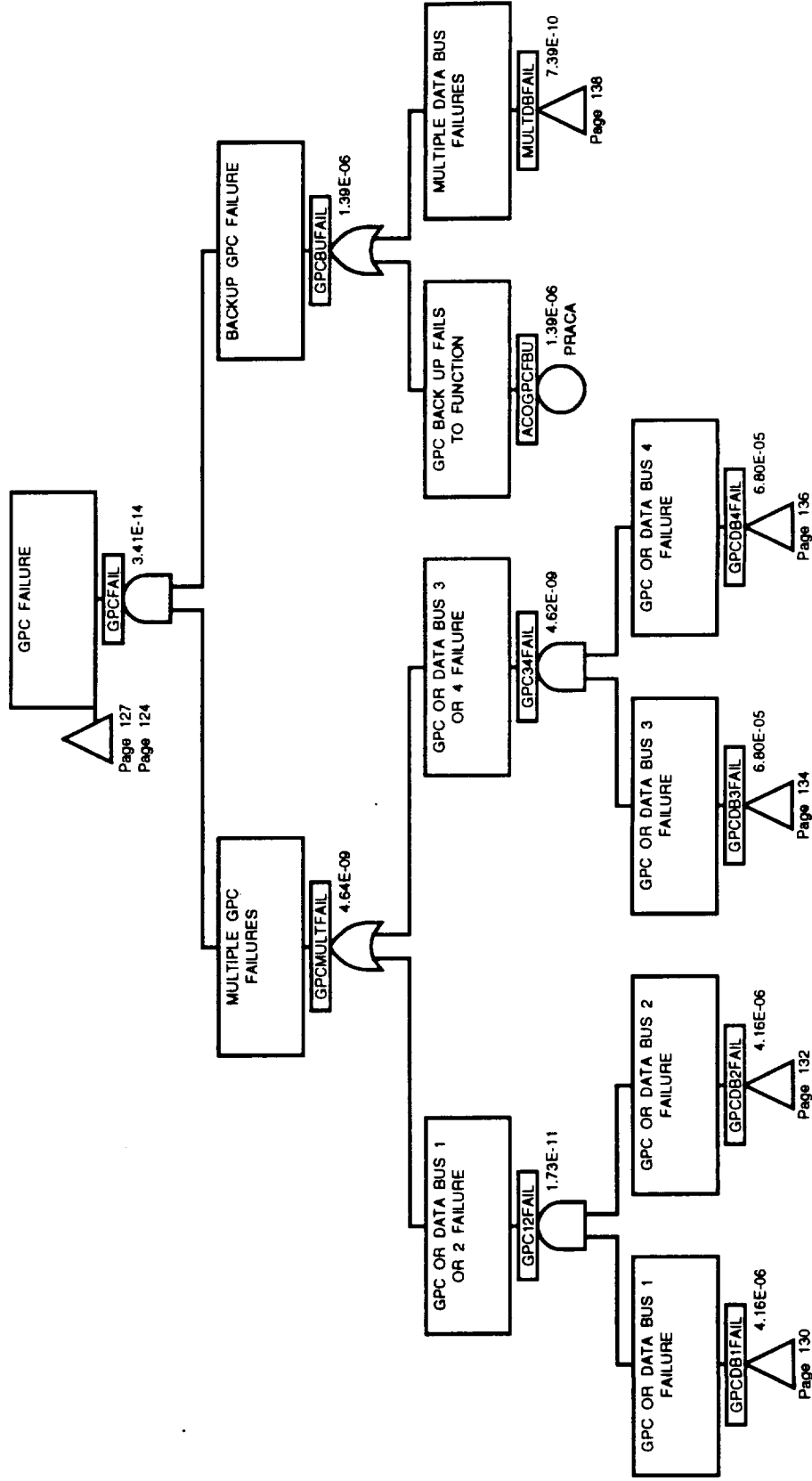


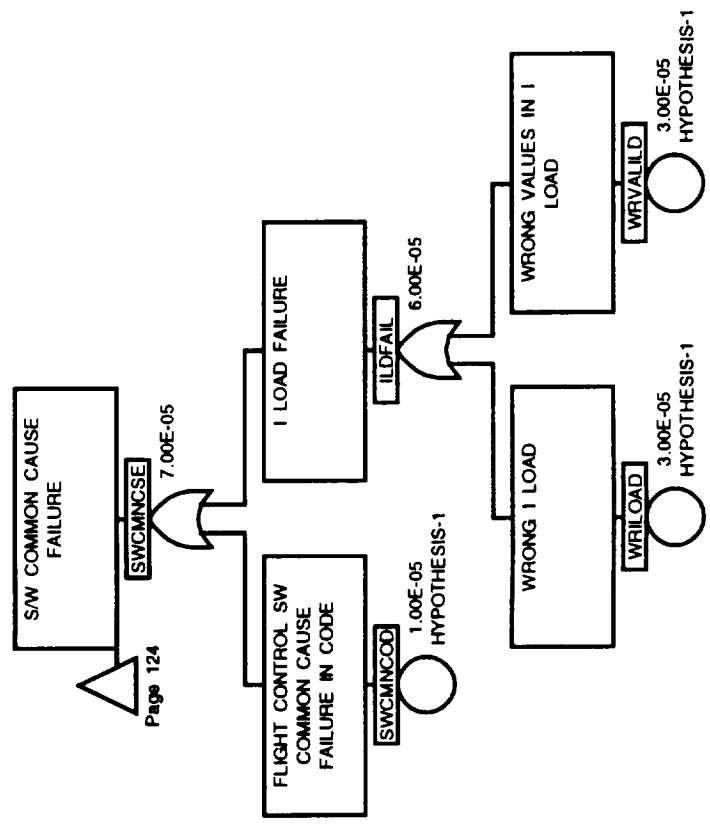


Page 90
Page 150

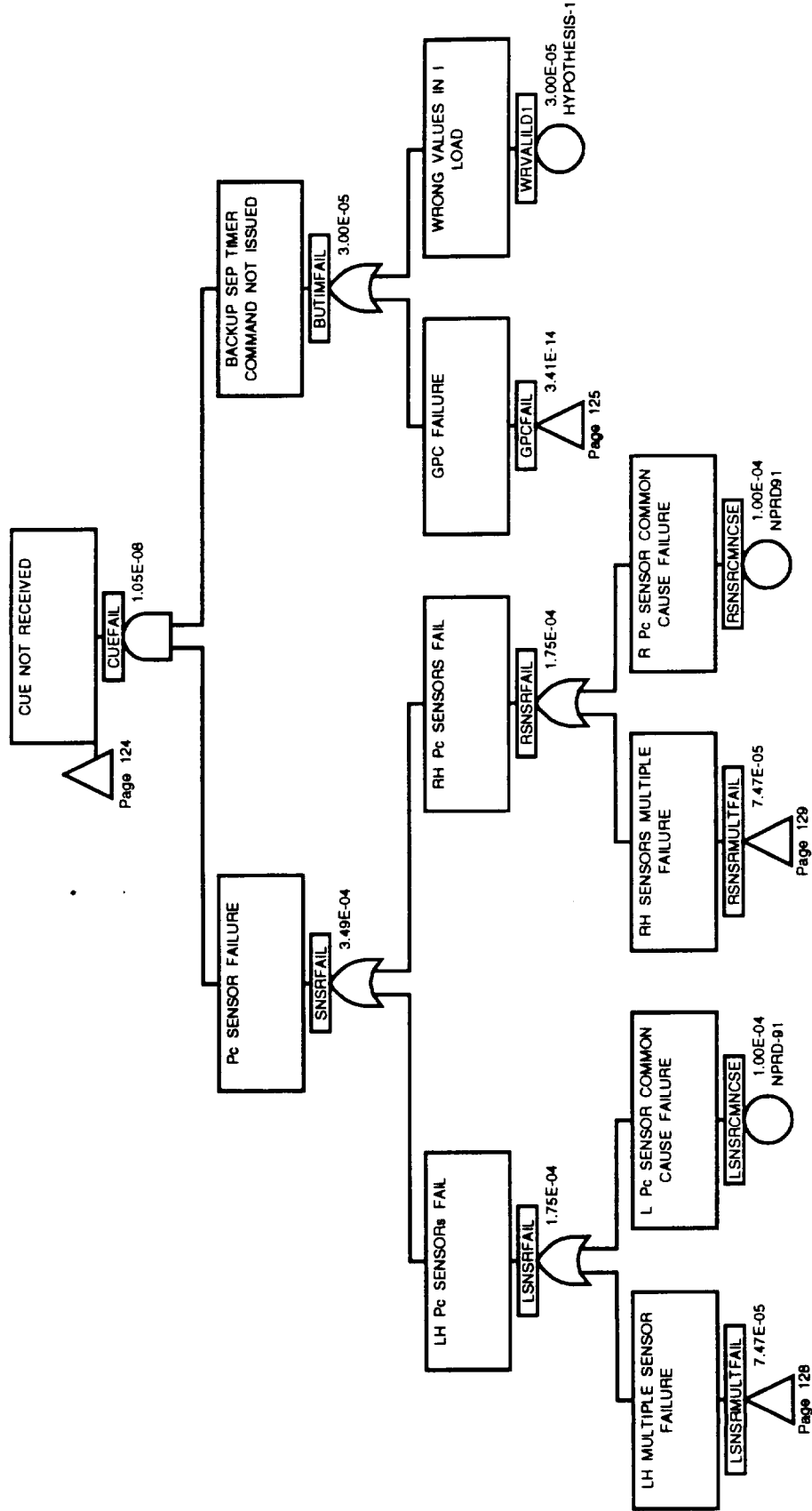
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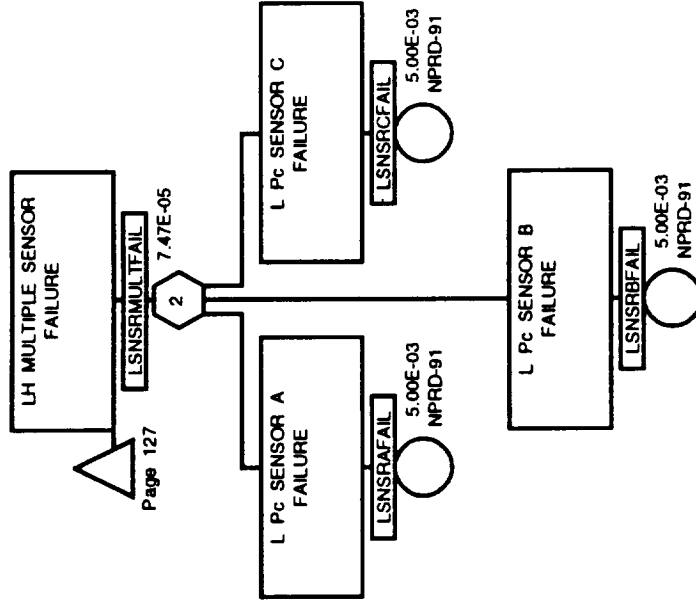




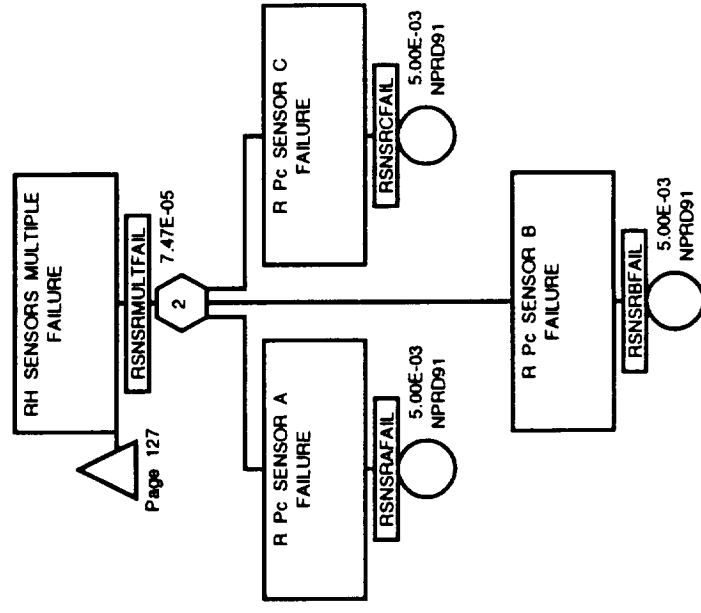


Page 124

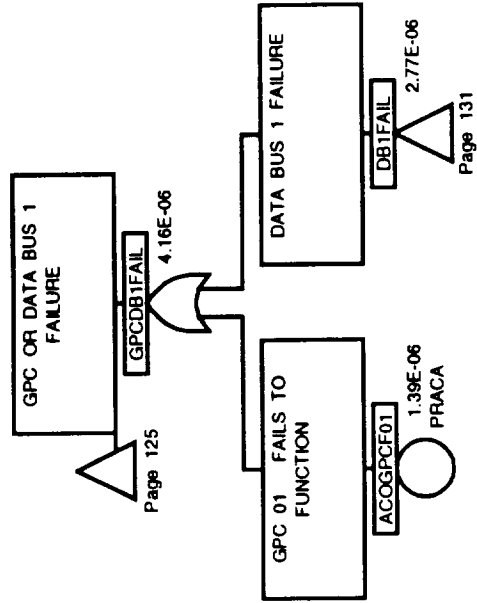




Page 127



Page 127



Page 125

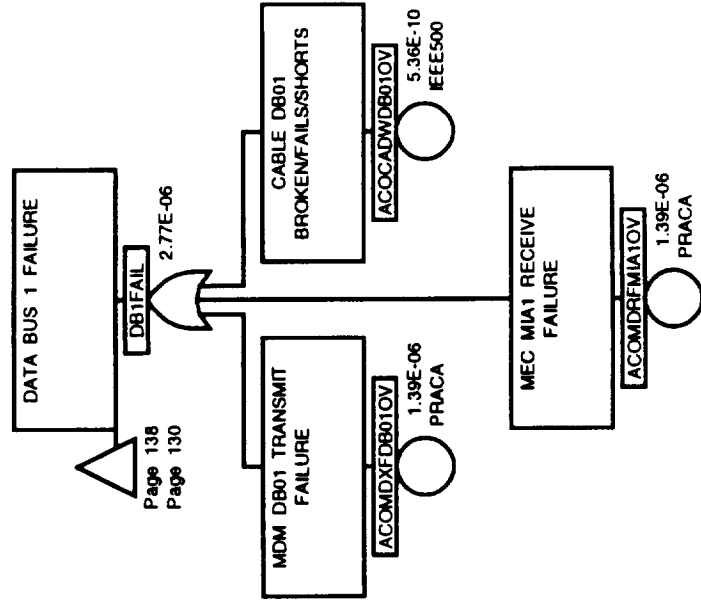
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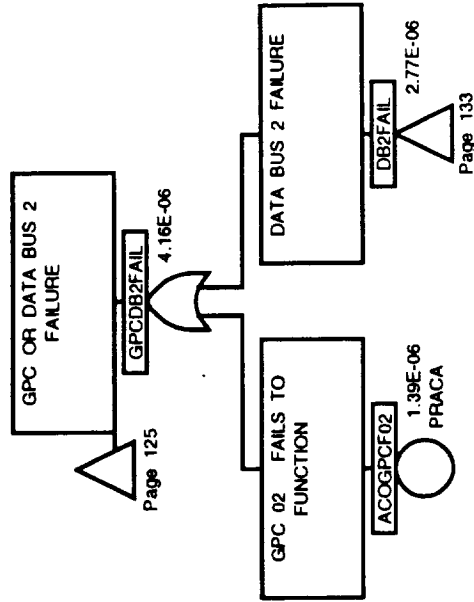
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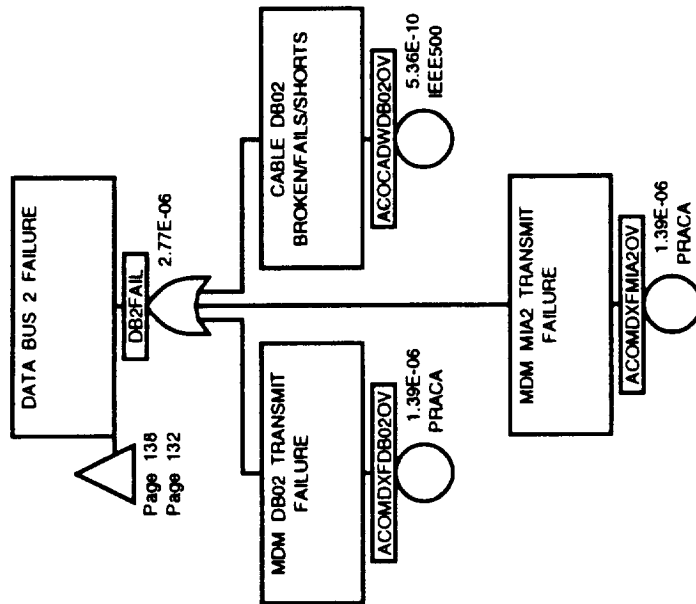
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Page 131

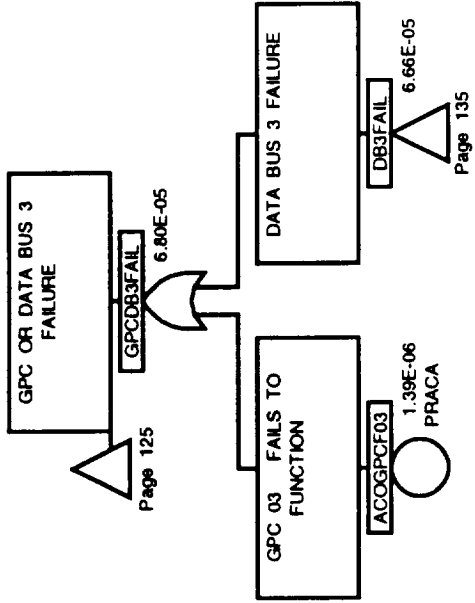


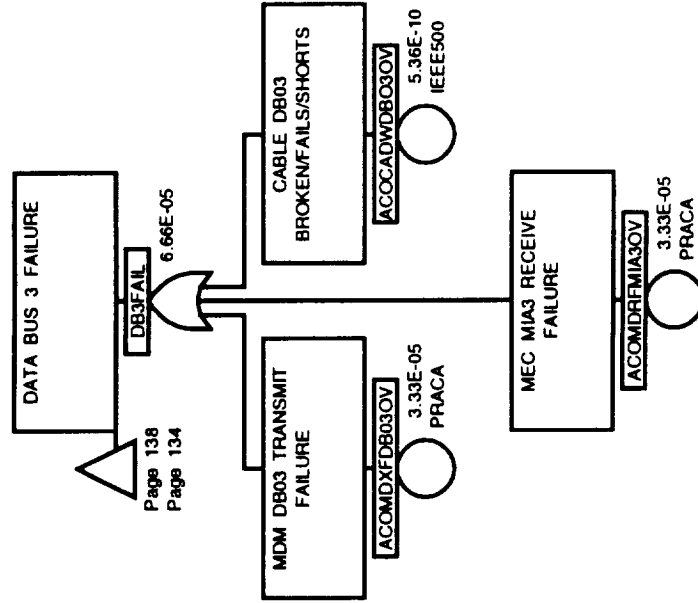
Page 138
Page 130



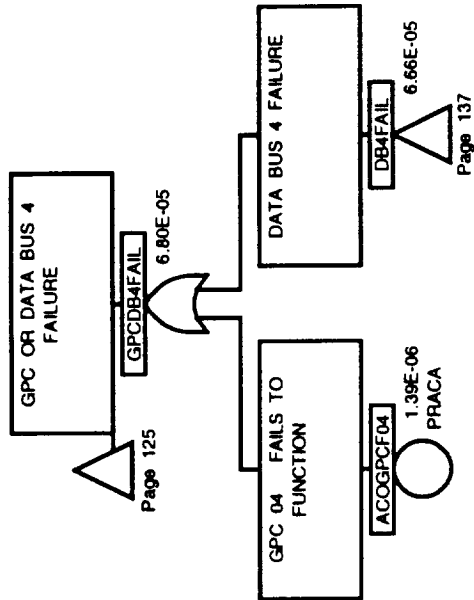


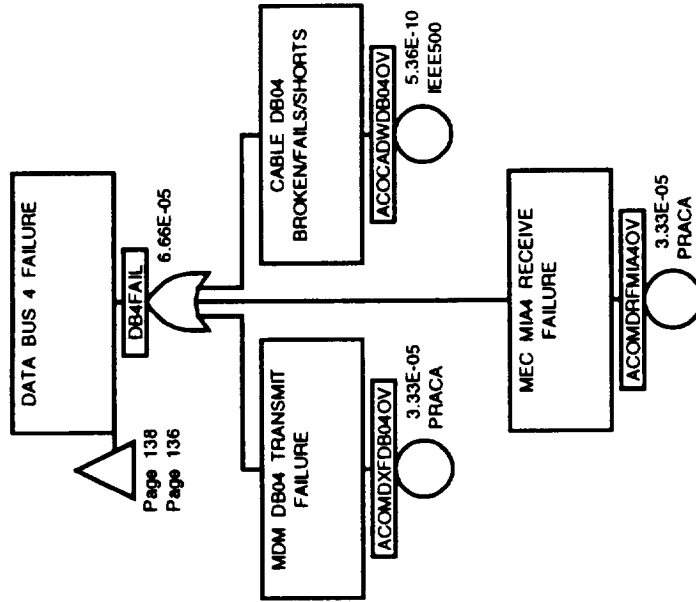
Page 138
Page 132



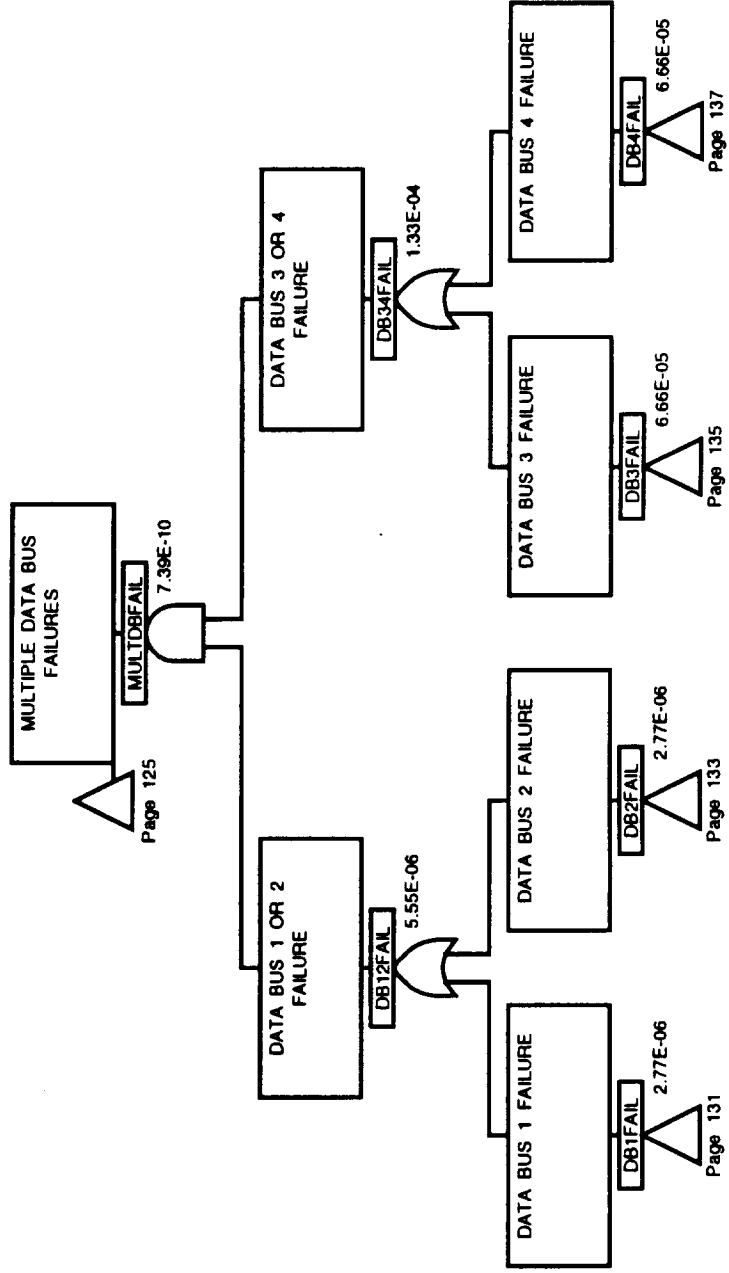


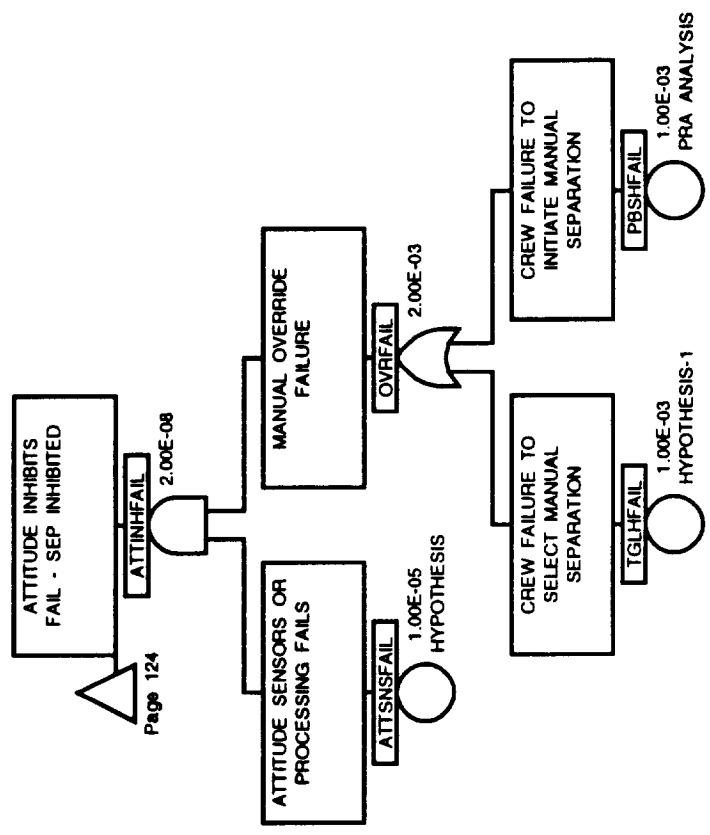
Page 136
Page 134



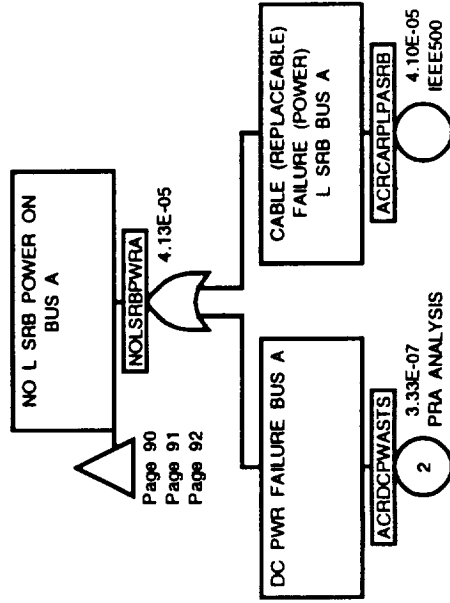


Page 138
Page 136

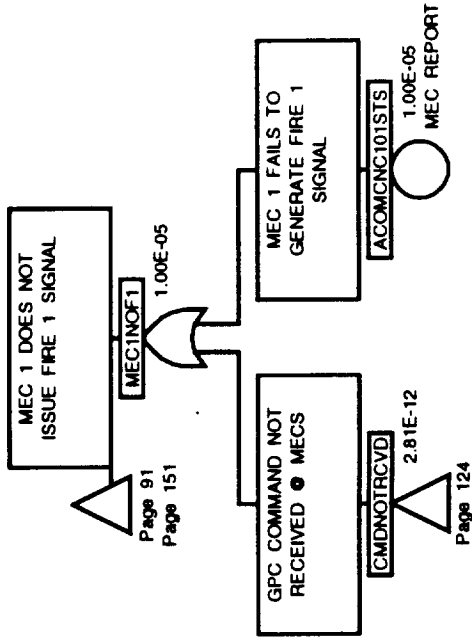


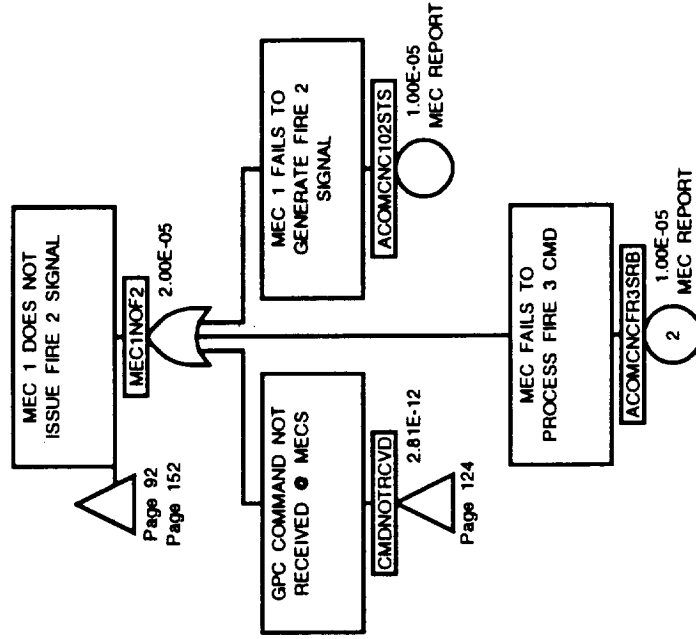


Page 124



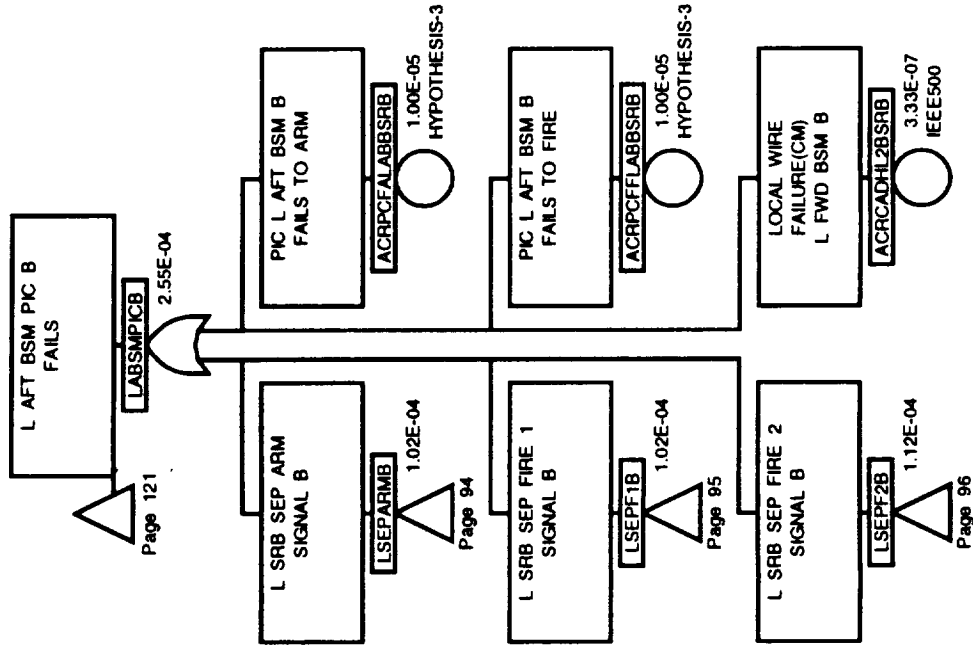
Page 90
Page 91
Page 92





Page 92
Page 152

Page 124

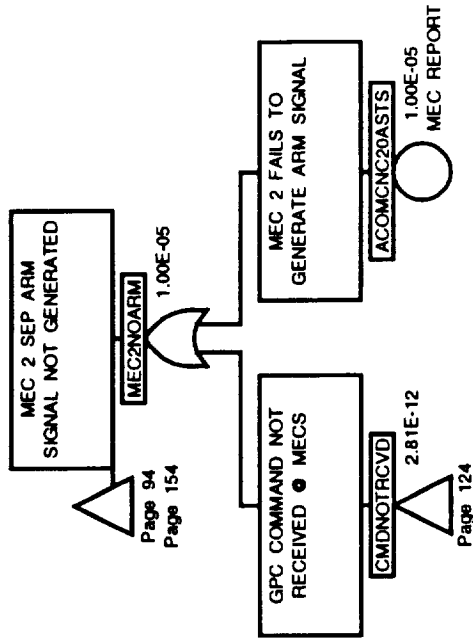


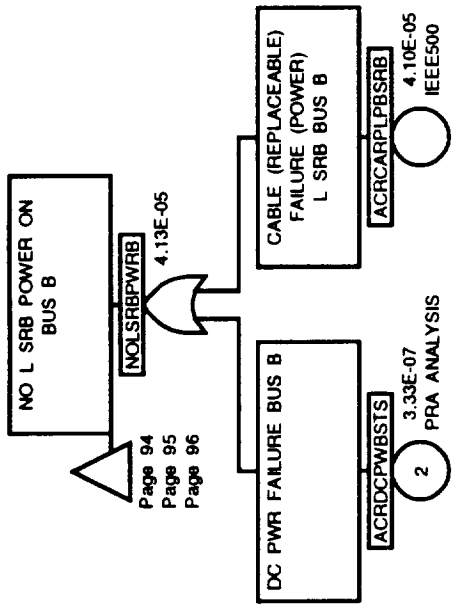
Page 121

Page 94

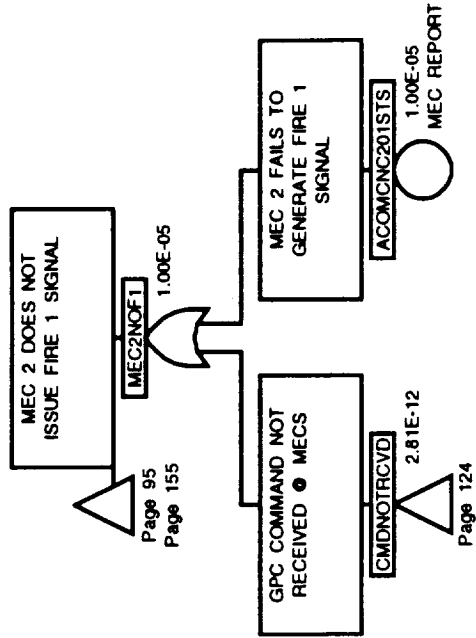
Page 95

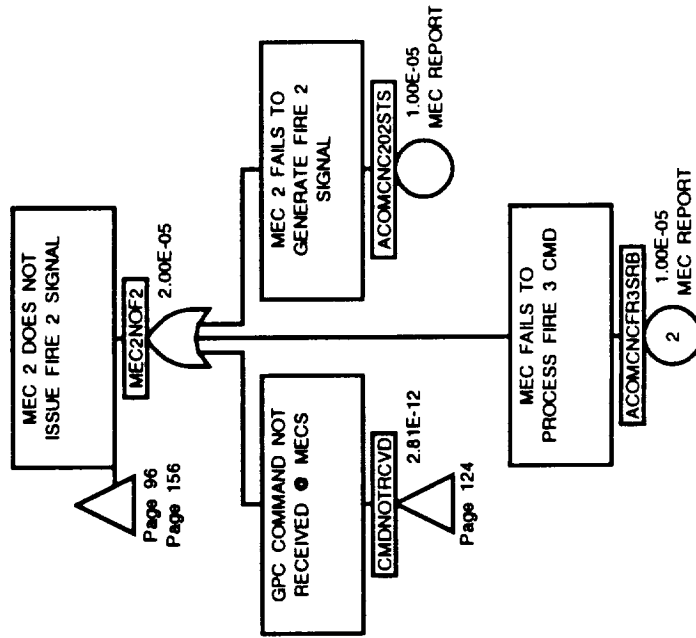
Page 96

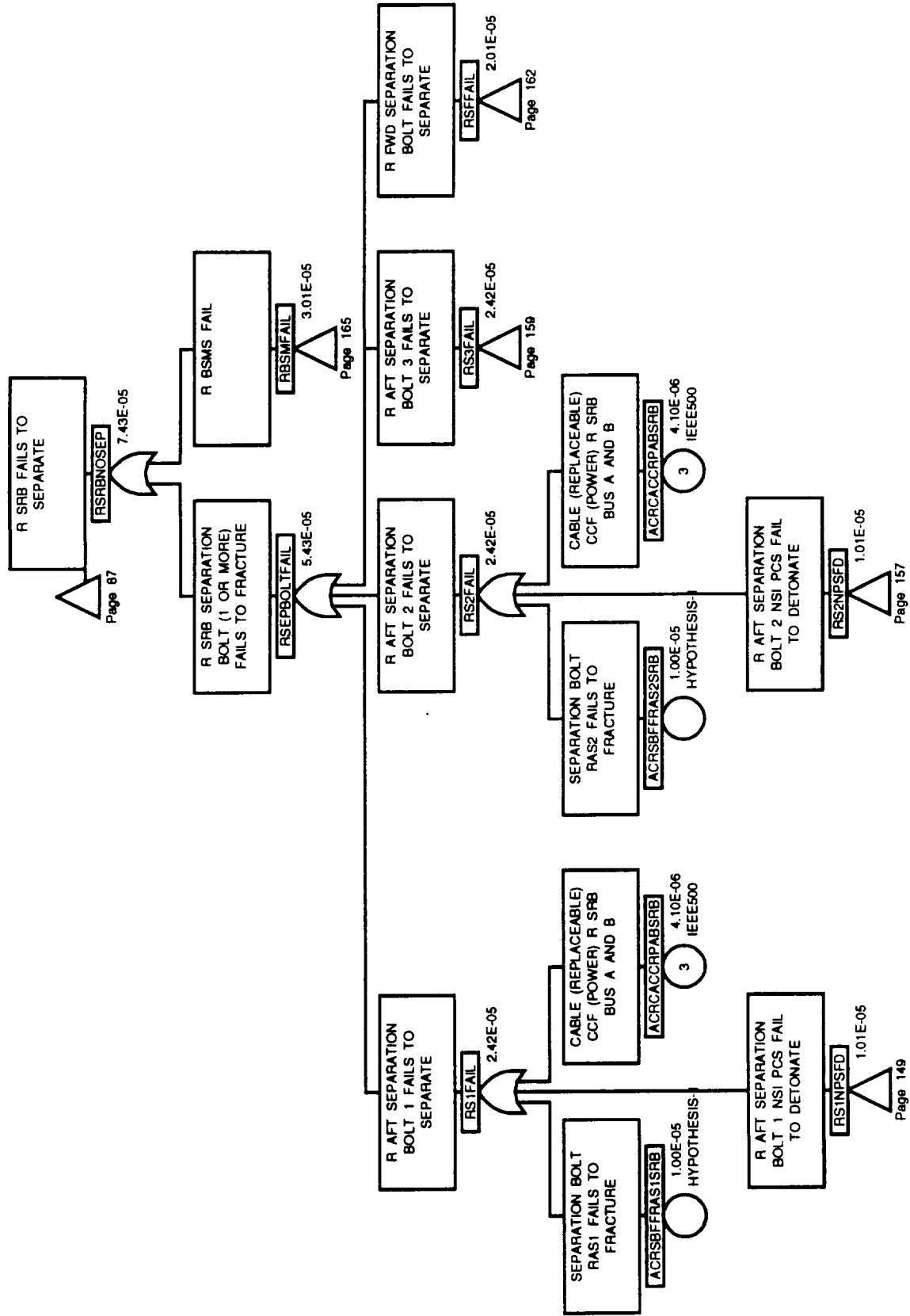


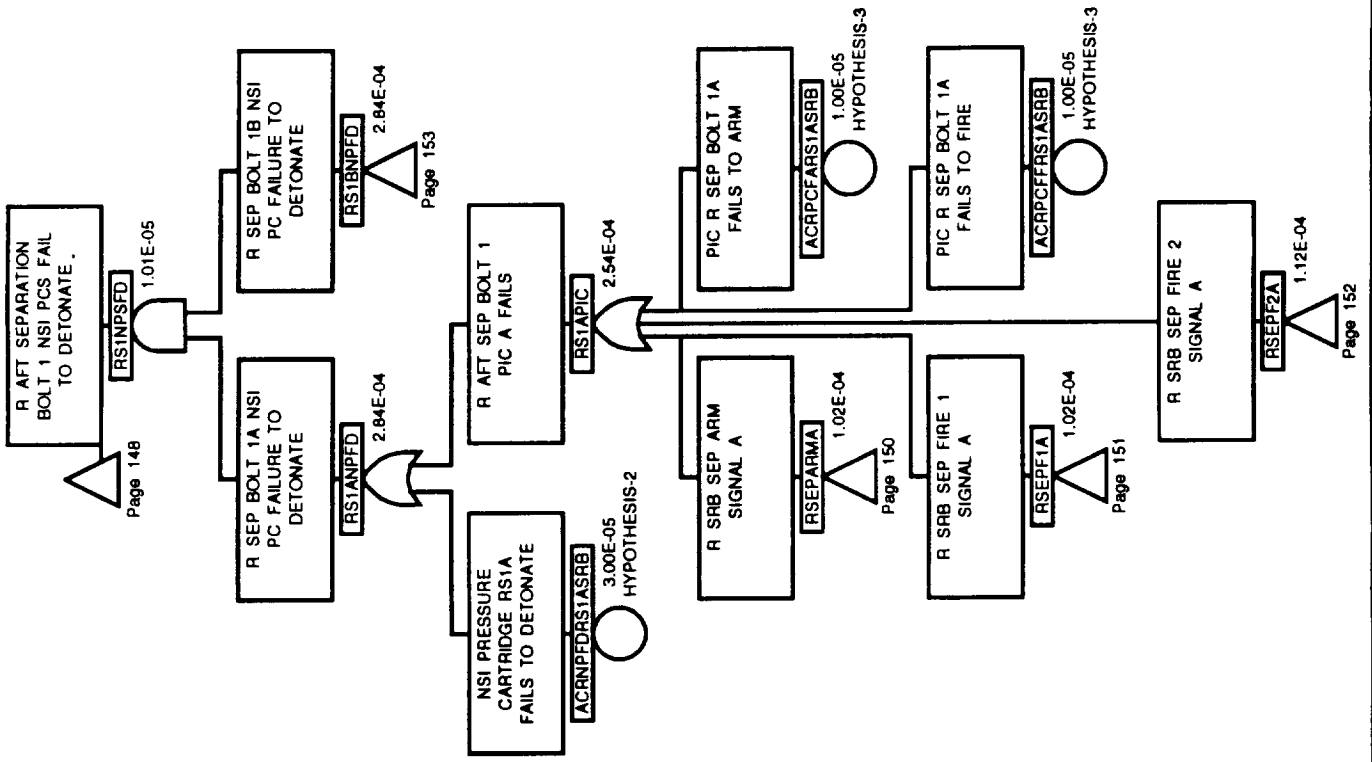


Page 94
Page 95
Page 96









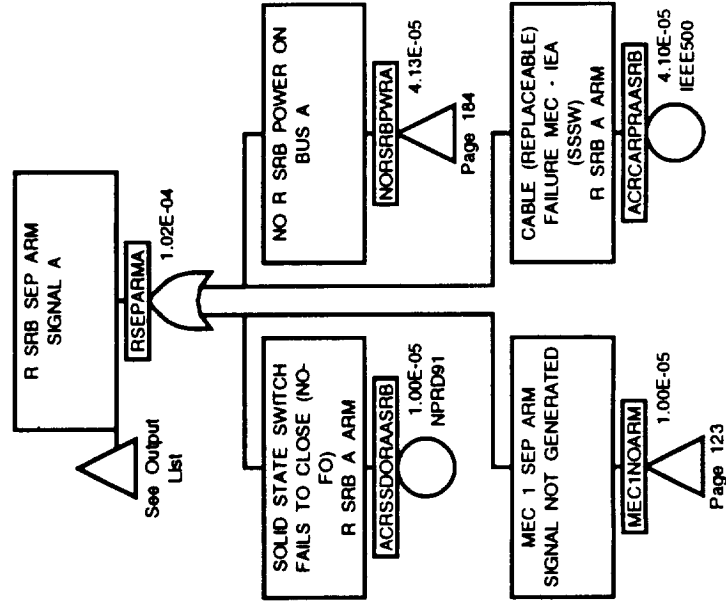
Page 148

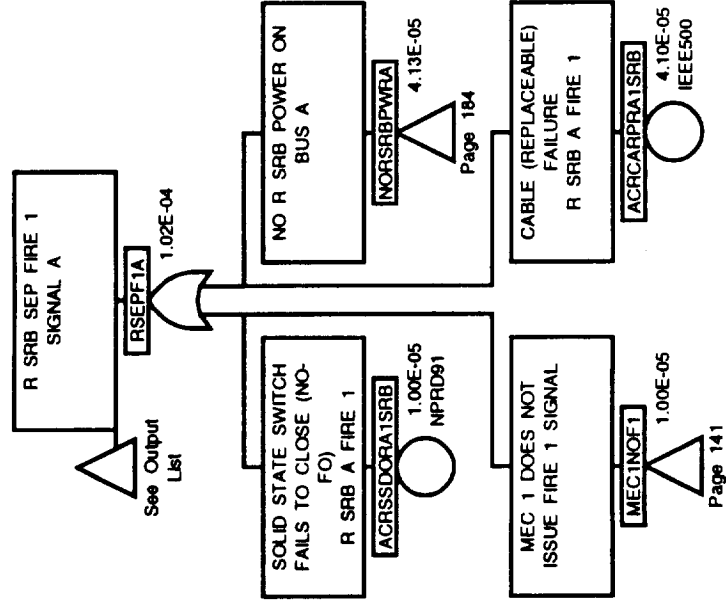
Page 153

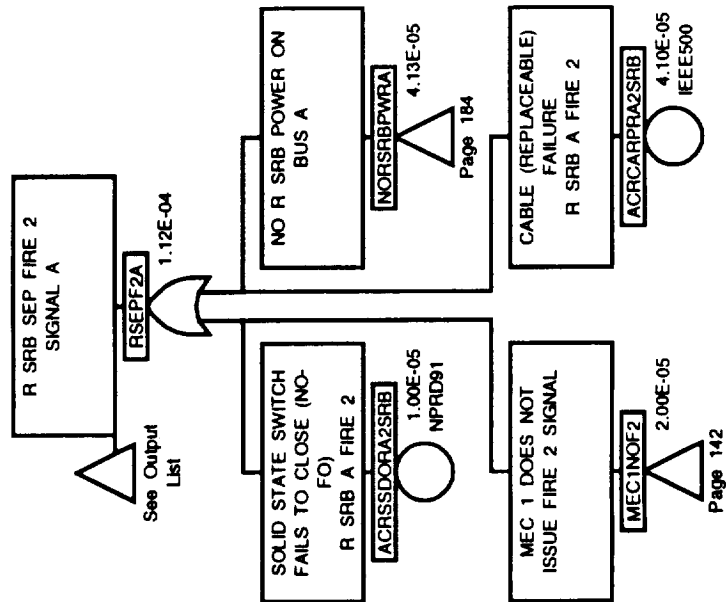
Page 150

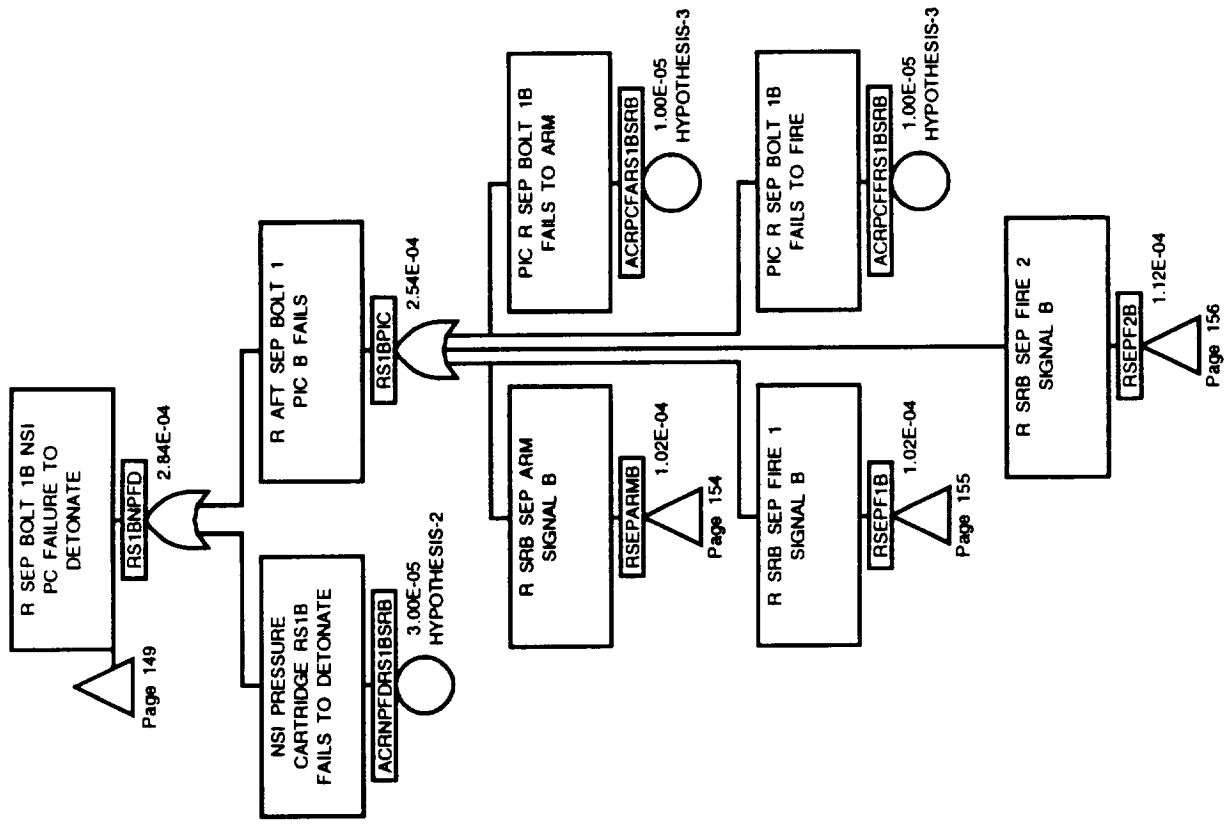
Page 151

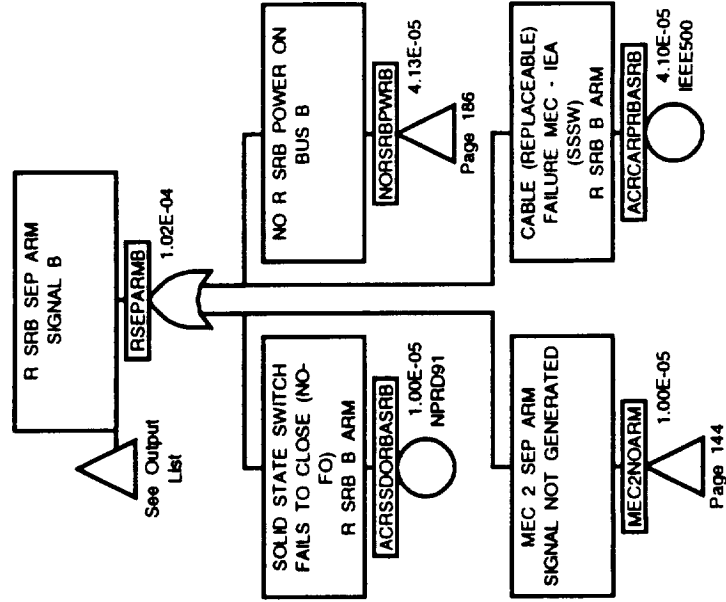
Page 152

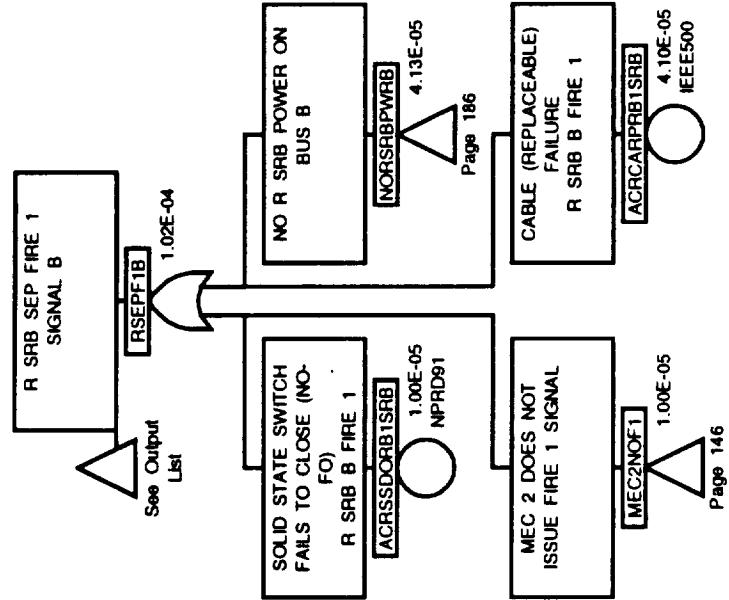


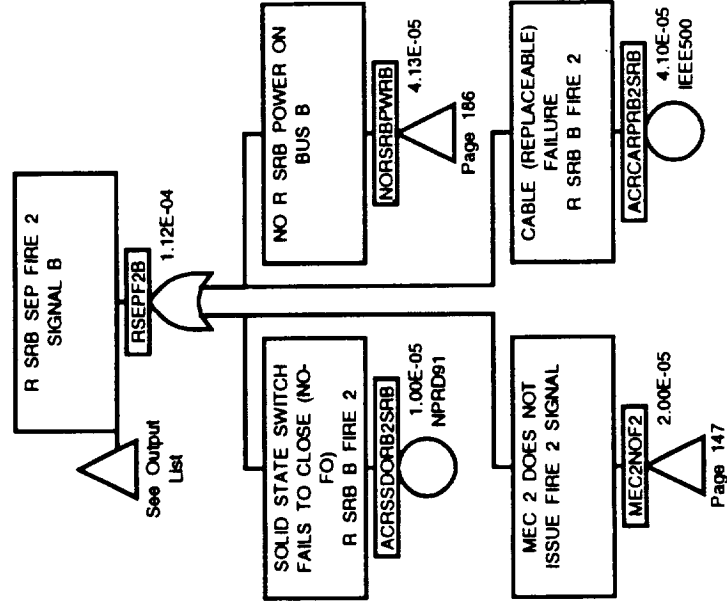


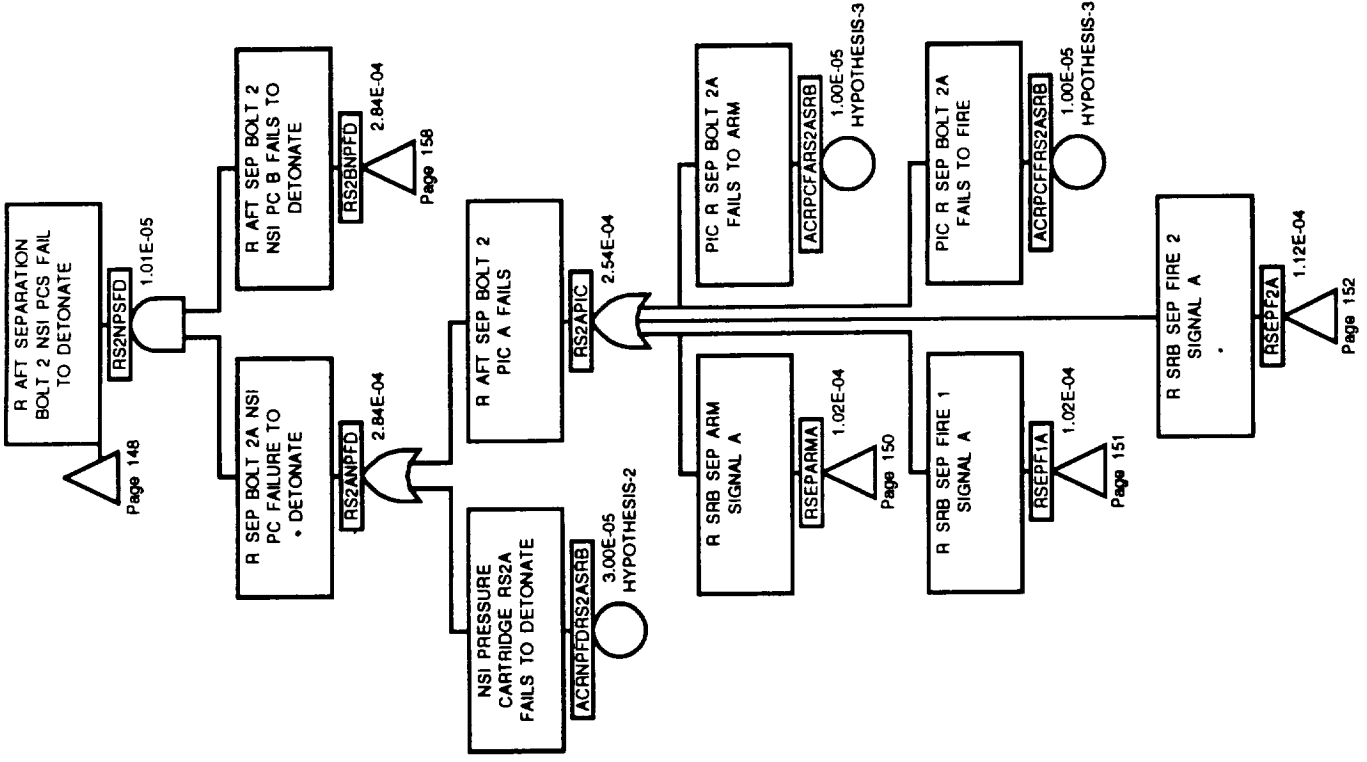












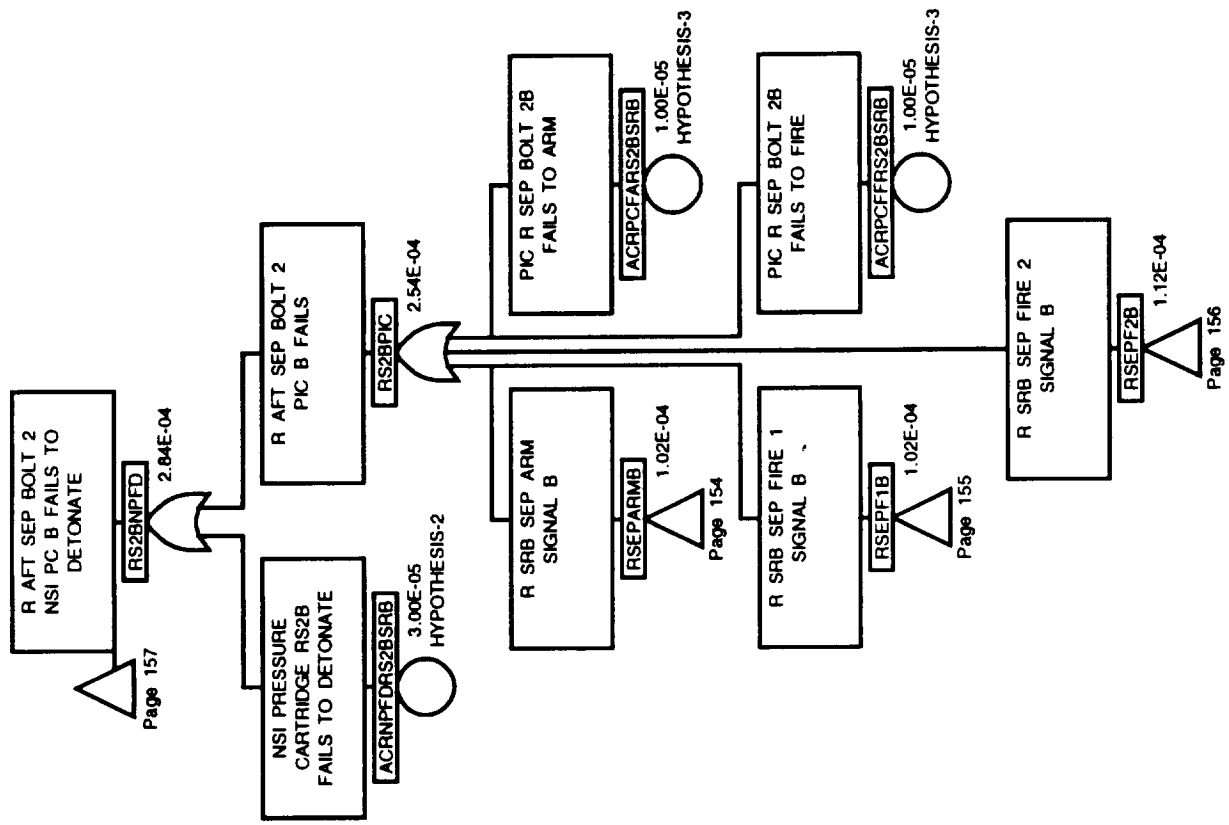
Page 148

Page 158

Page 150

Page 151

Page 152

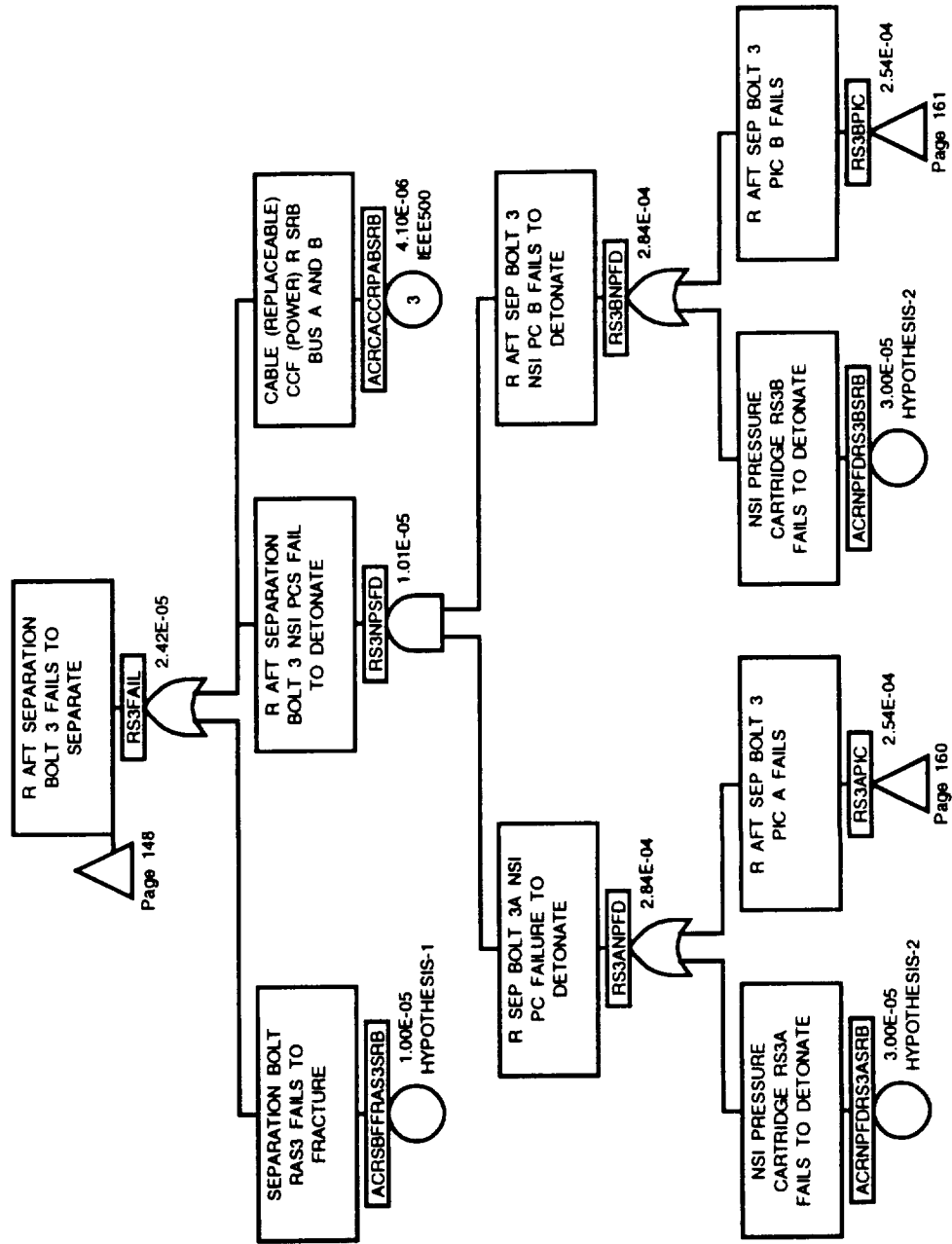


Page 157

Page 154

Page 155

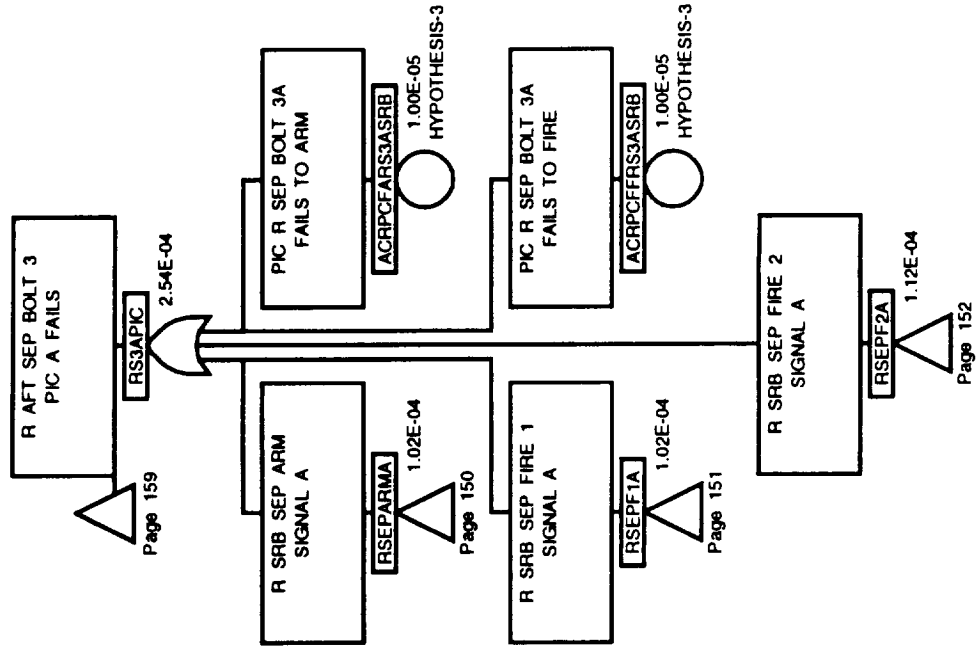
Page 156



Page 148

Page 160

Page 161

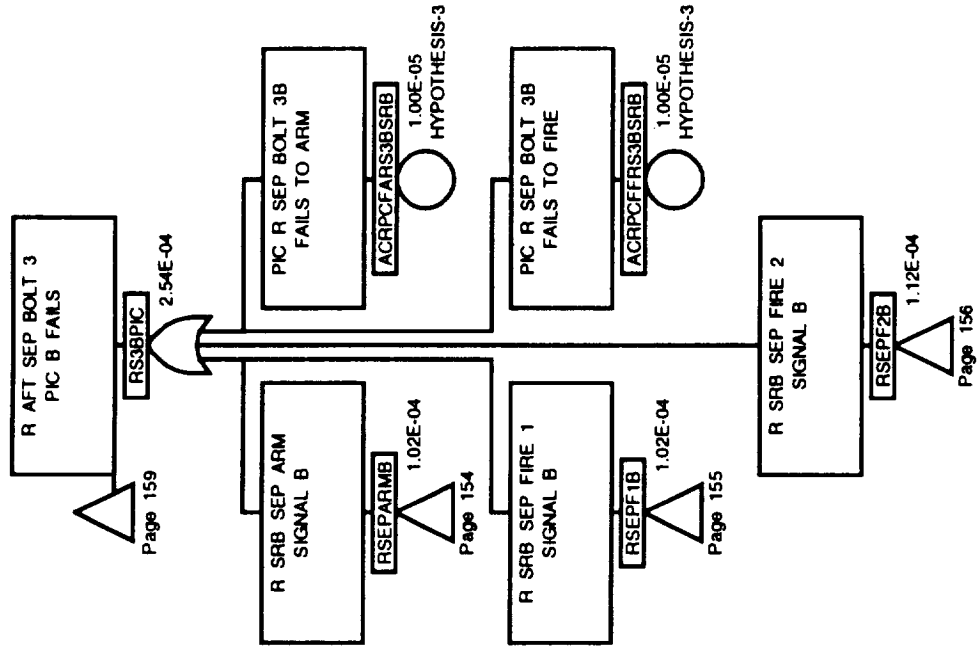


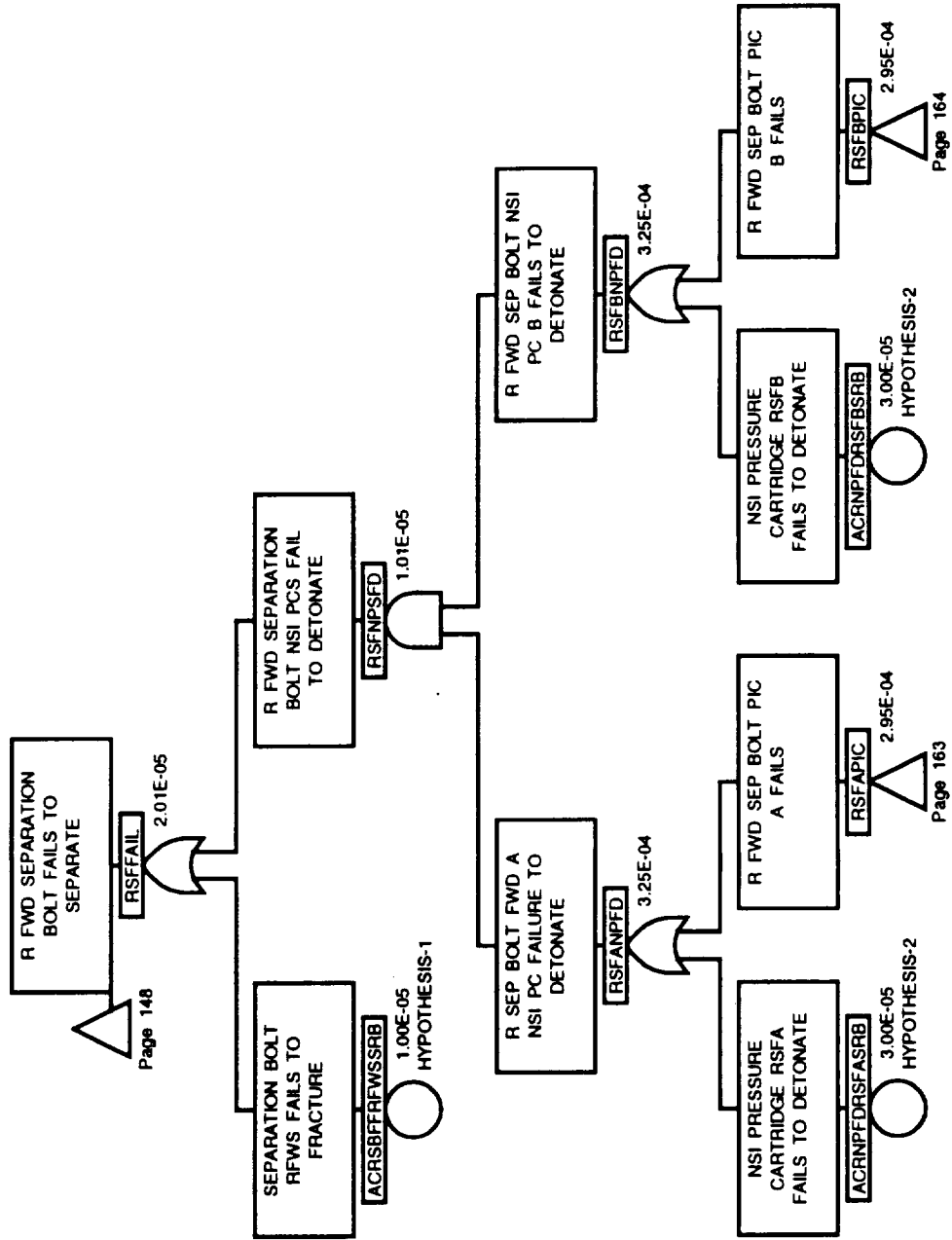
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Page 150

