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Aircraft Emission Inventories Projected in Year 2015 for a High Speed Civil Transport (HSCT) Universal Airline Network

Steven L. Baughcum and Stephen C. Henderson

Contract NAS1-19360 Prepared for Langley Research Center

July 1995

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Aircraft Emission Inventories Projected in Year 2015 for a High Speed Civil Transport (HSCT) Universal Airline Network

Steven L. Baughcum and Stephen C. Henderson Boeing Commercial Airplane Group • Seattle, Washington

National Aeronautics and Space Administration Langley Research Center • Hampton, Virginia 23681-0001 Prepared for Langley Research Center under Contract NAS1-19360

July 1995

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Executive Summary

This report describes the development of a database of aircraft fuel burned and emissions from projected fleets of high speed civil transports (HSCTs) on a universal airline network. Inventories for 500 and 1000 HSCT fleets were calculated. Inventories of Year 2015 subsonic aircraft fleets in service with these HSCT fleets were also calculated. These emissions inventories were developed under the NASA High Speed Research Systems Studies (HSRSS) contract NAS1-19360, Task Assignment 40.

The objective of this work was to evaluate the changes in geographical distribution of the HSCT emissions as the fleet size grew from 500 to 1000 HSCTs. For this work, a new expanded HSCT network has been used and flights projected using a market penetration analysis rather than assuming equal penetration (as was assumed for the emission scenarios developed for the 1993 AESA assessment). Emission inventories on this network were calculated for both Mach 2.0 and Mach 2.4 HSCT fleets with NOx cruise emission indices of approximately 5 and 15 grams NOx/kilogram fuel.

These emissions inventories will be available for use by atmospheric scientists conducting the Atmospheric Effects of Stratospheric Aircraft (AESA) modeling studies. Fuel burned and emissions of nitrogen oxides (NOx as NO₂), carbon monoxide, and hydrocarbons have been calculated on a 1 degree latitude x 1 degree longitude x 1 kilometer altitude grid and delivered to NASA as electronic files. This report describes the assumptions and methodology for the calculations and summarizes the results of these calculations.

The work presented here shows that the total global fuel burned and emissions from a fleet of 500 HSCTs is not very different whether the expanded HSCT network or the 1993 AESA assessment network is used. The geographical distribution of emissions at stratospheric cruise is sensitive to the market penetration assumptions used to distribute projected HSCT passenger demand.

An increase in HSCT fleet size from 500 to 1000 units has been shown to approximately double emissions at stratospheric cruise. However, as the fleet grows, emissions in different geographical regions grow at different rates. Consequently, stratospheric emissions in northern mid-latitudes are not projected to double as the fleet size doubles, while emissions in the northern tropics and southern hemisphere mid-latitudes are expected to more than double.

For an HSCT combustor with a NOx emission index of 5, the analyses show that the total NOx emissions below 13 kilometers altitude are not very sensitive to the presence or absence of an HSCT fleet. This suggests that to first-order the assessment of the effects of an HSCT fleet are largely decoupled from the assessment of subsonic aircraft effects.

During this work, we discovered several errors made in our previous study (NASA CR 4592) and present the corrected data in this report. For the HSCT, it was found that the operating empty weight used in the emission scenario calculation had been incorrectly entered into the analysis data file and was not consistent with the performance data for the baseline model used in the study. This was corrected and revised emission inventories for Mach 2.0 and Mach 2.4 HSCTs on the 1993 AESA assessment network were calculated. delivered to NASA Langley, and described in this report. The fuel burned for the revised Mach 2.4 HSCT scenario on the 1993 AESA assessment network increased by 7% and the cruise altitude decreased by about 1100 feet when compared with the results presented earlier in NASA CR 4592. In addition, the fuel performance improvement factor for the very large aircraft (P900) projected for 2015 was incorrectly implemented. This was corrected and revised 2015 subsonic aircraft emission scenarios are described in this report. This correction increased the total projected fuel burned by a future all subsonic fleet by 2 %, well below the uncertainty in projected future emissions.

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GLOSSARY

AEAP AESA	Atmospheric Effects of Aviation Project Atmospheric Effects of Stratospheric Aircraft
APU	Auxiliary power unit
ASM	Available seat mile (the number of seats an airline provides
	times the number of miles they are flown)
ATC	Air traffic control
ATM	Available ton-miles (the number of tons capable of being carried times the number of miles flown)
BCAG	Boeing Commercial Airplane Group
BMAP	Boeing Mission Analysis Process
CO	Carbon Monoxide
CO2	Carbon Dioxide
EI(ĈO)	Emission Index (grams CO/kg fuel burn)
EI(HC)	Emission Index [grams hydrocarbon (as CH4)/kg fuel burn]
EI(NOx)	Emission Index (grams NOx (as NO ₂)/kg fuel burn)
FAA	Federal Aviation Administration
GAEC	Global Atmospheric Emissions Code
GCD	Great circle distance
GE	General Electric
	gram
gm HC	Unburned hydrocarbon
H ₂ O	Water
HSCT	High Speed Civil Transport
HSRP	High Speed Research Program (NASA)
ICAO	International Civil Aviation Organization
ISA	International standard atmosphere
kg	kilogram
lb Lood Foster	pound Demonstrate of an aimlana's cost consulty cooupled by
Load Factor	Percentage of an airplane's seat capacity occupied by
	passengers on a given flight
LTO cycle	Landing takeoff cycle Mach number
M	
MDC	McDonnell Douglas Corporation Maximum takeoff weight
MTOW	\mathbf{v}
NASA	National Aeronautics and Space Administration Nautical mile
nm Nov	Oxides of nitrogen (NO + NO ₂) in units of gram equivalent
NOx	
	NO2
OAG	Official Airline Guide
OEW	Operating Empty Weight
P&W	Pratt & Whitney
PAX	passengers
RAM	Revenue air mile
RPM	Revenue passenger miles (the number of paying
	passengers times the number of miles they fly)

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RTM	Revenue ton-miles (number of tons carried times the number of miles flown)
SO2	Sulfur dioxide
TBE	Turbine bypass engine
TOGW	Takeoff gross weight
ton	2000 pounds
3D	Three dimensional

1. Introduction

A major goal of the NASA High Speed Research Program (HSRP) and of the Boeing High Speed Civil Transport (HSCT) program is to design an HSCT that will not cause a significant impact on the stratospheric ozone layer. To help achieve that goal, NASA has funded the Atmospheric Effects of Stratospheric Aircraft (AESA) project to assess the effect of a fleet of commercial supersonic transports on the atmosphere. To support that assessment, Boeing was contracted to calculate three-dimensional inventories of emissions from fleets of HSCTs. Scenarios of projected subsonic air traffic, both with and without HSCT fleets, were also calculated for use in the atmospheric assessment. Both HSCT and subsonic fleets were projected for the year 2015.

Earlier projections of HSCT emission inventories used in the 1993 AESA assessment were based on an average of Boeing and McDonnell Douglas forecasts to project future passenger demand. (Baughcum, *et. al.*, 1994; Wuebbles, *et. al.*, 1993; Landau, *et. al.*, 1994) Simple ground rules were defined to identify the accessible HSCT market and to create projected departure schedules. Market penetration (the proportion of the passenger demand captured by the HSCT) was assumed to be equal for all HSCT city pairs. Emission scenarios were calculated for Mach 2.0 and Mach 2.4 HSCT fleets by Boeing (Baughcum, *et. al.*, 1994) and for Mach 1.6 by McDonnell Douglas. (Landau, *et. al.*, 1994)

Two-dimensional modeling calculations have shown that the HSCT impact on the ozone layer depends on both the amount of NOx emissions injected into the stratosphere and on the HSCT flight altitudes. (Albritton, *et. al.*, 1993; Stolarski and Wesoky, 1993). More recent calculations have shown that the calculated impact depends on the geographical location as well. (Considine, *et. al.*, 1995) Their model predicts that flights in the tropics will have a much larger impact than flights at mid-latitudes. Thus, in developing emission scenarios, it is important that we realistically project the geographical location of future flights, as well as the total quantity of emissions. It is also important that we understand how sensitive these geographical distributions of emissions are to our assumptions about the HSCT market.

The work presented herein is an extension of the earlier Boeing work (Baughcum, *et. al.*, 1994) of scheduled air traffic emissions. For this study, the Boeing baseline forecast (Boeing, 1993) of passenger demand has been projected to year 2015. A new HSCT route system and schedule have been developed with HSCT passenger demand calculated via a market penetration analysis, rather than assuming that penetrations of all markets will be equal. The flights were then scheduled assuming a single universal airline. As with the previous study, it was assumed that the HSCT would fly supersonically only over water. The work presented here is for fleets of approximately 500 and 1000 HSCTs in active flight operations. (The total number manufactured would be higher to account for maintenance, inspections, etc.)

Future fleets of HSCTs must be able to compete economically with subsonic aircraft; so,the HSCT will be utilized on routes which can take advantage of its speed. Since it is anticipated that the HSCT will only fly supersonically over water, this means that some routes will be more attractive than others. In this study, the HSCT market capture for flights between individual cities is calculated explicitly taking into account the time saved by supersonic flights. It is believed that this will give a more realistic geographical distribution of future HSCT emissions than was obtained with the scenarios calculated for the 1993 AESA assessment, which assumed equal market penetration for all city pairs which satisfied certain simple ground rules.

In order to evaluate how growth of an HSCT fleet would alter the geographical distribution of HSCT emissions used in the AESA assessments, schedules corresponding to the passenger demands of approximately 500 and 1000 active HSCTs were created. The emission inventories developed from these schedules can then be used to evaluate how parametric changes in fleet size affect the HSCT impact on the stratospheric ozone layer.

Fuel consumption and emissions of nitrogen oxides (NOx), carbon monoxide (CO), and hydrocarbons (HC) were calculated for all flight segments and are reported on a three-dimensional grid with a resolution of 1 degree latitude x 1 degree longitude x 1 km altitude. Given the fuel burned in each grid cell, emissions of water vapor, carbon dioxide, and sulfur dioxide can be determined from the fuel properties. The following scenarios were calculated:

- Projected 2015 HSCT traffic for 500 and 1000 Mach 2.4 HSCTs with nominal NOx emission indices of 5 and 15 gm NOx/kg fuel burned at cruise.
- Projected 2015 HSCT traffic for Mach 2.0 HSCTs with nominal NO_X emission indices of 5 and 15 gm NO_X/kg fuel burned at cruise (passenger demand corresponding to 500 and 1000 Mach 2.4 HSCTs).
- Projected 2015 scheduled subsonic aircraft (assuming no HSCT fleet exists).
- Projected 2015 scheduled subsonic aircraft (assuming an HSCT fleet with passenger demand corresponding to 500 Mach 2.4 HSCTs was flying).
- Projected 2015 scheduled subsonic aircraft (assuming an HSCT fleet with passenger demand corresponding to 1000 Mach 2.4 HSCTs was flying).

The fuel burned and emission characteristics of the HSCT and future subsonic aircraft were based on estimated performance. The HSCT performance and emissions were the best estimate available at the beginning of this study and were "frozen" in order to develop new emission scenarios in time for the 1995 AESA assessment. Since then, preliminary design work has continued on both the airframe and the engine. The final design of the HSCT will likely have some characteristics different from those assumed for this study; hopefully, it will be more fuel efficient. The HSCT emission projections are based on the HSRP program goal and the estimates of the engine companies and are treated parametrically in this study and in the AESA assessment. As combustor rig test data becomes available, it will be possible to better refine these projections.

The details of the emission calculation process are described in NASA CR-4592 (Baughcum, *et. al.*, 1994) and will only be summarized in this report. The results obtained in this study are compared with the emission scenarios calculated for the 1993 AESA assessment (Baughcum, *et. al.*, 1994). The effects of fleet growth on the geographical distribution of HSCT emissions are analyzed and discussed.

During this work, we discovered several errors made in our previous study and present the corrected data in this report. For the HSCT, it was found that the operating empty weight used in the emission scenario calculation had been incorrectly entered into the analysis data file and was not consistent with the performance data for the baseline model used in the study. This was corrected and revised emission inventories for Mach 2.0 and Mach 2.4 HSCTs on the 1993 AESA assessment network were calculated, delivered to NASA Langley, and described in this report. In addition, the fuel performance improvement factor for the very large aircraft (P900) projected for 2015 was incorrectly implemented. This was corrected and revised 2015 subsonic aircraft emission scenarios are described in this report.

The work on HSCT and Year 2015 emission scenarios described in this report was conducted under NASA Langley Contract NAS1-19360, Task 40. The NASA Langley Task Manager was Donald L. Maiden.

Within the Boeing HSCT engineering group, overall program management was provided by Thomas Derbyshire, John D. Vachal, and John H. Gerstle. The principal investigator of the task was Steven L. Baughcum. Chief contributors were Stephen C. Henderson, Terry Higman, Thomas T. Odell, and Richard Bateman in market analysis; Peter S. Hertel in computer support; and Debra R. Maggiora in data analysis.

2.0 New Expanded HSCT Network

2.1 Total Passenger Demand Forecast for 2015

The total passenger demand forecast for the year 2015 was created by escalating 1991 reported regional flow passenger demand data using the annual growth rates developed by Boeing and published in the 1993 Current Market Outlook (Boeing, 1993). This yearly publication shows the Boeing Commercial Airplane Group's traffic and airplane demand forecasts. The results of this forecast, including regional flow growth rates and passenger demand (revenue passenger miles or RPMs), are summarized in Table 2-1 below. A more detailed table of the passenger demand for each of the forecast regions is shown on Appendix A, with the interim years of 1995, 2000, 2005 and 2010 also shown, along with the interim year-to-year growth rates.

	Average Annual					
Regional Flow	1991 RPMs (millions)	Growth Rate 1991- 2015	2015 RPMs (millions)			
Intra & Domestic N. America	358,741	4.019/	001 565			
N. America-Europe	121,400	4.01% 4.78%	921,565			
N. America-Asia/Pacific	87,065	4.78% 7.03%	372,129			
Other N. America	3,565	4.08%	445,013			
N. America-Latin America	36,476	4.08% 5.20%	9,306			
Intra & Domestic Europe	148,216	4.62%	123,092			
Europe-Asia/Pacific	46,430	4.02 <i>%</i> 8.05%	437,999			
Europe-Indian Sub Continent	9,718	3.54%	297,690			
Europe-Mid East	19,578	5.07%	22,376			
Europe-Africa	25,811		64,163 72,950			
Europe-Latin America	26,869	4.48%	73,850			
Intra & Domestic Asia/Pacific		5.34%	93,627			
Misc. Long Range	86,003	7.92%	535,482			
Japan	40,348	5.70%	152,698			
Intra & Dom Indian Sub Continent	33,773	4.16%	89,918			
	6,779	5.81%	26,316			
Other Indian Subcontinent	14,261	4.75%	43,461			
Intra & Domestic Mid East/Africa	18,455	5.01%	59,695			
Other African	8,002	5.38%	28,163			
Intra & Domestic Latin America	27,023	5.26%	92,463			
CIS International	13,842	3.70%	33,098			
MAC Charter	5,657	-2.36%	3,191			
Total	1,138,012	5.29%	3,925,296			

Table 2-1. World Traffic Forecast

2.2 HSCT Universal Route System

The "Universal" HSCT route system is meant to simulate the operation of HSCTs as a mature fleet in a global airline network. The "Universal" system can be considered the sum of several global airlines, although it it scheduled as if it is a single airline. This approach can be justified by making the assumption that in the future, airline alliances and code-sharing will be more extensive than today (particularly among international airlines).

A "Universal" HSCT route system was originally developed as part of the 1993 AESA HSCT assessment (Baughcum, *et. al.*, 1994). The route system used in this study is based on the original system, but has been enlarged and refined to add many more city-pairs and to provide more efficient land-avoiding flight tracks. Gateway cities were established in the countries of each of the regions included in the regional traffic flow forecasts and assumed to be the focus of HSCT flights in year 2015. Thus HSCT flights from Britain are assumed to operate from London, flights from France operate from Paris, etc. Some countries were given more than one gateway city, due to the size of the market and/or the size of the country. (For example, the United States has 18 gateways, Japan 2 gateways, Australia and Germany 3 gateways each)

A list of the assumed gateway cities for HSCT operations is shown in Appendix B.

The total year 2015 world passenger demand (measured as passengers) was distributed among the gateway city-pairs in each region by using the share of the total passenger available seat miles (ASM) that each city pair included in the regional flows generated in 1993 (as derived from the Official Airline Guide schedules). For each city-pair in each region, total passenger demand in 2015 was forecast as follows:

Passenger Demand _{CITY-PAIR, 2015} =

(RPM REGIONAL FLOW, 2015 X (ASM_{CITY-PAIR}/ASM_{REGION})₁₉₉₃)/Distance _{CITY-PAIR}

2.3 HSCT Passenger Traffic Demand - Market Penetration

Due to the operating characteristics of the HSCT (sonic boom restrictions and high operating costs, particularly on short routes), only a certain subset of the total regional passenger demands are candidates for HSCT service. (U.S. Domestic, Intra Europe, and the domestic demand of other regions are excluded, for example). The suitability of the HSCT for the remaining passenger demand must be determined according to some logical assessment criteria.

In the previous 1993 AESA HSCT emission database study (Baughcum, *et. al.*, 1994), routes for HSCT service were selected according to a set of "static" criteria mutually agreed upon between Boeing and McDonnell Douglas. Routes were selected using the following ground rules:

- No supersonic flight over land
- Flight distance must be greater than 2000 nautical miles
- No more than 50% over land routing
- No more than 20% diversion from great circle routing
- Passenger demand must be sufficient to support at least one flight/day at 70% load factor

Once the routes that satisfied these criteria were selected, equal market penetration of the HSCT was assumed on all markets. The penetration level was adjusted to produce the 500 Mach 2.4 airplane fleet size used in that study.

One of the goals of the current fleet growth study is to determine how an increasing fleet of HSCT's would change the global distribution of emissions. Therefore, this study does <u>not</u> use a "static" set of criteria for determining the proportion of city-pair demand likely to be captured by the HSCT. Instead, demand captured by the HSCT is assumed to depend <u>only</u> on travel time saved and the fare differential over a subsonic airplane serving the same city-pair. (The travel time saved is in turn determined by the routing required to minimize flight over land, see Section 2.4.) HSCT demand capture in this study was determined by a proprietary market penetration model developed within Boeing. The proportion of each city-pair market captured by the HSCT was found by:

$P = f(R,T,F,Z,L_{min})$

where

P = percent of total passenger demand carried by the HSCT,

R = range of the HSCT,

T = Trip time saved versus a subsonic airplane,

F = Fare premium over the subsonic airplane,

Z = stop factor (whether the HSCT flight is non-stop or not), and $L_{min} =$ the minimum load factor allowed on a flight.

The only explicit constraint operating in the penetration model is the prohibition of supersonic flight over land.

As the amount of time saved increased or the fare premium decreased, or the number of stops decreased, the proportion of the passenger demand carried by the HSCT increased. If the application of the penetration model lowered the HSCT passenger demand on a city-pair to less than 180 passengers per day, that city-pair was dropped from the HSCT system. The fare premium parameter (F) of the model was first adjusted so that the passenger demand carried by the HSCT in 2015 required approximately 500 Mach 2.4 airplanes, forming the baseline case for the calculation of HSCT emissions distribution. The fare premium parameter was then reduced so that the increased passenger demand required approximately 1000 Mach 2.4 airplanes, creating the alternate case. The average load factor was 65%.

The higher demand carried by the 1000 airplane fleet came from both an increased penetration on the same markets served by the 500 airplane fleet and an increase in the number of city-pairs served. The city-pairs, number of departures and other system data are listed in Appendix C for the 500 and 1000 unit HSCT fleets. The route system maps for fleets of 500 and 1000 HSCTs are shown in Figures 2-1 and 2-2, respectively. The routes added as the fleet grew from 500 to 1000 are shown in Figure 2-3.

Emission inventories of HSCT airplanes designed with cruise speeds of Mach 2.0 using the same route systems defined by the Mach 2.4 airplanes were also calculated. Passenger demand levels and route systems which required nominally 500 (actually 499) and nominally 1000 (actually 991) Mach 2.4 airplanes required 528 and 1062 Mach 2.0 airplanes, respectively.

1994 EMISSIONS ROUTE SYSTEM 500 AIRPLANE HSCT FLEET

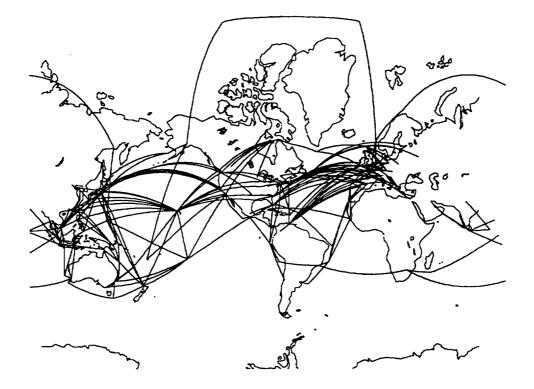


Figure 2-1. Universal Network Route System, 500 HSCT fleet

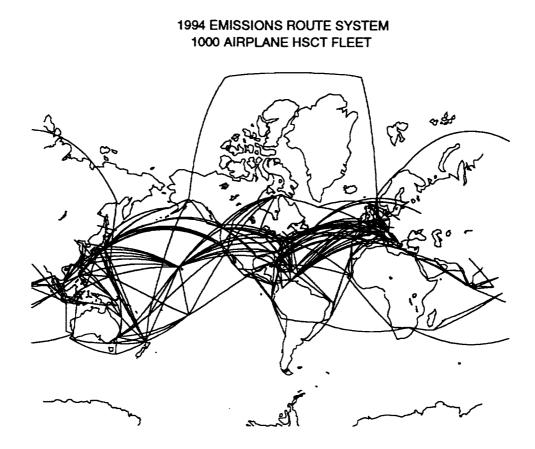


Figure 2-2. Universal Network Route System, 1000 HSCT fleet

1994 EMISSIONS ROUTE SYSTEM ROUTES ADDED BY INCREASING FLEET TO 1000

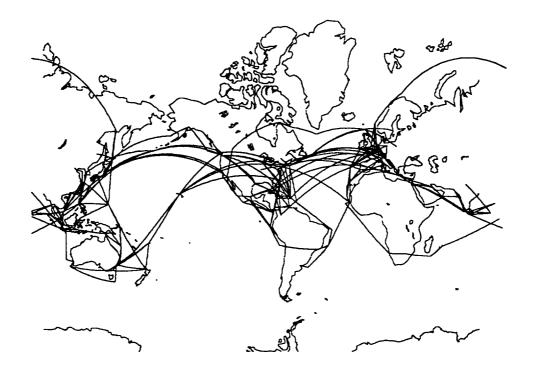


Figure 2-3. Universal Network Route System, New Routes added when increasing fleet to 1000 HSCTs.

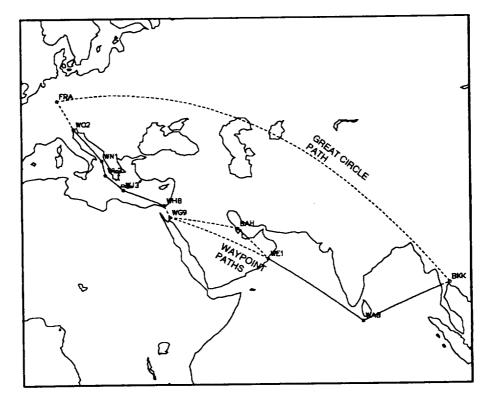
2.4 HSCT Flight Paths - Waypoint Routing

As was noted previously, the amount of trip time saved by the HSCT versus a subsonic airplane serving the same city-pair is one of the determinants of HSCT market penetration. Since it is assumed that the HSCT must fly at subsonic speeds over land masses, each potential HSCT city-pair route was examined to find the reasonable routing which minimized (or at least reduced) the percentage of the flight spent over land. The flight routing was accomplished by establishing "waypoints", a set of specific latitude-longitude positions which defined the HSCT flight path. (The HSCT flight path between waypoints was flown as a great circle.)

As an example, consider HSCT flights from Frankfurt (FRA) to Bangkok (BKK) (See Figure 2-4). The shortest (great circle) flight path is 4841 nautical miles, all over land and therefore flown subsonically. The flight path between BKK and FRA can be altered by requiring the HSCT to fly between "waypoints". established at defined latitude-longitude positions designed to minimize the amount of overland flight. As shown in Figure 2-4, waypoints can be used to route the HSCT subsonically from Frankfurt to near Venice, then supersonically down the Adriatic, across the Mediterranean to the Sinai, subsonically across the Arabian peninsula, then supersonically again around India to Bangkok. This new path reduces the amount of flight overland to only 1993 nautical miles. but increases the total flight path to 6130 nautical miles, a distance greater than the 5000 nautical design range of the study airplane. Flying this path requires a stop at Bahrain (BAH) to refuel (and pick up passengers). After the Bahrain stop, the HSCT resumes the flight as defined above. The new path (with a stop) adds 28% to total miles flown, but reduces the subsonic flight portion of the path by 62%. (See Table 2-2)

Route Segment	Great Circle Distance (nmi)	Flight Path Distance (nmi)	Supersonic Distance (nmi)	Subsonic Distance (nmi)
Frankfurt - Bangkok (Great Circle Path)	4,841	4,841	0	4,841
Frankfurt - Bangkok (Direct, HSCT Waypoints)	4,841	6,130	4,137	1,993
Frankfurt - Bahrain - Bangkok (Stop at Bahrain, HSCT W	5,292 /aypoints)	6,181	4,319	1,862
Percent Change in Flight I from direct Great Circle	Path	28%		-62%

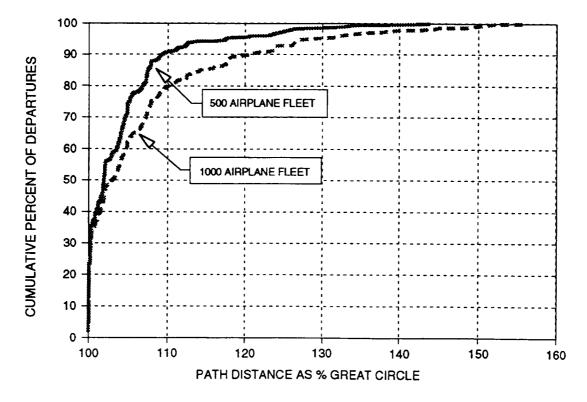
Та	ble	e	2-2	. Examp	le of	i wav	<i>r</i> point	routina	-	Frankfurt	to	Bangkok



FRANKFURT - BANGKOK HSCT FLIGHT PATHS EXAMPLE OF WAYPOINT ROUTING

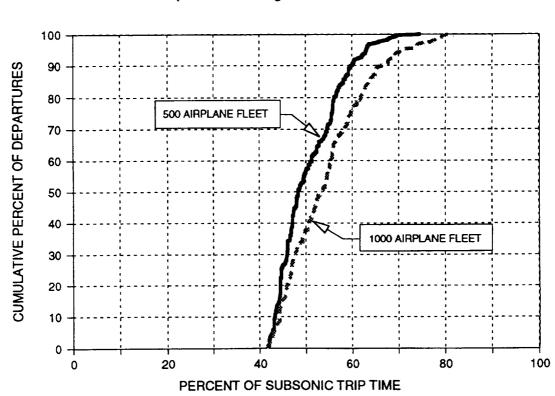
Figure 2-4. Example of Waypoint Routing

The above example shows a somewhat extreme change in flight path. Using the new waypoint routing and the market penetration model, the HSCT route system used in this study is very efficient - adding only about 5% to total route miles flown. 90% of HSCT trips are penalized less than 10% in flight path distance over the minimum Great Circle distance (Figure 2-5). 90% of HSCT trips also operate at 60% or less of subsonic block time (Block time is the total time for the flight including roll back, taxi-out, flying, and taxi-in. Subsonic block time is the block time that a subsonic aircraft would require.) Almost 60% of HSCT trips operate at less than half of subsonic block time (These statistics for for the 500 airplane fleet) (Figure 2-6). The 1000 airplane fleet, with its greater market penetration, includes more routes which are less desirable from an HSCT efficiency standpoint - lowering the overall waypoint routing efficiency and fleet time savings by a small amount. Waypoints and their positions for all HSCT routes flown are compiled as part of the flight path listing in Appendix D.



Waypoint Routing Efficiency

Figure 2-5 Waypoint Routing Efficiency



Trip Time Savings - HSCT Fleets

Figure 2-6 Trip Time Savings - HSCT Fleets

2.5 HSCT Scheduling

A description of the method of scheduling the HSCT fleet is provided in Appendix E. The resulting utilization statistics are summarized below. The nonlinear nature of both the penetration model and the scheduling model made it difficult to exactly achieve the goal of 500 and 1000 airplane HSCT fleets. The fleet size was adjusted by varying the fare premium in the penetration model so that the nominal "500" unit Mach 2.4 fleet was actually 499 units and the nominal "1000" unit fleet was actually 991 units. These were felt to be close enough to the target fleet sizes for these parametric studies and additional iterations were not performed.

	Mach 2.4		Mach 2.0	
Units	499	991	528	1062
Average Stage Length - n.m.	3555	3026	3555	3020
Average Daily Use (hours)	21.95	22.24	21.87	22.17
Average Hours/Segment	3.67	3.30	4.07	3.62
Average Hours/Trip	4.26	3.78	4.71	4.13
Average Block Hours/Day	16.00	16.10	16.75	16.49
Percent of Subsonic Trip Time	49.97	53.25	55.21	58.28
Network Flight Path % of GCD	103.98	106.16	103.98	106.16
% of Trip in Supersonic Cruise	75.16	71.18	78.66	74.92
% of Trip in Subsonic Cruise	12.52	15.46	12.54	15.49
Percent Nonstop Trips	87.88	89.39	87.88	89.39
Average Trip Load Factor	65.16	65.09	65.16	65.09
Annual RPMs (Billion)	551	1,043	551	1,043
Annual ASMs (Billion)	846	1,602	846	1,602
Annual Departures	793,510	1,765,140	793,510	1,765,140
Annual RAMs (GCD - Million)	2,713	5,031	2,713	5,031
Annual RAMs (Path - Million)	2,821	5,341	2,821	5,341

Table	2-3.	Utilization s	statistics f	for the	universal	airline	HSCT	network.
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Because of its speed, the HSCT has the ability to serve a large set of cities and still remain within the preference/curfew time "windows", which are always defined in local time.

2.6 2015 Subsonic Traffic

Subsonic air traffic for the year 2015 was projected using the passenger demand forecasts used in NASA Contractor Report 4592 (Baughcum, *et. al.*, 1994). Displacement of subsonic traffic by the HSCT passenger demand was included as described in the earlier study.

3.0 Emissions Calculation Procedure

3.1 Overview of Emissions Calculation

The primary emissions from aircraft engines are water vapor (H₂O) and carbon dioxide (CO₂) produced by the combustion of jet fuel. Nitrogen oxides (NO_X), carbon monoxide (CO) and hydrocarbons are also produced in the combustors and vary in quantity according to the temperature, pressure, and other combustor conditions. Nitrogen oxides consist of both nitric oxide (NO) and nitrogen dioxides (NO₂). Sulfur dioxide (SO₂) may also be produced due to sulfur impurities in jet fuel. Soot is also produced, particularly at high power settings, but its characterization is beyond the scope of the current work.

Emission indices of water, carbon monoxide, and sulfur dioxide are determined by the jet fuel properties. These were discussed in our previous contractor report (Baughcum, *et. al.*, 1994) and are summarized below.

· · · · · · · · · · · · · · · · · · ·	Emission Index			
Emission	1990	2015		
Carbon Dioxide (CO ₂) Water (H ₂ O)	3155 1237	3155 1237		
Sulfur dioxide (SO ₂)	0.8	0.4		

Table 3-1.Recommended emission indices in units of grams
emission/kilogram fuel for 1990 and 2015.

The emission levels from aircraft engines are discussed by Miake-Lye (Miake-Lye, *et. al.*, 1992). The emissions are characterized in terms of an emission index in units of grams of emission per kilogram of fuel burned. For NOx, the emission index [EI(NOx)] is given as gram equivalent NO₂ to avoid ambiguity. Although hydrocarbon measurements of aircraft emissions by species have been made (Spicer, *et. al.*, 1992), only total hydrocarbon emissions are considered in this work, with the hydrocarbon emission index [EI(HC)] given as equivalent methane (CH₄).