Page 151

Page 152

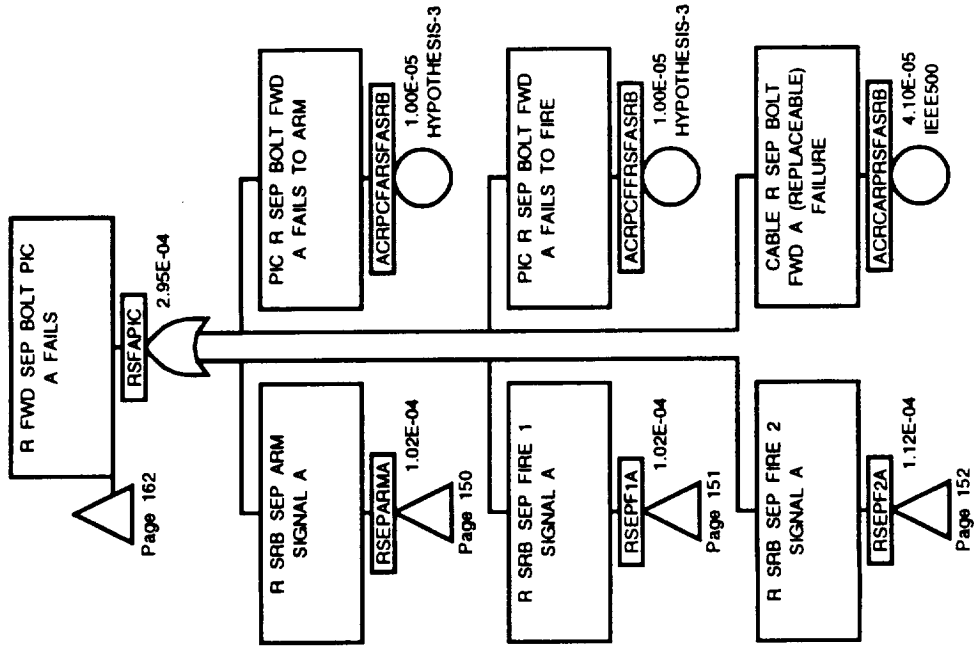


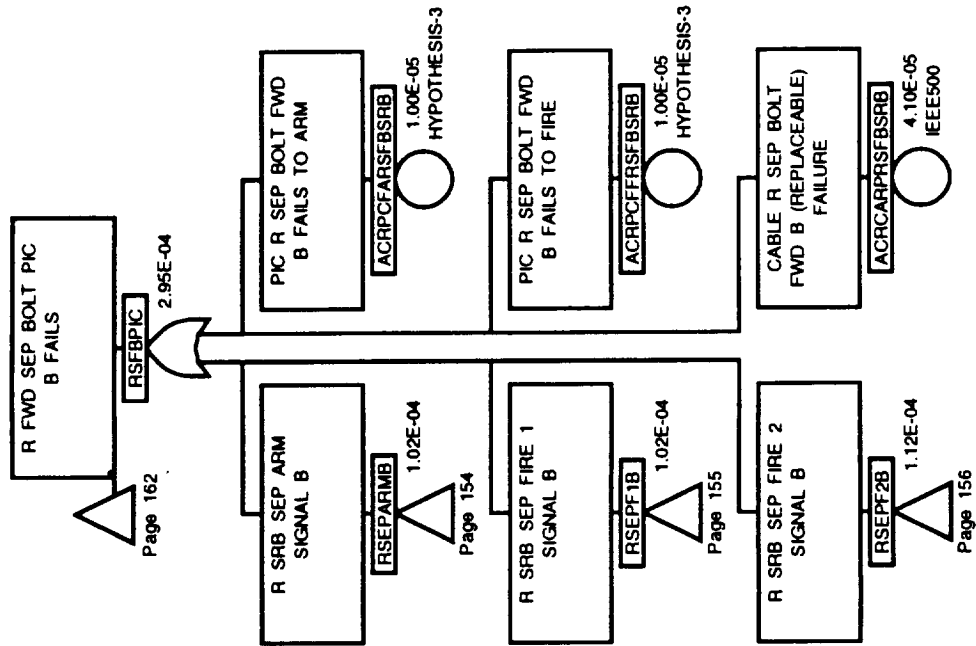


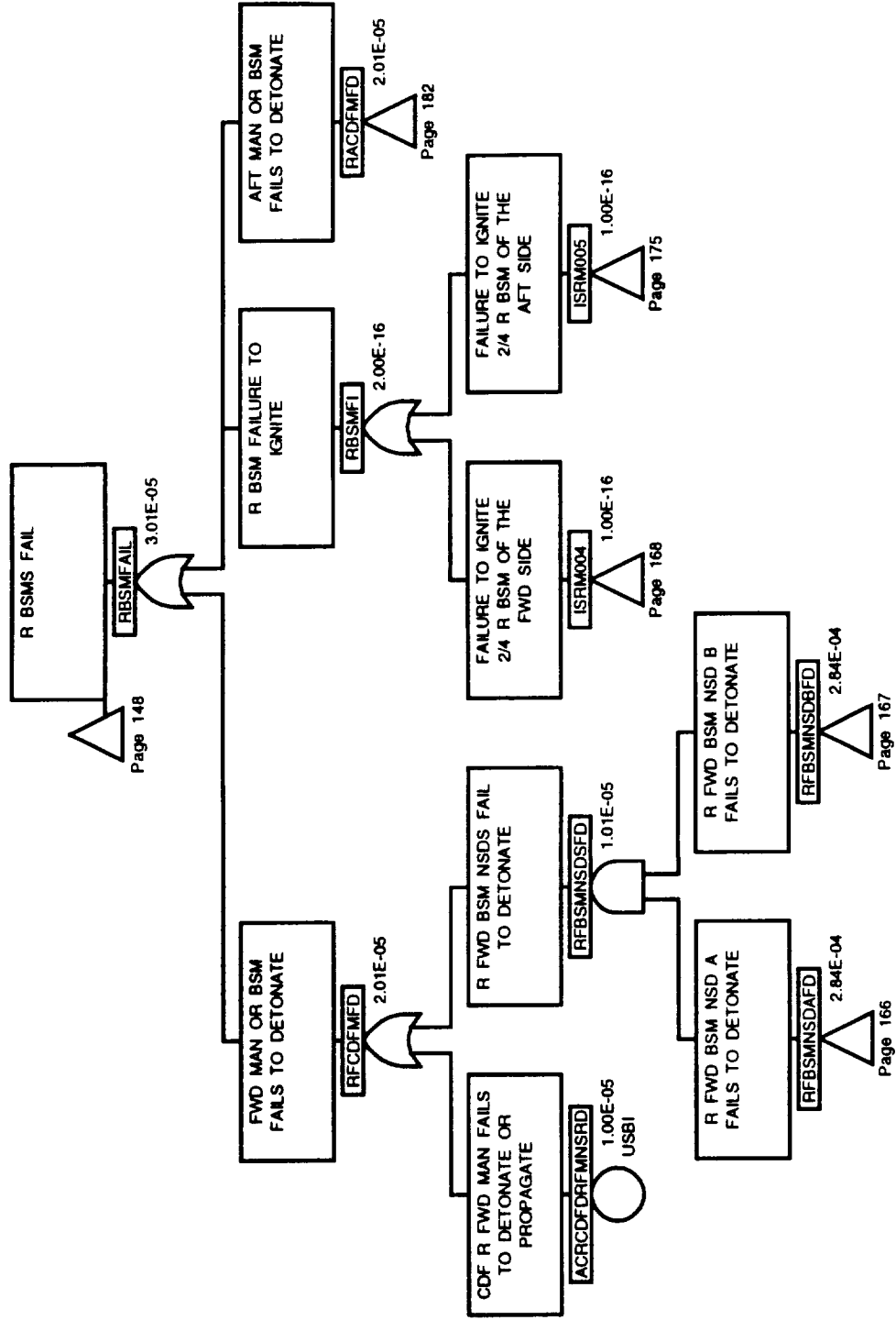
Page 148

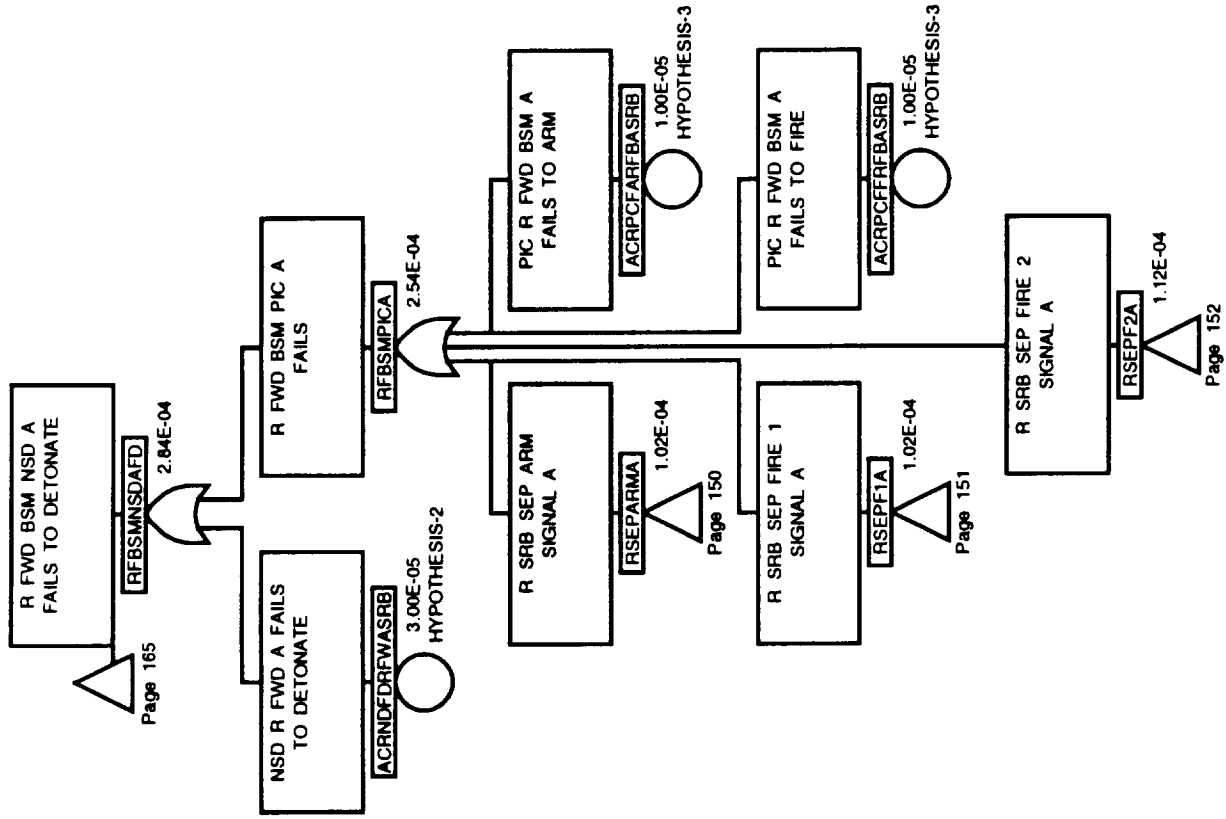
Page 163

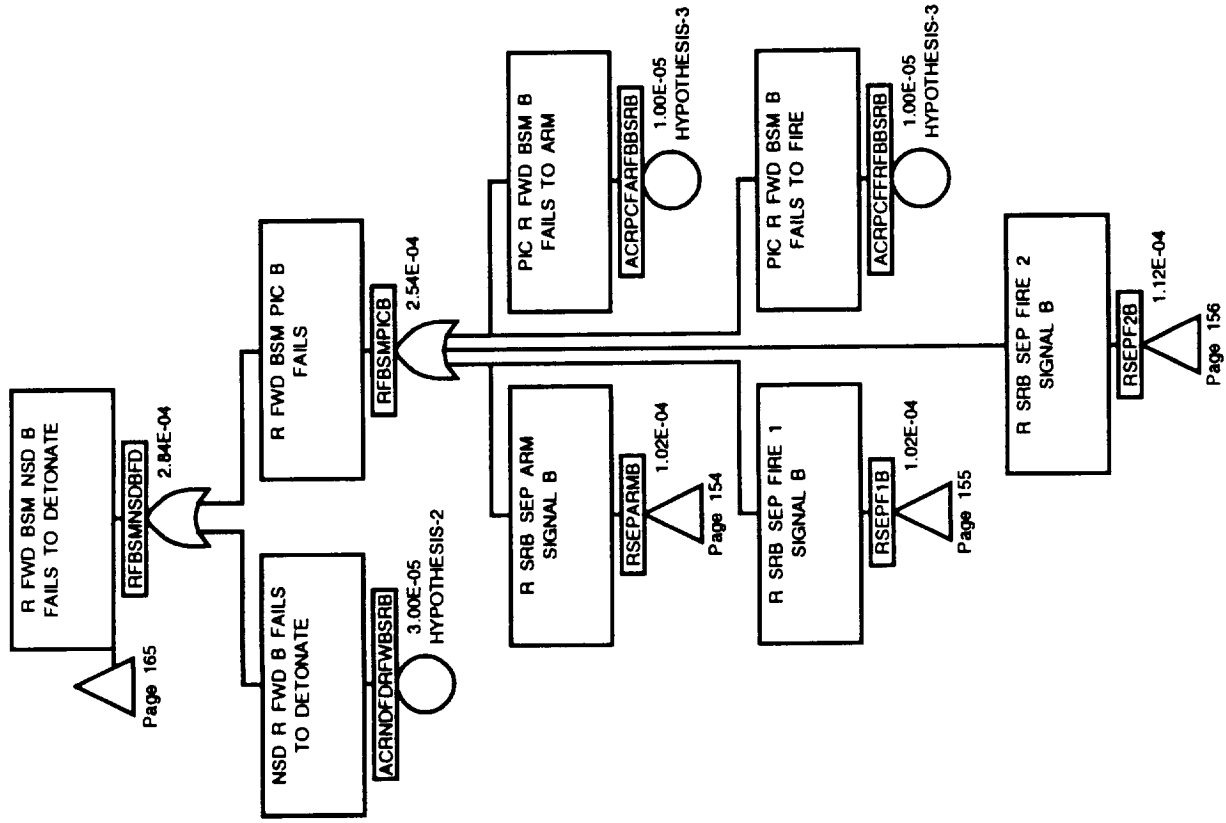
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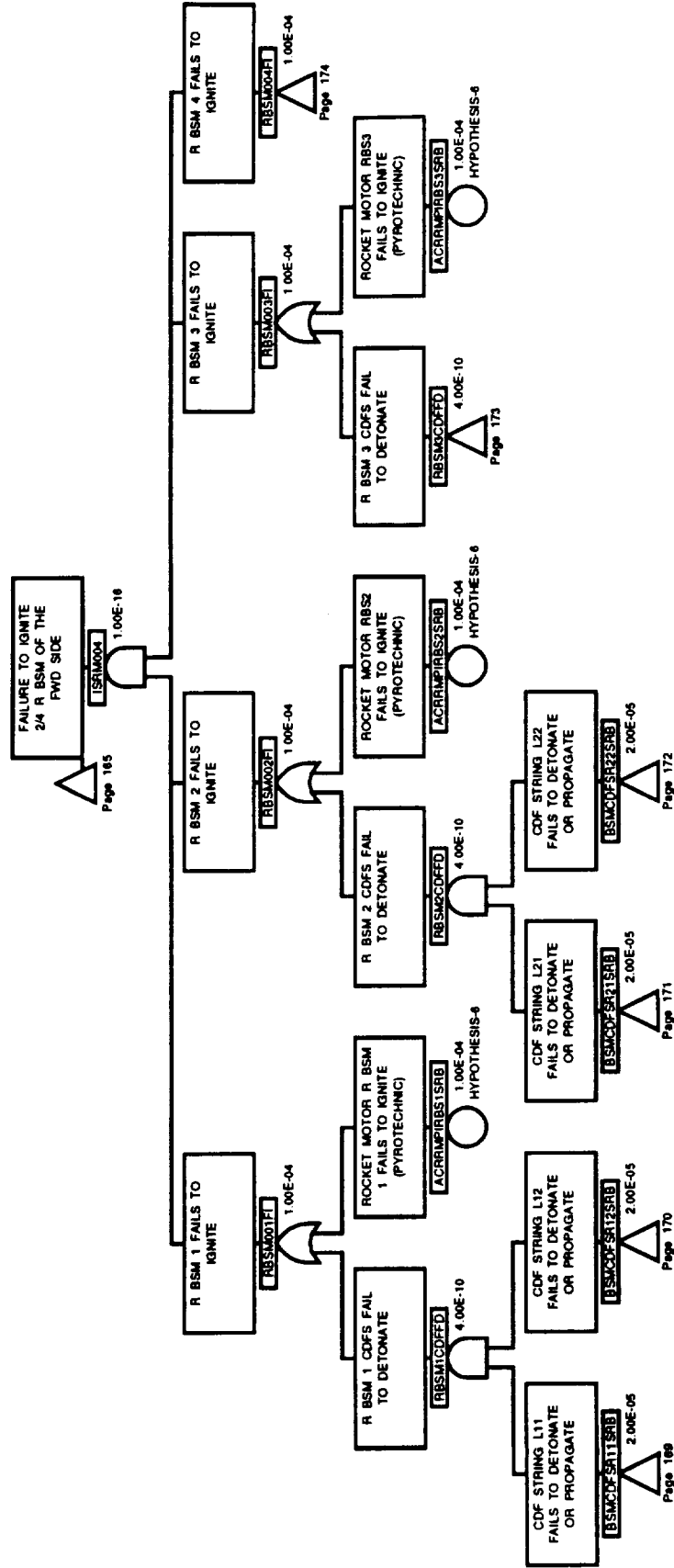


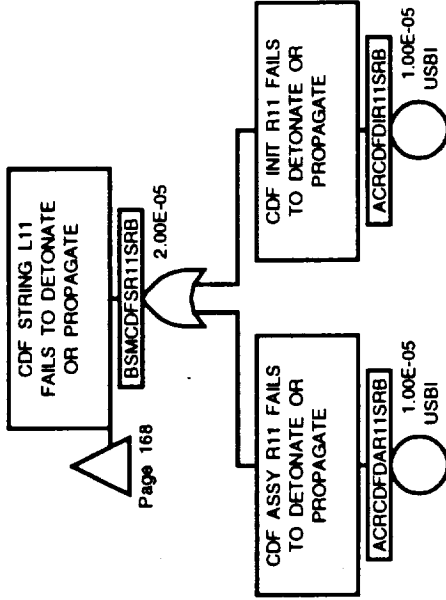




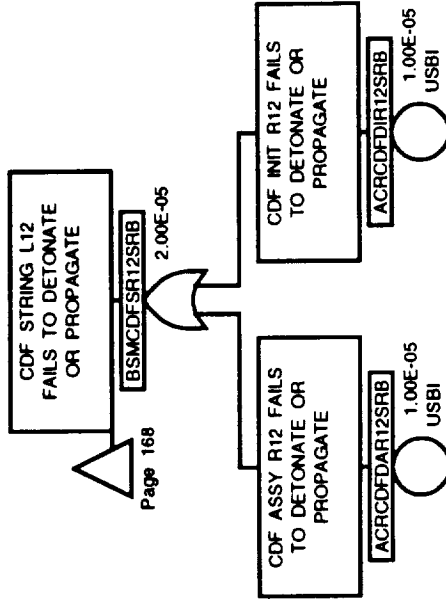




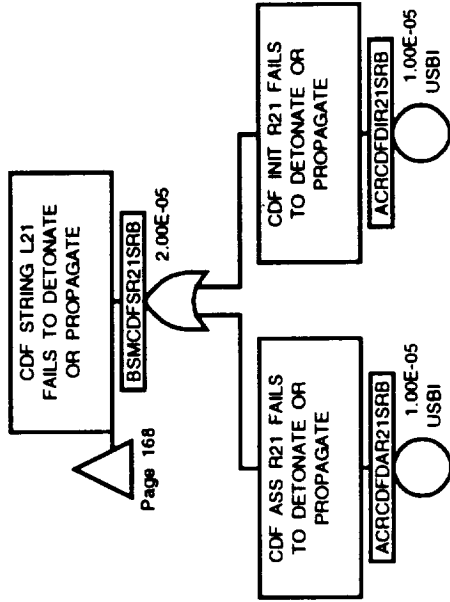




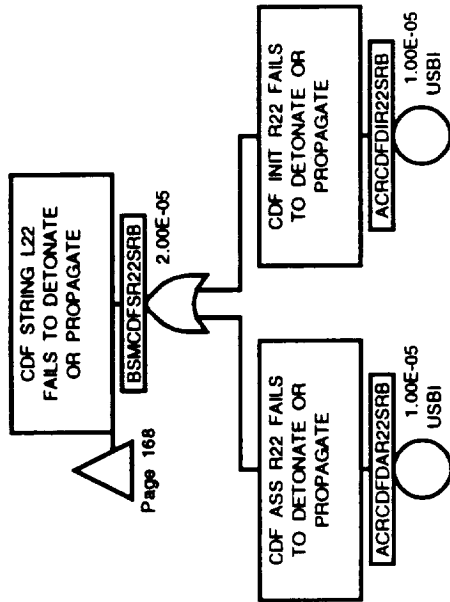
Page 168



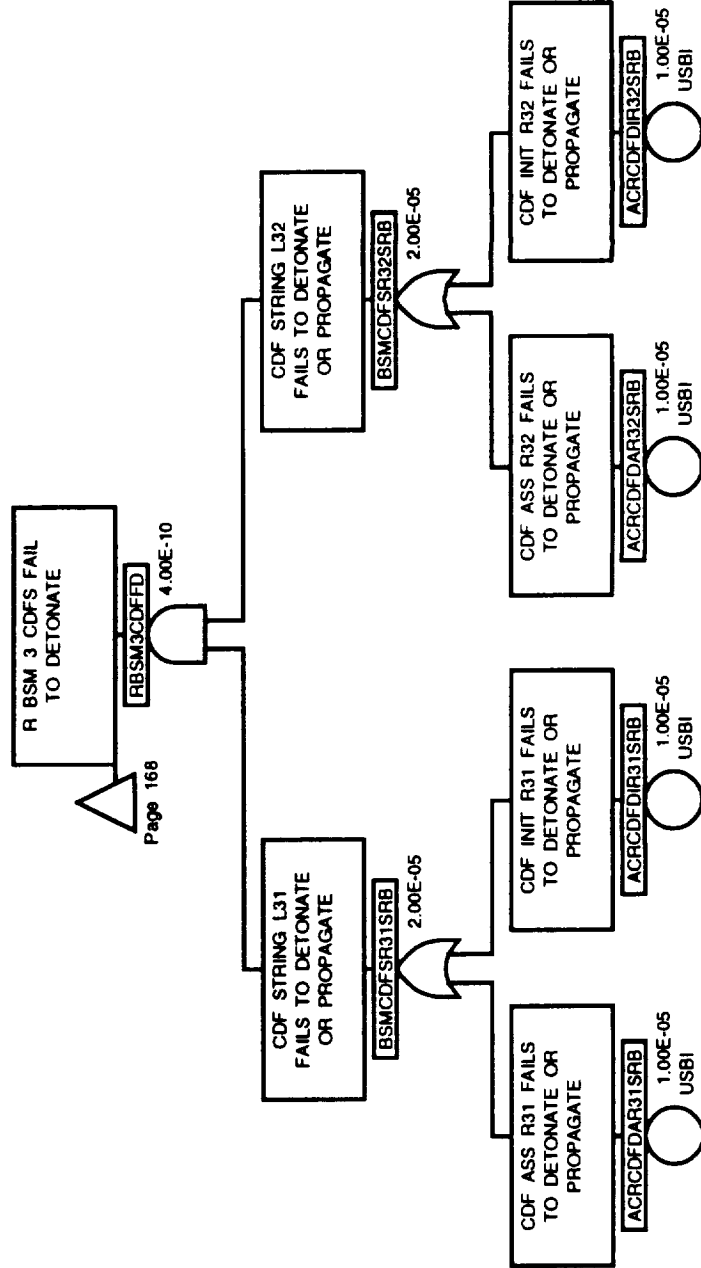
Page 168



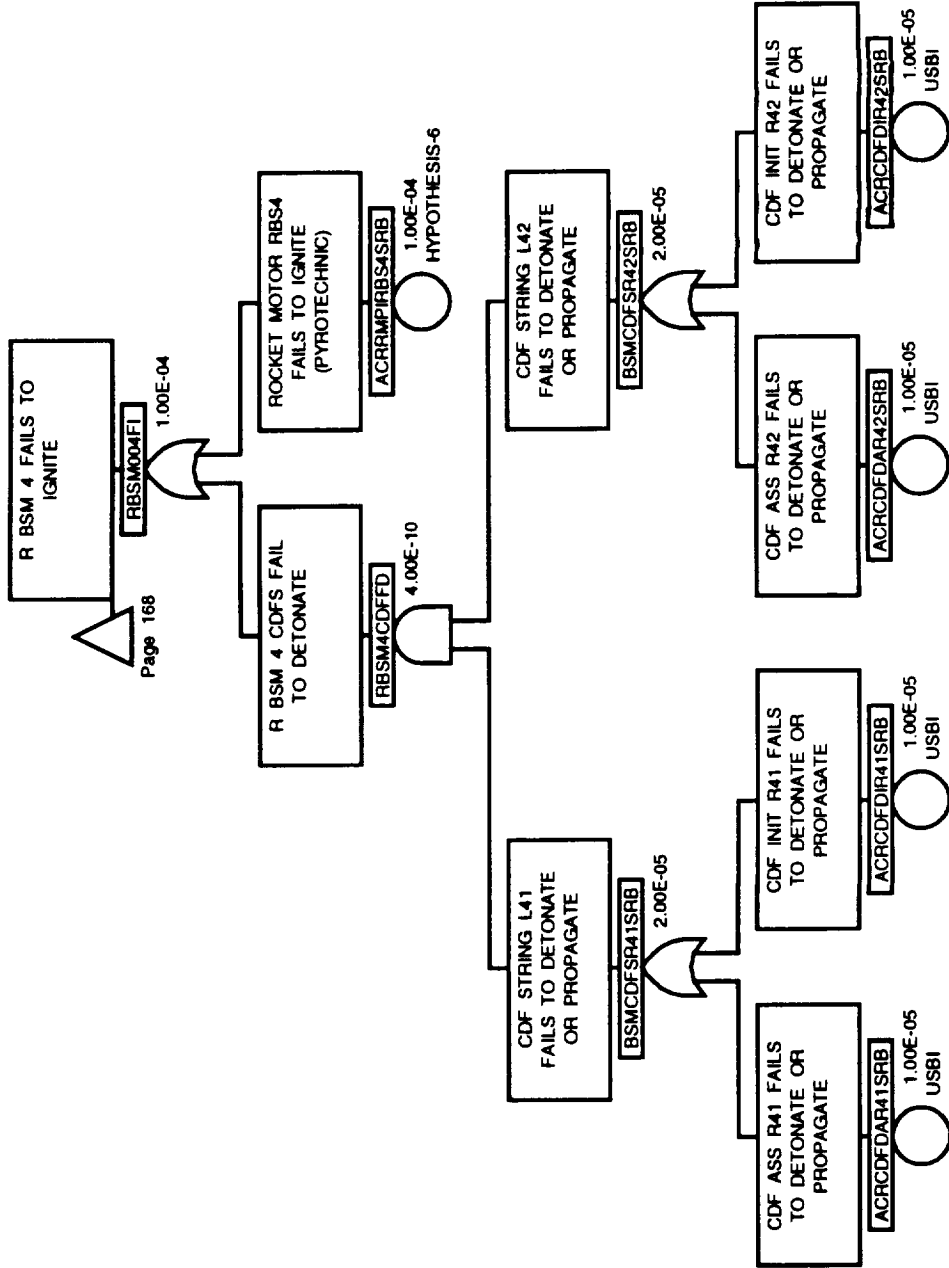
Page 168



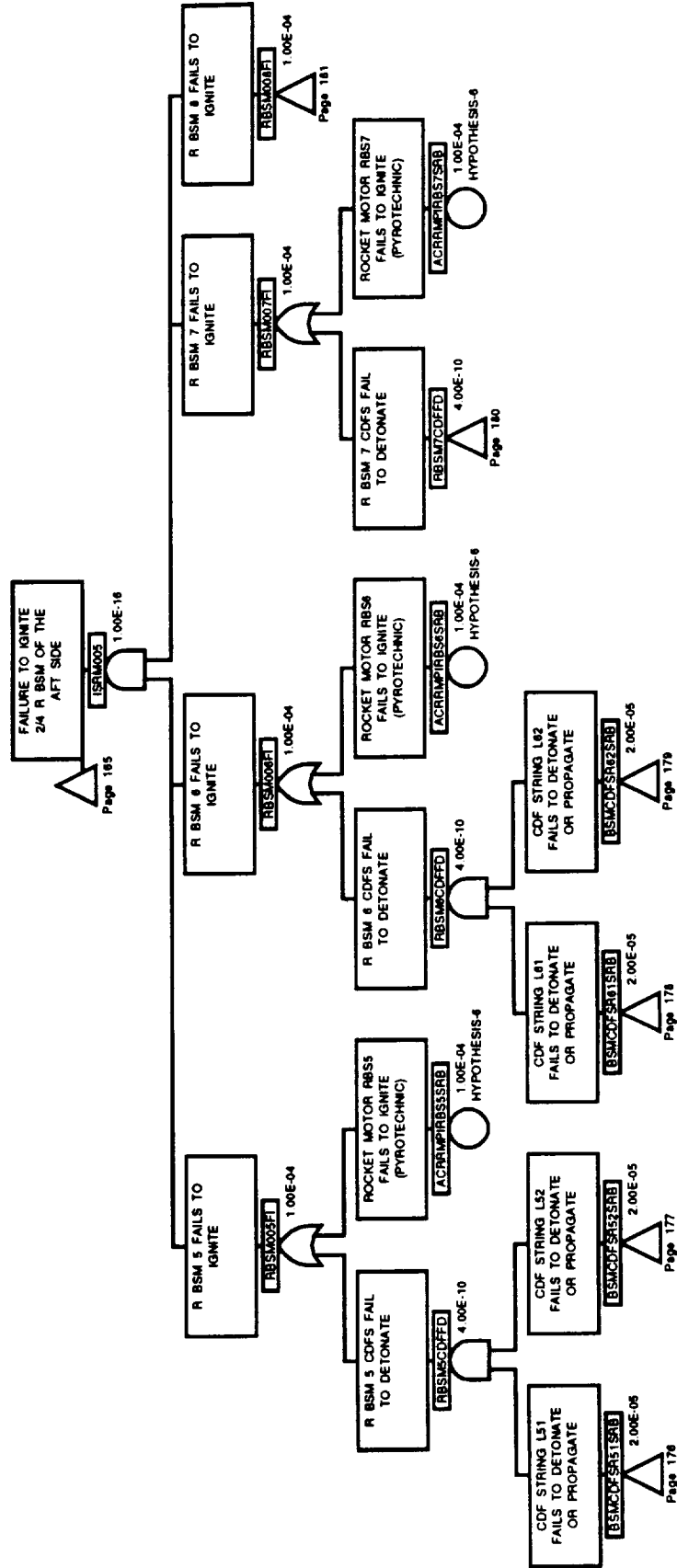
Page 168

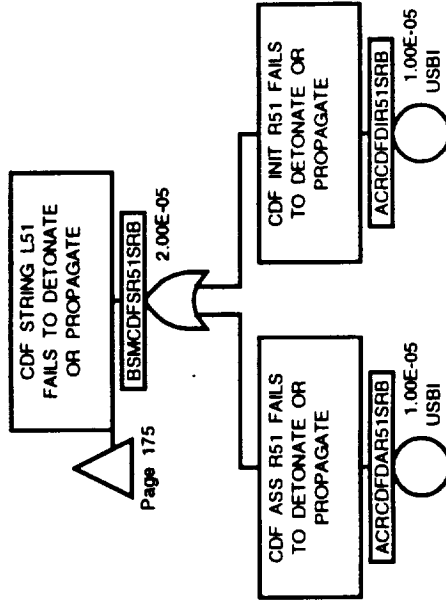


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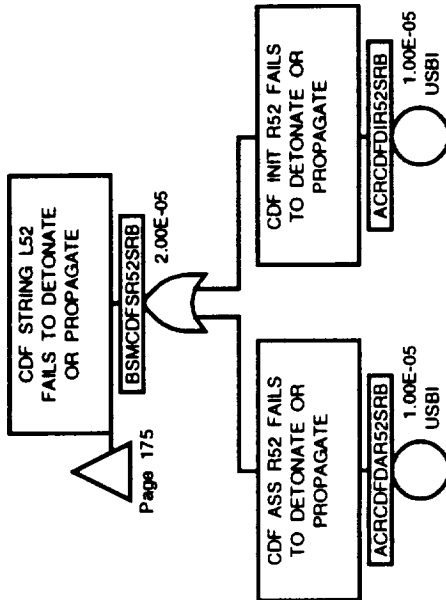


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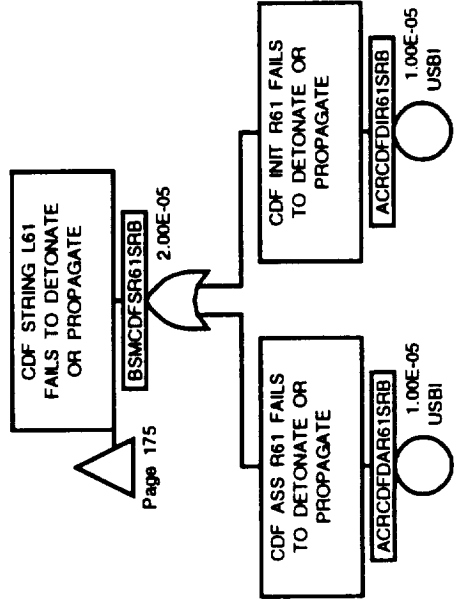




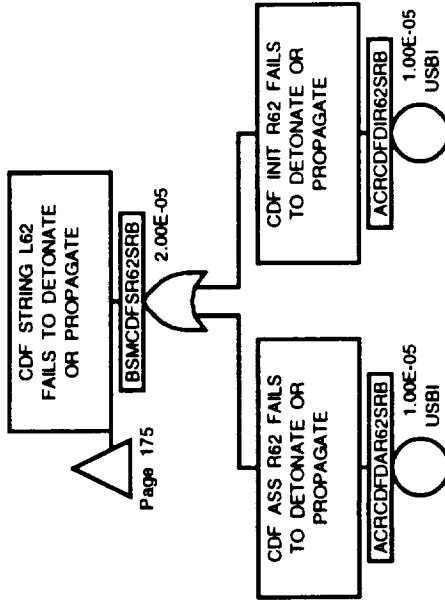
Page 175



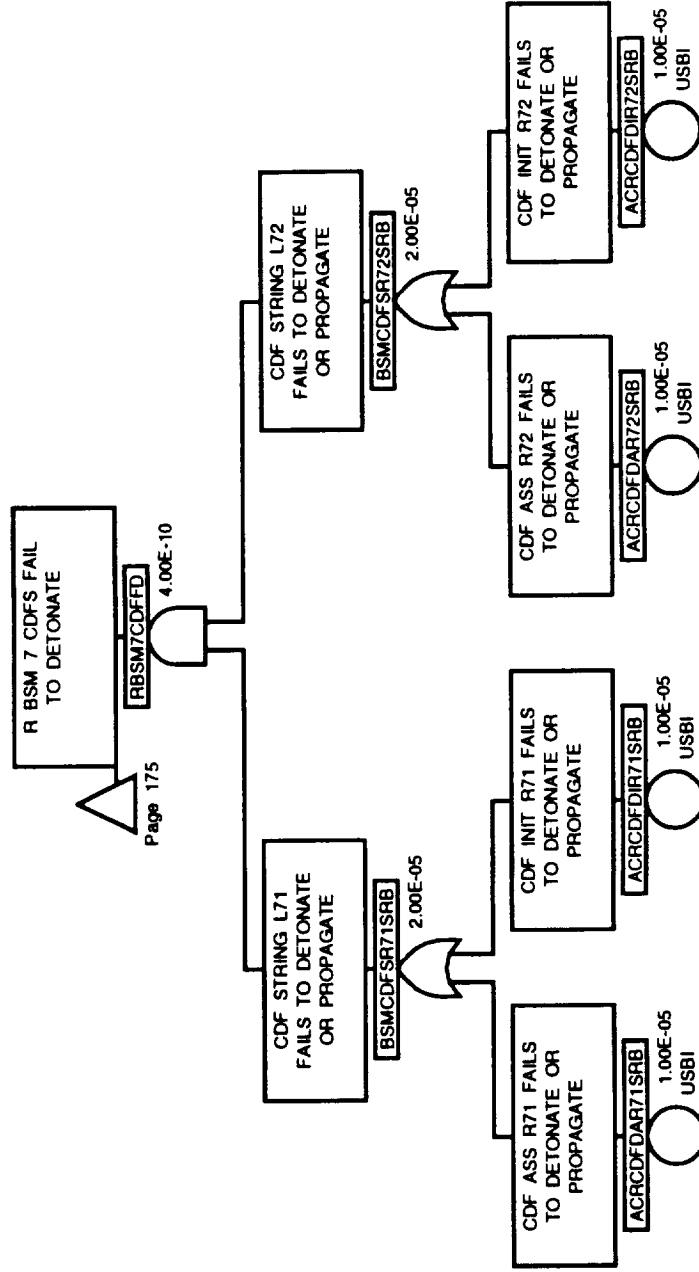
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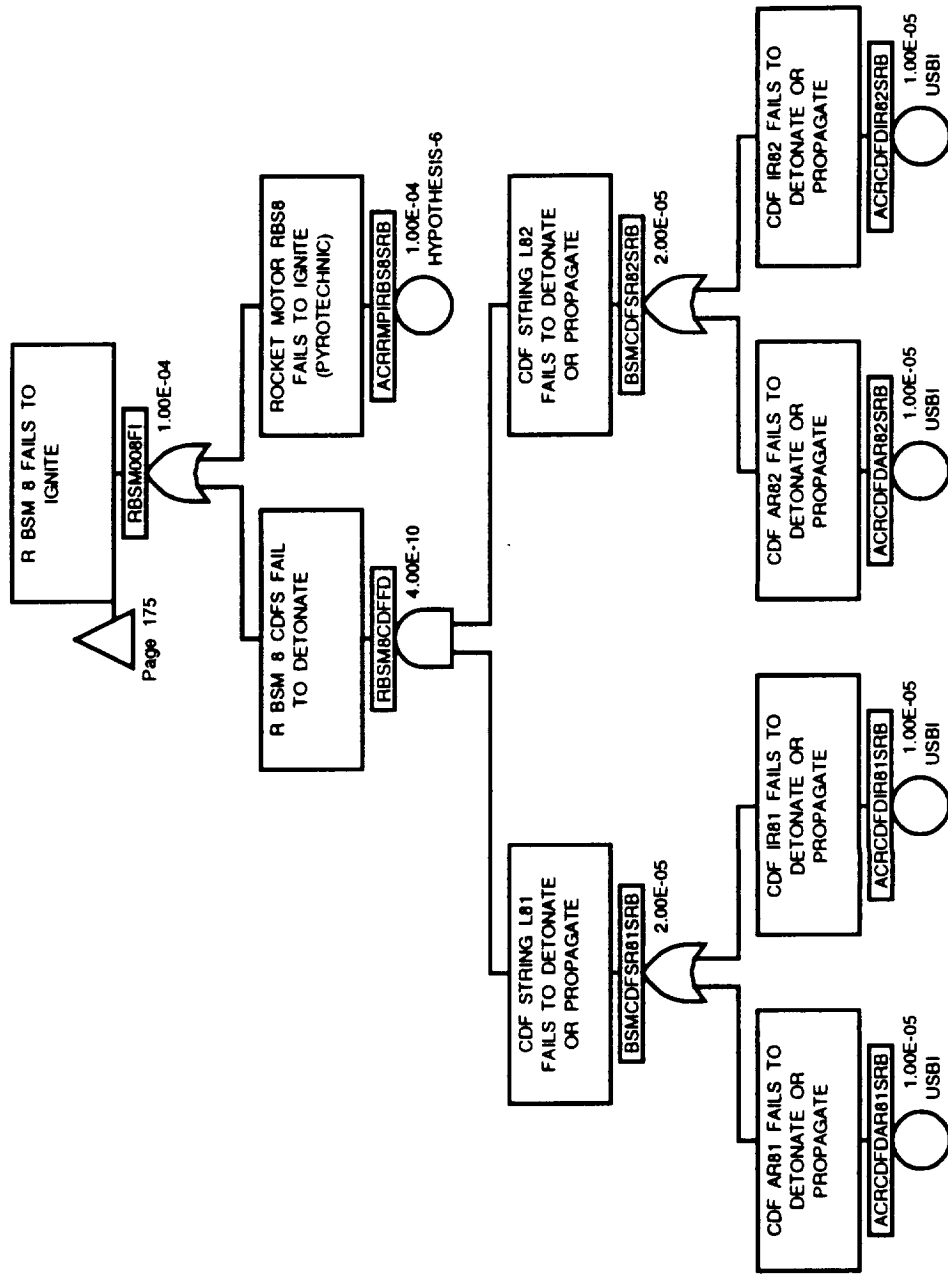
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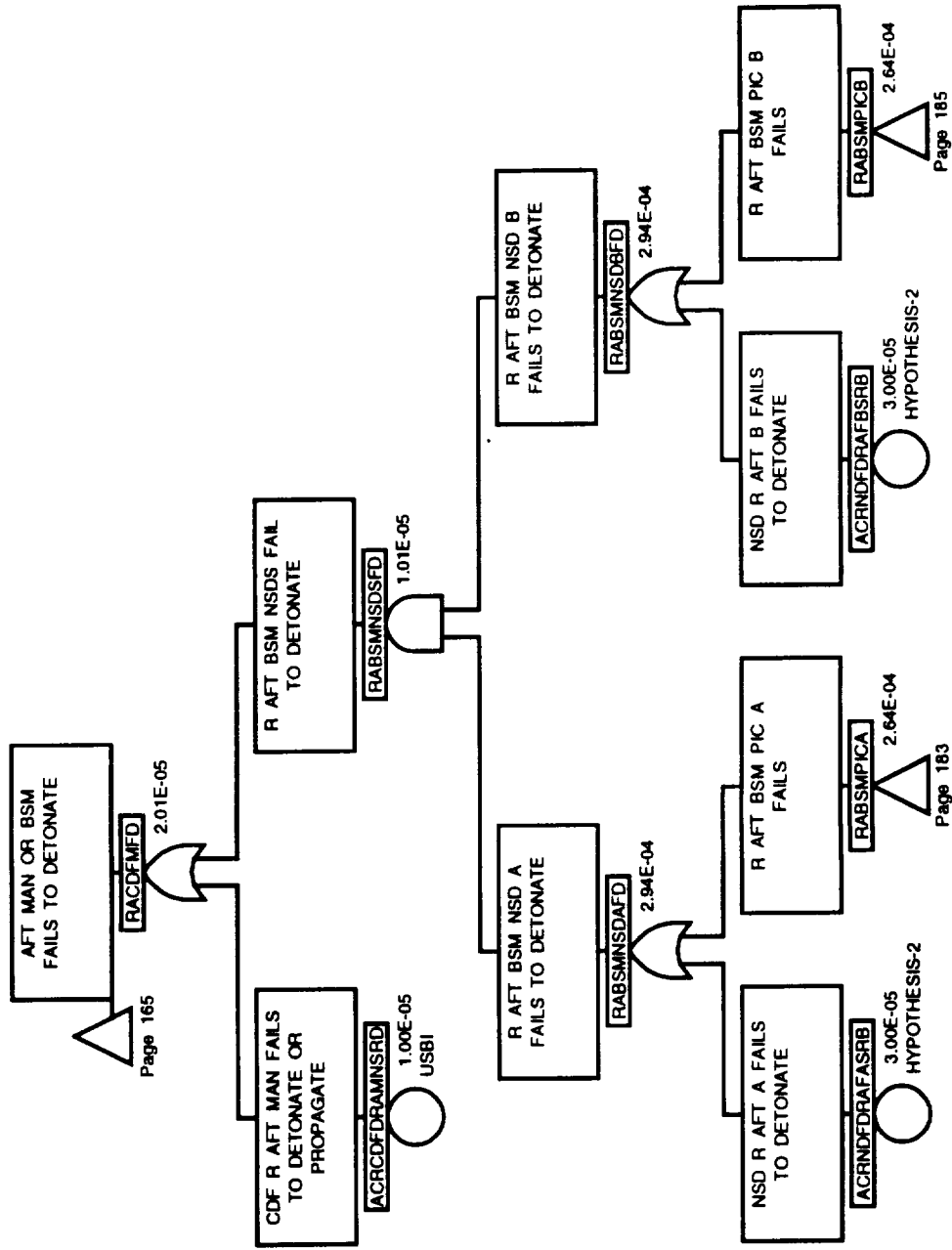
Page 175



Page 175



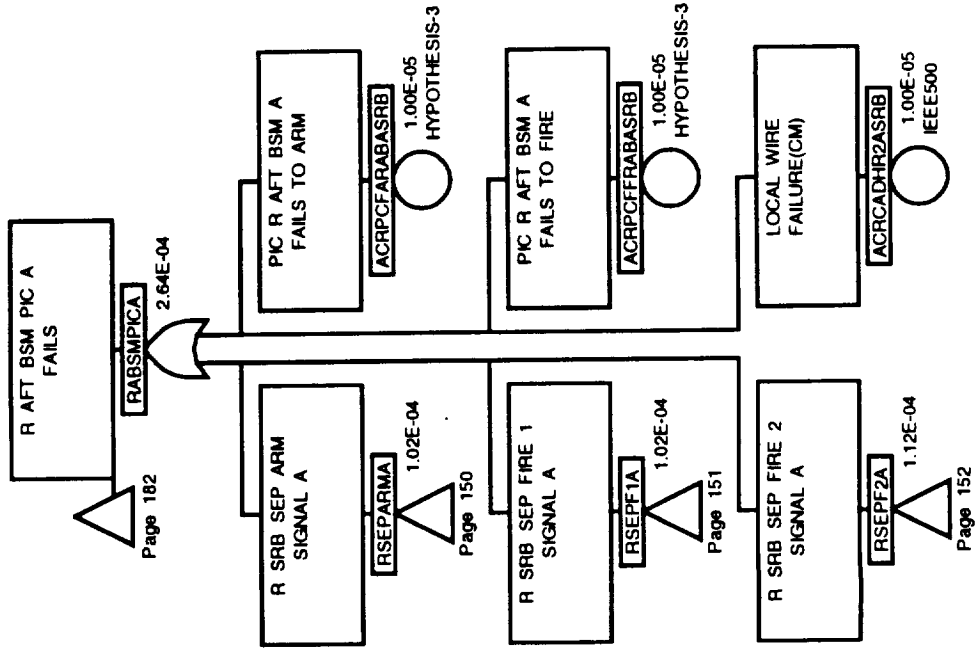
Page 175



Page 165

Page 183

Page 185

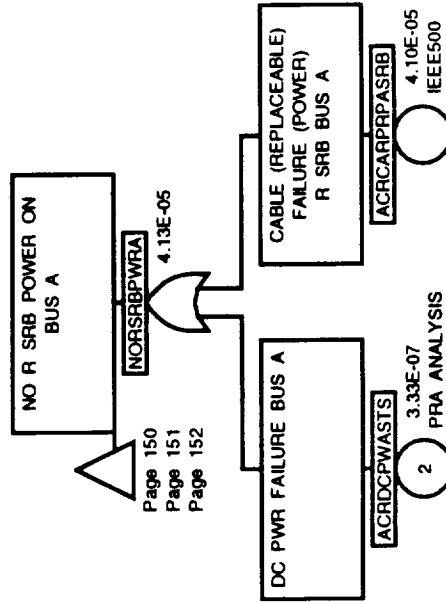


Page 182

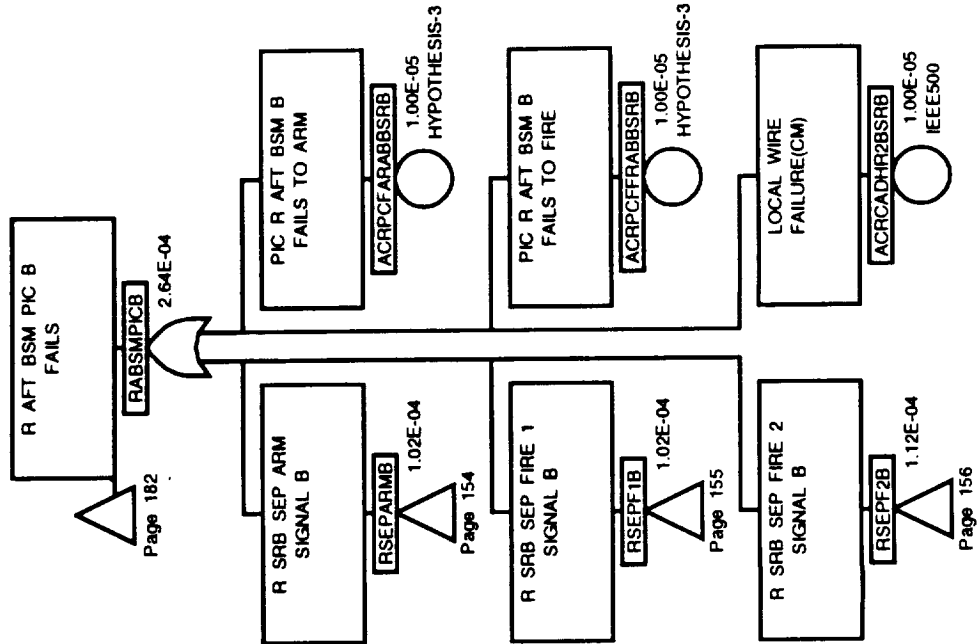
Page 150

Page 151

Page 152



Page 150
Page 151
Page 152

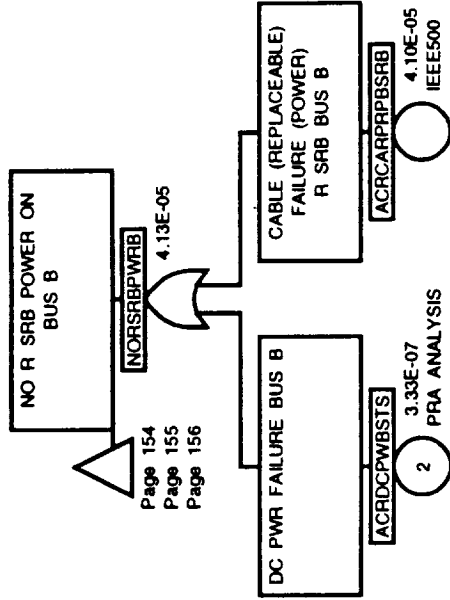


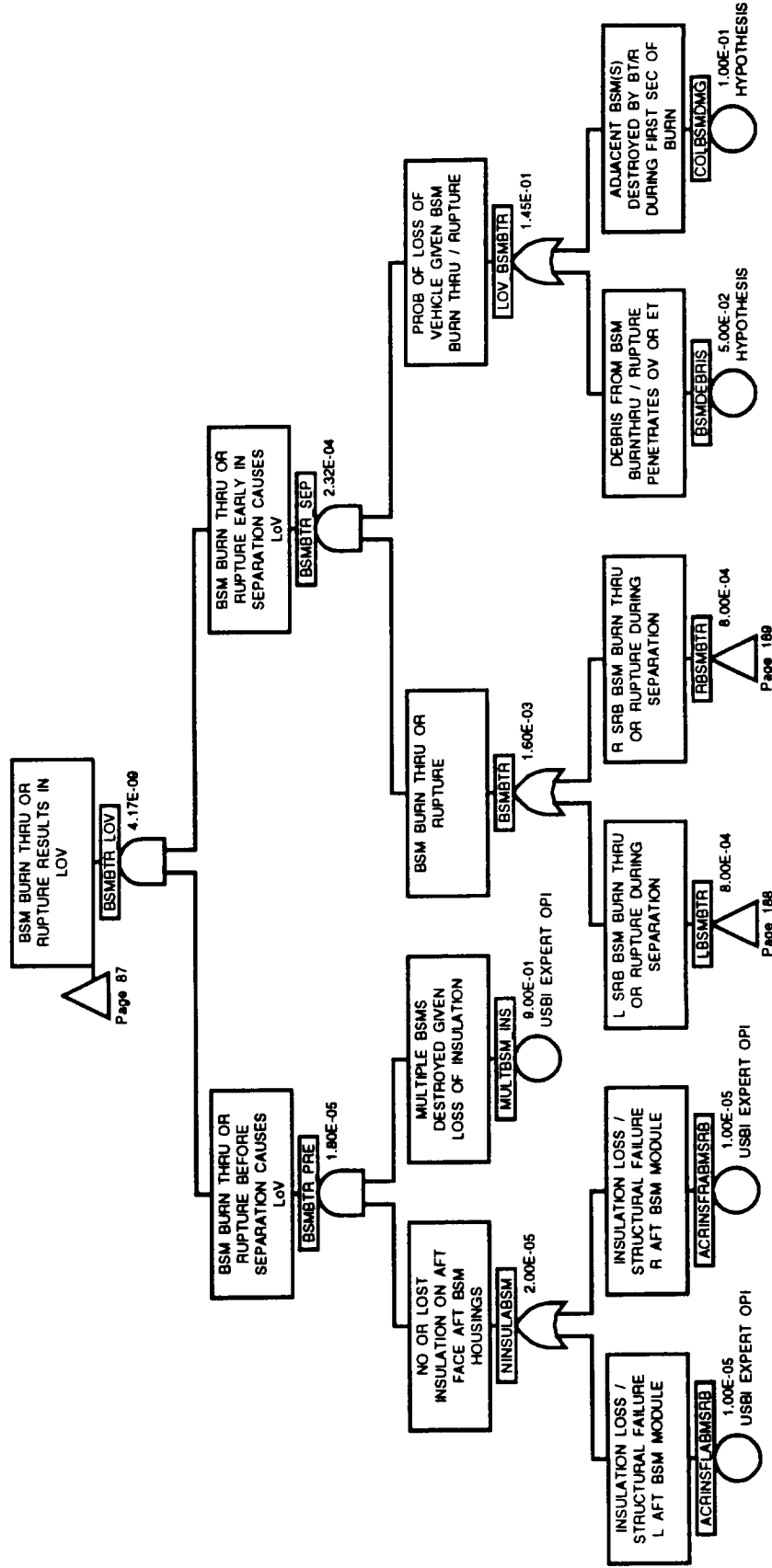
Page 182

Page 154

Page 155

Page 156

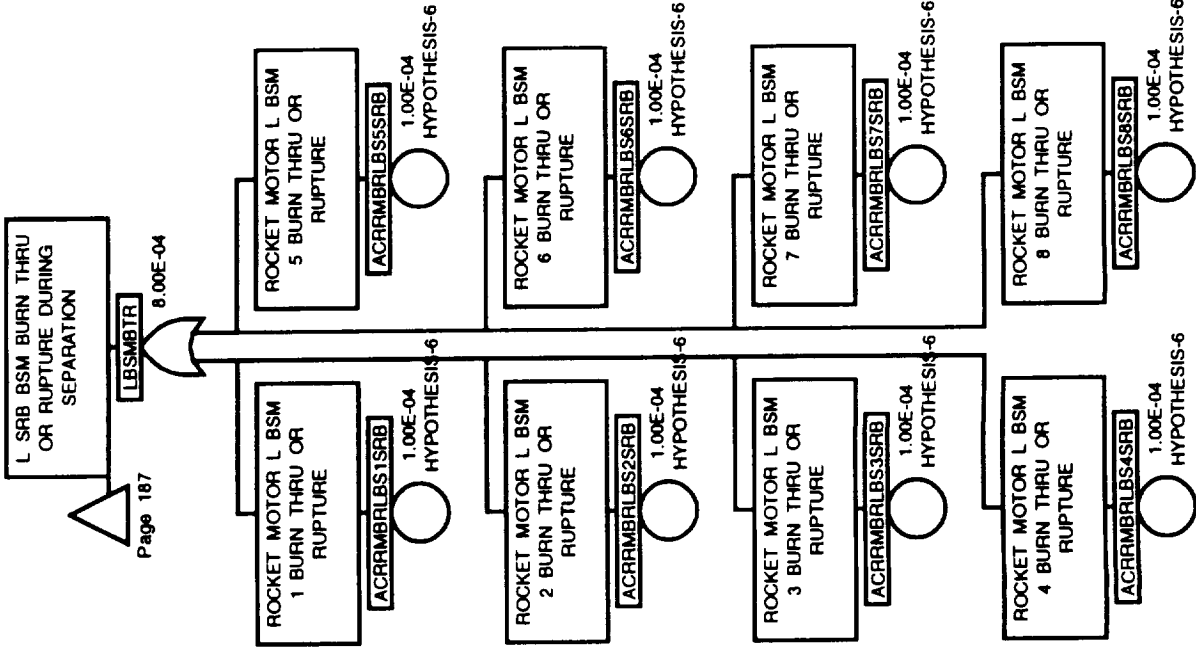




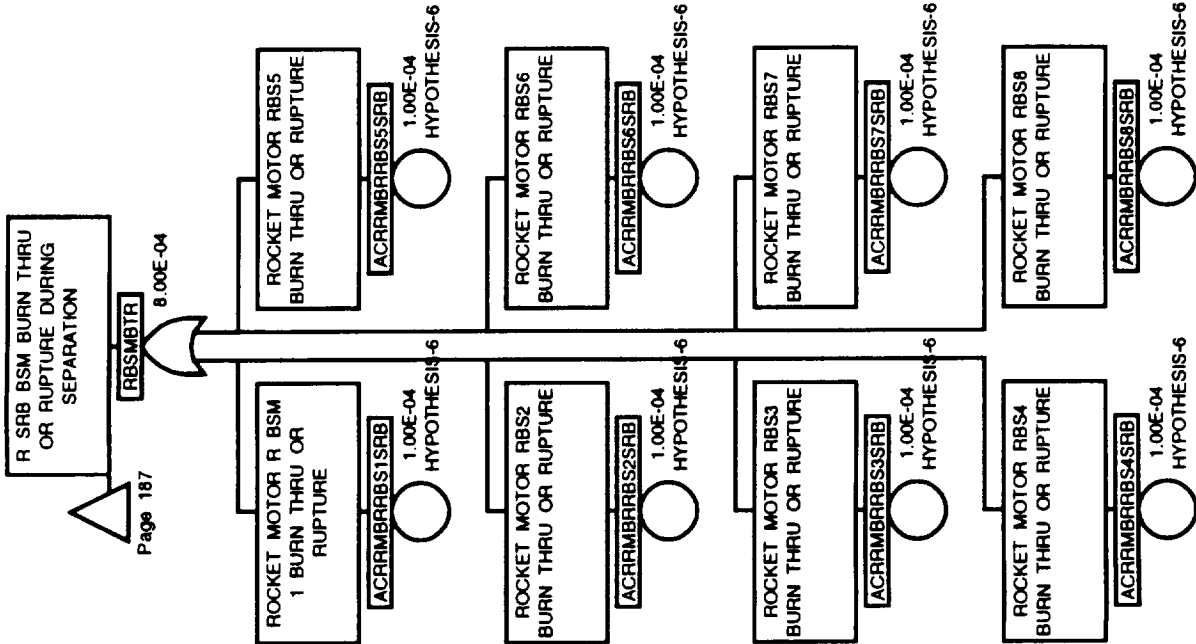
Page 87

Page 188

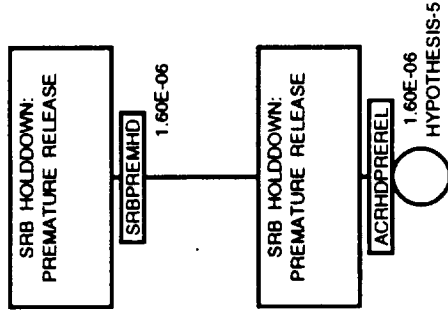
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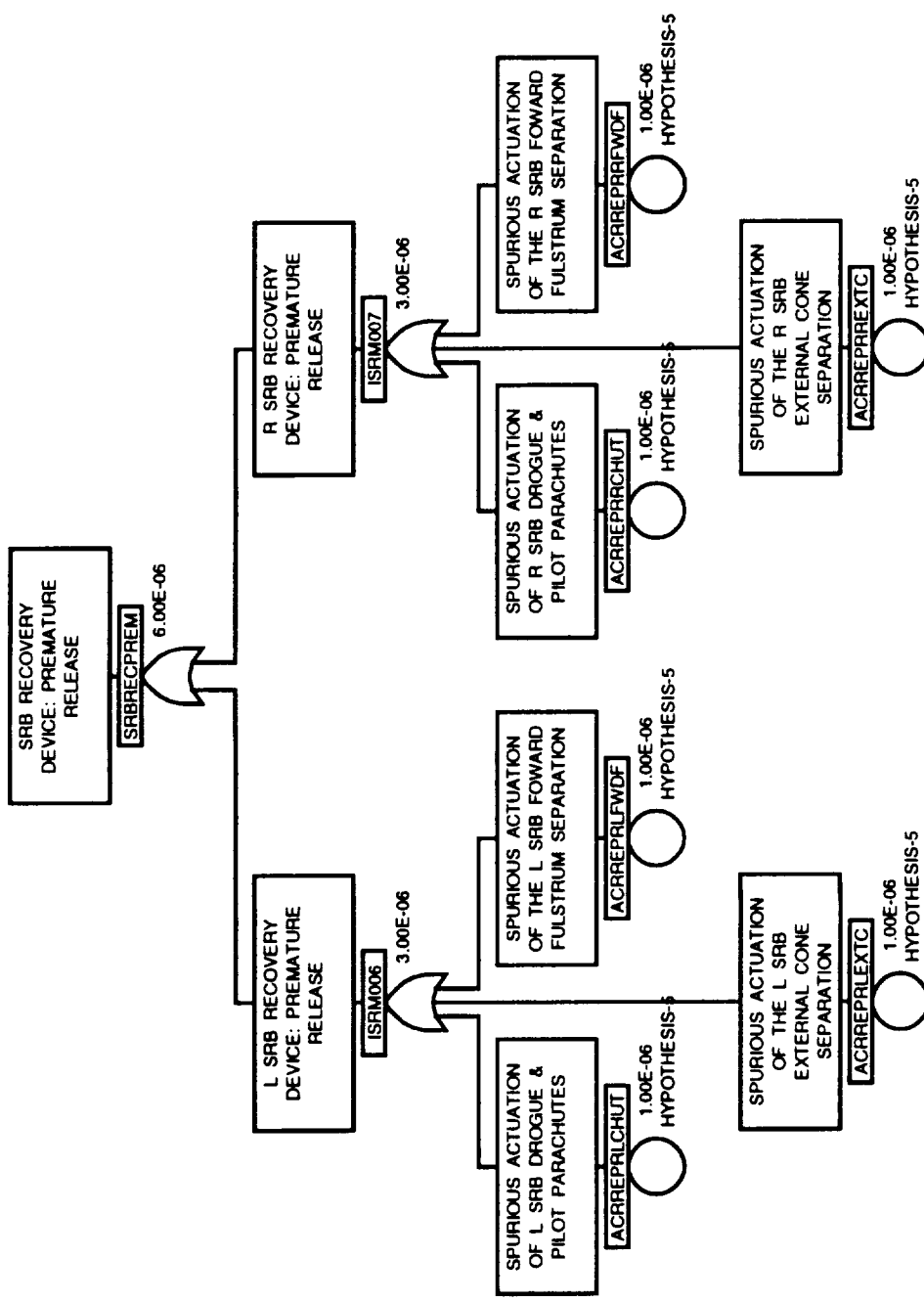


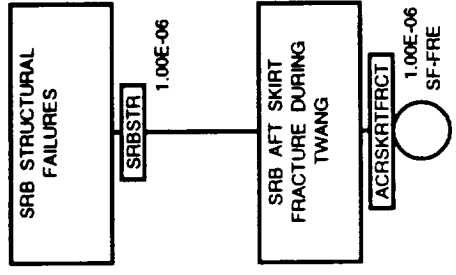
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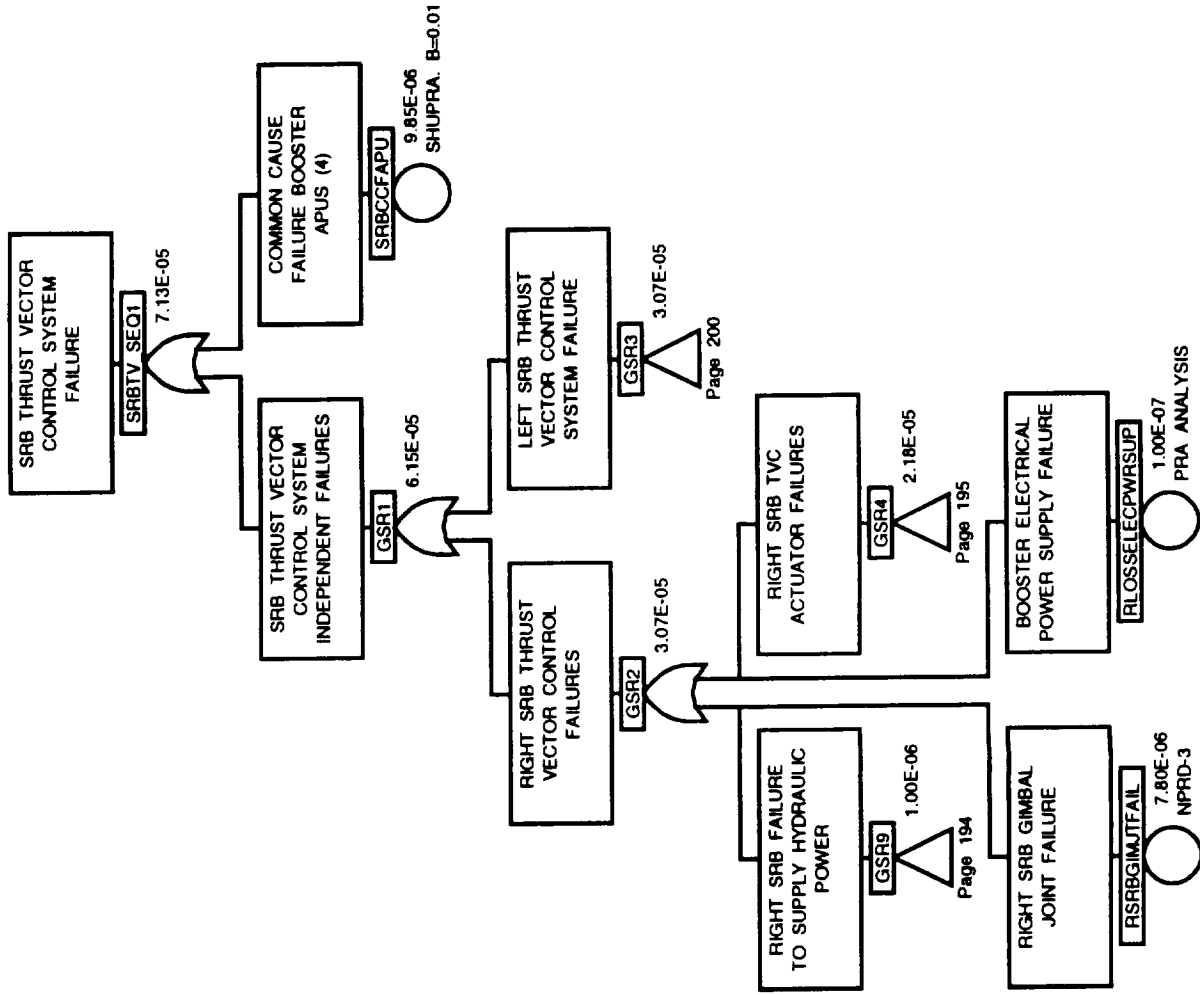