Nitrogen oxides are produced in the high temperature regions of the combustor primarily through the thermal dissociation of oxygen followed by oxygen atom reactions with molecular nitrogen. Thus, the NOx produced by an aircraft engine is sensitive to the length of the combustor, the pressure, and the temperature within the combustor. The emissions vary with the power setting of the engine (highest at high thrust conditions). By contrast, carbon monoxide and hydrocarbon emissions are highest at low power settings when the temperature of the engine is low and incomplete combustion occurs.

Once a schedule of city-pairs and departures was determined, the next step in the development of the scenario data set was to use aircraft/engine performance and emissions data to calculate the fuel use and emissions as a function of altitude and location. For each mission, fuel consumption and emissions are calculated including all the flight segments (taxi-out, takeoff, climb, cruise, descent, landing, taxi-in), distributing the emissions in space along the route between city-pairs. The emissions were then combined for all flights into the resulting three-dimensional database.

3.2 HSCT Description

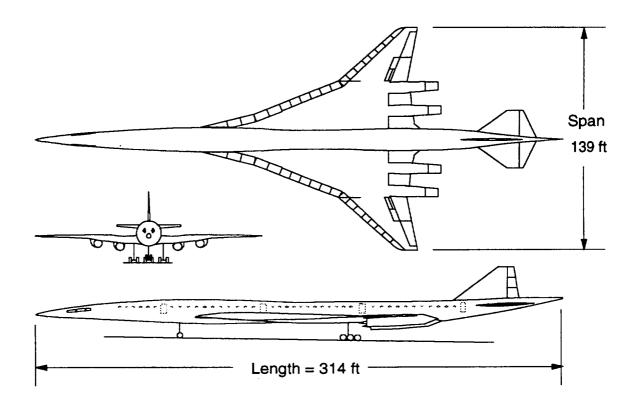
The Mach 2.4 HSCT scenarios were calculated using the Boeing preliminary design model 1080-924 with four Pratt & Whitney STJ989 turbine bypass engines (TBE) with mixed compression translating center body (MCTCB2) inlets and two-dimensional semi-stowable (SS2D) nozzles. The aircraft has a cranked-arrow wing planform (see Figure 3-1) and a mostly composite structure. Overall body length is approximately 314 feet with a wing span of 139 feet. It was designed to carry 309 passengers for a range of 5000 nautical miles.

The Mach 2.0 HSCT scenarios were developed based on the preliminary design model 1080-938 with four P&W STJ1016 turbine bypass engines with MCTCB2 inlets and SS2D nozzles. The characteristics of both these aircraft are summarized in Table 3-2.

	Mach 2.4	Mach 2.0
Model Number	1080-924	1080-938
Engine	PW STJ989	PW STJ1016
Range (nautical miles)	5000	5000
Passengers	309	309
Design Payload (Ibs)	64,890	64,890
Max. Takeoff Weight (lbs)	784,608	802,872
Wing Span (ft)	139	140
Wing Area (sq. ft.)	8180	8260

Table	3-2.	Summary of HSCT aircraft characteristics used in the
		development of the Mach 2.0 and Mach 2.4 HSCT emission
		scenarios.

Model 1080-924



Configuration Description:

Maximum takeoff weight Wing Area Engine Payload Range 784,600 pounds 8,180 square feet STJ989 309 passengers, tri-class 5,000 nmi - supersonic cruise

Figure 3-1. HSCT General Characteristics

The performance and emission characteristics for both Mach 2.0 and 2.4 were the same as those used as in the previous NASA contract work. (Baughcum, *et. al.*, 1994) However, it was found that the operating empty weights used in the previous emission scenario calculations had been incorrectly entered into the analysis data file and were not consistent with the performance data for the baseline model used in the study. This was corrected and revised emission inventories for Mach 2.0 and Mach 2.4 HSCTs on the 1993 AESA assessment network were calculated and delivered to NASA Langley. In this report, these revised 1993 AESA assessment scenarios are summarized and compared to the present universal airline results.

Emissions data for NOx, CO, and hydrocarbons were provided by GE/P&W for a generic HSCT combustor with a nominal NO_x emission index at supersonic cruise of approximately 5 gm NO_x (as NO₂)/kg fuel. Nitrogen oxides, carbon monoxide, and hydrocarbon emission levels were calculated from these data as a function of power setting and altitude. A similar calculation was completed to scale to a nominal cruise EI (NO_x)=15 scenario. For this scaling, the combustor was assumed to operate as a conventional combustor at low power settings and as an advanced low-NO_x combustor at higher settings. Based on discussions with both engine companies, the EI(NO_x) for this case was unchanged at low power settings and increased by a factor of 3 at higher thrust settings.

3.3 Mission Profiles

The mission profile procedures were described in detail in our previous NASA contractor report (Baughcum, *et. al.*, 1994). The basic HSCT mission profile was assumed as follows:

- 10 minute taxi-out
- all engine takeoff ground-roll and liftoff
- climbout to 1500 feet and accelerate
- climb to optimum cruise altitude (subsonic or supersonic, depending on whether over land or water)
- climbing supersonic cruise at constant Mach
- descent to 1500 feet
- approach and land
- 5 minute taxi-in

For a given HSCT model, fuel burned and emissions data were calculated for parametric mission cases: various takeoff weights (in increments of 50,000 pounds), two passenger-loading factors (100% and 65%), and with two cruise speeds (Mach 2.4 and Mach 0.9). These subsonic and supersonic mission profiles of varying range were used with a regression analysis to develop generalized performance for each HSCT mission segment as a function of weight. The details of this analysis were described in our previous NASA contractor report. (Baughcum, *et. al.*, 1994)

HSCT flight profiles of fuel burn and emissions were calculated from these performance and emissions data for each HSCT mission. These profiles combined with projected HSCT flight frequencies were then used to calculate the three-dimensional database, as described in our previous contractor report. (Baughcum, *et. al.*, 1994)

When calculating the flight profiles, all aircraft were assumed to fly according to design performance. For subsonic aircraft, cruise altitudes were calculated as a climbing cruise with the optimum altitude determined by the weight of the aircraft. For the HSCT, supersonic flight was allowed only over water and thus the mission profiles were more complicated than for subsonic aircraft.

Design optimum flight profiles between city-pairs were used to distribute emissions during takeoff, subsonic and supersonic climb and cruise, and descent. Based on these mission profiles, the calculated fuel burned and emissions were then transformed onto the database grid. Two missions, which are representative of the way in which an actual HSCT would be flown, are shown in Figures 3-2 and 3-3.

The simplest mission (Figure 3-2) is a flight almost exclusively over water, such as Seattle to Tokyo. The HSCT would take off and climb subsonically and then supersonically to a supersonic cruise altitude. It would then fly at supersonic cruise at the optimum altitude determined by its gross weight. As it approached Tokyo, it would descend and land. The cumulative fraction of the total NO_X emissions is plotted on the right axis. The plot illustrates that approximately 40% of the NO_X emissions would occur during takeoff, subsonic climb, and supersonic climb prior to supersonic cruise.

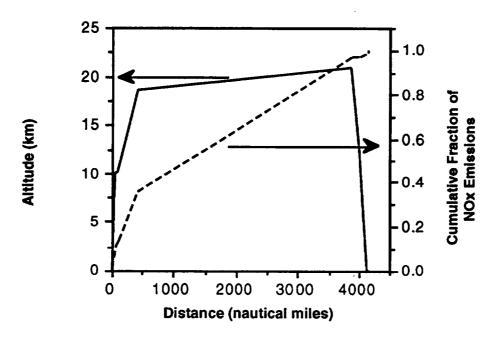


Figure 3-2. Mission profile for Mach 2.4 HSCT from Seattle to Tokyo.

A more complicated but still common mission is a flight in which one leg would be flown subsonically over land. This is illustrated in Figure 3-3 for a flight from Seattle to London. The HSCT would take off and climb to subsonic cruise altitudes. It would then cruise at subsonic speeds until it reached Hudson Bay where it would begin to climb supersonically. The HSCT would then cruise at supersonic speeds (altitude determined by the optimum performance) until descending near London. An even larger fraction (approximately 60%) of the NO_X emissions would occur during the subsonic climb, subsonic cruise, and supersonic climb prior to supersonic cruise.

A still more complicated mission, which was included in the calculations but not shown graphically, is a flight in which the aircraft might descend and climb several times to avoid flying supersonically over land. An example would be the Frankfurt to Bangkok route. In this case, the HSCT would fly subsonically over Europe, supersonically over the Mediterranean, subsonically over Arabia (stopping in Bahrain) supersonically over the Indian Ocean, and then subsonically inland over the Malay peninsula. Because of the high fuel consumption of supersonic climbs, such flight profiles were kept to a minimum in the scenario development.

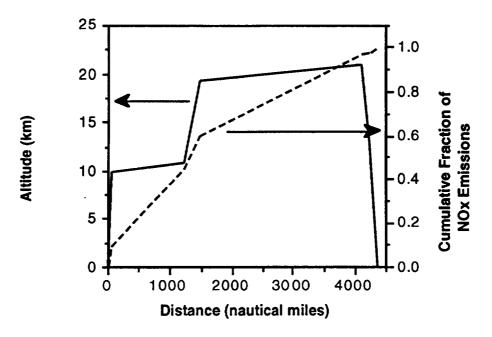


Figure 3-3. Mission profile for Mach 2.4 HSCT from Seattle to London.

3.4 Emission Calculation Procedures

All aircraft were assumed to fly according to design optimum performance. Altitudes and mission profiles were calculated based on the performance of the aircraft for its mission weight. Air traffic control constraints on routings were not considered. For each aircraft type considered, a separate three-dimensional data set of fuel burned and emissions was calculated. Subsonic aircraft were flown along great circle routes between cities. For the HSCT, routing between waypoints to avoid supersonic flight over land was used for many of the citypairs. The HSCT was flown along great circle routes between these waypoints. For all flights, prevailing winds were not considered, based on the assumption that wind effects would largely be canceled out for round trips.

To calculate the global inventory of aircraft emissions, a computer model was developed which basically combines scheduling data (city pairs, departures, aircraft type) with aircraft performance and emissions data. The Global Atmospheric Emissions Code (GAEC) computer model was used to calculate fuel burned and emissions from files of airplane performance and engine emissions data. The aircraft performance file contains detailed performance input data for a wide range of operating conditions. Each engine emission input file contains emission indices tabulated as a function of the fuel flow rate. The GAEC model was described in more detail in the earlier report (Baughcum, *et. al.*, 1994).

For each route flown by the airplane/engine type, the takeoff gross weight required was calculated as a function of the city-pair route distance. The fuel burned was calculated for the following flight segments:

- Taxi-out
- Takeoff
- Climbout
- Subsonic Climb
- Subsonic Cruise
- Supersonic Climbout
- Supersonic Cruise
- Supersonic Descent
- Descent
- Approach and Land
- Taxi-in

For year 2015 subsonic aircraft, emissions of nitrogen oxides (NOx), hydrocarbons (HC) and carbon monoxide (CO) were projected from the ground level emission indices reported to the International Civil Aviation Organization (ICAO) for current aircraft. These measurements are reported at four thrust settings. The Boeing fuel flow correlation methodology was used to calculate emission indices for different flight phases, corrected for ambient temperature, pressure, and humidity. (Baughcum, *et. al.*, 1994; R. L. Martin, C. A. Oncina, and J. Zeeben, private communication). This methodology will be described in more detail in a future NASA contractor report describing the development of subsonic aircraft emission inventories for each month of 1992. (S. L. Baughcum, T. G. Tritz, and S. C. Henderson, private communication)

Subsonic aircraft emission inventories were calculated using the same technology improvements as reported in NASA CR-4592 (Baughcum, *et. al.*, 1994) except that a small error for the largest airplane type (P900) was discovered. The technology improvement factor for fuel flow given in Table 6-4 of NASA CR-4592 for the P900 aircraft had not been correctly used in the previous calculation. This was corrected so that the calculations are now consistent with the improvement factors shown in NASA CR-4592. As described later in this report, this makes only an approximately 2% change in the fuel use projected for the 2015 all subsonic fleet. Emission inventories for scheduled subsonic air traffic were calculated for the cases of fleets of 0, approximately 500, and approximately 1000 HSCTs on the universal airline network. Displacement of subsonic air traffic by HSCTs on individual routes was explicitly taken into account. The results are described in Sections 4 and 5 of this report.

Distributions of fuel usage and emissions were calculated for 1° latitude x 1° longitude x 1 km altitude cells. The altitudes used are pressure altitudes, not geometrical altitudes. The altitude corresponds to the geopotential altitudes of the U.S. Standard Atmosphere temperature and pressure profile and is thus pressure-gridded data. (U. S. Standard Atmosphere, 1976) Commercial aircraft measure their altitudes using pressure altimeters. For each city-pair, the total route distance was calculated. The fuel burn rate and airplane gross weight were then calculated at discrete distances along the route path which corresponded to points where the airplane entered or left a cell (crossed any of the cells boundaries) or points where a transition in flight conditions occurred (climbout/climb, climb/cruise, cruise/descent, descent/approach and land, taxiout/climbout, approach and land/taxi-in). The fuel burn rate would change dramatically at these transition points.

The emissions were calculated for each flight segment between the above described discrete points using the fuel burn rate within the segment. The total fuel burned in the segment was calculated as the difference in airplane gross weight at the segment end-points. The emissions were then assigned to a cell based on the coordinates of the endpoints.

4.0 Emission Inventory Results

A summary of the network statistics is shown in Table 4-1. An increase in the size of the HSCT fleet results in a greater number of city pairs included in the network. To satisfy the same passenger demand, a Mach 2.0 HSCT fleet requires about 6% more aircraft than needed for Mach 2.4 and flies at supersonic cruise about 4000 feet lower.

Doubling the size of the fleet results in an approximate doubling of the number of departures and an approximate doubling in the global fuel burn for the fleet. Comparison of the departure frequencies shown in Appendix C indicates that doubling the fleet size increases the flight frequencies on some routes but not on others, since it is sensitive to the market penetration analyses. Thus, changes in the geographical distribution of emissions may occur upon fleet growth. This will be discussed in more depth in Section 5.

The minimum altitudes shown in Table 4-1 correspond to the lowest altitudes at which supersonic cruise is reached. Because the Mach 2.4 HSCT must climb to higher altitudes which takes both time and distance, the Mach 2.0 is able to supersonically cruise on some segments for which the Mach 2.4 aircraft cannot.

	1993 AESA Assessment Network (revised)	New Universal Network "500"	New Universal Network "1000"	
Mach 2.4	4			
Number of Aircraft	500	499	991	
Number of city pairs	193	243	392	
Total daily departures	2,192	2,174	4,836	
Total distance (miles/day)	7,458,802	7,728,939	14,632,996	
Total Fuel (million lbs/day)	493.03	509.46	961.33	
Maximum flight altitude (feet)	67,904	67,854	67,865	
Minimum cruise altitude (feet)	57,722	57,547	57,547	
Mach 2.0	-			
Number of Aircraft	532	528	1062	
Number of city pairs	193	243	392	
Total daily departures	2,192	2,174	4,836	
Total distance (miles/day)	7,458,802	7,728,939	14,632,996	
Total Fuel (million lbs/day)	504.79	524.27	979.92	
Maximum flight altitude (feet)	63,956	63,907	63,920	
Minimum cruise altitude (feet)	52,881	53,674	53,674	

 Table 4-1.
 Summary of departure statistics for HSCT networks.

The fuel use and emissions for the different scenarios considered are summarized in Table 4-2 below. As shown below, the change from the simple ground rules to the market-driven universal airline network has only a small effect on the global fuel usage and NOx emissions for a fleet of 500 HSCTs. The biggest changes occurred in the geographical distribution of the emissions.

Table 4-2			se and emiss		and the second		
Mach Number	EI(NOX)	Number of HSCTs	Network	Fuel (kg/yr)	NOx (kg/yr)	HC (kg/yr)	CO (kg/yr)
Mach 2.4 f	leet						
2.4	5	500	1993 AESA	8.16E+10	5.37E+08	2.99E+07	2.42E+08
2.4	5	499	universal	8.21E+10	5.35E+08	2.97E+07	2.41E+08
2.4	5	991	universal	1.57E+11	1.04E+09	5.88E+07	4.76E+08
2.4	15	500	1993 AESA	8.16E+10	1.46E+09	2.99E+07	2.42E+08
2.4	15	499	universal	8.21E+10	1.48E+09	2.97E+07	2.41E+08
2.4	15	991	universal	1.57E+11	2.82E+09	5.88E+07	4.76E+08
Mach 2.0 F	Fleet						
2.0	5	532	1993 AESA	8.36E+10	5.02E+08	2.89E+07	2.45E+08
2.0	5	528	universal	8.45E+10	5.04E+08	2.90E+07	2.47E+08
2.0	5	1062	universal	1.60E+11	9.65E+08	5.66E+07	4.78E+08
2.0	15	532	1993 AESA	8.36E+10	1.47E+09	2.89E+07	2.45E+08
2.0	15	528	universal	8.45E+10	1.48E+09	2.90E+07	2.47E+08
2.0	15	1062	universal	1.60E+11	2.82E+09	5.66E+07	4.78E+08
2015 Scheo	luled Subs	onic Air T	raffic				
Subsonic pas Subsonic pas Subsonic pas 2015 Cargo A	senger aircra	aft (with 500 N		2.50E+11 2.22E+11 1.97E+11 5.64E+09	2.32E+09 2.05E+09 1.75E+09 4.91E+07	9.93E+07 9.34E+07 1.95E+08 3.56E+06	1.11E+09 1.05E+09 1.32E+09 2.77E+07

 Table 4-2.
 Summary of fuel use and emissions for the different scenarios.

The fuel burned and emissions for the network used in the 1993 AESA assessment (Baughcum, *et. al.*, 1994) differ somewhat from those reported earlier. An error in the weight of the aircraft used in the performance calculations was discovered upon later analysis. Using the corrected weights, the emission inventories for the 1993 AESA assessment network were rerun. The total fleet fuel burn for the 500 aircraft fleet increased by about 7% from that reported earlier (Baughcum, *et. al.*, 1994) for the Mach 2.4 HSCT fleet. In addition, with the correct (heavier) weight, the supersonic cruise altitudes were slightly lower than those used in the earlier study. In the earlier report

(Baughcum, *et. al.*, 1994), the Mach 2.4 HSCT cruise altitudes were in the range of 59,639-69,098 feet. The corrections in the aircraft weight result in cruise altitudes about 1100 feet lower for the new scenarios. Similar problems were discovered and corrected for the Mach 2.0 emission inventories.

In this section, the results for the individual component inventories will be presented and discussed. In the next section, the overall results and changes between the different scenarios will be analyzed.

4.1 Mach 2.4 HSCT Fleet Results

Details of the results of HSCT fleet operations for different flight segments for the Mach 2.4 HSCT fleets are summarized in Tables 4-3 and 4-4. Table 4-5 shows the revised results for the 1993 AESA study. For all cases considered, the majority of the miles flown, fuel used and NOx emissions occur during supersonic cruise, where the actual EI at cruise is 5.42 (close to the nominal value of 5). The nominal EI=15 case was calculated by scaling the EI(NOx) at cruise by a factor of 3 as described in CR 4592 (Baughcum, *et. al.*, 1994). The calculated EI(NOx) at cruise for the nominal EI=15 case is 16.4 (see Appendix F).

The calculated fuel burned, emissions, and effective emission indices as a function of altitude (summed over latitude and longitude) for the Mach 2.4 HSCTs (both EI(NOx)=5 and 15) are tabulated in Appendix F. Also included in Appendix F are the revised results for the 1993 AESA assessment network.

Segmen			Doily		
			Daily	Daily	
		Daily	Fuel	NOx	
Flight Segment		Mileage (nmi)	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out		0	6,376	42	6.56
Initial Climb		96,929	40,780	353	8.65
Supersonic Climb		688,696	91,822	795	8.65
Supersonic Cruise		5,808,829	318,909	1,728	5.42
Supersonic Descent		264,008	1,714	11	6.56
Subsonic Cruise		555,250	34,864	289	8.30
Final Descent		315,230	12,559	82	6.56
Taxi in		0	2,435	16	6.56
Ţ	otal	7,728,942	509,460	3,316	6.51

Table 4-3.Daily mileage, fuel consumption, NOx emissions, and NOx
emission index for the Mach 2.4 HSCT, nominal EI=5 flight
segments. (Universal Network, 500 HSCTs)

······································		Daily	Daily	
	Daily	Fuel	NOx	
Flight Segment	Mileage	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out	0	14,184	93	6.56
Initial Climb	208,556	85,784	742	8.65
Supersonic Climb	1,369,248	180,857	1,565	8.65
Supersonic Cruise	10,415,248	561,414	3,041	5.42
Supersonic Descent	585,600	3,802	25	6.56
Subsonic Cruise	1,353,126	81,939	680	8.30
Final Descent	701,220	27,938	183	6.56
Taxi in	0	5,416	36	6.56
Тс	otal 14,632,998	961,333	6,365	6.62

Table 4-4.	Daily mileage, fuel consumption, NOx emissions, and NOx
	emission index for the Mach 2.4 HSCT, nominal EI=5 flight
	segments. (Universal Network, 1000 HSCTs)

Table 4-5.Daily mileage, fuel consumption, NOx emissions, and NOx
emission index for the Mach 2.4 HSCT, nominal EI=5 flight
segments. (1993 AESA assessment network(revised), 500
HSCTs)

16613)		Daily	Daily	
	Daily	Fuel	NOx	
Flight Segment	Mileage	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out	0	6,429	42	6.56
Initial Climb	96,929	40,599	351	8.65
Supersonic Climb	666,449	88,815	769	8.65
Supersonic Cruise	5,380,866	295,890	1,603	5.42
Supersonic Descent	256,932	1,668	11	6,56
Supersonic Cruise & Descent	22,686	2,218	19	8.65
Subsonic Cruise	717,101	42,289	351	8.30
Final Descent	317,840	12,663	83	6.56
Taxi in	0	2,455	16	6.56
Total	7,458,803	493,027	3,245	6.58

The three-dimensional character of the emission inventories is illustrated in Figure 4-1, which shows the daily NOx emissions from a fleet of 500 Mach 2.4 (EI(NOx)=5) HSCTs on the universal airline network. The top panel shows NOx emissions as a function of altitude and latitude (summed over longitude). This represents the input to a 2-dimensional (altitude and latitude) stratospheric chemistry model, such as those used in the AESA assessment. Peak emissions occur at supersonic cruise at northern mid-latitudes. The bottom panel illustrates the route segments occurring at altitudes above 13 kilometers, which correspond to supersonic climb and cruise.

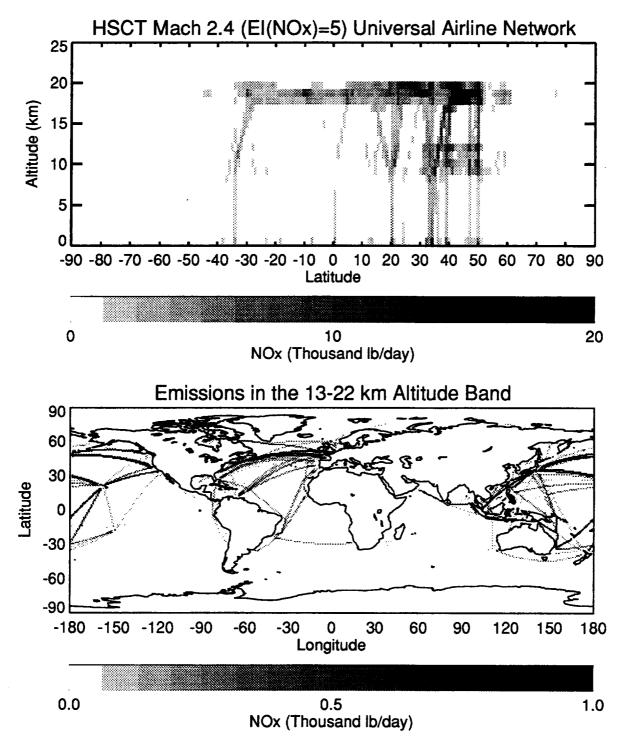


Figure 4-1. NOx emissions for a fleet of 500 Mach 2.4 HSCTs on the Universal Airline Network, as a function of altitude and latitude (summed over longitude, top panel) and as a function of latitude and longitude (summed over the 13-22 km altitude band, bottom panel). (Values greater than maximum are plotted as black.) The fuel burned and emissions (NOx, hydrocarbons, and CO) as a function of altitude are shown in Figure 4-2 for fleets of 500 and 1000 Mach 2.4 HSCTs (EI(NOx)=5) on the present universal airline network. Not surprisingly, the larger fleet has approximately twice as much emissions and shows the same altitude distribution as the 500 HSCT fleet. Figure 4-3 shows the cumulative fraction of fuel burn and emissions plotted as a function of altitude for the two fleet sizes. The additional shorter routes for the 1000 HSCT fleet results in a larger fraction of the fuel burn and emissions occurring at lower altitudes for takeoff, climbout, and supersonic climb. Although the majority of the fuel use and NOx emissions will occur in the 18-21 kilometer altitude band, a significant fraction of the emissions occurs below 10 kilometers and between 10 and 18 kilometers.

The emission indices as a function of altitude are shown in Figure 4-4. The variation in emissions as a function of altitude reflect the changes in fuel burn rate at different stages of the flights and changes in power setting (with resulting changes in emission indices). Changes in HSCT fleet size have relatively little impact on the emission indices averaged over all missions.

The geographical distribution of the emissions for the universal airline network is displayed in Figure 4-5 for fleets of 500 and 1000 Mach 2.4 HSCTs. For these plots, the emissions for the entire fleet have been been summed over longitude and then plotted as a function of latitude. The plots show that most of the HSCT flights will occur at northern midlatitudes. Figure 4-6 shows the cumulative fraction as a function of latitude for each of the emissions, summing over the entire altitude range (0-22 km). For both fleet sizes, approximately 20% of the emissions occur in the Southern hemisphere, but the majority occur north of 30° North latitude.

The emissions injected above 13 kilometers in altitude, which will have the greatest impact on the stratospheric ozone layer, are shown in Figure 4-7 as a function of latitude for fleets of 500 and 1000 Mach 2.4 HSCTs. Figure 4-8 shows the cumulative fraction as a function of latitude for each of the emissions, summing over the 13 to 22 kilometer altitude band. Approximately 60% of the stratospheric NOx from the HSCT fleets will be injected north of 30° North latitude.

Growth of the fleet to 1000 active HSCTs causes only small changes in the geographical distribution. A more detailed discussion of the changes in emissions as the fleet grows from 500 to 1000 HSCTs will be presented in Section 5.

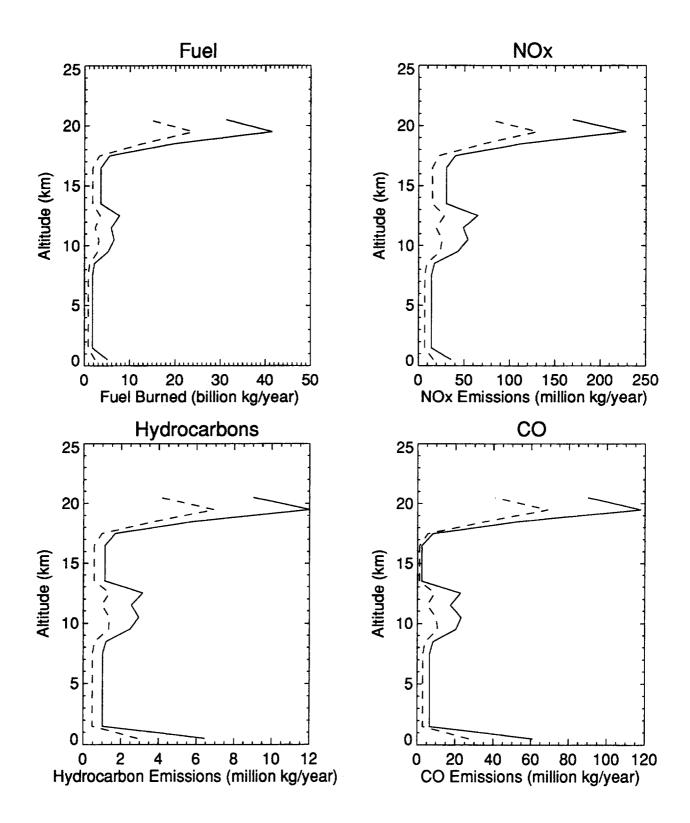


Figure 4-2. Fuel burned and emissions as a function of altitude for the universal airline HSCT network for a fleet of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with EI(NOx) of approximately 5 at supersonic cruise (summed over latitude and longitude).

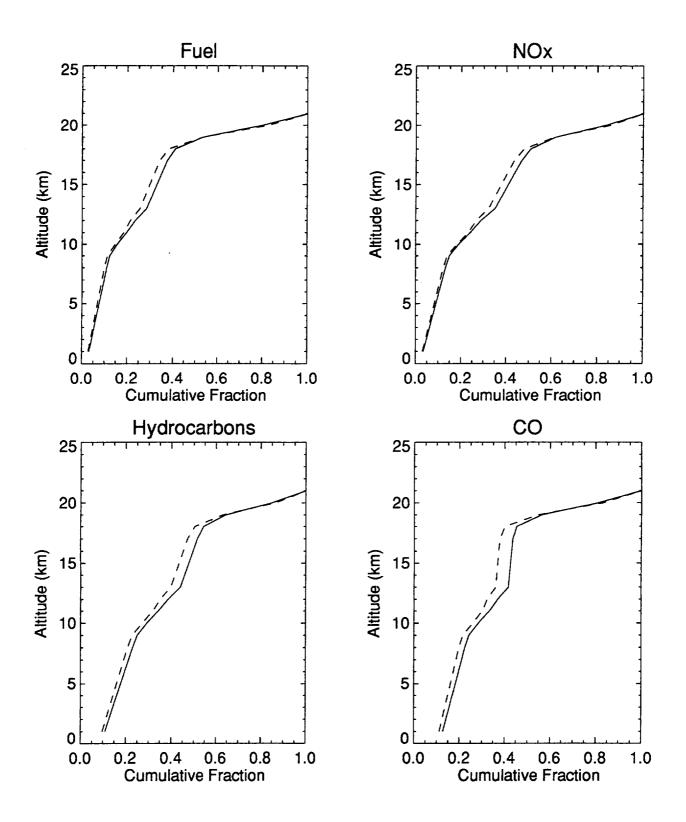
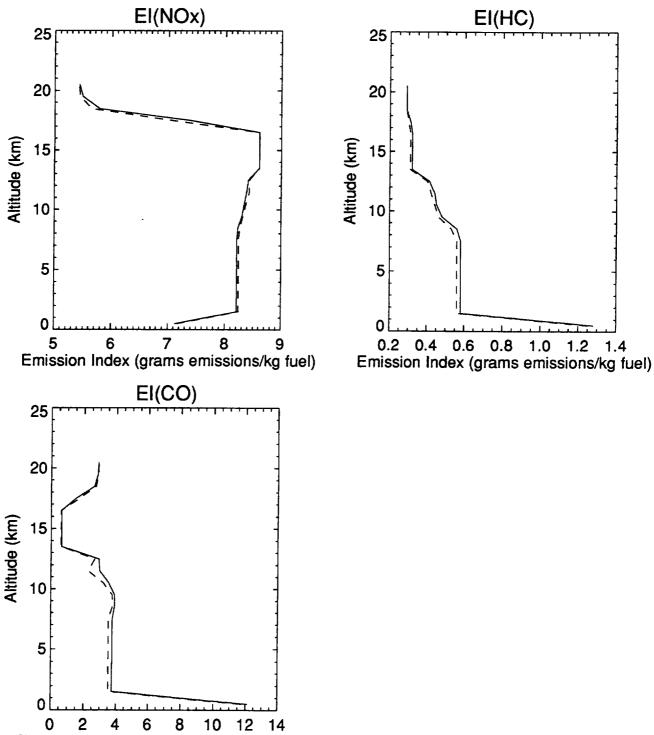


Figure 4-3. Cumulative fraction of fuel burned and emissions as a function of altitude for the universal airline HSCT network for a fleet of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with EI(NOx) of approximately 5 at supersonic cruise (summed over latitude and longitude).



Emission Index (grams emissions/kg fuel)

Figure 4-4. Emission indices as a function of altitude for the universal HSCT network for a fleet of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with EI(NOx) of approximately 5 at supersonic cruise (summed over latitude and longitude).

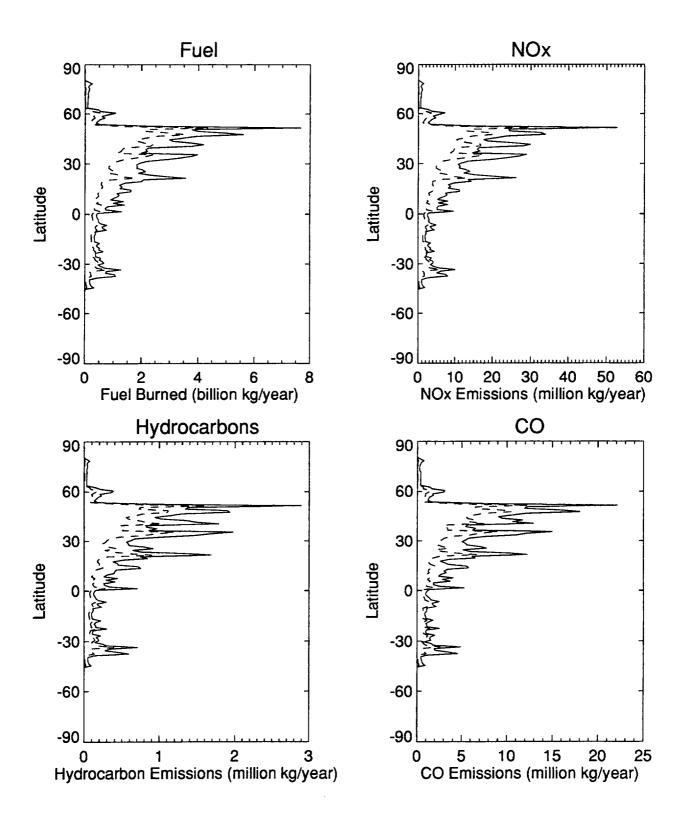


Figure 4-5. Fuel burned and emissions as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

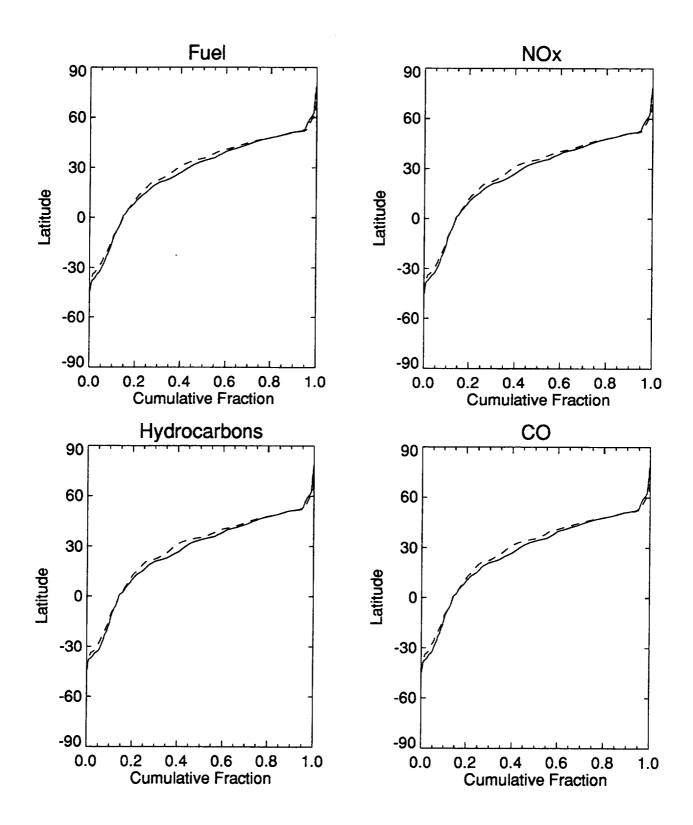


Figure 4-6. Cumulative fraction of fuel burned and emissions as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

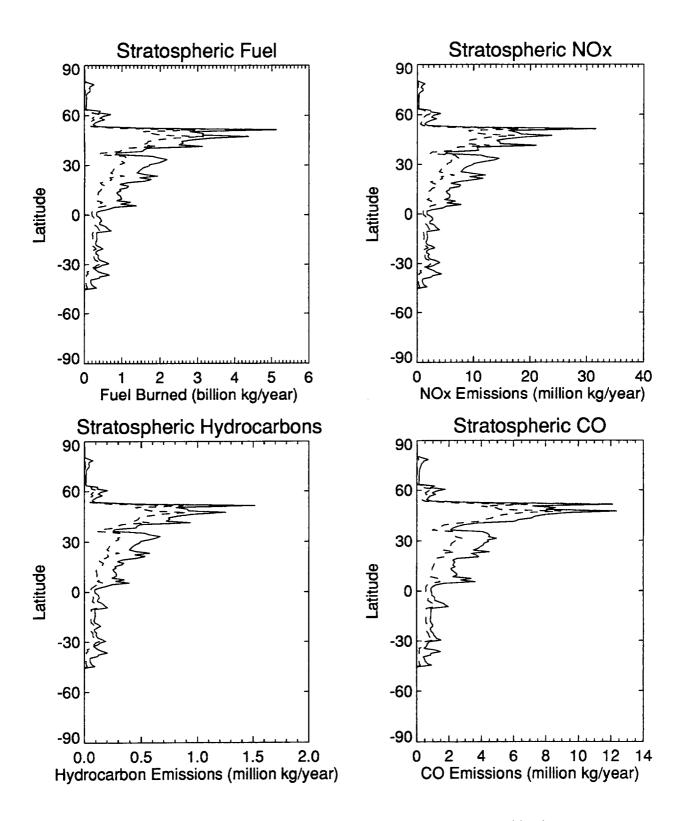


Figure 4-7. Fuel burned and emissions above 13 kilometers altitude as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

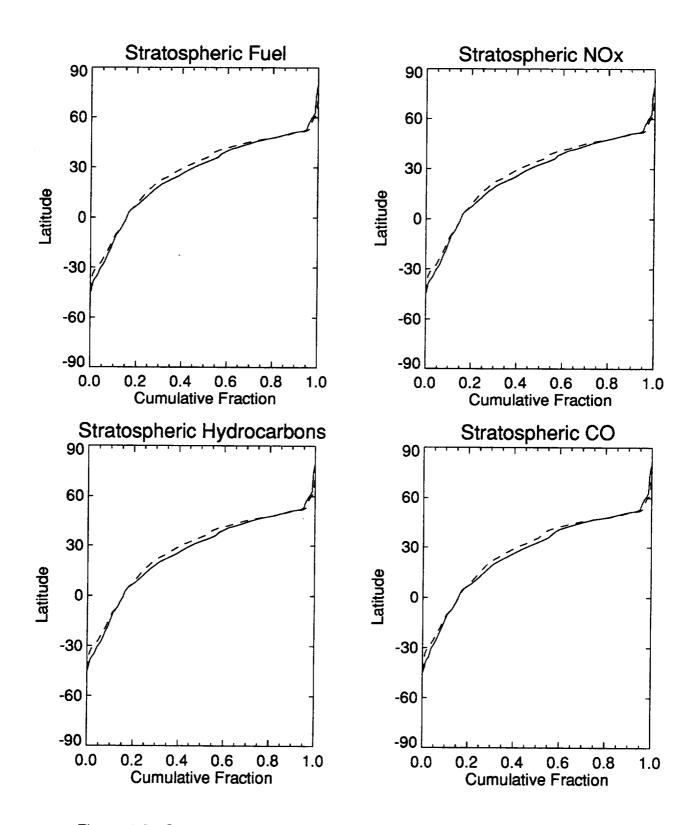


Figure 4-8. Cumulative fraction of fuel burned and emissions above 13 kilometers altitude as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

4.2 Mach 2.0 HSCT fleet Results

Details of the results for different flight segments for the Mach 2.0 HSCT fleets are summarized in Tables 4-6 and 4-7. Table 4-8 shows the revised results for the 1993 AESA study. For all cases considered, the majority of the miles flown, fuel used and NOx emissions occur during supersonic cruise, where the calculated EI is 5.24.

The calculated fuel burned, emissions, and effective emission indices as a function of altitude (summed over latitude and longitude) for the M2.0 HSCTs (both EI(NOx)=5 and 15) are tabulated in Appendix G. Also included in Appendix G are the revised results for the 1993 AESA assessment network for Mach 2.0 HSCTs.

Since the same passenger demand was used for the Mach 2.0 fleet as was used for the Mach 2.4 fleet, the geographical distribution of emissions for the Mach 2.0 case is the same as for Mach 2.4. The altitude distributions are similar except that the supersonic cruise emissions occur approximately 4000 feet lower.

	C	Daily	Daily Fuel	Daily NOx	
Flight Segment	Milea	ge (nmi)	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out		0	5,752	40	7.00
Initial Climb		87,860	36,689	297	8.10
Supersonic Climb	4	82,933	66,765	541	8.10
Supersonic Cruise	6,0	79,332	367,116	1,925	5.24
Supersonic Descent	1	97,106	1,375	10	6.99
Subsonic Cruise	5	62,131	32,536	214	6.57
Final Descent	3	19,578	11,818	83	6.99
Taxi in		0	2,222	16	6.99
1	otal 7,7	28,940	524,273	3,125	5.96

Table	4-6.	Daily mileage, fuel consumption, NOx emissions, and NOx
		emission index for the Mach 2.0 HSCT, nominal EI=5 flight
		segments. (Universal Network, passenger demand
		corresponding to 500 Mach 2.4 HSCTs)

correspon	nding to 1000 Ma	Daily	S) Daily	
	Daily	Fuel	NOx	
Flight Segment	Mileage (nmi)	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out	0	12,796	90	7.00
Initial Climb	188,134	76,870	623	8.10
Supersonic Climb	965,212	131,653	1,067	8.10
Supersonic Cruise	10,963,144	648,318	3,400	5.24
Supersonic Descent	437,346	3,052	21	6.99
Subsonic Cruise	1,368,262	76,000	499	6.57
Final Descent	710,892	26,288	184	6.99
Taxi in	0	4,942	35	6.99
Tot	al 14,632,990	979,919	5,918	6.04

Table 4-7.Daily mileage, fuel consumption, NOx emissions, and NOx
emission index for the Mach 2.0 HSCT, nominal EI=5 flight
segments. (Universal Network, passenger demand
corresponding to 1000 Mach 2.4 HSCTs)

Table 4-8.Daily mileage, fuel consumption, NOx emissions, and NOx
emission index for the Mach 2.0 HSCT, nominal EI=5 flight
segments. (1993 AESA assessment network (revised),
passenger demand corresponding to 500 Mach 2.4 HSCTs)

		Daily	Daily	
	Daily	Fuel	NOx	
Flight Segment	Mileage (nmi)	(1000 lbs)	(1000 i bs)	EI(NOx)
Taxi out	0	5,800	4 1	7.00
Initial Climb	87,777	36,453	295	8.10
Supersonic Climb	472,821	65,351	529	8.10
Supersonic Cruise	5,649,821	341,743	1,792	5.24
Supersonic Descent	194,285	1,356	9	6.99
Supersonic Cruise & Descent	11,777	1,146	9	8.10
Subsonic Cruise	720,099	38,788	255	6.57
Final Descent	322,224	11,916	83	6.99
Taxi in	0	2,240	16	6.99
Total	7,458,804	504,792	3,030	6.00

Since the Mach 2.0 and Mach 2.4 HSCT fleets are flown on the same passenger demand network in this study, the primary difference between the two fleets is that the Mach 2.0 fleet requires about 6% more aircraft to satisfy the same passenger demand and the aircraft cruise supersonically about 4000 feet lower. Tables of the emissions as a function of altitude for Mach 2.0 are included as Appendix G.

4.3 Year 2015 Subsonic Fleet Results

For year 2015 subsonic passenger aircraft, 10 jet categories and one generic turboprop were considered. These are summarized in Table 4-9. These are the same categories as used in our previous study (Baughcum, *et. al.*, 1994). Aircraft performance and emissions characteristics were the same as used in the previous study except that an error in the performance data used for the P900 aircraft type (> 900 passengers) was corrected, as described in Section 3. This increased the total projected fuel burn for the all subsonic 2015 scheduled passenger fleet by about 2%.

Results are presented here for the the subsonic passenger fleet in use for the cases where there are 0, 500, and 1000 Mach 2.4 HSCTs in use on the universal network. Subsonic cargo aircraft data was not updated from that presented earlier (Baughcum, *et. al.*, 1994) but is included in the summaries.

Class	Seating Capacity	Average Seats
TBP (turboprop)	0 - 49	30
P060	50 - 69	60
P080	70 - 109	85
P120	110 - 139	120
P180	140 - 19 9	170
P250	200 - 299	250
P350	300 - 399	350
P500	400 - 599	500
P700	600 - 799	700
P900	> 800	900

Table 4-9.	Classes of "Generic" Subsonic Passenger Aircraft Used in the
	2015 Scenario Construction

The results for the three subsonic passenger fleets are summarized by aircraft type in Tables 4-10, 4-11, and 4-12. Fuel use by subsonic passenger jets was projected to drop by approximately 11% because of the displacement caused by 500 HSCTs in operation and 21% in the presence of 1000 HSCTs. As discussed in Section 5, total fuel usage for the combined fleet of subsonic and HSCT fleets would increase as HSCTs displace subsonic aircraft.

The calculated fuel burn, emissions, and effective emission indices as a function of altitude (summed over latitude and longitude) for the year 2015 subsonic passenger fleets are tabulated in Appendix G.

Table 4-10Globally Computed Fuel Burned, Emissions, and Emission
Indices by Aircraft Type for 2015 Scheduled Subsonic Airliners if
500 Mach 2.4 HSCTs are in operation on the universal network.

					Globally Averaged Emission Indices		
5 11.	Fuel	NOx	HC	CO	EI	EI	EI
File	(kg/yr)	. (kg/yr)	(kg/yr)	(kg/yr)	(NO _x)	(HC)	(CO)
P060	2.63E+09	1.49E+07	1.47E+06	1.44E+07	5.66	0.56	5.50
P080	8.67E+09	6.84E+07	2.91E+06	6.59E+07	7.88	0.34	7.60
P120	1.42E+10	1.04E+08	8.02E+06	1.25E+08	7.37	0.57	8.85
P180	2.34E+10	1.73E+08	5.80E+06	1.23E+08	7.39	0.25	5.26
P250A	2.49E+10	2.15E+08	1.64E+07	1.63E+08	8.64	0.66	6.56
P250B	1.65E+10	1.21E+08	1.16E+07	6.23E+07	7.33	0.70	3.77
P350	4.09E+10	4.29E+08	1.48E+07	1.56E+08	10.50	0.36	3.82
P500	5.07E+10	4.74E+08	1.80E+07	2.15E+08	9.33	0.35	4.25
P700	2.24E+10	2.61E+08	4.18E+06	5.46E+07	11.66	0.19	2.44
P900	1.37E+10	1.45E+08	3.02E+06	4.22E+07	10.59	0.22	3.07
TBP	4.13E+09	4.40E+07	7.29E+06	2.41E+07	10.65	1.76	5.83
Total	2.22E+11	2.05E+09	9.34E+07	1.05E+09	9.23	0.42	4.71

Table 4-11Globally computed fuel burned, emissions, and emission Indices
by Aircraft Type for 2015 Scheduled Subsonic Airliners if 1000
Mach 2.4 HSCTs are in operation on the universal network.

					Globally Averaged Emission Indices		
	Fuel	NOx	HC	CO	EI	EI	ΕI
File	(kg/yr)	(kg/yr)	(kg/yr)	(kg/yr)	(NO _x)	(HC)	(CO)
P060	2.63E+09	1.49E+07	1.47E+06	1.44E+07	5.66	0.56	5.50
P080	8.67E+09	6.84E+07	2.91E+06	6.59E+07	7.88	0.34	7.60
P120	1.41E+10	1.04E+08	8.01E+06	1.25E+08	7.37	0.57	8.86
P180	2.34E+10	1.73E+08	5.81E+06	1.23E+08	7.39	0.25	5.26
P250A	2.46E+10	2.13E+08	1.63E+07	1.62E+08	8.65	0.66	6.58
P250B	1.31E+10	9.59E+07	9.54E+06	5.11E+07	7.32	0.73	3.90
P350	3.65E+10	3.85E+08	1.38E+07	1.45E+08	10.56	0.38	3.97
P500	4.79E+10	4.49E+08	1.69E+07	2.02E+08	9.36	0.35	4.22
P700	1.64E+10	1.95E+08	3.61E+06	4.60E+07	11.92	0.22	2.80
P900	5.41E+09	6.10E+07	1.42E+06	1.91E+07	11.28	0.26	3.53
TBP	4.13E+09	4.40E+07	7.29E+06	2.41E+07	10.65	1.76	5.83
Total	1.97E+11	1.80E+09	8.71E+07	9.78E+08	9.16	0.44	4.97

					Glob: Emis	-	
- ' 4 -	Fuel	NOx	HC	, co	EI	EI	EI
File	(kg/yr)	(kg/yr)	(kg/yr)	(kg/yr)	(NO _x)	(HC)	(CO)
P060	2.63E+09	1.49E+07	1.47E+06	1.44E+07	5.66	0.56	5.50
P080	8.67E+09	6.84E+07	2.91E+06	6.59E+07	7.88	0.34	7.60
P120	1.42E+10	1.04E+08	8.02E+06	1.25E+08	7.37	0.57	8.85
P180	2.35E+10	1.73E+08	5.81E+06	1.23E+08	7.39	0.25	5.25
P250A	2.49E+10	2.15E+08	1.64E+07	1.63E+08	8.64	0.66	6.56
P250B	2.10E+10	1.54E+08	1.39E+07	7.59E+07	7.33	0.66	3.61
P350	4.31E+10	4.51E+08	1.52E+07	1.61E+08	10.48	0.35	3.74
P500	5.25E+10	4.88E+08	1.86E+07	2.23E+08	9.31	0.35	4.26
P700	3.15E+10	3.61E+08	5.11E+06	6.84E+07	11.48	0.16	2.17
P900	2.40E+10	2.46E+08	4.63E+06	6.66E+07	10.22	0.19	2.77
TBP	4.13E+09	4.40E+07	7.29E+06	2.41E+07	10.65	1.76	5.83
Total	2.50E+11	2.32E+09	9.94E+07	1.11E+09	9.28	0.40	4.44

Table 4-12Globally Computed Fuel Burned, Emissions, and Emission
Indices by Aircraft Type for 2015 Scheduled Subsonic Airliners if
no HSCT Fleet Exists (revised from NASA CR 4592)

5.0 Analysis and Discussion

5.1 Comparison of HSCT Universal Fleet Emissions with Old Network Results

The weight corrections discussed earlier resulted in an increase in global fuel use of 7% by the HSCT fleet and cruise altitudes about 1100 feet lower than those described earlier ((Baughcum, *et. al.*, 1994) and used in the 1993 AESA assessment. Changing from the 1993 AESA assessment network to the new universal airline network for the same number of active HSCTs in-service has little effect (less than 1%) on the global fuel burn or emissions for the HSCT fleet, when the correct OEW is used, as shown in Table 5-1.

 Table 5-1. Comparison of the new universal network fuel use and emissions with the revised 1993 AESA assessment network results.

Mach 2.4 HSCT EI(NOx)=5		Fuel (kg/year)	NOx (kg/year)	HC (kg/year)	CO (kg/year)
1993 AESA assessment network (500 HSCTs) (Baughcum, <i>et. al.</i> , 1994)		7.64E+10	5.00E+08	2.83E+07	2.33E+08
1993 AESA assessment network (500 HSCTs)(revised)		8.16E+10	5.37E+08	2.99E+07	2.42E+08
new universal network (500 HSCTs)		8.21E+10	5.35E+08	2.97E+07	2.41E+08
difference relative to the 1993 AESA		5.02E+08	-2.63E+06	-2.09E+05	-1.15E+06
network (revised)	Percent change	0.61%	-0.49%	-0.70%	-0.47%

The change in ground rules has a much larger effect on the geographical distribution of the emissions. This is shown in Figure 5-1 where the 3dimensional inventory of emissions calculated for the universal airline network is compared with the 1993 AESA assessment network (revised to account for the correct OEW). The top panel shows the increases in NOx emissions as a function of latitude and altitude when the universal airline network is compared with the 1993 AESA assessment network results (revised). The bottom panel shows the decreases in NOx emissions when the universal airline network is compared with the 1993 AESA assessment network results (revised). The bottom panel shows the decreases in NOx emissions when the universal airline network is compared with the 1993 AESA assessment network results (revised). In general, the new universal airline network has the HSCT flying at subsonic cruise less than in the 1993 AESA assessment network. There are also fewer emissions at high northern latitudes and more in the Southern hemisphere for the new network.

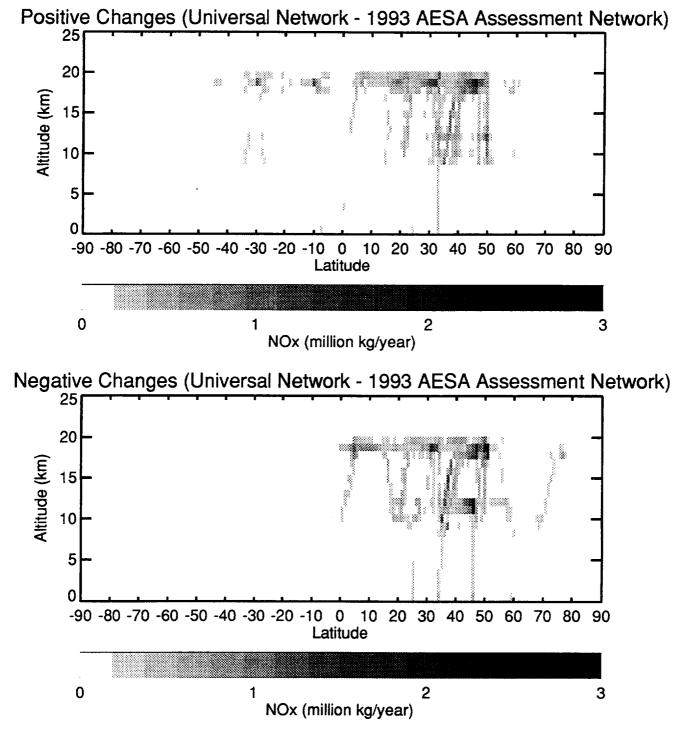


Figure 5-1. Comparison of NOx emissions from the universal airline network with the revised 1993 AESA assessment network for 500 Mach 2.4 [EI(NOx)=5] HSCTs. The top panel shows positive changes, while the bottom panel shows negative changes. (summed over longitude)

Since the changes in the high altitude emissions are expected to have the largest effects on ozone impact, the discussion will focus on changes in stratospheric NOx emissions. Figure 5-2 shows a comparison of the NOx emissions above 13 kilometers altitude for the 1993 AESA assessment network (revised) and the new 500 HSCT universal airline network. High altitude NOx emissions are greater in the southern hemisphere for each of the 10 degree latitude bands shown here. NOx emissions at extremely high northern latitudes (>70N) are less than with the old network. The analysis shows a net increase in the tropics of high altitude NOx emissions compared with the old network. At northern mid-latitudes the results are approximately the same.

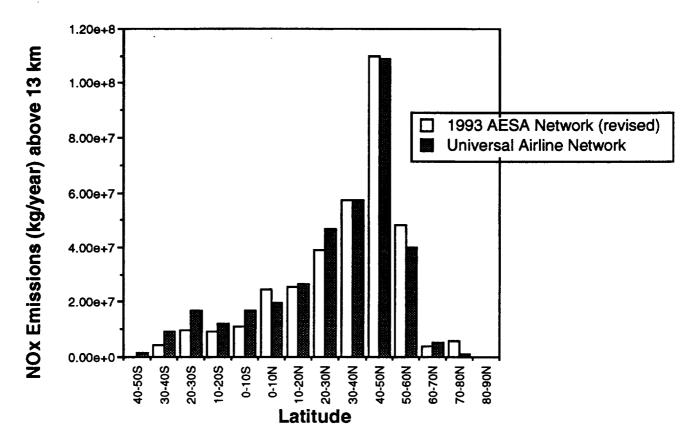


Figure 5-2. NOx emissions above 13 kilometers as a function of latitude, comparing the new universal airline scenario with the 1993 AESA assessment network scenario (revised) for 500 Mach 2.4 HSCTs.

Figure 5-3 shows the differences in fuel burned and NOx emissions at high resolution (1 degree latitude) as a function of latitude (summed over longitude). For these cases, the results are shown summed over all altitudes (the two top figures) and summed over altitudes above 13 km (bottom two figures). The high resolution plots illustrate that although there are systematic differences between the two networks in some latitude bands (e.g., the

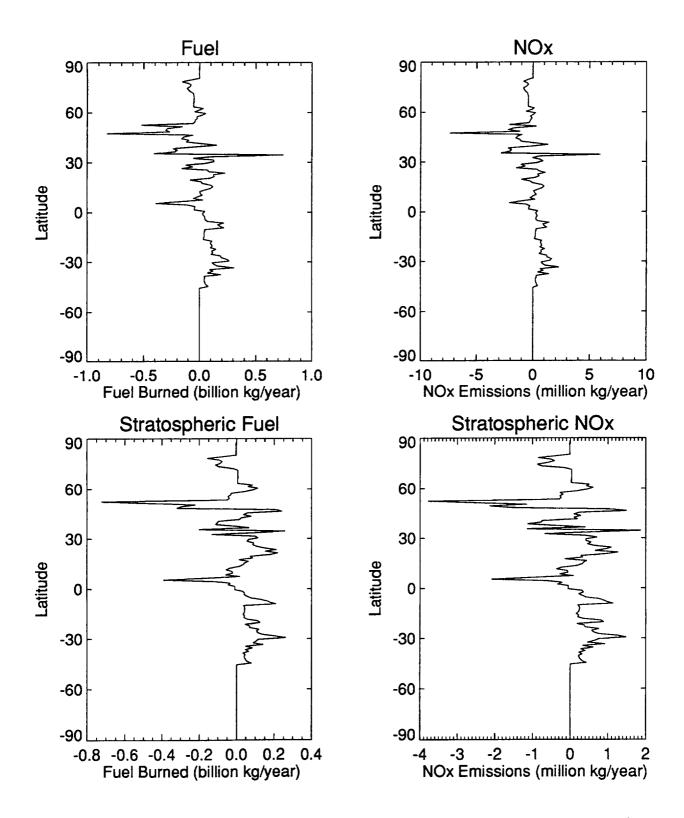
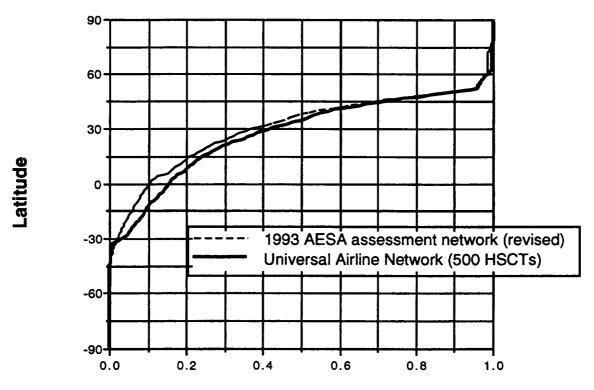


Figure 5-3. Differences in fuel burn and emissions between the new universal HSCT network and the 1993 AESA assessment network (revised) for a fleet of 500 Mach 2.4 HSCTs with EI(NOx) at cruise of approximately 5, plotted as a function of latitude. Stratospheric emissions here refer to emissions above 13 km.

Southern hemisphere), in other bands the differences are much more complicated (e.g., 30-40 North latitude).

Figure 5-4 shows the cumulative fraction of NOx emissions above 13 kilometers, emphasizing that in the new network about 15% of the stratospheric NOx emissions will occur in the southern hemisphere, compared to 10% for the old network. Most of the changes are an increase in stratospheric cruise occurring in the tropics. Since 2-D modeling calculations have indicated that HSCT emissions in the tropics may have greater impact on stratospheric ozone than for similar injections at mid-latitudes, these changes are worth noting for the AESA assessment calculations.



Cumulative Fraction NOx Emissions (above 13 km)

Figure 5-4. Cumulative fraction of NOx emissions above 13 km plotted as a function of latitude, comparing the results for the universal airline network with the revised 1993 AESA assessment network for the Mach 2.4 HSCT (EI(NOx)=5)).

5.2 Fleet Growth Effects

The effect of doubling the HSCT fleet from 500 to 1000 HSCTs on the universal airline network is summarized in Table 5-2. The global fuel use and emissions are projected to almost double with the fleet size.

 Table 5-2. Comparison of the fuel use and emissions between the 500 and 1000 aircraft HSCT fleets.

Mach 2.4 HSCT El(NOx)=5	Fuel (kg/year)	NOx (kg/year)	HC (kg/year)	CO (kg/year)
universal network (500 HSCTs)	8.21E+10	5.35E+08	2.97E+07	2.41E+08
universal network (1000 HSCTs)	1.57E+11	1.04E+09	5.88E+07	4.76E+08
difference (1000-2 x 500)	-7.52E+09	-3.11E+07	-5.25E+05	-7.09E+06
% difference (1000-2 x 500)	-4.58%	-2.91%	-0.88%	-1.47%

If we compare the NOx emissions injected at altitudes above 13 kilometers (Figure 5-5), it is clear that emissions in some latitude bands increase at different rates as the HSCT fleet is doubled.

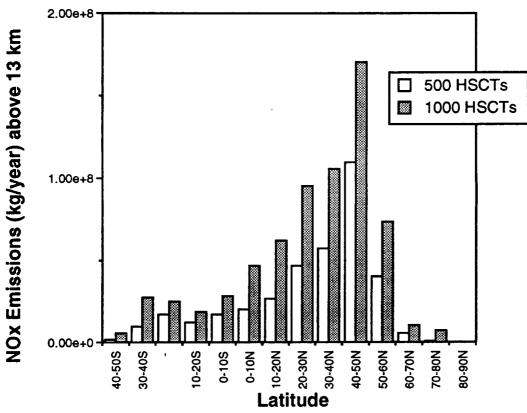
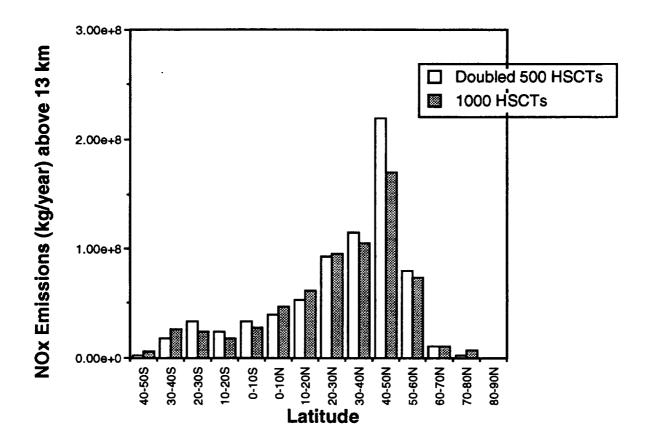
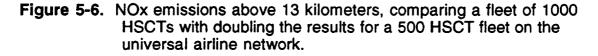


Figure 5-5. NOx emissions above 13 kilometers altitude as a function of latitude for 500 and 1000 Mach 2.4 HSCTs on the universal airline network.

To illustrate more clearly how the geographical distribution is modified as the fleet grows, Figure 5-6 shows the NOx emissions as a function of latitude for a fleet of 1000 Mach 2.4 HSCTs and compares them with the doubled emissions of the 500 HSCT fleet. In some regions (e.g., southern mid-latitudes, northern hemisphere tropics), the emissions have more than doubled compared with the 500 aircraft fleet; while in other regions (e.g., northern midlatitudes), the emissions have not grown linearly with the fleet size.