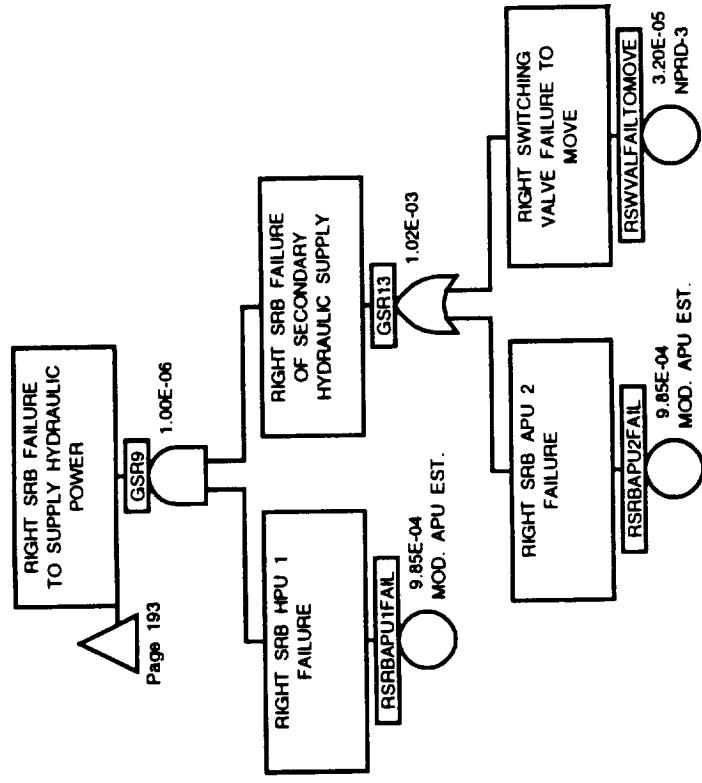
Page 187



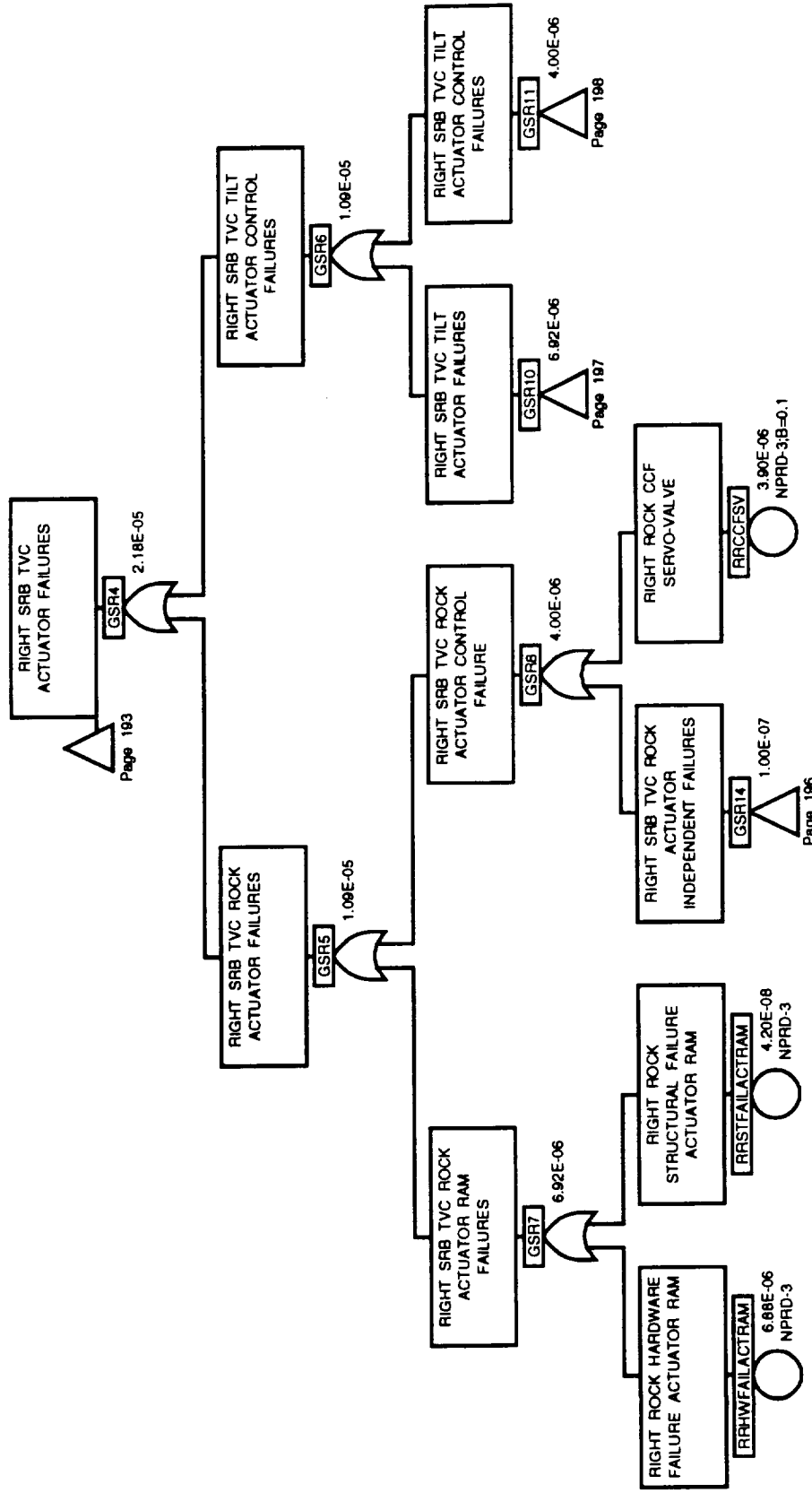


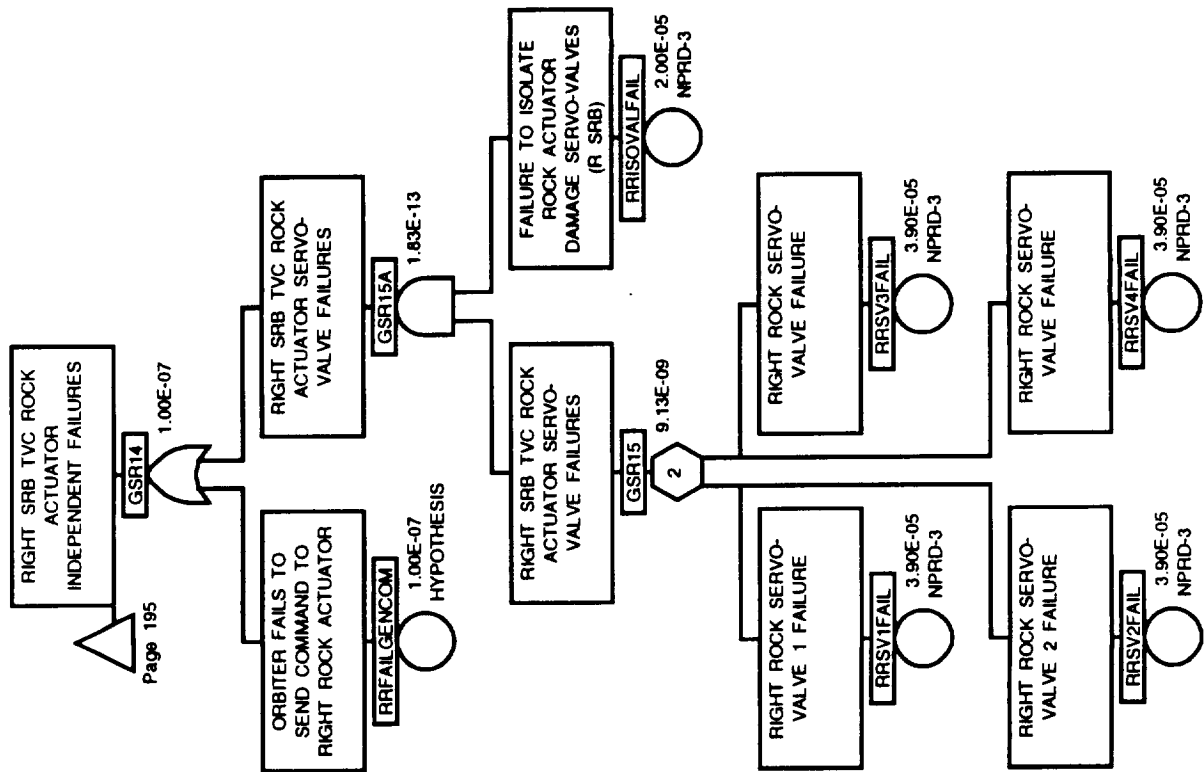




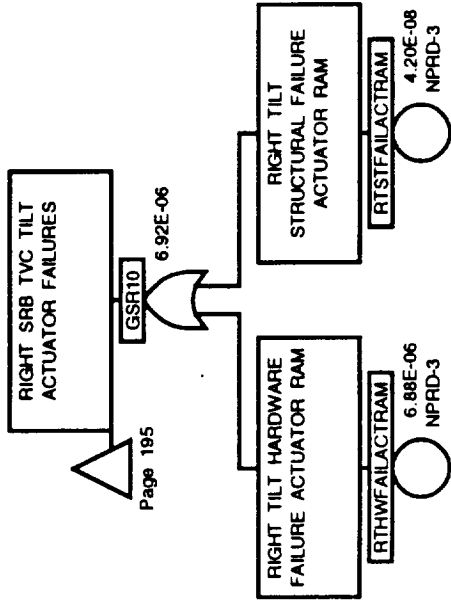


Page 193

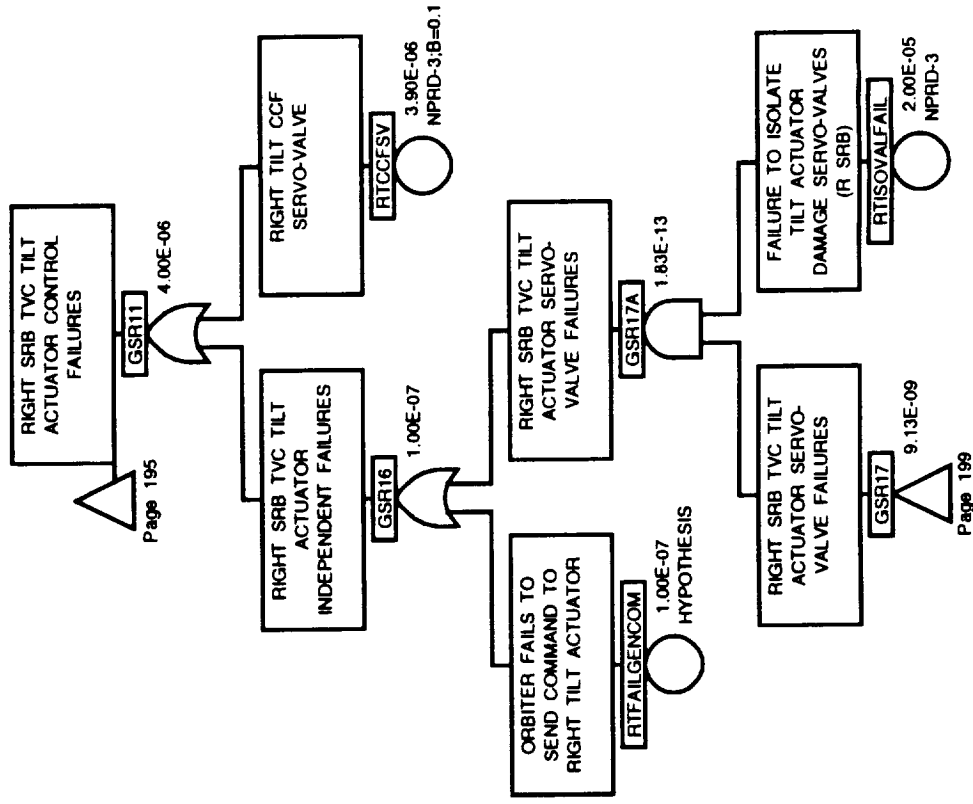




Page 195

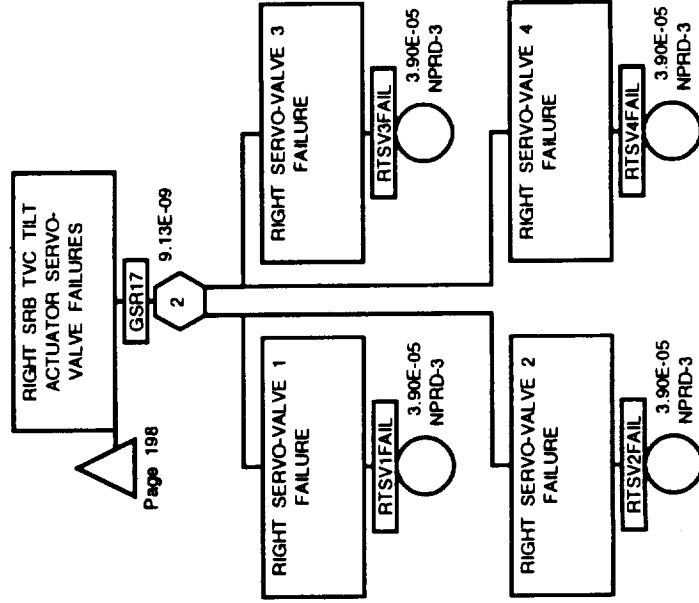


Page 195

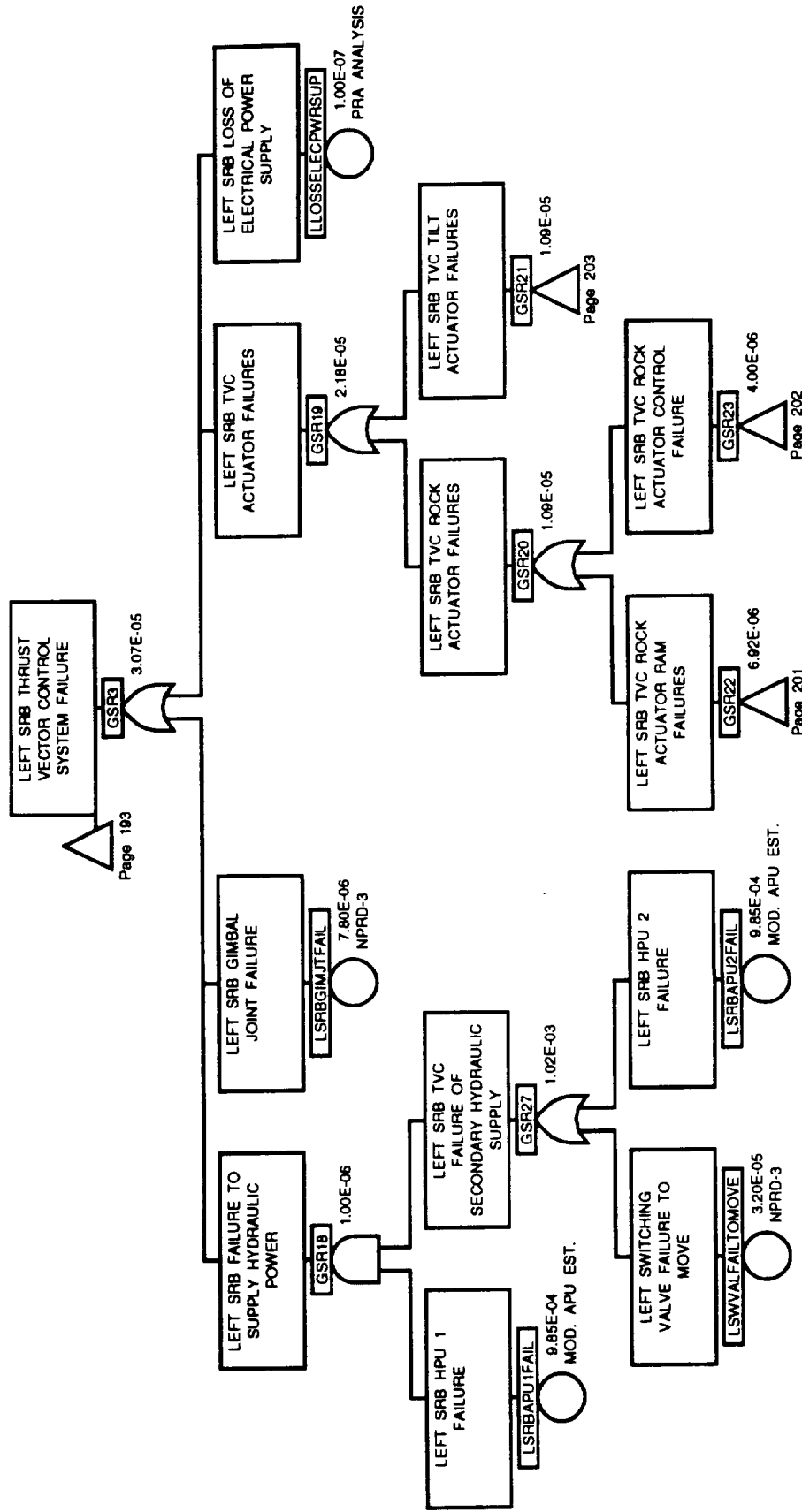


Page 195

Page 196



Page 198

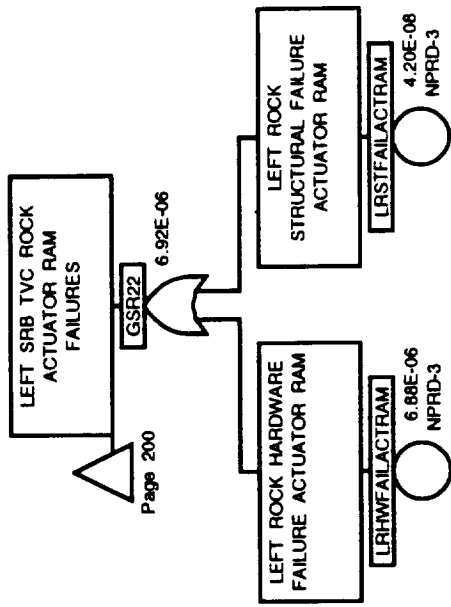


Page 193

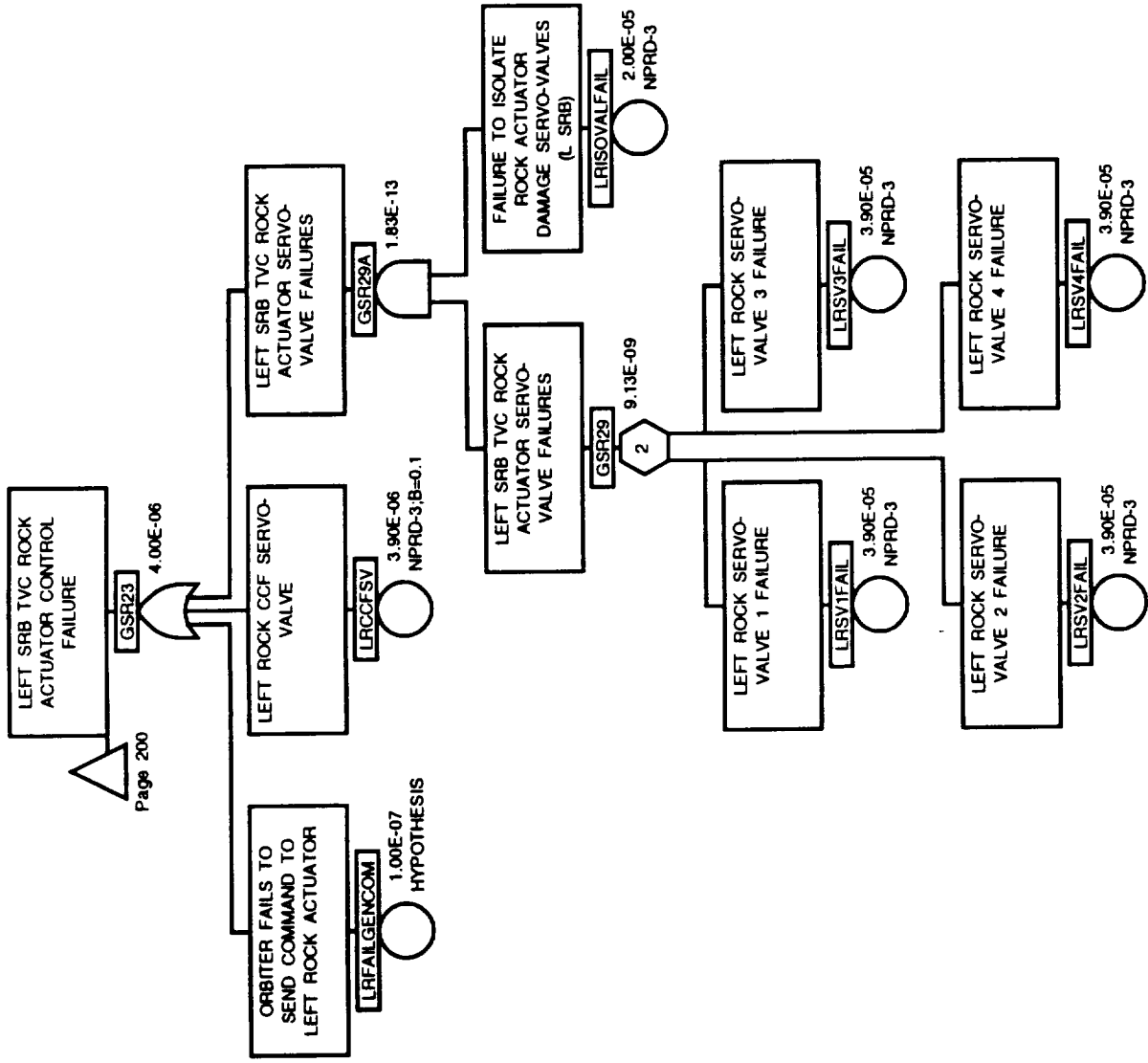
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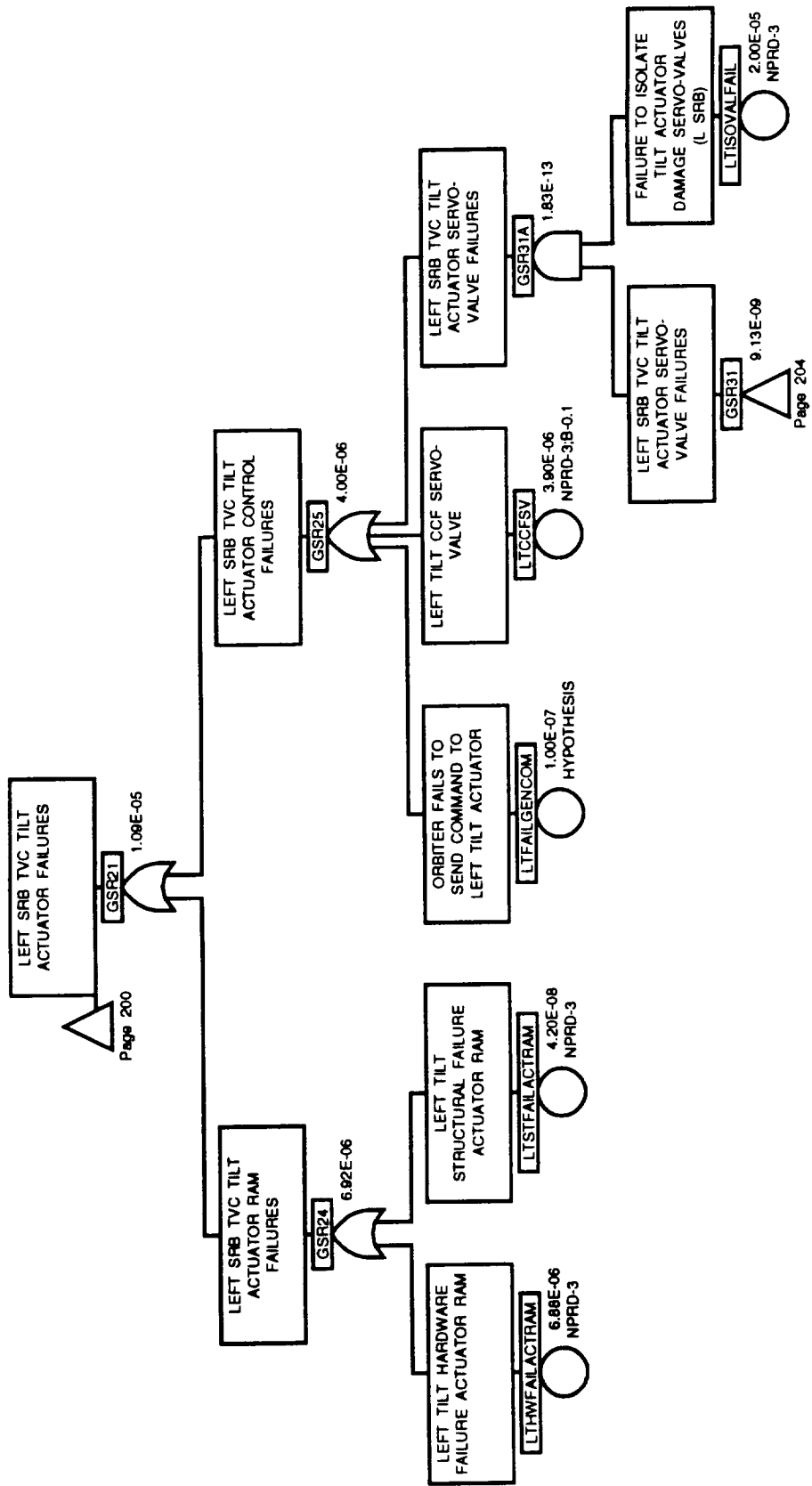
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Page 200

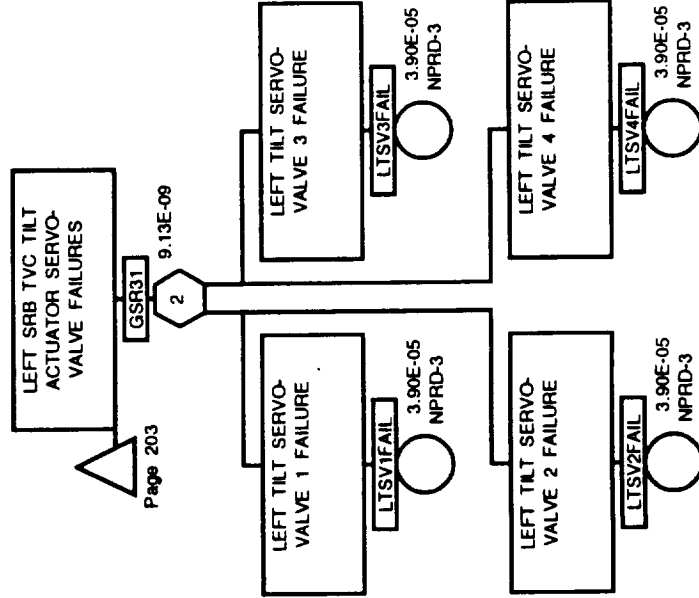


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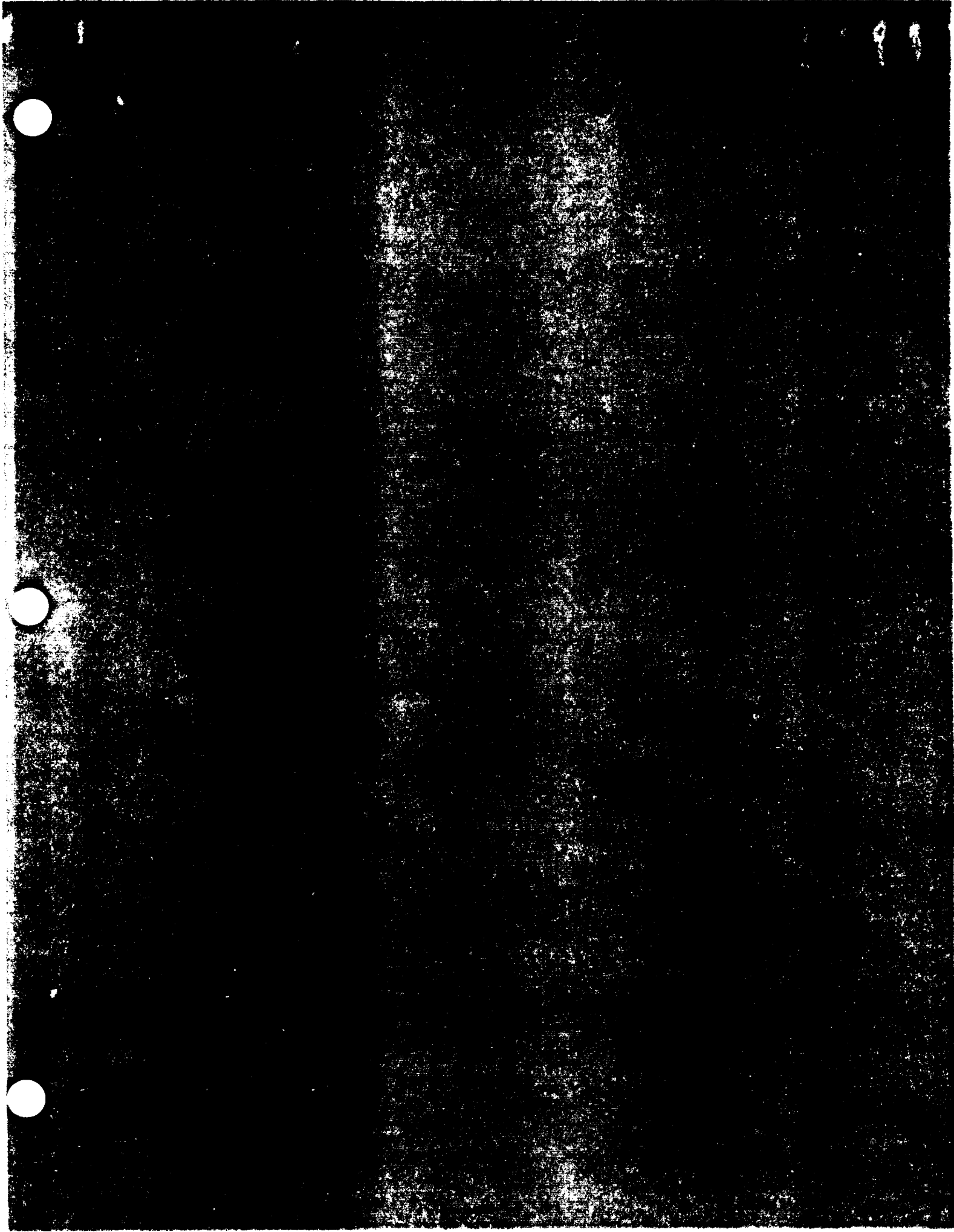


Page 200

Page 204



Page 203



SRB Component Data

COMPONENT	QTY/FLIGHT	# OF FLIGHTS	GROUND TESTS	TOTAL	FAILURES*
Frangible Nut	8	62	141	637	0
Booster Ctdg (Frangible Nut)	16	62	189	1181	0
NSI Pressure Cartridge	20	62	271	1511	0
CDF Manifold	18	62	292	1408	0
CDF Assembly**	56	62	838	4310	0
CDF Initiator	32	62	409	2393	***1
Booster Separation Bolt	16	62	104	1096	0
Forward Separation Bolt	2	62	77	201	0
Aft Separation Bolt	8	62	141	637	0
* Only failures which could lead to loss of vehicle are included.					
** Similar designs (at E.F., Inc.) have had over 75,000 successful firings with no failures					
*** Failure successfully screened by LAT, lot rejected at vendors's facility (not counted as flight failure)					
Additional CDF related information obtained from Explosive Technologies: 19,460 test firings with no failures					
CDF Failure Probability Estimate > $1 / (3 * (19460 + 2 * (4310) + 1408 + 2393)) = 1.05E-5$					

RSRM Joint Leak Data

NOZZLE-TO-CASE JOINTS

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
Polysulfide	Flights 1-37,39,41	78			5
	Static Tests	9			1
	Totals:	87			6
Wiper O-Ring	Flights 1-37,39,41	6	78		
	Static Tests	1	9		
	NUES/TPTA,QM6	1			
	Totals:	8	87	0.2	1
Vent Port Plug Primary O-Ring (nozzle and case combined) (47 motors counted as 23 tests)	Flights 1-37,39,41		234		
	Static Tests		30		
	TPTA 1.3,2.1,2.2	7			
	NUES/JES 3C	4			1
	SPC (70lb Motor)	23	23		
	Totals:	34	287	0.9	1
Vent Port Plug Second O-Ring (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1,2.2	3			
	NUES/JES 3C	3			
	Totals:	6	352	0.9	0
Closure Vent Port Plug (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1	2			
	NUES/JES 3C	2			
	Totals:	4	352	0.6	0
Primary O-Ring	Flights 1-37,39,41		78		
	Static Tests		9		
	TPTA 1.2,2.1	2			
	NUES 3A,PVM1	2			
	Totals:	4	87	0.6	0
Leak Check Port Plug (case/nozzle/igniter combined)	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fid)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0
Stat-O-Seal	Case	100	9000		
	Igniter		5040		
	Nozzle	100	6776		
	Totals:	200	20816	0.9	0
Secondary O-Ring	Flights 1-37,39,41		78		
	Static Tests		10		
	TPTA 1.3	1			
	NUES 3B	1			
	Totals:	2	88	0.9	0

RSRM Joint Leak Data

IGNITER INTERNAL JOINTS

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
S&A Primary Gasket	Static Tests	12	12		
	SRM, HPM, RSRM	128	128		
	Totals:	140	140	0.6	0
S&A Secondary Gasket	Static Test		12		
	SRM, HPM, RSRM		128		
	Totals:		140	0.9	0
COMMON CAUSE Leak Check Port Plug (case/nozzle/igniter)	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0
OPT Primary O-Ring (3/igniter)	Static Tests	36			
	SRM,HPM,RSRM	384			
	Minuteman	3300			
	Totals:	3720			0
OPT Secondary O-Ring (3/igniter)	TPTA-2.2	3	0		
	JES-3C	3	24		
	TPTA-1.3	3	256		
	Totals:	9	280	0.9	0
COMMON CAUSE Rotor Primary O-Rings	Static Tests	12	12		
	SRM,HPM,RSRM	128	128		
	Totals:	140	140	0.6	0
Rotor Secondary O-Rings	Static Tests	2	12		
	SRM,HPM,RSRM		128		
	Totals:	2	140	0.9	0
COMMON CAUSE SII Primary O-Ring	Static Tests	24	24		
	SRM,HPM,RSRM	256	256		
	Totals:	280	280	0.9	0
SII Secondary O-Ring	Static Tests	2	24		
	SRM,HPM,RSRM		256		
	Totals:	2	280	0.9	0

RSRM Joint Leak Data

IGNITER-TO-CASE JOINT

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
INNER J-LEG	FSM-3	1			
	RSRM 23,35-37,39,41	12			
	Totals:	13			0
Special Bolt O-Ring (4/igniter)	Static Test	48	48		
	SRM,HPM,RSRM	512	512		
	Totals:	560	560	0.6	0
Outer J-Leg	FSM-3	1			
	RSRM 23,35-37,39,41	12			
	Totals:	13			0
Inner Gasket/Inner Seal	blow-holes (RSRM)	60			
	Static Tests		12		
	SRM,HPM,RSRM		128		
	Totals:	60	140	0.6	0
Inner Gasket/Outer Seal	blow-hole (RSRM)	60			
	Static Tests		12		
	SRM,HPM,RSRM		128		
	Totals:	60	140	0.9	0
Outer Gasket/Inner Seal	blow-holes (RSRM)	60			
	Static Tests		12		
	SRM,HPM,RSRM		128		
	Totals:	60	140	0.6	0
Outer Gasket/Outer Seal	Static Tests				
	SRM,HPM,RSRM		12		
	Totals:		128		
Stat-O-Seals (36/igniter)	Case	100	9000		
	Igniter		5040		
	Nozzle	100	6776		
	Totals:	200	20816	0.9	0
Leak Check Port Plug (case/nozzle/igniter)	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0

RSRM Joint Leak Data

CASE FIELD JOINT

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
J-Seal	Flights 1-37,39,41	234			
	Static Tests	15			
	JES 3A	2			
	TPTA 1.1, 2.1	3			
	Totals:	254			0
Capture Feature O-Ring	Flights 1-37,39,41		234		
	Static Tests		24		
	JES 3B	1	0		
	QM-6	1	2		
	PVM-1	1	1		
	Totals:	3	261	0.6	0
Vent Port Plug Primary O-Ring (nozzle and case combined) (47 motors counted as 23 tests)	Flights 1-37,39,41				
	Static Tests				
	TPTA 1.3,2.1,2.2	7			
	NUES/JES 3C	4			1
	SPC(70lb Motor)	23	23		
Totals:	34	287	0.9	1	
Vent Port Plug Second O-Ring (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1,2.2	3			
	NUES/JES 3C	3			
	Totals:	6	352	0.9	0
Closure Vent Port Plug (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1	2			
	NUES/JES 3C	2			
	Totals:	4	352	0.5	0
Primary O-Ring	Flights 1-37,39,41		234		
	Static Tests	1	27		
	TPTA 1.3,2.1,2.2	5			
	JES3B/3C	2			
	Totals:	8	261	0.9	0
Outer Gasket/Outer Seal	Static Tests				
	SRM,HPM,RSRM		12		
	Totals:		128		
Leak Check Prot Plug (case/nozzle/igniter combined)	Flights 1-37,39,41		780		
	static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.5	0
Secondary O-Ring	Flights 1-37,39,41		234		
	Static Tests		27		
	TPTA 2.2	2			
	JES 3C	1			
	Totals:	3	261	0.9	0

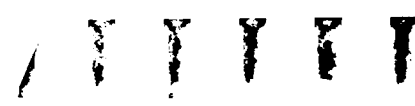
RSRM Joint Leak Data

NOZZLE JOINT

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
RTV Backfill	Joint 1	90			5
	Joint 2	18			7
	Joint 3	88			10
	Joint 4	88			10
	Joint 5	88			6
	Totals:	372			38
Primary O-Ring	Flight	24	390		
	Static Tests	14	50		
	Totals:	38	440	0.6	0
Secondary O-Ring	Flight		390		
	Static Tests		50		
	Totals:	0	440	0.9	0
Stat-O-Seals	Case	100	9000		
	Igniter		5040		
	Nozzle	100	6776		
	Totals:	200	20816	0.9	0
Leak Check Port Plug	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0



B.3. Orbiter Auxiliary Power
Unit/Hydraulics



9.0 DEVELOPMENT OF PROBABILITY DISTRIBUTIONS FOR FAULT TREES

The development of probability distributions for the fault trees is done using Bayesian updating methods. Prior probability distributions for failure rates are taken from the 1987 APU/HPU study, NPRD-95, IREP, IEEE Std. 500, WASH 1400, Shuttle experience and expert judgment. System level priors for the entire APU/HYD/WSB system (failure to start and failure to run distributions) are developed using component data mostly from the 1987 study. Bayesian updating was done at the system level using data found in the in-flight anomaly list (IFAS), PRACA reports, and Post Flight Mission Safety Evaluation Reports.

Data obtained shows that there have been four APU shutdowns on ascent due to the water spray boiler failing to provide adequate cooling, and a near hydraulic system failure due to a massive hydraulic leak during descent.

Due to the fact that the APU/HYD/WSB systems have redundancy, i.e., they are a two-out-of-three or better system, common cause failures become a concern. The fault trees are evaluated using the Multiple Greek Letter (MGL) method to determine the common cause and independent failure rates.

Section 9.1 describes how the MGL method is used to determine the independent failure rates and common cause failure rates from the generic failure rate for each sequence.

Section 9.2 describes the prior distributions used in the study. Fault trees are included in this section to show how prior distributions are calculated for APU/HYD/WSB failure to start, APU/HYD/WSB failure to run, and APU turbine wheel runaway.

9.1 Models/Equations for Fault Tree Basic Events

9.1.1 List of Basic Events

Table 9.1-1 is a complete list of the basic events found in the fault trees, and their two letter identification code used throughout the model.

9.1.2 Assumptions

Several assumptions have been made concerning data input probability distributions. The first is that given a common cause leak, all three APU units leak. The second assumption pertains to the detection/confirmation of the leaks. If all three units leak, and a leak is detected in one unit, then the leaks in all units are assumed to be found. A third assumption concerns the restarts of APU units. All units will have to go through a restart process sometime during the reentry process. Some scenarios have APU hydrazine leaks detected, in which case an APU unit is shutdown during the entry sequence. After an APU unit is shutdown, if another unit fails, then the shutdown unit is restarted. However, in the sequence, only one restart of the shutdown APU is considered. There are several reasons for this simplistic modeling. First, the reentry sequence will not begin until an APU unit is working to perform the flight controls check. Second, leaking APUs are shutdown only when a leak is detected and confirmed, and the probability of a leak being detected is only about one in twenty, so these scenario simplifications will not have a significant impact on the total risk.

Identification	Basic Event
CE	Flight critical equipment damaged given LL or TU
CF	Common cause failure to run
CL	Common cause leak
CO	No containment given turbine overspeed
CS	Common cause failure to start or run
HB	Hub breakup given turbine overspeed
ID	Independent/dependent failure to run (ascent)
IF	Independent failure to run (ascent)
IS	Independent failure to start or run (descent)
LA	Leak detected/confirmed given all three APU units leak
LD	Leak detected/confirmed given that one APU unit leaks
LF	Own leakage induced failure (ascent)
LK	Leak in one APU unit
LL	Large exhaust gas or hydrazine leak
LO	Leakage from another unit induced failure (ascent)
LS	Leakage from other unit induced failure to start or run (descent)
LU	Leak undetected given that one APU unit leaks
LZ	Leak undetected given that all three APU units leak
O1	APU unit okay given that one other APU unit leaks
O3	APU unit okay given that all three APU units leak
OK	APU unit okay
OL	APU unit okay given that it leaks
OS	Own leakage induced failure to start or run (descent)
SI	Structural integrity of aft compartment fails given LL or TU
SR	Successful restart of shutdown APU unit
TU	Turbine overspeed or hub failure at normal speed
UL	Unsuccessful single APU/HYD unit reentry, TAEM and landing

Table 9.1-1: List of Basic Events and Descriptions

9.1.3 Derivation of Common Cause Failure Equations

As components fail, it is not always entirely clear which failures are truly independent and which are common cause. In order to estimate the frequency of common cause failures from the total estimated frequency, several methods, such as the Multiple Greek Letter (MGL) or beta factor

methods, are used. In this analysis, the MGL method was used. The labeling of the APU units is as follows: if a single APU unit is leaking hydrazine, then that unit is labeled as unit 1, or if all three APU units are leaking hydrazine, then the unit that is shutdown (if the leaks are detected/confirmed) is labeled as unit 1.

9.1.3.1 One APU Unit Leaks Hydrazine During Reentry, TAEM and Landing (LO State)⁽¹⁾

Sequence 4

In this sequence, APU units 1 and 2, or 1 and 3, fail. This is basically a 1 out of 3 system, denoted $Q(1/3)$. There are two ways in which independent failures of this type can occur: Q_1Q_2 and Q_1Q_3 . For the common cause failures, there are also two ways that those may occur: Q_{12} and Q_{13} . Rewriting those terms in the MGL format using Q_1 for independent failures and Q_2 for common cause failure of two components yields the following equation for system failures:

$$Q(1/3) = 2Q_2 + 2Q_1^2$$

In this form of the MGL method where we are dealing both with common cause failures for two systems and common cause failures for three systems. The MGL method defines two parameters: β and γ . Beta is the ratio of two and three unit common cause failures of each unit to all failures for each unit. Gamma is the ratio of three unit common cause failures to two and three unit common cause failures. For each unit, beta is thus:

$$\beta = \frac{2Q_2 + Q_3}{Q_1 + 2Q_2 + Q_3}$$

and gamma is:

$$\gamma = \frac{Q_3}{2Q_2 + Q_3}$$

Omitting the algebra, the single system and common cause for two system failures can be written as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

Since Q represents the failures due to start or run failures, it should be rewritten as:

$$Q = q_s + \lambda t$$

⁽¹⁾The LO descent initiating event state is equivalent to the IL0 ascent end state.

where q_s is the failure to start probability, and λt is the probability of a failure during the run time.^(2,3) If we substitute into $Q(1/3)$ for Q_1 , Q_2 and Q , then the equation for failures becomes:

$$Q(1/3) = [(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t] + 2[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

This is the total failure rate. We now need to relate the above equation to the fault tree basic events. The first term in the above equation is the common cause term, and does not need to be changed. The second term in the above equation needs to represent the independent failures as depicted in the fault tree. For example, if we examine the fault tree for the sequence 4 LOV with the initiating L0 state (one APU unit is leaking), then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(1, 2 \text{ or } 1, 3) = P(1 \text{ IF})P(2 \text{ IF}) + P(1 \text{ IF})P(3 \text{ IF}) + P(\text{CCF}) + P(1 \text{ IF})P(3 \text{ LO}) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the fourth and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(\text{CCF}) = [(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t]$$

$$2P(\text{IF})^2 = 2[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

If we reduce the independent failure rate probability, we get:

$$P(\text{IF}) = \sqrt{[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2}$$

which reduces to:

$$P(\text{IF}) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

Sequence 6

In this sequence, both APU units 2 and 3 have failed. This is basically a 1 out of 3 system, denoted $Q(1/3)$. There is one way in which independent failures of this type can occur: $Q_2 Q_3$. For the common cause failures, there is also only one way that this may occur: Q_{23} . Rewriting those terms in the MGL format using Q_1 for independent failures and Q_2 for common cause failure of two components yields the following equation for system failures:

$$Q(1/3) = Q_1^2 + Q_2$$

As before, the single and common cause (for two systems) factors are defined as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

⁽²⁾ In this analysis the β_s and β_r are given the same numerical value, and γ_s and γ_r are given the same numerical value.

⁽³⁾ For ascent sequences, λt is the probability of basic event ID (or IF) in Table 9.3-1. For descent sequences $q_s + \lambda t$ is the probability of a basic event IS in Table 9.3-1.

Since Q represents the failures due to start or run failures, it should be rewritten as:

$$Q = q_s + \lambda t$$

where q_s is the failure to start probability, and λt is the probability of a failure during the run time. If we substitute into $Q(1/3)$ for Q_1 , Q_2 and Q , then the equation for failures becomes:

$$Q(1/3) = \frac{1}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t] + [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

As before, we can see that the first term represents the common cause failure rate, and the second term represents the independent failure rate. If we examine the fault tree for the sequence 6 LOV with the initiating LO state, then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(2, 3) = P(2 IF)P(3 IF) + P(CCF) + P(2 IF)P(3 LO) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the third and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(CCF) = \frac{1}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t]$$

$$P(IF)^2 = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

If we reduce the independent failure rate probability, we get:

$$P(IF) = \sqrt{[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2}$$

which reduces to:

$$P(IF) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

This is the same expressions as determined in the Sequence 4 LOV.

Sequence 7

In this sequence, since there is no leak detection, no distinction is made between which units fail and which do not. All three units fail, even though 1 out of 3 is needed for survival, so this is denoted $Q(1/3)$. There is one way in which independent failures of this type can occur: $Q_1 Q_2 Q_3$. For the common cause failures, there is also only one common cause for all three, Q_{123} . There are three combinations of pairs of common cause failures for two systems, i.e., Q_{12} and Q_{23} is one pair, and three combinations of an independent failure and a common cause failure for two systems, i.e., Q_1 and Q_{23} , and one pair. Rewriting those terms in the MGL format using Q_1 for independent failures, Q_2 for common cause failures of two components and Q_3 for common cause failures of three components yields the following equation for system failures:

$$Q(1/3) = Q_3 + 3Q_1 Q_2 + 3Q_2^2 + Q_1^3$$

Omitting the algebra, the failures can be written as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

$$Q_3 = \gamma\beta Q$$

Substituting for Q_1 , Q_2 and Q_3 into $Q(1/3)$ yields:

$$Q(1/3) = \gamma\beta Q + \frac{3}{2}(1 - \beta)\beta(1 - \gamma)Q^2 + \frac{1}{2}\frac{(1 - \gamma)}{(1 - \beta)}\beta\left[\frac{3}{2}(1 - \beta)\beta(1 - \gamma)Q^2\right] + (1 - \beta)^3 Q^3$$

If we examine the above expression, we see that there are four terms, which from left to right we'll call one, two, three and four. The third term is negligible because

$$\frac{1}{2}\frac{(1 - \gamma)}{(1 - \beta)}\beta \ll 1$$

and is, furthermore, much less than the second term. As before:

$$Q = q_s + \lambda t$$

where q_s is the failure to start probability, and λt is the probability of a failure during the run time. Substitute Q into $Q(1/3)$ with the simplifying assumption yields:

$$Q(1/3) = (\gamma_s\beta_s q_s + \gamma_r\beta_r \lambda t) + \frac{3}{2}\{[(1 - \beta_s)\beta_s(1 - \gamma_s)q_s^2] + [(1 - \beta_s)\beta_r(1 - \gamma_r)q_s \lambda t] + [(1 - \beta_r)\beta_s(1 - \gamma_s)q_s \lambda t] + [(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2]\} + [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^3$$

As before, we can see that the first term represents the common cause failure rate, and the second term represents the independent failure rate. If we examine the fault tree for the sequence 7 LOV with the initiating LO state, then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(1, 2, 3) = P(1 IF)P(2 IF)P(3 IF) + P(CCF) + P(1 LO)P(2 IF)P(3 IF) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the third and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(CCF) = \gamma_s\beta_s q_s + \gamma_r\beta_r \lambda t + \frac{3}{2}\{[(1 - \beta_s)\beta_s(1 - \gamma_s)q_s^2] + [(1 - \beta_s)\beta_r(1 - \gamma_r)q_s \lambda t] + [(1 - \beta_r)\beta_s(1 - \gamma_s)q_s \lambda t] + [(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2]\}$$

$$P(IF) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

Sequence 11

In this sequence, two APU units fail, and since the event is undetected, no distinction is made as to which two have failed. System failures are thus defined as:

$$Q(1/3) = 3Q_2 + 3Q_1^2$$

As before, the failures are defined as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

Since Q represents the failures due to start and run failures, it should be rewritten as:

$$Q = q_s + \lambda t$$

where q_s is the failure to start probability, and λt is the probability of a failure during the run time. If we substitute into $Q(1/3)$ for Q_1 , Q_2 and Q , then the equation for failures becomes:

$$Q(1/3) = \frac{3}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t] + 3[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

As before, we can see that the first term represents the common cause failure rate, and the second term represents the independent failure rate. If we examine the fault tree for the sequence 11 LOV with the initiating L0 state, then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(2 \text{ fail}) = P(1 \text{ IF})P(2 \text{ IF}) + P(1 \text{ IF})P(3 \text{ IF}) + P(2 \text{ IF})P(3 \text{ IF}) + P(\text{CCF}) + P(2 \text{ IF})P(3 \text{ LO}) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the fifth and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(\text{CCF}) = \frac{3}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t]$$

$$3P(\text{IF})^2 = 3[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

If we reduce the independent failure rate probability, we get:

$$P(\text{IF}) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

Sequence 12

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for IL0 sequence 7.

Sequence 16

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

This sequence also models the remaining two APU units developing a common cause leak, given the initial leak in one unit.⁽¹⁾ As described for OK sequence 21, the formula for common cause leakage is given by:

$$P(CCF) = \gamma_L \beta_L \lambda_{L,t} + \frac{3}{2}(1 - \beta_L) \beta_L (1 - \gamma_L) \lambda_L^2 t^2$$

Here, $\lambda_{L,t}$ is the probability of the initial state, L0. So, since the conditional probability of developing the common cause leak is multiplied against the initial state probability, and given that the first term in the equation is by far the dominant factor, the common cause conditional probability should be entered as:

$$P(CCF) = \gamma_L \beta_L$$

Sequence 18

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6. The equation for a common cause leak is the same as that described for L0 sequence 16.

Sequence 19

This sequence occurs when all APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for a common cause leak is the same as that described for L0 sequence 16.

Sequence 23

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11. The equation for a common cause leak is the same as that described for L0 sequence 16.

Sequence 24

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for a common cause leak is the same as that described for L0 sequence 16.

9.1.3.2 All Three APU Units Leak Hydrazine During Reentry, TAEM and Landing (LT State)

Sequence 4

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

⁽¹⁾ λ_L is the frequency of event LK in Table 9.3-1.

Sequence 6

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6.

Sequence 7

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7.

Sequence 11

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11.

Sequence 12

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 12.

9.1.3.3 All Three APU Units are OK During Reentry, TAEM and Landing (OK State)

Sequence 4

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11.

Sequence 5

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7.

Sequence 9

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

This sequence also involves a common cause treatment of APU leaks. Here, we are modeling any one of the three APUs develops a leak, which is basically a 1 out of 3 system, denoted as $Q(1/3)$. There are three ways in which independent failures of this type can occur: Q_1 , Q_2 , or Q_3 . Rewriting those terms in the MGL format using Q_1 for the independent failures yields the following equation for system failures:

$$Q(1/3) = 3Q_1$$

As before, the failures are identified as:

$$Q_1 = (1 - \beta)Q$$

Since Q in this case represents leakage failures over the exposure time, Q is replaced by:

$$Q = \lambda_L t$$

where λ_L is the leakage failure rate and t is the exposure time of the system. If we substitute into Q(1/3) for Q1, then the equation for failures becomes:

$$Q(1/3) = 3(1 - \beta_L)\lambda_L t$$

Since independent failures are the only contributors in this equation, we get:

$$P(IF) = 3(1 - \beta_L)\lambda_L t$$

Sequence 11

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6. The equation for independent leaks is the same as that described for OK sequence 9.

Sequence 12

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for independent leaks is the same as that described for OK sequence 9.

Sequence 16

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11. The equation for independent leaks is the same as that described for OK sequence 9.

Sequence 17

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for independent leaks is the same as that described for OK sequence 9.

Sequence 21

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

This sequence also involves a common cause treatment of APU leaks. Here, we are modeling all three APUs develop leaks. The equations for independent and common cause failures are similar to those described for L0 sequence 7, but with Q defined differently as in OK sequence 9. Omitting the algebra, the new independent and common cause failure rates can be determined by the following equations:

$$P(CCF) = \gamma_L \beta_L \lambda_L t + \frac{3}{2}(1 - \beta_L)\beta_L(1 - \gamma_L)\lambda_L^2 t^2$$

$$P(IF) = (1 - \beta_L)\lambda_L t$$

Sequence 23

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

Sequence 24

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

Sequence 28

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

Sequence 29

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

9.1.3.4 All Three APU Units are OK During Ascent (OK State)

For the ascent phase, it is assumed that all APU units are already started, otherwise the launch sequence would not have been completed. Hence, Q is now defined as:

$$Q = \lambda t$$

Sequence 4

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are similar to those described for L0 sequence 7, but with Q defined differently. Omitting the algebra, the new independent and common cause failure rates can be determined by the following equations:

$$P(IF) = (1 - \beta_r)\lambda t$$

$$P(CCF) = \gamma_r \beta_r \lambda t + \frac{3}{2}(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2$$

9.1.3.5 At Least One APU Unit is Leaking Hydrazine During Ascent (LK State)

Sequence 6

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equation for independent leaks is the same as that described for OK sequence 9.

Sequence 7

This sequence occurs when one APU unit has an undetected leak. The equation for independent leaks is the same as that described for OK sequence 9.

Sequence 12

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equation for independent leaks is the same as that described for OK sequence 9.

Sequence 16

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

Sequence 17

This sequence occurs when all three APU units have undetected leaks. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

Sequence 20

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

9.1.3.6 MGL Parameters

The following point estimates are generic over all components and all failure modes. They were developed as part of a recent effort funded by EPRI to completely automate the process of analyzing common cause failures in PRAs. The software is available through Boyer Chu at EPRI. This recent effort was based on previous data development and MGL method development found in EPRI INP 3967 (1985), NUREG/CR-4780 (1988), and NUREG/CR-5801 (1993).

For information on methods and procedures for common cause failure you can refer to NUREG/CR-4780 (1988) and NUREG/CR-5801 (1993).

APU component failure rates are generally within the variability range of the generic database from which the Beta and Gamma factors are derived. We believe, therefore, that these are an indication of future failure rates of the APU, and the generic factors apply to the APUs.

We also used the generic data for common cause hydrazine leakage. We have found six leaks (see Section 9.2.2.6). Two of the leaks happened in the same mission (STS-9) for a common cause (carbonization and stress cracking of the injector). The Beta factor could be estimated as 1/3 (3 of 6). However, we know that the manufacturing process has been altered to reduce the likelihood of this cause. There has also been an effort to reduce the exposure of the nozzles to hydrazine between missions. We have used, therefore, a generic Beta factor of 0.1 instead of the

data driven Beta factor of 1/3. We see no justification to apply a Beta factor less than indicated by the generic level.

9.1.4 Equations Graphed in Fault Tree for Illustration

As an example of how the independent failure rate and common cause failure rate equations developed in the previous section are applied, see Figure 9.1-1. In the figure is a simple fault tree that shows the sequence 4 LOV for the ascent phase in which no hydrazine leaks have occurred.

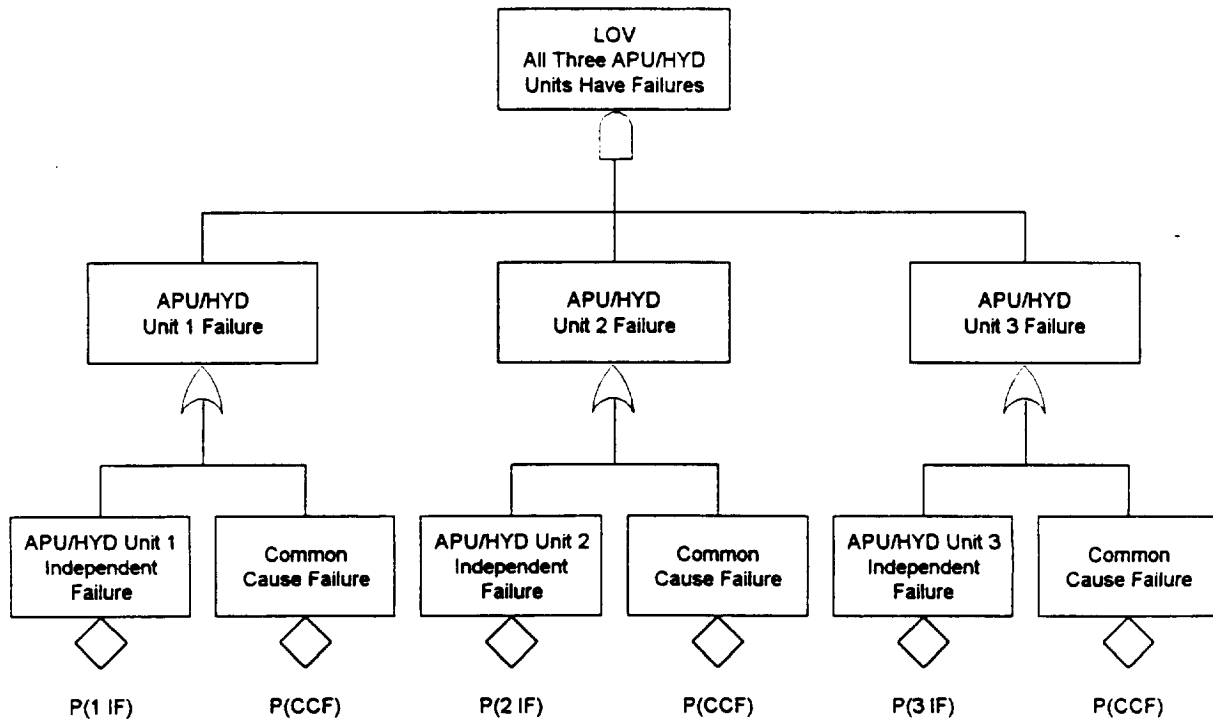


Figure 9.1-1: Fault Tree for LOV Sequence 4 for an OK State During Ascent

For the LOV to occur, all three APU/HYD systems must fail. System failures can occur independently, or as common cause failures. These failure rates were determined from the total failure rate using the Multiple Greek Letter method previously described, and are shown under the basic events to which they pertain.

From before, we defined $P(CCF)$ and $P(IF)$ as:

$$P(IF) = (1 - \beta_r)\lambda t$$

$$P(CCF) = \gamma_r \beta_r \lambda t + \frac{3}{2}(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2$$

9.2 Prior Distribution for Model

The priors used in the assessment of $P(IF)$ came from a previous study (McDonnell Douglas Astronautics Company Engineering Services, Space Shuttle Probabilistic Risk Assessment Proof-of-Concept Study Volume III: Auxiliary Power Unit and Hydraulic Power Unit Analysis Report, paper WP-VA88004-03, 1987). As described previously, the priors were updated at the system level with observed Shuttle in flight failures.

9.2.1 Inputs Needed to Develop Priors

The study performed in 1987 was done at a component level; i.e., the failure rates of the components in the system were calculated, and no quantification was done on the system level. This study has defined basic events on the system level in order to have such information for future decision-making. Two prior distributions, the failure to start on demand and the run failure rate, were estimated using the component level data.

The fault tree in Figure 9.2-1 depicts the component failures that most contribute to a system failure to run. These components failure rates were agglomerated to obtain a prior distribution for APU system failure to run (events, ID, IF and IS).

Similarly, Figure 9.2-2 depicts a fault tree in which any of the component failures may cause a failure to start condition. These component failure rates were agglomerated for the start contribution of event IS.

The 1987 study performed a detailed fault tree for turbine overspeed. Quantification of that tree showed that four events dominated the failure probability. These are shown in a simplified fault tree in Figure 9.2-3.

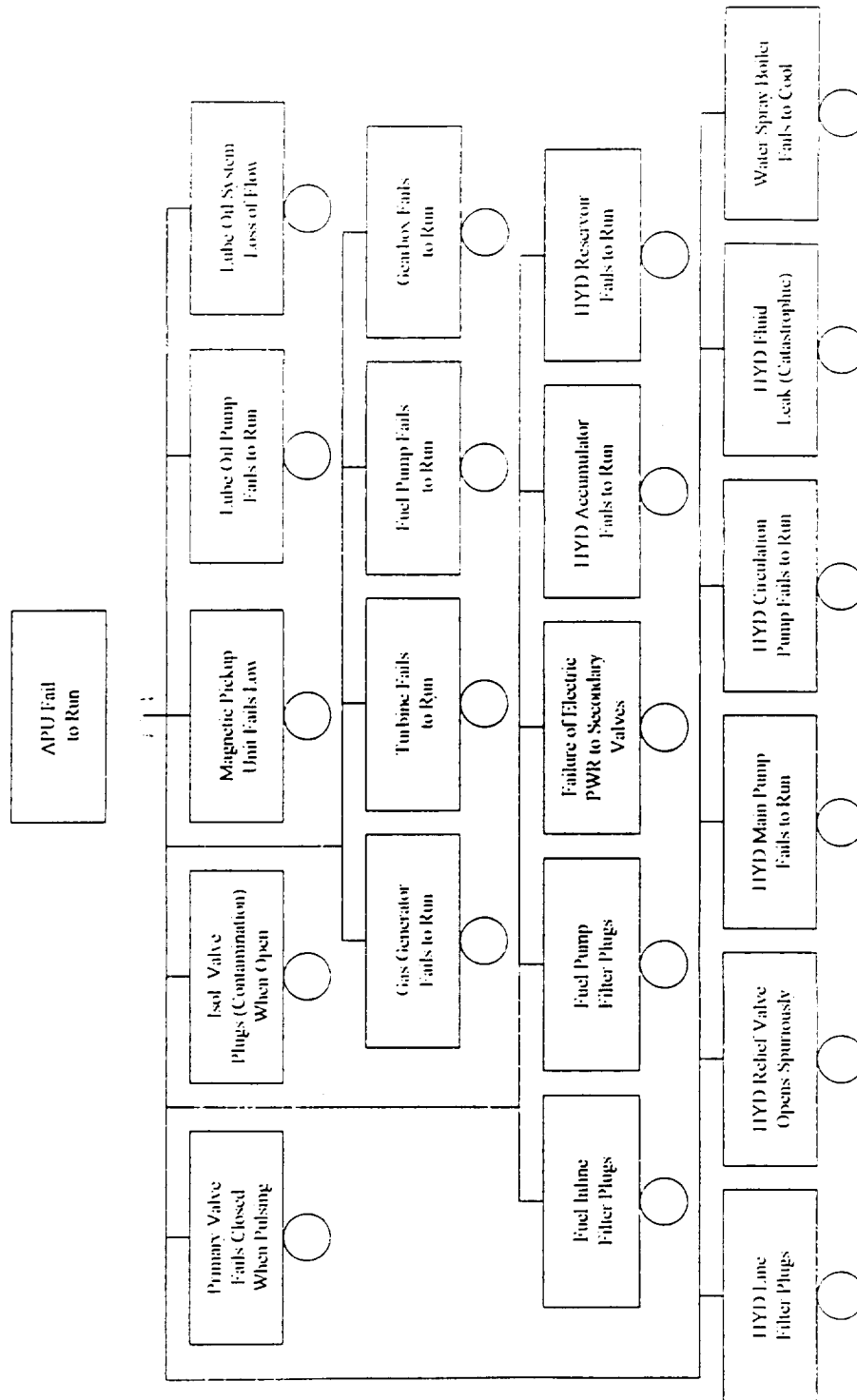


Figure 9.2-1: Fault Tree for APU/HYD/WSB Run Failures

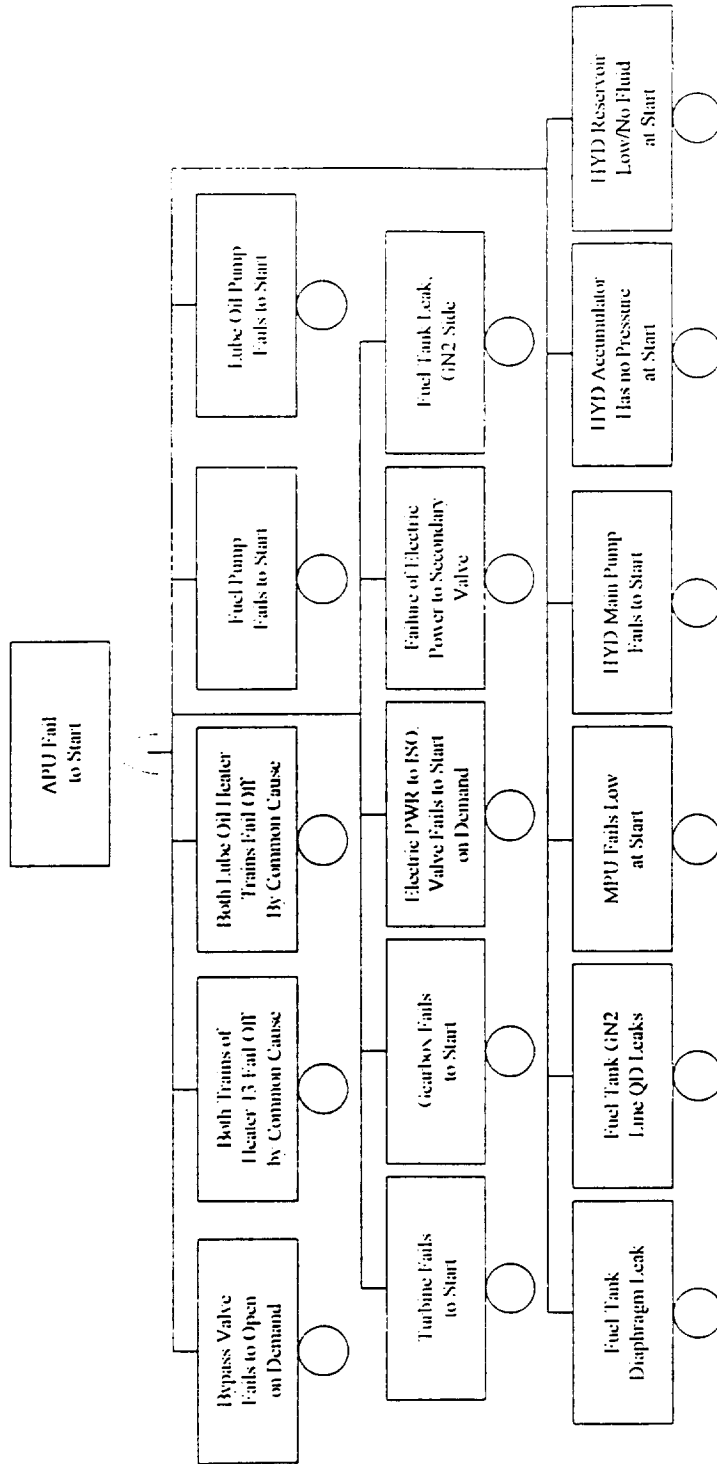


Figure 9.2-2: Fault Tree for APU/HYD/WSB Start Failures

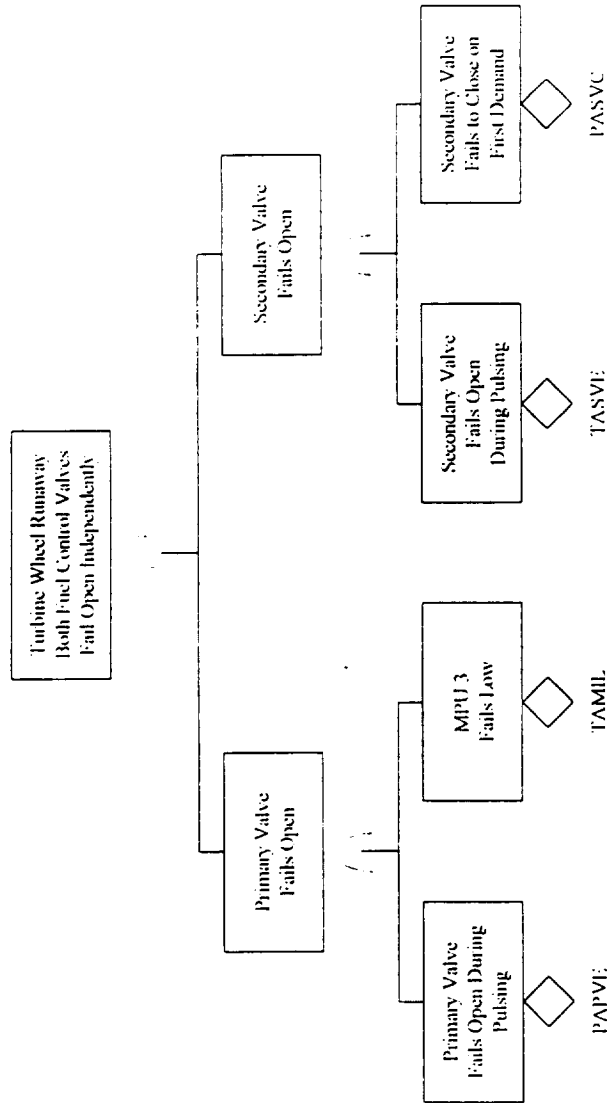


Figure 9.2-3: Fault Tree for Turbine Overspeed Failures

9.2.2 Output Distributions for Priors

9.2.2.1 APU Failure to Run

The first prior calculated is that for an APU to fail to run. Table 9.2-1 lists the component failures frequency distributions that were in the model for APU subsystem run failures.