Although the emission in all latitude bands do not exactly double when the fleet size doubles, the differences are relatively small in most regions. To first order, for 2-dimensional model calculations, treating the fleet size as a scalar appears to be justified. Subtle effects due to transport processes in the tropics or 3-dimensional effects will need to be evaluated for their sensitivity. The scenarios developed here should be useful for that purpose.

As shown, simply doubling the number of airplanes flown may not accurately reflect the distribution of emissions. A higher resolution comparison of the 1000 and doubled 500 HSCT fleet is shown in Figure 5-7. The top panel

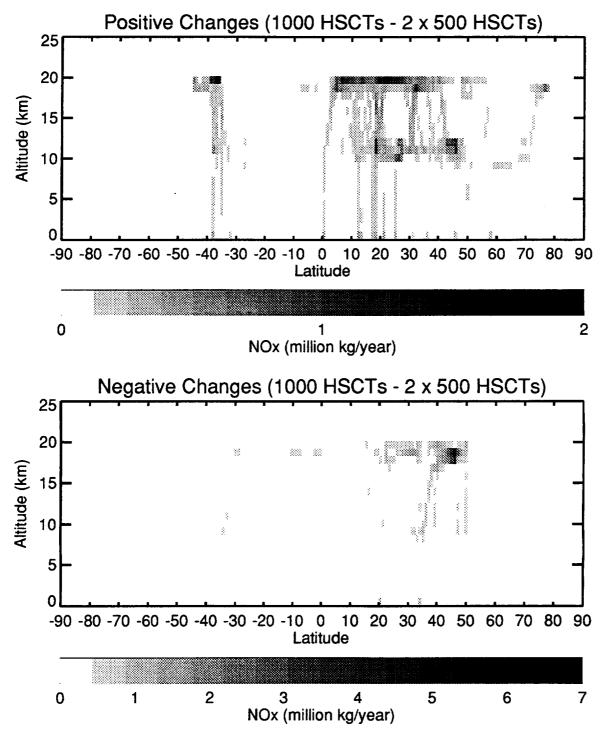


Figure 5-7. Comparison of NOx emissions from the 1000 HSCT fleet with emissions from doubling the 500 HSCT fleet on the universal airline network for Mach 2.4 [EI(NOx)=5] HSCTs. The top panel shows positive changes, while the bottom panel shows negative changes. (summed over longitude)

of Figure 5-7 shows the regions where the 1000 HSCT fleet has more than twice the emission levels of the 500 HSCT fleet. The bottom panel shows the locations where the emissions from the larger fleet are less than twice those of the smaller fleet. The bottom panel illustrates that flights in northern midlatitudes are projected to saturate and not increase linearly with fleet size. By contrast, emissions in the Southern hemisphere (particularly between 30-45° S latitude) and in the northern tropics (0-30° N latitude) are projected to increase faster than linear. In addition, emissions for the larger fleet at subsonic cruise altitudes would increase as new routes are added.

An increase of the fleet size from 500 to 1000 HSCTs would essentially double the total emissions from the HSCT fleet. However, as illustrated in Figure 5-7, the increase in fleet size shows growth in different geographical regions. As the fleet size increases, routes between new city pairs are introduced (see Appendix C).

Figure 5-8 shows the differences in fuel burned and NOx emissions as a function of latitude (summed over longitude) between the 1000 HSCT fleet and doubling the 500 HSCT fleet. The top two figures show the results considering all altitudes, while the bottom two figures consider only altitudes above 13 kilometers. For stratospheric NOx, emissions at southern mid-latitudes and the northern hemisphere tropics have grown faster than linear when the fleet increases from 500 to 1000 HSCTs, while northern mid-latitude emissions have increased at less than a linear rate.

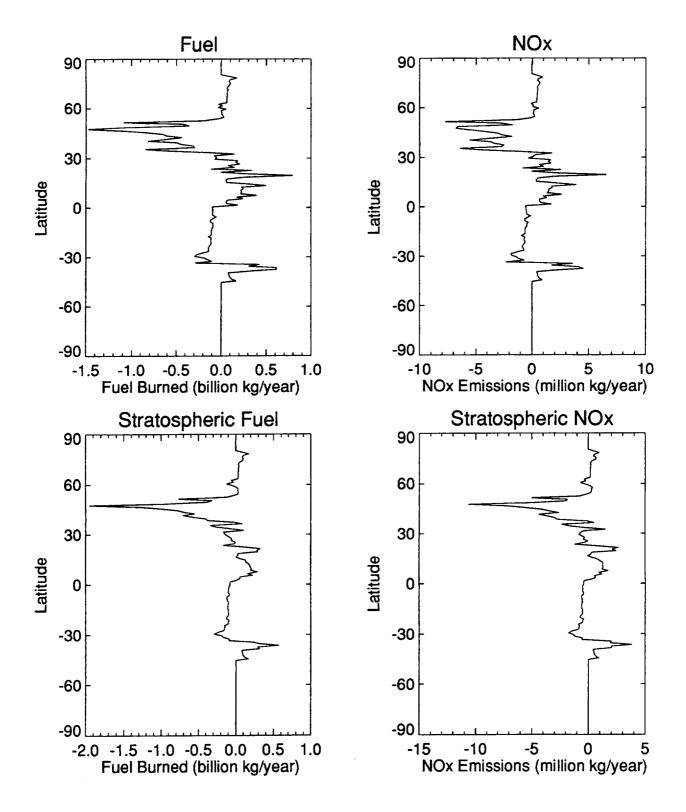
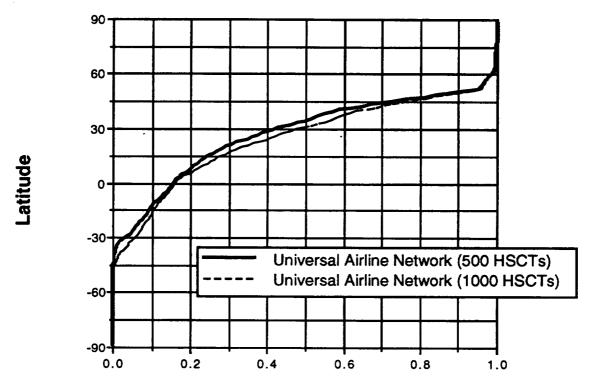


Figure 5-8. Differences in fuel burn and NOx emissions between 1000 HSCTs and simply doubling the 500 HSCT fleet, plotted as a function of latitude for the new universal HSCT network (Mach 2.4 HSCTs with EI(NOx) at cruise of approximately 5). Stratospheric emissions here refer to emissions above 13 km.

As shown in Figure 5-9, the relative partitioning of emissions between the northern and southern hemisphere is unchanged as the fleet doubles in size.



Cumulative Fraction NOx Emissions (above 13 km)

Figure 5-9. Cumulative fraction of stratospheric NOx emissions as a function of latitude for the 500 and 1000 HSCT fleets on the universal airline network.

5.3 Comparison of Fleet Growth Effects on 2015 Subsonic Emissions Inventory

The effect of a fleet of HSCTs on the subsonic fleet is summarized in Table 5-3. As discussed earlier, the corrections made to the P900 subsonic aircraft performance data files changed the global emissions by about 2%.

Not surprisingly, the fuel burn and emissions from the subsonic fleet decrease as more HSCTs are introduced into service. A fleet of HSCTs results in a drop of about 11% and 21% in total subsonic fleet fuel use for fleets of 500 and 1000 HSCTs, respectively, as HSCTs displace subsonic aircraft. The combined fuel use of subsonic and HSCT fleets will be discussed in Section 5.4.

Year 2015 Subsonic Passenger fleet	Fuel (kg/year)	NOx (kg/year)	HC (kg/year)	CO (kg/year)
No HSCT fleet exists (Baughcum, <i>et. al.</i> , 1994)	2.45E+11	2.24E+09	9.20E+07	1.09E+09
No HSCT fleet exists (revised)	2.50E+11	2.32E+09	9.94E+07	1.11E+09
In the presence of 500 M2.4 HSCTs (universal network)	2.22E+11	2.05E+09	9.34E+07	1.05E+09
In the presence of 1000 M2.4 HSCTs (universal network)	1.97E+11	1.80E+09	8.71E+07	9.78E+08

 Table 5-3. Comparison of the fuel use and emissions for the subsonic scheduled passenger fleets with and without the HSCT fleets

5.4 Total 2015 Scheduled Aircraft Emissions for Fleets of 0, 500, and 1000 HSCTs

The total global emissions for all projected scheduled air traffic scenarios for 2015 are summarized in Table 5-4. Since the HSCT uses more fuel on a per passenger mile basis than do subsonic aircraft, global jet fuel use is greater for the scenarios in which HSCTs are included in the projections. Fuel usage by scheduled passenger traffic in 2015 with a fleet of 500 HSCTs or 1000 HSCTs is projected to be 21% and 40% higher, respectively, compared to an all subsonic fleet.

These numbers shown in Table 5-4 include only air traffic due to scheduled subsonic passenger jets, cargo jets, turboprop aircraft, and HSCTs. They do not include charter traffic, military, or most of the projected air traffic in the former Soviet Union. As discussed in Chapter 2, the traffic forecasts for year 2015 are projected based on current air traffic schedules which do not include much of the internal air traffic within the former Soviet Union. Projections of charter, military, and former Soviet Union traffic have been done previously by McDonnell Douglas under contract to NASA. (Landau, *et. al.* 1994).

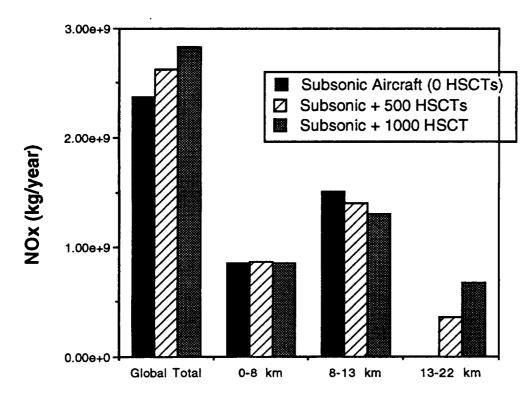
Comparisons of NOx emissions as a function of altitude for scheduled air traffic, with and without an HSCT fleet, were made in our previous work (Baughcum, *et. al.*, 1994) and will not be repeated here. The data necessary for such calculations is included in Appendices F, G, and H of this report.

	Fuel NOx HC			CO
	(kg/year)	(kg/year)	(kg/year)	(kg/year)
Total 2015 Scheduled Air Traffic without an HSCT fleet	2.56E+11	2.37E+09	1.03E+08	1.14E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.4 HSCT fleet (EI(NOx)=5) (universal network)	3.10E+11	2.63E+09	1.27E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.4 HSCT fleet (EI(NOx)=15) (universal network)	3.10E+11	3.58E+09	1.27E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.4 HSCT fleet (EI(NOx)=5) (universal network)	3.59E+11	2.89E+09	1.49E+08	1.48E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.4 HSCT fleet (EI(NOx)=15) (universal network)	3.59E+11	4.67E+09	1.49E+08	1.48E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.0 HSCT fleet (EI(NOx)=5) (universal network)	3.12E+11	2.60E+09	1.26E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.0 HSCT fleet (EI(NOx)=15) (universal network)	3.12E+11	3.57E+09	1.26E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.0 HSCT fleet (EI(NOx)=5) (universal network)	3.62E+11	2.82E+09	1.47E+08	1.48E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.0 HSCT fleet (EI(NOx)=15) (universal network)	3.62E+11	4.67E+09	1.47E+08	1.48E+09

Table 5-4. Summary of fuel use, NOx, hydrocarbons, and carbon monoxide for the total scheduled air traffic scenarios for 2015

Note: NOx is given as gram equivalent NO₂

An evaluation of the effects of aircraft on the upper troposphere is one aspect of the NASA Atmospheric Effects of Aviation Project (AEAP). Based on these scenarios, the introduction of a fleet of Mach 2.4 (EI(NOx)=5) HSCTs would, change the NOx emissions due to aircraft at altitudes below 13 kilometers from 2.37 x 10^{10} kilograms/year to 2.27 x 10^{10} kilograms/year (-4%) for 500 HSCTs or to 2.15 x 10^{10} kilograms/year (-9%) for 1000 HSCTs. It is clear that the emissions of NOx above 13 kilometers (into the stratosphere) would be much higher with an HSCT fleet than without. As shown in Figure 5-10, the introduction of a fleet of HSCTs would be expected to decrease the NOx emissions in the upper troposphere.



Altitude Band

Figure 5-10. Total projected NOx emissions from 2015 scheduled air traffic for different altitude bands for fleets of 0, 500, and 1000 Mach 2.4 HSCTs with EI(NOx) at supersonic cruise of approximately 5.

5.5 Conclusions

A detailed database of projected 2015 subsonic and HSCT (both Mach 2.0 and 2.4) operational scenarios was developed using a universal airline network with HSCT fleet sizes of 0, 500, and 1000 active HSCTs. Threedimensional data files of fuel burned and emissions (NOx, hydrocarbons, and carbon monoxide) on a 1° latitude x 1° longitude x 1 km altitude grid were calculated and delivered electronically to the Upper Atmospheric Data Program (UADP) system at the NASA Langley Research Center.

The work presented here shows that although the total global fuel burned and emissions from a fleet of 500 HSCTs is not very sensitive to whether the universal airline or the 1993 AESA assessment network is used, the geographical distribution of emissions at stratospheric cruise is sensitive to the market penetration assumptions used to distribute projected HSCT passenger demand.

An increase in HSCT fleet size from 500 to 1000 units has been shown to approximately double emissions at stratospheric cruise. However, as the fleet grows, emissions in different geographical regions grow at different rates. Consequently, stratospheric emissions in northern mid-latitudes are not projected to double as the fleet size doubles, while emissions in the northern tropics and southern hemisphere mid-latitudes are expected to more than double.

For an HSCT combustor with a NOx emission index of 5, the analyses show that the total NOx emissions below 13 kilometers altitude are not very sensitive to the presence or absence of an HSCT fleet. This suggests that to first-order the assessment of the effects of an HSCT fleet are largely decoupled from the assessment of subsonic aircraft effects. In some geographical regions, however, the changes may be greater (e.g., the North Atlantic).

The aircraft emissions inventories for scheduled air traffic developed in this study have been combined at NASA Langley with results for non-OAG scheduled operations (charter, military, and internal former Soviet Union) to create inventories of total aircraft emissions in the year 2015. These inventories are being used by the NASA Atmospheric Effects of Aviation Project (AEAP) in the 1995 AESA assessment of HSCT ozone impact.

5.6 Database Availability

The inventories of jet fuel burned and emissions (NOx, CO, total hydrocarbons) have been calculated for projected subsonic and HSCT fleets for the year 2015. These data will be available on a 1 degree latitude x 1 degree longitude x 1 km altitude grid by contacting Karen H. Sage (sage@uadp2.larc.nasa.gov) at NASA Langley Research Center or by sending a request to the Atmospheric Sciences Division, NASA Langley Research Center, Hampton, VA 23681-0001.

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WORLD PASSENGER TRAFFIC FORECAST RPMs IN MILLIONS	IC FORECA	ST		Crowd h		drough		Growth	-	Growth		Average Growth
Year Regional Flow	1991 1	Rate 1991-1995	1995 1	Rate 1995-2000	2000	Rate 2000-2005	2005 21	Rate 2005-2010	2010 20	Rate 2010-2015	2015	Rate 1991-2015
Intra & Domestic N. America	358,741	4.87%	433,867	4.66%	544,736	3.94%	660,974	3.51%	785,276	3.25%	921,565	4.01%
N. America-Europe	121,400	6.56%	156,540	5.36%	203,233	4.42%	252,344	4.06%	307,900	3.86%	372,129	4.78%
N. America-Asia/Pacific	87,065	7.94%	118,193	7.71%	171,327	7.07%	241,051	6.54%	330,855	6.11%	445,013	7.03%
Other N. America	3,565	5.50%	4,416	4.39%	5,474	3.96%	6,645	3.54%	7,907	3.31%	9,306	4.08%
N. America-Latin America	36,476	4.91%	44,191	5.91%	58,876	5.48%	76,883	4.92%	97,742	4.72%	123,092	5.20%
Intra & Domestic Europe	148,216	6.20%	188,512	5.04%	241,004	4.41%	299,023	4.15%	366,412	3.63%	437,999	4.62%
Europe-Asia/Pacific	46,430	12.34%	73,938	8.40%	110,684	7.53%	159,139	6.69%	219,963	6.24%	297,690	8.05%
Europe-Indian Sub Continent	9,718	2.08%	10,552	4.16%	12,938	3.74%	15,545	3.78%	18,713	3.64%	22,376	3.54%
Europe-Mid East	19,578	8.26%	26,897	4.94%	34,231	4.58%	42,821	4.22%	52,652	4.03%	64,163	5.07%
Europe-Africa	25,811	3.79%	29,950	5.57%	39,271	4.62%	49,215	4.32%	60,816	3.96%	73,850	4.48%
Europe-Latin America	26,869	8.11%	36,700	5.38%	47,689	4.78%	60,236	4.59%	75,387	4.43%	93,627	5.34%
Intra & Domestic Aisa/Pacific	86,003	8.92%	121,034	8.85%	184,989	7.93%	270,878	7.45%	388,063	6.65%	535,482	7.92%
Misc Long Range	40,348	3.99%	47,179	7.04%	66,288	6.05%	88,926	5.74%	117,570	5.37%	152,698	5.70%
Japan	33,773	5.26%	41,455	4.40%	51,413	4.22%	63,217	3.78%	76,119	3.39%	89,918	4.16%
Intra & Dom Indian Sub Continent	6,779	9.41%	9,714	5.54%	12,722	5.17%	16,367	4.95%	20,839	4.78%	26,316	5.81%
Other Indian Subcontinent	14,261	6.65%	18,449	4.69%	23,204	4.46%	28,858	4.25%	35,534	4.11%	43,461	4.75%
Intra & Domestic Mid East/Africa	18,455	8.00%	25,107	4.91%	31,904	4.43%	39,627	4.27%	48,849	4.09%	59,695	5.01%
Other African	8,002	11.33%	12,291	4.75%	15,500	4.28%	19,110	4.02%	23,276	3.88%	28,163	5.38%
Intra & Domestic Latin America	27,023	7.61%	36,239	5.25%	46,811	4.82%	59,232	4.63%	74,275	4.48%	92,463	5.26%
CIS International	13,842	-6.10%	10,761	7.14%	15,191	6.23%	20,555	5.18%	26,458	4.58%	33,098	3.70%
MAC Charter	5,657	-7.56%	4,131	-3.00%	3,547	-1.20%	3,339	-0.90%	3,191	0.00%	3,191	-2.36%
	1,138,012		1,450,116	5.79%	1,921,030	5.19%	2,473,985	4.87%	3,137,799	4.58%	3,925,296	5.29%

Appendix A - World Passenger Demand Forecast

Appendix	B	-	нѕст	Route	System	Gateway	Cities	

City	City	City	City
Code	Name	Code	Name
ACA	Acapulco, Mexico	MIA	Miami, Florida, USA
AKL	Auckland, New Zealand	MIL	Milan, Italy
AMS	Amsterdam, The Netherlands	MNL	Manila, Philippines
ANC	Anchorage, Alaska, USA	MOW	Moscow, Russian Republic
ATH	Athens, Greece	MRU	Mauritius, Mauritius
ATL	Atlanta, Georgia, USA	MSP	Minneapolis-St, Paul, Minnesota, USA
BAH	Bahrain, Bahrain	MUC	Munich, Germany
BER	Berlin, Germany	NAN	Nandi, Fiji
BKK	Bangkok, Thailand	NYC	New York, New York, USA
BOG	Bogota, Columbia	OSA	Osaka, Japan
BOM	Bombay, India	OSL	Oslo, Norway
BOS	Boston, Massachusetts, USA	PAR	Paris, France
BRU	Brussels, Belgium	PEK	Beijing, China
BUE	Buenos Aires, Argentina	PER	Perth, Autralia
CAI	Cairo, Egypt	PHL	Philadelphia, Pennsylvania, USA
CAN	Guangzhou, China	PPT	Papeete, Tahiti, French Polynesia
ccs	Caracas, Venezuela	PTY	Panama City, Panama
CHI	Chicago, Illinois, USA	RIO	Rio de Janeiro, Brasil
CMB	Colombo, Sri Lanka	ROM	Rome, Italy
СРН	Copenhagen, Denmark	SCL	Santiago, Chile
CVG	Cincinnati, Ohio, USA	SEA	Seattle, Washington, USA
DEL	Delhi, India	SEL	Seoul, Korea
DFW	Dallas, Texas, USA	SFO	San Francisco, California, USA
DHA	Dharan, Saudia Arabia	SHA	Shanghai, China
DKR	Dakar, Senegal	SIN	Singapore, Singapore
DTW	Detroit, Michigan, USA	SJU	San Juan, Puerto Rico
FDF	Fort-de-France, Martinique	SNN	Shannon, Ireland
FRA	Frankfurt, Germany	STL	Saint Louis, Missouri, USA
GUM	Guam, Guam	STO	Stockholm, Sweden
GVA	Geneva, Switzerland	SYD	Sydney, Australia
HAV	Havana, Cuba	TLV	Tel Aviv, Israel
HEL	Helsinki, Finland	TPE	Taipei, Taiwan
HKG	Hong Kong, Hong Kong	TYO	Tokyo, Japan
HNL	Honolulu, Hawaii, USA	VIE	Vienna, Austria
HOU	Houston, Texas, USA	WAS	Washington, DC, USA
JKT	Jakarta, Indonesia	WAW	Warsaw, Poland
JNB	Johannesburg, South Africa	YHZ	Halifax, Nova Scotia, Canada
KHI	Karachi, Pakistan	YMQ	Montreal, Quebec, Canada
KHV	Khabarovsk, Russian Federation	YVR	Vancouver, British Columbia, Canada
LAX	Los Angeles, California, USA	YYC	Calgary, Alberta, Canada
LIM	Lima, Peru	YYZ	Toronto, Ontario, Canada
LIS	Losbon, Portugal		
LON	London, England, UK		
MAD	Madrid, Spain		
MEL	Melbourne, Australia		
MEX	Mexico City, Mexico		
MEX	Mexico City, Mexico	_]	

Appendix C. Departure Statistics

This appendix is a table of departure statistics for the universal network for a fleets of 500 and 1000 active Mach 2.4 HSCTs. For each gateway citypair, flight distances for the great circle route, supersonic flight legs, and total path length are given in nautical miles. Stops enroute are identified in the column marked via. Block time and total trip times are given in hours with the fraction of time compared to an all subsonic flight. Daily departures and load factors are shown for both fleets of 500 and 1000 HSCTs. The first section of the table shows city pairs used by the 500 unit fleet, while the second section includes flights used only by the 1000 unit fleet.

	Load Factor	67	99	67	8 9	65	63	65	68	67	83	68	67	99	67	67	63	67	67	61	67	67	67	67	67	61	67	64	67	67	67	67
1000 Units	Departures		26	3	20	4	24	24	60	4	80	Ø	9	16	4	4	10	2	4	20	4	9	4	2	10	14	4	10	2	12	2	4
	Load Factor	61	9 9	67	88	67	63	9 9	68	67	67	68	67	64	67	67	67	65	67	62	67	67	67	67	<u>9</u> 9	62	61	67	67	62	67	60
500 Units	Daily Departures	4	22	8	16	0	14	10	80	4	9	4	4	14	8	2	4	8	2	12	2	4	7	8	Ø	9	4	9	0	10	8	4
	Percent subsonic	09	43	46	57	43	49	47	56	44	43	54	51	46	61	59	59	47	56	50	57	60	58	50	48	57	53	52	51	48	49	54
(s	Trin	6.45	3.58	4.19	6.96	4.53	3.14	2.39	6.86	4.38	4.43	7.10	4.31	4.26	4.85	5.53	4.46	4.13	4.50	3.52	3.78	5.45	4.14	4.77	4.26	5.31	4.73	4.59	4.50	3.87	4.05	4.91
Time (hours)	Block	5.45	3.58	4.19	5.96	4.53	3.14	2.39	5.86	4.38	4.43	6.10	4.31	4.26	4.85	5.53	4.46	4.13	4.50	3.52	3.78	5.45	4.14	4.77	4.26	5.31	4.73	4.59	4.50	3.87	4.05	4.91
	Dath	5085	3825	4530	6042	4833	3236	2210	5907	4833	4766	6174	4001	4232	3876	4630	3672	4038	4017	3247	3347	4483	3517	4892	4234	4317	4415	4214	4135	3806	3848	4340
(n.m.)	Cruisa	3757	3165	3751	4817	3936	2614	1635	4691	4055	3918	4913	2844	3239	2214	2819	2218	3048	2716	2325	2267	2661	2238	3835	3244	2520	3141	2948	2898	2906	2826	2879
Distance (n.m.)	55	4937	3826	4123	5659	4834	2879	2209	5671	4541	4768	6130	3812	4230	3567	4262	3412	4015	3607	3155	2972	4160	3232	4397	4057	4273	4089	3997	4005	3648	3756	4155
	Via																															
	Via	MOd			HNL				HNL			HNL																				
	Dest	HKG E	HNL	JKT	LAX	OSA	PER	Ърт	SFO	SIN	1Y0	YVR	ATL	ccs	Œ	DFW	DTW	MIA	MSP	NVC	YMQ	YVR	ZYY	HKG	TPE	NYC	BER	FRA	GVA	LON	MAD	MUC
	Origin	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AMS	ANC	ANC	ATH	ATL	ATL	ATL	ATL	ATL	ATL										

	Load	Factor	67	67	61	65	67	99	67	63	67	62	67	67	63	67	67	67	67	63	66	67	61	67	67	62	67	67	61	62	67	99	67
1000 Units	Daily	Departures	2	8	16	22	9	9	8	26	8	9	8	4	16	4	8	24	9	22	50	8	12	2	4	24	Ø	4	4	18	8	4	4
	Load	Factor	67	67	67	67	67	67	67	62	65	67	67	67	61	67	62	67	67	67	65	62	67	67	67	62	67	67	67	67	67	67	67
500 Units	Daily	Departures	2	2	4	2	8	4	9	16	0	2	7	4	10	2	7	9	0	7	20	7	7	7	2	14	4	0	8	9	8	2	4
	Percent	subsonic	50	48	62	62	64	53	56	54	55	65	62	48	54	55	61	59	58	62	54	50	54	52	51	47	49	47	60	48	49	55	57
ırs)		Trip ^s	4.18	3.55	4.03	2.93	4.92	4.46	4.89	4.10	4.04	5.46	6.15	4.54	4.13	4.41	5.78	3.05	3.79	2.87	3.10	4.79	2.62	3.66	3.62	2.99	3.31	2.67	4.74	3.41	3.69	3.67	7.41
Time (hours)		Block	4.18	3.55	4.03	2.93	4.92	4.46	4.89	4.10	4.04	5.46	6.15	4.54	4.13	4.41	5.78	3.05	3.79	2.87	3.10	4.79	2.62	3.66	3.62	2.99	3.31	2.67	4.74	3.41	3.69	3.67	6.41
		Path	3965	3476	3460	2093	4743	3861	4671	3663	3444	4189	4943	4440	3559	3748	4670	3009	3077	2783	3111	4334	2545	3286	3270	2937	3100	2607	3868	3239	3428	3339	6525
(n.m.)		Cruise	2897	2656	2239	1008	3484	2515	3407	2501	2202	2202	2803	3333	2312	2379	2681	2343	1844	2137	2459	2971	1965	2270	2275	2275	2271	2021	2289	2401	2467	2343	5207
Distance (n.m.)		GC	3806	3327	2893	2024	3449	3801	3976	3412	3274	3820	4517	4311	3436	3627	4306	2259	2889	1989	2505	4333	2110	3177	3185	2827	2985	2506	3602	3176	3370	3000	6009
		Via																															
		Via																															DKR
		Dest	PAR	SNN	BKK	CMB	HKG	JKT	MNL	SIN	BOS	CHI	DFW	MIA	NYC	WAS	YVR	OSA	PER	SEL	ΤYΟ	MAD	SIN	FRA	GVA	LON	PAR	SNN	CHI	NYC	WAS	γMQ	LON
		Origin	ATL	ATL	BAH	BAH	BAH	BAH	BAH	BAH	BER	BKK	BKK	BKK	BKK	BOG	BOM	BOS	BOS	BOS	BOS	BOS	BRU	BRU	BRU	BRU	BUE						

	Load	Factor	8	67	67	67	67	67	65	67	62	61	67	63	67	62	99	65	67	67	67	67	67	67	61	67	67	67	65	62	67	68	67
1000 Units	Daily	Departures	20	80	4	4	4	2	14	2	20	9	8	12	9	10	26	9	12	æ	7	24	80	8	4	2	8	9	12	4	9	18	4
	Load	Factor	67	67	67	67	67	67	67	67	67	67	67	67	09	67	67	09	67	67	8	67	67	63	67	67	67	67	67	67	67	89	67
500 Units	Daily	Departures	12	8	4	8	2	8	10	7	4	4	8	9	4	4	14	4	4	4	2	80	9	8	8	8	0	8	æ	~	4	12	8
	Percent	subsonic	61	58	57	47	43	43	46	46	49	45	53	61	09	66	58	59	70	59	60	69	45	60	57	53	59	59	56	56	58	67	53
rs)		Trip	7.14	7.55	7.65	4.48	3.34	3.82	3.80	4.41	2.13	4.06	5.17	5.08	5.04	5.34	4.41	5.13	8.45	4.72	5.53	8.18	3.32	5.56	4.71	4.04	5.76	4.32	5.09	5.27	5.40	10.69	4.49
Time (hours)		Block	6.14	6.55	6.65	4.48	3.34	3.82	3.80	4.41	2.13	4.06	5.17	5.08	5.04	5.34	4.41	5.13	7.45	4.72	5.53	7.18	3.32	5.56	4.71	4.04	5.76	4.32	5.09	5.27	5.40	8.69	4.49
		Path	5870	6549	6652	4359	3509	4073	3781	4348	1897	4109	4498	4030	4014	3680	3681	4178	5959	3844	4364	5636	3480	4592	3911	3562	4784	3282	4435	4477	4594	6772	3880
(n.m.)		Cruise	4401	5126	5180	3262	2878	3354	2925	3297	1359	3213	2906	2269	2274	1508	2274	2456	3667	2271	2415	3397	2849	2738	2384	2389	2871	1725	2880	2803	2871	4058	2514
Distance (n.m.)		GC	5441	5989	6282	4357	3508	4031	3780	4347	1837	4118	4497	3761	3806	3678	3423	3922	5614	3595	4176	5435	3339	4214	3777	3432	4455	3280	4115	4303	4286	6691	3824
_		Via																														0XT	
		Via	DKR	DKR	1 <u>7</u> 0														SEA			SEA										SEA	
		Dest	MAD	PAR	LAX	FRA	LIS	LON	MAD	MIL	NYC	PAR	ROM	FRA	GVA	HNL	LON	MUC	OSA	PAR	ROM	TYΟ	NYC	SEA	FRA	LON	FRA	HNL	LON	MAD	PAR	TPE	JKT
		Origin	BUE	BUE	CAN	ccs	ccs	ccs	ccs	ccs	ccs	ccs	ccs	Ē	CHI	CHI	CHI	CHI	EHI	EHI	E	CHI	СРН	CPH	CVG	CVG	DFW	DFW	DFW	DFW	DFW	DFW	DHA

	Load	Factor	61	67	60	67	67	67	67	60	65	67	65	63	67	67	62	65	99	62	64	53	63	61	65	60	64	61	68	67	67	68	68
1000 Units	Daily	Departures	10	8	4	8	8	4	12	14	28	4	8	32	8	8	4	9	2	9	18	4	36	16	8	9	9	20	68	4	4	4	28
	Load	Factor	67	67	67	63	67	67	62	67	63	67	67	99	67	67	64	9 9	62	. 29	62	99	6 6	64	67	67	67	67	68	67	61	68	68
500 Units	Daily	Departures	9	2	2	2	2	2	10	80	22	2	9	20	2	9	2	4	7	0	14	2	7	10	4	2	4	4	60	7	4	4	24
	Percent	subsonic	56	54	43	59	54	49	44	47	46	57	48	50	50	51	57	60	57	57	43	46	52	50	56	52	42	49	56	54	46	58	56
Irs)		Trip	4.92	4.13	3.48	4.68	4.13	4.17	3.52	3.49	3.76	5.67	4.40	3.74	3.83	4.02	4.01	5.74	5.05	4.37	3.18	2.99	1.74	3.71	3.98	4.13	4.37	2.04	7.54	4.78	3.37	7.02	7.20
Time (hours)		Block	4.92	4.13	3.48	4.68	4.13	4.17	3.52	3.49	3.76	5.67	4.40	3.74	3.83	4.02	4.01	5.74	5.05	4.37	3.18	2.99	1.74	3.71	3.98	4.13	4.37	2.04	6.54	4.78	3.37	6.02	6.20
		Path	4690	3682	3692	3826	3615	3948	3635	3359	3699	4786	4239	3401	3476	3590	3502	4675	4345	3671	3298	3058	1356	3385	3483	3742	4842	1782	6591	4912	3545	6010	6306
(n.m.)		Cruise	3406	2500	3043	2273	2396	2878	2922	2523	2826	2949	3140	2380	2427	2447	2323	2719	2776	2293	2679	2461	829	2385	2314	2590	4075	1245	5175	3857	2908	4713	5022
Distance (n.m.)		S	4001	3436	3691	3603	3430	3909	3590	3313	3668	4545	4188	3339	3420	3534	3161	4351	4062	3422	3296	2869	1358	3346	3191	3565	4812	1761	6283	3992	3256	5625	5994
		Via																															
		Via																											ΤYO			TΥO	TYO
		Dest	MNL	SIN	HAV	FRA	PAR	FRA	LON	MAD	PAR	NOH	MIA	NVC	PHL	WAS	YMQ	YVR	YYC	ZYY	HNL	SYD	TYΟ	NYC	YMQ	NYC	HNL	JKT	LAX	MEL	PER	SEA	SFO
		Origin	DHA	DHA	DKR	DTW	DTW	FDF	FOF	FDF	FDF	FRA	FRA	FRA	GUM	GUM	GUM	GVA	GVA	ΗËL	HKG												

	Daily Load	es Factor	94 67	14 65	80 64	40 68	4 67	8 68	84 66	65 65	22 62	68 65	16 63	12 67	16 66	36 64	6 61	24 63	4 61	124 66	10 61	8 66	4 67	6 67	4 67	18 62	12 67	12 64	24 65	2 67	4 67	
1000 Units	Da	Departures										-								Ŧ												
	Load	Factor	09	61	49	67	67	67	63	58	61	9 9	62	67	67	64	67	64	67	99	99 90	67	67	67	67	65	67	67	65	67	67	ë
500 Units	Daily	Departures	10	12	9	32	0	4	36	9	20	52	80	4	12	14	2	20	8	06	4	9	8	4	3	Ø	4	Ø	18	0	4	
	Percent	subsonic	52	47	56	59	58	55	47	45	42	44	46	47	48	47	65	42	42	44	47	54	55	48	46	26	50	45	51	47	63	
urs)		Trip	1.75	4.12	2.12	7.08	4.37	6.93	2.38	4.68	4.20	3.49	2.49	2.50	4.15	2.28	5.12	4.03	4.04	3.26	2.52	4.95	5.26	3.13	2.95	3.76	2.37	3.18	4.35	4.77	8.08	
Time (hours)		Block	1.75	4.12	2.12	6.08	4.37	5.93	2.38	4.68	4.20	3.49	2.49	2.50	4.15	2.28	5.12	4.03	4.04	3.26	2.52	4.95	5.26	3.13	2.95	3.76	2.37	3.18	4.35	4.77	7.08	
		Path	1397	4532	1865	5835	3391	6000	2217	4799	4599	3567	2383	2325	4440	2082	3581	4419	4395	3312	2349	4377	4536	3183	2957	3997	2126	3285	3859	4729	7173	1.4 6 4
(.m.n)		Cruise	879	3810	1316	4548	1852	4786	1652	3764	3845	2846	1822	1723	3651	1525	1530	3707	3670	2634	1747	2908	2898	2541	2337	3291	1516	2657	2599	3585	5659	0.960
Distance (n.m.)		GC	1392	3981	1585	5533	3396	5825	2216	4789	4597	3557	2383	2324	3950	2080	3579	4409	4394	3311	2347	4200	4365	2940	2849	2968	2053	3145	3859	4666	5948	17.77
		Via																														
		Via				TγO		GUM																							PER	
		- 1																										TYO				
		Origin	HKG	HKG	HKG	HKG	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	HNL	NOH	NOH	JKT	JKT	JKT	JKT	JKT	JNB	SNB	2NB	IAX

	Load	Factor	68	67	99	67	62	67	68	68	67	63	64	67	66	60	64	61	65	60	67	67	67	67	67	63	62	64	67	61	60	62	62
1000 Units	Daily	Departures	4	2	44	4	8	52	8	48	44	99	18	4	10	12	26	9	80	9	80	9	10	4	9	12	40	26	Ø	Ø	æ	28	10
	Load	Factor	88	67	64	67	65	67	68	68	9 9	64	09	67	67	62	61	67	99	99	67	67	67	67	62	67	67	62	67	67	67	67	67
500 Units	Daily	Departures	4	8	40	4	9	32	4	48	40	58	80	2	9	10	22	2	50	9	4	4	9	2	4	9	12	18	4	4	4	14	80
	Percent	subsonic	54	42	46	63	43	63	47	48	55	43	58	55	45	44	44	58	46	46	60	60	63	44	57	60	68	47	53	60	56	54	49
Jrs)		Trip	7.41	4.36	4.95	7.43	3.39	7.10	8.32	7.41	7.04	4.43	3.03	3.87	2.93	4.02	3.69	4.45	3.08	3.16	6.55	5.47	6.38	3.51	4.59	12.53	7.63	3.35	3.34	5.40	4.71	3.70	5.17
Time (hours)		Block	6.41	4.36	4.95	6.43	3.39	6.10	7.32	6.41	6.04	4.43	3.03	3.87	2.93	4.02	3.69	4.45	3.08	3.16	5.55	5.47	6.38	3.51	4.59	10.53	6.63	3.35	3.34	5.40	4.71	3.70	5.17
		Path	6372	4799	4957	6373	3567	5390	7626	6636	5913	4726	2402	3379	2916	4336	3843	3857	3052	3127	5376	4376	4851	3634	3824	9860	5560	3241	3153	4323	3994	3322	4893
(n.m.)		Cruise	4942	4019	3790	4929	2929	3859	6159	5359	4520	3859	1167	1710	2291	3594	3111	2511	2386	2432	4127	2479	2468	2930	2343	7181	3519	2452	2327	2458	2513	2298	3203
Distance (n.m.)		GC	6335	4798	4956	5416	3566	5178	7612	6508	5894	4724	2276	3164	2915	4163	3835	3476	2989	3070	4993	4156	4649	3633	3638	9184	5175	3184	2817	4090	3786	3079	4892
		Via																								GUM							
		Via	TYΟ			Tγo		TΥO	ΟΫ́	HNL	TYO										DKR					gDX	GDX						
		Dest	MNL	NAN	OSA	PEK	РРТ	SEL	SIN	SYD	TPE	ΤYΟ	MIA	NYC	NVC	RIO	MIA	MSP	NYC	РНГ	RIO	SEA	SFO	SJU	STL	SYD	ΤYO	WAS	YMQ	YVR	ΥΥC	ZYY	MEX
		Origin	LAX	LAX	LIM	LIM	LIS	LIS	LON	LON	LON	ron	LON	LON	LON	ron	LON	LON	LON	LON	LON	LON	LON	LON	MAD								

			Distance (n.m.)) (n.m.)		Time (hours)	(s		500 Units		1000 Units	
								Percent	Daily	Load	Daily	Load
Dest V	Via	Via	GC	Cruise	Path	Block	Trip	subsonic	Departures	Factor	Departures	Factor
MIA			3835	2993	3836	3.82	3.82	45	4	67	9	67
NYC			3109	2327	3124	3.28	3.28	47	10	67	18	8
RIO			4396	3594	4592	4.50	4.50	47	10	67	12	65
Ŋ			3306	2394	3313	3.56	3.56	48	8	67	2	67
4			4378	3733	4808	4.74	4.74	49	8	67	2	67
F			3614	2788	3614	3.65	3.65	46	9	<u>66</u>	æ	65
	HNL		6828	5289	6881	6.96	7.96	49	4	68	4	68
7			3258	3652	4679	4.59	4.59	63	9	61	14	65
0			4412	3717	4763	4.67	4.67	48	4	67	9	99
<u>с</u>			4339	3071	4364	4.72	4.72	50	4	9 9	4	67
PAR			3976	3090	3989	3.99	3.99	46	9	. 64	9	9 9
0			3624	3983	4781	4.38	4.38	55	12	67	20	65
M			4493	3232	4495	4.77	4.77	49	4	62	4	67
ч.			3592	2983	3689	3.55	3.55	45	4	67	9	67
ç			3459	2542	3529	3.79	3.79	49	14	65	20	99
AS			3656	2607	3718	4.07	4.07	50	7	61	8	67
õ			3380	3196	3920	3.73	3.73	50	2	67	4	64
0			1645	1083	1646	1.98	1.98	51	4	99	24	99
Q			4036	2573	4207	5.03	5.03	. 57		62	9	61
ų			3496	2569	3549	3.79	3.79	49	12	61	16	65
AS			3691	2635	3738	4.07	4.07	50	8	67	4	67
æ			4501	2679	4828	6.08	6.08	62	8	65	8	. 67
			4216	2736	4499	5.39	5.39	58	2	62	8	67
	ANC		8068	7057	9143	80 [.] 6	10.08	49	4	67	4	67
	Ā		5996	3667	6566	8.62	9.62	74	4	67	20	67
ц Ц			3192	2610	3340	3.35	3.35	47	8	67	4	67
œ			3147	2382	3215	3.39	3.39	48	28	63	42	99
ROM			3704	2548	3739	4.18	4.18	51	14	67	20	67
SIN S	SEA	ТХО	8276	5697	9143	11.24	13.24	69	9	68	9	89
SJU			1386	870	1391	1.75	1.75	52	4	67	56	65

	Load	Factor	67	68	65	99	67	63	62	67	99	67	67	67	67	63	67	67	99	67	63	67	65	67	65	67	64	67	67	60	67	67	68
1000 Units	Daily	Departures	9	12	36	Ø	8	14	18	46	12	æ	8	4	16	4	16	12	18	80	9	4	32	80	12	8	4	9	4	18	æ	12	20
	Load	Factor	67	67	67	67	67	65	62	64	67	67	67	67	67	67	67	67	61	67	67	64	64	67	67	62	67	<u>66</u>	67	65	67	67	68
500 Units	Daily	Departures	4	4	4	4	2	12	16	26	1	9	2	4	80	0	4	Ø	10	4	2	4	24	4	9	8	2	0	4	16	4	9	16
	Percent	subsonic	50	6 6	74	55	46	44	43	47	44	45	46	51	62	62	68	49	55	53	53	51	43	60	62	52	57	44	57	43	42	47	53
Jrs)		Trip ^{\$}	3.75	7.02	9.35	4.49	3.78	4.18	4.35	2.84	4.08	4.24	3.28	9.91	6.70	6.50	7.74	3.67	3.65	3.81	2.94	4.82	3.18	6.68	14.20	4.48	4.80	4.30	6.52	3.90	4.48	2.66	7.31
Time (hours)		Block	3.75	6.02	8.35	4.49	3.78	4.18	4.35	2.84	4.08	4.24	3.28	8.91	5.70	6.50	6.74	3.67	3.65	3.81	2.94	4.82	3.18	5.68	12.20	4.48	4.80	4.30	5.52	3.90	4.48	2.66	6.31
		Path	3548	5113	6243	3779	3840	4468	4756	2797	4428	4393	3264	8795	5400	4988	5716	3404	3316	3459	2919	4287	3303	5664	10879	3924	4010	4602	5332	4145	4904	2571	6501
(n.m.)		Cruise	2600	3331	3397	2359	3032	3667	3965	2183	3684	3503	2550	6360	4046	2583	3669	2448	2323	2417	2290	2869	2689	4439	7361	2592	2461	3774	4058	3397	4080	1976	5233
Distance (n.m.)		00	3395	4920	5844	3671	3694	4344	4670	2668	4217	4260	3228	8478	4956	4835	5239	3343	2984	3248	2422	4287	3301	5096	10000	3901	3823	4503	5264	4131	4887	2511	6448
		Via																							LAX								
		Via		LON	SEA									MIA	DKR		GDX							GUM	ACA				TYO				HNL
		Dest	STO	TLV	TYO	VIE	WAW	SEA	SFO	SIN	SYD	YVR	PHL	РРТ	RIO	SFO	TYO	WAS	YMQ	ZYY	SIN	Tγo	SYD	TYO	TYO	WAS	ΣΥΥ	SEL	TPE	Tγο	SFO	SIN	SYD
		Origin	NYC	NYC	NYC	NYC	NVC	OSA	OSA	OSA	OSA	OSA	PAR	PAR	PEK	PER	ЪРТ	ЪРТ	RIO	ROM	ROM	SEA	SEA	SEA	SEL	SEL	SFO						

	Load	Factor	89	65	99	65	65	67	99	67	8	57	61	65	99	99	99	67	67	67	68	67	67	67	67	67	5	67	67	67	67	62
1000 Units	Daily	Departures	20	28	46	99	88	2	24	16	16	Ø	9	32	4	100	8	0	8	4	4	4	4	8	8	8	32	8	2	2	2	14
	Load	Factor	89	62	65	<u>99</u>	9 9	67	62	67	64																					
500 Units	Daily	Departures	16	26	90	14	56	8	22	12	12																					
	Percent	subsonic	55	42	52	51	45	46	43	59	45	58	58	55	55	55	79	51	65	63	79	65	69	53	56	69	59	51	57	65	58	61
urs)		Trip	6.70	4.08	3.94	2.08	2.89	3.97	4.02	6.58	3.97	2.00	13.00	1.90	1.60	1.59	4.63	3.44	2.70	7.03	9.73	2.72	7.49	3.91	4.76	3.95	1.83	3.40	2.27	5.60	3.65	1.98
Time (hours)		Block	5.70	4.08	3.94	2.08	2.89	3.97	4.02	5.58	3.97	2.00	11.00	1.90	1.60	1.59	4.63	3.44	2.70	6.03	8.73	2.72	6.49	3.91	4.76	3.95	1.83	3.40	2.27	5.60	3.65	1.98
		Path	5628	4441	4300	1741	2900	4314	4383	5257	4070	1720	10273	1424	1164	1166	2914	3132	1836	5603	6577	1946	5503	3418	4154	3614	1362	3079	1788	3904	3085	1385
(n.m.)		Cruise	4367	3706	3603	1151	2300	3597	3668	3893	3233	1183	7442	800	638	648	930	2215	791	4090	3431	948	3543	2272	2718	2548	761	2166	1066	1642	1715	676
Distance (n.m.)		SC	5607	4439	3400	1740	2893	3931	4226	5176	4050	1439	6066	1423	1163	1164	2576	2993	1772	5158	5669	1787	5028	3349	3868	2536	1254	2975	1683	3902	2771	1339
		Via											GDX																			
		Via	TYO							ΤYΟ			GUM							DKR	BAH		GDX									
		Dest	TPE	TYO	SYD	TPE	ΟΫ́	TPE	TYO	YVR	YVR	LAX	LON	MEL	NAN	SYD	BAH	BOS	CAI	ЫО Ю	SIN	TLV	170	WAS	YYC	KHV	SEA	ΤYO	ccs	HNL	LIM	SJU
		Origin	SFO	SFO	SIN	SIN	SIN	SYD	SYD	TPE	TYO	ACA	AKL	AKL	AKL	AKL	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	ANC	ANC	ANC	ATL	ATL	ATL	ATL

	Load	Factor	. 67	67	99	65	64	61	67	67	67	67	67	67	67	67	67	67	6 6	67	62	67	67	67	67	67	67	67	67	64	67	67	67
1000 Units		Departures	4	8	4	22	8	9	8	4	8	8	9	8	8	8	9	10	24	12	8	80	4	8	7	9	10	2	0	26	8	4	0
	Load	Factor																															
500 Units	Daily	Departures																															
	Percent	subsonic	02	66	75	78	75	11	68	64	69	61	99	69	58	62	55	63	65	7	51	64	55	79	76	65	62	78	49	59	52	52	54
ırs)		Trip ^{\$}	8.95	4.99	4.16	4.85	3.95	4.53	2.55	7.54	2.56	4.75	2.56	5.98	1.83	4.07	1.72	2.90	1.92	6.34	5.47	2.05	2.73	6.21	6.11	3.44	6.81	6.48	3.33	1.63	4.11	1.83	2.97
Time (hours)		Block	7.95	4.99	4.16	4.85	3.95	4.53	2.55	6.54	2.56	4.75	2.56	5.98	1.83	4.07	1.72	2.90	1.92	5.34	5.47	2.05	2.73	6.21	6.11	3.44	6.81	6.48	3.33	1.63	4.11	1.83	2.97
		Path	6037	4772	2672	3029	2676	2860	1756	5866	1866	3830	2342	4461	1286	3479	1282	2755	1536	5160	4931	1314	2168	4093	4045	3625	4402	4232	3124	1163	3620	1458	2707
(n.m.)		Cruise	3397	3476	936	928	1118	932	793	4087	950	2225	1698	2191	642	2238	724	2067	959	3958	3328	506	1290	1151	1155	2976	1124	1140	2291	610	2418	911	1937
Distance (n.m.)		С С С			2422	2748	2307	2602	1563	5396	1549	3496	1623	3915	1287	2918	1259	1998	1186	4070	4902	1314	2156	3545	3623	2320	3892	3774	3014	1094	3544	1454	2416
		Via																															
		Via	SEA							DKR										POM													
		Dest	TYO	CAN	GVA	LON	MIL	PAR	CAI	RIO	TLV	ZYY	BOM	CAI	CMB	DHA	JKT	KHI	MNL	SYD	FRA	MIA	NYC	FRA	GVA	HKG	LON	PAR	BRU	MIA	ROM	nrs	DKR
		Origin	ATL	BAH	BAH	BAH	BAH	BAH	BER	BER	BER	BER	BKK	BKK	BOG	BOG	BOG	BOM	BOM	BOM	BOM	BOM	BOS	BOS	BOS	BOS	BRU						

C-11.

	Load	Factor	65	67	67	67	60	67	67	67	67	67	67	67	67	99	67	67	67	67	67	67	67	65	99	67	67	67	67	64	65	67	62
1000 Units		Departures	2	4	4	2	2	4	7	9	4	2	~	7	7	20	7	7	9	8	2	4	7	9	æ	2	N	4	2	80	4	2	8
	Load	Factor																															
500 Units	Daily	Departures																															
	Percent	subsonic	83	68	62	62	61	99	53	64	61	50	53	62	67	55	57	61	66	62	57	63	70	54	62	73	56	67	4	4	68	76	59
(s		Trip	2.61	7.59	8.06	2.33	2.23	2.92	2.27	2.60	1.78	2.11	1.82	3.09	4.69	1.61	4.65	5.25	2.80	5.09	5.11	2.96	6.70	1.93	3.18	5.16	2.45	8.08	4.17	4.76	8.40	4.44	3.03
Time (hours)		Block	2.61	6.59	7.06	2.33	2.23	2.92	2.27	2.60	1.78	2.11	1.82	3.09	4.69	1.61	4.65	5.25	2.80	5.09	5.11	2.96	6.70	1.93	3.18	5.16	2.45	7.08	4.17	4.76	7.40	4.44	3.03
		Path	1891	5586	6555	1642	1594	1951	1816	1782	1348	1811	1426	2206	3952	1184	4110	4125	1801	4177	4469	2112	4760	1537	2271	4854	2001	5585	2696	3005	5967	2835	2700
(n.m.)		Cruise	949	3592	4468	795			1116	792	780	1237	871	1048	2464	663	2734	2271	655	2487	2915	1008	1758	926	1077	3464	1252	3397	936	929	3538	933	1878
Distance (n.m.)		SC	1754	5103	6019	1575	1522	1904	1806	1731	1159	1799	1416	2180	3139	1183	3697	3916	1795	3698	4056	2046	4352	1479	2240	3188	1872	5569	2379	2731	5715	2584	2231
		Via																															
		Via		GDX	DKR																							SEA			LIS		
		Dest	TLV	ΤYO	ROM	FRA	GVA	LON	MAD	PAR	ROM	JKT	SIN	EH	LAX	MIA	СРН	MIL	SJU	STO	WAW	DHA	FRA	SIN	SIN	20	SJU	1Y0	FRA	LON	NYC	PAR	GVA
		Origin	BRU	BRU	BUE	CAI	CAI	CAI	CAI	CAI	CAI	CAN	CAN	ccs	ccs	ccs	CHI	CHI	CHI	CHI	EH	CMB	CMB	CMB	DEL	DEL	DFW	DFW	DHA	DHA	DHA	DHA	DKR

C-12

	Load	Factor	67	64	67	67	67	67	67	68	68	67	67	64	63	65	67	59	<u>66</u>	64	67	68	9 9	67	. 67	67	60	65	67	61	67	67	67
1000 Units	Daily	Departures	2	4	7	4	Ø	8	4	4	4	4	4	7	9	9	4	7	12	18	4	4	9	4	7	8	16	36	4	24	8	8	0
	Load	Factor																															
500 Units	Daily	Departures																															
	Percent	subsonic	54	54	55	71	11	61	75	11	63	64	78	48	62	62	71	48	53	53	54	76	60	71	55	45	81	61	82	64	45	20	68
(sır		Trip ^s	1.95	2.83	4.02	8.80	8.52	2.85	9.71	8.46	7.07	7.20	9.35	4.18	12.70	2.34	7.81	2.75	1.7	1.78	2.20	9.26	2.25	8.16	4.24	3.95	9.10	2.00	9.21	1.81	2.79	6.59	6.04
Time (hours)		Block	1.95	2.83	4.02	7.80	7.52	2.85	8.71	7.46	6.07	6.20	8.35	4.18	10.70	2.34	6.81	2.75	1.77	1.78	2.20	8.26	2.25	7.16	4.24	3.95	8.10	2.00	8.21	1.81	2.79	6.59	6.04
		Path	1660	2583	3477	6138	5815	2202	6581	5393	5346	5655	6383	3974	10000	1752	5700	2702	1385	1374	1954	6335	1704	5871	3663	4027	7549	1665	7705	1421	2756	4321	4032
(n.m.)		Cruise	1129	1851	2278	3667	3397	1245	3450	2776	3631	4035	3435	2909	7255	953	3592	2107	849	820	1388	3437	954	3566	2386	3179	5419	1096	5569	870	2161	1473	1482
Distance (n.m.)		ပ္ပ	1508	2280	3261	5712	5542	2014	6001	5030	5153	5163	5543	3970	8901	1594	5054	2549	1385	1375	1734	5663	1575	5295	3455	4027	5205	1341	5183	1122	2756	4320	4029
		Via													GUM																		
		Via				SEA	SEA		BAH	ΥΥC	MIA	DKR	BAH		GDX		GDX					BAH		GDX			GDX		GDX				
		Dest	LIS	PAR	LON	OSA	TΥO	ZΥΥ	JKT	LAX	MEX	RIO	SIN	SJU	SYD	TLV	TYO	JKT	MNL	OSA	SEL	NIS	TLV	TYO	ZYY	MAD	LON	OSA	PAR	SEL	NAN	NYC	ZYY
		Origin	DKR	DKR	DTW	DTW	DTW	FDF	FRA	FRA	FRA	GUM	GUM	GUM	GUM	GVA	GVA	GVA	GVA	HAV	HKG	HKG	HKG	HKG	HNL	HNL	HNL						

C-13

	Load	Factor	67	67	68	67	67	67	65	64	61	67	99	67	67	67	67	67	68	65	67	67	67	67	65	61	61	67	64	67	67	67	67
1000 Units	Daily	Departures	3	4	4	0	0	8	12	8	4	2	34	4	8	8	4	16	20	10	2	2	7	8	24	22	12	2	20	8	4	12	2
	Load	Factor											,																				
500 Units	Daily	Departures					-																										
	Percent	subsonic	51	68	47	20	56	50	78	58	54	51	69	74	51	59	71	71	79	65	50	51	53	54	64	09	61	99	65	69	69	55	62
rs)		Trip	2.07	8.47	8.61	4.41	2.01	3.18	8.27	2.28	8.76	2.96	2.27	8.77	2.66	1.85	8.96	7.92	9.95	2.94	2.79	2.28	3.55	2.59	2.24	1.67	2.60	2.11	2.51	2.65	7.48	1.93	2.30
Time (hours)		Block	2.07	7.47	7.61	4.41	2.01	3.18	7.27	2.28	7.76	2.96	2.27	7.77	2.66	1.85	7.96	6.92	8.95	2.94	2.79	2.28	3.55	2.59	2.24	1.67	2.60	2.11	2.51	2.65	6.48	1.93	2.30
		Path	1773	5789	8011	4377	1710	3231	6671	1759	7415	2958	1596	6153	2298	1419	7328	5916	6692	2061	2510	1925	3224	2087	1776	1107	2385	1464	1893	2353	5338	1445	1751
(n.m.)		Cruise	1211	3397	6516	3343	1162	2579	4727	1015	5483	2332	765	3502	1549	837	5193	3842	3428	945	1778	1274	2269	1275	1074	491	1736	691	1037	1640	3305	810	986
Distance (n.m.)		ပ္ပ	1719	5780	7789	2802	1499	2824	4896	1654	6923	2554	1348	5470	2289	1266	5809	5128	5868	1936	2473	1912	3004	2086	1456	1106	1816	1297	1634	1620	4986	1444	1550
		Via																															
		Via		SEA	TΥO				DKR		DKR			ACA			GDX	GDX	BAH												DKR		
	i	Dest	SJU	Σ	LAX	MEL	MNL	PEK	Lon	MRU	NVC	NIS	MEX	RIO	MEX	РТΥ	MNL	OSA	SIN	TLV	ZHY	TLV	YMQ	NAN	PER	MIA	NYC	РТΥ	SFO	WAS	RIO	OSA	PEK
		Origin	NOH	NOH	JKT	JKT	JKT	JKT	JNB	JNB	SNB	KHI	LAX	LAX	LĩM	LIM	LON	LON	LON	LON	LON	MAD	MAD	MEL	MEL	MEX	MEX	MEX	MEX	MEX	MIL	MNL	MNL

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	Load	Factor	61	67	67	67	67	67	67	67	67	68	67	67	67	65	67	67	67	68	67	64	67	68	67	67	
1000 Units	Daily	Departures	16	16	2	8	8	9	8	Ø	4	4	8	14	9	54	4	2	8	4	8	14	4	4	4	4	4836
	Load	Factor																									
500 Units	Daily	Departures																									2174
	Percent	subsonic	60	53	48	99	56	49	48	74	71	11	56	63	56	65	67	58	45	46	52	56	99	47	72	74	
Irs)		Trip	2.05	1.69	3.21	2.07	4.42	2.00	2.17	6.76	8.03	9.62	4.71	2.61	2.73	2.72	7.21	4.59	4.36	76.7	2.44	1.86	2.59	7.55	9.15	8.84	
Time (hours)		Block	2.05	1.69	3.21	2.07	4.42	2.00	2.17	5.76	7.03	8.62	4.71	2.61	2.73	2.72	6.21	4.59	4.36	6.97	2.44	1.86	2.59	6.55	8.15	7.84	
		Path	1432	1282	3018	1613	3820	1711	1928	5196	6072	6523	3961	1891	2298	2688	5406	3861	4527	7341	2298	1368	1942	6768	6142	5876	
(n.m.)		Cruise	692	754	2219	956	2481	1172	1374	3663	3992	3432	2461	949	1492	2106	3388	2407	3610	6006	1728	744	1051	5455	3397	3233	
Distance (n.m.		GC	1415	1284	3013	1433	3583	1710	1924	4170	5179	5783	3808	1773	2112	1768	4949	3557	4411	7331	2044	1362	1659	6745	5851	5557	
		Via																									
		Via								SJU	GDX	BAH				;	DKR			TYO				HNL	SEA	YVR	
		Dest	SEL	SIN	SIN	TLV	ZYY	SYD	PTγ	RIO	PAR	SIN	STL	TLV	SIN	SYD	ROM	YMQ	YVR	NIS	SIN	WAS	ZYY	YVR	WAS	ZΥΥ	
		Origin	MNL	MNL	MRU	MUC	MUC	NAN	NYC	NYC	OSA	PAR	PAR	PAR	PER	PER	RIO	ROM	SEL	SFO	SHA	SJU	SJU	SYD	TYO	TYO	

Appendix D. HSCT Routing Table

The following table provides a list of the city paris which make up the universal HSCT route system. It also includes the waypoints (latitude, longitude) between each city-pair used to avoid supersonic flight over land. Great circle routes were flown between city pairs unless waypoint routing was necessary. If waypoints were used, great circle routes were flown between the waypoints.