Failure	Mean-Dist	5th percentile	Median	95th percentile	Ref. (1)
Primary Valve Fails Closed When Pulsing	4.481E-03	3.494E-04	2.404E-03	1.225E-02	1
Isol. Valve Plugs (Contamination) When Open	1.086E-06	4.681E-08	4.343E-07	3.875E-06	1
Magnetic Pickup Unit Fails Low	2.240E-03	1.747E-04	1.202E-03	6.127E-03	1
Fuel Pump Fails To Run	7.685E-05	2.791E-06	2.887E-05	2.797E-04	1
Lube Oil Pump Fails To Run	7.685E-05	2.791E-06	2.887E-05	2.797E-04	1
Lube Oil System Loss Of Flow	2.664E-03	9.334E-05	9.698E-04	9.681E-03	1
Gas Generator Fails To Run	1.436E-04	9.020E-07	2.467E-05	4.429E-04	1
Turbine Fails To Run	6.041E-04	2.722E-05	2.350E-04	1.837E-03	1
Gearbox Fails To Run	2.628E-05	9.323E-07	9.672E-06	9.651E-05	1
Fuel Inline Filter Plugs	7.959E-06	2.799E-07	2.907E-06	2.894E-05	1
Fuel Pump Filter Plugs	2.040E-04	2.722E-06	5.002E-05	6.507E-04	1
Failure Of Electric Pwr To Secondary Valves	4.926E-05	9.231E-07	1.357E-05	1.866E-04	1
HYD Accumulator Fails To Run	2.664E-05	1.0E-06	1.0E-05	1.0E-04	2
HYD Reservoir Fails To Run	2.664E-05	1.0E-06	1.0E-05	1.0E-04	2
HYD Line Filter Plugs	7.840E-06	6.0E-06	7.746E-06	1.0E-05	3
HYD Relief Valve Opens Spuriously	1.212E-05	3.0E-06	9.487E-06	3.0E-05	5
HYD Main Pump Fails To Run	4.040E-05	1.0E-05	3.162E-05	1.0E-04	2.5
HYD Circulation Pump Fails To Run	1.127E-04	7.0E-06	5.292E-05	4.0E-04	2.3
HYD Fluid Leak (Catastrophic)	4.332E-04	5.0E-06	5.0E-05	5.0E-04	1,3,4
Water Spray Boiler Fails To Cool	3.385E-05	1.0E-04	2.236E-05	5.0E-06	2.5
Total Fail To Run/Hr	9.150E-03	3.059E-03	6.956E-03	2.174E-02	

(1)

- | | | |
|-------------------|--------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 1. 1987 APU Study | 4. OREDA | 6. Shuttle history of 0 failures is 882 demands in a maximum entropy log normal: $882 = (6 \text{ APU Starts/Missions} + 4 \text{ HPU starts} + 4 \text{ HPU Hot Fire Tests}) \times 63$ |
| 2. NPRD-95 | 5. WASH-1400 | |
| 3. IEEE-STD-500 | | |

Table 9.2-1: Component Failures Leading to APU System Run Failure (Failures/hour)

In order to calculate the distribution of the sum of these failures, an @Risk Monte Carlo simulation (20,000 trials) in a Lotus 1-2-3 spreadsheet was used. A graphical representation of this distribution can be seen in Figure 9.2-4.

9.2.2.2 APU Failure to Start

In Table 9.2-2, various component failures are listed that will lead to a failed-start condition. Once again, to calculate the failed-start distribution based on the sum of the various component failures, an @Risk Monte Carlo simulation (20,000 trials) in a Lotus 1-2-3 spreadsheet was used.

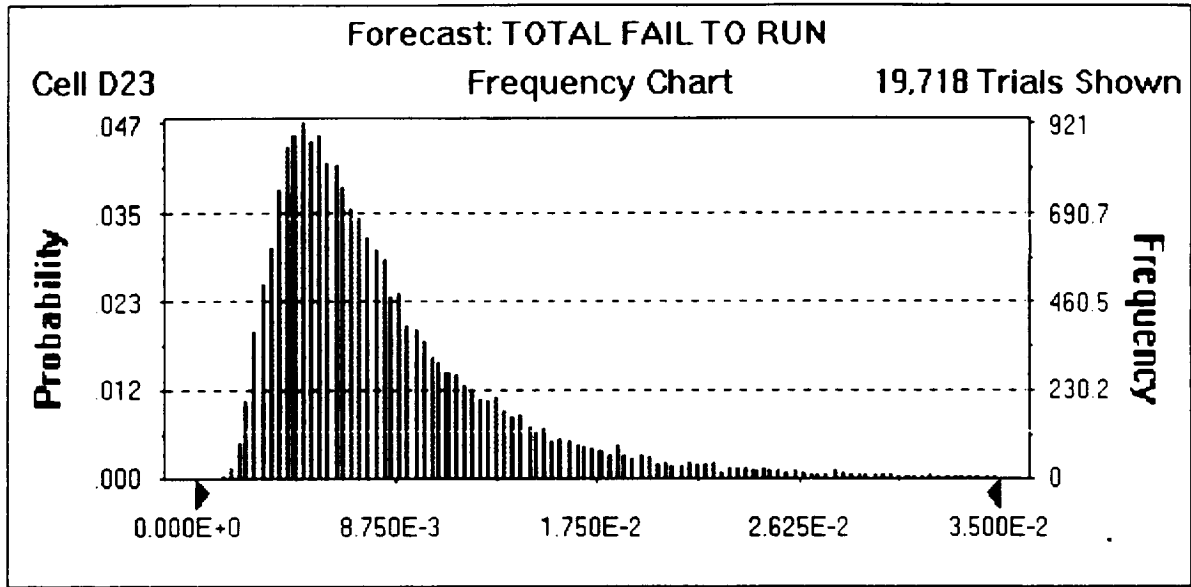


Figure 9.2-4: @Risk Simulation Results for Failure to Run Frequency

Failure	Mean-Dist	5th percentile	Median	95th percentile	Reference
Bypass Valve Fails To Open On Demand	4.689E-04	1.690E-05	1.730E-04	1.276E-03	1
Common Cause Heater Train 13 Failure	6.5E-05	4.6E-006	3.6E-05	1.5E-04	1
Common Cause Lube Oil Heater Train Failure	2.1E-05	5.3E-07	7.8E-06	5.7E-05	1
Fuel Pump Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Lube Oil Pump Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Turbine Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Gearbox Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Electric Pwr To Primary Valve Fails	6.2E-04	1.3E-05	2.0E-04	1.9E-03	1
Electric Power To Secondary Valve Fails	6.207E-04	1.329E-05	2.045E-04	1.879E-03	1
MPU Fails Low	7.409E-04	3.447E-05	3.260E-04	2.032E-03	1
HYD Main Pump Fails To Start	4.0E-04	4.683E-05	2.426E-04	1.257E-05	6
HYD Accumulator Has No Pressure At Start	4.475E-03	1.68E-04	1.680E-03	1.68E-02	2 ⁽¹⁾
HYD Reservoir Low/No Fluid At Start	4.475E-03	1.68E-04	1.680E-03	1.68E-02	2 ⁽¹⁾
Total Failures To Start	1.205E-02	3.322E-03	7.949E-03	3.342E-02	

⁽¹⁾ Converted hourly failure rate to a start failure by multiplication by exposure time (168 hours)

1. 1987 APU Study
2. NPRD-95
3. IEEE-STD-500

4. OREDA
5. WASH-1400

6. Shuttle history of 0 failures is 882 demands in a maximum entropy log normal: $882 = (6 \text{ APU Starts/Missions} + 4 \text{ HPU Starts} + \text{HPU Hot Fire Tests}) \times 63$

Table 9.2-2: Component Failures Leading to APU System Start Failure (Failures/Demand to Start)

The @Risk Monte Carlo simulation (20,000 trials) for the failure to start probability distribution can be seen in Figure 9.2-5.

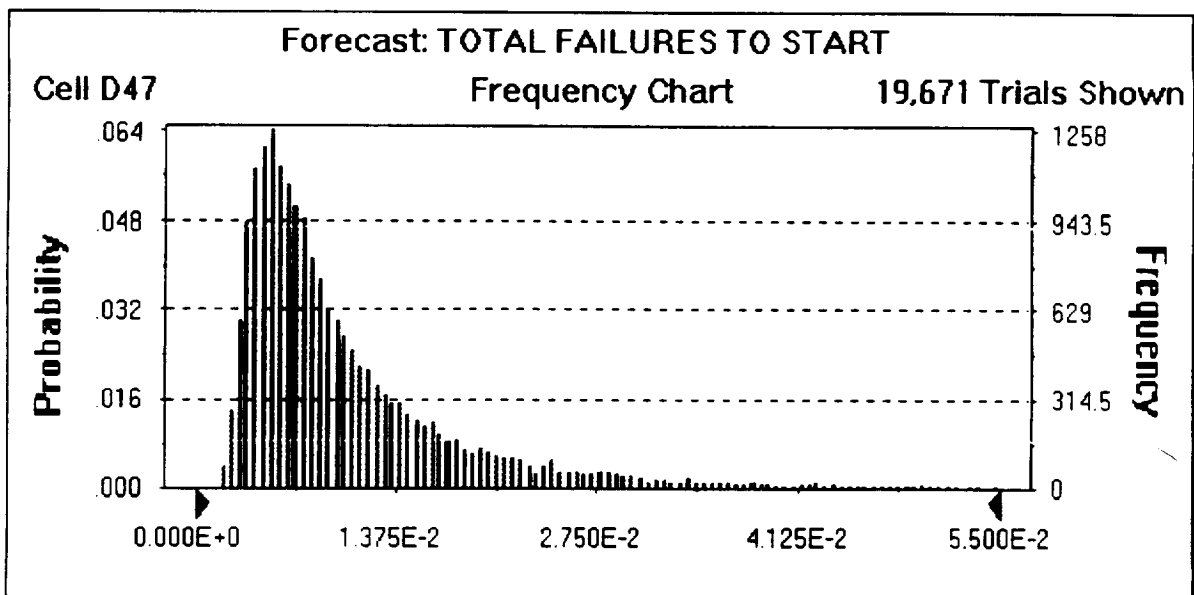


Figure 9.2-5: @Risk Simulation Results for Failure to Start Frequency

9.2.2.3 Turbine Overspeed and Hub Failure at Normal Speed

Figure 9.2-3 depicted the fault tree for a turbine overspeed condition which is an initiating event (TU). Prior distributions were obtained from the 1987 APU study. The following Table 9.2-3 provides the priors and the in-flight shuttle data used for the likelihood function. The posterior failure rates of these various components are listed in Table 9.2-5. To calculate the turbine overspeed frequency distribution based on fault tree logic, @Risk Monte Carlo simulation (20,000 trials) in a Lotus 1-2-3 spreadsheet was used.

Event	Prior (Log Normal) 5 Percentile	Prior (Log Normal) 95 Percentile	Shuttle Specific Data
PASVC	$8 \times 10^{-5}/D$	$7 \times 10^{-3}/D$	1/378 Demands ⁽¹⁾
TASVE	$1 \times 10^{-4}/hr$	$1 \times 10^{-2}/hr$	0/0 ⁽²⁾
TAMIL	$5 \times 10^{-5}/hr$	$5 \times 10^{-3}/hr$	1/796 hrs ⁽³⁾
PAPVE	$1 \times 10^{-4}/hr$	$1 \times 10^{-2}/hr$	1/292 hrs ⁽⁴⁾

⁽¹⁾ 2 Demand/APU x 63 millions x 3 APUs/Missions = 378 Demands

⁽²⁾ Failure of primary valve in mission SB-31 generated a demand on the secondary valve for a few minutes before the launch was scrubbed. The secondary valve did not fail.

⁽³⁾ 1.33 hours/APU x 3 APUs/Missions x 3 HPUs/APUs x 63 Missions = 796 hours

⁽⁴⁾ 1.33 hours/APU x 3 APUs/Missions x 63 Missions = 292

Table 9.2-3: Priors and In-Flight Shuttle Data Used for the Likelihood Function

Shuttle in-flight failures used in the above table are described below in Table 9.2-4:

Car No.	Date	Flight No.	APU No.	Basic Event	Description
AC8511-01	08/06/84	41B	3	PASVC	GGVM Shut off valve leaking at a rate of 248 scim due to a broken poppet valve seat
AC0055-01	07/24/81	1	2	TAMIL	MPU #2 was inopr.; MPU resistance measured open
IFA STS-31-01	04/24/91	STS-31	1	PAPVE	Primary pulse control valve chipped (valve seat failure) allowing hydrazine to continue flowing. Secondary valve took over. Launch scrubbed.

Table 9.2-4: APU Turbine Component Failure Descriptions

The @Risk Monte Carlo simulation (20,000 trials) for the failure to start probability distribution can be seen in Figure 9.2-6.

Failure	Mean-Dist	5th percentile	Median	95th percentile
Primary Valve Fails Open During Pulsing	1.477E-03	6.852E-05	6.500E-04	4.054E-03
Magnetic Pickup Unit Fails Low	2.240E-03	1.747E-04	1.202E-03	6.127E-03
Secondary Valve Fails Open During Pulsing	9.602E-04	5.032E-05	4.484E-04	2.685E-03
Secondary Valve Fails To Close On Demand	2.631E-03	2.305E-04	1.504E-03	7.500E-03
Total Probability For Turbine Overspeed/Flight ⁽¹⁾	2.518E-04	6.733E-06	7.530E-05	9.403E-04

(1) All APUs included

Table 9.2-5: Posterior Failure Rate Data for Component Failures Leading to Turbine Overspeed

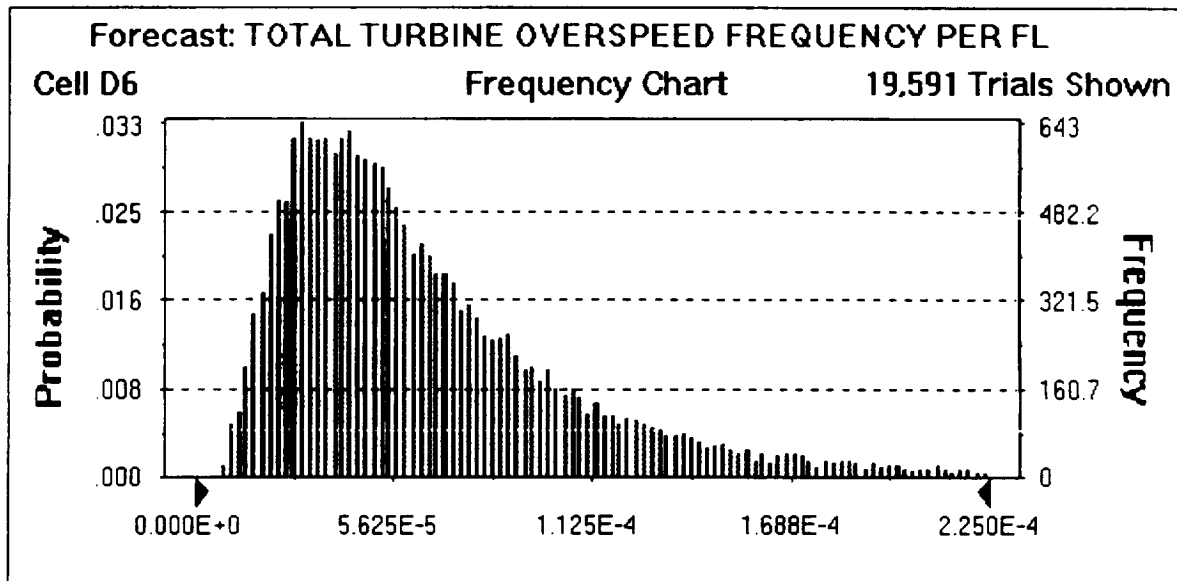


Figure 9.2-6: @Risk Simulation Results for Turbine Overspeed Frequency

Turbine hub failure at normal speed is not a significant contributor to the probability of this event. APU hub cracking is mapped and it has been shown by analysis (at JSC) that the likelihood of blade cracking propagating to a hub crack is very small. Furthermore, experiments on hub breakup show that even a notched or drilled hub requires a speed significantly above nominal to induce hub failure. NPRD-95 has a value of turbine failure of about 10⁻⁵/hr. for all modes combined, not just hub failure. Therefore, hub failure at normal speed is at least an order of magnitude less in probability than turbine overspeed.

9.2.2.4 Other Prior Distributions

The remaining prior distributions were taken directly from the 1987 study, were defined by MGL analysis, or were a result of our assessment. All of the prior distributions are in Table 9.2-8. The two letter descriptions were discussed previously in Table 9.1-1.

Some events, such as an APU OK state, are not in this table since they are not incorporated into the quantification of the scenarios. For some inputs only a mean value was estimated.

9.2.2.5 Large Exhaust Gas or Hydrazine Leak (LL)

This prior distribution was generated by breaking the event down into its three major contributors: tank/pipe rupture; hot gas leak; and isolation valve leak/rupture. For both the tank/pipe rupture and hot gas leak modes, a failure rate range based on variability was defined from Nonelectronic Parts Reliability Data 1995 (NPRD-95). The median value from this range was multiplied by the 1.5 hour total APU run time for ascent and descent, and times 3 for the number of APUs, to get a point estimate failure probability for the system per flight.

A failure rate range was also defined for the isolation valve leak from NPRD-95. In this case, the range was treated as defining the 5th and 95th percentiles of a lognormal distribution which was used as the prior in a Bayesian update. The evidence data consisted of two incidents in which cracks were found in APU and HPU isolation valves which did not propagate to a through crack of the valve casing that separates the flow path from the solenoid cavity. The concern here is that when hydrazine comes in contact with the solenoid it could decompose and rupture the isolation valve causing an unisolatable leak. These were not "hard" failures, but are valid evidence of failure potential. They were treated, therefore, by a near miss methodology as follows.

The solution was to treat the data according to the probability that these incidents might propagate into "hard" failures on other flights, where the circumstances might be different. This is a matter of judgment on the part of the analyst. In this case, since these incidents were determined to have a low probability of propagating to "hard" failures, the evidence was treated as having a 5% probability of representing 1 failure in 72000 hours (a lower bounding estimate of the total exposure time for APU and HPU isolation valves), and a 95% chance of representing zero failures in 72000 hours. The overall posterior distribution was then generated by taking a weighted average (according to the previously determined weights) of the two possible posterior distributions.

The following Table 9.2-6 shows the prior distributions.

	5 Percentile	95 Percentile	Exposure Time
Tank/Pipe Replace (prior only)	10 ⁻⁹ /hr.	10 ⁻⁷ /hr.	63 x 3 x 1.5 hrs.
Hot Gas Leak (prior only)	same	same	same
Isolation Valve (prior)	1 x 10 ⁻⁷ /hr.	10 ⁻⁷ /hr.	72000 hrs.
Isolation Valve (updated)	1.2 x 10 ⁻⁹ /hr.	8 x 10 ⁻⁸ /hr.	

Table 9.2-6: Distributions for Large Hydrazine or Exhaust Gas Leak

The data used in the isolation valve analysis is anecdotal. We are aware of a crack discovered in an APU isolation valve before STS-1. We are also aware of a recent crack found in an HPU, that when tested post-flight, leaked hydrazine into the solenoid cavity.

9.2.2.6 Leak in One APU Unit (LK)

A Bayesian analysis was not performed for hydrazine leaks. Shuttle in-flight experience was used to generate a point estimate of the rate at which hydrazine leaks develop. This rate was based on the data in Table 9.2-7, showing 6 leaks in 31752 hours of exposure time (63 flights x 3 APUs x assumed average flight duration of 7 days x 24 hours/day). To generate a probability distribution, the point estimate was assumed to be the mean value of a maximum entropy ($\sigma = 1.0$) lognormal distribution.

This assessment was based on a number of assumptions. We assume that the APUs are leak checked and only launched if found acceptable. Hydrazine leaks may occur at any time during the mission. Exposure to hydrazine may cause leaks even without the system operating. However, the leaks may only be revealed when the system is operating.

CAR	IFAS	Flight	Date	APU #	Description
**		1CR	04/12/81	1	Hyd. leak from fuel pump cover
**		1CR	04/12/81	2	Hyd. leak at fuel pump inlet fitting
09F012-01		STS-9	11/28/83	1	Hyd. leak from cracked fuel injector tube *
09F013-01		STS-9	11/28/83	2	Hyd. leak from cracked fuel injector tube *
	X	STS-51F	07/29/85	1	Hyd. leak into gearbox ***
	X	STS-45	03/24/92	1	Hyd. leak into gearbox ****
<p>* APU failed due to the hydrazine leak</p> <p>** Data from APU subsystem manager database</p> <p>*** This leak was detected by increased pressure in the gearbox and the start of APU2 was delayed until Vrel=10k</p> <p>**** On this same mission APU2 leaked oil / GN2 from the gearbox to the aft compartment</p>					
	X	STS-45	03/24/92	2	Lube oil / GN2 leak from gearbox through turbine seal

Table 9.2-7: Hydrazine Leakage History on STS

The APUs contain many potential leakage sites. The data simply indicates that some have already occurred. Others have yet to become active. Because of this, we do not necessarily view corrective actions to individual leakage sites as reducing the predicted frequency of leaks. Rather, we treat past leaks as indicative of future rates.

9.2.2.7 Leak Detected Confirmed (LD and LA)

The first four leaks above were not detected during the mission. The last two leaks were detected by increased pressure in the gearbox. We assess the probability of leak detection, and APU delayed start, as 1 in 6 based on this data. Since no action has ever been taken on leaks during ascent, this indicated zero probability of leak detection on ascent. The use of zero detected and confirmed leaks during ascent avoids the paradox associated with a groundrule of this study. The groundrule is that aborts are assumed to be successful. Therefore, a failure that leads to an APU induced abort actually reduces the calculated risk. Flight rules call for an APU shutdown and an MDF abort if a single hydrazine leak is detected and confirmed. Two such leaks lead to a PLS abort. To avoid having to treat leaks as successes, we assume no detection on ascent.

9.2.2.8 Own Leakage/Other Leakage Induced Failures (LF and LO)

These prior distributions were defined through a data based assessment utilizing the 1987 study, PRACA records, hazards analyses and an understanding of the phenomenology of the failure modes. Specifically, the mean value for own leakage induced failure during descent was defined from the data shown in Table 9.2-7, indicating 2 APU failures in 6 leaks. The mean values for the other three conditional probabilities were then derived by maintaining the ratios between the values from the 1987 study and scaling them to the 0.3 defined for LF (des). This produced values of 0.2 for LO (des), 0.1 for LF (asc) and 0.008 for LO (asc).

An assessment of the applicable distributions was then made for the four probabilities. In the case of LF (des), an upper 4σ bound of 0.5 was defined for the distribution, assuming a normal distribution. For LF (asc), an upper 4σ bound of 0.2 was defined, again assuming a normal distribution. And for LO (asc), given the small value of the mean (0.008), a lognormal distribution was judged to be more applicable, as greater uncertainty is expected for small defined values. For this distribution, an Error Factor of 5 was assumed. For the normal distributions, values below zero should be truncated when using the defined distributions.

In the case of LO (des), data is available for a Bayesian update of the assessed value, so the distribution needs to be defined much broader than for the other cases (where the posterior was being defined directly), in order to overlap the likelihood function of the evidence. The prior distribution was defined using 0.2 as the mean value for a maximum entropy ($\sigma = 1.0$) lognormal distribution. This was updated with evidence of 0 APU failures in 12 APUs exposed to other units leaking. Note the following for each leak: There are 2 opportunities for another APU to fail owing to the leak and 1 opportunity for itself to fail. For 6 leaks, there are $6 \times 2 = 12$ opportunities for failure of another APU owing to the leak. None has occurred. The mean value of LO (des) drops to 0.07 given this evidence. The result of the Bayesian analysis is shown graphically in Figure 9.2-7.

9.2.2.8.1 Sensitivity Treatment of APU 3 Failures

The previous section described the baseline treatment of these conditional probabilities. In the case of APU failure due to another units leakage (LO), it could be argued that APU 3 needs to be treated differently. APU 3 is physically located about 6' (on the starboard side) from the other two units, which are only a few inches apart. Thus, we believe that there is a lesser chance of APU 3 failing due to leakage in unit 1 than an APU 2 failure.

Our fault tree treatment is conservative in that each APU is considered "identical". It does not capture "full credit" for cases in which the actual APU 3 is leaking, which would lead to reduced LO conditional probabilities for both of the other units.

One way of capturing this logic would be to drop the LO conditional probability to a lower value for all of the APU 3 terms. In order to illustrate the affect this would have on the results, two of the most significant leakage fault trees have been quantified, at the mean value, for these two cases. For the baseline case:

- OK Initial State on Entry, Seq. 16 4.159E-04
- OK Initial State on Entry, Seq. 17 1.700E-04

For the sensitivity case, using as an example 0.01 as the unit 3 LO (des) probability:

- OK Initial State on Entry, Seq. 16 2.479E-04
- OK Initial State on Entry, Seq. 17 6.214E-05

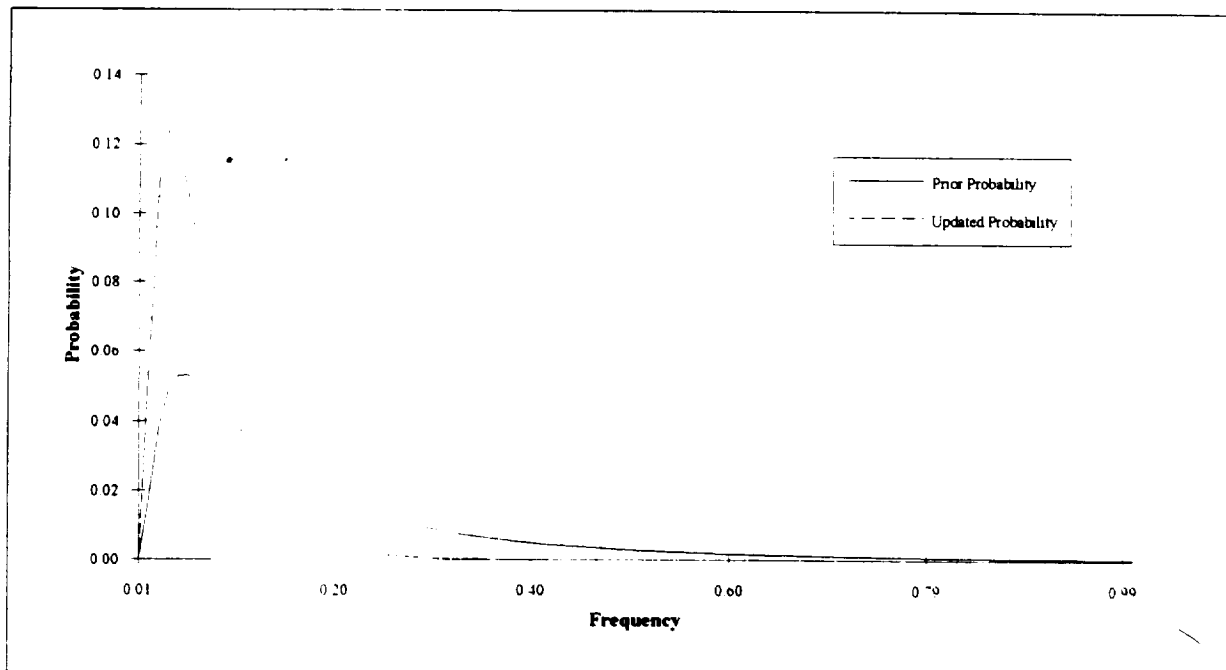


Figure 9.2-7: Bayesian Analysis Result for LO (Des)

9.2.2.9 Unsuccessful Single APU/HYD Unit Reentry, TAEM and Landing (UL)

This prior distribution was generated according to judgment weighted by several factors. First, such landings are regularly simulated successfully in training. To the extent that the simulator is successful in characterizing the vehicle response given a single APU/HYD unit, this gives credence to a very high probability of success. However, this is tempered by the fact that a single APU/HYD unit landing is not certified by the program. Unfavorable weather conditions coupled with slower control rates could potentially indicate a much higher probability of a failed landing. The assessment team has translated this into a range of 80% to 100% for a successful landing. It was also determined that the lack of a strong conviction for any values within this range warranted a uniform distribution for this range.

ID	$\beta\delta$ -factor	PRIOR (/hr or /demand)			
		Mean	Median	5th	95th
CE	N/A	0.5 (LL) 0.88 (TU)			
CF	Calculated	using applicable	MGL method	formulas	
CL	Calculated	using applicable	MGL method	formulas	
CO	N/A	1			
CS	Calculated	using applicable	MGL method	formulas	
HB	N/A	0.9			
ID	N/A	9.150E-03/hr	6.956E-03/hr	3.059E-03/hr	2.174E-02/hr
IF	N/A	9.150E-03/hr	6.956E-03/hr	3.059E-03/hr	2.174E-02/hr
IS	N/A	1.205E-02/start 9.150E-03/hr	7.949E-03/start 6.956E-03/hr	3.322E-03/start 3.059E-03/hr	3.342E-02/start 2.174E-02/hr
LA	N/A	0.0 (asc) 0.1667 (des)			
LD	N/A	0.0 (asc) 0.1667 (des)			
LF OS	N/A see posterior	1.0E-01 (asc)	1.0E-01 (asc)	6.0E-02 (asc)	1.4E-01 (asc)
LK	N/A	1.890E-04/hr	1.152E-04/hr	2.224E-05/hr	5.971E-04/hr
LL	N/A	2.8E-05			
LO LS	N/A	8.0E-03 (asc) 2.0E-1 (des)	5.0E-03 (asc) 1.2E -01	9.9E-04 (asc) 2.3E-02	2.5E-02 (asc) 6.36-01
LU	N/A	1.0 (asc) 0.8333 (des)			
LZ	N/A	1.0 (asc) 0.8333 (des)			
SI	N/A	1.0 (LL) 0.88 (TU)			
SR	N/A	0.98795/start	0.99205/start	0.99668/start	.96658/start
TU	N/A	2.518E-04	7.530E-05	6.733E-06	9.403E-04
UL	N/A	0.1	0.1	0.01	0.19

Table 9.2-8: Prior Probability Distributions

9.3 Posterior Distributions for APU/HYD/WSB Failure to Run and Start (Ascent and Descent)

Posterior distributions were determined by updating the prior distributions with available data using Bayes' Theorem. Data points not only include failures of the APU and HYD systems, but also the Water Spray Boiler (WSB). WSB failures, which lead to an APU shutdown and subsequent hydraulic loss, were not examined in the previous 1987 study, so data was extracted for these failures from all Shuttle flights. Other data points pertaining to these failures were taken from post-Challenger flights (1988) to STS-65 (flight 63, 7/8/94).

9.3.1 Water Spray Boiler Failures Used in the Analysis

9.3.1.1 03-23-1982 STS-3

WSB 3 freeze-up during ascent. APU temperature message at lift-off plus 4 minutes 23 seconds reported lube oil temperature climbing. Controller B was then selected, but the temperature continued to rise. APU 3 shutdown at liftoff plus 8 minutes, and the right main engine went into hydraulic lock-up. After ascent, at lift-off plus one hour, controller A was then selected; both controllers appeared to be working properly. The maximum APU 3 lube oil temperature was 330°F, and the maximum bearing temperature was between 355 and 360°F. FCS checkout tested both controllers, and both were 100% nominal. This situation was also seen on STS-1 and 2.

9.3.1.2 08-02-1991 STS-43

WSB 2 failed to provide cooling to the auxiliary power unit 2 lube oil throughout the mission. APU 2 (serial number 208) has been involved in lube oil over temperatures during seven of its eight flights. The WSB did not cool the lube oil on controller A following ascent. The crew switched to controller B when the lube oil return temperature reached approximately 297°F. The APU was operated an additional 1.5 minutes on the B controller, and still no cooling was observed. The APU was shutdown when the lube oil return temperature reached 323°F. The WSB is designed to control the lube oil temperature to 250±2°F.

An extended flight control system check-out using APU 2 was performed and the WSB was not cooling on either controller. The APU ran for 11 minutes during check-out, then was shutdown and declared lost. During descent, APU 2 was activated at terminal area energy management due to the lack of cooling. The lube oil reached 259°F before shutdown after wheel stop with no evidence of cooling. The spray boiler may not have had the chance to function, however, as this temperature is close to the 250°F control limit.

9.3.1.3 09-12-1992 STS-47

During ascent, WSB 3 (serial number 15) exhibited no cooling until just prior to the early shutdown of APU 3. The lube oil temperature reached approximately 292°F when the controller was switched from A to B. The lube oil temperature continued to rise to 311°F when the decision was made to shut down APU 3 early. Prior to APU 3 deactivation, the WSB GN2 regulator outlet pressure indicated that spraying had begun. WSB 3 continued to spray until the spray logic was turned off (1 minute 43 seconds). Steady-state cooling was never achieved on either controller since the lube oil temperature was not allowed to drop to 250°F prior to boiler spray logic shutdown.

APU 3 was selected to perform FCS checkout. The checkout time frame was extended to verify WSB 3 cooling performance. The extended run time demonstrated satisfactory cooling on both controllers (3 minutes 42 seconds for B, then 1 minute 47 seconds for A). WSB lube oil and hydraulic cooling performance during entry was nominal.

Spray bar freeze up remains the most likely cause of the WSB failure, although it could have resulted from spray valve or controller failures.

9.3.1.4 01-13-1993 STS-54

During ascent, WSB 3 (serial number 15) exhibited no cooling until just after the early shutdown of APU 3. The lube oil return temperature reached approximately 295°F when the WSB was switched from controller A to B. The lube oil return temperature reached 315°F when the decision was made to shut down APU 3 early. After deactivation, the WSB 3 GN2 regulator pressure indicated that spraying had started. WSB 3 continued to spray until the spray logic was turned off (approximately 35 seconds). Steady-state cooling was never achieved on controller A or B.

APU 3 was selected to perform the FCS check-out. The FCS checkout time frame was extended to verify WSB cooling performance. The extended APU 3 run-time demonstrated satisfactory cooling on both controllers, with a minor overcool observed on controller A. APU performance using controller B during entry was nominal.

Spray bar freeze-up remains the most probable cause of this cooling problem. However, data analysis also indicated that the local pressure at the vent nozzle of system 3 during ascent was somewhat higher than the other two systems. This high pressure is due to the location of the system 3 vent nozzle outlet (it is farther forward than the system 1 and 2 vent nozzle outlets). System 3's pressure remains higher than the other systems for the first 80 seconds of ascent, which is believed to be a contributing factor toward the repeated freeze-up anomalies observed in system 3.

Spray bar freeze-up conditions occur when the water triple point condition is met inside the heat exchanger. In the worst case freeze-ups, it is postulated the water triple point was reached prior to MECO. By increasing the water preload, the duration of heat exchanger tube bundle/water preload contact can be increased, which will reduce the likelihood/severity of spray bar freeze-up by maintaining pressure above the water triple point past MECO. The ongoing spray bar freeze-up test analysis indicates that the severity of the bar freeze-up at water triple point conditions may inversely correlate to the amount of water in the boiler. Therefore, KSC has been requested to preload WSB 3 to 5 +/-0.1 lbs. of water (normal is 3.75 +/-0.24 lbs.).

9.3.2 Possible Water Spray Boiler Failure

It is unknown whether or not this reported problem is an actual failure or not. For this analysis, it has not been considered as an actual data point.

9.3.2.1 04-29-1985 STS-51B

Shortly after MECO, the backup flight system indicated an APU 3 lube oil over temperature condition. The crew switched from controller A to B at a lube oil temperature of 320°F. The temperature continued to rise for an additional 20 seconds and reached a peak of 337°F. The crew was instructed to shutdown APU 3 to avoid reaching the lube oil temperature limit of 355°F. The

APU 3 lube oil temperature had decreased to approximately 320°F at shutdown, indicating that water spray boiler controller 3B was properly controlling lube oil cooling. Post flight testing has been unsuccessful in duplicating this problem. The A controller was replaced.

9.3.3 Possible Hydraulic System Failure

9.3.3.1 02-28-1990 STS-36

Appendix C contains descriptions from PRACA records and hazards analyses of a "near-miss" failure involving a flex hose rupture in the hydraulic system.

9.3.4 Updated Posterior Distribution

The four WSB failures in Section 9.3.1 were counted as APU shutdowns. All three of these failures occurred during the ascent phase. One of these failures was permanent and caused a late re-start of the APU during the entry phase, but was not counted as a failure during the reentry phase because it successfully completed its mission. For reentry, the hydraulic system rupture is counted as a possible APU/HYD unit failure in the update. The methodology for this type of update is described in section 9.2.2.5, where in this case the weighting uses 50% for 1 failure and 50% for zero failures. In the data column, if no data is available (i.e., no "trials"), an N/A for not applicable is placed in the box.

The common cause failure calculations for the MGL formulas used the ID and IS values, assuming 20 minutes for ascent and 1 hour for descent. The MGL calculations also used generic β and γ values of 0.1 and 0.27, respectively.

Table 9.3-1 lists the data and corresponding posterior probability distributions for the basic events. The means from these data distributions are used as basic event probability distribution inputs for use in SAIC's CAFTA model.

ID	Data	POSTERIOR (/hr or /demand)			
		Mean	Median	5th	95th
CE	N/A	0.5 (LL) 0.88 (TU)			
CF	Calculated	using applicable	MGL method	formulas	
CL	Calculated	using applicable	MGL method	formulas	
CO	N/A	1			
CS	Calculated	using applicable	MGL method	formulas	
HB	N/A	0.9			
ID	4/63 hrs	2.078E-02/hr	1.931E-02/hr	1.030E-02/hr	3.622E-02/hr
IF	4/63 hrs	2.078E-02/hr	1.931E-02/hr	1.030E-02/hr	3.622E-02/hr
IS	0/189 starts 0 to 1/252 hrs	5.677E-03/start 6.479E-03/hr	4.448E-03/start 5.614E-03/hr	1.433E-03/start 2.369E-03/hr	1.194E-02/start 1.219E-02/hr
LA	N/A	0.0 (asc) 0.1667 (des)			
LD	N/A	0.0 (asc) 0.1667 (des)			
LF	N/A	1.0E-01 (asc)	1.0E-01 (asc)	6.0E-02 (asc)	1.4E-01 (asc)
OS	2/6 Leaks	3.0E-01 (des)	3.0E-01 (des)	2.2E-01 (des)	3.8E-01 (des)
LK	N/A	1.890E-04/hr	1.152E-04/hr	2.224E-05/hr	5.971E-04/hr
LL	N/A	2.8E-05			
LO	N/A	8.0E-03 (asc)	5.0E-03 (asc)	9.9E-04 (asc)	2.5E-02 (asc)
LS	0/12 Leaks	7.0E-02 (des)	5.3E-02 (des)	1.4E-02 (des)	1.6E-01 (des)
LU	N/A	1.0 (asc) 0.8333 (des)			
LZ	N/A	1.0 (asc) 0.8333 (des)			
SI	N/A	1.0 (LL) 0.88 (TU)			
SR	N/A	0.99432/start	0.99555/start	0.99857/start	0.98806/start
TU	N/A	6.962E-05	5.501E-05	1.974E-05	1.672E-04
UL	N/A	0.1	0.1	0.01	0.19

Table 9.3-1: Posterior Probability Distributions

9.4 APU/HYD/WSB ANALYSIS FOR SSME MODEL

The APU failure probability assessment for the SSME model being produced at SAIC is somewhat different than that for this APU model. First, the exposure time is at most 520 seconds instead of 20 minutes. Second, only 1 of the WSB failures is relevant (STS-3) for purposes of calculating engine hydraulic lockup probability.

We started with the prior distribution for IF, given in Table 9.2-6, multiplied against the 520 second time period to produce a probability of failure (POF). We updated with 1 failure in 63 missions to produce a posterior. This represents the case in which the WSB failure and APU shutdown continues to be representative of how MCC and crew will react to a WSB failure. Since STS-3, other WSB failures have not resulted in a call for APU shutdown before MECO. Flight Rules indicate that APU shutdowns should occur post-MECO.

We also updated the same prior distribution for IF with 0 failures in 63 missions. This is like saying that STS-3 never happened and gives an overly optimistic assessment. An accurate assessment lies somewhere in between. We used a weighted average of each posterior where each update was given equal probability of being the correct one.

The Bayesian calculation is shown in Figure 9.4.1.

The MGL method was used to calculate the probability of loss of hydraulics for a single engine and for two engines as follows:

1 Engine Goes into Hydraulic Lockup via Hydraulic Failure During Ascent

$$Q = 3(1 - \beta)q_{APU} = 3(1 - 0.1)1.5E-04 = \mathbf{4E-04}$$

2 Engines Go into Hydraulic Lockup via Hydraulic Failure During Ascent (First 5.6 minutes)

$$Q = 3/2(1 - \gamma)\beta(336/520)q_{APU} + 3(1 - \beta)^2(336/520)^2 q_{APU}^2 = \\ 3/2(1 - 0.27)0.1(336/520)1.5E-04 + 3(1 - 0.1)^2(336/520)^2 1.5E-04 = \mathbf{1E-04}$$

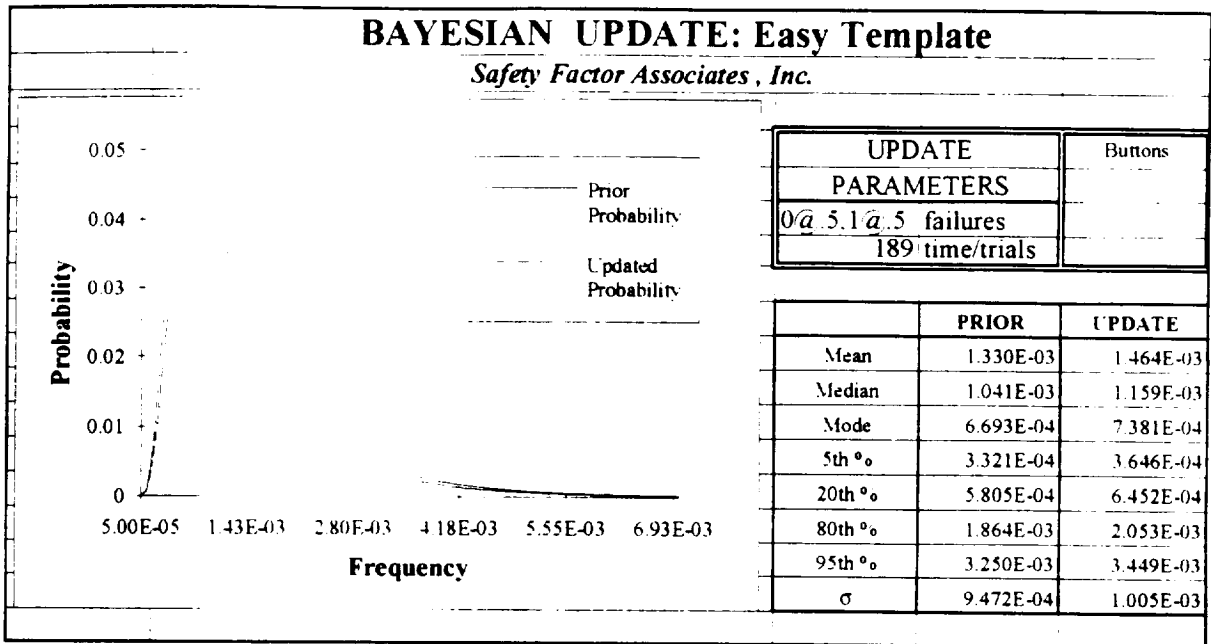
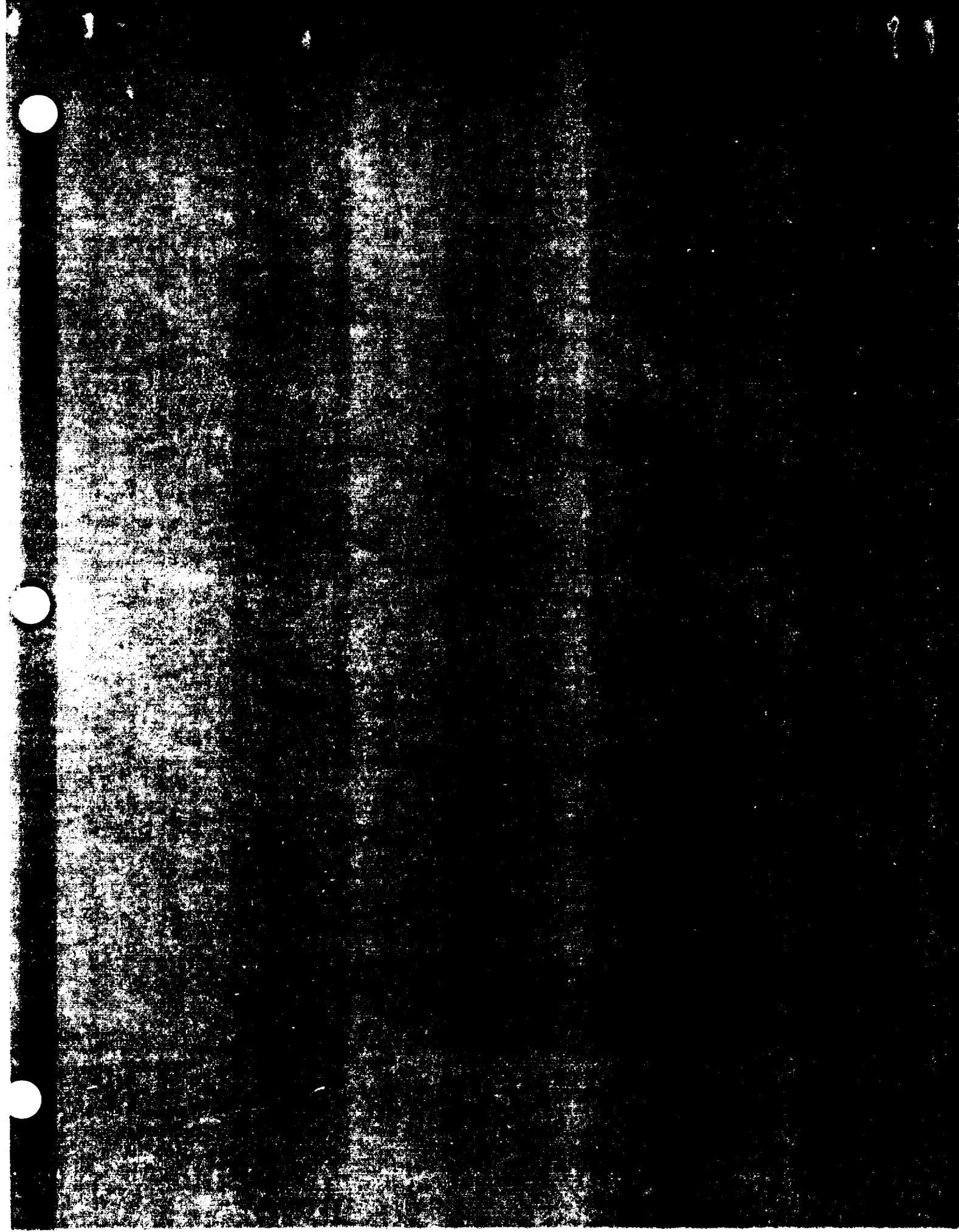
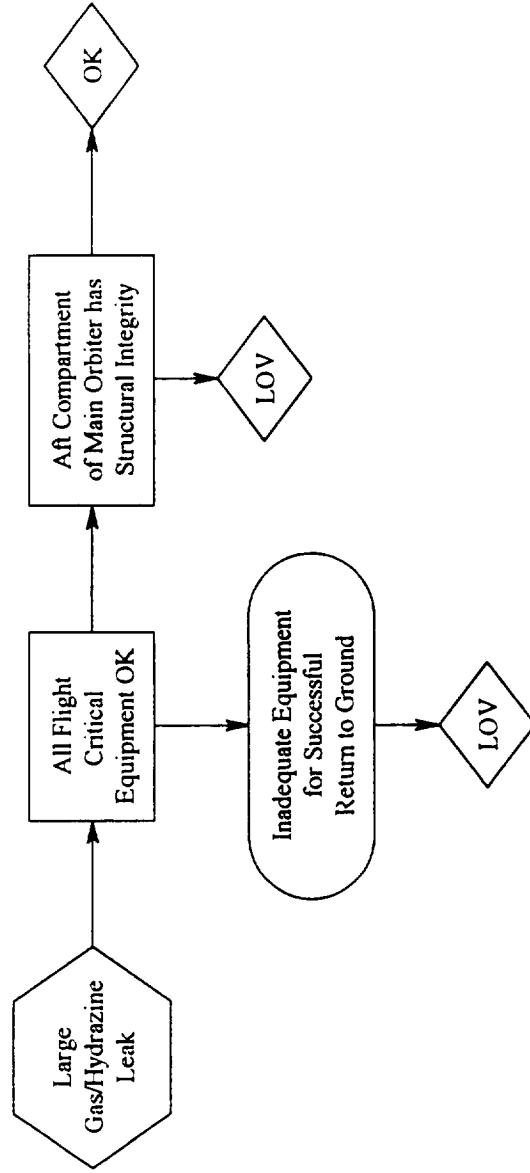


Figure 9.4-1: APU Failures on Ascent Causing SSME Hydraulic Lockup (POF)



Event Sequence Diagram of a Large Gas/Hydrazine Leak

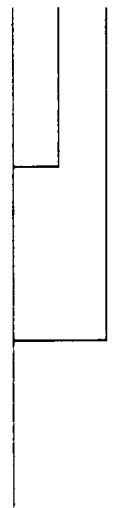


Assumption

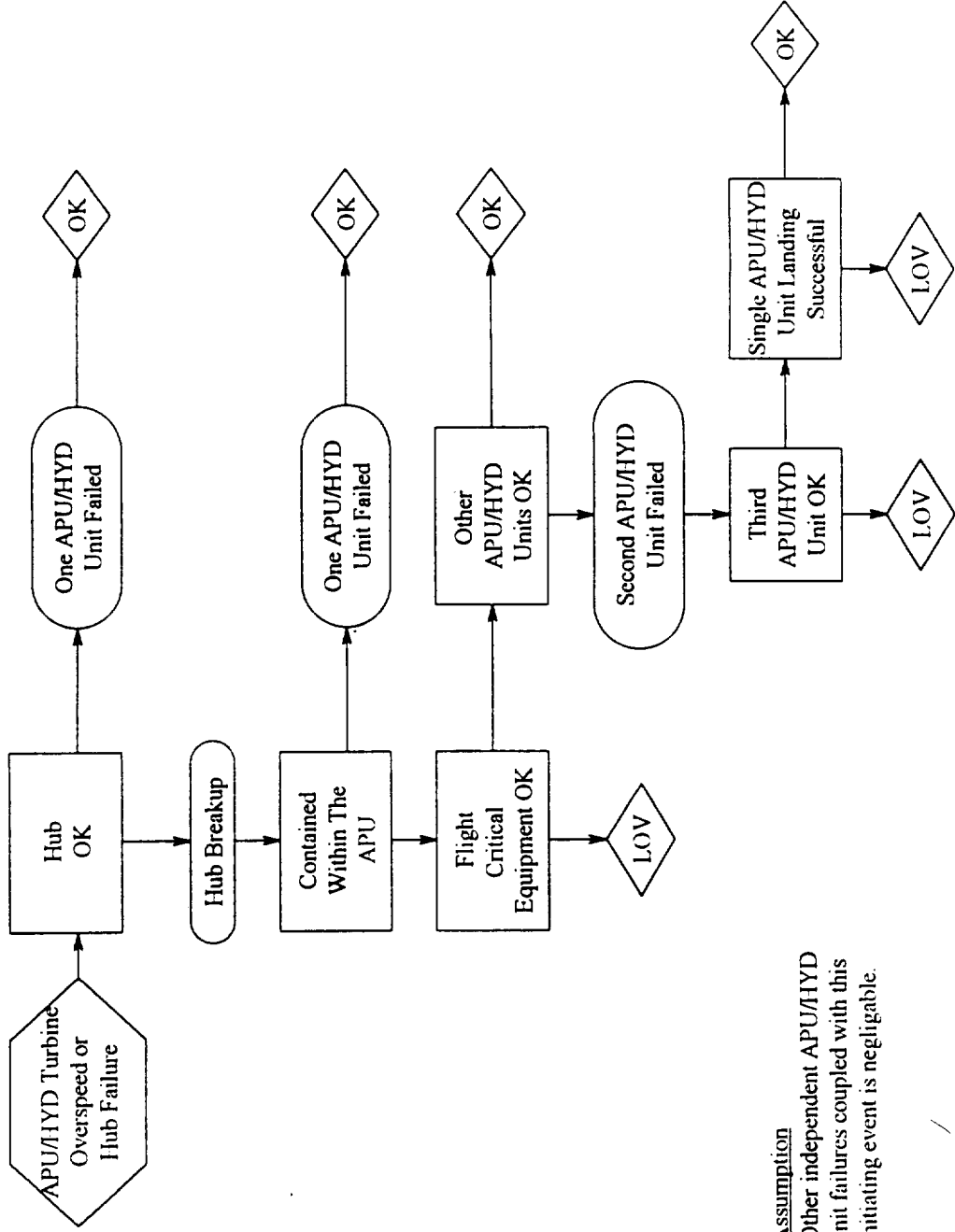
Because of the low frequency of severe exhaust gas leak, we have categorized this event with the unisolatable leaks. Separate categorization of the events would insignificantly change the estimated risk.

EVENT TREE OF A LARGE GAS/HYDRAZINE LEAK

LL	CE	SI	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
			1	LL	OK
			2	LLSI	LOV
			3	LLCE	LOV



Event Sequence Diagram for APU/HYD Turbine Overspeed and/or Hub Failure

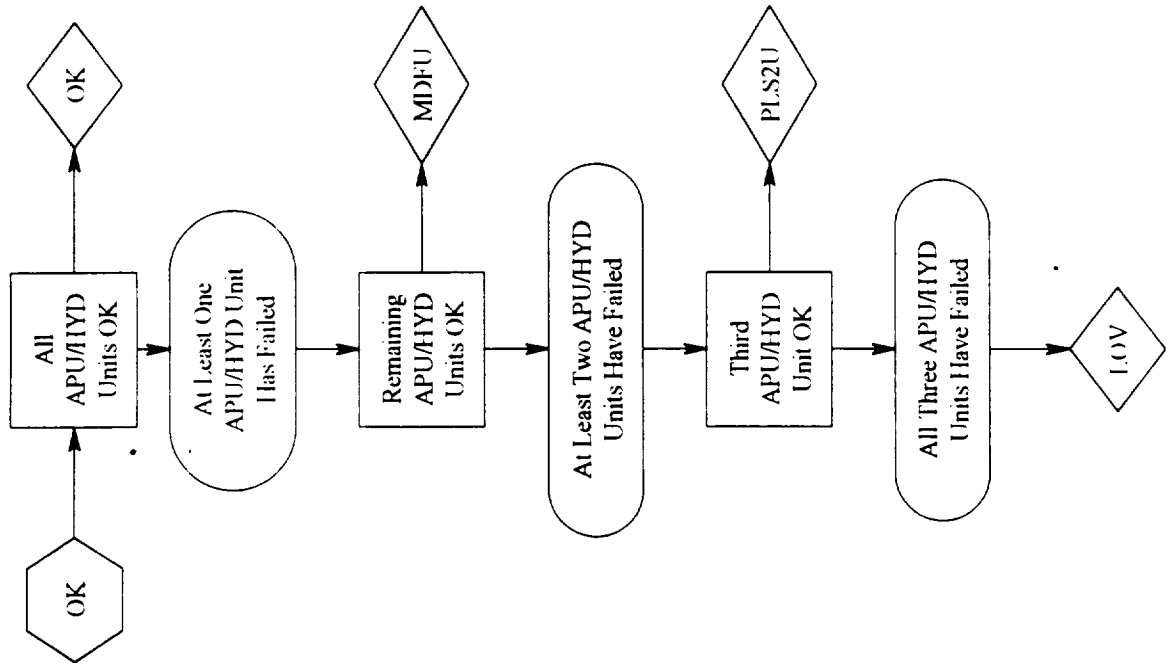


Assumption
Other independent APU/HYD
unit failures coupled with this
initiating event is negligible.

EVENT TREE OF APU/HYD TURBINE OVERSPEED AND/OR BREAKUP

TU	HB	CO	CE	2F	3F	UL	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
							1	TU	OK
							2	TUHB	OK
							3	TUHBCO	OK
							4	TUHBCO2F	OK
							5	TUHBCO2FUL	LOV
							6	TUHBCO2F3F	LOV
							7	TUHBCOCE	LOV

**Event Sequence Diagram for OK Start
Without a Hydrazine Leak During Ascent**

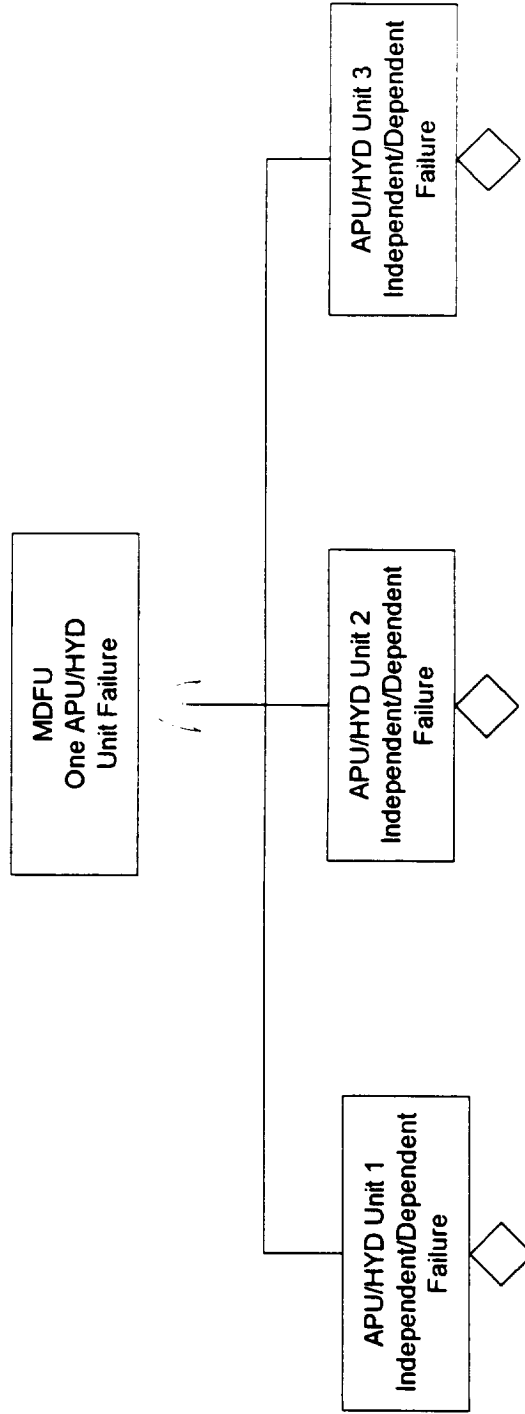


EVENT TREE OF AN OK START WITHOUT A HYDRAZINE LEAK DURING ASCENT

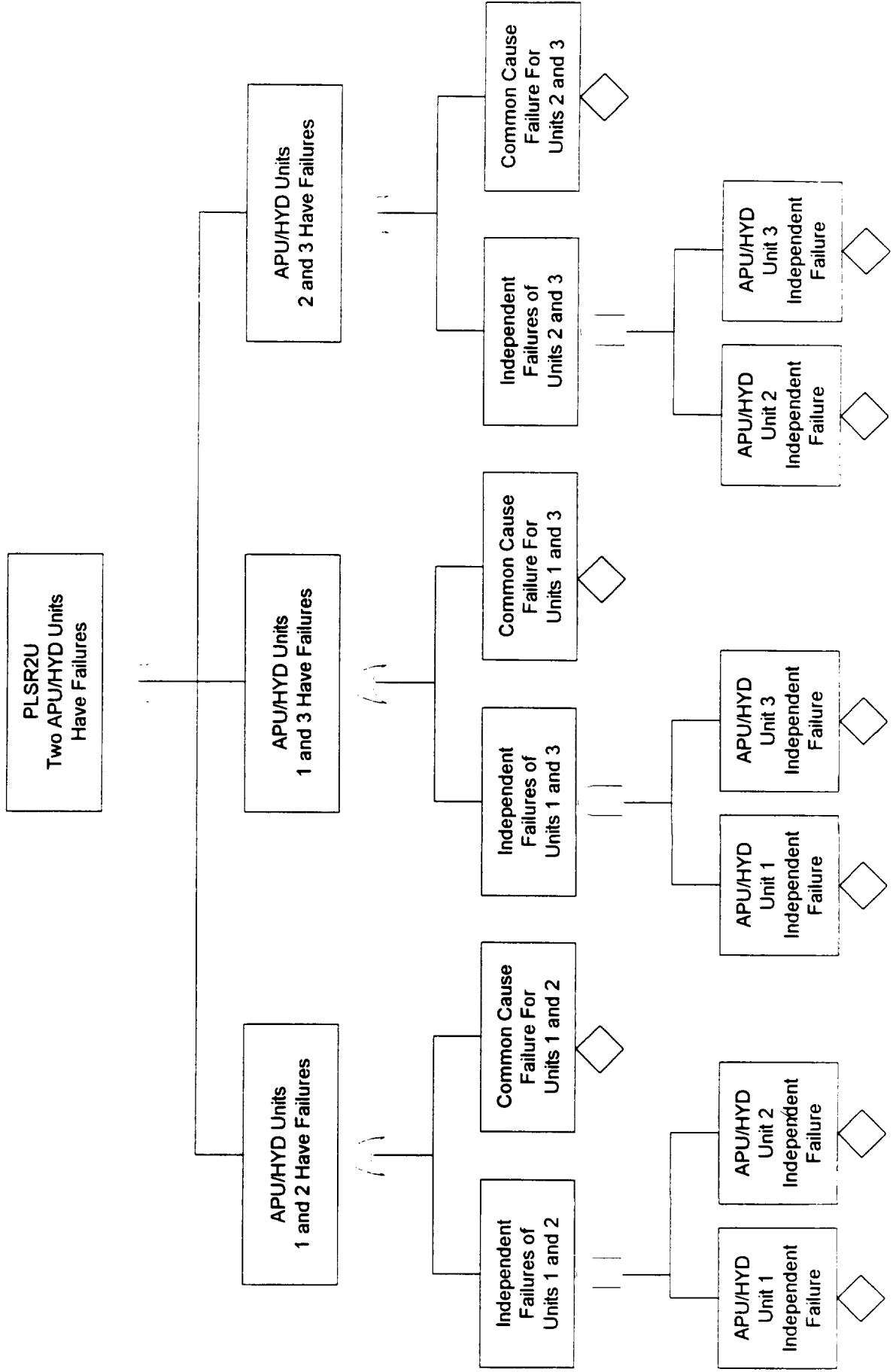
OK	1F	2F	3F	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	SEQUENCE STATE
_____	_____	_____	_____	1	OK	OK
_____	_____	_____	_____	2	OK1F	MDFU
_____	_____	_____	_____	3	OK1F2F	PLSR2U
_____	_____	_____	_____	4	OK1F2F3F	LOV

/

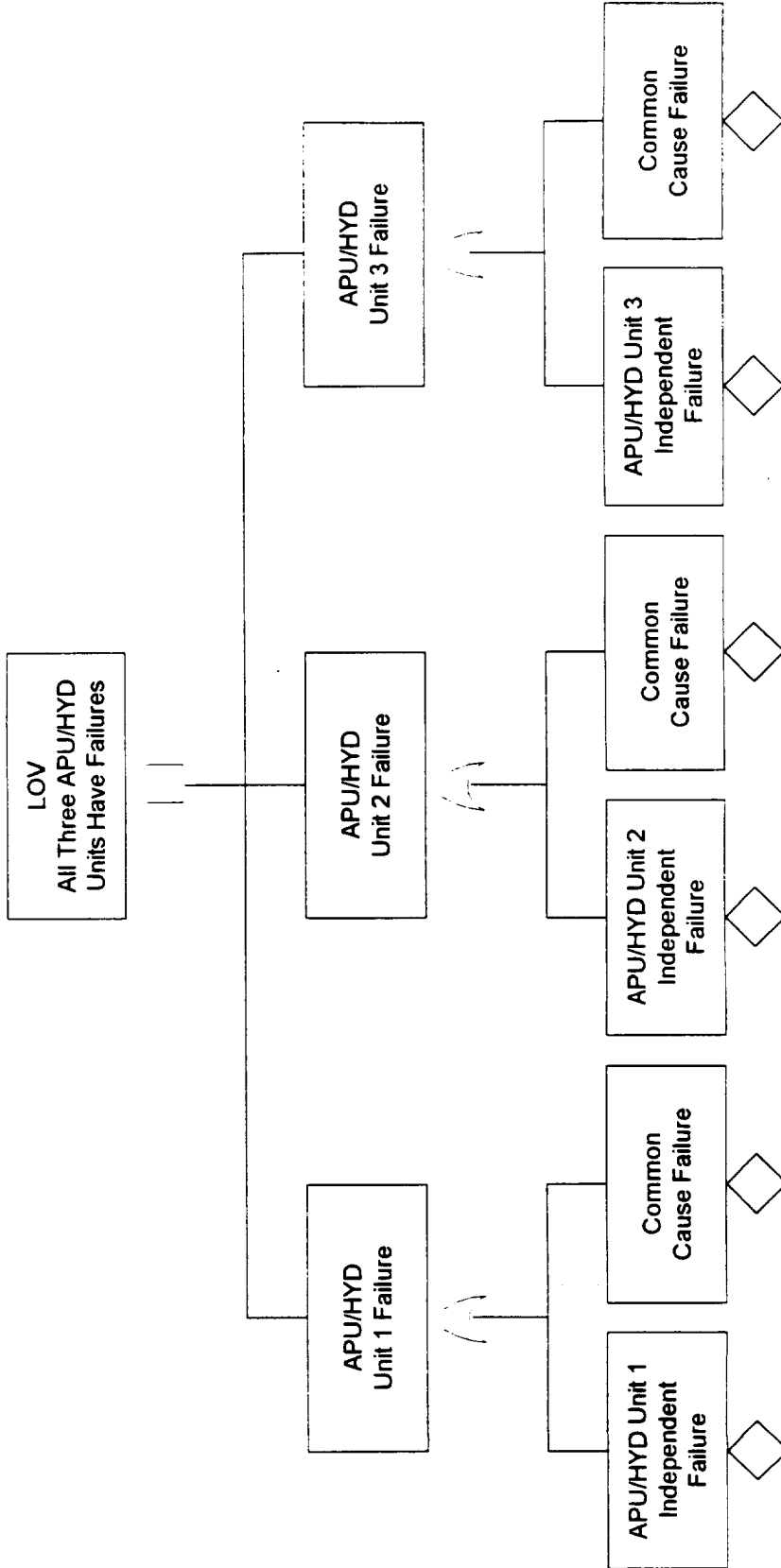
**Fault Tree For Sequence 2 MDFU
State From OK Start Without A
Hydrazine Leak During Ascent**



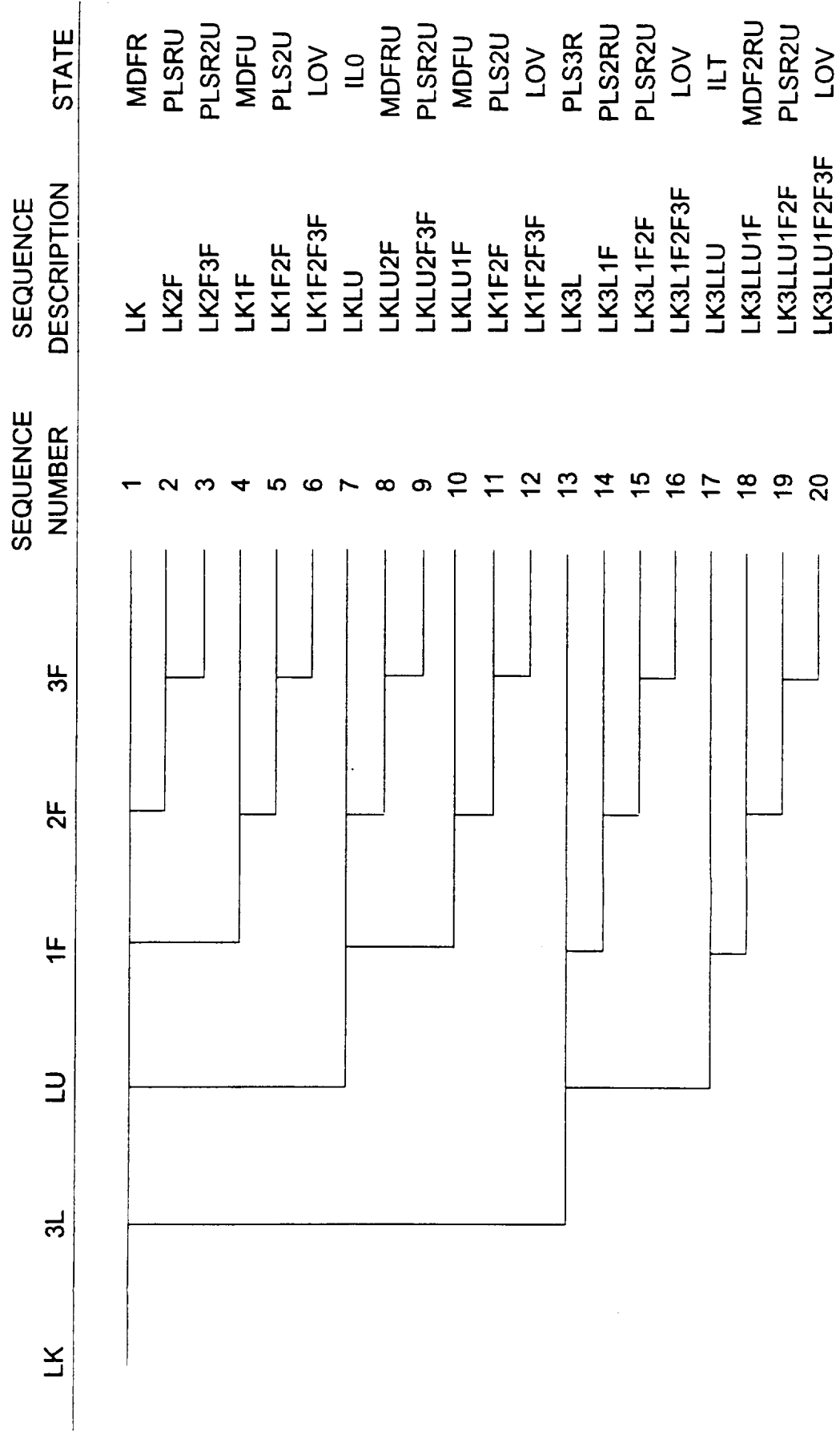
Fault Tree For Sequence 3 PLSR2U State From OK Start Without A Hydrazine Leak During Ascent



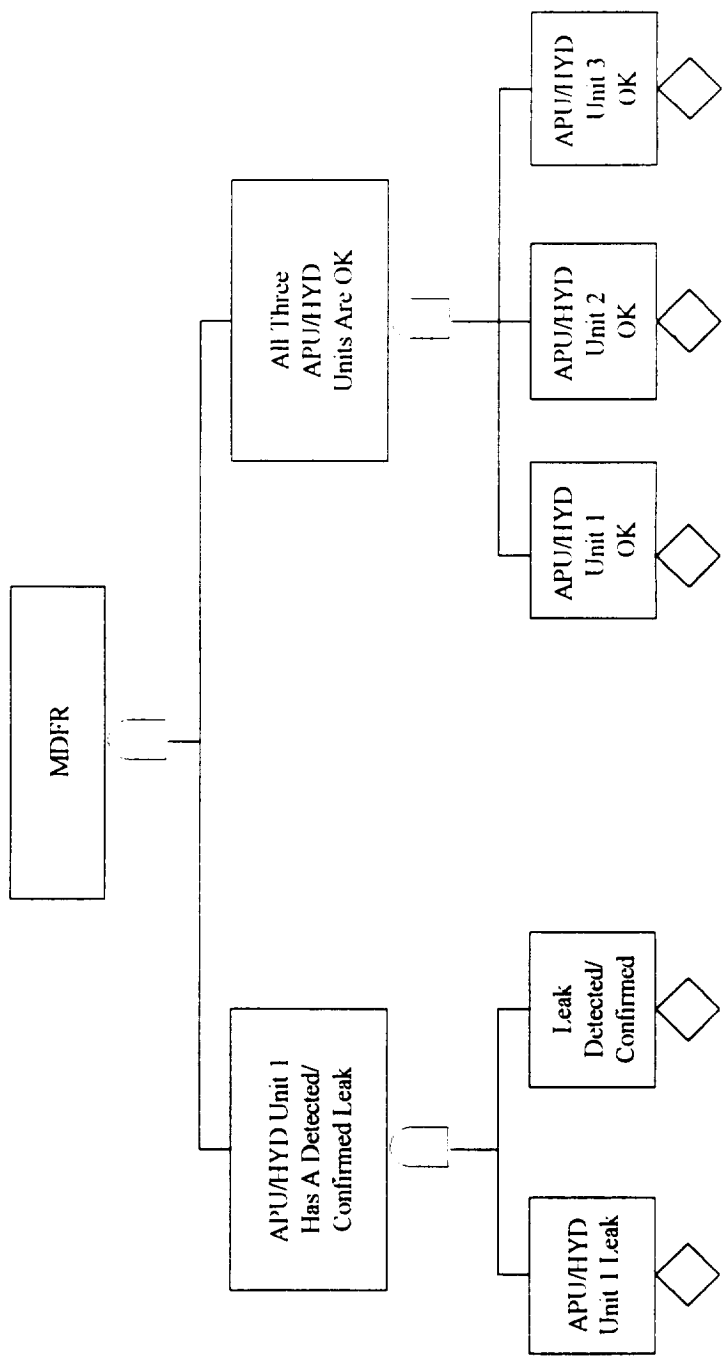
**Fault Tree For Sequence 4 LOV
State From OK Start Without A
Hydrazine Leak During Ascent**



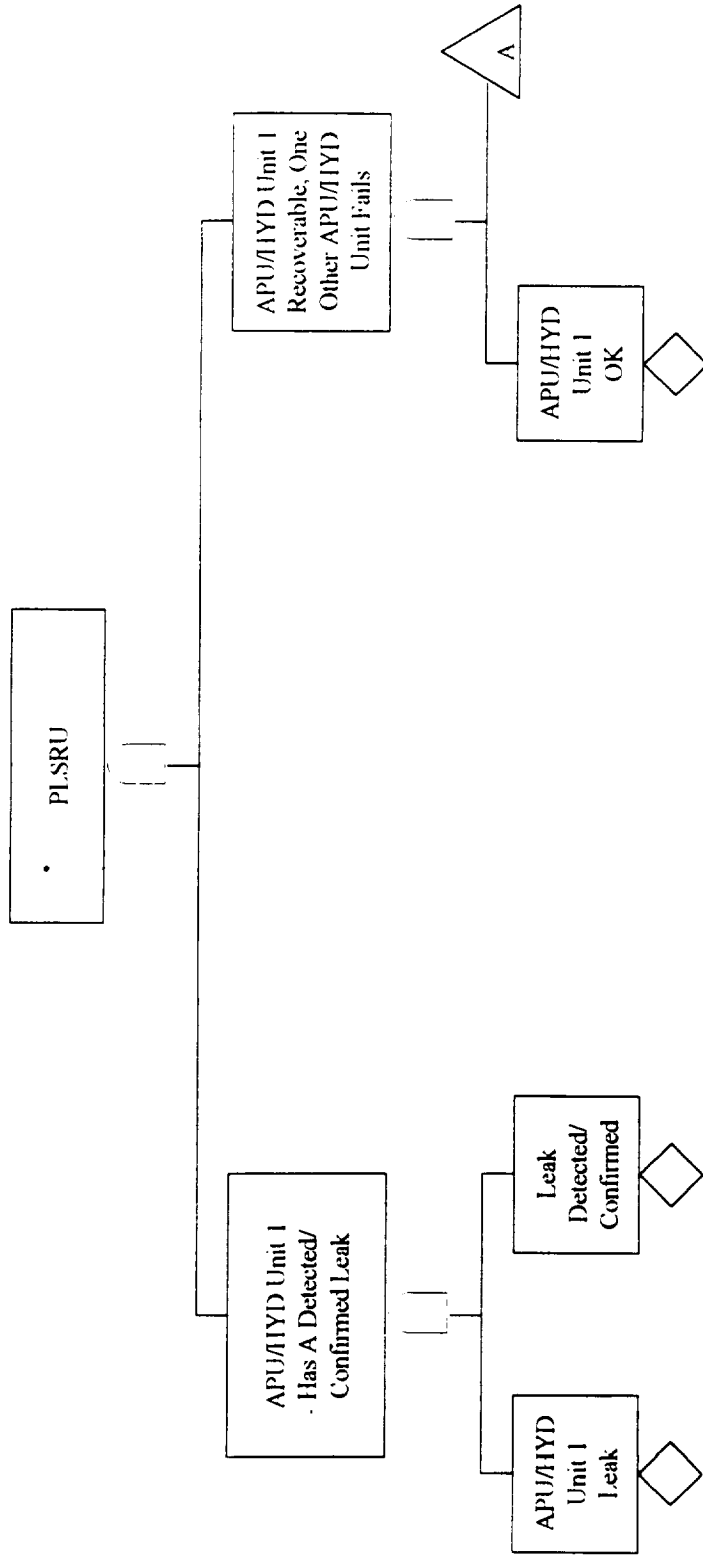
EVENT TREE OF APU/HYD HYDRAZINE LEAK STATE DURING ASCENT



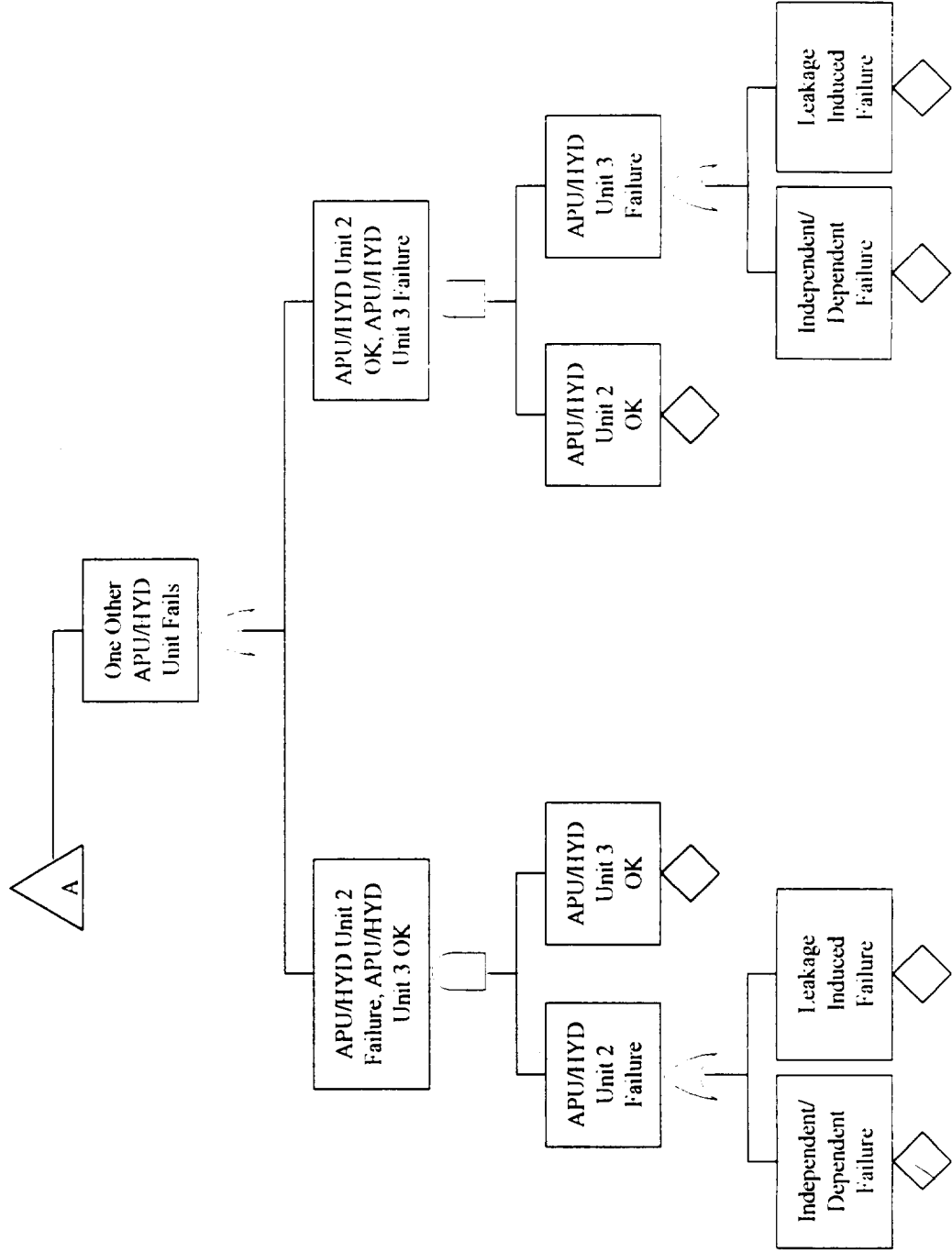
**Fault Tree for Sequence 1: MDRF State
From a Hydrazine Leak State During Ascent
one APU/HYD Unit has a Detected/Confirmed Leak
and is Recoverable**



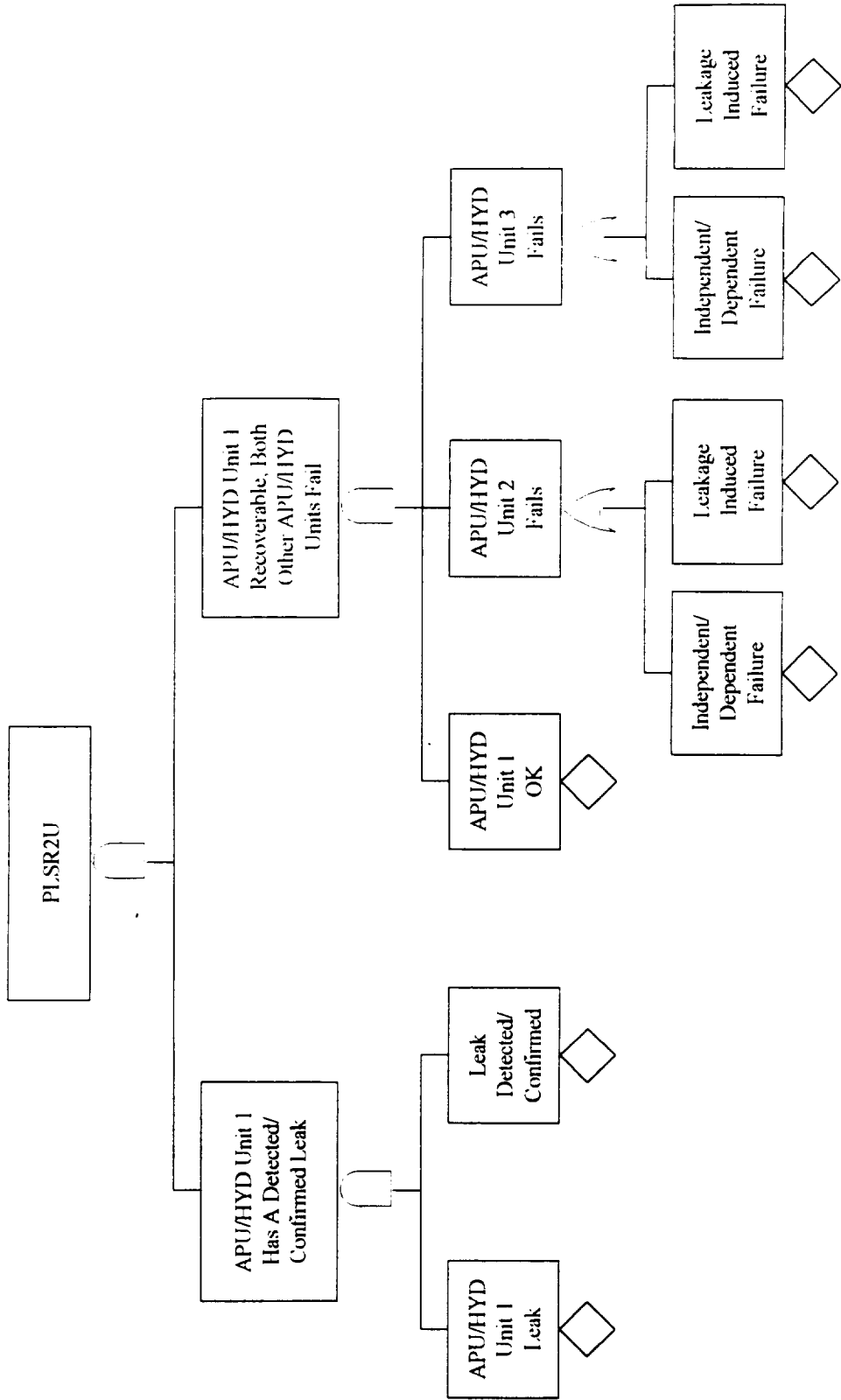
**Fault Tree for Sequence 4: PLSRU End State
 From a Hydrazine Leak During Ascent,
 one APU/HYD Unit has a Detected/Confirmed Leak
 and is Recoverable, one Other APU/HYD Unit Fails**



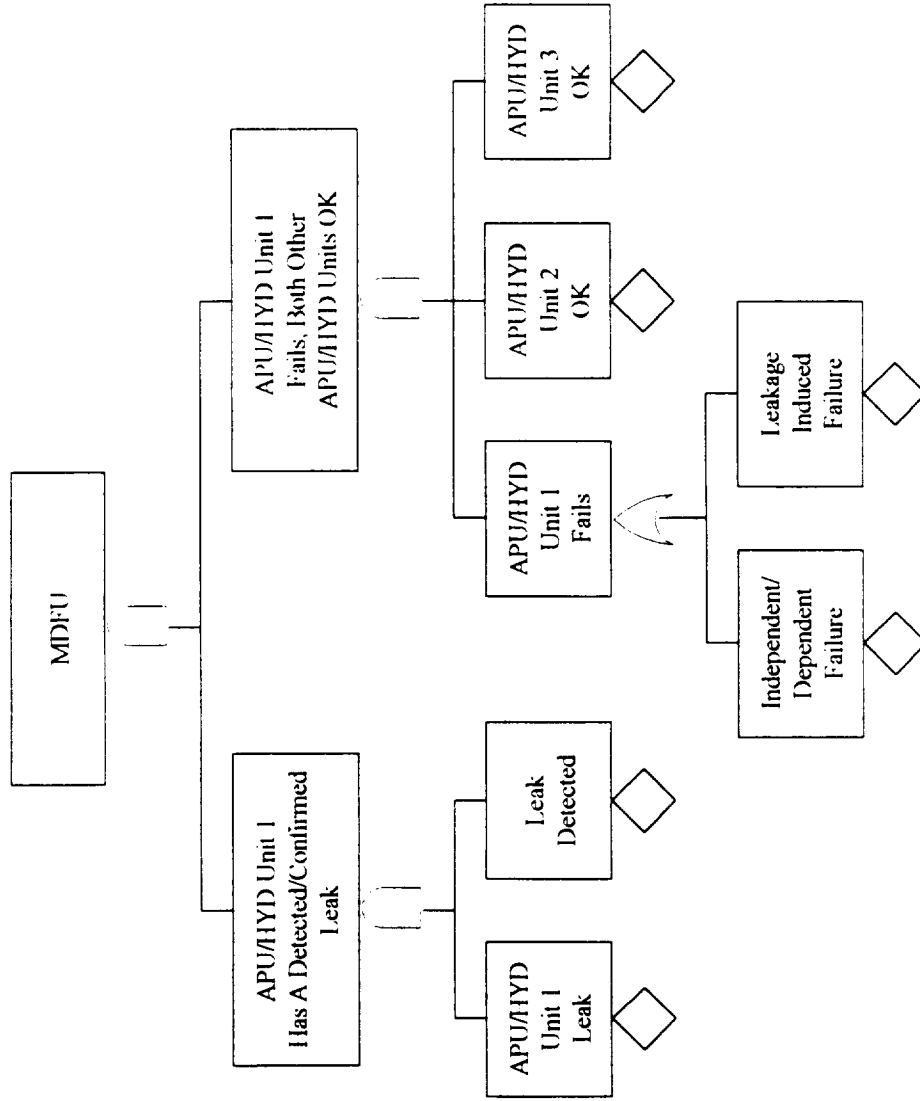
**Fault Tree for Sequence 2: PLSRU End State
 From a Hydrazine Leak Detected/Confirmed Leak
 one APU/HYD Unit has a Detected/Confirmed Leak
 and is Recoverable, one Other APU/HYD Unit Fails
 (Continued)**



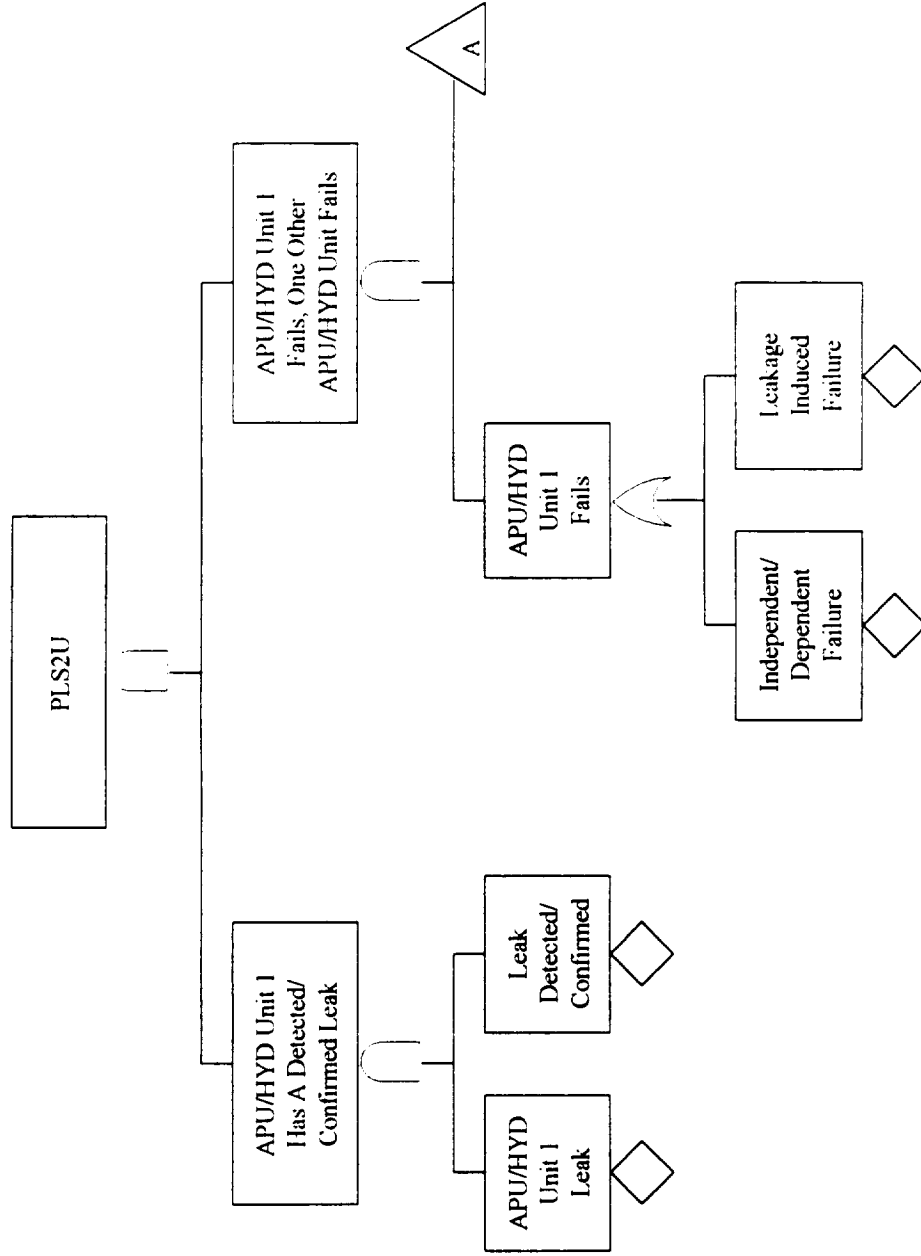
**Fault Tree for Sequence 3: PLSR2U End State
 From a Hydrazine Leak During Ascent, one APU/HYD
 Unit has a Detected/Confirmed Leak and is Recoverable,
 Both Other APU/HYD Units Fail**



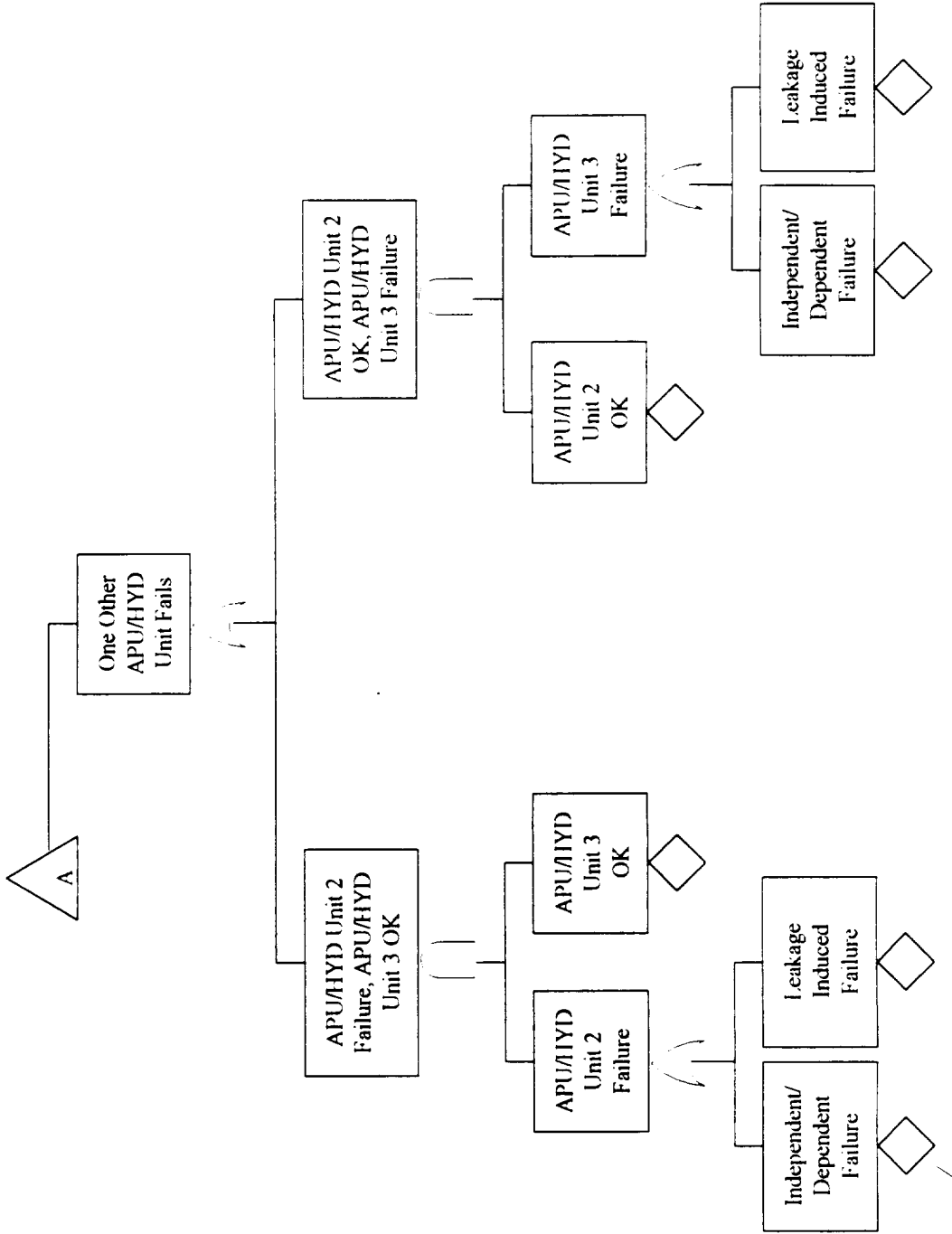
**Fault Tree for Sequence 4: MDFU End State
 From a Hydrazine Leak During Ascent, one
 APU/HYD Unit has a Detected/Confirmed Leak
 and Subsequent Failure**



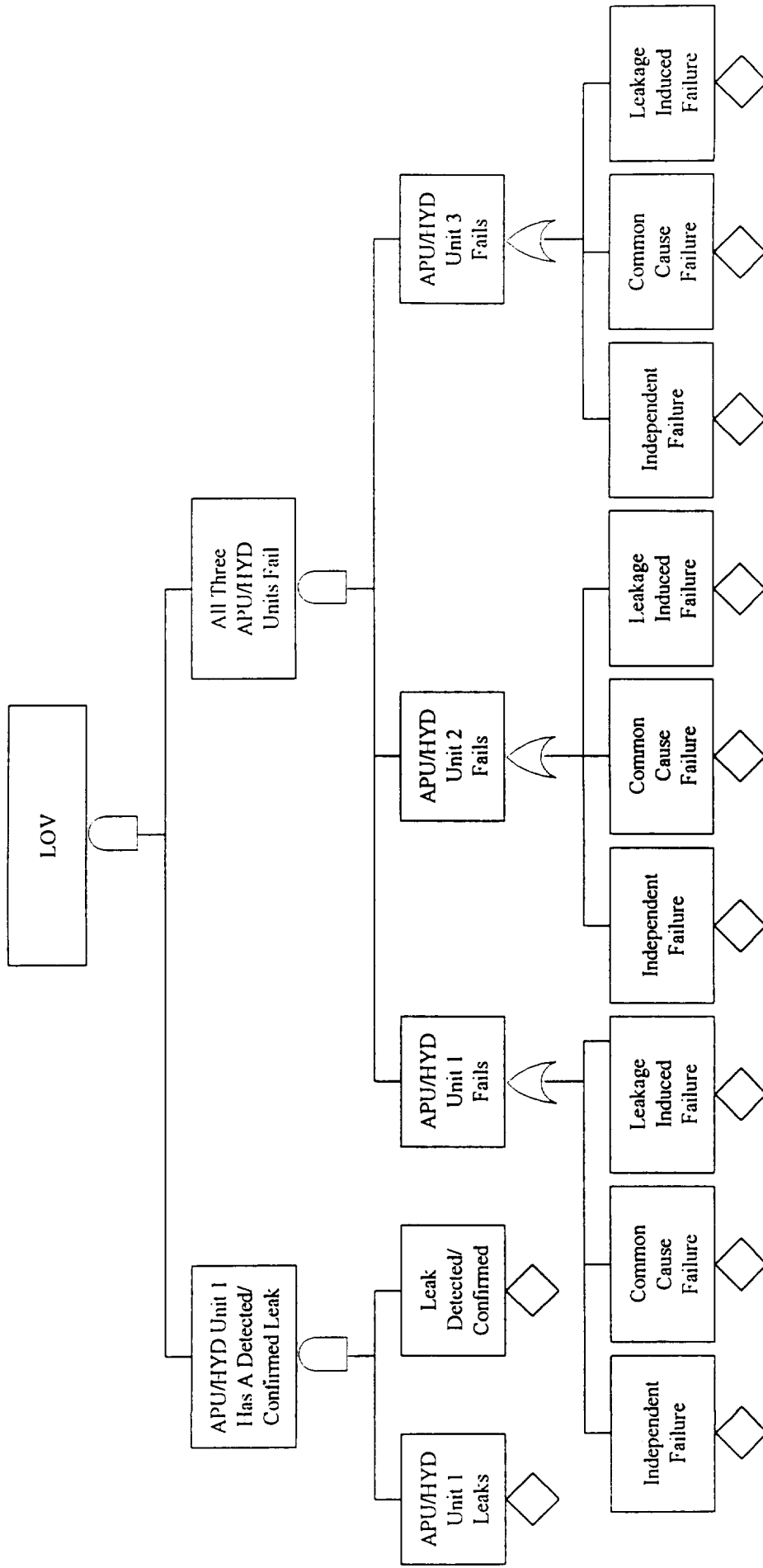
Fault Tree for Sequence 5: r'LS2U End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has a Detected/Confirmed Leak and Subsequent Failure, one Other APU/HYD Unit Also Fails



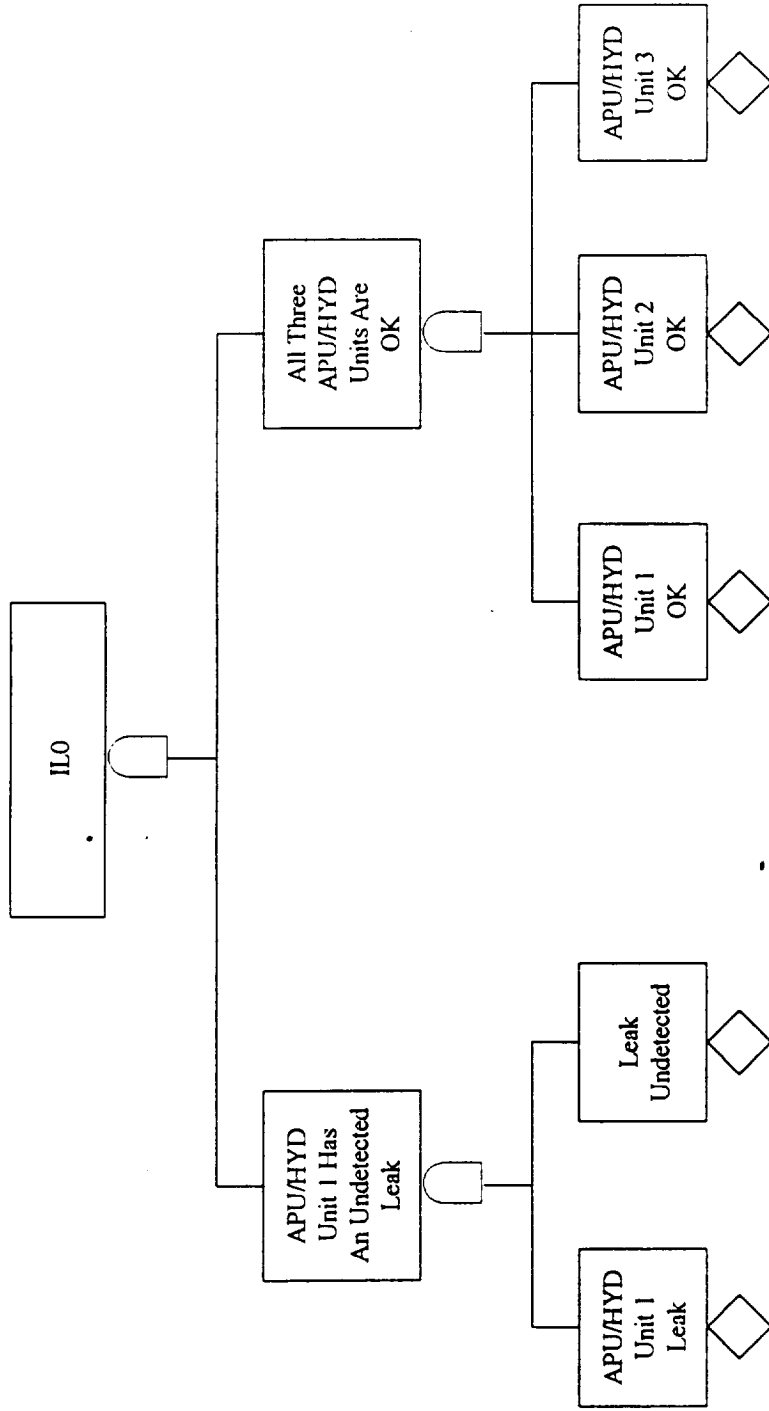
Fault Tree for Sequence 5: PLS2U End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has a Detected/Confirmed Leak and Subsequent Failure, one Other APU/HYD Unit Also Fails (Continued)



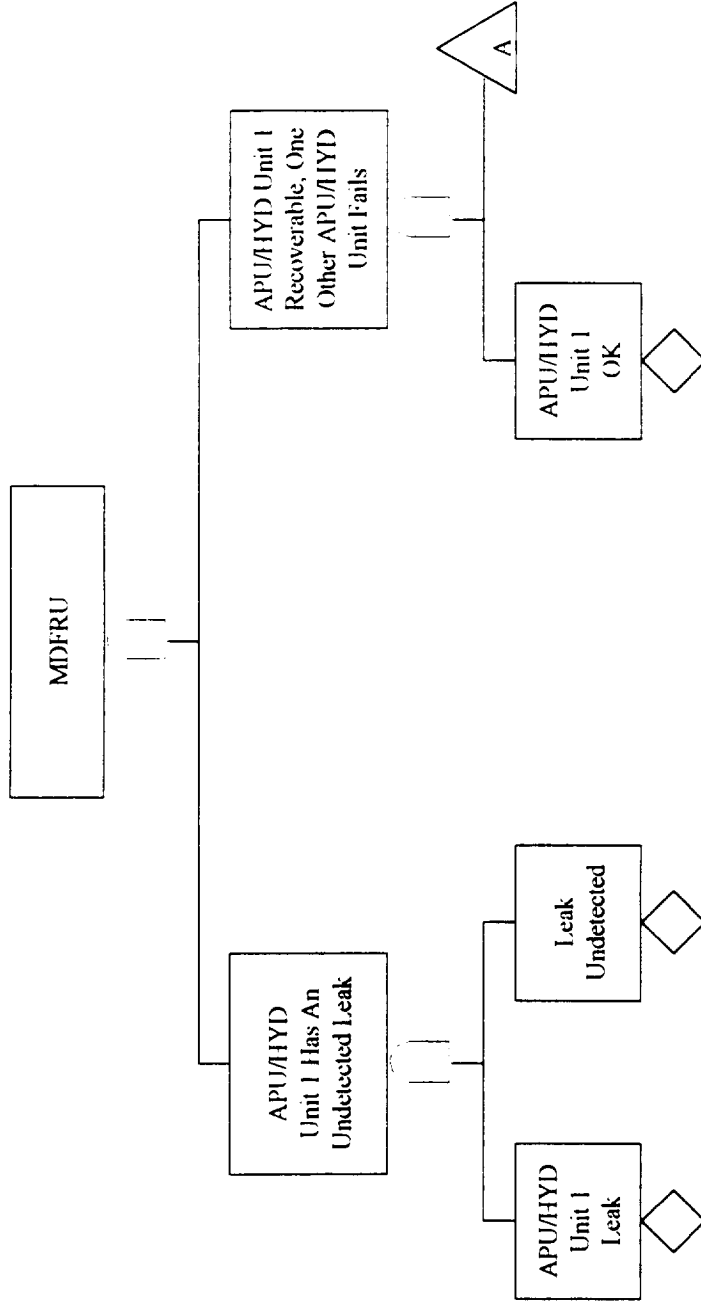
Fault Tree for Sequence 3: LOV End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has a Detected/Confirmed Hydrazine Leak and all Three APU/HYD Units Have Failures



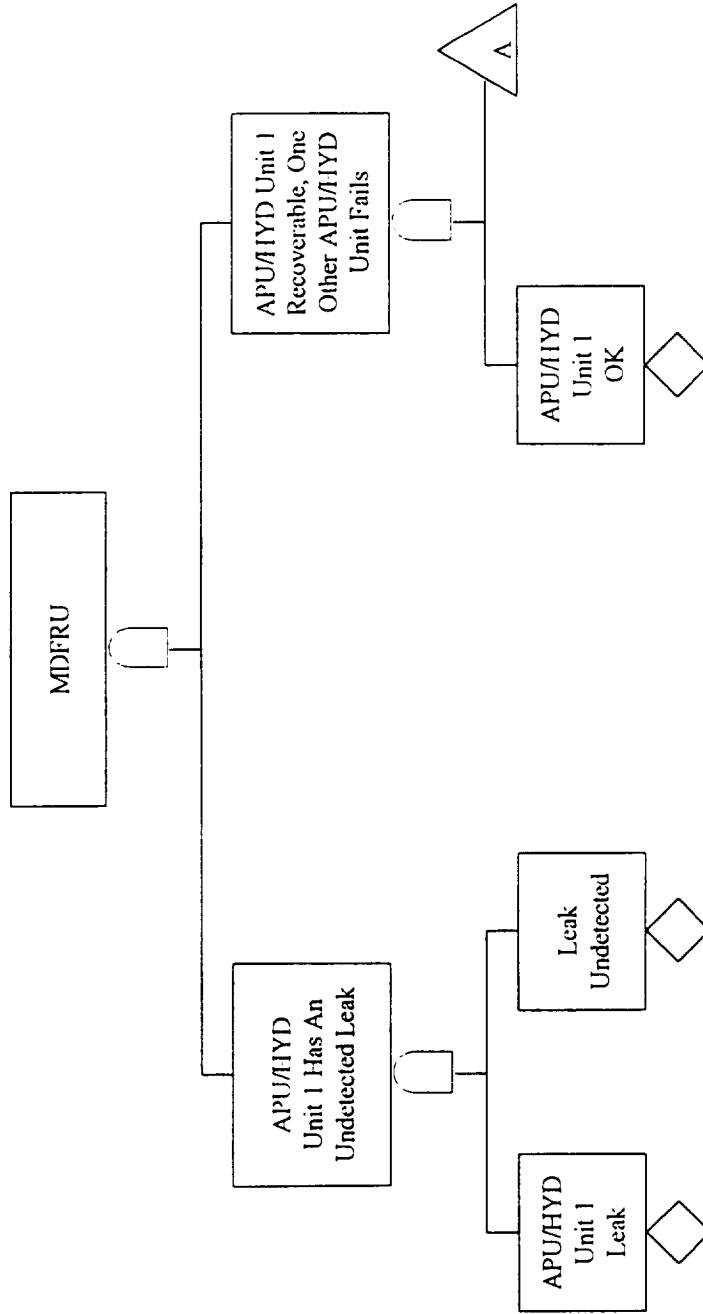
Fault Tree for Sequence 7: ILO End State From Hydrazine Leak During Ascent, one APU/HYD Unit has an Undetected Leak and no APU/HYD Units Have Failures



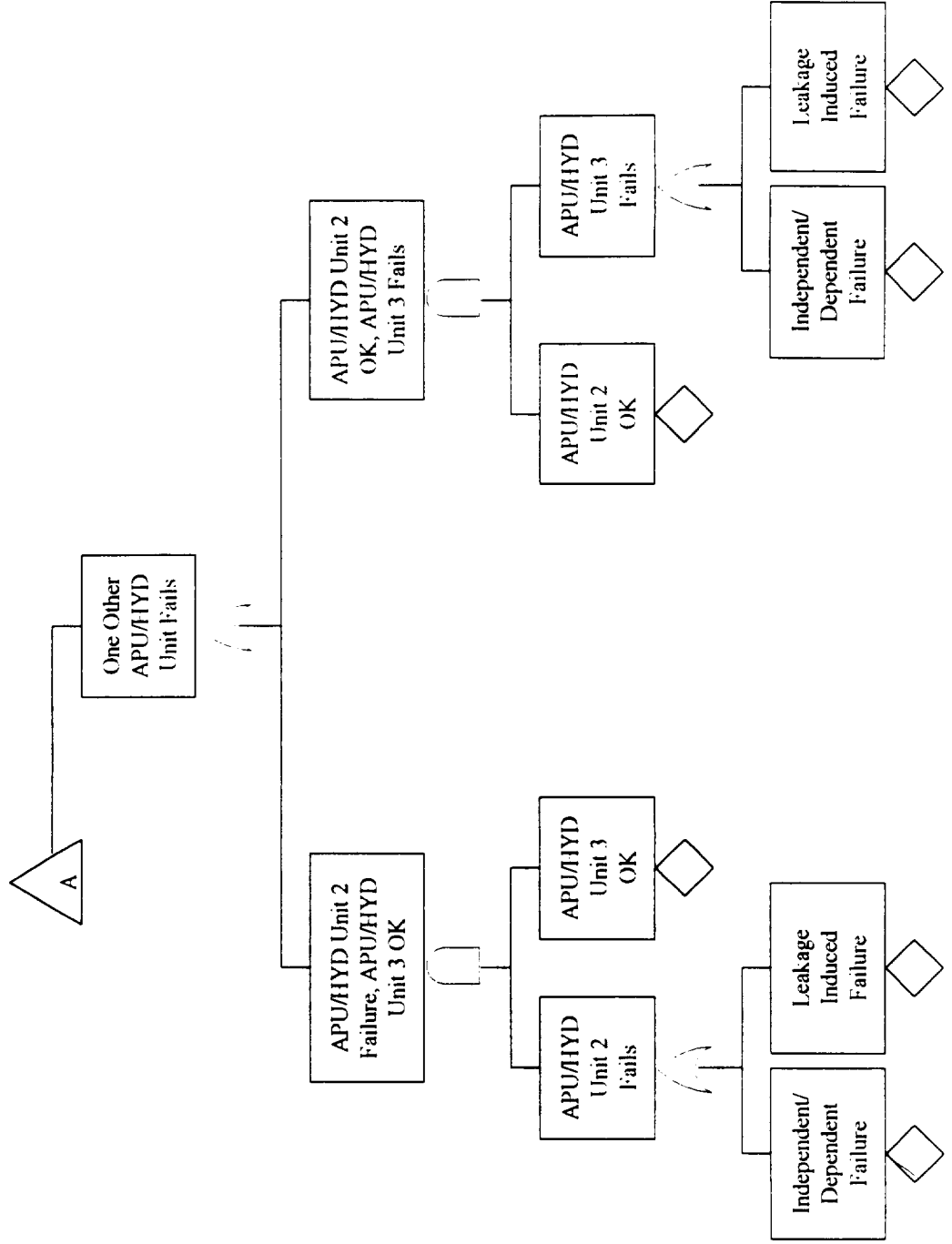
**Fault Tree for Sequence α : MDRU End State
 From a Hydrazine Leak During Ascent,
 one APU/HYD Unit has an Undetected Leak and is
 Recoverable, one Other APU/HYD Unit Fails**



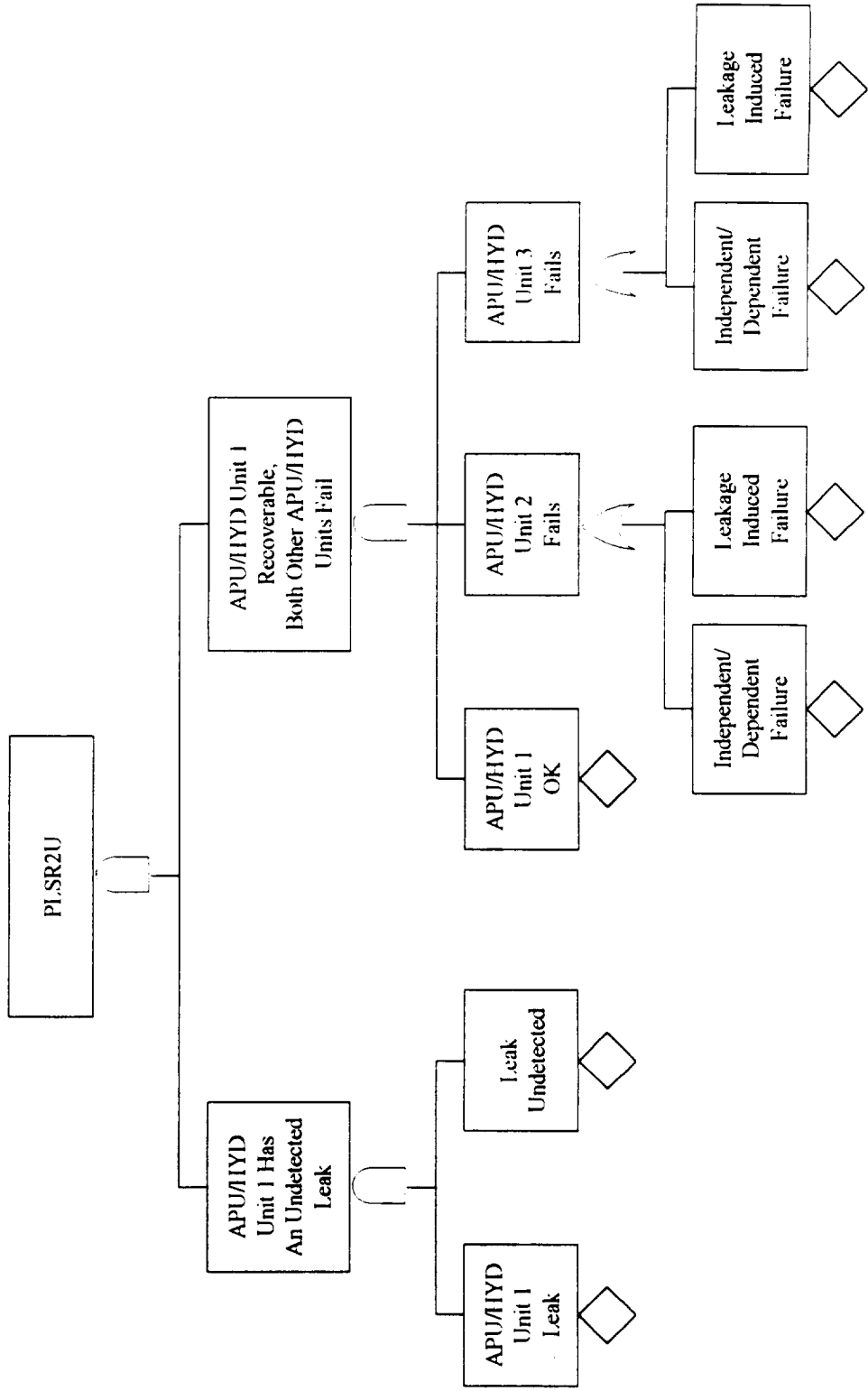
**Fault Tree for Sequence 6: MDRU End State
From a Hydrazine Leak During Ascent,
one APU/HYD Unit has an Undetected Leak and is
Recoverable, one Other APU/HYD Unit Fails**



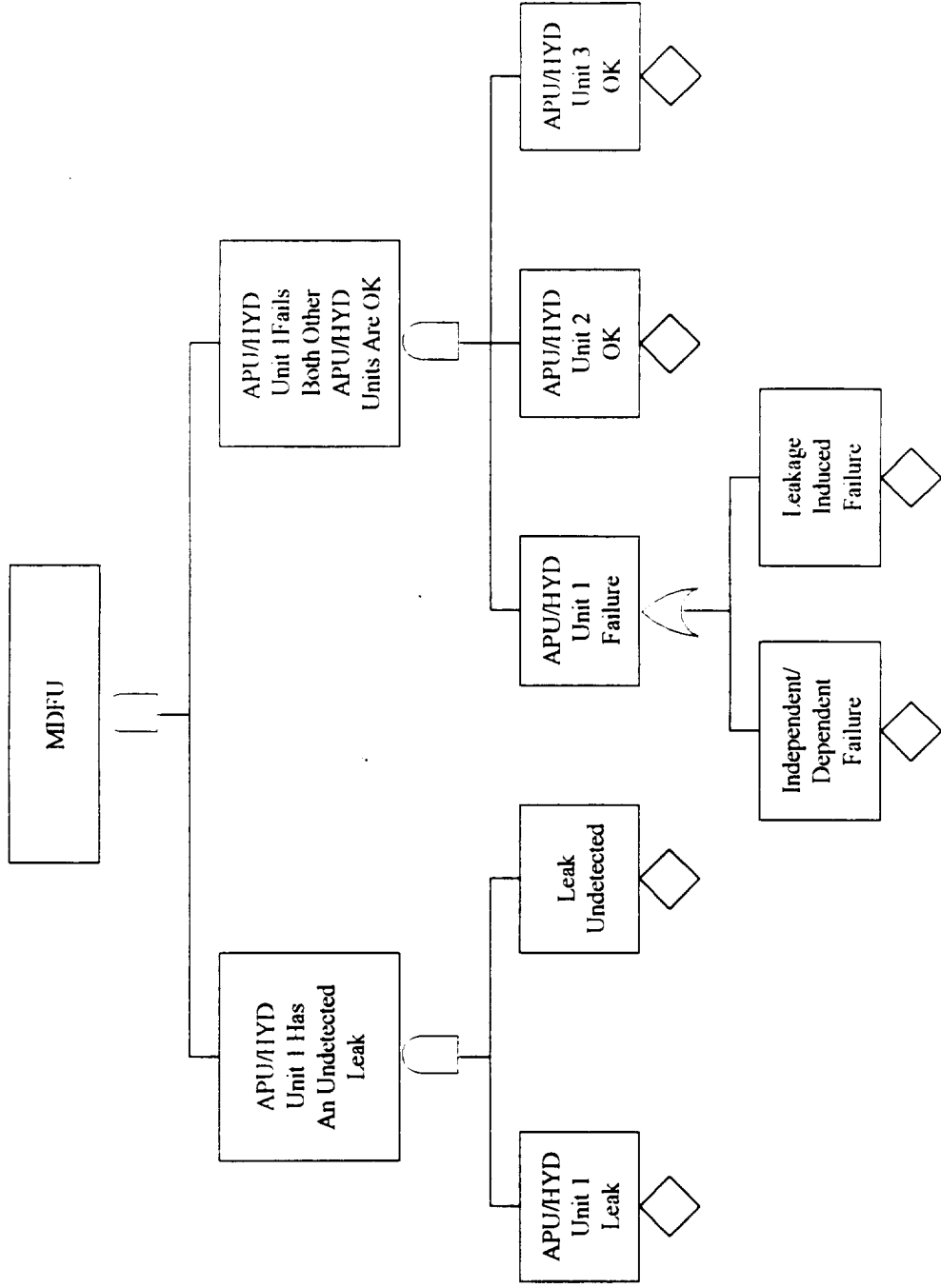
**Fault Tree for Sequence 8: MDFRU End State
From a Hydrazine Leak During Ascent,
one APU/HYD Unit has an Undetected Leak and is
Recoverable, one Other APU/HYD Unit Fails
(Continued)**



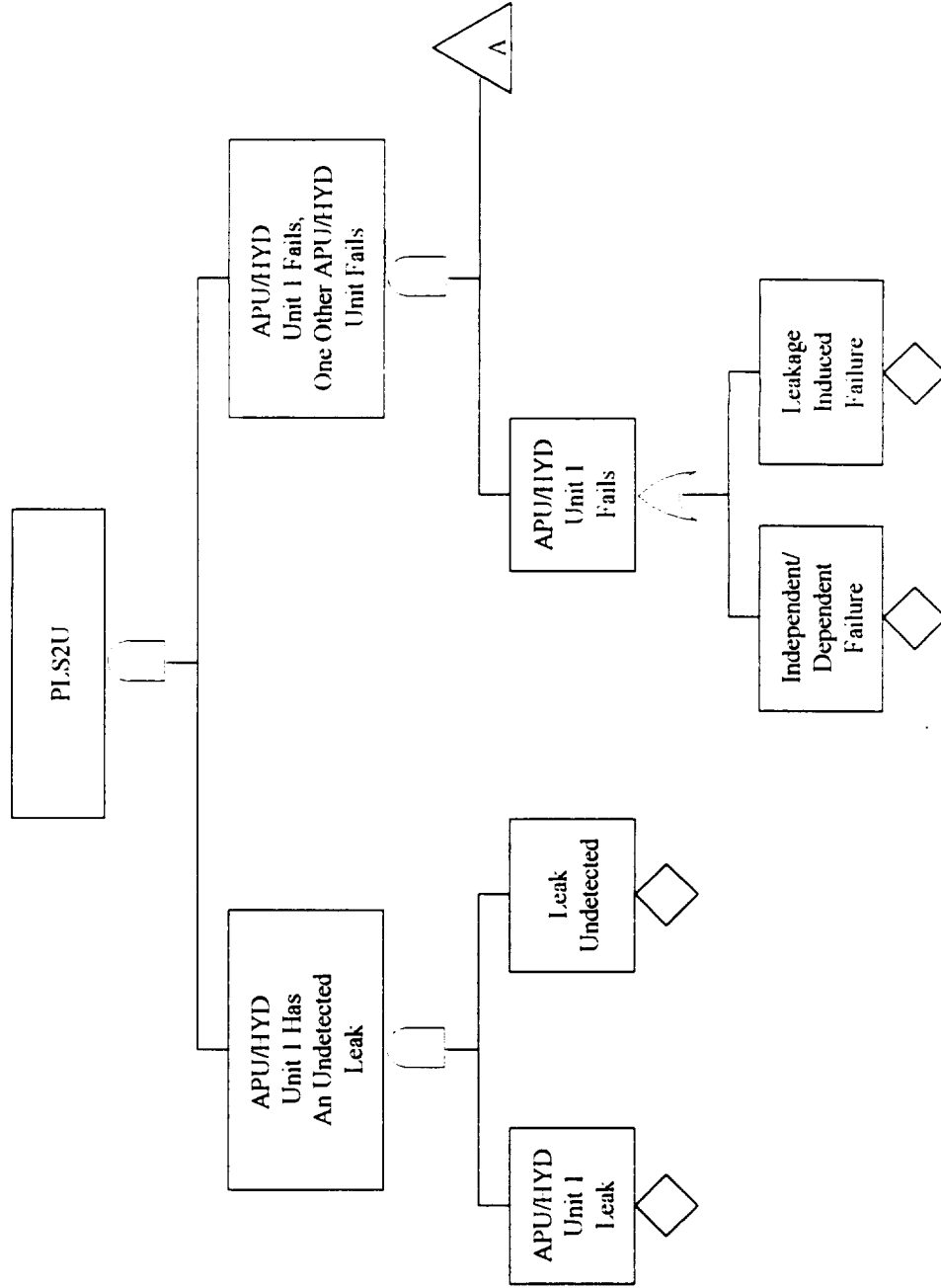
**Fault Tree for Sequence 9: PLSR2U End State
 From a Hydrazine Leak During Ascent, one APU/HYD
 Unit has an Undetected Leak and is Recoverable, Both Other
 APU/HYD Units Fail**



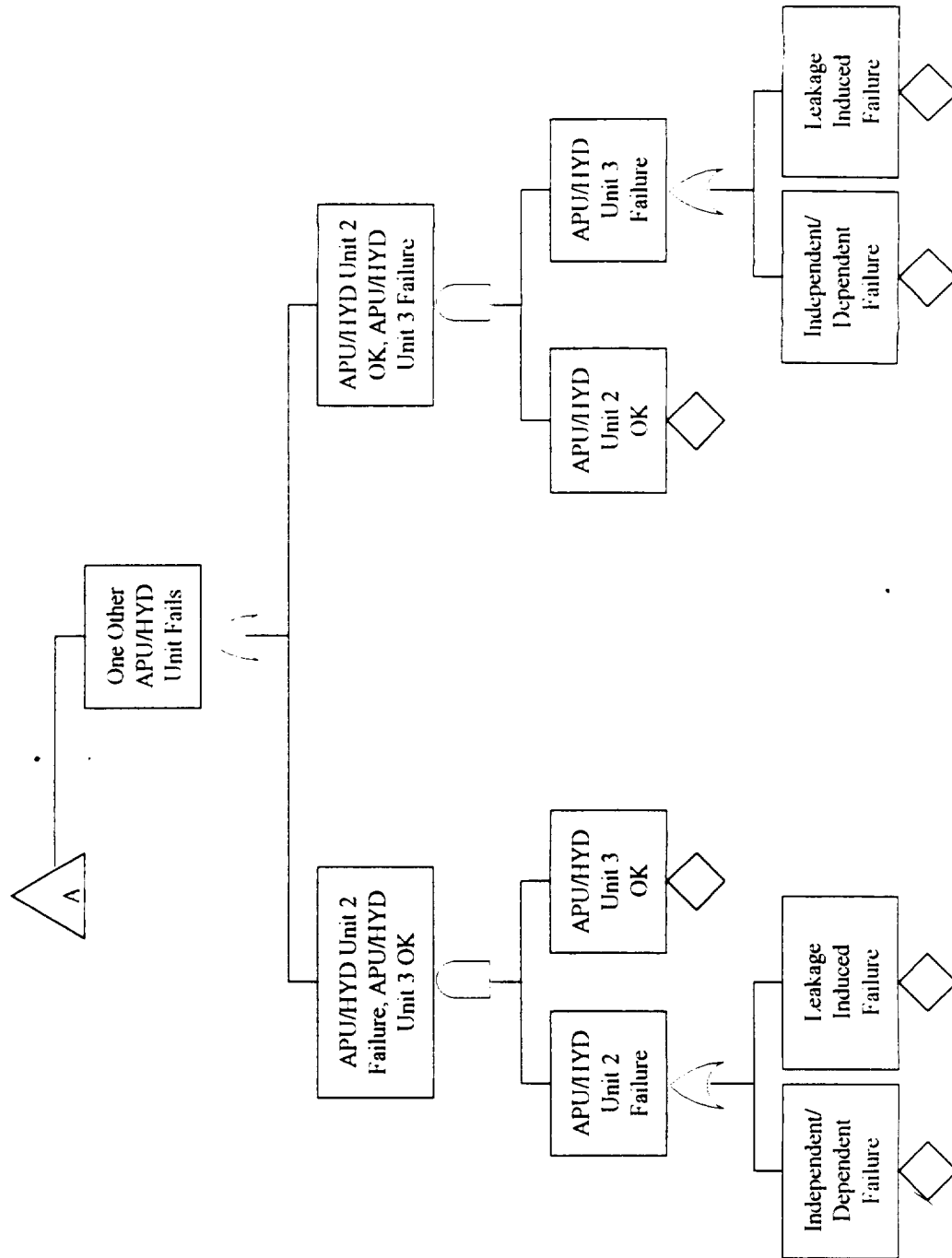
Fault Tree for Sequence 10: MDFU End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has an Undetected Leak and Subsequent Failure, no Other APU/HYD Units Fail



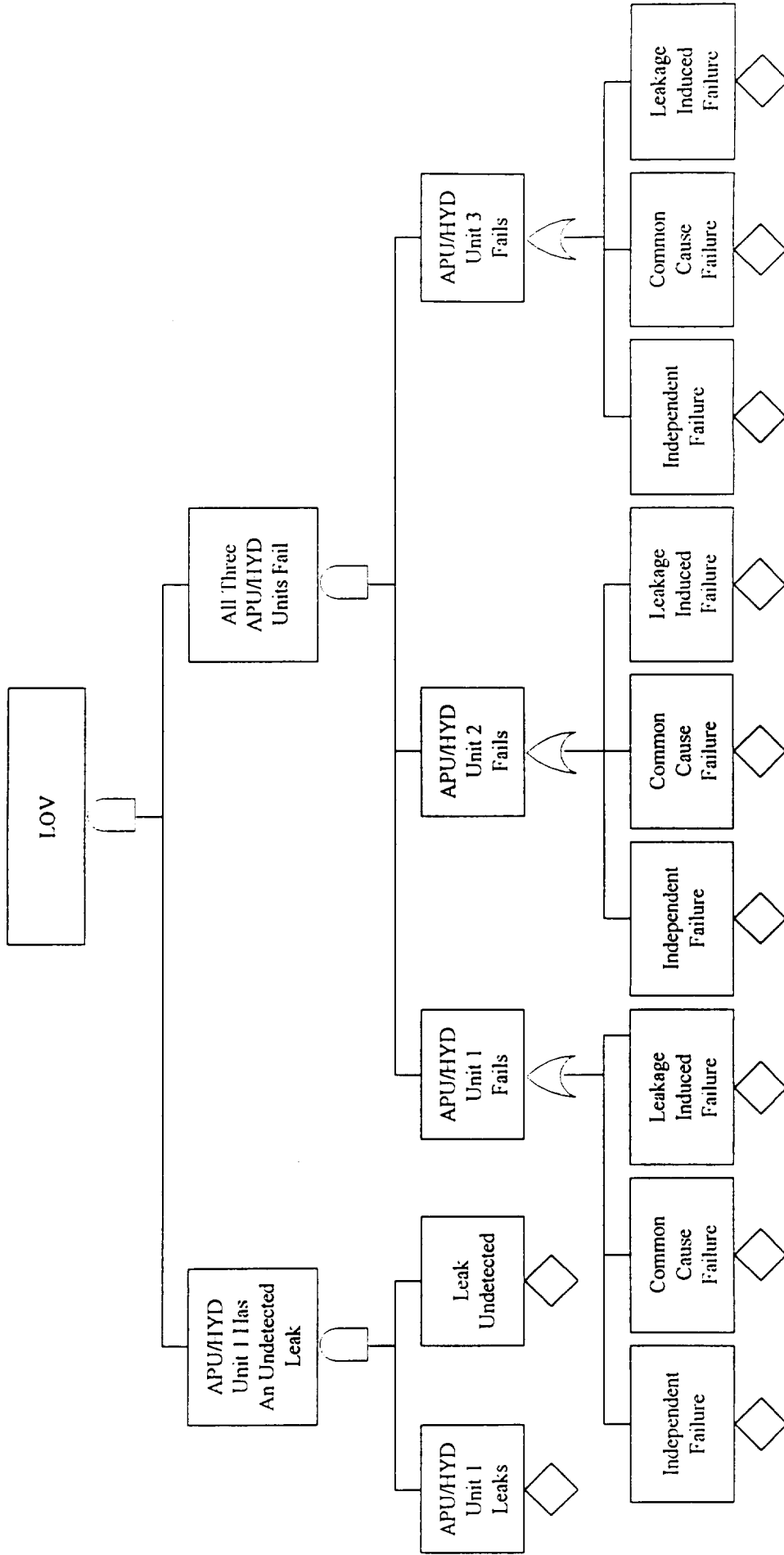
**Fault Tree for Sequence 11: PLS2U End State From
a Hydrazine Leak During Ascent, one APU/HYD Unit has an
Undetected Leak and Subsequent Failure, one Other APU/HYD
Unit Also Fails**



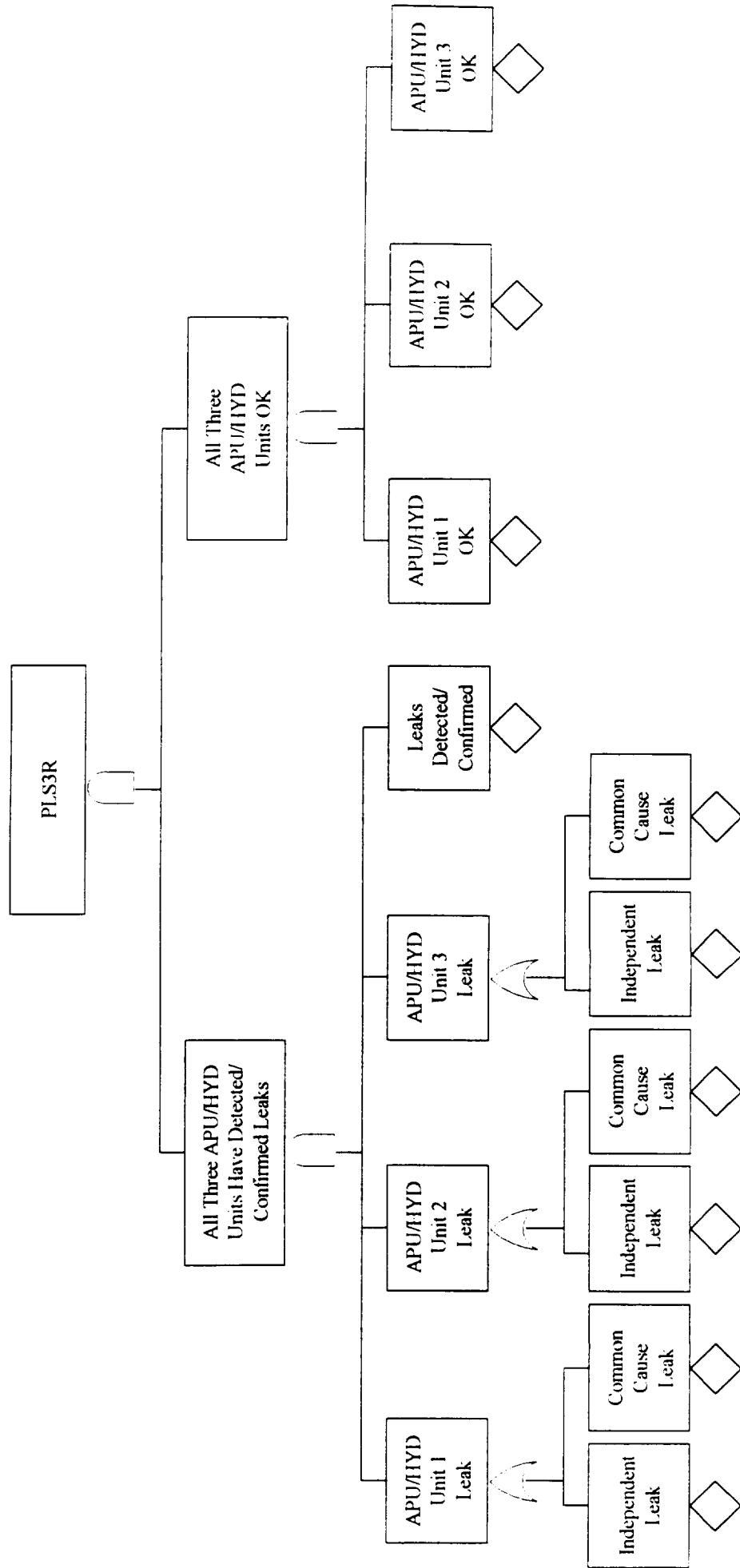
Fault Tree for Sequence 11: PLS2U End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has an Undetected Leak and Subsequent Failure, one Other APU/HYD Unit Also Fails (Continued)



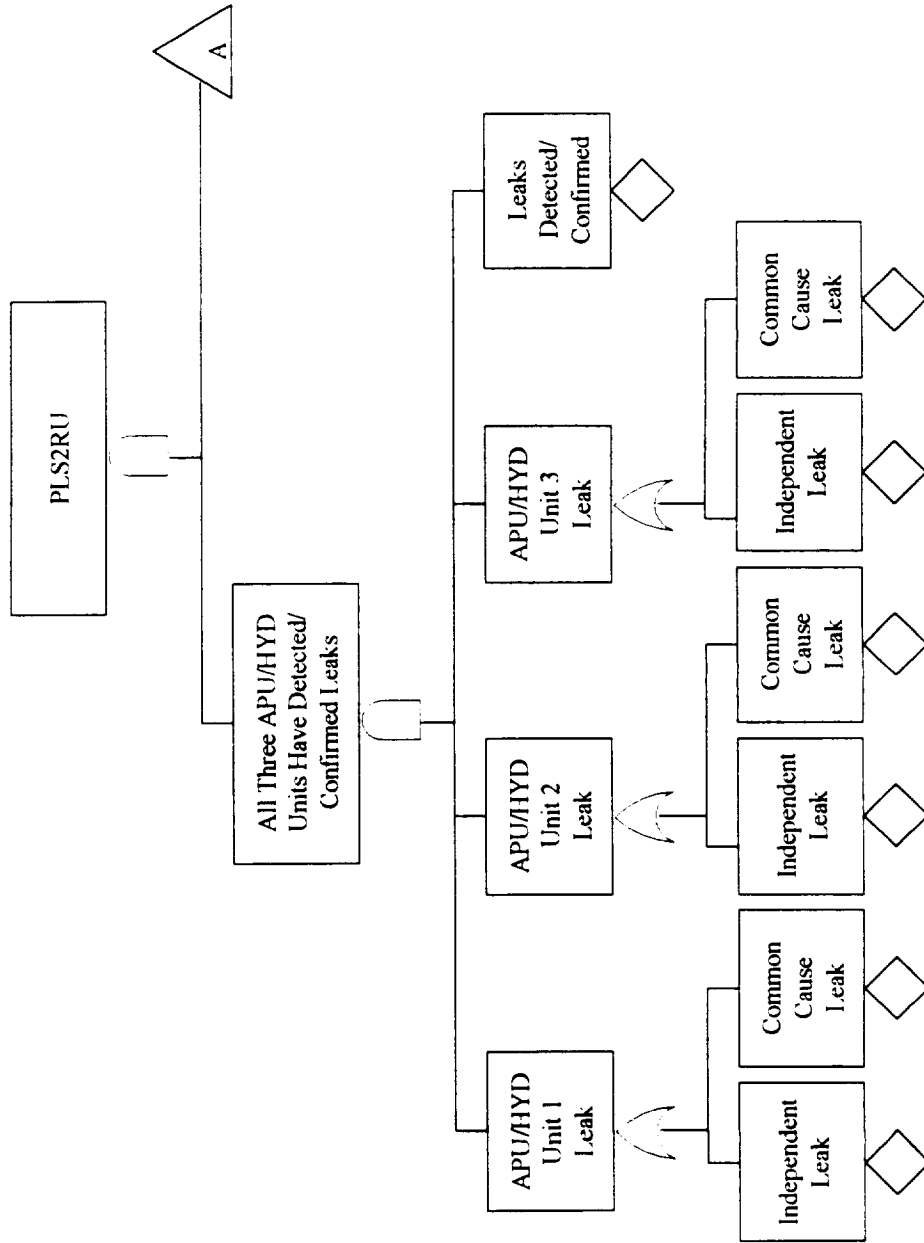
Fault Tree for Sequence 14. LOV End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has an Undetected Leak and all Three APU/HYD Units Fail