Long. Lot. Long. Long. <thl< th=""><th>•</th><th></th><th></th><th></th><th>:</th><th></th><th></th><th></th><th></th><th></th><th></th><th>2</th><th></th><th></th><th></th></thl<>	•				:							2			
L/L 16001 30001 1600V 30001 1600V 30001 1600V L/L 6000 6400V 20003 1760V 3000 1160V L/L 4000 6400V 20003 1260C 07600 1180V L/L 4000 1600C 1420C 0703 1200C 0003 L/L 2003 1600C 3720V 1200C 0003 1200C L/L 2003 1600C 3720V 0703 1200C 0003C L/L 2003 1500C 3720V 0100C 3720V 03076 L/L 2003 1500C 3720V 0100C 3720V 03076 L/L 2004 1700V 0200C 3720V 0100C 3420V 3460V L/L 2004 1700V 0200C 3720V 0100C 3420V 3460V L/L 2004 0700V 1200C 3120V 3420V 3420V 3460V			Ħ	Long.	E	Long.	Lat		Ĩ	Long.	Lat.		Lat		Long.
H.O. 100001 100001 110000 20001 110000 M.H. 20003 150004 20003 110004 20003 20004 M.H. 20003 150005 270004 20005 120005 20005 M.H. 20003 15006 20003 12006 23006 13006 M.H. 20003 15006 20003 12006 23006 13006 M.H. 20003 15006 20003 13006 23006 13006 M.H. 20003 15006 20003 13006 23006 23006 23006 M.H. 20003 15006 23006 13006 23006 23006 23006 M.H. 20004 23004 07025 23005 23006 <td></td> <td>24</td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		24				-									
RIO 6608 0300W 2008 0760W 2008 0760W 2008 0760W 2008 0760W 2008 0760W 2008 0760W 2008 1200E 2008 20		Š	Nongi	A0090L	2500N	11500W	NOOOD	11800W							
International 1500E 1600E 1700E	Š.	8	05008	W00680	2000S	07500W									
HIL Anticipant 1430E	KL	BUM													
MT 3006 1600E 1430E 7400E 740	KL	HNL													
ML ML ML ML 03 1500E 5608 1300E 5608 1300E 2400E <	KL	цК1	2000S	15500E	10008	142MDE	07000	10000							
Municipan Store 3608 1300E 37201 0147E 34281 2300E 31101 03325E 24681 111 51001 00000 77001 01801E 37201 01447E 34281 23260E 31101 03325E 24681 111 51001 00000 77001 01801E 37201 01447E 34281 23260E 24601E 24601E <td>NKL.</td> <td>MFI</td> <td></td>	NKL.	MFI													
CM CM <thcm< th=""> CM CM CM<!--</td--><td>5</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></thcm<>	5														
RM Model 1500 1100E 110E		NAN													
FER 46068 1500E 3608 1300E FT 2008 1560E 3608 1300E FT 2008 1560E 1420E 7003 1200E 2400E SN 700 1560E 1003 1200E 7201 1407E 2450E 20035 AT 5100 0900V 32281 07523V 7201 1947E 34281 2400E 31101 03325E 24651 AT 51001 0900V 32281 07623 1001E 37201 03147E 34281 2240E 23561 C41 45301 0121E 40001 0190E 37201 0147E 34281 2400E 21010 C41 45301 0121E 40001 0190E 37201 0147E 34281 2400E 2306 C41 45301 09300V 41001 06700V 41081 0700V 4301 0750V C41 51001 09900F 13270 <t< td=""><td>Ę</td><td>VSO</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	Ę	VSO													
POM 2005 15500 15	KL	PER	45008	15000E	35008	11300E									
PT PT PT PT SN 20005 1500E 10005 1200E 10005 1200E 2400E 2400E 2400E 2400E 2400E 2400E 2400E 2400E 240E 240E <t< td=""><td>KL</td><td>PON</td><td>20005</td><td>15500E</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	KL	PON	20005	15500E											
Sin 20005 1500E 1420E 0703 1200E 0373 1000E 2370 2006	KL	Ldd													
Yind Toole Toole <tht< td=""><td>3</td><td>CIN</td><td>anne</td><td>1 E E O E</td><td>00001</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tht<>	3	CIN	anne	1 E E O E	00001										
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TYO TYO A11 550N 01201E 4000U 3220N 01801E 3170N 01801E 3170N 03325E 2845N B03 510N 00800W 4700N 06600W 4108N 06700W 3170N 01801E 3720N 01801E 3720N 01801E 3720N 01801E 3720N 03325E 2845N 02400E 3110N 03325E 2845N 0325E 2845N 0325E 2845N 0325E 2845N 0325E 2845N 0325E 2845N 03325E	Į	STU													
ATL 51001 00900W 32281 07823W 01347E 3426N 02400E 3110N 03325E 2845N BAH 4530N 01221E 4000N 6500W 4108N 65700W 4108N 65700W 1347E 3425N 02400E 3110N 03325E 2845N CAI 4530N 01321E 4000N 6500W 4108N 65700W 1406N 6570W 1406N 6370N 01947E 3425N 02400E 3110N 03325E 2845N CHI 5100N 00900W 4700N 6500W 4108N 66700W 13230E 3425N 07600W 6320N 6700W 6320N 07500W 6320	Ę	<u>ک</u>													
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PAR 2845N 03440E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 4530N SIN 1930N 05740E 0500N 06000E 0610N 03700E 02400E 3720N 01947E 4000N 10200E SIN 1930N 05740E 0500W 4106N 03700E 02400E 0200N 10200E 4530N CAI 4530N 01221E 4000N 01900E 3720N 01947E 3425N 02400E 4530N CAI 4530N 01221E 4000N 01900E 3720N 01947E 3425N 02400E 4530N CAI 5100N 00900W 4700N 05000W 4108N 06700W 3425N 02400E 4530N DFW 4800N 01700W 2226N 070220E 3425N 02400E 3425N 02400E 4530N DFW 4800N 00700W 3720N 01947E 3425N 02400E 7400E 7400E <td>JAH</td> <td>MNL</td> <td>1930N</td> <td>05740E</td> <td>0500N</td> <td>08000E</td> <td>0610N</td> <td>09700E</td> <td>0800N</td> <td>10800E</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	JAH	MNL	1930N	05740E	0500N	08000E	0610N	09700E	0800N	10800E						
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BOS 5100N 00900W 4700N 05000W 4106N 06700W CAI 4530N 01221E 4000N 01900E 3720N 01947E 3425N 02400E CHI 6100N 00900W 4700N 05000W 4106N 06700W 4106N 06700W DFW 6100N 00900W 3226N 01807E 3425N 02400E DKR 4200N 00900W 3226N 07823W 4106N 06700W DKR 4200N 00900W 2700N 02000W 4106N 06700W MIA 4800N 00900W 4700N 05000W 4106N 06700W NYC 5100N 00900W 4700N 05000W 4106N 06700W YYR 5100N 00900W 4700N 05000W 4106N 06700W YYZ 5100N 00500W 4106N 06700W 6200N 07000W	BAH	NIS	1930N	06740E	0500N	0000E	0610N	09700E	0200N	10200E						
CAI 4530N 01221E 4000N 01907E 3720N 01947E 3425N 02400E CHI 6100N 00900W 4700N 05000W 4108N 06700W 226N 07823W DFW 6100N 00900W 3226N 07823W 4108N 06700W 4108N 06700W DKR 4200N 01700W 2000N 02000W 4108N 06700W 4108N 06700W NYC 5100N 00900W 4700N 05000W 4108N 06700W 3425N 02400E YYR 6100N 00900W 4700N 05000W 4108N 06700W 3425N 07600E YYR 6100N 00500W 4108N 06700W 6200N 6200N 07600W 6200N 6200N 07	BER	BOS	5100N	W00800	4700N	05000W	4108N	06700W								
CHI 6100N 00900W 4700N 05000W 4108N 06700W DFW 6100N 00900W 3226N 07823W 4108N 06700W DKR 4200N 01700W 2000N 02000W 4108N 06700W MIA 4800N 00900W 4700N 02000W 4106N 06700W NYC 5100N 00900W 4700N 05000W 4106N 06700W YVR 6000N 01221E 4000N 01947E 3425N 02400E YVR 6000N 01900E 3720N 01947E 3425N 02400E YVR 6000N 01900E 3720N 01947E 3425N 02400E YVR 6000N 05000W 4106N 06700W 6200N 07000W 6300N 07500W	3ER	CAI	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E						
DFW 6100N 00000W 3226N 07823W DKR 4200N 01700W 2000N 02000W MIA 4800N 00500W 4700N 02000W NYC 5100N 00900W 4700N 05000W 4106N NYC 5100N 00900W 4700N 05000W 4106N 06700W YYR 6100N 00500W 4106N 06700W 3425N 02400E YYR 6000N 01900E 3720N 01947E 3425N 02400E YYR 5100N 00500W 4106N 06500W 6200N 07000W 6300N 07500W	BER	H	5100N	W00800	4700N	05000W	4108N	06700W								
DKR 4200N 01700W 2000N 02000W MIA 4800N 00600W 4700N 05000W 4108N 06700W NYC 5100N 00900W 4700N 05000W 4108N 06700W 3425N 02400E TLV 4530N 01221E 4000N 01900E 3720N 01947E 3425N 02400E VIR 6000N 4700N 05000W 4106N 06500W 6200N 07000W 6300N 07500W 6230N YYZ 5100N 00900W 4700N 05000W 4106N 06500W 6200N 07000W 6300N 07500W 6230N	BER	DFW	5100N	W00600	3226N	07823W										
MIA 4800N 00600W NYC 5100N 00900W 4700N 05000W 4106N 06700W NYC 5100N 00900W 4700N 01900E 3720N 01947E 3425N 02400E TLV 4530N 01221E 4000N 01900E 3720N 01947E 3425N 02400E VAS 5100N 00900W 4700N 05000W 4106N 06500W 6200N	JER	DKR	4200N	01700W	2000N	02000W										
NYC 5100N 00900W 4700N 05000W 4108N 06700W TLV 4530N 01221E 4000N 01900E 3720N 01947E 3425N 02400E WAS 5100N 00900W 4700N 05000W 4106N 06700W 8200N 07000W 8300N 07500W 6230N YYZ 5100N 00500W 4106N 06500W 4106N 06500W 6200N 6200N 6200N 6230N	JER	MIA	4800N	00600W												
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WAS 5100N 00900W 4700N 05000W 4108N 06700W YVR 6000N 00500W 5800N 04500W 6100N 06500W 6200N 07000W 6300N 07500W 6230N YYZ 5100N 00900W 4700N 05000W 4108N 06700W	3ER	۲ ک	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E						
YVR 8000N 00500W 5800N 04500W 6100N 06500W 6200N 07000W 6300N 07500W 6230N YYZ 5100N 00900W 4700N 05000W 4106N 06700W	3ER	WAS	5100N	W00600	4700N	OSODOW	4108N	06700W								
YYZ 5100N 00900W 4700N 05000W 4106N 06700W	3ER	YNR	6000N	00500W	5800N	04500W	6100N	06500W	6200N	07000W	6300N	07500W	NUCCA			
		Ş	510M	Manana	A700N	DEMON	Atron	1002 au					NOC 20			
		711		Mmem												

Origin	Dest	Waypoint 1	11	Waypoint 2	12	Waypoint 3	13	Waypoint 4	-	Waypoint 5	9	Wavpoint 6		Wavpoint 7	17
		Lat	Long.	Let.	Long.	Ē	Long.	Ę	Long.		Long.		Long.		Lond
									6		A				.Runz
BXX	S	0600N	0000E	1930N	05740E	2845N	03440E								
BKK	CMB														
BKK	AHO	0000N	0000E	1930N	05740E										
BKK	L L L	N0010	10500E												
BKK	KHI	0500N	0000E	1000N	07500E	1730N	07200E								
BKK	MNL	0700N	10500E	NOOBO	10800E										
BKK	VSO	N0010	10500E	NOODO	1000E	NOOEE	13700E								
BKK	PER	0400N	10400E	10008	11000E	30005	11000E								
BKK	PON	03078	10900E	01005	12000E	10008	14200E								
BKK	SEL	0700N	10500E	NOODO	10800E	3000N	12500E	3500N	12500E						
BKK	0XT	0700N	10500E	NOOBO	1000E	NOOEE	13700E								
BOG	FRA	4200N	01700W												
BOG	MAD														
BOG	MIA														
BOG	NVC	2600N	07600W												
BOM	FRA	1930N	05740E	2845N	03440E	3110N	03325E	3425N	024005	3720N	01047E	NOON	20005	10011	110010
BOM	BVA	NOC61	05740E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	010476	Nooot		NOSOF	012215
BOM	НКО	1730N	07200E	1000N	07500E	0500N	0800E	0810N	09700F	DROON	1000E			Norch	
BOM	LON	1930N	05740E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947F	ADDN	010005	AFAAN	110010
BOM	PAR	1930N	05740E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947F	ADDN	01000E		012215
BOM	SIN	1730N	07200E	1000N	07500E	0500N	0800E	0610N	09700E	0200N	1020F				
BOS	BRU	410 BN	06700W	4700N	05000W	5100N	W00600								
BOS	FRA	4108N	06700W	4700N	05000W	5100N	W00800								
BOS	AVD	4106N	06700W	4800N	00600W										
BOS	LON	4106N	06700W	4700N	06000W	5100N	M00600								
BOB	VIN	3820N	06957W												
BOS	PAR	4106N	06700W	4800N	00600W										
BOS	NON	410 0 N	06700W												
BOS	SUU														
BOS	NNS	4106N	06700W	4700N	05000W										
BRU	E	6100N	W00800	4700N	05000W	4108N	06700W								
BRU	DKR	4200N	01700W	2000N	02000W										
BRU	ADX	6230N	00300E	7200N	02500E	7200N	13230E								
BRU	NYC	5100N	W00800	4700N	05000W	4108N	06700W								
BRU	7	4530N	01221E	- N0004	01900E	3720N	01947E	3425N	02400E						
BRU	WAS	6100N	M00600	4700N	0500W	4106N	06700W								
BRU	YMQ	5100N	W00600	4700N	0500W	4108N	06700W								
BUE	DKR	36005	06200W	20008	03500W										

Lat. Long. 1221E CA1 NYC 3428N 02400E 3700N 01907E 400N 01201E 4530N 01221E CA1 NYC 3428N 02400E 3700N 01307E 400N 01201E 4530N 01221E CA1 NYC 3428N 02400E 370N 01307E 400N 01201E 450N 01221E CA1 NYC 300N 1030N 0752N 0130N 0752N 01231E 400N 01		:				
FX 34261 34261 37201 11417 40001 01500E 45301 01221E UN 34261 02400E 37201 01447E 40001 01500E 45301 01221E UN 34261 02400E 37201 0147E 40011 01500E 45301 01221E UN 34261 22400E 37201 01301E 45301 01221E 45301 01221E UN 34261 22400E 37201 013016 45301 01221E 45301 01221E UN 34261 22400E 37201 01301E 45301 01221E UN 2400E 37201 01301E 47001 01301E 45301 01221E UN 2400E 37201 01321E 40016 45301 01221E UN 2400E 37201 017823W 017823W 01221E 45011 UN 17001 017821W 017823W 017823W 01221E 47011	Lat Long. Lat.	ong. Lat	Long.	Lat	Long. Lat	Long.
QV 34281 02400E 37201 01947E 40001 01900E 43201 01221E LON 34281 02400E 37201 01947E 40001 01900E 43301 01221E MT 34261 22401E 37201 01947E 40011 01900E 43301 01221E JTT 34261 22401E 37201 01347E 40011 01900E 43301 01221E JTT 24001 37201 01347E 40011 01900E 43301 01221E JTT 24001 20000 12301E 47001 01301E 45301 01221E JTT 24001 27001 01220E 4701 01301 45301 01221E JTT 24001 27001 01220E 4701 01301 45301 01221E JTT 24001 27001 01220E 45301 01221E 45011 JTT 24011 27001 0722801 0722801 0760	01900E AS30N	Ť				
LON 34281 02400E 3720N 01947E 400 N 01900E 4530 N 0121E MAD 34281 02400E 370 N 01307E 400 N 01300E 4530 N 01221E MAD 34281 02400E 370 N 01307E 400 N 01300E 4530 N 01221E MAD 34281 02400E 370 N 01307E 400 N 01300E 4530 N 01221E JKT 0800 N 1230E 700 N 01207E 400 N 01301E 4530 N 01221E JKT 0800 N 1230E 700 N 01307E 400 N 01221E JKT 130 N 07623 W 0782 N 0782 N 0647 N 0733 N 01221E LA 1730 N 0700 W 1036 N 0782 N 0783 N 0630 N 01221E LA 1730 N 0700 W 1036 N 0782 N 0647 N 0733 N 01221E LA 400 N 0700 N 0780 N <td>01900F AS30N</td> <td>ίμ</td> <td></td> <td></td> <td></td> <td></td>	01900F AS30N	ίμ				
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NVC 3425N 02400E 4106N 06700V 1137E 450N 01221E N/T 3425N 02400E 3720N 01347E 4000N 01307E 4530N 01221E SN 02400E 3720N 01347E 4000N 01300E 4530N 01221E SN 0200N 1280E 0723N 07833W 0637N 0530N 01221E LX 1130N 0700W 1036N 07833W 0647N 07334W 0630N 0600W LN 4200N 0700W 1036N 07823W 0647N 07334W 0630N 01221E LN 4700W 07823W 07823W 07834W 0630N 01221E LN 1730N 07823W 07823W 07834W 0630N 01221E LN 1730N 07823W 07823W 07834W 0630N 01221E LN 1730N 05807W 07834W 05807W 0830N 08000W LN		1				
PAR 3425N 02400E 3720N 01347E 4000N 01201E 4301N 01221E NT 000N 1000E 3700N 01300E 3720N 01201E 4300N 01201E SIN 000N 1060E 3700N 01200E 4700N 01201E SIN 000N 1260E 3700N 01700W 0753M 07934W 0930N 0920N LIN 1130N 07000W 1036N 07823W 07834W 0930N 0900W LIN 4200N 07000W 1036N 07828W 07834W 0930N 0930N LIN 4200N 07000W 1036N 07828W 07834W 0730N 0930N LIN 4200N 07000W 1036N 07824W 07934W 0930N 0930N LIN 4108N 0790W 07824W 07834W 07934W 0930N MIL 4108N 0600W 0500W 0500W 06000W 07904W						
ROM 3425N 02400E 3700N 01200E JKT 0800N 10800E 3700N 01200E JKN 0800N 10800E 3730N 07823W 07823W LX 11730N 07000W 3226N 07823W 0847N 0930N 0800W LX 11730N 07000W 1036N 07823W 0847N 07334W 0830N 0800W LX 1130N 07000W 10782N 07823W 0847N 07334W 0830N 0800W LNX 1130N 07000W 10782N 0782N 0847N 07334W 0830N 0800W LNX 1730N 08600W 3820N 0857W 07934W 0930N 0800W ML NYC 730N 08600W 580N 0850W 590N 0800W ML 4108N 08700W 4700N 05000W 510N 0990W 510N 510N 510N 510N 510N 510N 510N 5	01900E 4530N	16				
JKT 00001 10000E SIN 20001 10000E FIA 2001 10000E LX 11201 01700W 32261 LX 11201 0700W 32261 07823W LX 11301 07000W 10361 07834W 06301 08000W LX 11301 07000W 10361 07823W 07873W 08301 08000W LX 11301 07000W 10361 07823W 07873W 08471 07934W 08301 08000W LON 48001 07600W 10361 07834W 07834W 08301 08300W 08301						
SN 00001 10800E TYO 20001 12500E TYO 20001 12500E LAX 17301 07000W 32281 07623W LAX 11301 07000W 10361 07823W 0847N 06301V 08000W LAX 11301 07000W 10361 07828W 0847N 06301V 08000W LAX 11301 07000W 10361 07828W 0847N 07334W 06300W LON 48001 07000W 10360 07828W 0847N 06300W ML NYC 17301 08800W 47001 05600W 51001 06900W ML NYC 4108N 06700W 4700N 65000W 5100N 09500W ML 4108N 06700W 4700N 65000W 5100N 09500W ML 4108N 06700W 4700N 65000W 5100N 09500W ML 4108N 06700W 4700						
TYO 2000N 1260E 3258N 07823W 6847N 07834W 6630N 2000N FRA 4200N 01700W 0786N 07823W 0787N 0630N 06000W LAX 1130N 07000W 1038N 07823W 0847N 07334W 0630N 06000W LON 4800N 07000W 1038N 07823W 0847N 07334W 0630N 06000W LON 4800N 06800W 8520N 0887W 0847N 07334W 0630N 06000W ML NYC 1730N 06800W 8500N 6600N 06900W 0000W ML NYC 1730N 06800W 8100N 06000W 9100N 9100N PAR 4108N 06700W 4100N 65000W 8100N 90000W 9100N HL 4108N 06700W 4100N 65000W 8100N 90000W 9100N HL 4108N 06700W 8100N 90600W						
CH 1730N 06600W 3226N 07823W 0781N 07834W 0847N 07934W 0800N 0800N LX 1130N 07000W 1038N 07928W 0847N 07934W 0800N 08000W LS 4800N 07000W 1038N 07928W 0847N 07934W 0800N 08000W LDN 4800N 06600W 3820N 06957W 0847N 07934W 0830N 0800N ML 1730N 06600W 3820N 06957W 0847N 07934W 0830N 0800N ML ML 1730N 06600W 3820N 06900N 05000W 07934W 0847N 0830N ML HIL 4108N 06700W 4700N 05000W 01000W 05000W 05000W 06000W 05000W 06500W 06500						
FIA 4200N 01700W 0735N 07828W 0847N 07934W 0600W 0000W LLS 1130N 07000W 1036N 07928W 07934W 0630N 0000W LLS 4000N 06600W 1036N 07928W 0647W 07934W 0630N 0600W LLN 400N 06600W 3820N 06957W 5100N 06900W 5100N 00500W 5100N 5100N <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td></t<>						
LAX 1130N 07000W 1036N 07924W 0630N 0600N LIS LON 4800N 00600W 1036N 07924W 0630N 0600N LIS LON 4800N 00600W 3820N 06957W 0630N 0600N ML NYC 1730N 06900W 3820N 06957W 6000N 69500W PAR 4106N 06700W 4770N 65000W 5100N 00500W RML 4106N 06700W 4770N 65000W 5100N 00500W HNL 4106N 06700W 4700N 65000W 5100N 69000W HNL 4106N 06700W 4700N 6000W 5100N 6900W </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
LS LON 4800N 00600W MAD MIL NYC 1730N 06600W 3820N 06657W FRA 4106N 06700W 4700N 65000W 6100N 00500W FRA 4106N 06700W 4700N 65000W 6100N 00500W GVA 4106N 06700W 4700N 65000W 6100N 00500W MIL 4106N 06700W 4700N 65000W 5100N 00500W MIL 4106N 06700W 4700N 65000W 5100N 00500W FRA 4106N 06700W 4700N 65000W 5100N 00500W MIL 4106N 06700W 4700N 65000W 5100N 00500W MIL 4106N 06700W 4700N 65000W 5100N 00500W FRA 4106N 06700W 4700N 65000W 5100N 00500W MIL 4106N 06700W 4700N 65000W 5100N 00500W MIL 4106N 06700W 4700N 65000W 5100N 00500W MIL 4106N 26400W 4700N 65000W 5100N 00500W FRA 770N 07500E 2845N 03440E 3110N 0520E 3425N 02400E FRA 7730N 07500E 2845N 03440E 3110N 03235E 3425N 02400E	N0690 W4670	0W 1500N	10500W	2500N 11500W	000 3000N	11800W
LON 4800N 00600W MAD MAD MAL MAD MIL MIL MIL MIL MIL MID MIL MID MIL MID MIL MID MIL 4106N PAR 400N Addition 06500W FIA 4106N Addition 65000W GVA 4106N Addition 65000W GVA 4106N Addition 65000W GVA 4106N Addition 65000W MIL 4106N						
MAD MIA MIA MIA MIL NYC 1730N 06900W 3820N 06957W PAR 4800N 00500W 3820N 06957W 4700N 05000W PAR 4800N 06700W 4700N 05000W 6100N 00500W PAR 4108N 06700W 4700N 05000W 6100N 00500W PAR 4108N 06700W 4700N 05000W 6100N 00500W PAR 4108N 06700W 4700N 05000W 5100N 00900W MIL 4108N 06700W 4700N 05000W 5100N 00900W MIL 4108N 06700W 4700N 05000W 5100N 00300W MIL 4108N 06700W 4700N 05000W 5100N 00300W MIL 4108N 06700W 4700N 05000W 5100N 03000W SLU 4108N 06700W 4700N 0500W 510						
ML ML NYC 1730N 06800W 3820N 06957W PAR 4900N 00600W 3820N 06957W PAR 4900N 00600W 3820N 06957W PAD 06700W 4700N 65000W 6000N 00500W PAD 4106N 06700W 4700N 65000W 6100N 00500W PAL 4106N 06700W 4700N 05000W 6100N 00500W PAR 4106N 06700W 4700N 05000W 5100N 00900W PAR 4106N 06700W 4700N 05000W 5100N 00900W PAR 4106N 06700W 4700N 05000W 5100N 00900W PAR 0730N 07500E 294M 3110N 03325E 3425N 02400E						
MIL NYC 1730N 06900W 3820N 06957W PAR 4800N 00600W 4700N 05000W 6000N 00500W FRA 4106N 06700W 4700N 05000W 5100N 00500W FNA 4106N 06700W 4700N 05000W 5100N 00900W ALL 4106N 06700W 4800N 00600W 5100N 00900W MIL 4106N 06700W 4700N 05000W 5100N 00900W MIL 4106N 0730N 07500E 2945N 03440E 3110N 03325E 3425N 03440E						
NYC 1730N 06000W 3820N 06957W PAR 4500N 00600W 3820N 06957W PAR 4500N 00600W 4700N 05000W 6000N PAR 4106N 06700W 4700N 05000W 5100N 00500W PAR 4106N 06700W 4700N 05000W 5100N 00500W PAR 4106N 06700W 4700N 05000W 5100N 00900W PAR 4106N 06700W 4700N 05000W 5100N 00900W PAR 4106N 06700W 4700N 05000W 5100N 09900W PAR 4106N 06700W 4700N 05000W 5100N 09900W PAR 4106N 06700W 4700N 05000W 5100N 09900W PAR 0730N 0730N 0730N 09500W 09000N PAR 0730N 0730N 0730N 09500W 04000 PAR <						
PAR 4900H 00600W 4700H 05000W 65000W 6500W 65						
ROM CPH 4106H 06700W 4700N 05000W 6100N 00500W FA 4106H 06700W 4700N 05000W 6100N 00500W FNA 4106H 06700W 4700N 05000W 6100N 00500W FNA 4106H 06700W 4700N 05000W 5100N 00500W HNL LON 4106H 06700W 4700N 05000W 5100N 00500W MIL 4106H 06700W 4700N 05000W 5100N 00500W MIL 4106H 06700W 4700N 05000W 5100N 00500W SLU 2000 06500W 5100N 00500W 5100N 00500W SLU 4106H 06700W 4700N 05000W 6000N 0500W SLU 2100H 0730H 0730H 0730H 0730H 2440E PAR 0730H 0730H 0730H 03335E 3426N 02400E						
CPH 4106N 06700W 4700N 05000W 6100N 06500W FRA 4106N 06700W 4700N 05000W 6100N 00500W HNL 06700W 4700N 05000W 6100N 06500W 6100N 00500W HNL 06700W 4700N 05000W 6100N 06900W 6100N 00900W HNL 4106N 06700W 4700N 05000W 5100N 09900W MIL 4106N 06700W 4700N 05000W 5100N 09900W ROM 4106N 06700W 4700N 05000W 5100N 09900W SLU 4106N 06700W 4700N 05000W 5100N 09900W SLU 4106N 06700W 4700N 05000W 510N 09900W SLU 510N 06500W 6000N 0500W 6000N 6000W SLU 60700W 4106N 06500W 6000N 6000N 6000W						
FA 4106H 06700W 4700H 05500W 5100H 00500W GVA 4106H 06700W 4000H 05600W 5100H 00500W HNL LON 4106H 06700W 4700H 05600W 5100H 00500W HNL LON 4106H 06700W 4700H 05600W 5100H 00500W MIL 4106H 06700W 4700H 05600W 5100H 00500W MIL 4106H 06700W 4700H 05600W 5100H 00500W ROM 4106H 06700W 4700H 05600W 5100H 00500W SLU 510H 0730H 07500E 1930H 05500W 510H 03325E 3425H 02400E PAR 0730H 07500E 2845H 03440E 3110H 03325E 3425H 02400E						
QV 4106N 06700W 4800N 00600W HNL 4106N 06700W 4700N 5100N 09900W HNL 4106N 06700W 4700N 5100N 09900W ML 4106N 06700W 4700N 5100N 09900W ML 4106N 06700W 4700N 05000W 5100N 09900W PAR 4106N 06700W 4700N 05000W 5100N 09900W ROM 4106N 06700W 4700N 05600W 6000N 6000W SLU 5100N 0700W 4700N 05600W 6000N 6000W ML 4106N 06700W 4700N 05600W 6000N 6000N MAW 4106N 0730N 07500E 1930N 05740E 3110N 03325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02400E						
HNL LON 4106N 06700W 4700N 05000W 5100N 00900W MIL 4106N 06700W 4700N 05000W 5100N 00900W MUC 4106N 06700W 4800N 05000W 5100N 00900W PAR 4106N 06700W 4800N 00600W SEA SJU STO 4106N 06700W 4700N 05000W MAW 4106N 06700W 4700N 05000W DHA 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02400E						
LON 4106N 05700W 4700N 05000W 5100N 09900W MIL 4106N 06700W 4700N 05000W 5100N 09900W MUC 4106N 06700W 4700N 05000W 5100N 09900W PAR 4106N 06700W 4800N 06600W 5100N 09900W ROM 4106N 06700W 4800N 06600W 6000W 5100N 09900W SEA SJU 06700W 4700N 06600W 6000N 0600W VAW 4106N 06700W 4700N 05600W 6000N 0600W PIA 0730N 07560E 1930N 05740E 3110N 03325E 3425N 02400E PAR 0730N 07560E 2845N 03440E 3110N 03325E 3425N 02400E						
MIL 4106N 06700W 4700N 05700W 5100N 00900W MUC 4106N 06700W 4700N 05000W 5100N 00900W PAR 4106N 06700W 4800N 06600W 5100N 00900W ROM 4106N 06700W 4800N 06600W 5100N 00900W SEA SJU 06700W 4700N 05600W 6000N 00500W SLU 4106N 06700W 4700N 05000W 6000N 00500W VAW 4106N 0730N 07500E 1930N 05740E 3110N 03325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02400E						
MUC 4100N 05700W 4700N 05000W 5100N 00900W PAR 4100N 06700W 4800N 06600W 5100N 00900W ROM 4100N 06700W 4800N 06600W 5100N 00900W ROM 4100N 06700W 4800N 06600W 6000W 510N SEA SJU 9700W 4700N 05600W 6000N 6000W VAW 4100N 06700W 4700N 05600W 6000N 6000W DHA 0730N 07560E 1930N 05740E 3110N 03325E 3425N 02400E PAR 0730N 07560E 2845N 03440E 3110N 03325E 3425N 02400E						
PAR 4106N 06700W 4800N 00600W ROM 4106N 06700W 4800N 06600W SEA SEA SI 4106N 06700W SIU 106N 4106N 06700W 4700N SIU 4106N 06700W 4700N 05000W VAW 4106N 06700W 4700N 05000W DHA 0730N 07500E 1930N 05740E 3110N 03325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02400E						
ROM 41060 06700W SEA SEA SLU SJU STO 41060 06700W STO 41060 06700W 4700N 05000W VAW 41060 06700W 4700N 05000W DHA 0730N 07500E 1930N 05740E 3110N 03325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02460E						
SEA SJU SJU STO 4106N 06700W 4700N 05000W WAW 4106N 06700W 4700N 05000W DHA 0730N 07500E 1930N 05740E 3110N 0325E 3425N 02400E FRA 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E						
SJU STO 4106N 06700W 4700N 05000W WAW 4106N 06700W 4700N 05000W 6000N 00500W DHA 0730N 07500E 1930N 05740E 3110N 0325E 3425N 02400E FRA 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E						
STO 4100N 06700W 4700N 05000W 05000W 05000W 05000W 0500W 0500E 05400E 2440E 3110N 03325E 3425N 02400E 2450F 05400E 2450F 05400E						
WAW 4108N 06700W 4700N 05000W 6000N 00500W DHA 0730N 07500E 1930N 05740E 3110N 0325E 3425N 02400E FRA 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E						
DHA 0730N 07500E 1930N 05740E FRA 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E						
FRA 0730N 07500E 2845N 03440E 3110N 03325E 3425N 02400E PAR 0730N 07500E 2845N 03440E 3110N 0325E 3425N 02400E						
PAR 0730N 07600F 2845N 03440E 3110N 03326E 3425N 02400F	03325E 3425N	0E 3720N	01947E	4000N 01900E	0E 4530N	01221F
	03325E 3425N		019475			

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CPH N	NYC 6000N	00500W	4700N	05000W	4108N	06700W								
	SEA 6000N	00500W	5800N	04500W	6100N	06500W	6200N	07000W	6300N	07500W	6230N	08000W		
CVG FF	FRA 4106N	06700W	4700N	05000W	5100N	W00800								
CVG LC	LON 4106N	06700W	4700N	05000W	5100N	M00600								
DEL SI	SIN DETON	09700E	0200N	10200E										
DEL J	TYO 0610N	09700E	NOOBO	10800E	3300N	13700E								
	FRA 3226N	07823W	5100N	W00800										
DFW HI	HNL													
DFW LC	LON 3226N	07623W	5100N	W00600										
DFW M	MAD 3226N	07823W												
DFW -PJ		07823W	4800N	00600W					,					
DFW SJ	SJU 2900N	09500W	2400N	06230W	2350N	08000W	2350N	07500W						
DHA FF	FRA 2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E		
HA LHO			0500N	0000E										
DHA LI	LIS 3110N	03325E	3425N	02400E	NOE7E	01200E	NOCOC	00730E						
DHA LC	LON 2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E		
	MNL 1930N	05740E	0500N	0000E	0610N	09700E	0800N	10800E						
	PAR 2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E		
	NOC61 NIS	05740E	0500N	0000E	0610N	09700E	0200N	10200E						
	GVA 2000N	02000W	4200N	01700W										
	HAV													
		0200W	2700N	02000W										
	LON 2000N	0200W	4200N	01700W										
	MAD 2000N	0200W	NOOOE	01800W	3701N	00756W								
	NVC													
	PAR 2000N	0200W	4200N	01700W										
DKR R	RIO 2000S	03500W												
	ROM 2000N	02000W	N000E	01800W	3701N	00756W								
DTW FF	FRA 4108N	06700W	4700N	06000W	5100N	M00600								
DTW LC		06700W	4700N	05000W	5100N	W00600								
LA WTO	PAR 4106N	06700W	4700N	05000W	5100N	W00600								
DTW SE	SEA	·												
55	FRA 4800N	W00900												
		M00600												
FDF	-													
_	PAR 4800N	0000M												