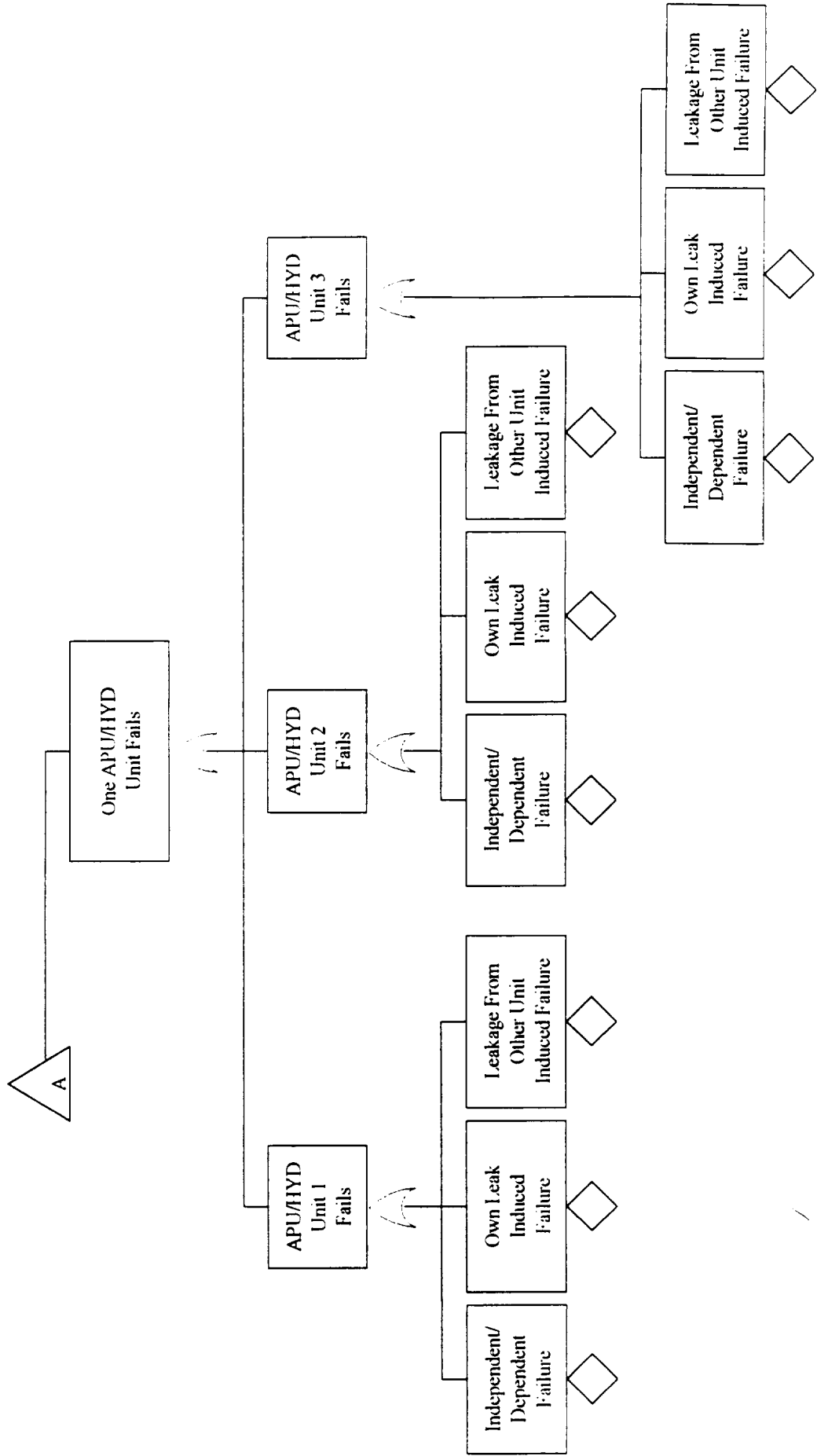
Fault Tree for Sequence 13: PLS3R End State From a Hydrazine Leak Detected During Ascent, all Three APU/HYD Units Have Detected/Confirmed Leaks and no Failures



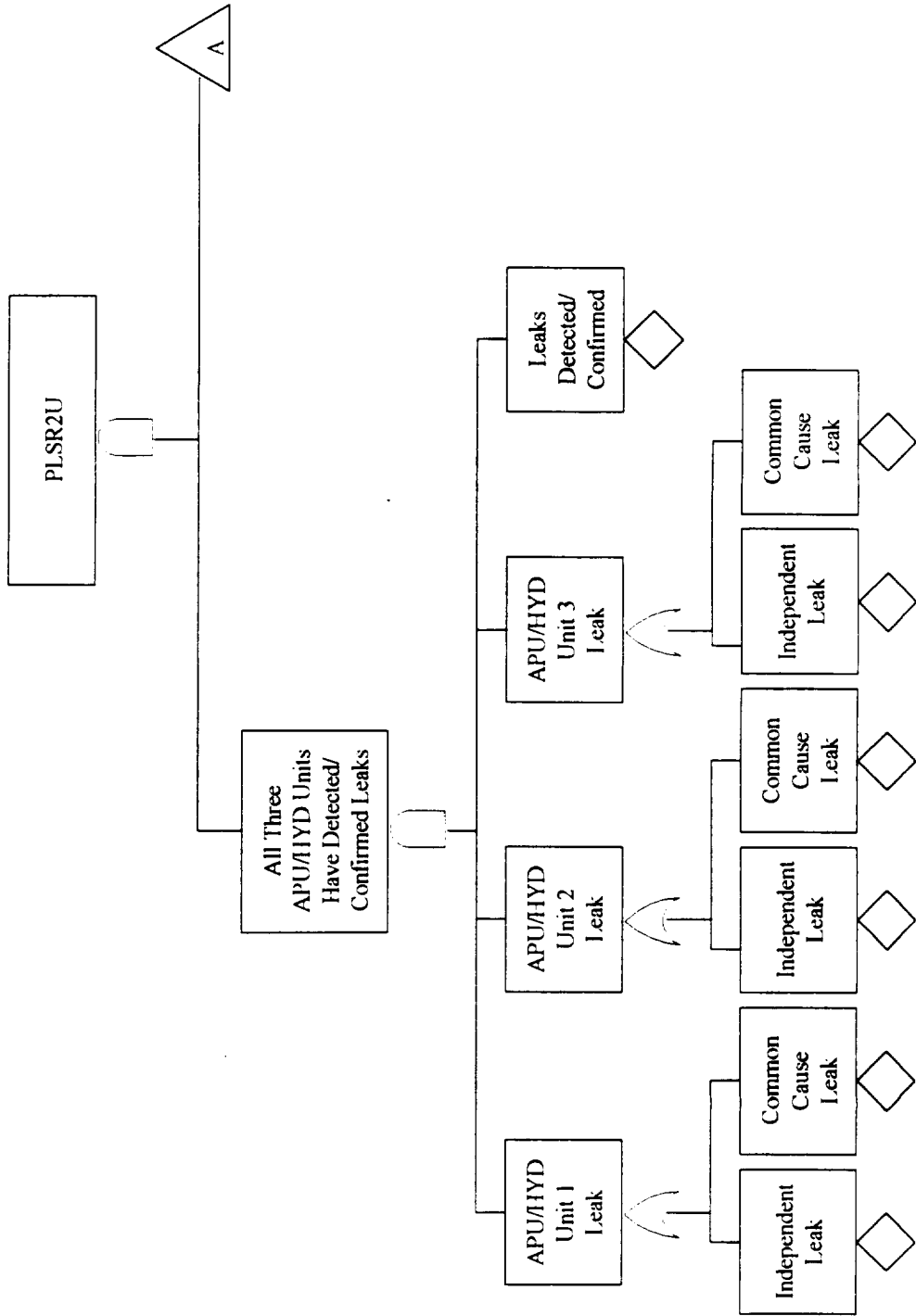
Fault Tree for Sequence 14: PLS2RU End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Detected/Confirmed Leaks and one APU/HYD Unit Fails



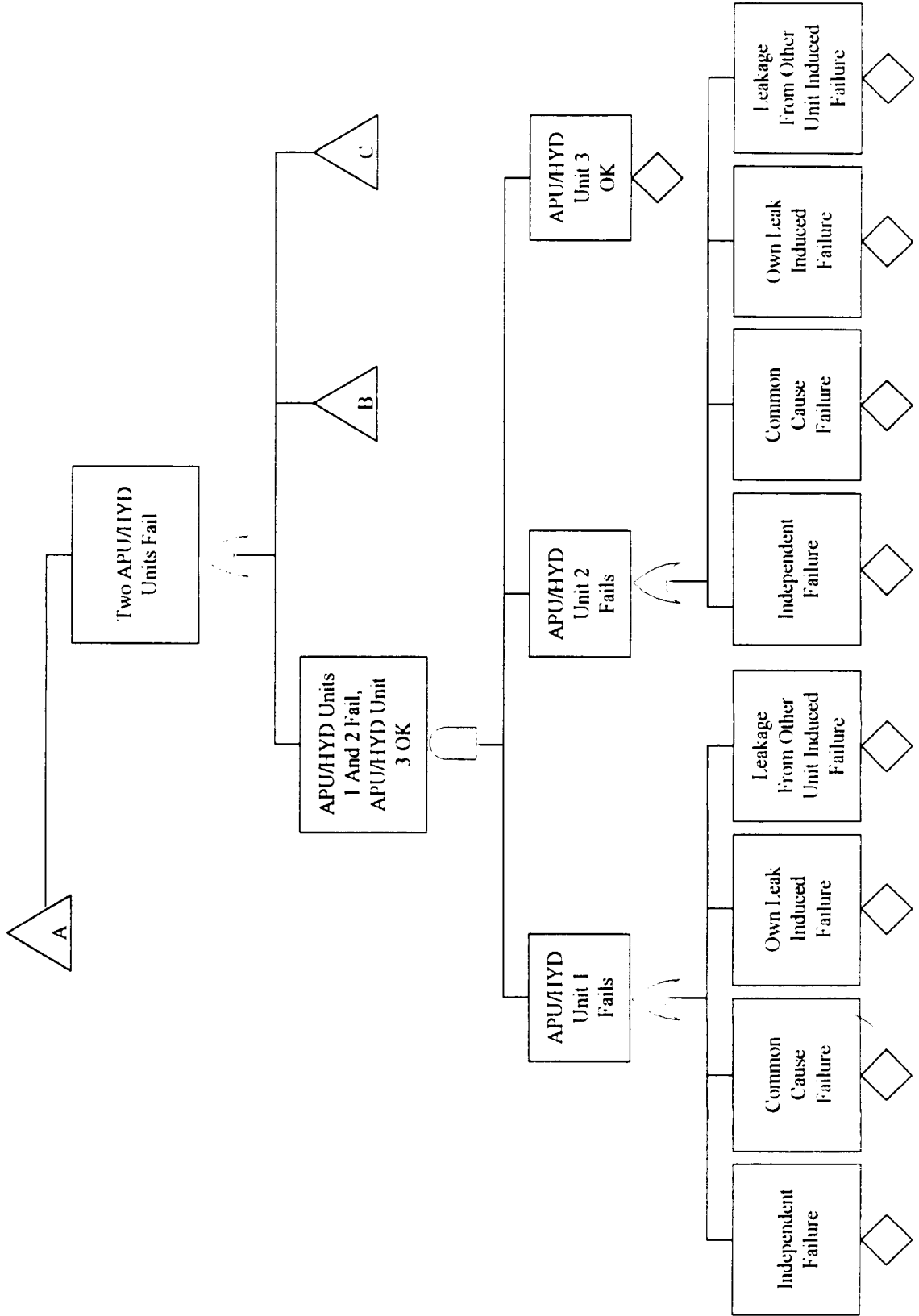
**Fault Tree for Sequence 14: PLS2RU End State From a
Hydrazine Leak During Ascent, all Three APU/HYD Units
Have Detected/Confirmed Leaks and one APU/HYD Unit Fails
(Continued)**



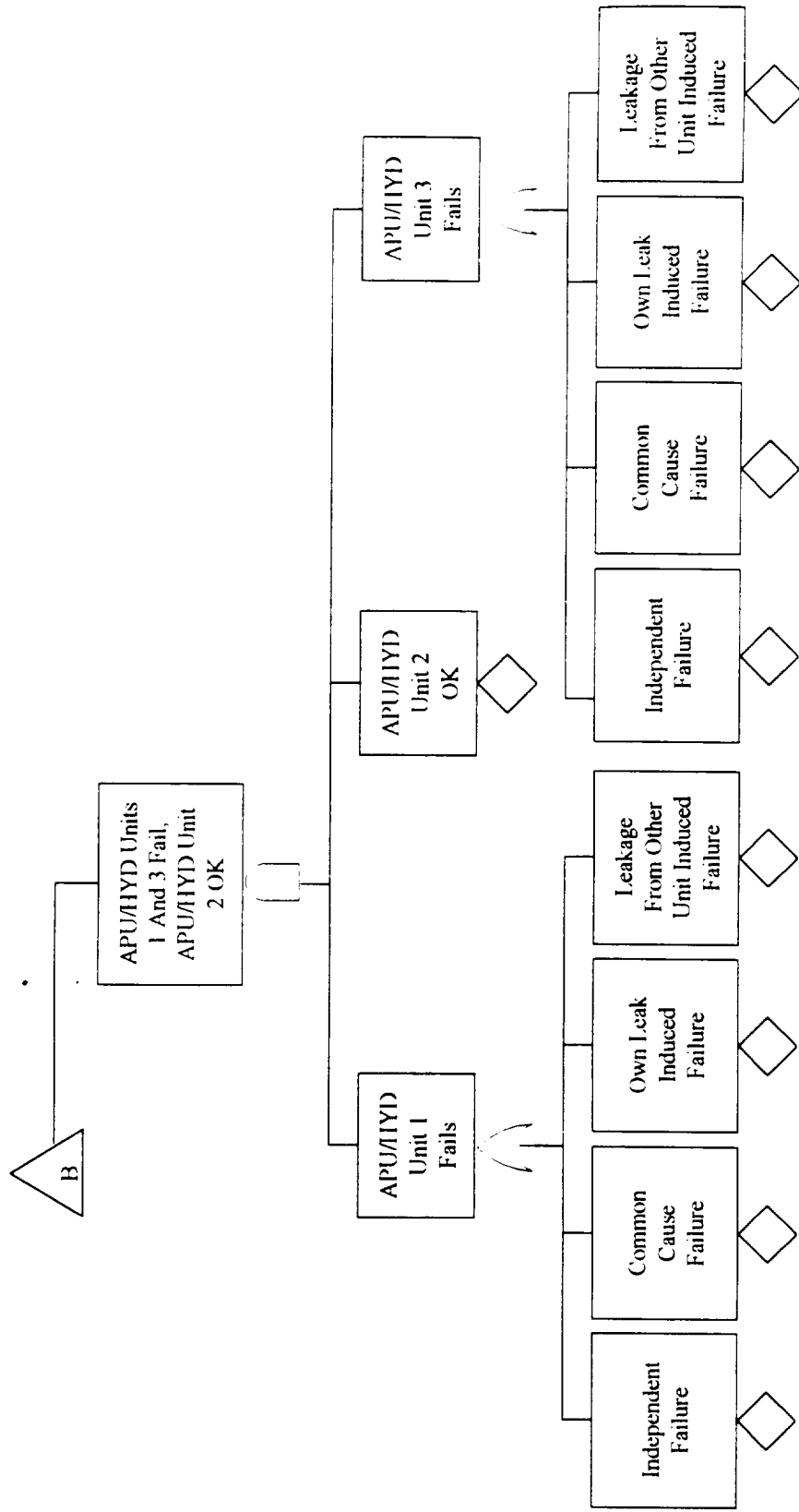
**Fault Tree for Sequence 15: PLSR2U End State From
Hydrazined Leak During Ascent, all Three APU/HYD Units
Have Detected/Confirmed Leaks, two APU/HYD Units Fail**



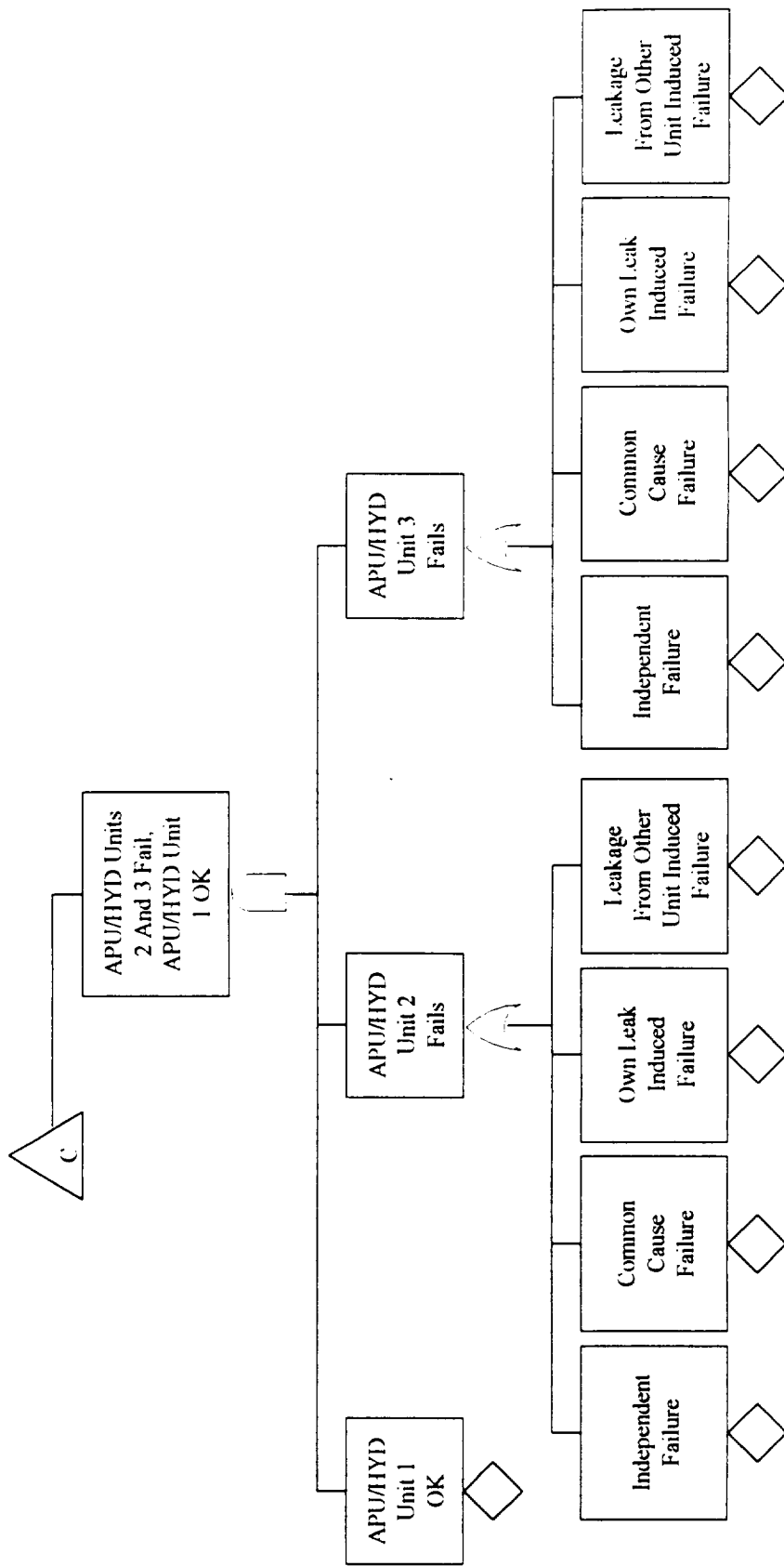
**Fault Tree for Sequence 1s: PLSR2U End State From
Hydrazined Leak During Ascent, all Three APU/HYD Units
Have Detected/Confirmed Leaks, two APU/HYD Units Fail
(Continued)**



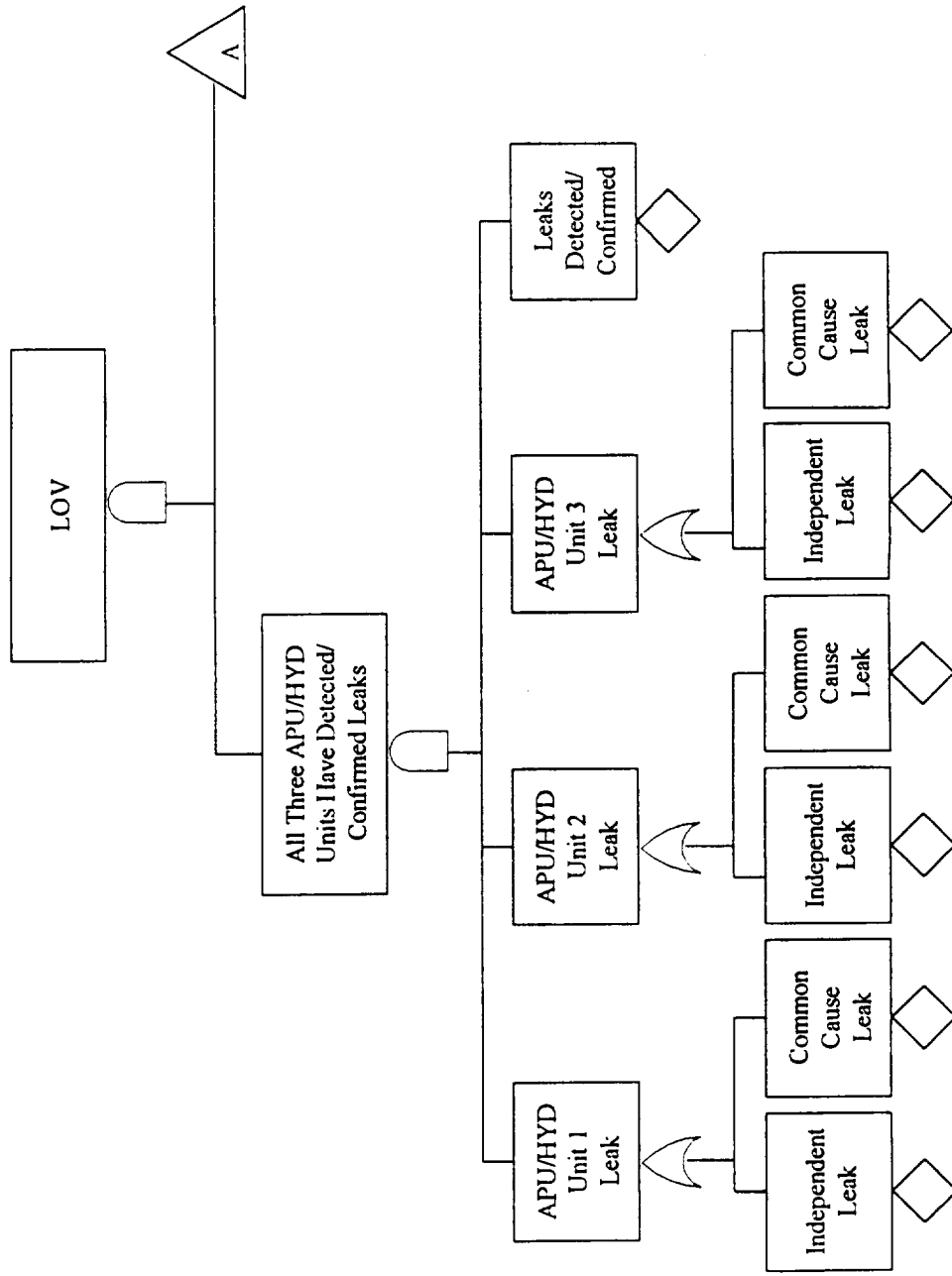
**Fault Tree for Sequence 15: PLSR2U End State From
Hydrazined Leak During Ascent, all Three APU/HYD Units
Have Detected/Confirmed Leaks, two APU/HYD Units Fail
(Continued)**



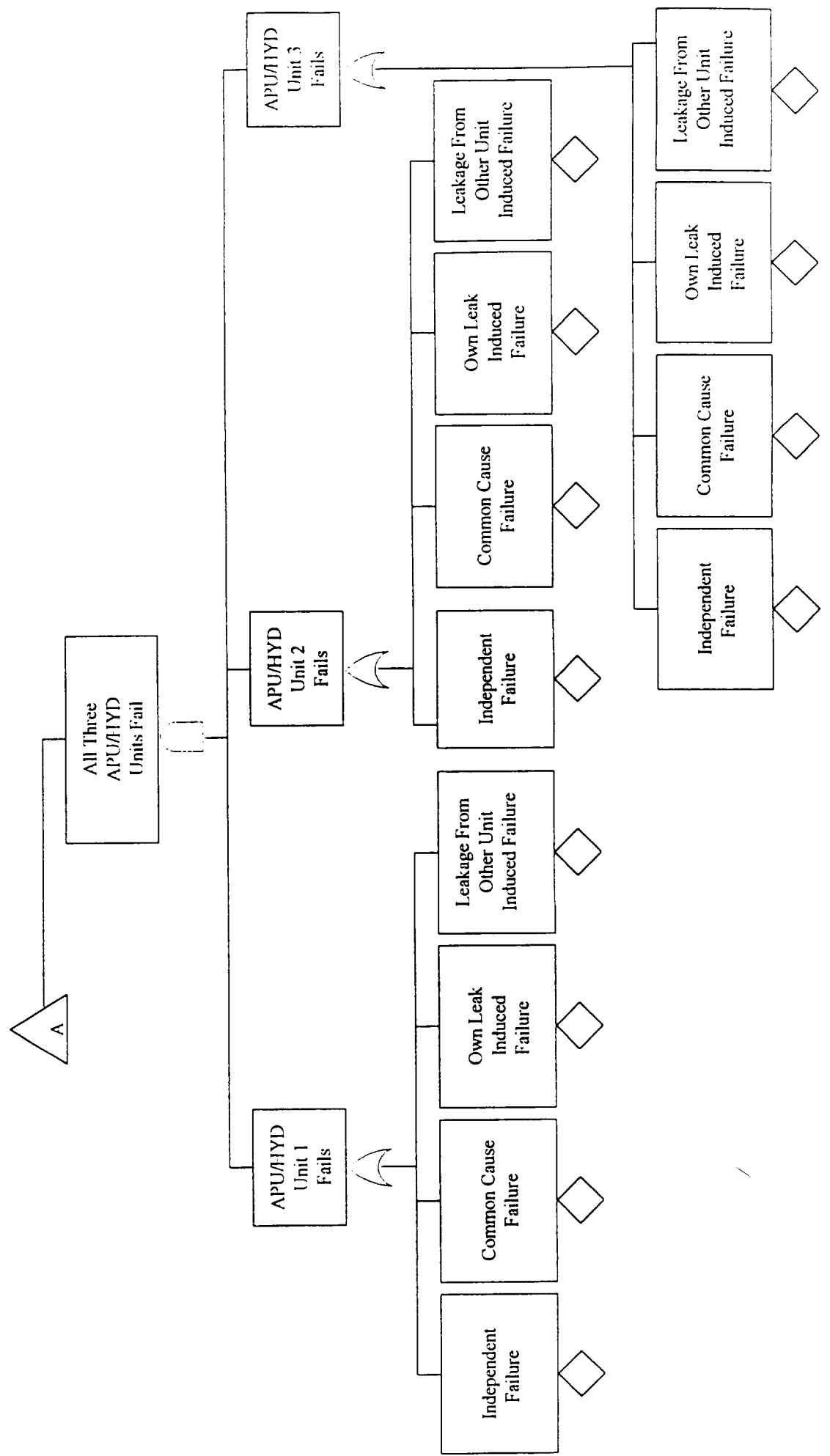
**Fault Tree for Sequence 15: PLSR2U End State From
Hydrazined Leak During Ascent, all Three APU/HYD Units
Have Detected/Confirmed Leaks, two APU/HYD Units Fail
(Continued)**



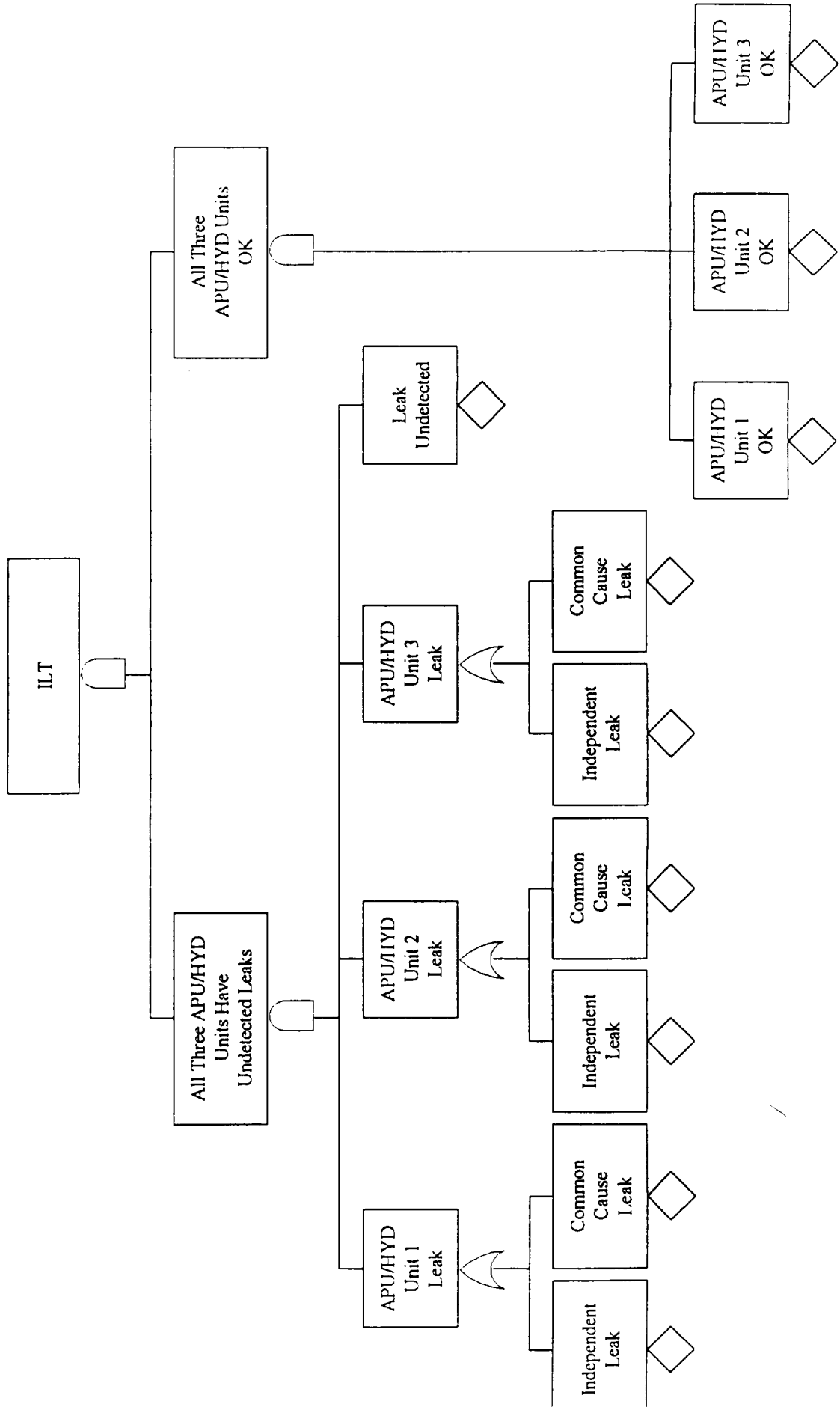
Fault Tree for Sequence 16: LOV End State From Hydrazine Leak During Ascent, all Three APU/HYD Units Have Detected/Confirmed Leaks and all Three APU/HYD Units Fail



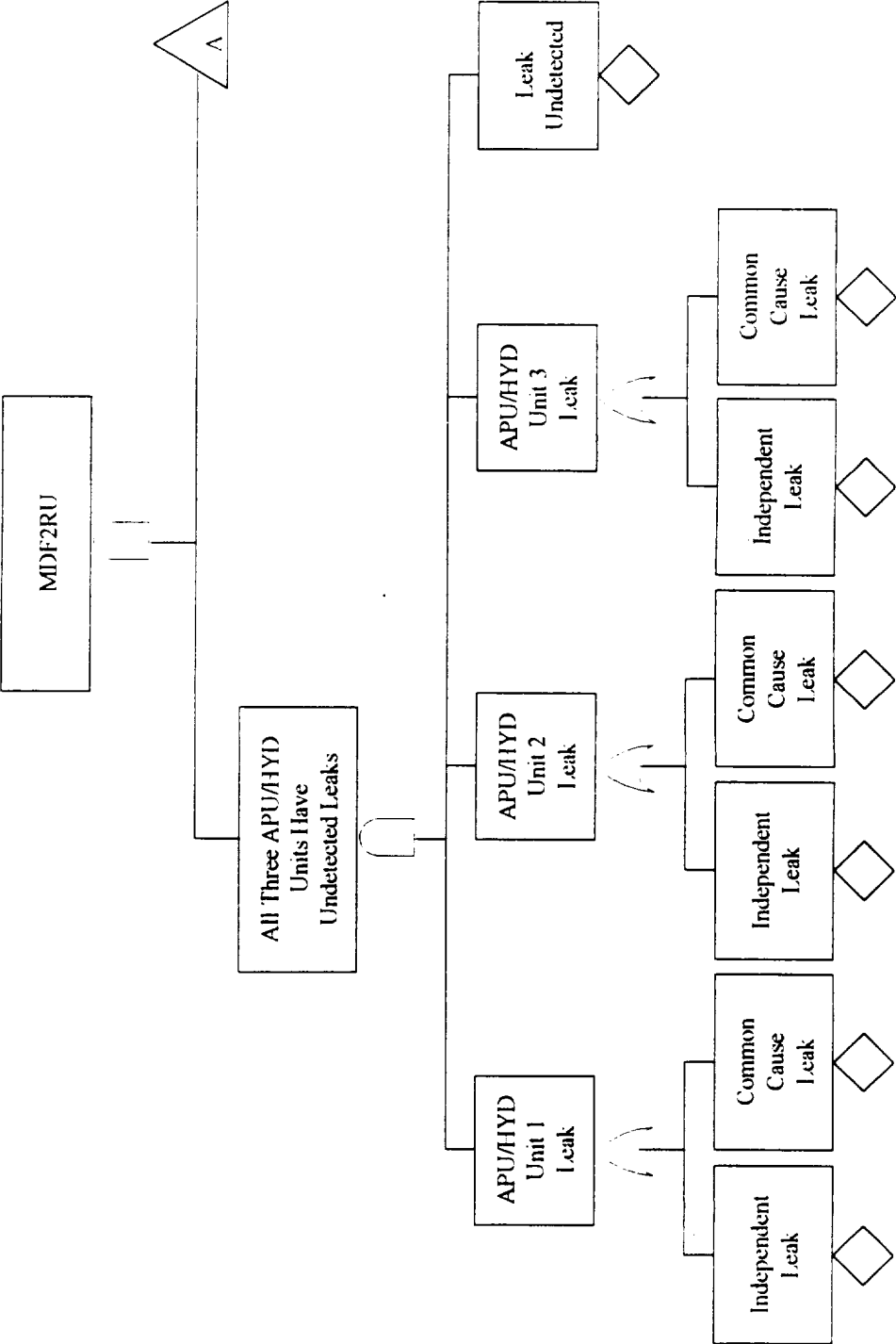
Fault Tree for Sequence 16: LOV End State From Hydrazine Leak During Ascent, all Three APU/HYD Units Have Detected/Confirmed Leaks and all Three APU/HYD Units Fail (Continued)



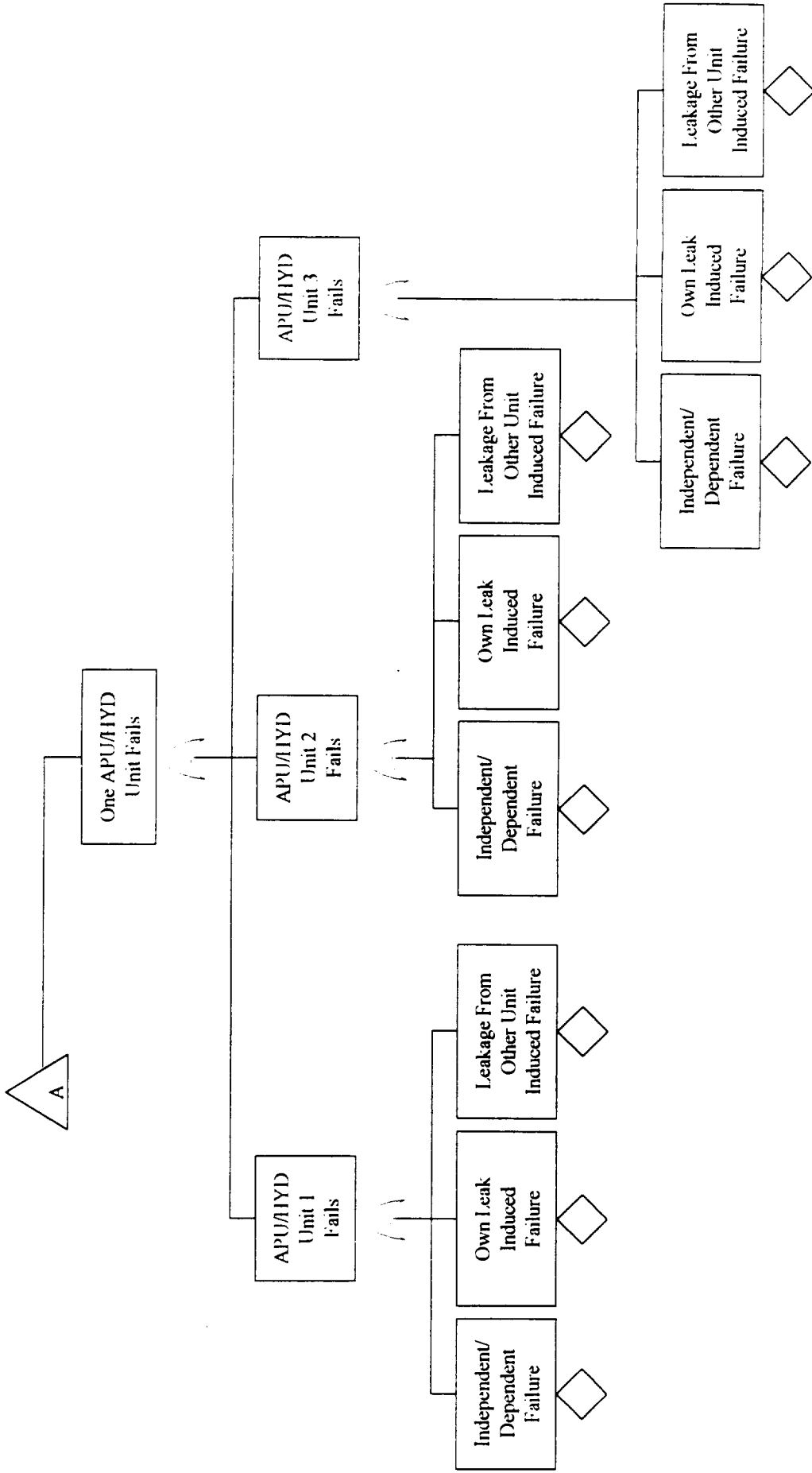
Fault Tree for Sequence 17: ILT End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks and no Failures



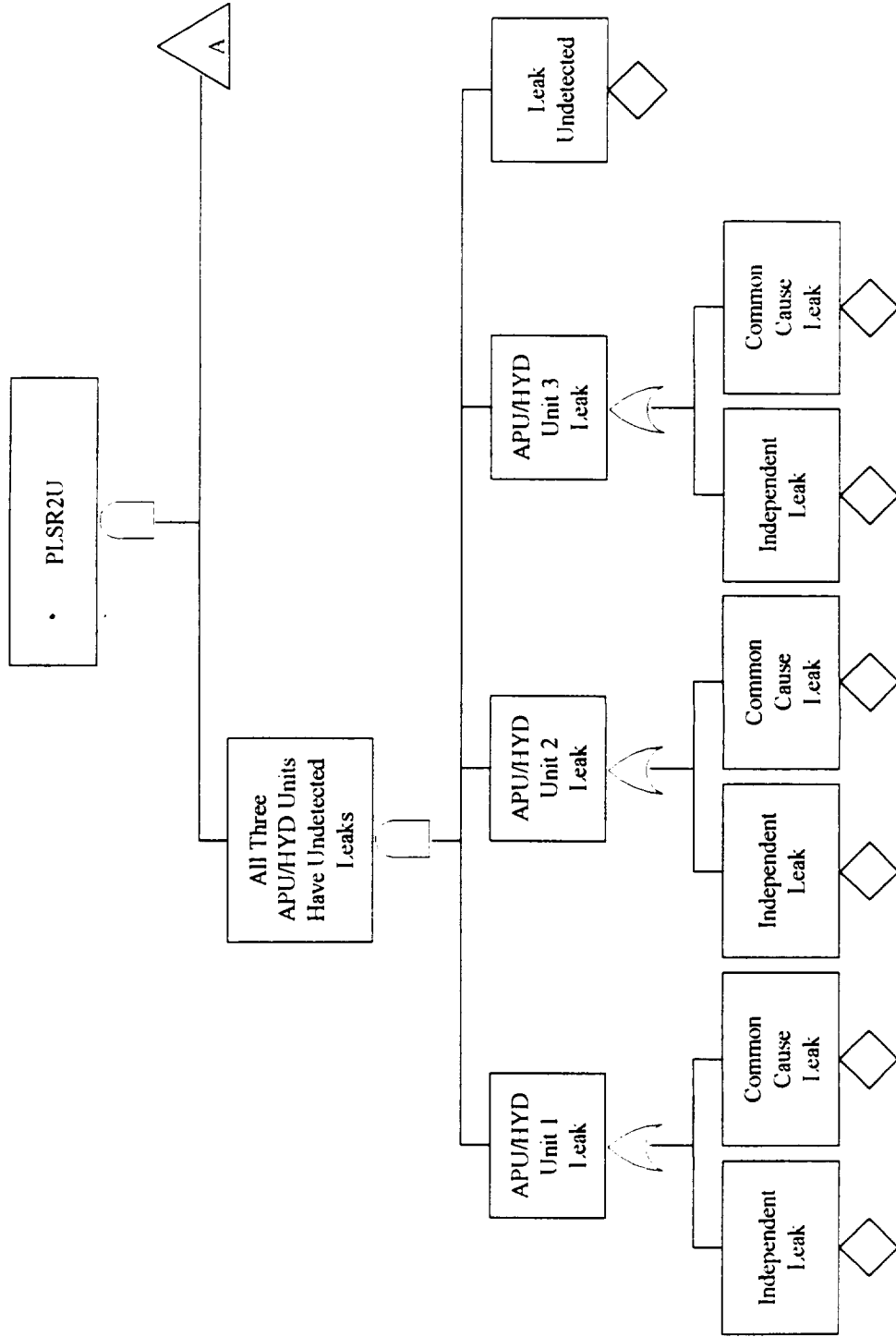
Fault Tree for Sequence 18: MDF2RU End State From a Hydrazine Leak During Ascent, one APU/HYD Unit Fails



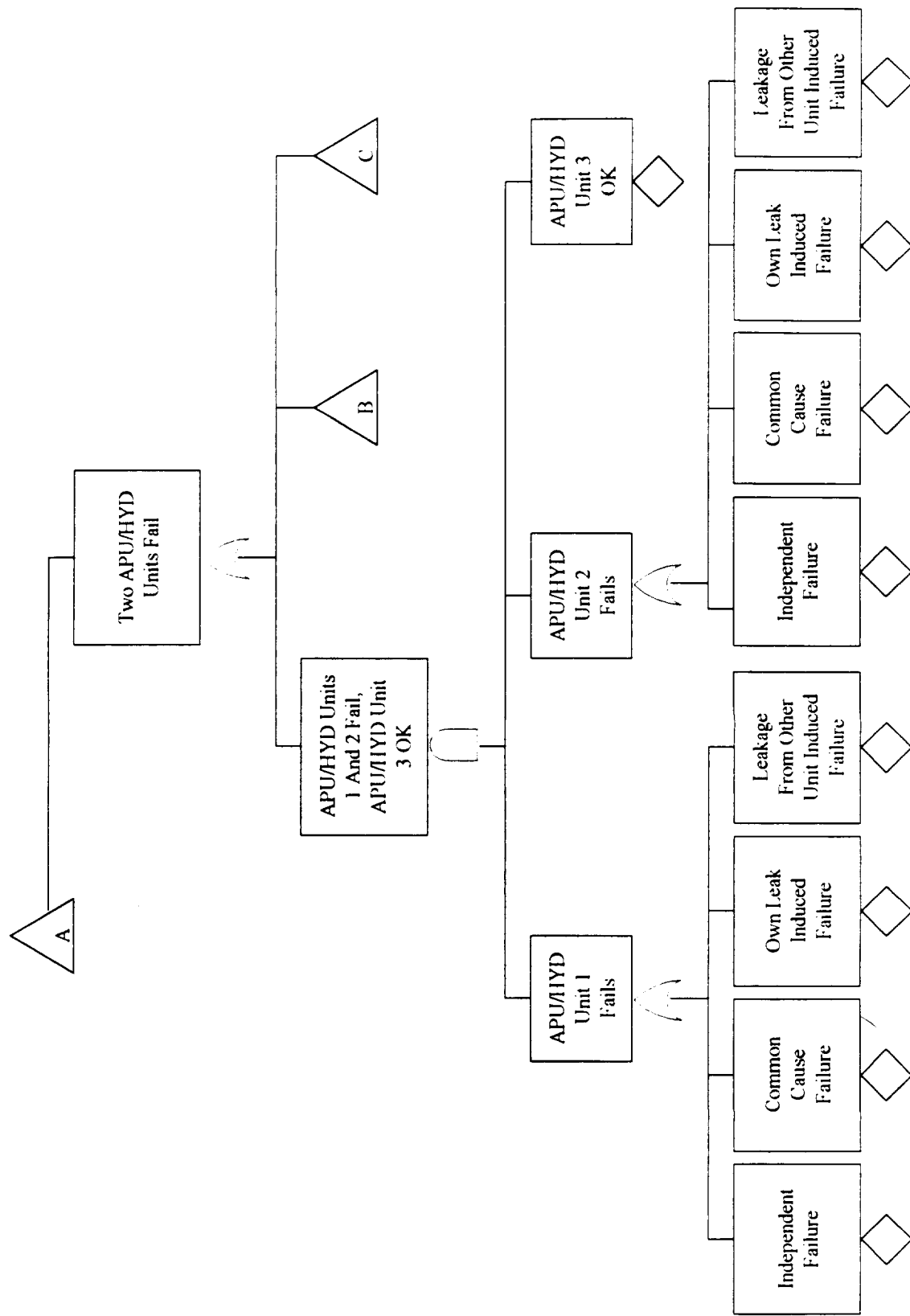
**Fault Tree for Sequence 18: MDF2RU End State
From a Hydrazine Leak During Ascent, one
APU/HYD Unit Fails (Continued)**



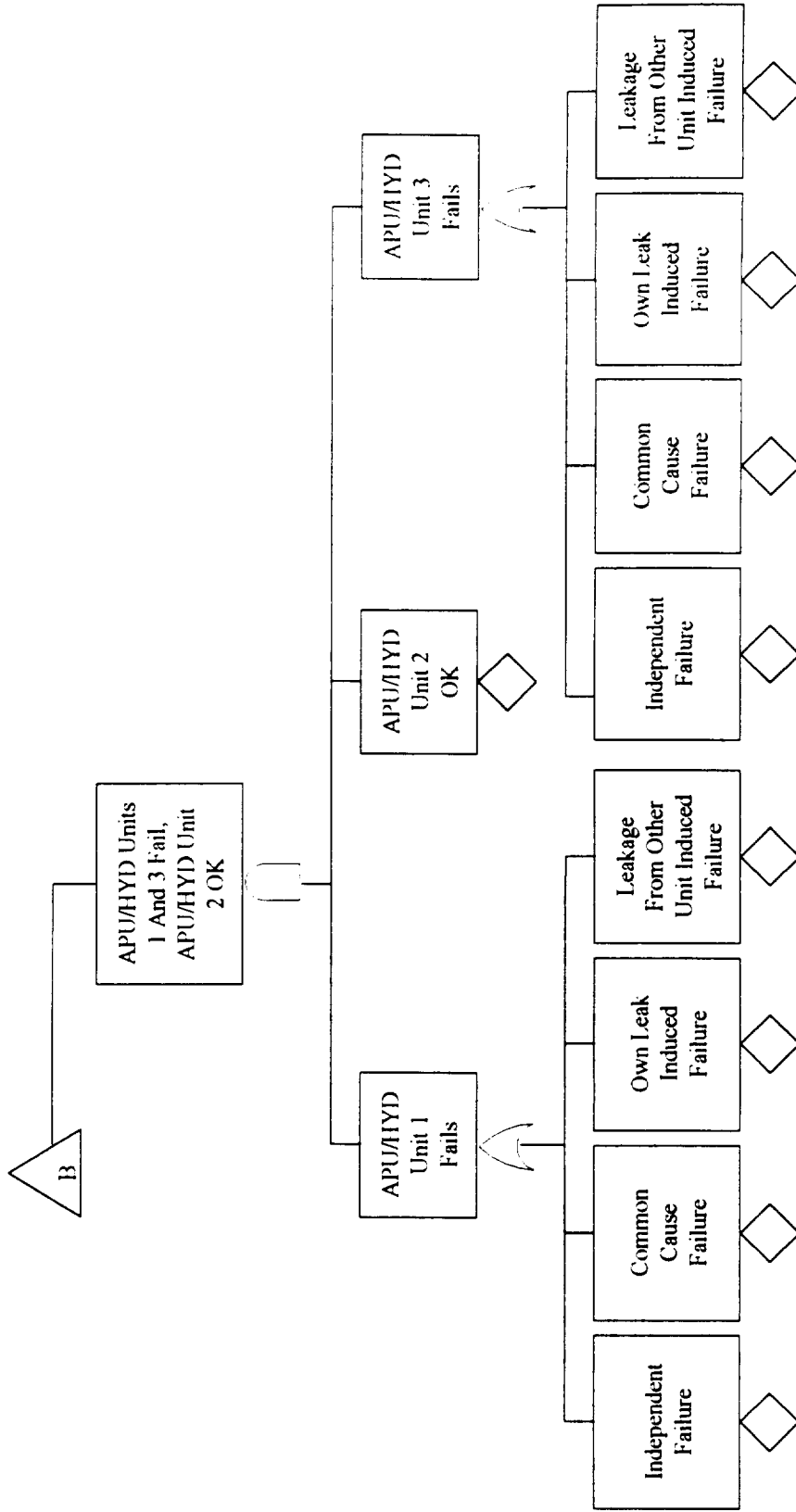
Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail



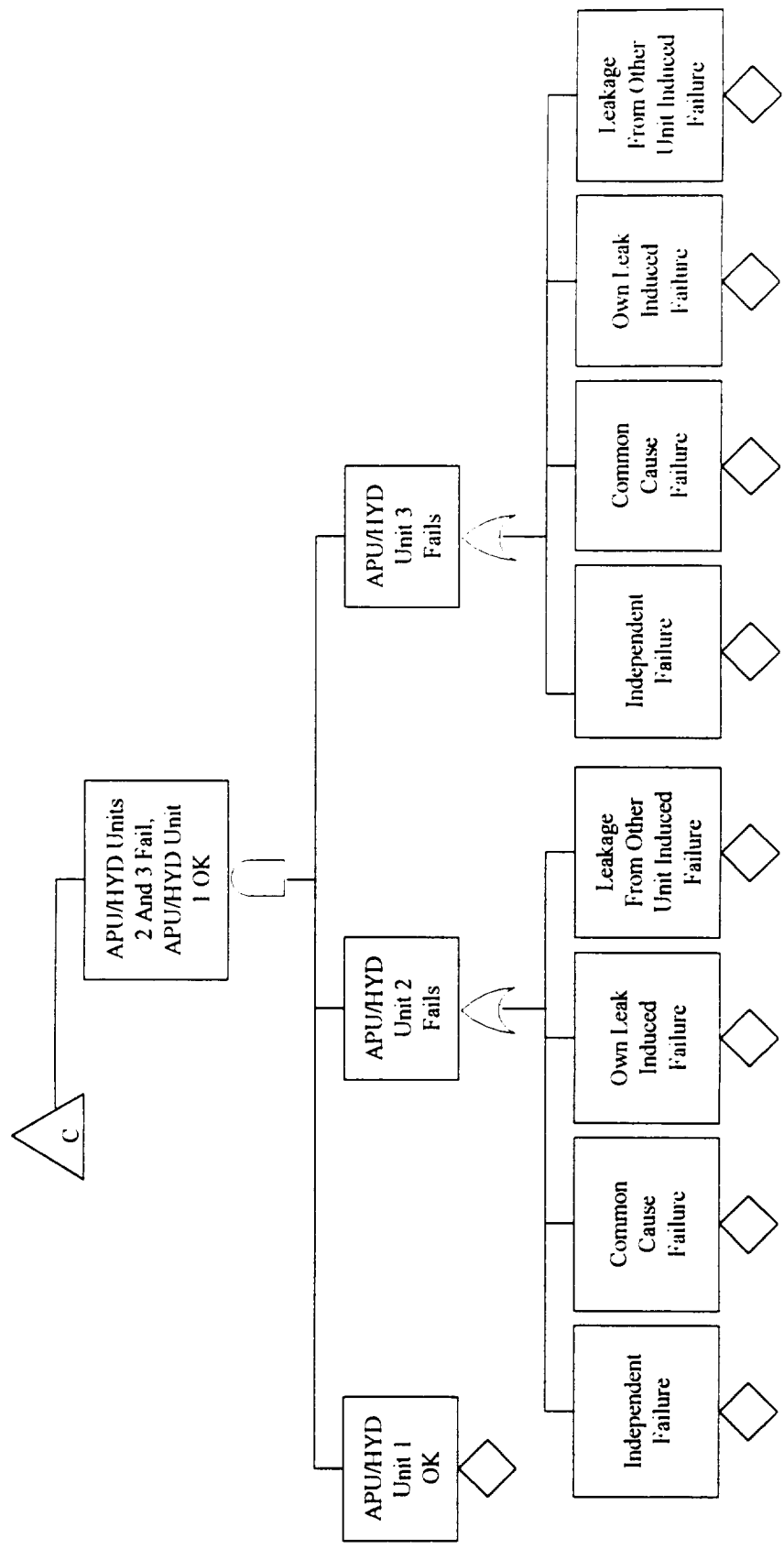
Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail (Continued)



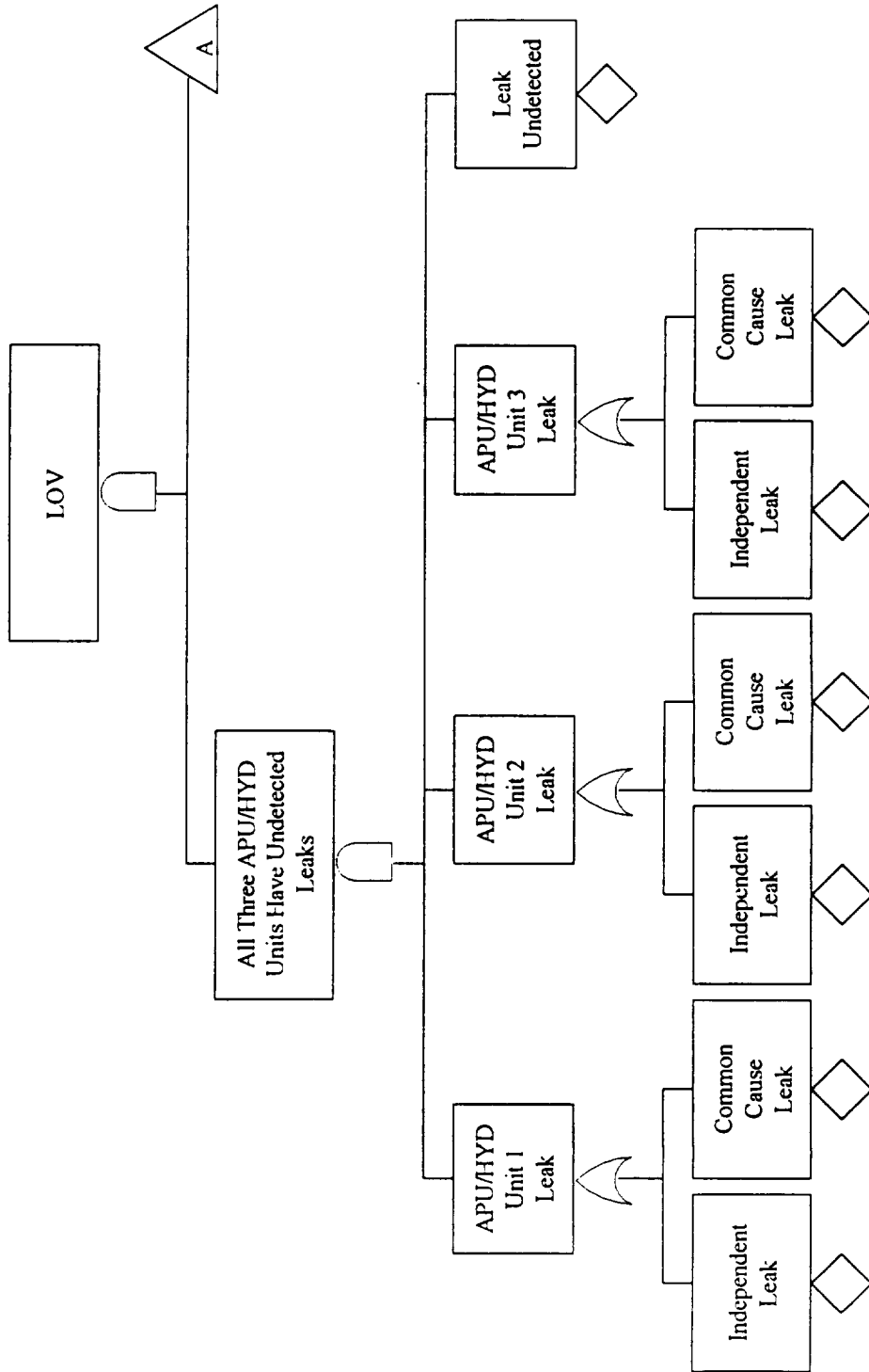
Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail (Continued)



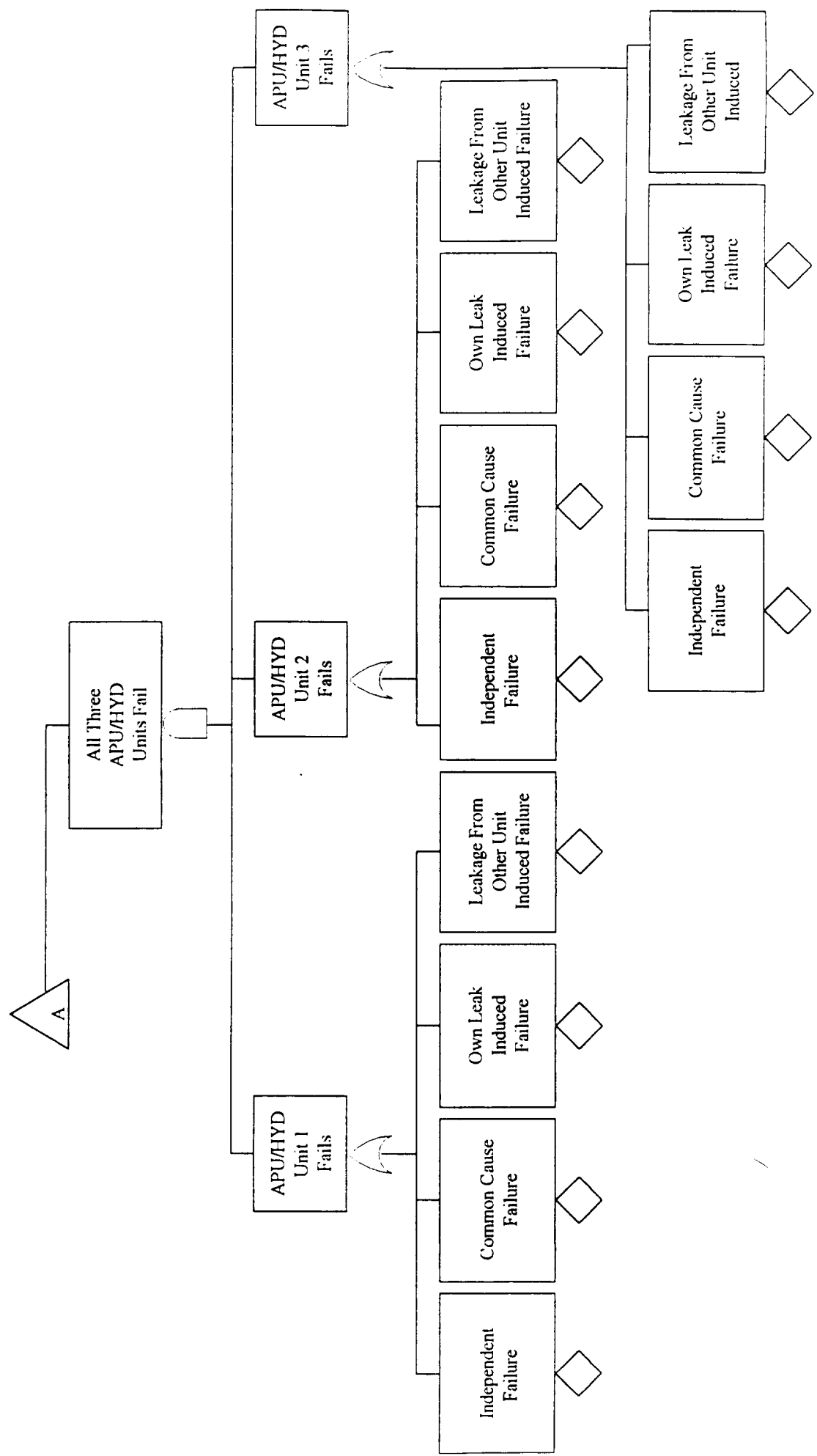
Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail (Continued)



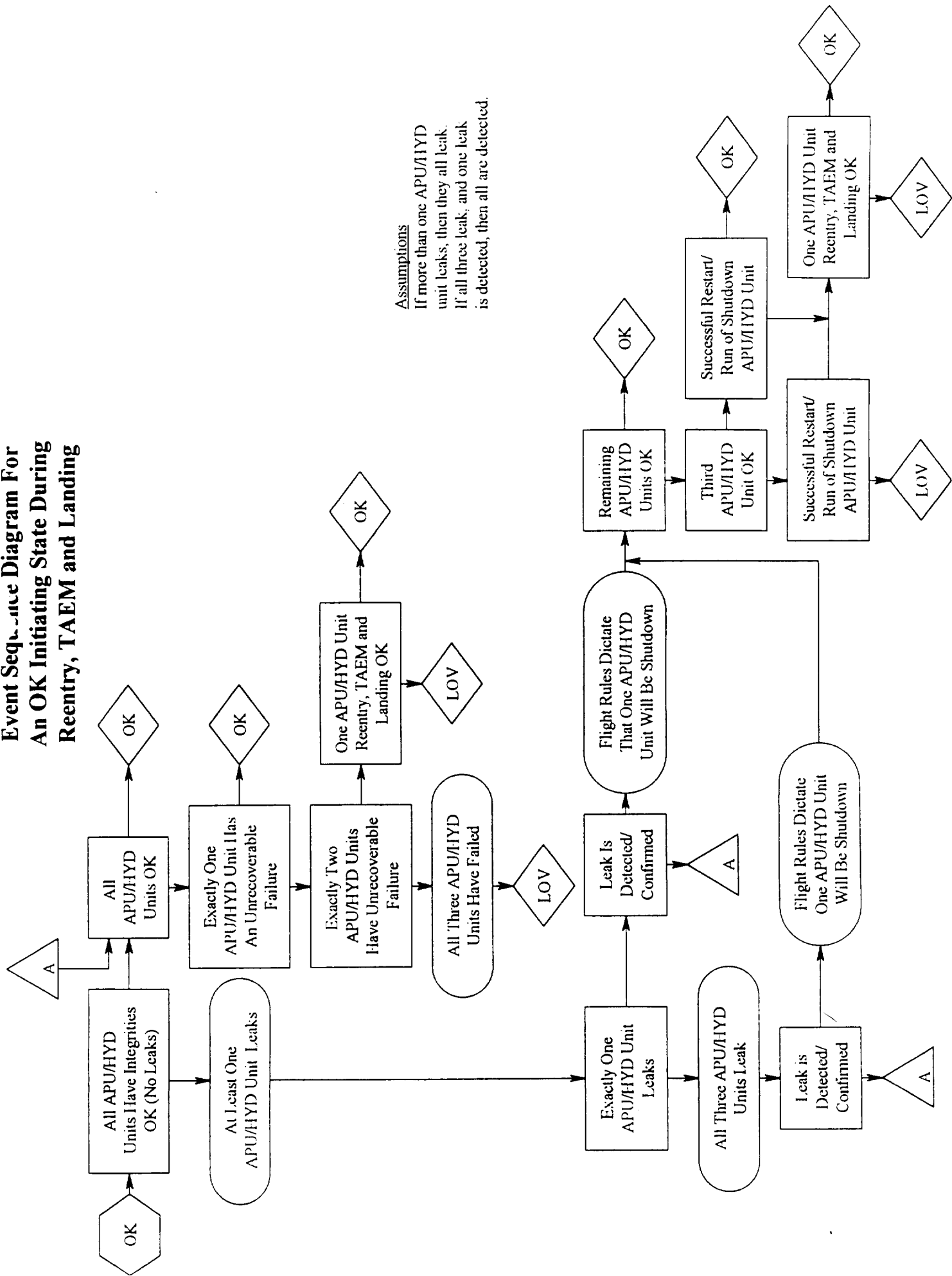
Fault Tree for Sequence 20: LOV End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Fail



**Fault Tree for Sequence 20: LOV End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Fail
(Continued)**



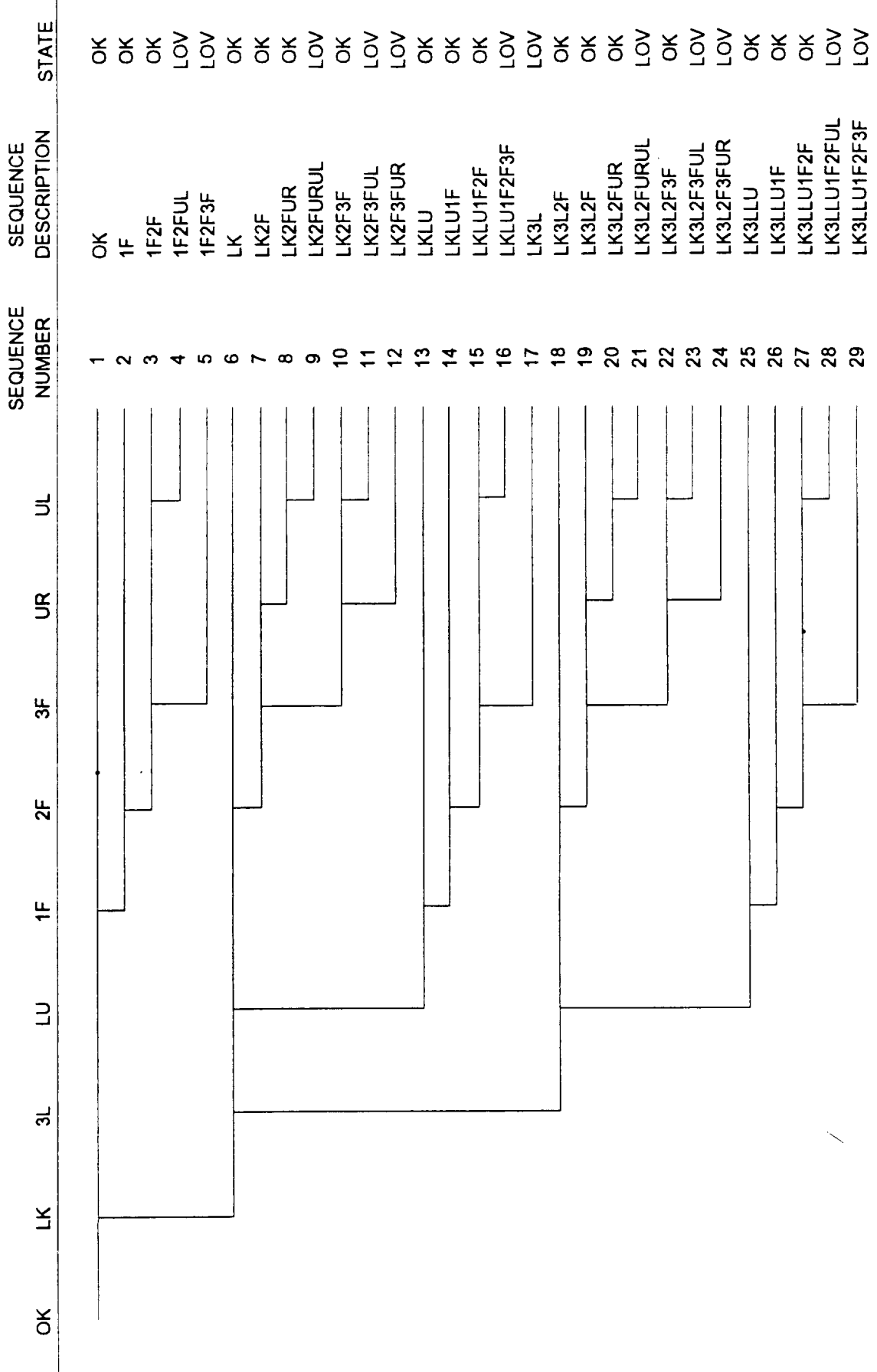
Event Sequence Diagram For An OK Initiating State During Reentry, TAEM and Landing



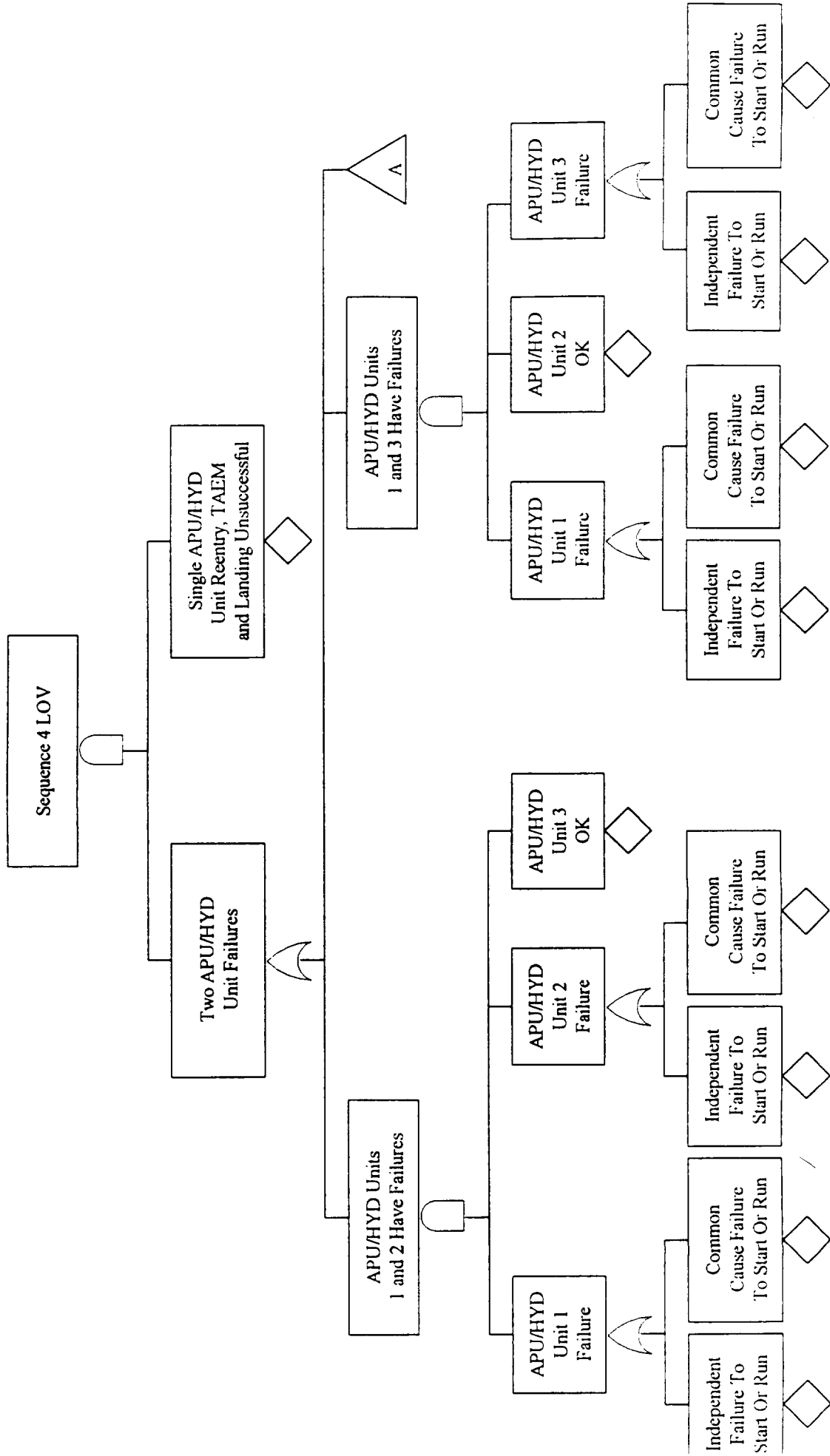
Assumptions

If more than one APU/HYD unit leaks, then they all leak.
 If all three leak, and one leak is detected, then all are detected.