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		F	Long.	Ę	Long.	Ę	Long.	Ę	Long.	F	Long.	Lat	Long.	L.	Long.
FRA	BAH	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E	A110N	03325F	2845N	DRADE		
FRA	DKR	4200N	01700W	2000N	02000W										
FRA	GDX	5219N	00447E	6230N	00300E	7200N	02500E	7200N	13230E						
FRA	Ŋ	4800N	00600W	3226N	07823W										
FRA	MIA	4800N	00600W												
FRA	NYC	5100N	W00600	4700N	05000W	4108N	06700W								
FRA	PHL	5100N	W00600	4700N	05000W	4108N	06700W								
FRA	SJU	4800N	00600W												
FRA	건	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E						
FRA	WAS	5100N	W00800	4700N	05000W	4108N	06700W								
FRA	YNG	5100N	W00800	4700N	05000W	4108N	06700W								
FRA	T	N0009	00500W	500N	04500W	6100N	06500W	6200N	07000W	6300N	07500W	6230N	08000W		
FRA	λc	00009	00500W	5800N	04500W	6100N	06500W	6200N	07000W	6300N	07500W	6230N	08000W		
FRA	227	5100N	W00600	4700N	05000W	4108N	06700W								
XDD	GUM														
GDX	LON	7200N	13230E	7200N	02500E	6230N	00300E								
GDX	MNL	3700N	14700E	3500N	14200E										
	OSA	3700N	14700E	3400N	14100E										
	PAR	7200N	13230E	7200N	02500E	6230N	00300E								
	۲ 0	3700N	14700E												
	GDX														
GUM	HNL														
BUM	КТ	0300N	12200E	N0000	11830E	0500S	11700E								
GUM	MNL														
GUM	OSA														
	SEL	3000N	12500E	3500N	12500E										
	SYD	0500S	15400E	20008	15500E	3230S	15400E								
	20														
	BAH	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E	3110N	03325E	2845N	03440E		
•	QDX	5219N	00447E	8230N	00300E	7200N	02500E	7200N	13230E						
AVD	NYC	4800N	00600W	4106N	06700W										
AVD	ک	4530N	01221E	N000#	01900E	3720N	01947E	3425N	02400E						
AVD	YNQ	4700N	05000W	410BN	06700W										
AVA	ZX	5100N	M00600	4700N	05000W	4108N	06700W								
HAV	MAD														
Ē	NYC	4700N	05000W	4106N	06700W										
HKG	QDX	2000N	12500E	3500N	14200E	3700N	14700E								

R.						waypoint 3		waypoint 4	•	Waypoint 5		Waypoint 6	16	Waypoint 7	
		j	Long.	j	Long	j	Long.	Le L	Long.	Ę	Long.	٦	Long.	E.	Long.
-	JKT	N0080	10000E												
_		2000N	12200E	03305	14700E	10005	15200E	20005	15500F	2600S	IREADE	20105	1 KAME		
-	VSO	2000N	12500E										1000-01		
	PER	NOOBO	10 00 E	10008	11000E	30005	11000E								
	SEL	2200N	12230E												
	SIN	N0080	1000E												
HKG S	SYD	2000N	12200E	03305	14700E	10005	16200F	20000	166ME		4FEAAE	00000	7007.1		
	۶ ۲	2000N	12500E							SUCT		200720	104WE		
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		3000N	13000E	3500N	12500E										
	SFO														
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		3226N	07823W	5100N	W00800										
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	SEA														
_	Su Su	2400N	06230W	2350N	00000	2360N	07500W								
		0700S	12000E	10008	14200E	20005	15500E	25003	15500F	30206	1EAME				
		0000N	10800E												
	OSA VSO	NOOBO	1000E	3300N	13700E										
	PEX	N0090	1000E	NOOOE	12300E	3800N	12300E	3900N	11800F						
		0000	10800E	3000N	12500E	3500N	12500E								
JKT S'		0700S	12000E	10008	14200E	20005	15500E	2500\$	15500F	32208	1KANNE				
JKT T	TPE	N0080	10000E							26.96					

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BN	DKR 2600S	S 01500E	1400N	02100W										
and	_													
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BND	RIO													
BNC	SIN 28005	S 04800E												
×	ACA 3000N		2500N	11500W	1500N	10500W								
Ň	HNL													
~	LON 6230N	N00000 N	N0068	07500W	6200N	07000W	6100N	06500W	5800N	04500W	5100N	W00900		
Ě	MEX 3000N	N 11800W		11000W										
~	NAN													
~	OSA 3400N	N 14100E												
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LM	MEX 1500N	W00700 N												
LIM	-			·										
LIM	NYC 0500S	-	2500N	07500W										
LIM		N006300W												
	NVC													
	RIO 3000N	N 01800W	0730S	03200W	20005	03500W								
	BAH 4530N	N. 01221E	4000N	01900E	3720N	01947E	3425N	02400E	3110N	03325E	2845N	03440E		
	DKR 4200N	N 01700W	2000N	02000W										
7	GDX 6230N	N 00300E	7200N	02500E	7200N	13230E								
LON	MIA 5100N	M00600 N												
z	MSP 5100N	M00600 N	500N	04500W	6100N	06500W	6200N	07000W	N00E9	07500W	6230N	08000W		
z	NYC 5100N	M00600 N	4700N	05000W	4108N	06700W								
z	PHL 5100N	M00600 N	4700N	05000W	4108N	06700W								
z	SEA 5100N	M00600 N	500N	04500W	6100N	· 06500W	\$200N	07000W	NOOES	07500W	6230N	08000W		
LON	SFO 5100N	M00600 N		04500W	6100N	06500W	6200N	07000W	6300N	07500W	6230N	08000W		
LON	SJU 5100N	M00600 N												
LON	STL 5100N	M00600 N	47 00N	05000W	4108N	06700W								
z	TLV 4530N	N 01221E	4000N	01900E	3720N	01947E	3425N	02400E						
LON		M00600 N	4700N	05000W	4108N	06700W								
LON	YHZ 5100N	M00600 N	4700N	05000W										
LON	YMQ 5100N	M00600 N	4700N	05000W	4108N	06700W								
LON	YVR 5100N	M00600 N	5000N	04500W	6100N	06500W	6200N	07000W	8300N	07500W	6230N	W00080		
LON		M00600 N		04500W	6100N	06500W	6200N	07000W	N00E9	07500W	6230N	08000W		
LON	YYZ 5100N	-		05000W	410BN	W00700								
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Origin	Deet.	Waypoint 1	at 1	Waypoint 2	112	Waypoint 3	13	Waypoint 4		Wavpoint 5	19	Wavpoint 6		Wavpoint 7	
		j	Long.	Ę	Long.	Lat	Long.	Ē	Long.	Ē	Long.	Lat	Long.	Ĩ	Long.
		NOOIL	AA no/on												
MAD	0 ² 2	3701N	00756W	2700N	02000W	20005	03500W								
MAD	۲ ۷	3700N	01200E	3425N	02400E										
MAD	WAS	4108N	06700W												
MAD	DMY	4106N	06700W												
MEL	HNL	25005	16500E												
MEL	NAN														
MEL	VSO	3230S	15400E	25005	15500E	20008	15500F	DEADS	15 AME						
MEL	PER	35005	11300E					20000							
MEL	Tqq														
MEL	NIS	32305	15400E	25008	15500E	20005	15500E	10005	142005	07005	120005	03076	10000		
MEL	0 <u>7</u>	32305	15400E	25008	15500E	20005	15500F	USONS	15400E			0 000			
MEX	VIN														
MEX	NVC	2400N	08230W	2350N	00000M	2350N	07600W								
MEX	μ	1500N	W00760	N0670	08230W										
MEX	SFO	2000N	11000W	3356N	12200W										
	WAS	2400N	08230W	2350N	W00080	2350N	07600W	SROON	07E00W						
VIII 1	MEX														
MIA	MUC	4800N	00600W												
VIN	PAR	4800N	00600W												
MIA	μ														
MIA	BIO	2600N	07600W	2000N	00000M	0730S	03200W	2000S	03500W .						
MIA	MON														
VIN	SCL	05003	08300W												
W	DKR	3701N	00756W	NOOOE	01800W	2000N	02000W								
Ĩ	NYC	4800N	00800W	4108N	06700W										
, III	WAS	4600N	W00800	4108N	06700W										
MNL	VSO														
MNL	PEK	2000N	12200E	N000E	12300E	3800N	12300E	NOOBE	11800E						
MNL	SEL	3000N	12500E	3500N	12500E										
MNL	NB														
MNL	SYD	03305	14700E	10005	15200E	2000S	15500E	25005	15500E	32305	15400F				
MNL	7 Y0						I								
MOM	NYC	N0009	00500W	4700N	05000W	4108N	06700W								
MRU	Nis														
MUC	NYC	5100N	M00600	4700N	05000W	4108N	06700W								
MUC	У, Г	4530N	01221E	1000 1	01900E	3720N	01947E	3426N	02400E						
MUC	WAS	5100N	M00600	4700N	05000W	4106N	06700W								

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MUC YYR MUC YYC MUC YYZ MAN ANC NAN ANC NYC LON NYC OSL	Lat. 6000N 6000N	Long.	ł	Long.										
	N0009					Long.	Ę	Long.	۲ ۳	Long.	Lat.	Long.	Lat	Long.
	N0009	00500W	KAOON	MEMW	A100N	MEDNU		110000						
		00500W	5800N	DAEDOW	A100N	Necow.		M00010		M009/0	N0520	M00080		
	5100N	W00800	4700N	OSOOW	410RN	De Zonw			10000	Mone /n	NUCED	A nonso		
	4108N	06700W	4700N	05000W	5100N	W00800								
	4108N	06700W	4700N	05000W										
	4108N	06700W	4800N	00600W										
C PTY	2500N	07500W												
NYC ROM	4108N	06700W	4600N	00800W										
	4108N	06700W	4700N	OFOONW										
	4108N	06700W	4700N	05000W										
-	4108N	06700W	4800N	00600W										
NYC WAW	4108N	06700W	4700N	0500W	8000N	00500W								
OSA GDX	3400N	14100E	3700N	14700E										
OSA SEA	3400N	14100E	5000N	17900W										
OSA SFO	3400N	14100E												
OSA SIN	NOOCE	13700E	N0080	10800E										
OSA SYD	05003	15400E	2000S	15500E	2500S	15500E	3230S	15400E						
OSA YVR	3400N	14100E	5000N	17900W										
PAR BAH	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E	3110N	03325F	PRASN	034405		
	4200N	01700W	2000N	02000W										
•	6230N	00300E	7200N	02500E	7200N	13230E								
_	4800N	00600W												
PAR PHL	5100N	W00800	4700N	05000W	4108N	06700W								
	5100N	W00800	5800N	04500W	6100N	06500W	6200N	07000W	6300N	07500W	NOSCO	0R000W		
PAR STL	5100N	W00900	4700N	05000W	4108N	06700W								
PAR TLV	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E						
PAR WAS	4800N	00600W	4108N	06700W										
	4800N	W00800	4108N	06700W										
PAR YYZ	5100N	W00900	4700N	05000W	4108N	06700W								
PEK SIN	3900N	11800E	NOOBE	12300E	3000N	12300E	NOOBO	1080E						
PER SYD	35005	11300E	45005	15000E										
PER TYO	0100N	11930E	0500N	12600E ·	3000N	13500E								
_	03308	14700E	2000N	12200E										
POM SYD	20005	15500E	25005	15500E	32205	154005								

68 0000W 1000W 06700W 101 06700W 101 06700W 101 06700W 101 06700W 1000E 000H 1060E 11 1100E 000H 12 1200E 1200E 2003 1550E 13 1200E 2003 1550E 2003 1540E 13 1370E 2003 1550E 2333 1470E 13 1370E 2003 1550E 2333 1470E 13 1370E 2003 1550E 2333 1470E 13 1300E 2003 1550E 2303 1540E 13 1560E 2003 1500E 2303 1470E 13 1300E 300N 1230E 300N 1600E	Waypoint 1 Way Lat Long. I	Long.		Waypoint 2 Lat	2 Long.	Waypoint 3 Lat.	t 3 Long.	Waypoint 4 Lat.	Long.	Waypoint 5 Lat.	5 Long.	Waypoint 6 Lat	e Long.	Waypoint 7 Lat	Long
0470W 1410E 1260E 060N 1060C 1260E 100S 1420E 250S 1550C 250S 1550C 233S 1420E 200S 1420C 2003 1550C 250S 1550C 233S 1370C 2003 1550C 033S 1550C 230S 1550C 230S 1370C 2003 1550C 033S 1550C 230S 1550C 230S 1550C 2003 1550C 2003 1520C 230S 1550C 230S 1550C 230S 1550C 2005 1550	2000S 07500W 0		ð	05003	W00680										
06700% 1100E 12600E 000N 10600E 10000E 1000S 14200E 2500S 15500E 2500S 15500E 2200S 13700E 200S 1500E 2000S 15500E 2300S 15500E 2300S 15500E 2000S 15500E 2300N 12500E 230N 12500E 200N 120	03500W 06700W														
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1260E 000N 1080E 1090E 1000S 14200E 2500S 15500E 3230S 1070E 200S 14200E 2000S 15500E 3230S 1370E 200S 15500E 2000S 15500E 3230S 1370E 200S 15500E 2000S 15500E 3230S 1550E 200S 15500E 000S 15200E 330S 1550E 200S 15500E 000S 15200E 330S 1550E 200S 15200E 330S 14700E 1550E 2500S 15200E 3900N 11900E 1000E 350N 12500E 3900N 11900E	17900W		e,	400N	14100E										
1260E 000N 1000E 10000E 10003 14200E 25005 15500E 2305 17000E 10003 14200E 20005 15500E 2305 17000E 20003 15500E 20005 15500E 2305 17000E 20003 15500E 10003 15200E 2305 15500E 20003 15500E 03305 14700E 2305 15500E 20003 15500E 03003 15200E 2305 14700E 15000E 20003 15500E 23003 15200E 2305 14700E 15000E 3500N 12500E 3500N 12300E 3900N 11900E 10000E 3500N 12500E 3900N 12300E 3900N 11900E	6000N 17900W	17900W													
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13700E 03200W 2000S 03500W 03200E 2000S 15500E 1000S 15200E 0330S 15500E 2000S 15500E 0500S 15400E 0330S 15500E 3000N 12500E 0500S 15400E 3900N 13000E 3500N 12500E 3800N 12300E 3900N 10800E 3500N 12500E 3800N 12300E 3900N	10800E									20002		20676	10400		
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13000E 3500N 12500E 3800N 12300E 3900N 10800E															
13000E 3500N 12500E 3800N 12300E 3900N 10800E															
		14100E		NOOOE	13000E	3500N	12500E		12300E	NOOSE	11800E				
	5000N - 17900W	17900W													
	13700E		~	NOOBC	10900E										
	13700E														
	5000N 17900W	17900W													

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Appendix E. Universal Airline System Scheduling

The passenger demand for HSCT service between city-pairs is determined by forecast growth rates and the HSCT market penetration. Once the demands between city-pairs are determined, an acceptable schedule for the HSCT fleet must be created. The schedule is built using a Boeing-developed "Sequential Itinerary" model which dynamically links the cities and demands in the HSCT route network, finding a suitable set of city-pairs for each airplane to serve. The model accounts for airport curfews and for passenger-preferred departure and arrival time "windows". The following is a brief explanation of the model operation:

(Refer to Figure E-1). At the start of the operational day at city "A", the model examines all possible routes that could be flown to carry demand from city "A", looking ahead one leg beyond the first destination. Passenger preference time windows for departure and arrival and airport curfews will likely limit the routes that can be served. In this example, flights are restricted to A-B, then B-F or B-G.

The first airplane is assigned to route A-B (Figure E-2, I). At B, the model looks ahead for the routes to serve which will minimize the time on the ground at B. The model assumes that the minimum ground time for a "turn", that is the end of a flight number, is 1.5 hours. The minimum ground time for a through stop, that is an intermediate stop in the flight required for refueling, is 1.0 hours. In this example (Figure E-2, II), serving B-F then F-P will require stopping at F until the airplane can clear the preference/curfew "window" at P. Since the ground time to serve B-F-P would be longer than that required to serve B-G and then G-K, the model assigns the airplane to the latter routes.

As the airplane "flies" the city-pairs, the model tracks accumulated time for that airplane. The operational day for the airplane (block time for the flights, ground time for "turns" and through stops) is limited to 24 hours less a set maintenance interval, since the model logic works with daily demand. The model uses the 24 hour limit as well as the preference/curfew "windows" in assigning routes. The time limit is obviously more restrictive near the end of the operational day.

As airplane number 1 reaches city P, (Figure E-2, III) its operational day ends with an accumulated time of 20+ hours. At that point airplane number 2 is assigned to serve the cities that receive demand from P. The model schedules airplane 2 in the same manner as number 1, linking together cities which have HSCT demand assigned until the end of the operational day for airplane 2, at which point airplane 3 is assigned. This process continues until all the city-pair demand is served, which takes 500 airplanes and 500 "airplane-days" in the base case. While the model links single airplanes and itineraries sequentially, the results are the same as if multiple airplanes operated together at the same time on the schedule determined by the model.

"Sequential Itinerary" Scheduling Model

City pairs and trip frequencies available for airplane starting the operational day at city "A", "looking ahead" one leg.

Passenger preference"windows" and airport curfews restrict the number F of cities that can actually be reached. В G Η С J **8** K D L Cities unreachable \bigotimes due to passenger preference 🐼 М "windows" and airport curfews

Figure E-1. Sequential Intinerary Scheduling Model Schematic, 1 airplane

"Sequential Itinerary" Scheduling Model

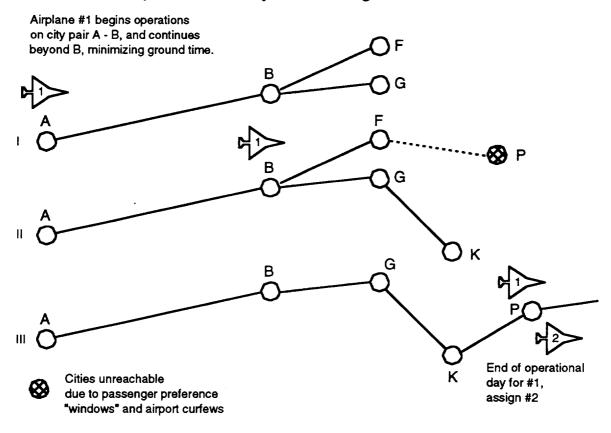


Figure E-2. Sequential Itinerary Scheduling Model Schematic, 3 airplanes.

Table E-1 shows the details of the scheduling of the first 5 airplanes in the 1994 HSCT emissions route system. Because of its speed, the HSCT has the ability to serve a large set of cities and still remain within the preference/curfew time "windows", which are always defined in local time. Thus airplane #1 in the example in Table E-1 begins the day in New York at 0800 New York time, flies to Warsaw and back, then on to Tokyo via Seattle, ending its day at 2023 local time after the short flight from Tokyo to Manila. Airplane #2 starts at Manila at 2153, and can reach Singapore at 2335, then off to Sydney, arriving at 0701 the next morning. From Sydney, the airplane can reach Tokyo at 1131, then to Washington via Seattle, arriving at 0815 local time. Airplane #3 starts from Washington, and ends its day in Guam. Airplane #4 starts in Guam and ends up in Singapore, airplane #5 starts in Singapore and ends up back in Singapore after six trips. Airplane #6 starts in Singapore, and ends its day in Los Angeles. Airplane #7 starts in Los Angeles and ends its day in Seattle and so on until all demand on all city pairs is satisfied.

					Local Time		Block	Ground Time (Hrs)	Ground Time (Hrs)
Airplane #	Flight #	Origin	Dest.	Via	Depart	Arrive	Time (Hrs)	(Turn)	(at Via Cities)
1	1	NYC	WAW		800	1744	3.8	1.5	
1	2	WAW	NYC		1913	1703	3.8	1.5	
1	3	NYC	TYO	SEA	1832	1826	8.4	1.0	1.0
1	4	TYO	MNL		1925	2023	2.0		
					.	Totals	17.9	4.0	1.0
					Operational Hours	Day	22.8		
2	5	MNL	SIN		2153	2335	1.7	1.5	
2	6	SIN	SYD		105	701	3.9	1.5	
2 2 2 2	7	SYD	TYO		831	1131	4.0	1.5	
2	8	TYO	WAS	SEA	1301	745	8.2		1.0
						Totals	17.8	4.5	1.0
					Operational Hours	Day	23.3		
3	9	WAS	TYO	SEA	937	907	8.2	1.2	1.0
3	10	TYO	YVR		1018	2114	4.0	1.5	
3	11	YVR	TYO		2243	1943	4.0	1.5	
3	12	TYO	GUM		2113	2358	1.7		
					• • •	Totals	17.8	4.2	1.0
					Operational Hours	Day	23.0		
4	13	GUM	TYO		645	728	1.7	1.5	
4	14	TYO	SYD		858	1400	4.0	1.5	
4	15	SYD	TPE		1529	1726	4.0	1.5	
4	16	TPE	SIN		1856	2104	2.1		
						Totals	11.8	4.5	0.0
					Operational Hours	Day	16.3		
5	17	SIN	MRU		2234	2150	3.2	1.5	
5	18	MRU	SIN		2320	630	3.2	1.5	
5	19	SIN	TYO		759	1151	2.9	1.5	
5	20	TYO	SIN		1321	1515	2.9	1.5	
5	21	SIN	TPE		1645	1847	2.1	1.5	
5	22	TPE	SIN		2016	2224	2.1		
						Totals	16.4	7.5	0.0
					Operational Hours		23.8		

Table E-1. HSCT "Sequential Itinerary" Scheduling Model

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Appendix F. Altitude Distribution of Emissions for Mach 2.4 HSCT fleets

This appendix contains the tables which summarize the different Mach 2.4 HSCT emission scenarios. For each of the scenarios considered, the fuel burned and emissions (NOx, CO, and hydrocarbons) were summed over latitude and longitude and tabulated as a function of altitude in 1 km altitude increments (the resolution of the data set).

Cumulative fractions of fuel burned and emissions were calculated from the ground up to provide a simple way to evaluate how the emissions were distributed vertically. In addition, the effective emission index for each altitude band was calculated and tabulated.

The global total of fuel burned and emissions were calculated and listed at the bottom of each table. Also, included is the effective emission index for NOx, CO, and hydrocarbons, globally averaged over all locations and altitudes.

For the charts shown, the notation 1.00E+08 is equivalent to 1.00×10^8 . The emissions are in units of kilograms per year and the emission indices have units of grams of emissions per kilogram of fuel burned.

US Standard Atmosphere (1976) pressures and temperatures were used in the calculations. These altitudes correspond to the geopotential altitudes of the US Standard Atmosphere grid.

able F-1. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude
ourinitied over Latitude and Longitude) for the Mach ∠.4 (Nominal Et(NUX)=5) HSCT fileet only, ssuming 500 HSCTs are flying on the universal network.

	Ĕ	-				
	EI(HC)	1.25	0.56	0.56	0.56	0.56
	EI(NOX)	7.17	8.24	8.24	8.24	8.24
Ititude	cum CO EI(NOX) EI(HC) EI((%)	11.26%	12.48%	13.70%	14.92%	16.14%
a function of a	CO (kg/year)	2.72E+07	2.94E+06	2.94E+06	2.94E+06	2.94E+06
i indices as T fleet only,	cum HC (%)	9.75%	11.32%	12.90%	14.48%	16.05%
and emissior VOx)=5) HSC	HC (kg/year)	2.89E+06	4.67E+05	4.68E+05	4.68E+05	4.67E+05
of emissions, Nominal El(f	cum NOX (%)	3.11%	4.39%	5.68%	6.97%	8.25%
ve fractions c ne Mach 2.4 (irsal network.	NOX (kg/year)	1.66E+07	6.88E+06	6.88E+06	6.89E+06	6.87E+06
ons, cumulati gitude) for th on the unive	cum fuel (%)	2.82%	3.83%	4.85%	5.87%	6.88%
Irned, emissic tude and Lor Ts are flying	Fuel (kg/year)	2.32E+09	8.34E+08	8.34E+08	8.36E+08	8.34E+08
Table F-1. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal El(NOX)=5) HSCT fleet only, assuming 500 HSCTs are flying on the universal network.	Attitude Band (km)	0 - 1	1 - 2	2 - 3	3 - 4	4 - 5

	Altitude Band	Fuel	cum fuel	NOX	cum NOX	<u>H</u>	cum HC	8	cum CO	EI(NOX)	EI(HC)	EI(CO)
I	(km)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	,		
	0 - 1	2.32E+09	2.82%	1.66E+07	3.11%	2.89E+06	9.75%	2.72E+07	11.26%	71.7	1.25	11.73
	1 - 2	8.34E+08	3.83%	6.88E+06	4.39%	4.67E+05	11.32%	2.94E+06	12.48%	8.24	0.56	3.53
	2 - 3	8.34E+08	4.85%	6.88E+06	5.68%	4.68E+05	12.90%	2.94E+06	13.70%	8.24	0.56	3.53
	3 - 4	8.36E+08	5.87%	6.89E+06	6.97%	4.68E+05	14.48%	2.94E+06	14.92%	8.24	0.56	3.52
	4 - 5	8.34E+08	6.88%	6.87E+06	8.25%	4.67E+05	16.05%	2.94E+06	16.14%	8.24	0.56	3.53
	5 - 6	8.34E+08	7.90%	6.88E+06	9.54%	4.68E+05	17.63%	2.95E+06	17.36%	8.24	0.56	3.53
	6 - 7	8.34E+08	8.92%	6.88E+06	10.82%	4.68E+05	19.20%	2.95E+06	18.58%	8.24	0.56	3.53
	7 - 8	8.35E+08	9.93%	6.88E+06	12.11%	4.68E+05	20.78%	2.95E+06	19.80%	8.24	0.56	3.53
	8 - 9	1.12E+09	11.29%	9.23E+06	13.84%	5.94E+05	22.79%	4.22E+06	21.55%	8.26	0.53	3.77
	9 - 10	2.87E+09	14.79%	2.39E+07	18.30%	1.33E+06	27.26%	1.08E+07	26.02%	8.32	0.46	3.76
	10 - 11	3.11E+09	18.58%	2.60E+07	23.17%	1.36E+06	31.86%	9.96E+06	30.15%	8.37	0.44	3.20
	11 - 12	2.30E+09	21.38%	1.94E+07	26.81%	9.61E+05	35.10%	5.25E+06	32.32%	8.43	0.42	2.28
	12 - 13	3.41E+09	25.53%	2.87E+07	32.18%	1.36E+06	39.69%	9.13E+06	36.11%	8.43	0.40	2.68
	13 - 14	1.77E+09	27.68%	1.52E+07	35.03%	5.55E+05	41.56%	1.08E+06	36.55%	8.61	0.31	0.61
	14 - 15	1.77E+09	29.84%	1.53E+07	37.88%	5.56E+05	43.43%	1.08E+06	37.00%	8.61	0.31	0.61
	15 - 16	1.77E+09	32.00%	1.52E+07	40.73%	5.55E+05	45.30%	1.08E+06	37.45%	8.61	0.31	0.61
	16 - 17	1.77E+09	34.15%	1.52E+07	43.58%	5.55E+05	47.18%	1.08E+06	37.90%	8.61	0.31	0.61
	17 - 18	3.19E+09	38.04%	2.25E+07	47.80%	9.63E+05	50.42%	5.49E+06	40.17%	7.06	0:30	1.72
	18 - 19	1.28E+10	53.61%	7.21E+07	61.28%	3.71E+06	62.94%	3.49E+07	54.65%	5.64	0.29	2.73
	19 - 20	2.40E+10	82.78%	1.30E+08	85.66%	6.91E+06	86.25%	6.87E+07	83.11%	5.44	0.29	2.87
	20 - 21	1.41E+10	100.00%	7.67E+07	100.00%	4.08E+06	100.00%	4.08E+07	100.00%	5.42	0.29	2.88
	Global Total	8.21F+10		5 35F+08		2 97E±07		2 41 E 108		6 E1	0 36	10 0
I				0.000				2.71 1700		55	00.0	L.34

Table F-2. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=5) HSCT fleet only, assuming 1000 HSCTs are flying on the universal network.