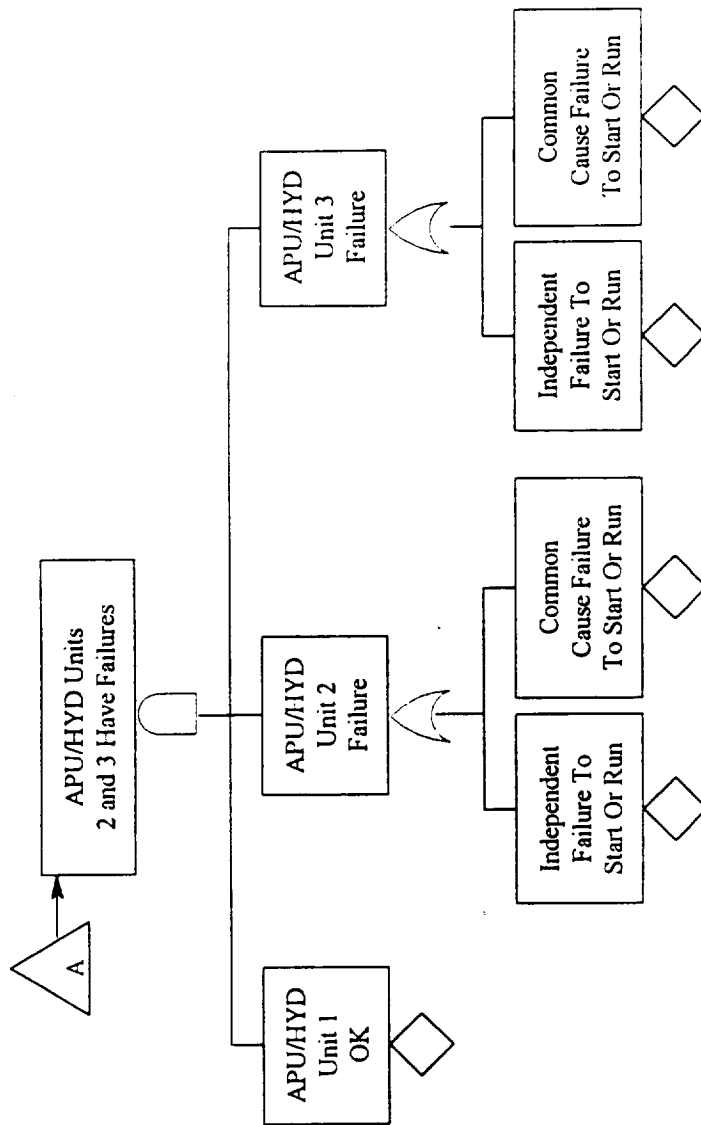
EVENT TREE OF OK STATE DURING REENTRY, TAEM AND LANDING



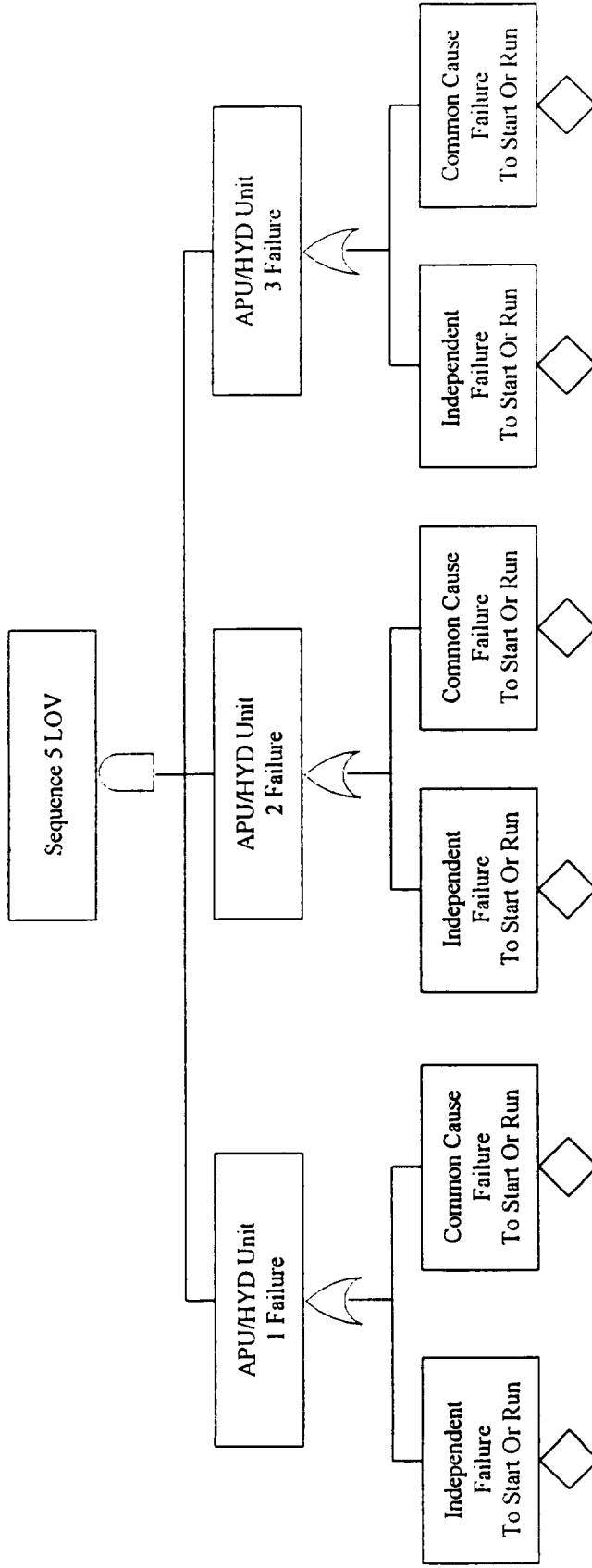
Fault Tree for Sequence 4 LOV: Two APU/HYD Units Fail Without Hydrazine Leaks and Single APU/HYD Unit Reentry, TAEM and Landing is Unsuccessful



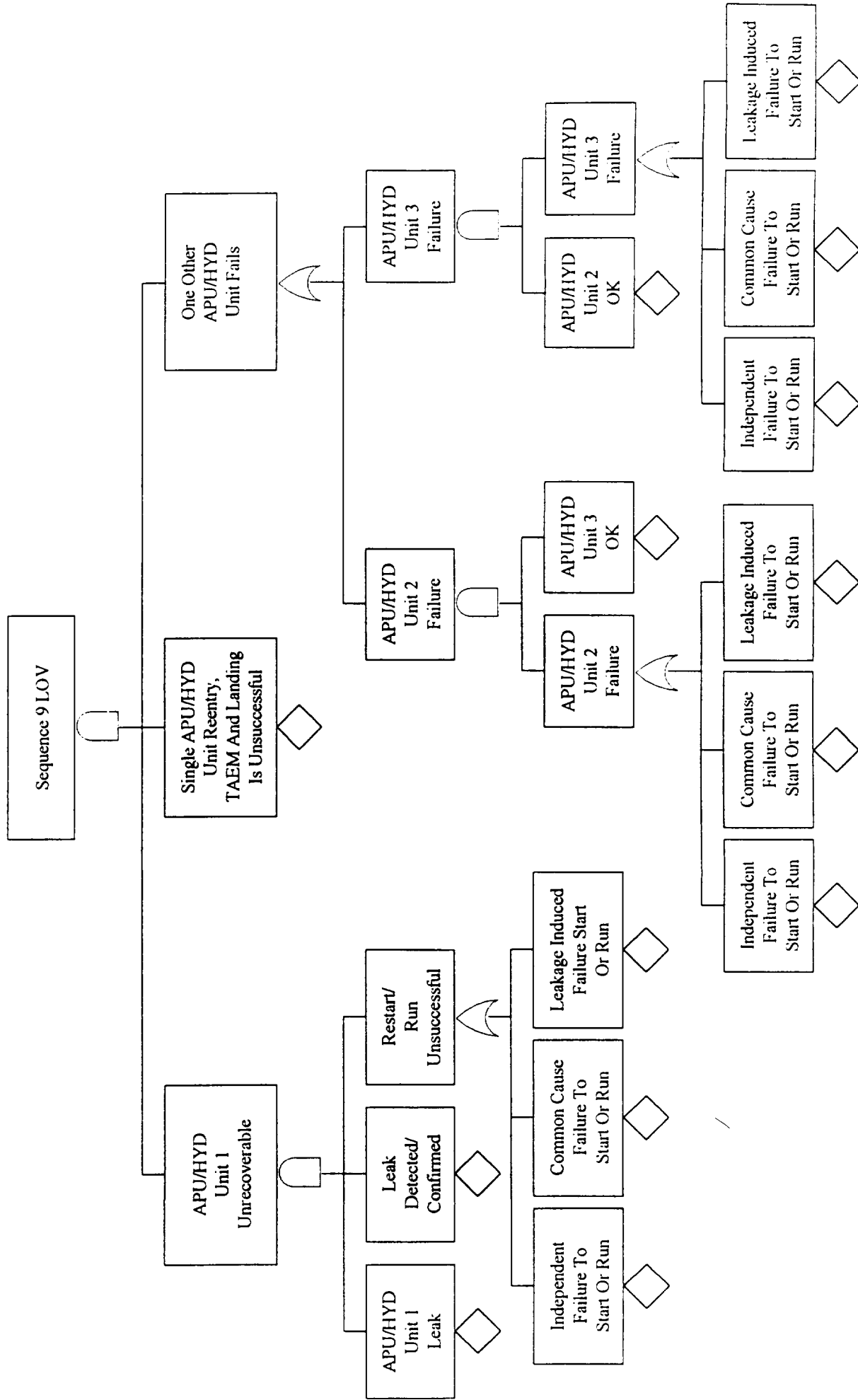
Fault Tree for Sequence 4 LOV: Two APU/HYD Units Fail Without Hydrazine Leaks and Single APU/HYD Unit Reentry, TAEM and Landing is Unsuccessful (Continued)



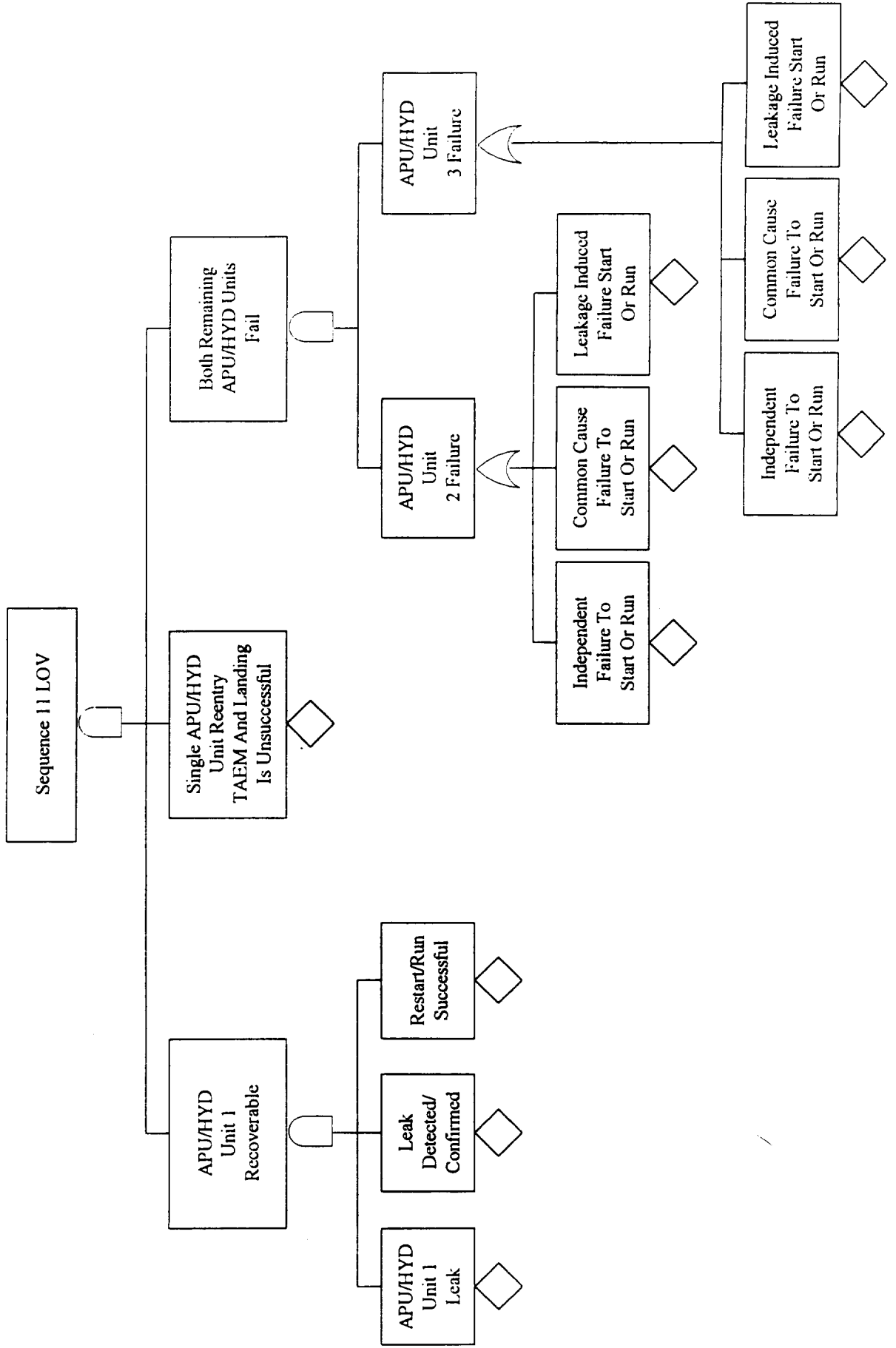
**Fault Tree for Sequence 5 LOV: All Three
APU/HYD Units Fail Without Hydrazine
Leaks During Reentry, TAEM and Landing**



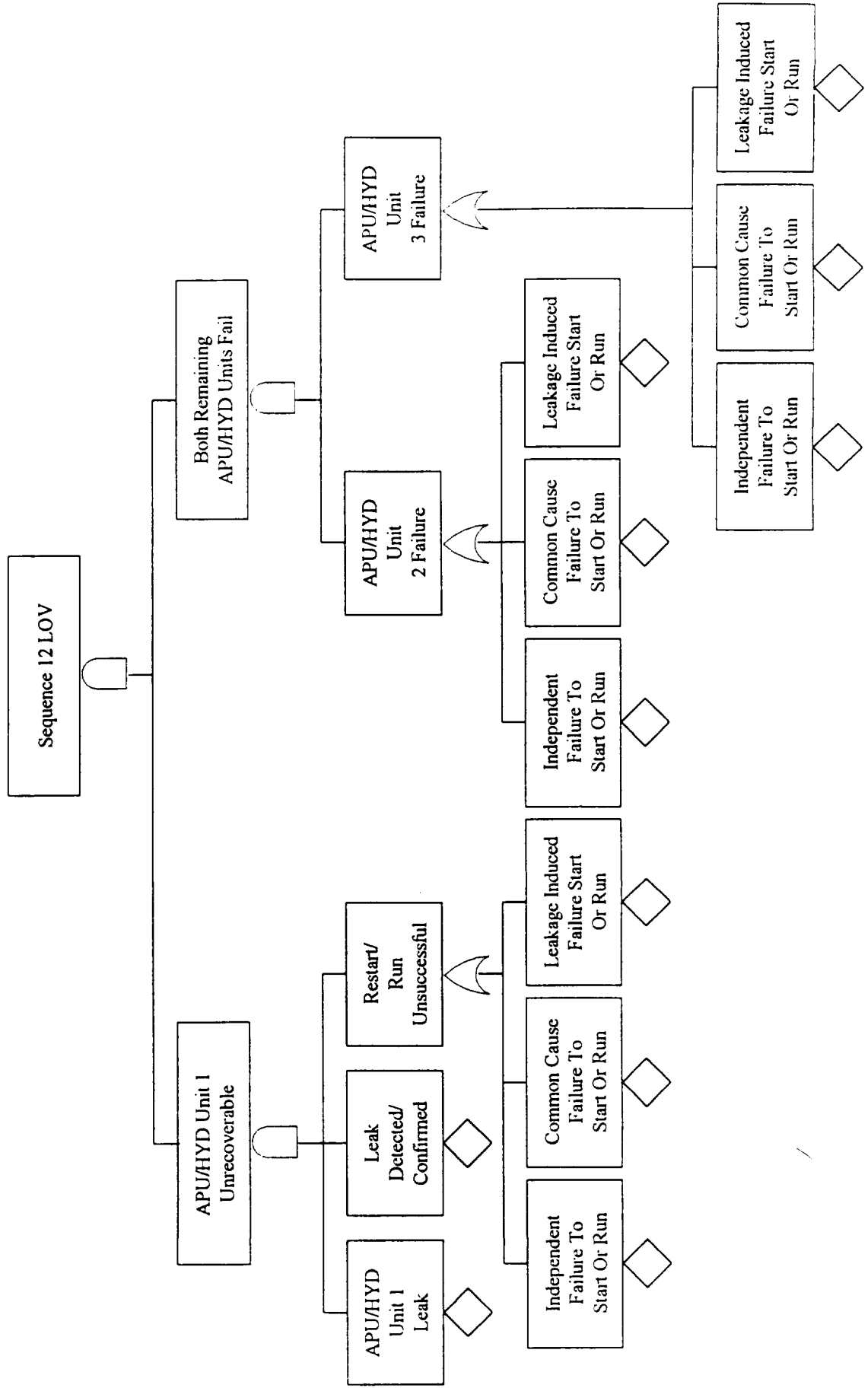
Fault Tree for Sequence 9 LOV: One APU/HYD Unit Leaks and is Shutdown, One Other Unit Fails, Restart of Shutdown APU/HYD Unit is Unsuccessful, and Single APU/HYD Unit Reentry, TAEM and Landing is Unsuccessful



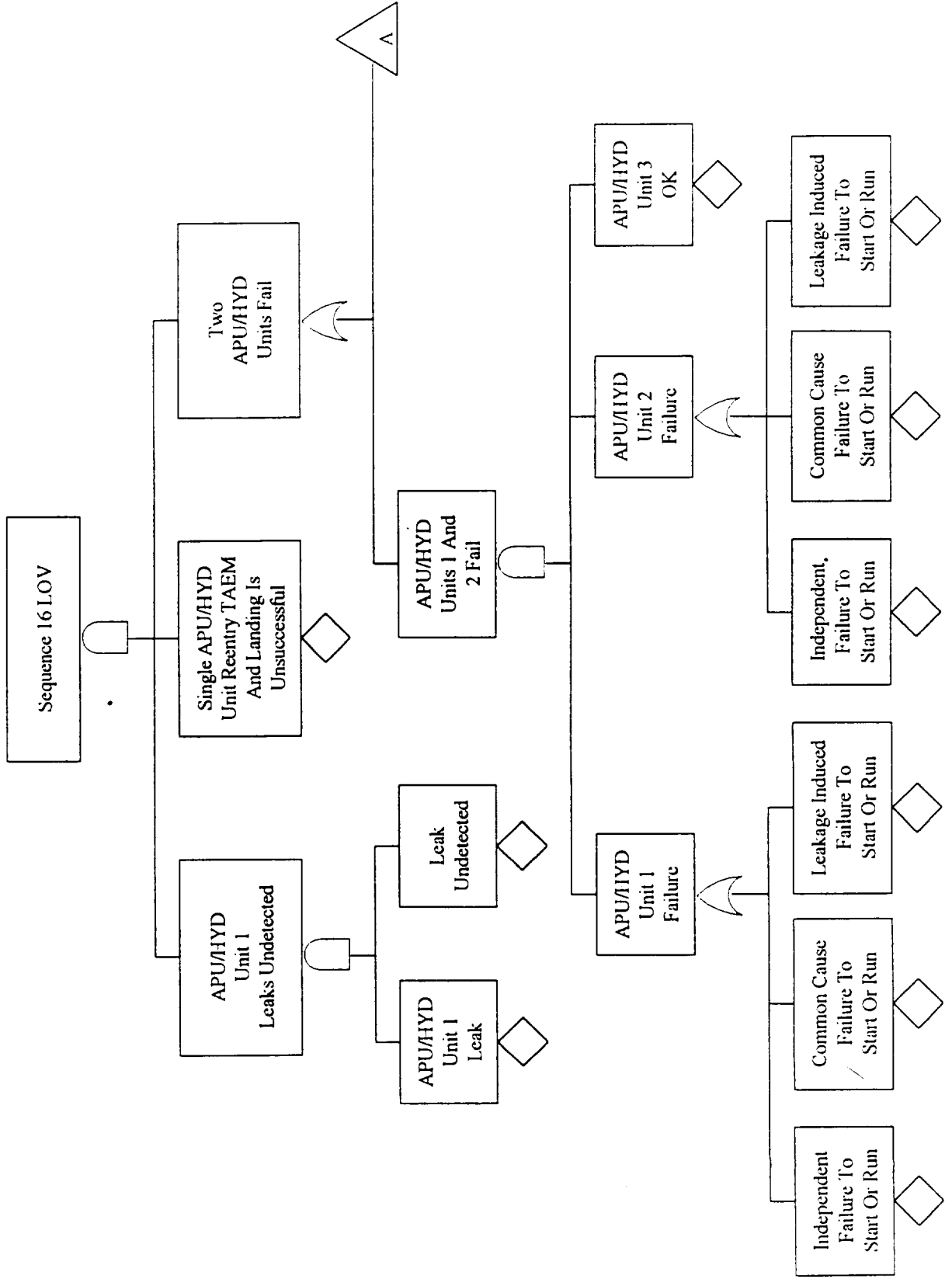
Fault Tree for Sequence 11 LOV: One APU/HYD Unit Leaks and is Shutdown, Remaining Units Both Fail, Restart of Shutdown APU/HYD Unit is Successful, but Single Unit Reentry, TAEM and Landing is Unsuccessful



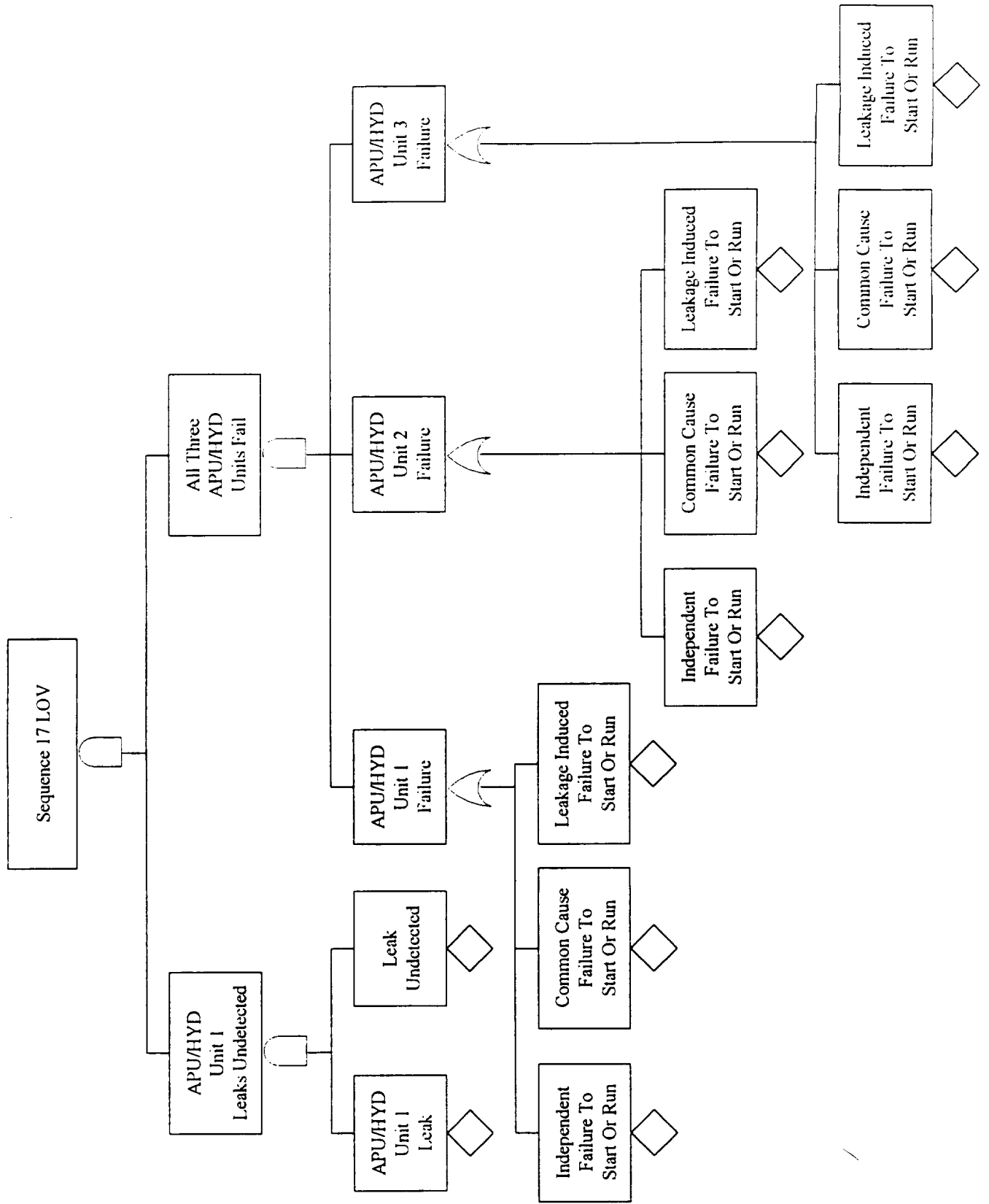
Fault Tree for Sequence 12 LOV: One APU/HYD Unit Leaks and is Shutdown, Both Remaining APU/HYDs Have Failures, and Restart of APU/HYD Unit 1 is Unsuccessful



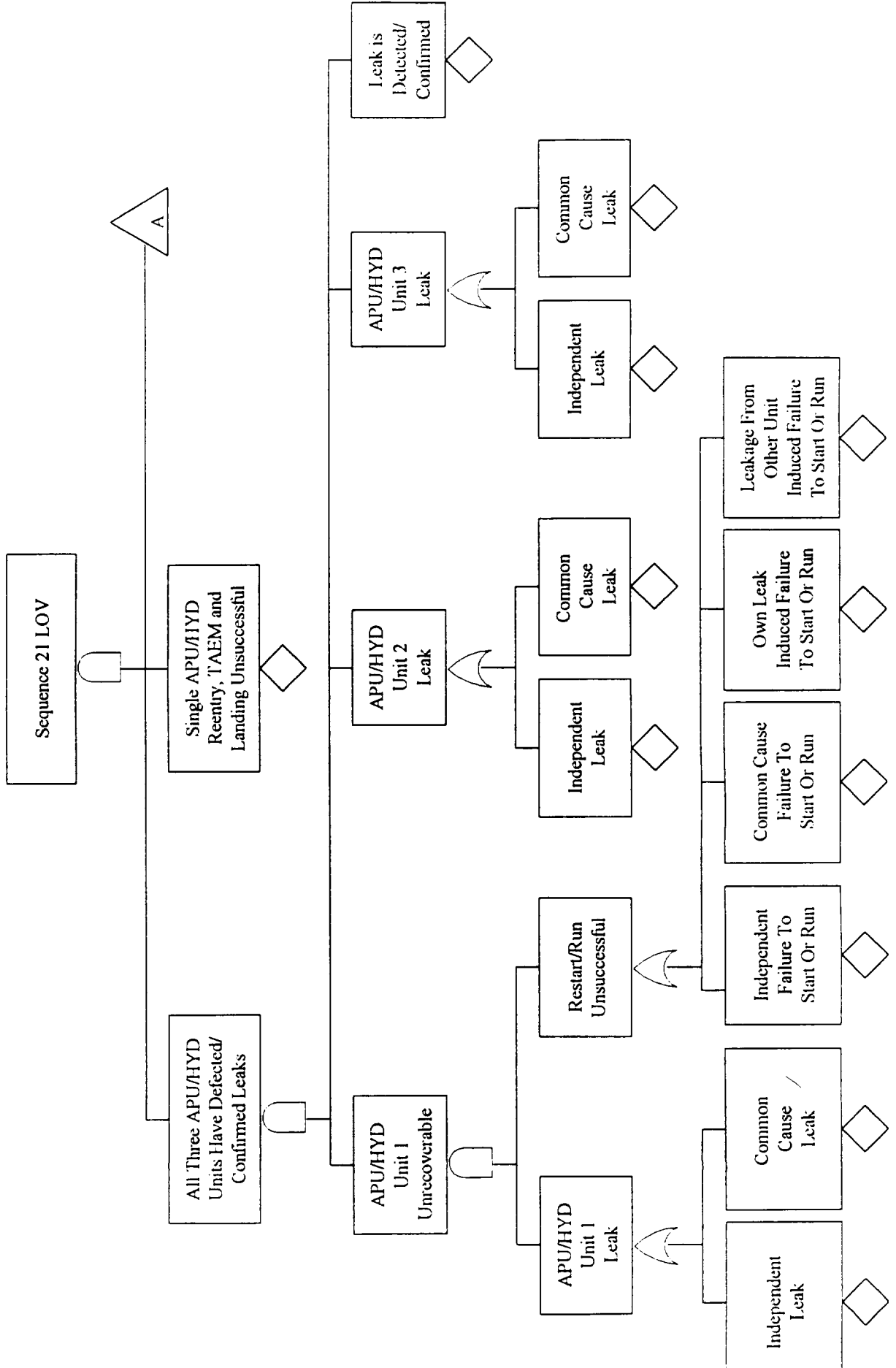
**Sequence 16 LOV: One APU/HYD Unit
Leaks Undetected, Two APU/HYD
Units Fail and Single APU/HYD Unit
Reentry, TAEM and Landing is Unsuccessful**



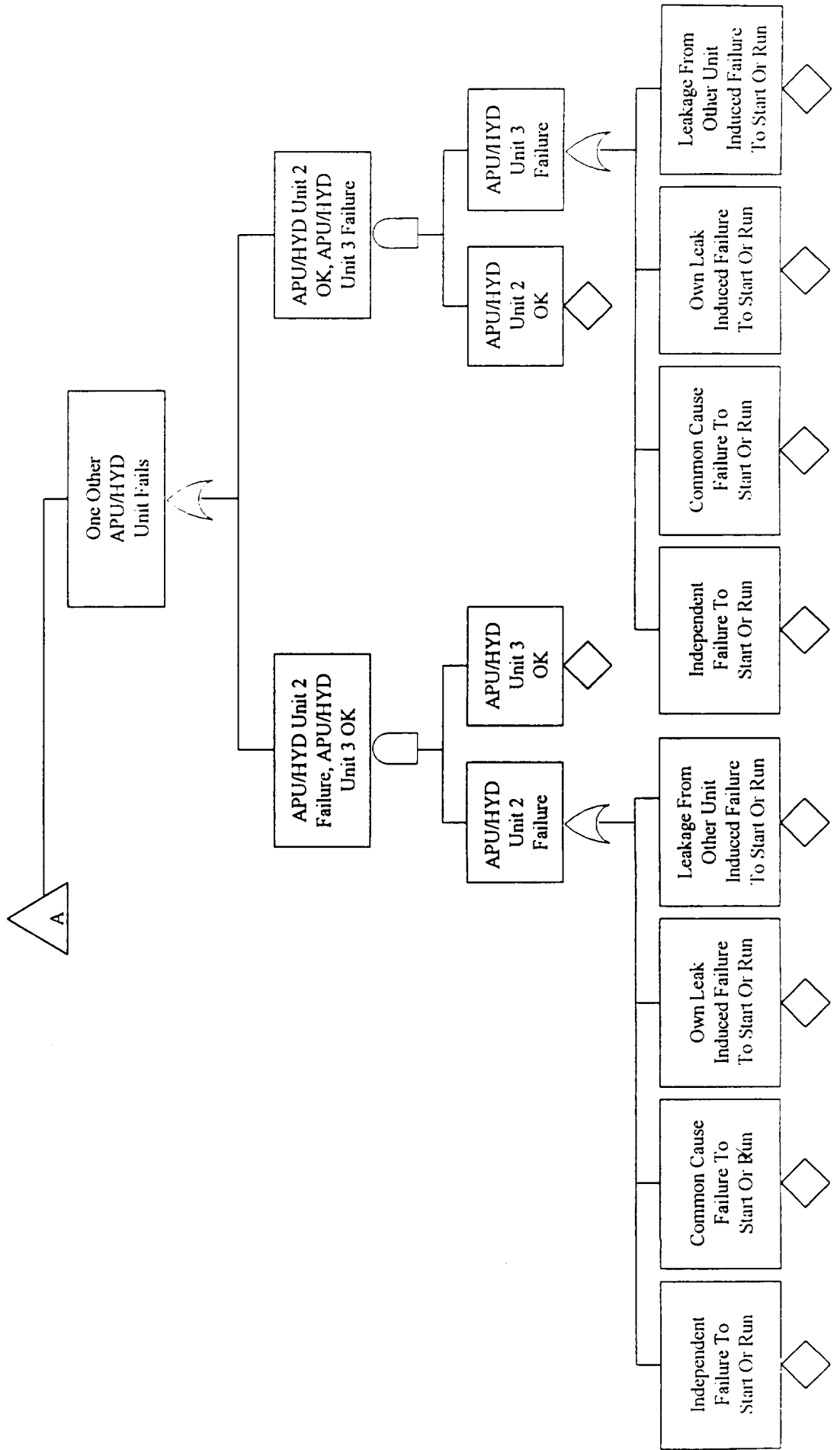
Sequence 17 LOV: One APU/HYD Unit Leaks Undetected and all Three APU/HYD Units Fail



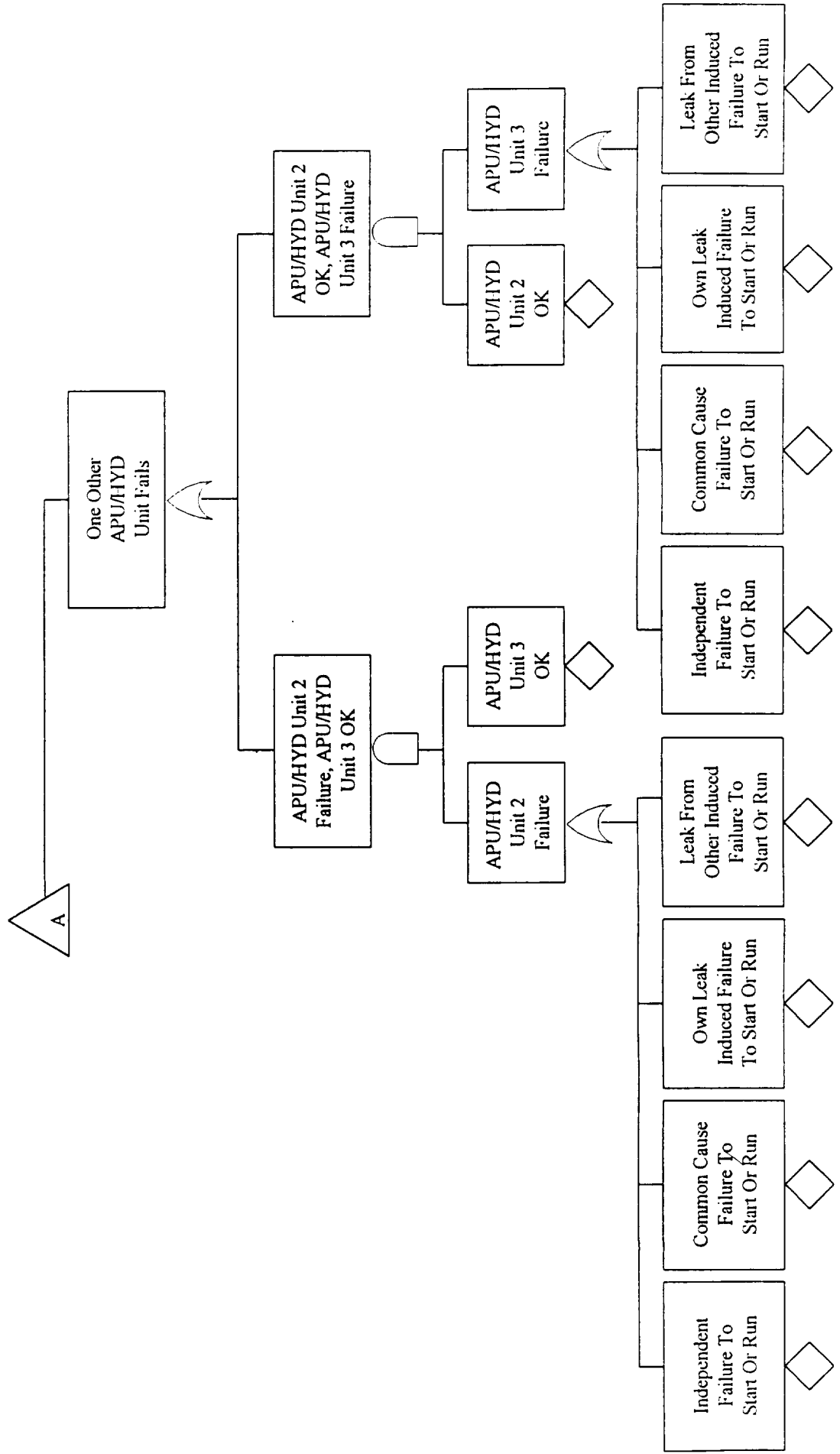
Fault Tree for Sequence 21 LOV: All Three APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, One Other Unit Fails, Restart of Shutdown Unit is Unsuccessful and Single APU/HYD Unit Loading is Unsuccessful



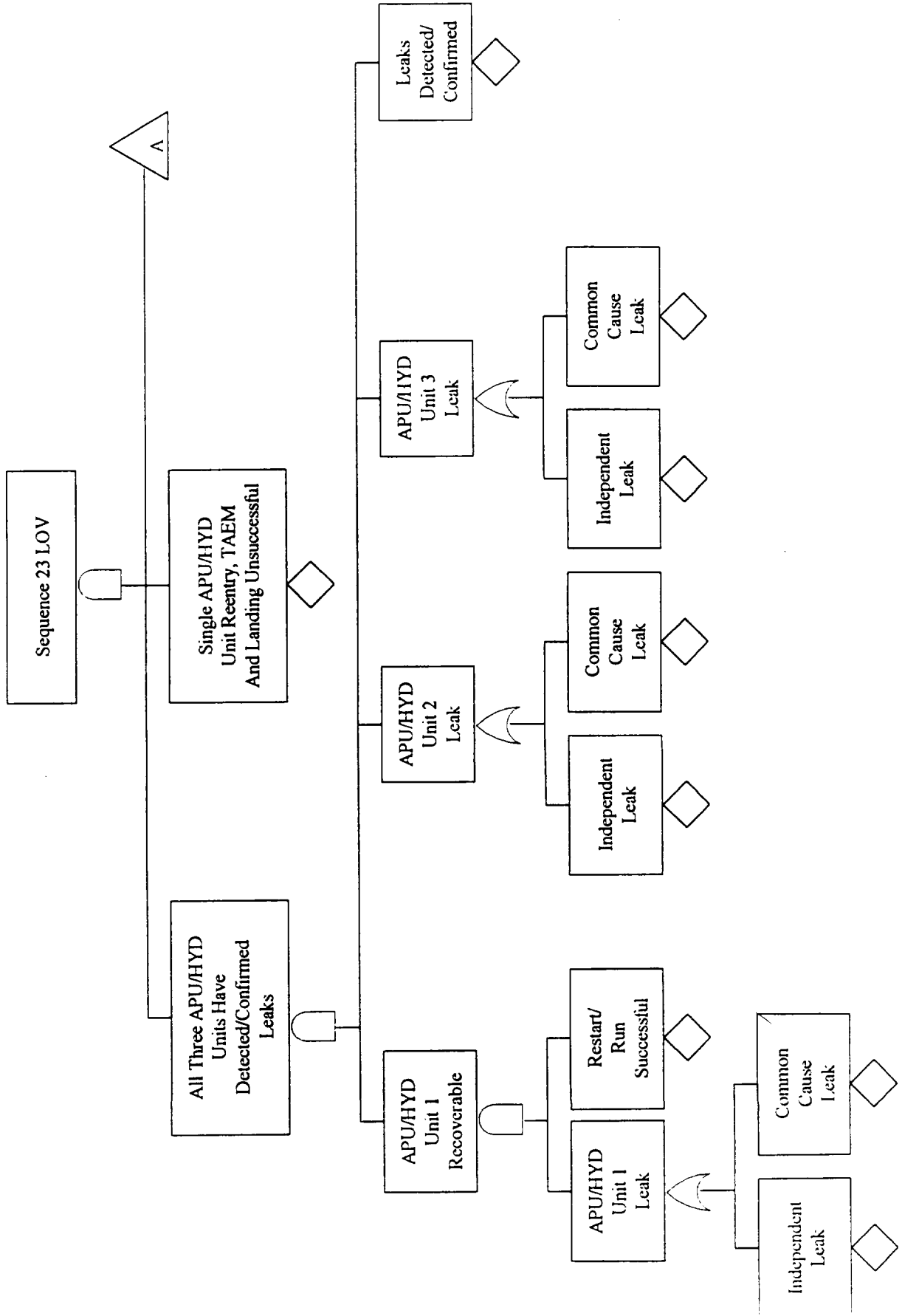
**Fault Tree for Sequence 4. LOV: All Three
 APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, One
 Other Unit Fails, Restart of Shutdown Unit is Unsuccessful
 and Single APU/HYD Unit Loading is Unsuccessful
 (Continued)**



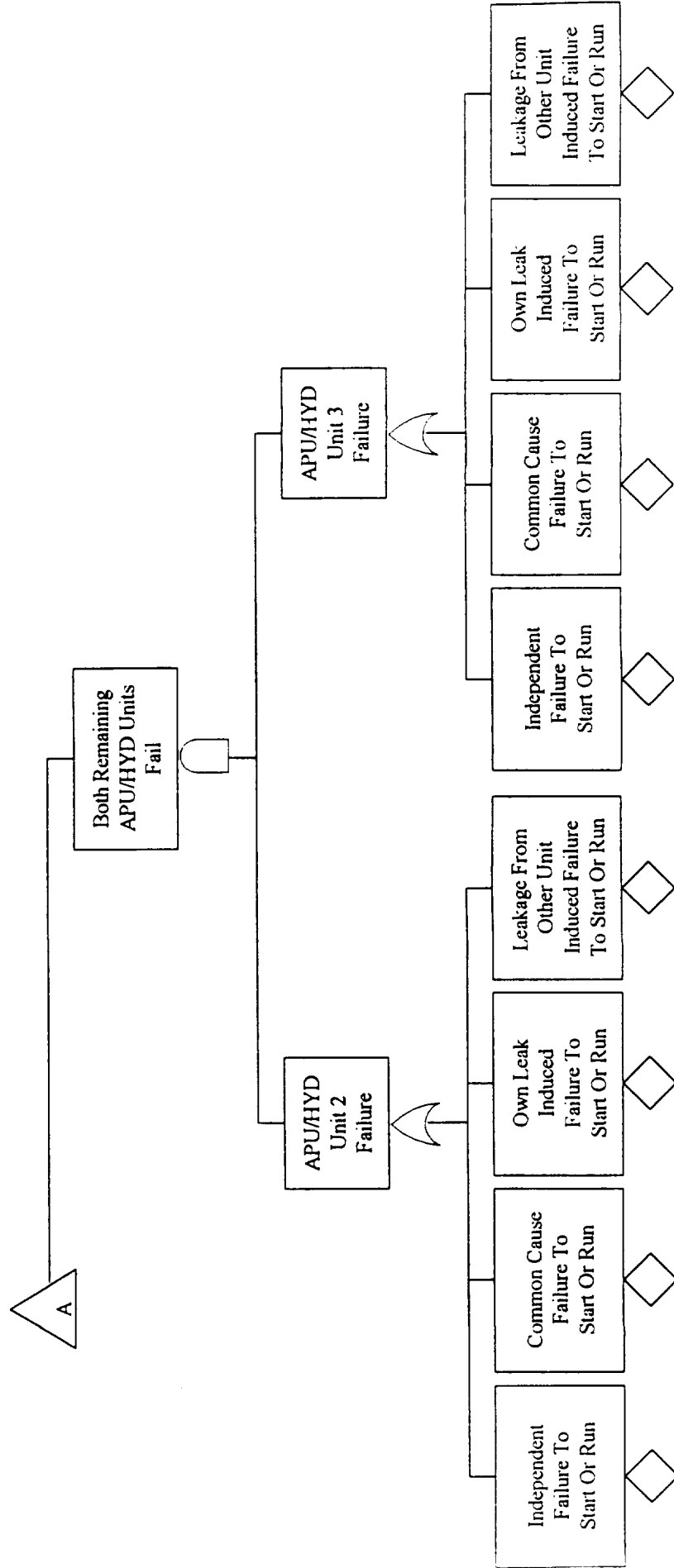
**Fault Tree for Sequence 21 LOV: All Three
 APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, One
 Other Unit Fails, Restart of Shutdown Unit is Unsuccessful
 and Single APU/HYD Unit Loading is Unsuccessful
 (Continued)**



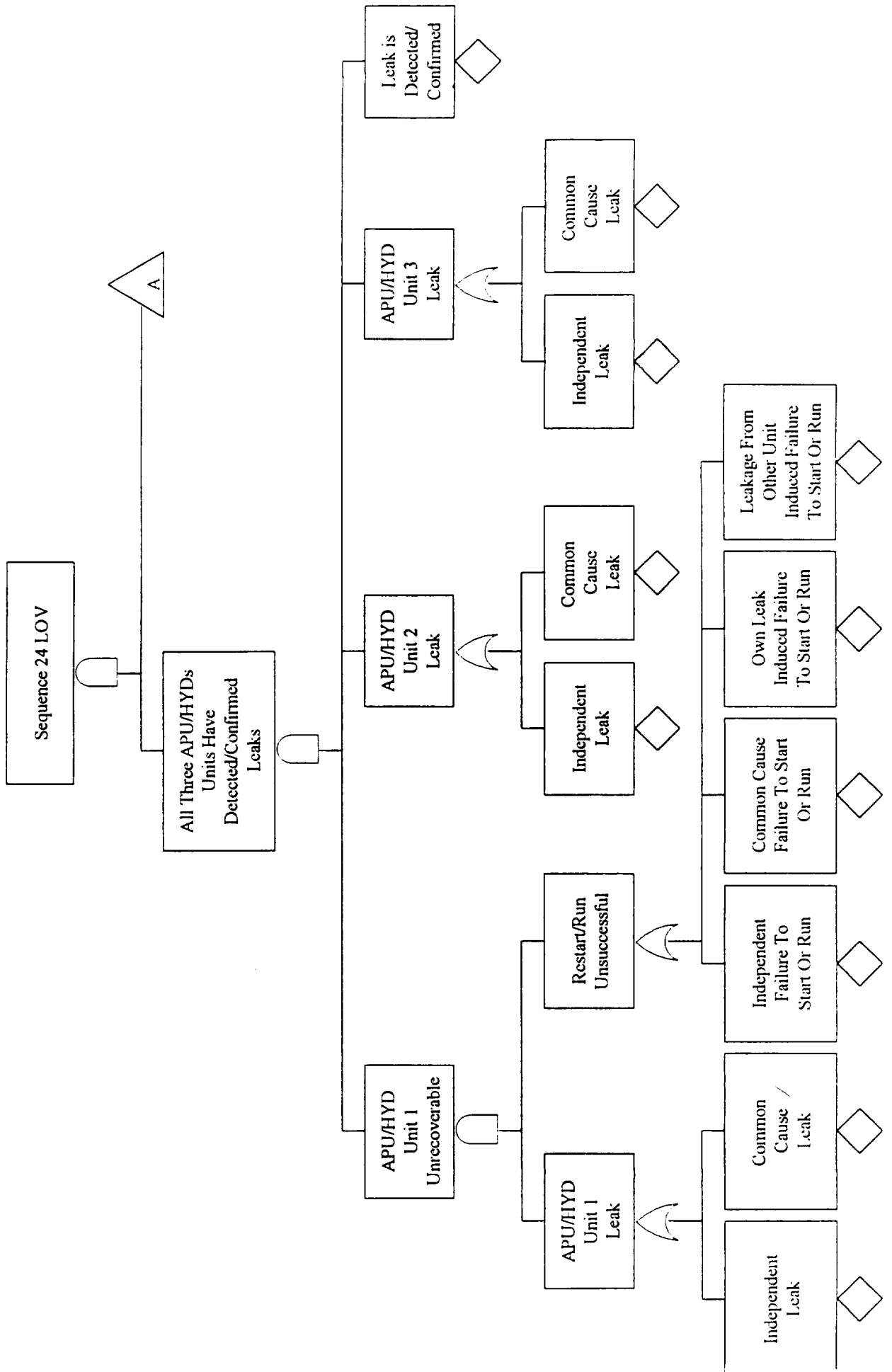
Fault Tree for Sequence 23 LOV: All Three APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, Both Remaining APU/HYD Units Fail, the Shutdown Unit is Restarted, but the Single APU/HYD Unit Reentry, TAEM and Landing is Unsuccessful



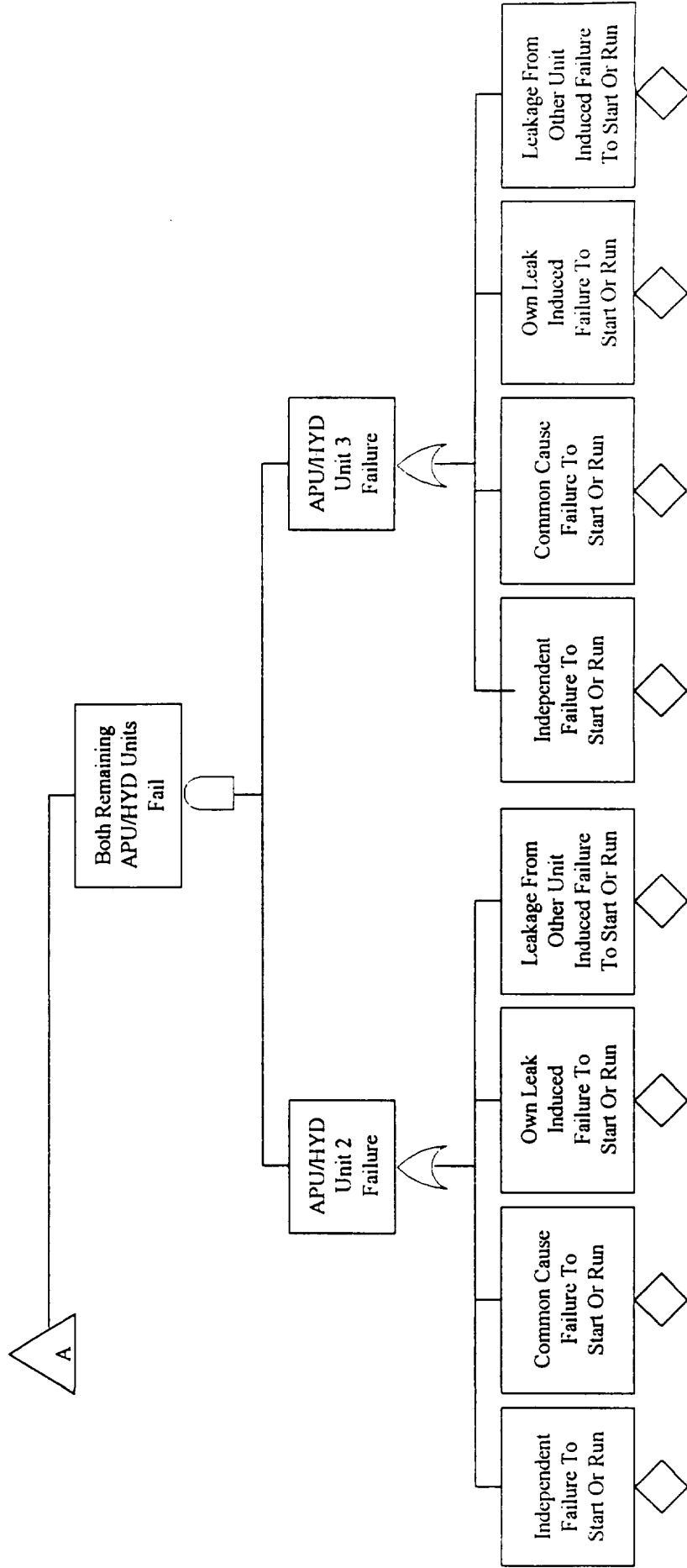
**Fault Tree for Sequence 23 LOV: All Three
 APU/HYD Units Leak, APU/HYD Unit 1 Shutdown, Both
 Remaining APU/HYD Units Fail and Restart of
 Shutdown APU/HYD Unit is Unsuccessful
 (Continued)**



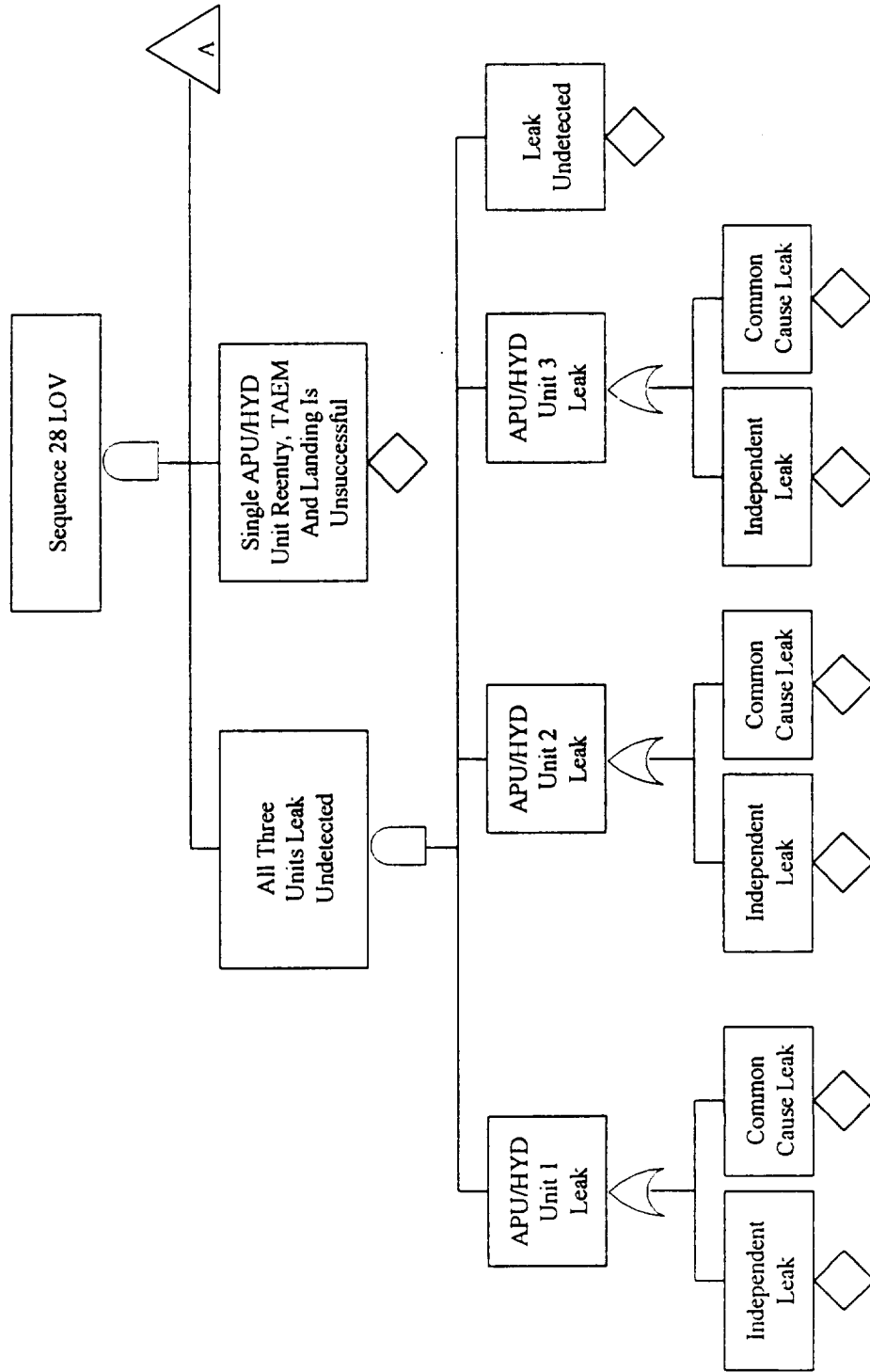
Fault Tree for Sequence 24 LOV: All Three APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, Both Remaining APU/HYD Units Fail and Restart of Shutdown APU/HYD Unit is Unsuccessful



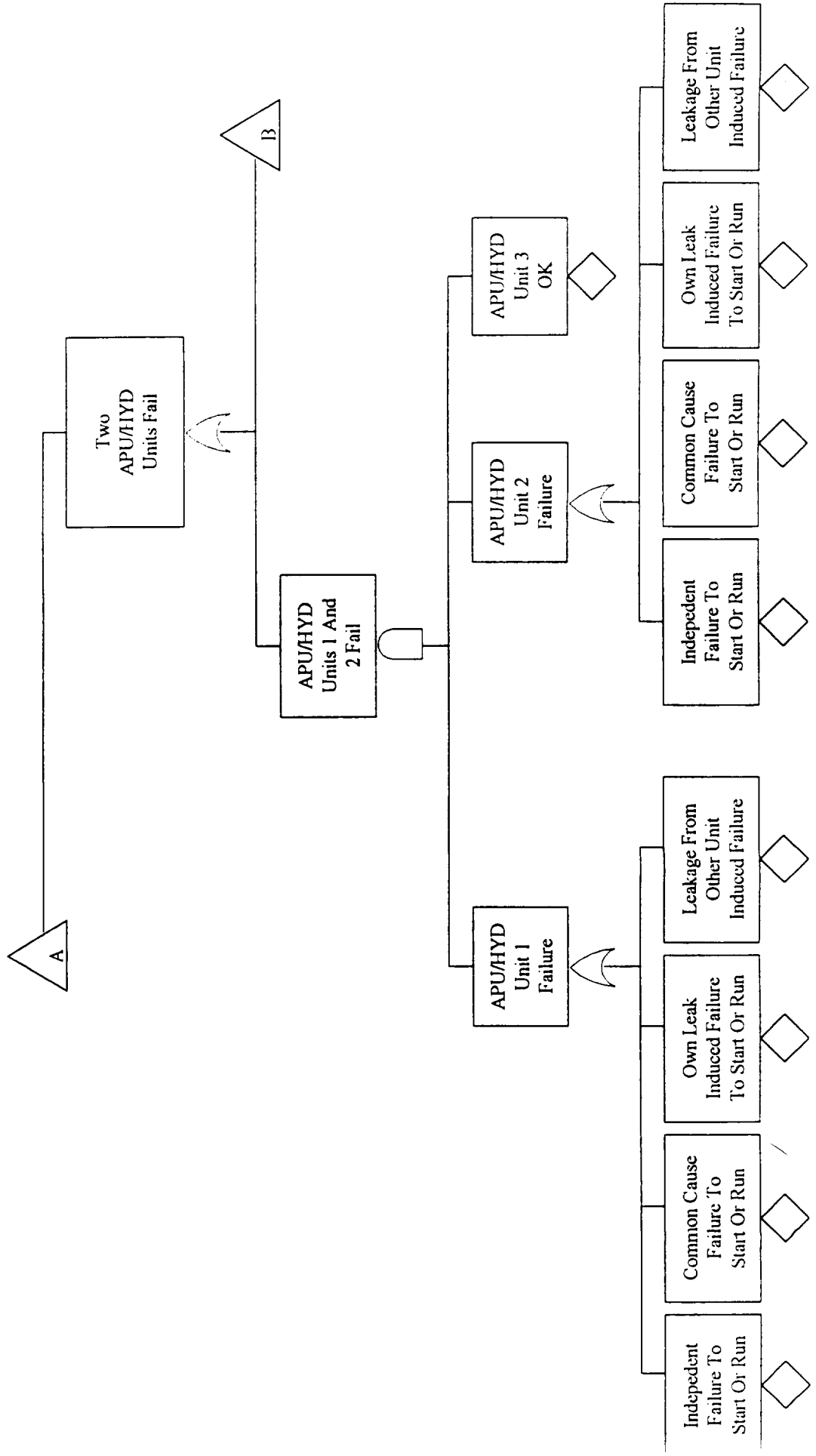
**Fault Tree for Sequence 24 LOV: All Three
 APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, Both
 Remaining APU/HYD Units Fail and Restart of
 Shutdown APU/HYD Unit is Unsuccessful
 (Continued)**



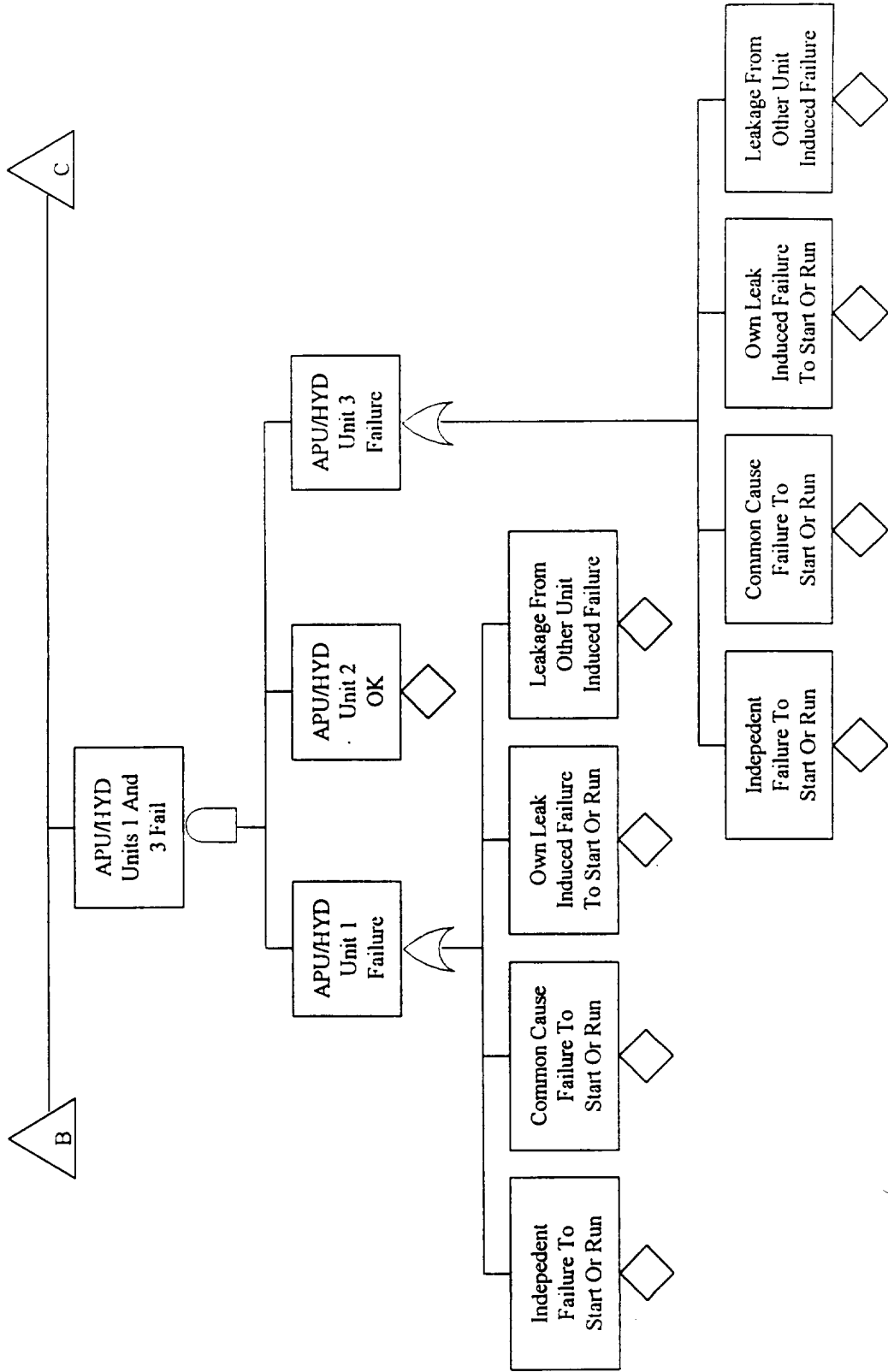
**Fault Tree for Sequence 28 LOV: All Three
APU/HYD Units Leak Undetected,
Two APU/HYD Units Fail, Single APU/HYD
Unit Landing Unsuccessful**



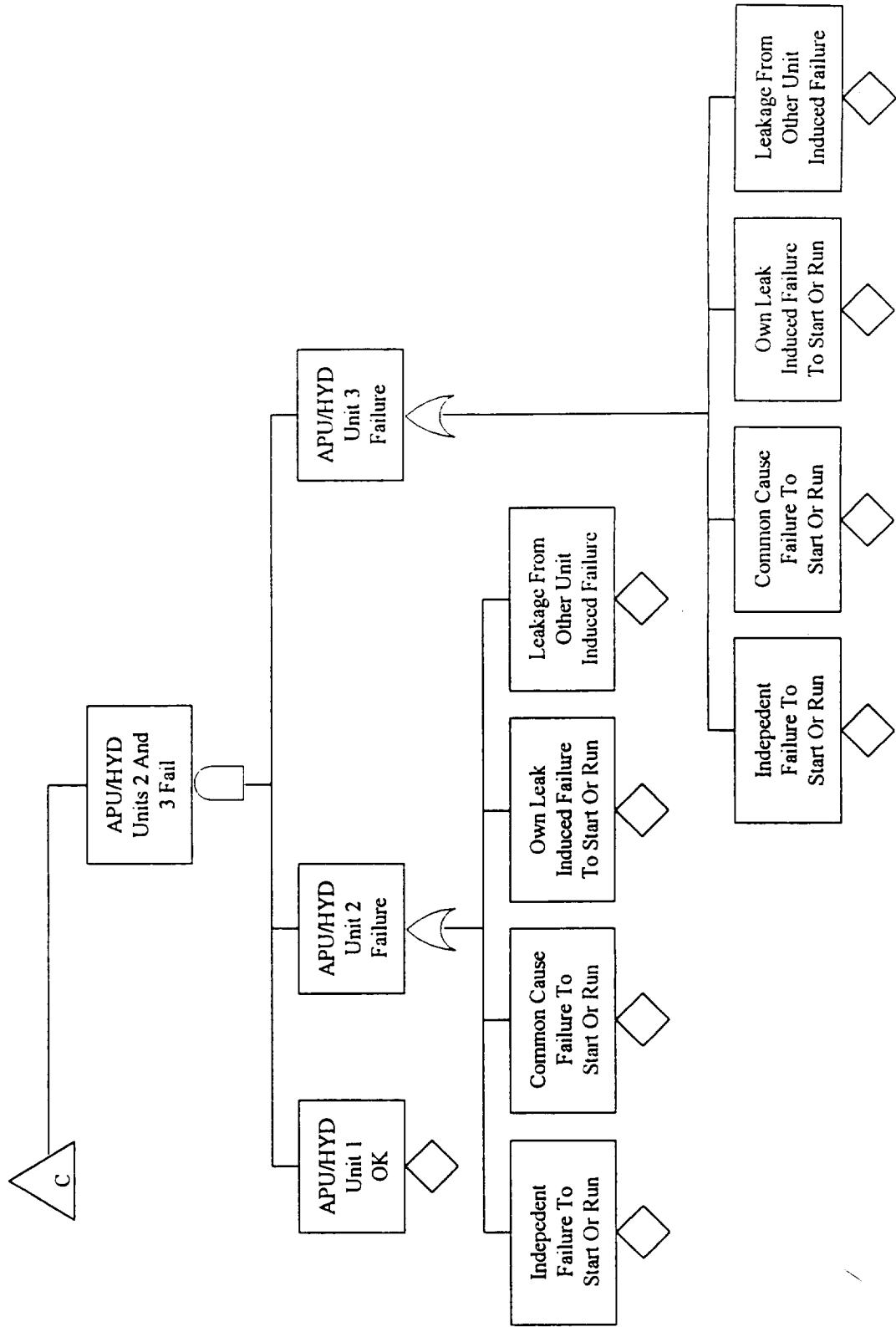
**Fault Tree for Sequence 28 LOV: All Three
APU/HYD Units Leak Undetected,
Two APU/HYD Units Fail, Single APU/HYD
Unit Landing Unsuccessful (Continued)**



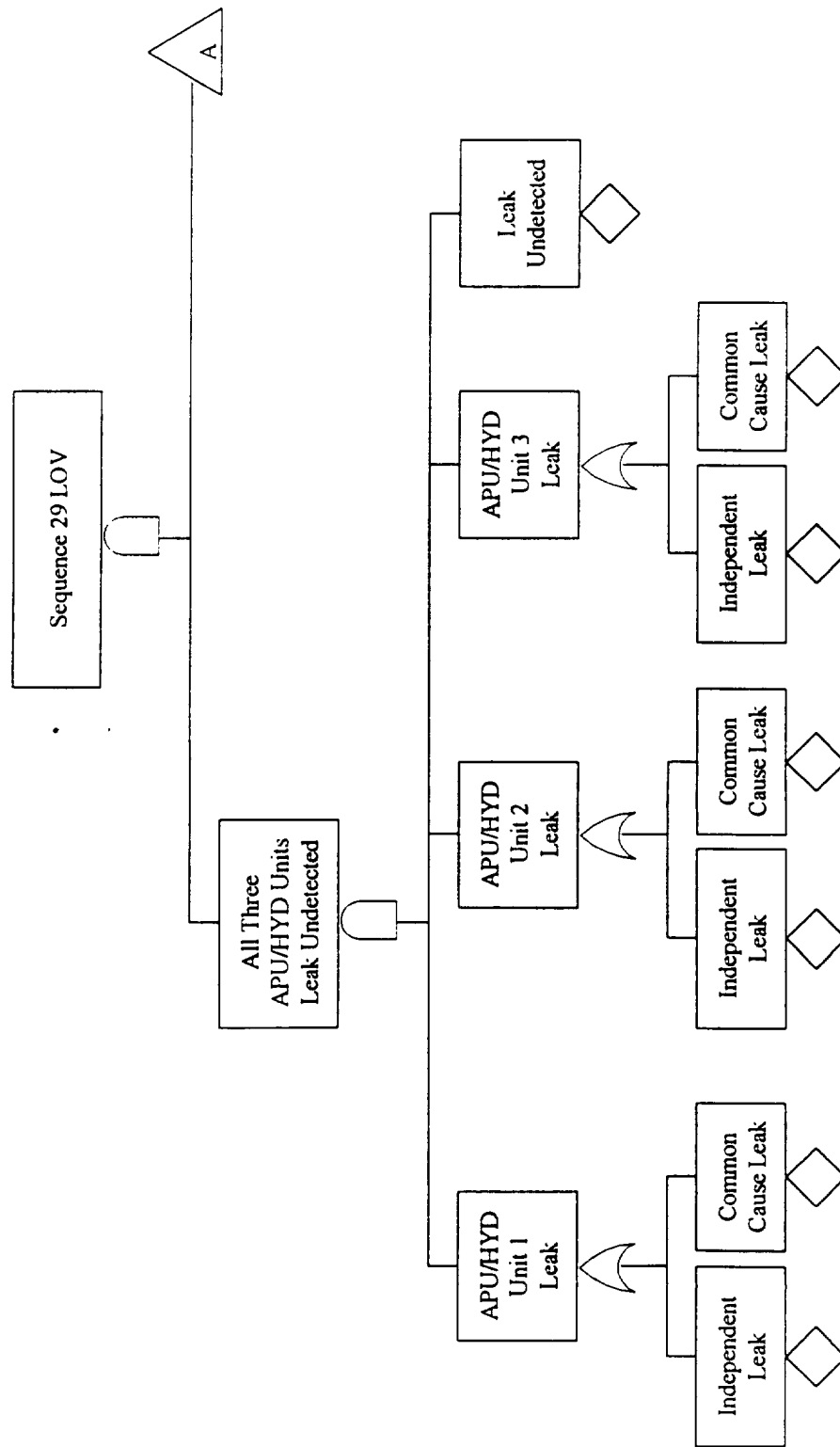
**Fault Tree for Sequence 28 LOV: All Three
APU/HYD Units Leak Undetected,
Two APU/HYD Units Fail, Single APU/HYD
Unit Landing Unsuccessful (Continued)**



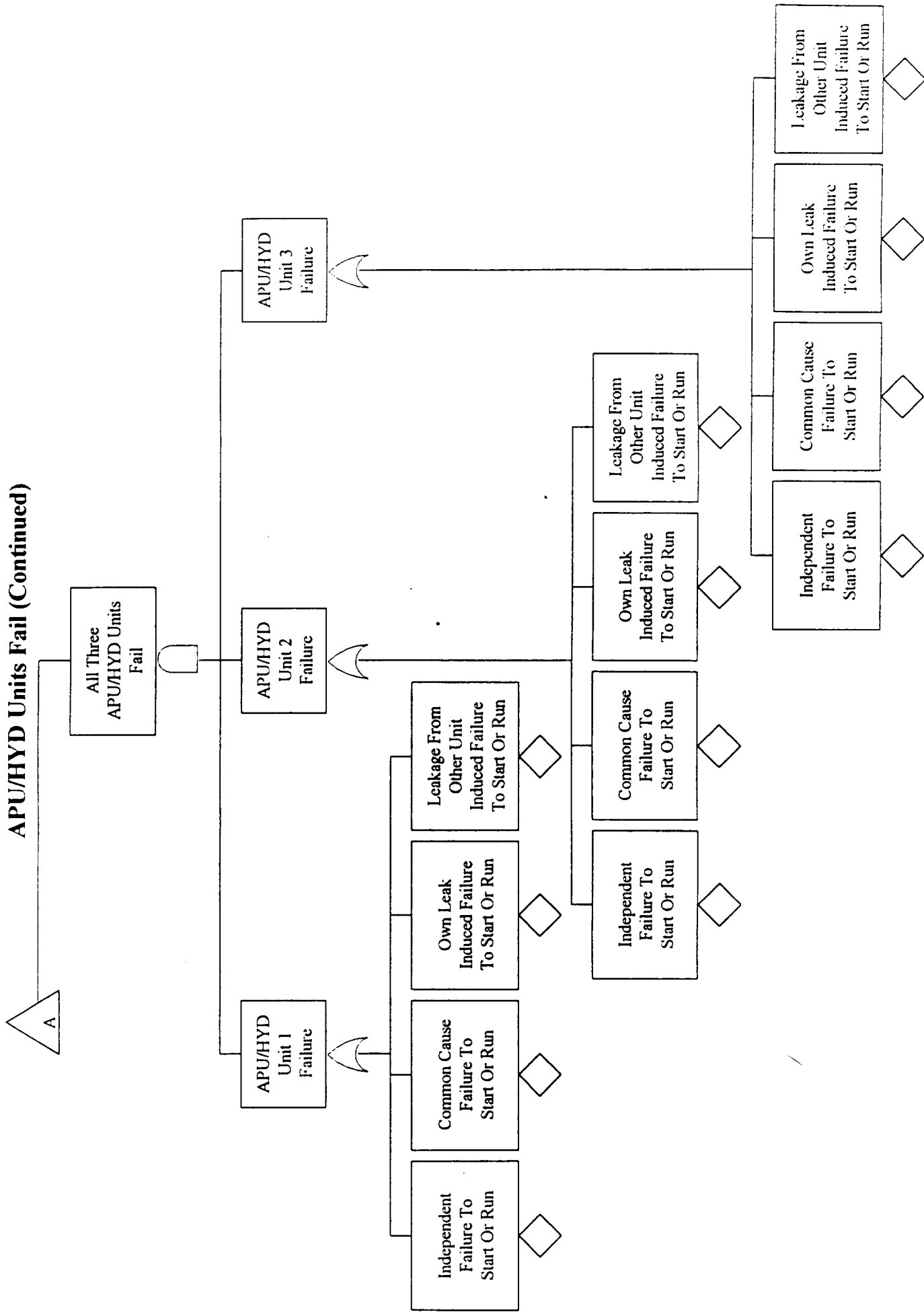
**Fault Tree for Sequence 28 LOV: All Three
APU/HYD Units Leak Undetected,
Two APU/HYD Units Fail, Single APU/HYD
Unit Landing Unsuccessful (Continued)**



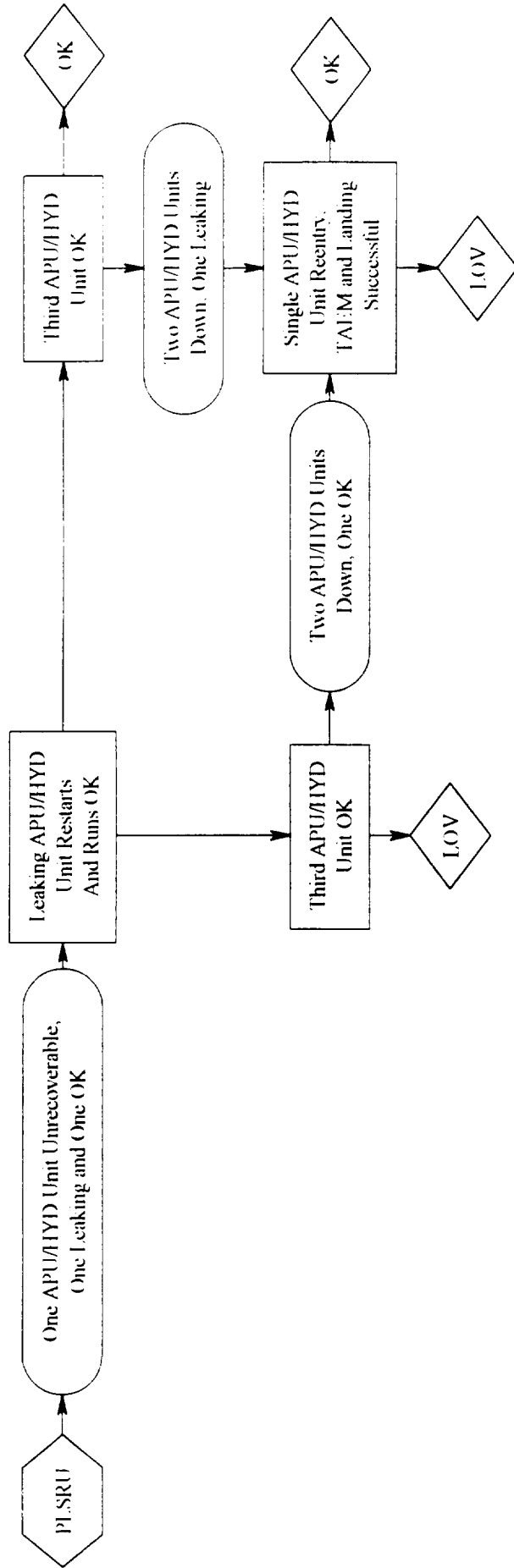
**Fault Tree for Sequence 29 LOV: All Three
APU/HYD Units Leak Undetected and all Three
APU/HYD Units Fail**



**Fault Tree for Sequence 29 LOV: All Three
APU/HYD Units Leak Undetected and all Three
APU/HYD Units Fail (Continued)**



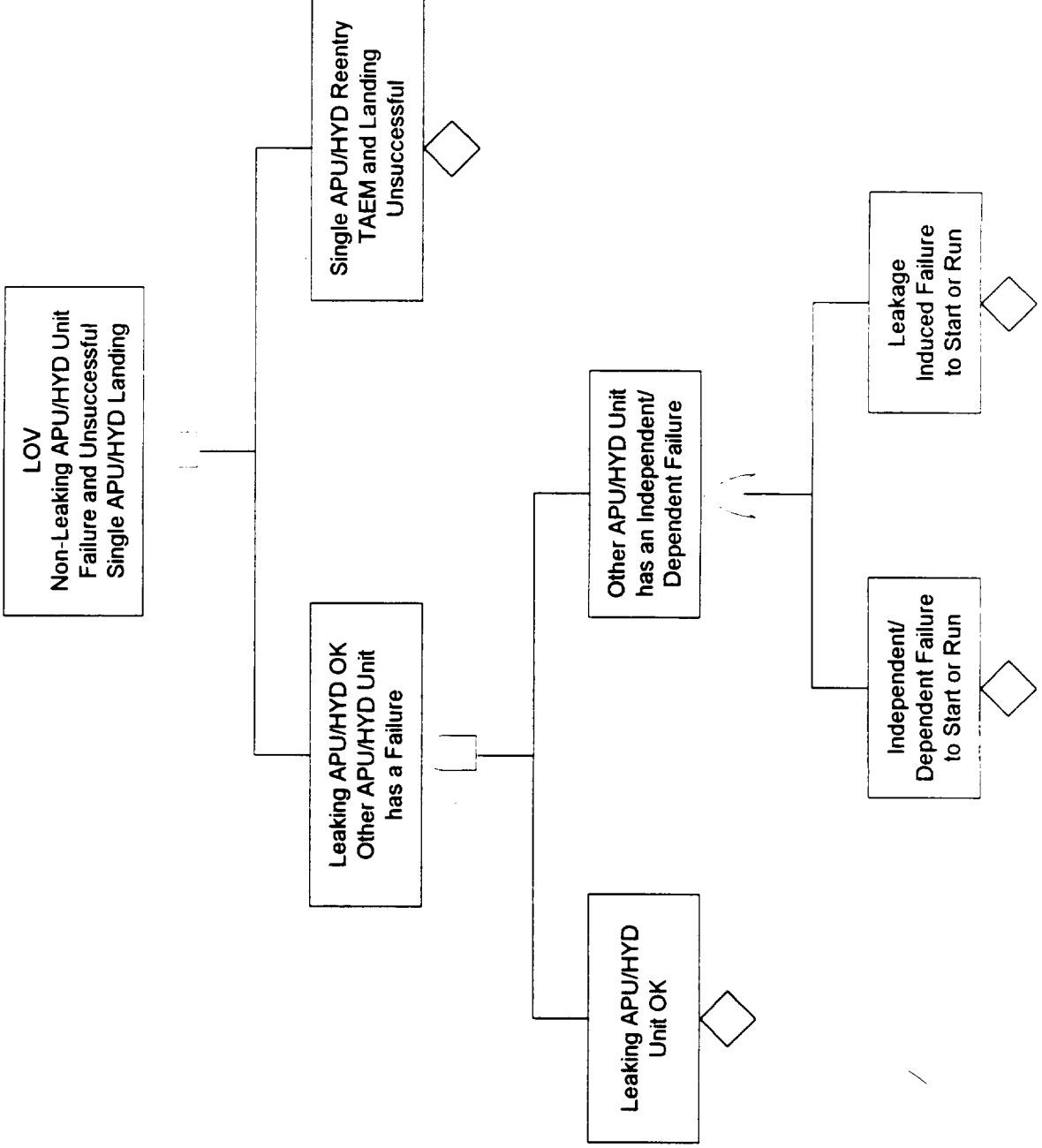
**Event Sequence Diagram
for a PLSRU State During
Reentry, TAEM and Landing**



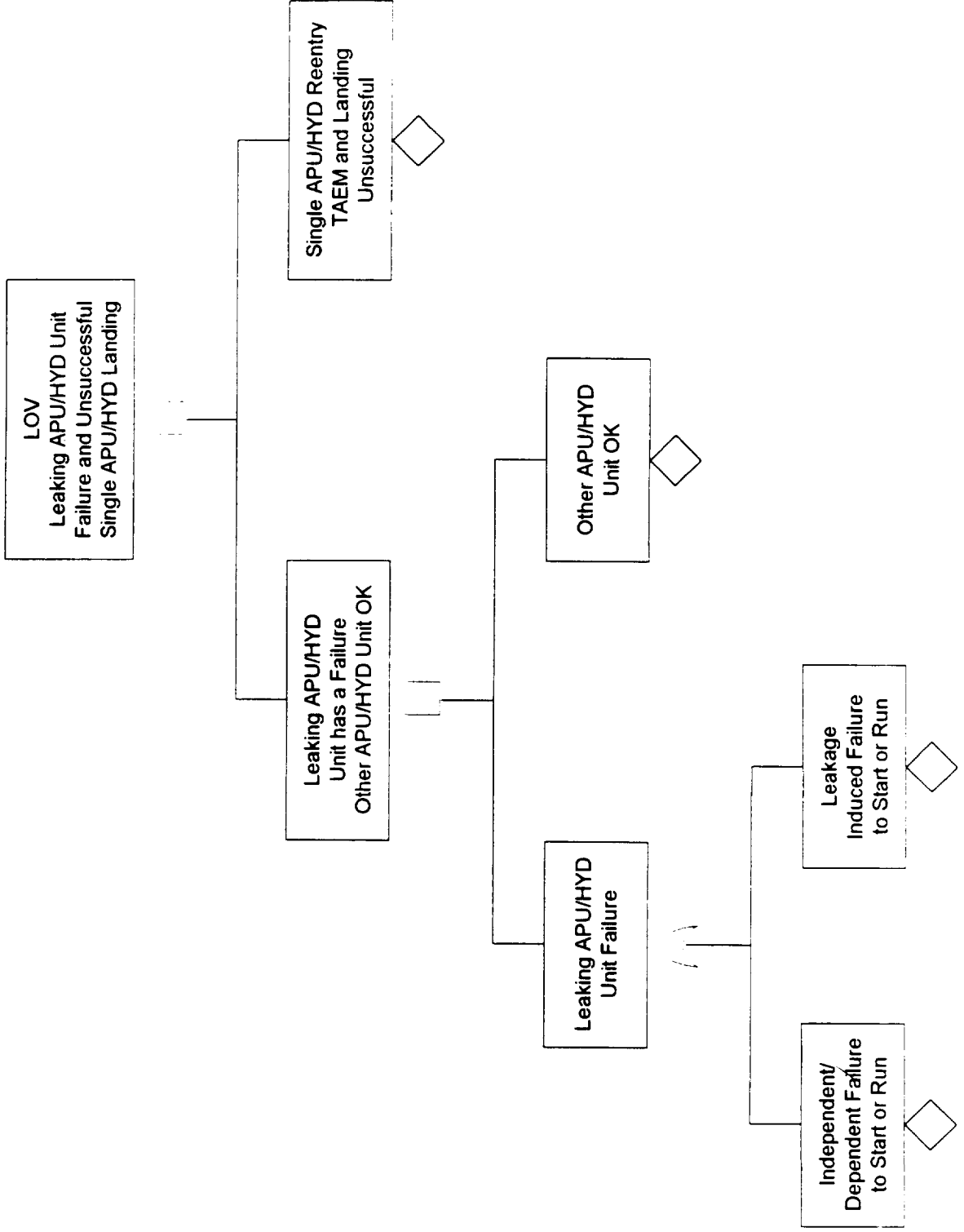
EVENT TREE OF A PLSRU INITIATING EVENT DURING REENTRY, TAEM AND LANDING

RU	UR	3F	UL	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
				1	RU	OK
				2	RU3F	OK
				3	RU3FUL	LOV
				4	RUUR	OK
				5	RUURUL	LOV
				6	RUUR3F	LOV

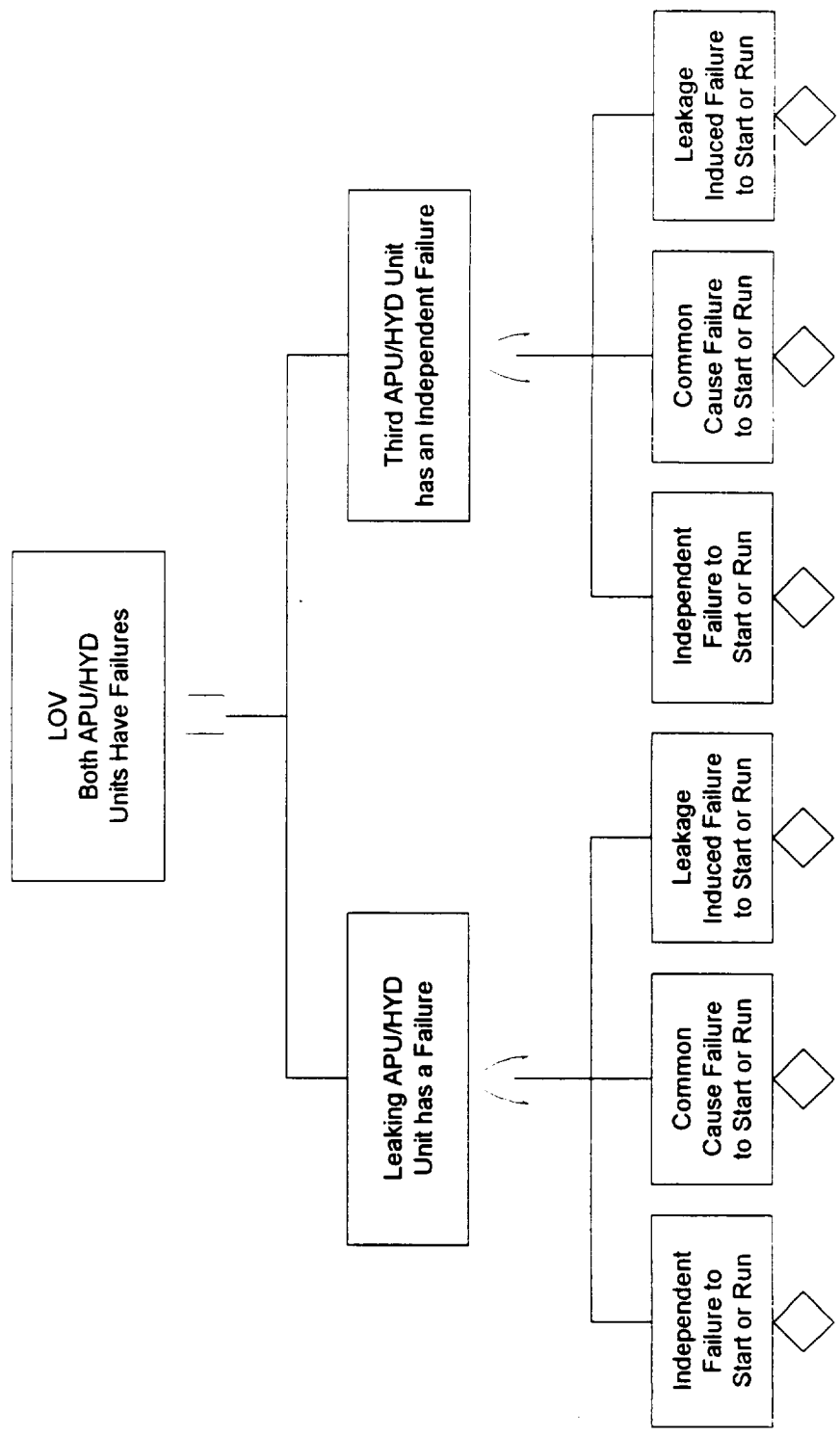
**Fault Tree For Sequence 3 LOV
State With PLSRU Initiating Event
During Reentry, TAEM and Landing**



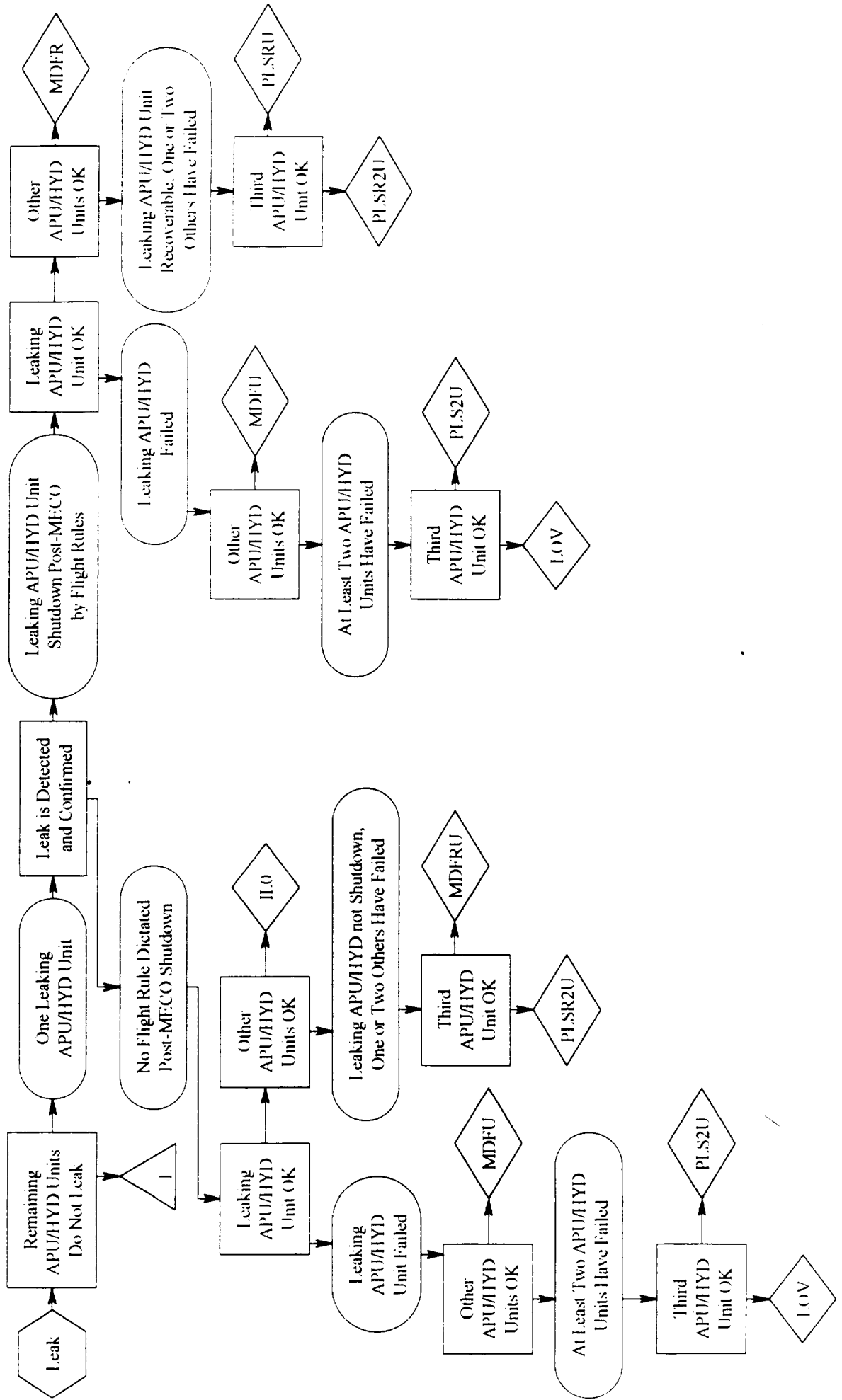
Fault Tree For Sequence 5 LOV State With PLSRU Initiating Event During Reentry, TAEM and Landing



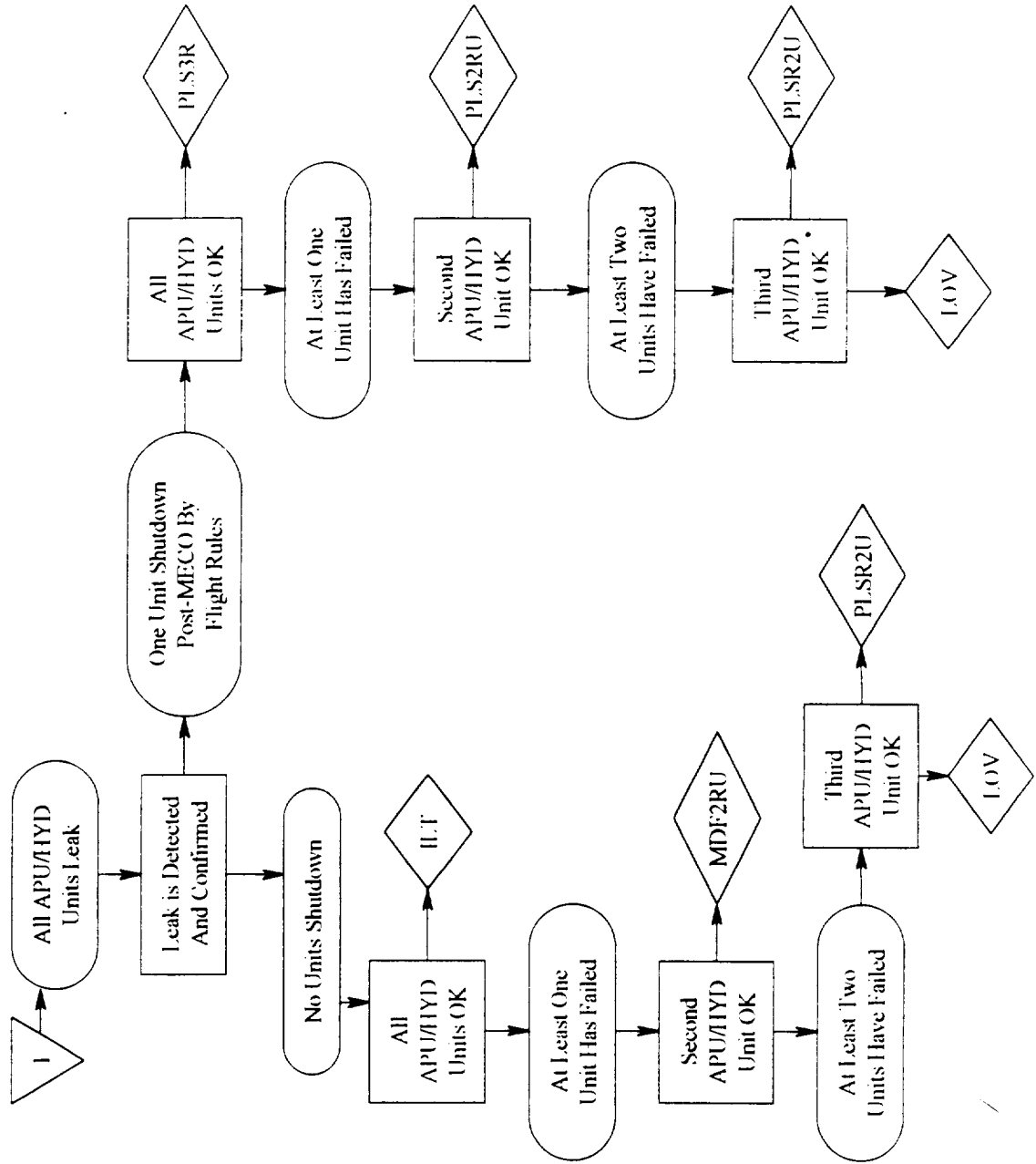
**Fault Tree For Sequence 6 LOV
State With PLSRU Initiating Event
During Reentry, TAEM and Landing**



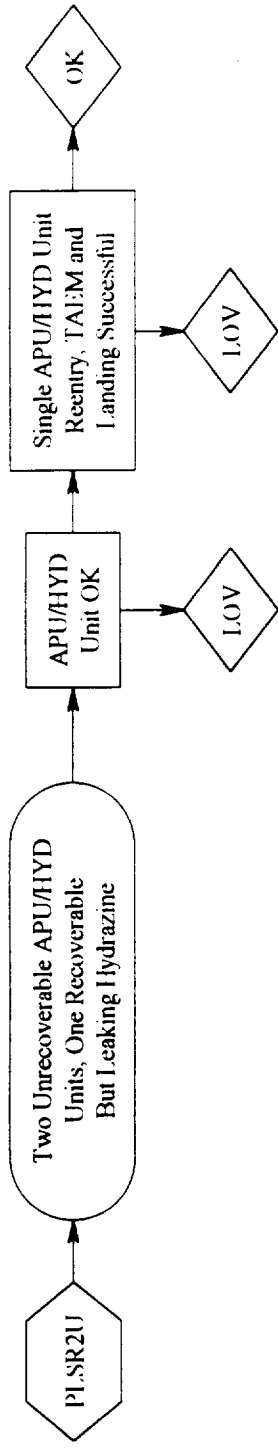
Event Sequence Diagram of APU/HYD Hydrazine Leaks During Ascent



Event Sequence Diagram of APU/HYD Hydrazine Leaks During Ascent (Continued)



**Event Sequence Diagram for
a PLSR2U State During Reentry,
TAEM and Landing**

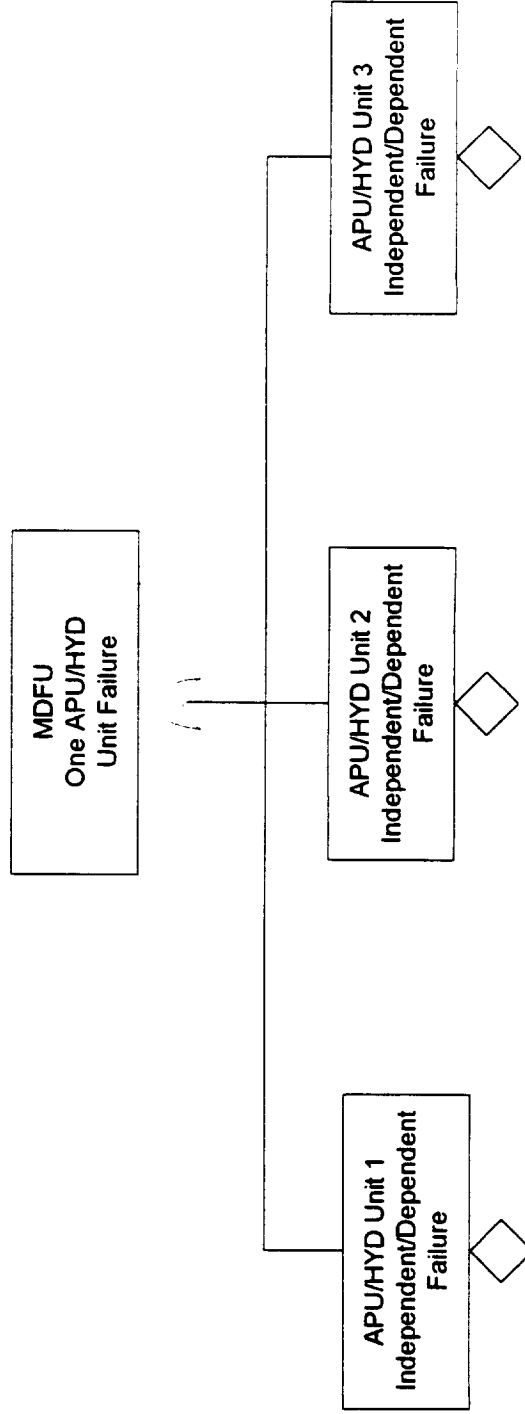


Assumption
Assuming remaining
APU/HYD unit restarted
before reentry.

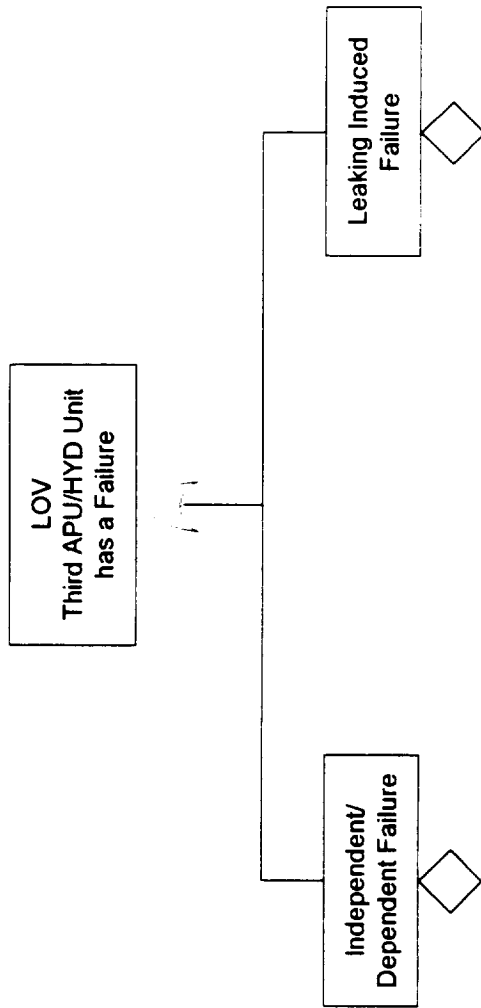
EVENT TREE OF A PLSR2U INITIATING EVENT DURING REENTRY, TAEM AND LANDING

2U	3F	UL	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
<p>The diagram is an event tree starting with a horizontal line labeled '2U'. A vertical line branches down to a horizontal line labeled '3F'. From '3F', a vertical line branches down to a horizontal line labeled 'UL'. From 'UL', a vertical line branches down to a horizontal line labeled '2U'. From '2U', a vertical line branches down to a horizontal line labeled '2UUL'. From '2UUL', a vertical line branches down to a horizontal line labeled '2U3F'.</p>			1	2U	OK
			2	2UUL	LOV
			3	2U3F	LOV

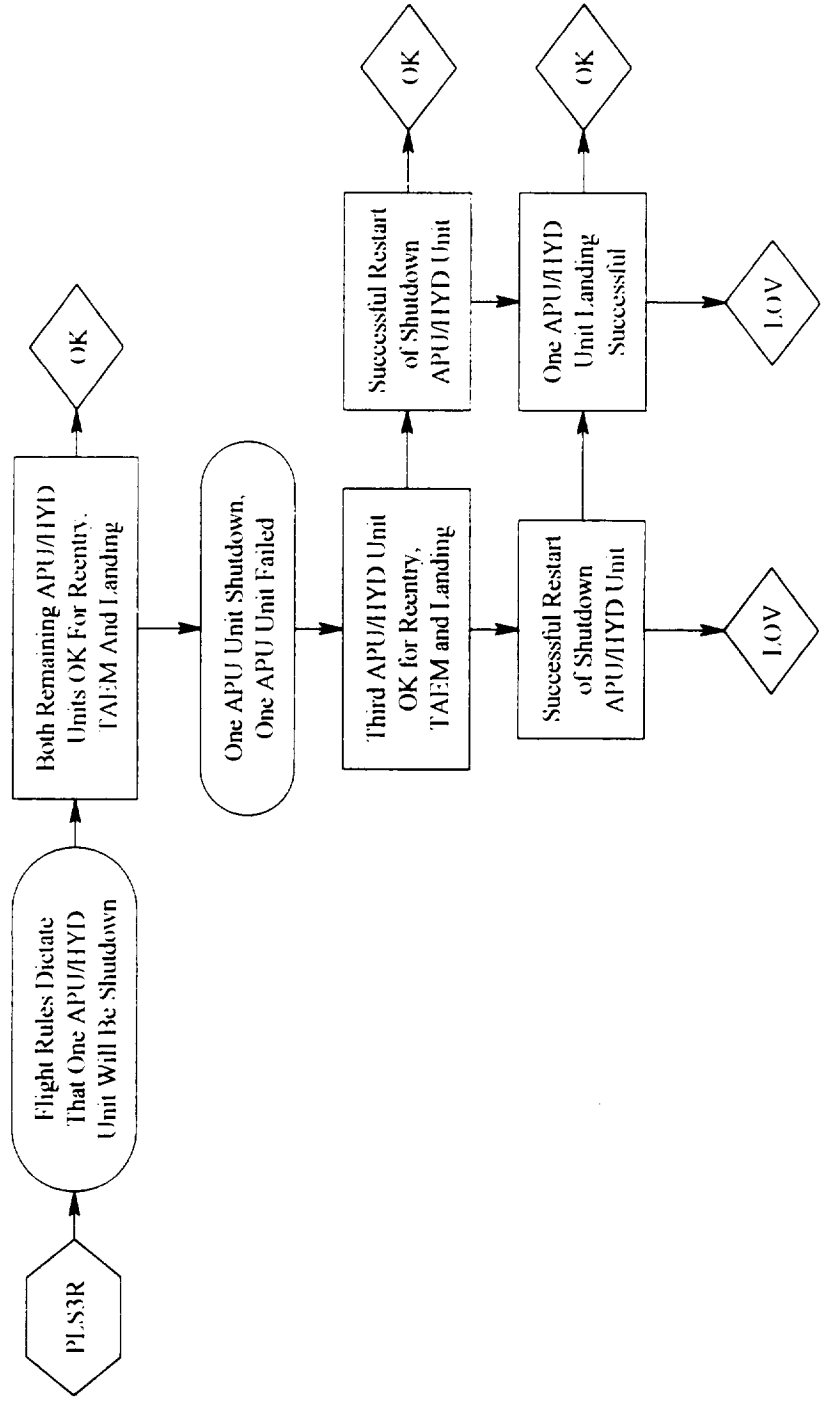
**Fault Tree For Sequence 2 MDFU
State From OK Start Without A
Hydrazine Leak During Ascent**



**Fault Tree For Sequence 3 LOV
State With PLSR2U Initiating Event
During Reentry, TAEM and Landing**



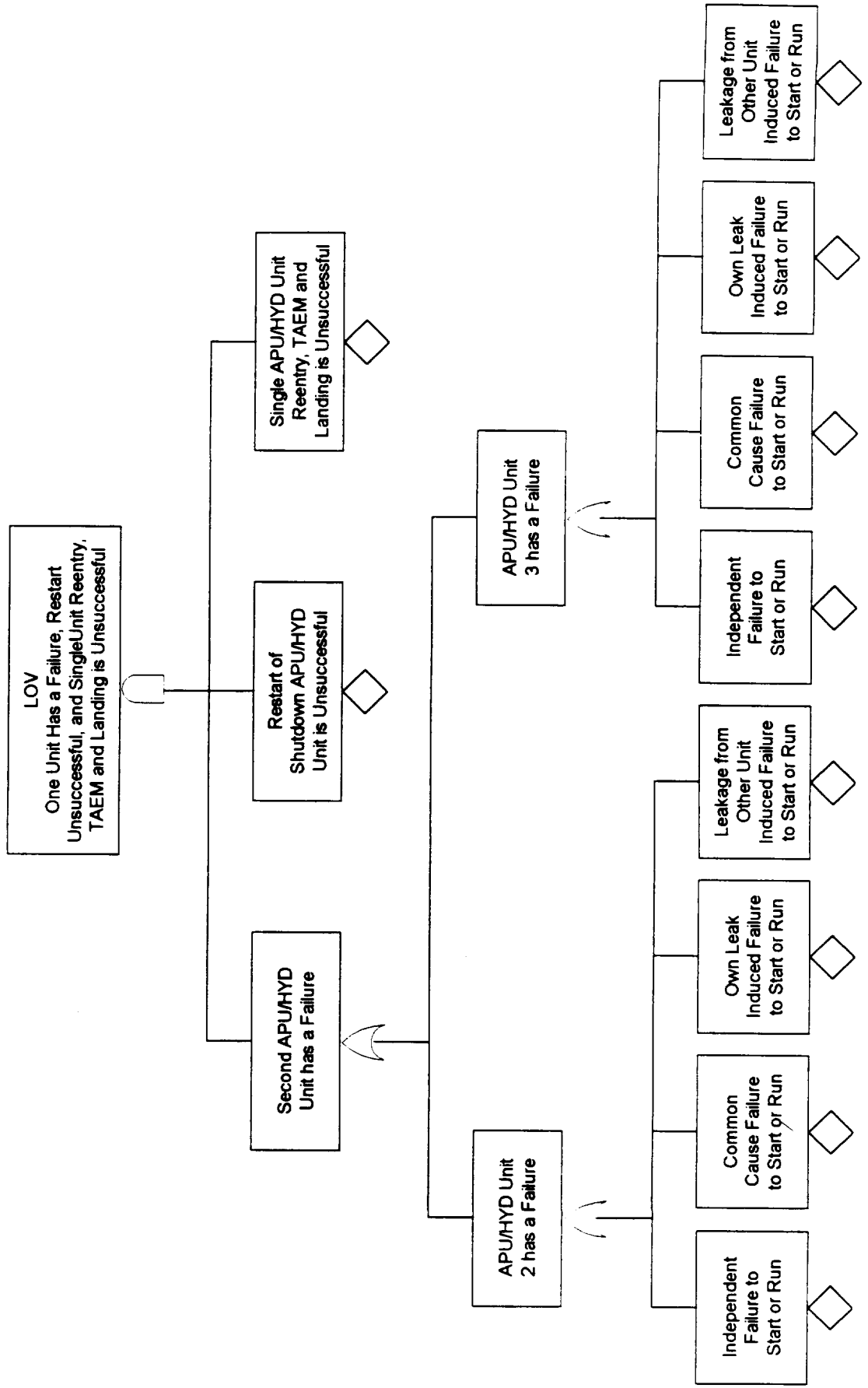
**Event Sequence Diagram of a PLS3R
State During Reentry, TAEM and Landing**



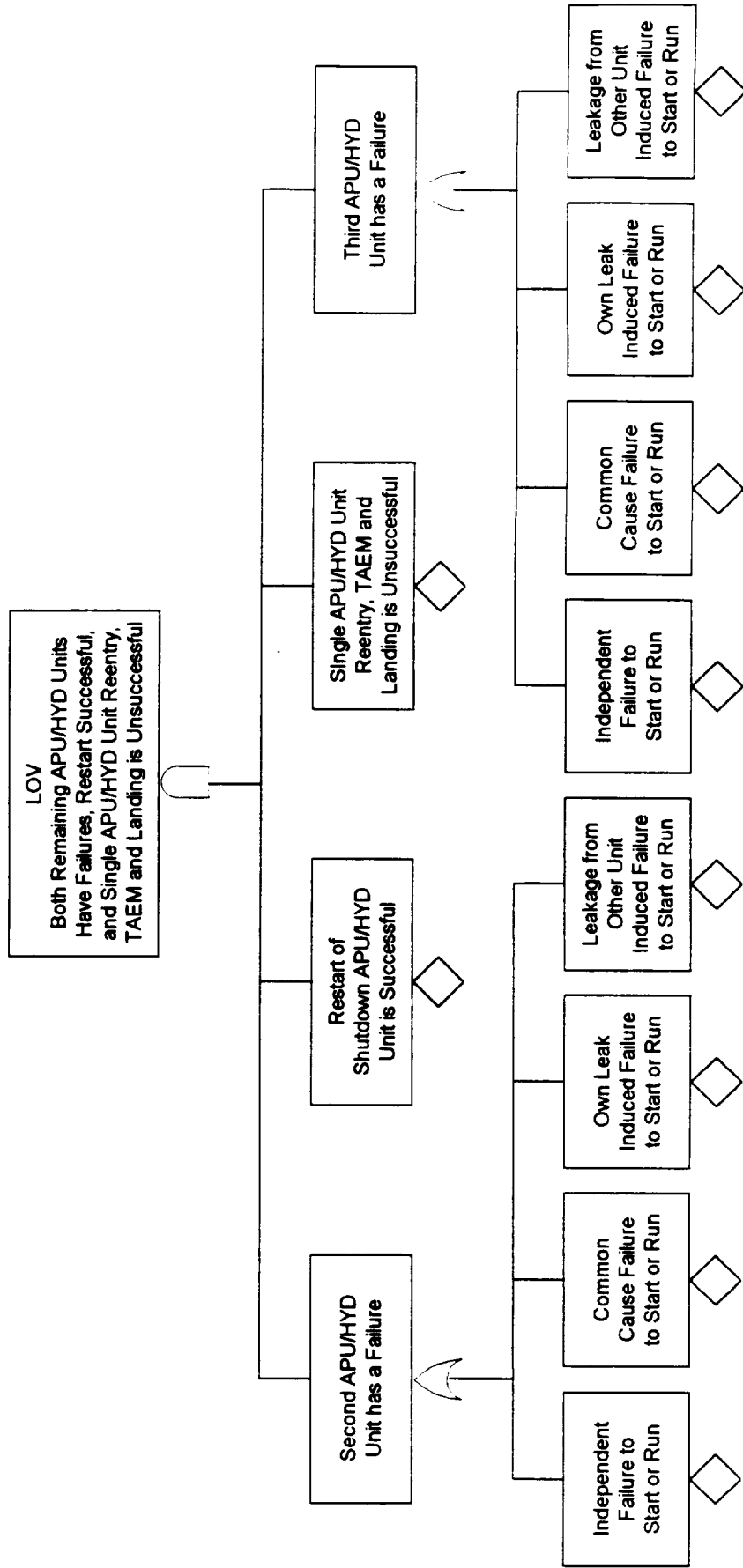
EVENT TREE OF A PLS3R INITIATING EVENT DURING REENTRY, TAEM AND LANDING

3L	2F	3F	UR	UL	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
					1	3L	OK
					2	3L2F	OK
					3	3L2FUR	OK
					4	3L2FURUL	LOV
					5	3L2F3F	OK
					6	3L2F3FUL	LOV
					7	3L2F3FUR	LOV

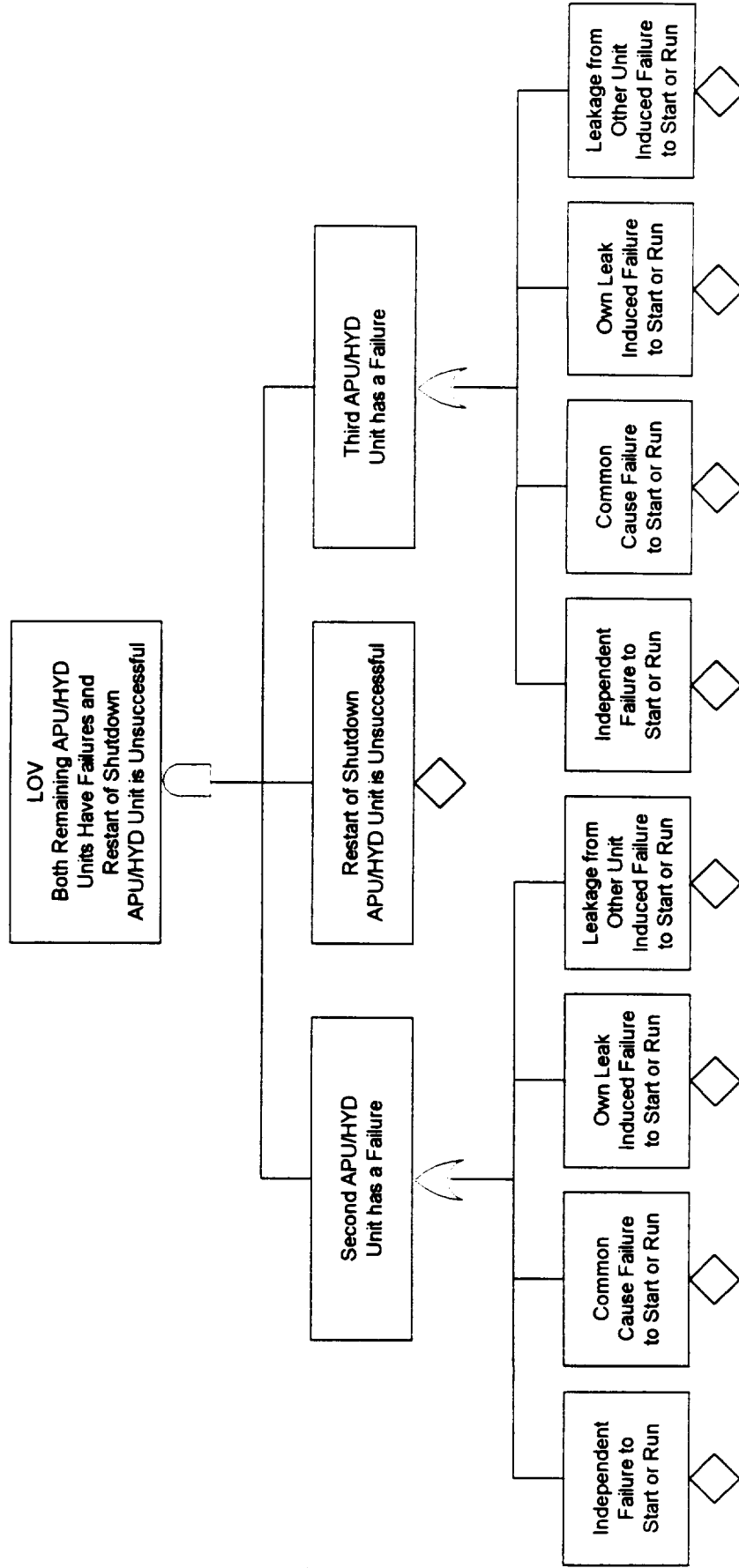
Fault Tree For Sequence 4 LOV State With A PLS3R Initiating Event During Reentry, TAEM and Landing



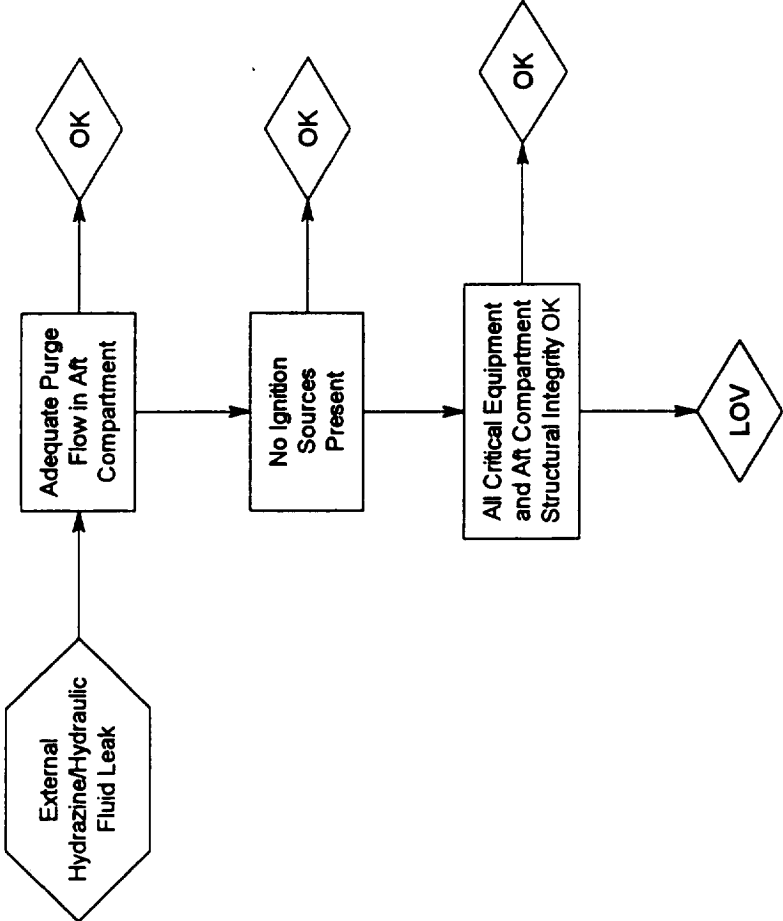
Fault Tree For Sequence 6 LOV State With A PLS3R Initiating Event During Reentry, TAEM and Landing



**Fault Tree For Sequence 7 LOV
State With A PLS3R Initiating Event
During Reentry, TAEM and Landing**



Event Sequence Diagram for an External Hydrazine or Hydraulic Fluid Leak



EVENT TREE OF AN EXTERNAL HYDRAZINE OR HYDRAULIC FLUID LEAK

EL	PF	IS	EI	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
				1	EL	OK
				2	ELPF	OK
				3	ELPFIS	OK
				4	ELPFISEI	LOV



B.4. Electrical Power System



**ORBITER ELECTRIC POWER SYSTEM:
EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.**

*See last page for key assumptions and risk classifications.

System failure	Failure sequence	Initiator or cause	Estimated sequence and state conditional probability/mission	Basis of screening conditional probability estimate	Risk class*	Comments
ELECTRIC POWER SYSTEM FUNCTIONAL FAILURE SEQUENCES:						
1. No or insufficient power to critical systems.	1.1.1. Shrapnel, jet impingement, or pipe whip causes either reactant manifold ruptures or multiple reactant system ruptures and suddenly depletes one or both reactants for 2 fuel cells.	1.1. Violent rupture of reactant tank, piping, or valve.	2E-06	1.1.1. [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-2 for severe consequential damage] = 1.7e-6/mission	Low	
Same	1.1.2. Shrapnel, jet impingement, or pipe whip disables 2 of 3 main distribution or mid power controller assemblies.	Same	2E-07	1.1.2 [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-3 for severe consequential damage] = 1.7e-7/mission	Very low	
Same	1.2. 2 out of 3 fuel cells fail suddenly and concurrently (complete outage or insufficient voltage).	1.2.1. Undetected pre-flight fuel cell processing error.	1E-07	1.2.1. [1e-2 for processing error]*[1e-3 for failure to detect before launch]*[1e-2 for failure progressing too fast for recovery or abort] = 1e-7/mission.	Very low	Low P(failure to detect) because FCs run under load and voltage is monitored for considerable period before launch.
Same	Same	1.2.2. Concurrent unrecoverable loss of ECLSS freon loops 1 and 2 (disables fuel cell cooling).	2E-06	2.1.2. See note 2.	Low	See note 2.
Same	1.3. Severe sustained overload fails one fuel cell; crew transfers load to another cell, which also fails on overload.	1.3. Severe sustained electrical overload.	1E-08	1.3. [1e-3 for severe sustained overload]*[1e-2 for crew transferring overload to second cell]*[1e-3 for failing to notice and correct in time] = 1e-8/mission.	Negligible	Low P(failure to detect overload) because overload this severe would cause symptoms obvious to crew.
Same	1.4. One (or both) fuel cell reactants is depleted before detection and isolation.	1.4.1. Severe spontaneous external leak or rupture of reactant manifold or associated valves, etc.	1E-08	1.4.1. [1e-6/hr for severe leak or rupture]* [168hrs for typical mission]* [1e-2 for failure to detect and isolate in time] = 1e-8/mission.	Negligible	
Same	Same	1.4.2. Relief valve on isolated reactant manifold section spontaneously fails closed, causing overpressure and undetected rupture; isolation valve is then opened.	8E-07	1.4.2. [2e-6/hr for relief valve failure]*[168hrs for typical mission]*[0.5 for leak or rupture on overpressure]*[1e-2 for failure to detect]*[0.5 for opening isolation valve] = 8e-7/mission.	Very low	

**ORBITER ELECTRIC POWER SYSTEM:
EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.**

*See last page for key assumptions and risk classifications.

System failure	Failure sequence	Initiator or cause	Estimated sequence end state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*	Comments
Same	Same	1.4.3. Multiple reactant tank relief valves fail open due to undetected pre-flight processing or pressure set-point error.	1E-05	1.4.3. [1e-3 for processing or set-point error]*[1e-2 for failure to detect before launch] = 1e-5/mission.	Moderate	
Same	Same	1.4.4. Severe sustained electrical overload depletes reactants before detection of overload or low reactant level.	1E-10	1.4.4. [1e-3 for severe overload]*[1e-4 for failure to detect overload before reactant depletion]*[1e-3 for failure to detect depletion in time] = 1e-10/mission	Negligible	Low P(failure to detect overload) because overload this severe would cause symptoms obvious to crew.
Same	1.5. 2 of 3 fuel cells or main busses turned off and not restored.	1.5. Crew error.	1E-09	1.5. [1e-5 for turning off FCs, main busses, or essential busses]*[1e-4 for failing to notice and correct] = 1e-9/mission.	Negligible	
Same	1.6. 2 of 3 dc distribution trains fail open.	1.6.1. Undetected, unrecoverable pre-flight processing error (e.g. failure to restore after testing, RPC setpoint error) in 2	1E-06	1.6.1. [1e-3 for unrecoverable processing error]*[1e-3 for failure to detect open before launch] = 1e-6/mission	Low	
Same	Same	1.6.2. Short circuit in one train propagates to second before interruption.	1E-11	1.6.2. [4e-4 for short circuit]*[1e-2 for vulnerable components of another train being close enough to allow propagation]*[5e-6 for failure to trip in time to prevent propagation] = 1e-11/mission	Negligible	See note 3 for basis of estimate of short circuit probability. P(failure to trip)=P(CB f.t. open on command)+P(prot. relay f.t. close)
Same	Same	1.6.3. Concurrent unrelated spontaneous failures of 2 trains.	6E-07	1.6.3. [8e-4 for failure of 1st train]*[8e-4 for failure of 2nd train] = 6e-7/mission.	Very low	Same basis of estimate as 1.5.2 except all failure modes considered.
2. No or insufficient ac power to critical systems.	2.1. 2 of 3 inverter sets fail suddenly (complete outage or unacceptable voltage, frequency, or waveform).	2.1.1. Undetected pre-flight processing error.	1E-06	2.1.1. [1e-2 for processing error]*[1e-4 for failure to detect before launch] = 1e-6/mission.	Low	

**ORBITER ELECTRIC POWER SYSTEM:
EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.**

*See last page for key assumptions and risk classifications.

System failure	Failure sequence	Initiator or cause	Estimated sequence end state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*	Comments
Same	Same	2.1.2. Concurrent unrecoverable loss of ECLSS H ₂ O cooling loops 1 and 2 disables inverter cooling.	2E-06	2.1.2. See note 2.	Low	See note 2.
Same	2.2. Mid-deck power components of 2 or 3 trains overheat and fail.	2.2. Concurrent unrecoverable loss of ECLSS freon cooling loops 1 and 2 disables mid-deck power component cooling.	2E-06	2.1.2. See note 2.	Low	See note 2.
Same	2.3. 2 of 3 inverters or ac busses turned off and not restored.	2.3. Crew error.	1E-09	2.3. [1e-5 for turning off inverters or busses][1e-4 for failing to notice and correct] = 1e-9/mission.	Negligible	
Same	2.4. Shrapnel, jet impingement, or pipe whip disables 2 or 3 trains of mid-deck power components.	2.4. Violent rupture of reactant tank, piping, or valve.	2E-07	2.4. [1e-6/hr for violent rupture][168hrs for typical mission][1e-3 for severe consequential damage] = 1.7e-7/mission	Very low	
Same	2.5. 2 of 3 ac distribution trains fail open.	2.5.1-2.5.3. Analogous to 1.6.1-1.6.3 above.	2E-07	2.5.1-2.5.3. 1.6e-7/mission.	Very low	Estimated by analogy to 1.6.1-1.6.3 above. Note: short circuit propagation is impossible because inverters lack necessary short circuit capacity.

ORBITER ELECTRIC POWER SYSTEM:

EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.

*See last page for key assumptions and risk classifications.

System failure	Failure sequence	Initiator or cause	Estimated sequence end state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*	Comments
SEQUENCES INITIATED BY ELECTRIC POWER SYSTEM						
3. Electrical fire damage to other systems.	3. Electrical short circuit or component overheating initiates uncontrolled fire that unrecoverably disables other critical system(s).	3.1. Undetected pre-flight processing error.	5E-12	3.1. [1e-2 for fire-initiating processing error][1e-2 for failure to detect before launch][1e-3 for failure to trip][1e-3 for presence of nearby combustibles when O2 is available][0.5 for ignition][0.1 for failure of fire suppression] = 5e-12/mission	Negligible	
Same	Same	3.2. Spontaneous component failure.	5E-11	3.2. [1e-3 for fire-initiating component failure][1e-3 for failure to trip][1e-3 for presence of nearby combustibles when O2 is available][0.5 for ignition][0.1 for failure of fire suppression] = 5e-11/mission	Negligible	
4. Crew is disabled by fire suppression system response to electrical fire.	4. Electrical short circuit or component overheating initiates Halon flood of crew compartment; Halon exposure disables crew.	4.1. Undetected pre-flight processing error.	1E-12	4.1. [1e-2 for fire-initiating processing error][1e-2 for failure to detect before launch][1e-3 for failure to trip][1e-3 for crew susceptibility to Halon][1e-2 for failure to don breathing apparatus in time] = 1e-12/mission	Negligible	
Same	Same	4.2. Spontaneous component failure.	1E-11	4.2. [1e-3 for fire-initiating component failure][1e-3 for failure to trip][1e-3 for crew susceptibility to Halon][1e-2 for failure to don breathing apparatus in time] = 1e-11/mission	Negligible	
5. Critical systems are disabled by fire suppression system response to electrical fire.	5. Electrical short circuit or component overheating initiates Halon flood of affected compartment; presence of Halon or its decomposition products damages critical components or disables equipment cooling.	5.1. Undetected pre-flight processing error.	1E-12	5.1. [1e-2 for fire-initiating processing error][1e-2 for failure to detect before launch][1e-3 for failure to trip][1e-3 for crew susceptibility to low Halon concentration][1e-2 for failure to don breathing apparatus in time] = 1e-12/mission	Negligible	

ORBITER ELECTRIC POWER SYSTEM: EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.						
*See last page for key assumptions and risk classifications.						
System failure	Failure sequence	Initiator or cause	Estimated sequence end state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*	Comments
Same	Same	5.2. Spontaneous component failure.	1E-11	5.2. [1e-3 for fire-initiating component failure]*[1e-3 for failure to trip]*[1e-3 for crew susceptibility to Halon]*[1e-2 for failure to don breathing apparatus in time] = 1e-11/mission	Negligible	
6. Orbiter structural failure.	6. Severe leak or rupture of fuel cell reactant tanks or associated piping and valves overpressurizes confined space leading to structural failure.	6. Rupture or severe external leak of tank, piping, or valve.	2E-06	6. [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-2 for severe consequential damage] = 1.7e-6/mission	Low	
7. Mechanical damage to other systems.	7. Shrapnel, jet impingement, or pipe whip unrecoverably disables other nearby critical system(s).	7. Rupture or severe external leak of tank, piping, or valve.	2E-06	7. [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-2 for severe consequential damage] = 1.7e-6/mission	Low	
Total end-state conditional probabilities of all sequences listed					3E-05	

NOTES:

1. Key assumptions: (1) probability estimates are based on IEEE Std 500-1984, IEEE Std 493-1990, and conservative (high) SAIC engineering estimates; (2) typical exposure is one-week (168-hour) mission time; (3) per PRA ground rules, only catastrophic failures leading to loss of vehicle (not abort) are considered; (4) loss of 2 of 3 power trains causes LoV.

2. Concurrent ECLSS freon loop failures: zero failures in 55 flights implies mean failure frequency is 3.03e-3 per flight per loop (using 1/3 failure approximation to zero). Assume 50% of failures are common cause/common mode. Double concurrent failure frequency is therefore 4.6e-6 per flight. Assuming 50% are recoverable, unrecoverable rate is 2.3e-6.

3. Estimate of probability of short circuit in distribution system: Assume each train comprises 6 equivalent circuit breakers, 1000 circuit feet of wire with 30 connections and splices, bare bars equivalent to 50 CB units. IEEE 493 App. A mean failure rates per unit/year: LV fixed CB=0.0035, LV cable=0.00141/1000ft, LV cable connection=0.000127, LV bus=0.00034 per equiv. CB unit. Assume 50% of failures are short circuits. P(short circuit)=0.50*[168hrs/mission]/(8766hrs/yr)*[6*0.0035+1*0.00141+30*0.000127+50*0.00034]=4e-4 per mission.

DEFINITIONS OF RISK CLASSES:	
Severe	P >= 1e-2
Very high	1e-3 <= P < 1e-2
High	1e-4 <= P < 1e-3
Moderate	1e-5 <= P < 1e-4
Low	1e-6 <= P < 1e-5
Very low	1e-7 <= P < 1e-6
Negligible	P < 1e-7