 Attitude Band	Fuel	cum fuel	NOX	cum NOX	Ч	cum HC	8	cum CO	EI(NOX)	EI(NOX) EI(HC)	EI(CO)
(km)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	·	.	· ·
0 - 1	5.03E+09	3.21%	3.59E+07	3.46%	6.45E+06	10.97%	6.09E+07	12.81%	7.13	1.28	12.10
1 - 2	1.74E+09	4.32%	1.43E+07	4.83%	1.01E+06	12.68%	6.53E+06	14.19%	8.21	0.58	3.75
2 - 3	1.74E+09	5.43%	1.43E+07	6.21%	1.01E+06	14.40%	6.53E+06	15.56%	8.21	0.58	3.75
3 - 4	1.74E+09	6.54%	1.43E+07	7.59%	1.01E+06	16.11%	6.53E+06	16.93%	8.21	0.58	3.75
4 - 5	1.74E+09	7.65%	1.43E+07	8.96%	1.01E+06	17.83%	6.56E+06	18.31%	8.21	0.58	3.77
5-6	1.74E+09	8.76%	1.43E+07	10.34%	1.01E+06	19.55%	6.56E+06	19.69%	8.21	0.58	3.77
6 - 7	1.74E+09	9.87%	1.43E+07	11.71%	1.01E+06	21.27%	6.56E+06	21.07%	8.21	0.58	3.77
7 - 8	1.74E+09	10.98%	1.43E+07	13.09%	1.01E+06	22.99%	6.56E+06	22.45%	8.21	0.58	3.77
6 - 8	2.15E+09	12.35%	1.77E+07	14.79%	1.19E+06	25.01%	8.39E+06	24.22%	8.23	0.56	3.91
9 - 10	5.17E+09	15.65%	4.29E+07	18.92%	2.48E+06	29.22%	2.02E+07	28.46%	8.30	0.48	3.91
10 - 11	6.47E+09	19.78%	5.40E+07	24.12%	2.94E+06	34.22%	2.29E+07	33.28%	8.34	0.45	3.54
11 - 12	5.83E+09	23.50%	4.89E+07	28.83%	2.55E+06	38.57%	1.74E+07	36.95%	8.38	0.44	2.99
12 - 13	7.69E+09	28.40%	6.46E+07	35.05%	3.15E+06	43.92%	2.25E+07	41.69%	8.41	0.41	2.93
13 - 14	3.55E+09	30.67%	3.05E+07	37.99%	1.12E+06	45.84%	2.29E+06	42.17%	8.61	0.32	0.65
14 - 15	3.55E+09	32.93%	3.06E+07	40.94%	1.13E+06	47.75%	2.29E+06	42.65%	8.61	0.32	0.65
15 - 16	3.55E+09	35.20%	3.05E+07	43.88%	1.12E+06	49.66%	2.29E+06	43.14%	8.61	0.32	0.65
16 - 17	3.55E+09	37.46%	3.05E+07	46.82%	1.12E+06	51.58%	2.29E+06	43.62%	8.61	0.32	0.65
17 - 18	5.45E+09	40.94%	4.03E+07	50.70%	1.67E+06	54.42%	8.21E+06	45.34%	7.39	0.31	1.50
18 - 19	1.98E+10	53.55%	1.14E+08	61.70%	5.77E+06	64.24%	5.21E+07	56.30%	5.78	0.29	2.64
19 - 20	4.15E+10	80.03%	2.28E+08	83.63%	1.20E+07	84.64%	1.18E+08	81.06%	5.49	0.29	2.84
20 - 21	3.13E+10	100.00%	1.70E+08	100.00%	9.03E+06	100.00%	9.01E+07	100.00%	5.43	0.29	2.88
			00 - L1 - T								
GIODAI I OTAI	1.5/E+11		1.04E+09		5.88E+U/		4./6E+U8		6.62	0.38	3.03

Altitude Band	Fuel	cum fuel	NOX	cum NOX	Я	cum HC	000	cum CO	EI(NOX)	EI(HC)	EI(CO)
(km)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	·		
0 - 1	2.32E+09	2.84%	1.66E+07	3.09%	2.95E+06	9.88%	2.78E+07	11.45%	7.17	1.27	11.98
1 - 2	8.47E+08	3.88%	6.97E+06	4.39%	4.77E+05	11.48%	3.02E+06	12.69%	8.24	0.56	3.57
2 - 3	8.47E+08	4.91%	6.97E+06	5.69%	4.77E+05	13.07%	3.02E+06	13.94%	8.24	0.56	3.57
3 - 4	8.47E+08	5.95%	6.97E+06	6.99%	4.77E+05	14.67%	3.02E+06	15.19%	8.24	0.56	3.57
4 - 5	8.47E+08	6.99%	6.97E+06	8.29%	4.77E+05	16.27%	3.02E+06	16.43%	8.24	0.56	3.57
5 - 6	8.47E+08	8.02%	6.97E+06	9.58%	4.77E+05	17.87%	3.02E+06	17.68%	8.24	0.56	3.57
6 - 7	8.47E+08	9.06%	6.97E+06	10.88%	4.77E+05	19.47%	3.02E+06	18.93%	8.24	0.56	3.57
7 - 8	8.47E+08	10.10%	6.97E+06	12.18%	4.77E+05	21.07%	3.02E+06	20.18%	8.24	0.56	3.57
8-9	1.21E+09	11.59%	1.00E+07	14.05%	6.33E+05	23.18%	4.45E+06	22.01%	8.27	0.52	3.66
9 - 10	2.57E+09	14.74%	2.15E+07	18.05%	1.16E+06	27.07%	8.44E+06	25.49%	8.35	0.45	3.28
10 - 11	3.25E+09	18.72%	2.72E+07	23.11%	1.42E+06	31.83%	1.04E+07	29.79%	8.37	0.44	3.21
11 - 12	3.25E+09	22.71%	2.73E+07	28.20%	1.39E+06	36.49%	9.55E+06	33.73%	8.39	0.43	2.94
12 - 13	4.38E+09	28.07%	3.68E+07	35.04%	1.79E+06	42.48%	1.33E+07	39.22%	8.40	0.41	3.04
13 - 14	1.75E+09	30.22%	1.51E+07	37.85%	5.50E+05	44.32%	1.07E+06	39.66%	8.61	0.31	0.61
14 - 15	1.75E+09	32.37%	1.51E+07	40.66%	5.50E+05	46.16%	1.07E+06	40.10%	8.61	0.31	0.61
15 - 16	1.75E+09	34.51%	1.51E+07	43.47%	5.50E+05	48.00%	1.07E+06	40.54%	8.61	0.31	0.61
16 - 17	1.75E+09	36.66%	1.51E+07	46.28%	5.50E+05	49.84%	1.07E+06	40.98%	8.61	0.31	0.61
17 - 18	3.36E+09	40.78%	2.33E+07	50.63%	1.01E+06	53.23%	6.06E+06	43.47%	6.94	0:30	1.80
•	1.26E+10	56.23%	7.10E+07	63.84%	3.66E+06	65.49%	3.45E+07	57.71%	5.63	0.29	2.74
19 - 20	2.27E+10	84.03%	1.24E+08	86.84%	6.55E+06	87.41%	6.50E+07	84.51%	5.45	0.29	2.86
20 - 21	1.30E+10	100.00%	7.07E+07	100.00%	3.76E+06	100.00%	3.76E+07	100.00%	5.42	0.29	2.88
Global Total	8.16E+10		5.37F+08		2 00F-107		2 42F108		6 FR	0.27	0 07
	>>		2211220		2.335441		2.425700		0.00	0.3/	

Table F-3. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal El(NOx)=5) HSCT fleet only,

Table F-4. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal El(NOx)=15) HSCT fleet only, assuming 500 HSCTs are flying on the universal network.
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xiii) xiii (xiii) xiii (xiii)	(kg/ear) 2.32E+09 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.35E+08	(%)			(Kovvear)					•	
0 0 @ 4 @ - 0 @ 4 @ 0	2.32E+09 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.35E+08			(%)		(%)	(kg/year)	(%)			
	8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.35E+08	0/ 70.7	3.54E+07	2.39%	2.89E+06	9.75%	2.72E+07	11.26%	15.28	1.25	11.73
0.04.0 	8.34E+08 8.36E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.35E+08	3.83%	1.92E+07	3.69%	4.67E+05	11.32%	2.94E+06	12.48%	22.97	0.56	3.53
3 - 4 - 5 - 5 - 6 - 5 - 8	8.36E+08 8.34E+08 8.34E+08 8.34E+08 8.34E+08 8.35E+08 1 12E+09	4.85%	1.92E+07	4.99%	4.68E+05	12.90%	2.94E+06	13.70%	22.97	0.56	3.53
4 - 5 5 - 6	8.34E+08 8.34E+08 8.34E+08 8.35E+08 1.12E+09	5.87%	1.92E+07	6.28%	4.68E+05	14.48%	2.94E+06	14.92%	22.98	0.56	3.52
5-6 8	8.34E+08 8.34E+08 8.35E+08 1 12E+09	6.88%	1.92E+07	7.58%	4.67E+05	16.05%	2.94E+06	16.14%	22.97	0.56	3.53
	8.34E+08 8.35E+08 1.12E+09	7.90%	1.92E+07	8.88%	4.68E+05	17.63%	2.95E+06	17.36%	22.97	0.56	3.53
6 - 7 8	8.35E+08 1.12E+09	8.92%	1.92E+07	10.17%	4.68E+05	19.20%	2.95E+06	18.58%	22.96	0.56	3.53
7 - 8 6	1.12E+09	9.93%	1.92E+07	11.47%	4.68E+05	20.78%	2.95E+06	19.80%	22.97	0.56	3.53
6 - 8		11.29%	2.15E+07	12.93%	5.94E+05	22.79%	4.22E+06	21.55%	19.24	0.53	3.77
9 - 10 2	2.87E+09	14.79%	4.15E+07	15.73%	1.33E+06	27.26%	1.08E+07	26.02%	14.45	0.46	3.76
10 - 11 3	3.11E+09	18.58%	5.16E+07	19.22%	1.36E+06	31.86%	9.96E+06	30.15%	16.57	0.44	3.20
11 - 12 2	2.30E+09	21.38%	4.94E+07	22.56%	9.61E+05	35.10%	5.25E+06	32.32%	21.44	0.42	2.28
12 - 13 3	3.41E+09	25.53%	5.94E+07	26.58%	1.36E+06	39.69%	9.13E+06	36.11%	17.44	0.40	2.68
13 - 14 1	1.77E+09	27.68%	4.54E+07	29.65%	5.55E+05	41.56%	1.08E+06	36.55%	25.65	0.31	0.61
14 - 15 1	1.77E+09	29.84%	4.54E+07	32.72%	5.56E+05	43.43%	1.08E+06	37.00%	25.65	0.31	0.61
15 - 16 1	1.77E+09	32.00%	4.54E+07	35.79%	5.55E+05	45.30%	1.08E+06	37.45%	25.65	0.31	0.61
16 - 17 1	1.77E+09	34.15%	4.54E+07	38.86%	5.55E+05	47.18%	1.08E+06	37.90%	25.65	0.31	0.61
17 - 18	3.19E+09	38.04%	6.73E+07	43.41%	9.63E+05	50.42%	5.49E+06	40.17%	21.06	0.30	1.72
18 - 19 1	1.28E+10	53.61%	2.16E+08	58.02%	3.71E+06	62.94%	3.49E+07	54.65%	16.88	0.29	2.73
19 - 20 2	2.40E+10	82.78%	3.91E+08	84.45%	6.91E+06	86.25%	6.87E+07	83.11%	16.31	0.29	2.87
20 - 21 1	1.41E+10	100.00%	2.30E+08	100.00%	4.08E+06	100.00%	4.08E+07	100.00%	16.25	0.29	2.88
Global Total 8	8.21E+10		1.48E+09		2.97E+07		2 41F+08		18 00	0.36	7 0 C

Altitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOX (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOX)	EI(NOX) EI(HC)	EI(CO)
0 - 1	5.03E+09	3.21%	7.55E+07	2.68%	6.45E+06	10.97%	6.09E+07	12.81%	14.99	1.28	12.10
1 - 2	1.74E+09	4.32%	3.96E+07	4.08%	1.01E+06	12.68%	6.53E+06	14.19%	22.77	Ŭ	3.75
2 - 3	1.74E+09	5.43%	3.96E+07	5.48%	1.01E+06	14.40%	6.53E+06	15.56%	22.77	0.58	3.75
0 - 4 4 - 0	1.74E+09	6.54%	3.96E+07	6.89%	1.01E+06	16.11%	6.53E+06	16.93%	22.77	0.58	3.75
4 - 5	1.74E+09	7.65%	3.96E+07	8.29%	1.01E+06	17.83%	6.56E+06	18.31%	22.75		3.77
5 - 6	1.74E+09	8.76%	3.96E+07	9.70%	1.01E+06	19.55%	6.56E+06	19.69%	22.75		3.77
6 - 7	1.74E+09	9.87%	3.96E+07	11.10%	1.01E+06	21.27%	6.56E+06	21.07%	22.74		3.77
7 - 8	1.74E+09	10.98%	3.96E+07	12.51%	1.01E+06	22.99%	6.56E+06	22.45%	22.75		3.77
6 - 8	2.15E+09	12.35%	4.30E+07	14.03%	1.19E+06	25.01%	8.39E+06	24.22%	20.00		3.91
9 - 10	5.17E+09	15.65%	7.54E+07	16.70%	2.48E+06	29.22%	2.02E+07	28.46%	14.59		3.91
10 - 11	6.47E+09	19.78%	9.95E+07	20.23%	2.94E+06	34.22%	2.29E+07	33.28%	15.36	0.45	3.54
11 - 12	5.83E+09	23.50%	1.05E+08	23.96%	2.55E+06	38.57%	1.74E+07	36.95%	18.03		2.99
12 - 13	7.69E+09	28.40%	1.26E+08	28.44%	3.15E+06	43.92%	2.25E+07	41.69%	16.42		2.93
13 - 14	3.55E+09	30.67%	9.09E+07	31.66%	1.12E+06	45.84%	2.29E+06	42.17%	25.62		0.65
14 - 15	3.55E+09	32.93%	9.10E+07	34.89%	1.13E+06	47.75%	2.29E+06	42.65%	25.62		0.65
15 - 16	3.55E+09	35.20%	9.09E+07	38.11%	1.12E+06	49.66%	2.29E+06	43.14%	25.62		0.65
16 - 17	3.55E+09	37.46%	9.09E+07	41.34%	1.12E+06	51.58%	2.29E+06	43.62%	25.62	0.32	0.65
17 - 18	5.45E+09	40.94%	1.20E+08	45.60%	1.67E+06	54.42%	8.21E+06	45.34%	22.03		1.50
18 - 19	1.98E+10	53.55%	3.42E+08	57.73%	5.77E+06	64.24%	5.21E+07	56.30%	17.30	0.29	2.64
19 - 20	4.15E+10	80.03%	6.82E+08	81.93%	1.20E+07	84.64%	1.18E+08	81.06%	16.45	0.29	2.84
20 - 21	3.13E+10	100.00%	5.09E+08	100.00%	9.03E+06	100.00%	9.01E+07	100.00%	16.27	0.29	2.88
Into Total O					100 L						000

Table F-6. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude assuming 500 HSCTs are flying on the 1993 AESA assessment network. (revised from NASA CR 4592) (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=15) HSCT fleet only,

Altitude Band (km)	l Fuel (kg/year)	cum fuel (%)	NOX (kg/year)	cum NOX (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)		EI(NOX) EI(HC) EI(CO)	EI(CO)
							•				
0 - 1	2.32E+09	2.84%	3.53E+07	2.41%	2.95E+06	9.88%	2.78E+07	11.45%	15.22	1.27	11.98
1 - 2	8.47E+08	3.88%	1.94E+07	3.74%	4.77E+05	11.48%	3.02E+06	12.69%	22.93	0.56	3.57
2 - 3	8.47E+08	4.91%	1.94E+07	5.07%	4.77E+05	13.07%	3.02E+06	13.94%	22.93	0.56	3.57
3 - 4	8.47E+08	5.95%	1.94E+07	6.40%	4.77E+05	14.67%	3.02E+06	15.19%	22.93		3.57
4 - 5	8.47E+08	6.99%	1.94E+07	7.72%	4.77E+05	16.27%	3.02E+06	16.43%	22.93	0.56	3.57
5 - 6	8.47E+08	8.02%	1.94E+07	9.05%	4.77E+05	17.87%	3.02E+06	17.68%	22.93	0.56	3.57
6 - 7	8.47E+08	9.06%	1.94E+07	10.38%	4.77E+05	19.47%	3.02E+06	18.93%	22.93		3.57
7 - 8	8.47E+08	10.10%	1.94E+07	11.71%	4.77E+05	21.07%	3.02E+06	20.18%	22.93	0.56	3.57
8 - 9	1.21E+09	11.59%	2.34E+07	13.31%	6.33E+05	23.18%	4.45E+06	22.01%	19.28		3.66
9 - 10	2.57E+09	14.74%	4.35E+07	16.28%	1.16E+06	27.07%	8.44E+06	25.49%	16.92		3.28
10 - 11	3.25E+09	18.72%	5.37E+07	19.96%	1.42E+06	31.83%	1.04E+07	29.79%	16.50		3.21
11 - 12	3.25E+09	22.71%	5.74E+07	23.88%	1.39E+06	36.49%	9.55E+06	33.73%	17.65	0.43	2.94
12 - 13	4.38E+09	28.07%	6.83E+07	28.55%	1.79E+06	42.48%	1.33E+07	39.22%	15.61	0.41	3.04
13 - 14	1.75E+09	30.22%	4.50E+07	31.63%	5.50E+05	44.32%	1.07E+06	39.66%	25.65		0.61
14 - 15	1.75E+09	32.37%	4.50E+07	34.71%	5.50E+05	46.16%	1.07E+06	40.10%	25.65		0.61
15 - 16	1.75E+09	34.51%	4.50E+07	37.78%	5.50E+05	48.00%	1.07E+06	40.54%	25.65		0.61
16 - 17	1.75E+09	36.66%	4.50E+07	40.86%	5.50E+05	49.84%	1.07E+06	40.98%	25.65		0.61
17 - 18	3.36E+09	40.78%	6.97E+07	45.63%	1.01E+06	53.23%	6.06E+06	43.47%	20.73	0:30	1.80
18 - 19	1.26E+10	56.23%	2.13E+08	60.17%	3.66E+06	65.49%	3.45E+07	57.71%	16.86	0.29	2.74
19 - 20	2.27E+10	84.03%	3.70E+08	85.50%	6.55E+06	87.41%	6.50E+07	84.51%	16.33	0.29	2.86
20 - 21	1.30E+10	100.00%	2.12E+08	100.00%	3.76E+06	100.00%	3.76E+07	100.00%	16.26	0.29	2.88
Clobal Total	0165110		1 465,00		2 00E 07		0 10E 00		17 04	70.0	70.0
מוטעמו וטומו			1.400+10		2.335+11		Z.4ZE+U0		18.71	19.0	2.97

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Appendix G. Altitude Distribution of Emissions for Mach 2.0 HSCT fleets

This appendix contains the tables which summarize the different Mach 2.0 HSCT emission scenarios. For each of the scenarios considered, the fuel burned and emissions (NOx, CO, and hydrocarbons) were summed over latitude and longitude and tabulated as a function of altitude in 1 km altitude increments (the resolution of the data set).

Cumulative fractions of fuel burned and emissions were calculated from the ground up to provide a simple way to evaluate how the emissions were distributed vertically. In addition, the effective emission index for each altitude band was calculated and tabulated.

The global total of fuel burned and emissions were calculated and listed at the bottom of each table. Also, included is the effective emission index for NOx, CO, and hydrocarbons, globally averaged over all locations and altitudes.

For the charts shown, the notation 1.00E+08 is equivalent to 1.00×10^8 . The emissions are in units of kilograms per year and the emission indices have units of grams of emissions per kilogram of fuel burned.

US Standard Atmosphere (1976) pressures and temperatures were used in the calculations. These altitudes correspond to the geopotential altitudes of the US Standard Atmosphere grid.

G-1. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude	ned over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=5) HSCT fleet only,	ning passenger demand corresponding to 500 Mach 2.4 HSCTs flying on the universal network.
Table G-1. Fuel	(Summed over	assuming pase

Attitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOX (kg/year)	cum NOX (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	cum CO EI(NOx) EI(HC) EI(CO) (%)	EI(HC)	EI(CO)
0 - 1	2.11E+09	2.50%	1.54E+07	3.06%	2.50E+06	8.62%	2.34E+07	9.48%	7.29	1.18	11.08
1 - 2	7.66E+08	3.41%	6.04E+06	4.25%	4.22E+05	10.07%	2.64E+06	10.55%	7.88	0.55	3.45
2 - 3	7.66E+08	4.31%	6.03E+06	5.45%	4.22E+05	11.53%	2.64E+06	11.62%	7.88	0.55	3.45
3 - 4	7.67E+08	5.22%	6.04E+06	6.65%	4.22E+05	12.98%	2.64E+06	12.69%	7.88		3.45
4 - 5	7.66E+08	6.13%	6.03E+06	7.85%	4.22E+05	14.44%	2.64E+06	13.76%	7.88		3.45
5 - 6	7.65E+08	7.03%	6.03E+06	9.04%	4.22E+05	15.89%	2.64E+06	14.83%	7.88		3.45
6 - 7	7.67E+08	7.94%	6.04E+06	10.24%	4.22E+05	17.35%	2.64E+06	15.90%			3.45
7 - 8	7.67E+08	8.85%	6.04E+06	11.44%	4.22E+05	18.80%	2.64E+06	16.97%	7.87		3.45
8-9	1.21E+09	10.29%	9.00E+06	13.23%	5.75E+05	20.79%	4.15E+06	18.65%	7.41		3.41
9 - 10	2.78E+09	13.58%	1.97E+07	17.14%	1.10E+06	24.57%	8.66E+06	22.16%	7.09		3.12
10 - 11	2.64E+09	16.69%	1.93E+07	20.97%	1.03E+06	28.11%	7.02E+06	25.00%	7.33		2.66
11 - 12	2.02E+09	19.09%	1.56E+07	24.06%	8.07E+05	30.90%	4.34E+06	26.76%	7.70		2.14
12 - 13	2.97E+09	22.60%	2.18E+07	28.39%	1.04E+06	34.47%	6.56E+06	29.42%	7.35		2.21
13 - 14	1.51E+09	24.39%	1.22E+07	30.81%	4.75E+05	36.11%	9.40E+05	29.80%	8.07		0.62
14 - 15	1.51E+09	26.18%	1.22E+07	33.23%	4.75E+05	37.75%	9.35E+05	30.18%	8.08		0.62
15 - 16	1.52E+09	27.97%	1.22E+07	35.66%	4.77E+05	39.39%	9.54E+05	30.56%	8.07	0.31	0.63
16 - 17	6.67E+09	35.86%	3.82E+07	43.25%	1.95E+06	46.12%	1.66E+07	37.30%	5.73	0.29	2.50
17 - 18	1.82E+10	57.44%	9.70E+07	62.51%	5.27E+06	64.29%	5.15E+07	58.14%	5.32	0.29	2.82
18 - 19	2.66E+10	88.88%	1.40E+08	90.22%	7.65E+06	90.67%	7.63E+07	89.04%	5.26		2.87
19 - 20	9.39E+09	100.00%	4.93E+07	100.00%	2.71E+06	100.00%	2.71E+07	100.00%	5.25	0.29	2.88
Global Total	8 45F+10		5 04F+08		2 90F107		2 47E 108		F OR		000
Global Total	8.45E+10		5.04E+08		2.90E+07		2.47E+08		- 1	5.96	5.96 0.34

Table G-2. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude assuming passenger demand corresponding to 1000 Mach 2.4 HSCTs flying on the universal network. (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=5) HSCT fleet only,

Altitude Band	Fuel	cum fuel	NOX	cum NOX	Ч	cum HC	8	cum CO	EI(NOX) EI(HC) EI(CO)	EI(HC)	EI(CO)
(km)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)			
0 - 1	4.58E+09	2.87%	3.33E+07	3.46%	5.57E+06	9.85%	5.25E+07	10.99%	7.28	1.22	11.46
1 - 2	1.59E+09	3.86%	1.25E+07	4.75%	9.06E+05	11.45%	5.85E+06	12.22%	7.86	0.57	3.68
2 - 3	1.59E+09	4.86%	1.25E+07	6.04%	9.06E+05	13.05%	5.85E+06	13.44%	7.86	0.57	3.68
3 - 4	1.59E+09	5.85%	1.25E+07	7.34%	9.06E+05	14.66%	5.85E+06	14.67%	7.86	0.57	3.68
4 - 5	1.59E+09	6.85%	1.25E+07	8.63%	9.09E+05	16.26%	5.88E+06	15.90%	7.86	0.57	3.70
5-6	1.59E+09	7.84%	1.25E+07	9.93%	9.09E+05	17.87%	5.89E+06	17.13%	7.86	0.57	3.70
6 - 7	1.59E+09	8.84%	1.25E+07	11.22%	9.10E+05	19.48%	5.89E+06	18.36%	7.86	0.57	3.70
7 - 8	1.59E+09	9.84%	1.25E+07	12.52%	9.10E+05	21.09%	5.89E+06	19.59%	7.86	0.57	3.70
8-9	2.22E+09	11.23%	1.67E+07	14.25%	1.12E+06	23.08%	8.00E+06	21.27%	7.50	0.51	3.60
9 - 10	5.03E+09	14.37%	3.57E+07	17.94%	2.07E+06	26.74%	1.65E+07	24.72%	7.09	0.41	3.28
10 - 11	5.57E+09	17.86%	4.01E+07	22.10%	2.22E+06	30.66%	1.64E+07	28.16%	7.21	0.40	2.95
11 - 12	5.23E+09	21.14%	3.87E+07	26.11%	2.08E+06	34.33%	1.38E+07	31.04%	7.39	0.40	2.63
12 - 13	6.72E+09	25.34%	4.88E+07	31.17%	2.38E+06	38.54%	1.62E+07	34.43%	7.26	0.35	2.41
13 - 14	3.03E+09	27.24%	2.45E+07	33.70%	9.63E+05	40.24%	2.00E+06	34.84%	8.07	0.32	0.66
14 - 15	3.03E+09	29.14%	2.45E+07	36.24%	9.62E+05	41.95%	1.99E+06	35.26%	8.07	0.32	0.66
15 - 16	3.04E+09	31.04%	2.45E+07	38.78%	9.65E+05	43.65%	2.02E+06	35.68%	8.07	0.32	0.66
16 - 17	1.01E+10	37.35%	6.00E+07	45.00%	2.98E+06	48.92%	2.34E+07	40.58%	5.96	0:30	2.33
17 - 18	2.89E+10	55.44%	1.56E+08	61.14%	8.37E+06	63.72%	8.01E+07	57.34%	5.39	0.29	2.77
18 - 19	4.88E+10	85.97%	2.57E+08	87.81%	1.41E+07	88.59%	1.39E+08	86.49%	5.28	0.29	2.86
19 - 20	2.24E+10	100.00%	1.18E+08	100.00%	6.46E+06	100.00%	6.45E+07	100.00%	5.25	0.29	2.88
Global Total	1 60E±11		0 655-08		5 RRE-07		A 785-08		e Di	0.35	00 6
	1.221				0.001701		4.1 ULTVO		5.5	22.2	C.33

G-3

		ravisa
ed, emissions, cumulative fractions of emissions, and emission indices as a function of attitude		demand corresponding to 500 Mach 2.4 HSCTs flying on the 1993 AESA assessment network (revise
n indices as	T fleet only,	1993 AFSA
and emissio	Ox)=5) HSC	ving on the
emissions,	ominal EI(N	A HSCTs fl
fractions of	Mach 2.0 (N	500 Mach 2
, cumulative	Ide) for the I	sponding to
d, emissions	de and Longitude) for the Mach 2.0 (Nominal El(NOx)=5) HSCT fleet only,	emand corre
able G-3. Fuel burned	tummed over Latitude	suming passenger de
able G-3.	Summed c	ssumina p

(km)	Fuel (kg/year)	cum ruei (%)	NOX (kg/year)	cum NOX (%)	(kg/year)	cum HC (%)	CO (kg/year)	cum co (%)		EI(HC)	
0 - 1	2.11E+09	2.52%	1.54E+07	3.07%	2.55E+06	8.81%	2.39E+07	9.75%	7.32	1.21	11.35
1 - 2	7.76E+08	3.45%	6.11E+06	4.29%	4.30E+05	10.30%	2.71E+06	10.85%		0.55	3.50
2 - 3	7.76E+08	4.38%	6.11E+06	5.51%	4.30E+05	11.79%	2.71E+06	11.96%	7.87	0.55	3.50
3 - 4	7.76E+08	5.30%	6.11E+06	6.72%	4.30E+05	13.27%	2.71E+06	13.06%	7.87	0.55	3.50
4 - 5	7.76E+08	6.23%	6.11E+06	7.94%	4.30E+05	14.76%	2.71E+06	14.17%		0.55	3.50
5 - 6	7.76E+08	7.16%	6.11E+06	9.16%	4.30E+05	16.25%	2.71E+06	15.27%		0.55	3.50
6 - 7	7.76E+08	8.09%	6.11E+06	10.38%	4.30E+05	17.74%	2.71E+06	16.38%	7.87	0.55	3.50
7 - 8	7.76E+08	9.02%	6.11E+06	11.59%	4.30E+05	19.22%	2.71E+06	17.48%	7.87	0.55	3.50
8 - 9	1.15E+09	10.39%	8.58E+06	13.30%	5.56E+05	21.15%	3.90E+06	19.07%	7.49	0.49	3.40
9 - 10	2.48E+09	13.35%	1.80E+07	16.90%	9.88E+05	24.56%	7.04E+06	21.94%	7.28	0.40	2.84
10 - 11	2.80E+09	16.70%	2.04E+07	20.97%	1.09E+06	28.32%	7.56E+06	25.03%	7.30	0.39	2.70
11 - 12	2.90E+09	20.17%	2.13E+07	25.22%	1.11E+06	32.17%	7.35E+06	28.02%	7.37	0.38	2.54
12 - 13	3.82E+09	24.74%	2.74E+07	30.69%	1.33E+06	36.78%	9.46E+06	31.88%	7.18	0.35	2.47
13 - 14	1.51E+09	26.55%	1.22E+07	33.13%	4.76E+05	38.42%	9.38E+05	32.26%	8.08	0.31	0.62
14 - 15	1.51E+09	28.37%	1.22E+07	35.57%	4.76E+05	40.07%	9.38E+05	32.65%	8.08	0.31	0.62
15 - 16	1.52E+09	30.18%	1.23E+07	38.02%	4.78E+05	41.72%	9.54E+05	33.03%	8.07	0.31	0.63
16 - 17	7.01E+09	38.57%	3.99E+07	45.97%	2.05E+06	48.81%	1.77E+07	40.25%	5.70	0.29	2.53
17 - 18	1.75E+10	59.46%	9.30E+07	64.51%	5.04E+06	66.25%	4.92E+07	60.32%	5.33	0.29	2.82
18 - 19	2.53E+10	89.76%	1.33E+08	91.05%	7.30E+06	91.48%	7.27E+07	89.96%	5.26	0.29	2.87
19 - 20	8.56E+09	100.00%	4.49E+07	100.00%	2.47E+06	100.00%	2.46E+07	100.00%	5.25	0.29	2.88
Global Total	8.36E+10		5.02E+08		2.89F+07		2.45F+08		900	0.35	204

Table G-4. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=15) HSCT fleet only, assuming passenger demand corresponding to 500 Mach 2.4 HSCTs flying on the universal network.

Altitude Band	Fuel	cum fuel	NOX	cum NOX	우	cum HC	8	cum CO	EI(NOX)	EI(HC)	EI(CO)
(km)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)			
·	0 110,000	2 E0%	3 155-07	0 13%	2.50E+06	8.62%	2.34E+07	9.48%	14.89	1.18	11.08
- c - - 	2.11E+U3 7 66E+08	3 41%	0.15C+0/	3 25%	4.22E+05	10.07%	2.64E+06	10.55%	21.58	0.55	3.45
- c	7.66E108	4.31%	1.65E+07	4.37%	4.22E+05	11.53%	2.64E+06	11.62%	21.58	0.55	3.45
0 V C	7.67F.408	5 22%	1.65E+07	5.49%	4.22E+05	12.98%	2.64E+06	12.69%	21.58	0.55	3.45
	7 66F-08	6 13%	1.65E+07	6.61%	4.22E+05	14.44%	2.64E+06	13.76%	21.58		
τ μ 1 - μ	7 655408	7 03%	1 65E+07	7.73%	4.22E+05	15.89%	2.64E+06	14.83%	21.58		3.45
	7 675-108	2000.1	1.65E+07	8.85%	4.22E+05	17.35%	2.64E+06	15.90%	21.58		3.45
- C	7 67F 108	8 85%	1.65E+07	9.97%	4.22E+05	18.80%	2.64E+06	16.97%	21.57		
	1 215-00	10.29%	2 54F+07	11.69%	5.75E+05	20.79%	4.15E+06	18.65%			
01.0	9 78F109	13.58%	5.75E+07	15.59%	1.10E+06	24.57%	8.66E+06	22.16%			3.12
0 0 F	2.7 JC 100	16.69%	5.64E+07	19.40%	1.03E+06	28.11%	7.02E+06	25.00%			
	2.07E+09	19 09%	4.51E+07	22.46%	8.07E+05	30.90%	4.34E+06	26.76%			2.14
10 10	2 97F109	22.60%	6.45E+07	26.83%	1.04E+06	34.47%	6.56E+06	29.42%	21.75		
12 14	1 51 1 400	24 39%	3.63E+07	29.29%	4.75E+05	36.11%	9.40E+05	29.80%	_		
	1 515-00	26.18%	3 63F+07	31.75%	4.75E+05	37.75%	9.35E+05	30.18%			0.62
0 + + + + + + + + + + + + + + + + + + +	1 596400	27.07%	3 64F+07	34.21%	4.77E+05	39.39%	9.54E+05	30.56%	23.98		
10 - 10 14 - 17	6.67E100	35.86%	1.14F+08	41.95%	1.95E+06	46.12%	1.66E+07	37.30%	17.15	0.29	2.50
17 - 18	1 R2F-10	57 44%	2.91E+08	61.65%	5.27E+06	64.29%	5.15E+07	58.14%	15.95		2.82
18 - 10	2 66F+10	88.88%	4.19E+08	89.99%	7.65E+06	90.67%	7.63E+07	89.04%	15.76	0.29	
19 - 20	9.39E+09	100.00%	1.48E+08	100.00%	2.71E+06	100.00%	2.71E+07	100.00%	, 15.73	0.29	2.88
Cickel Tedel	0 460-40		1 485-00		2 90F+07		2.47E+08		17.48	0.34	2.92
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Table G-5. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOX)=15) HSCT fleet only, assuming passenger demand corresponding to 1000 Mach 2.4 HSCTs flying on the universal network.

Altitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOX (ka/vear)	cum NOX	HC (ka/vear)	cum HC	CO	cum CO	EI(NOX) EI(HC)	EI(HC)	EI(CO)
				1	had your	(e)	(rg/year)	(%)			
0 - 1	4.58E+09	2.87%	6.69E+07	2.37%	5.57E+06	9 85%	5 255-07	10 00%	11 60	сс т	
1 - 2	1.59E+09	3.86%	3.40F+07	3 58%	O DEFIDE	14 AE0		9/ 66'01	14.00	7.1	11.40
2 - 3	1 595-00	4 86%	2 40E 07	0,000 A	9.00L-100	%C+7.11	00+300.0	12.22%	21.38	0.57	3.68
) - (*			0.4004.00	4./3%	8.00E+05	13.05%	5.85E+06	13.44%	21.38	0.57	3.68
	60+360.1	5.85%	3.40E+07	5.99%	9.06E+05	14.66%	5.85E+06	14.67%	21.38	0.57	3.68
4 r 0 0	1.59E+09	6.85%	3.40E+07	7.20%	9.09E+05	16.26%	5.88E+06	15.90%	21.36	0.57	3 70
0 - -	1.59E+09	7.84%	3.40E+07	8.40%	9.09E+05	17.87%	5.89E+06	17.13%	21.36	0.57	3 70
	1.59E+09	8.84%	3.40E+07	9.61%	9.10E+05	19.48%	5.89E+06	18.36%	21.36	0.57	3 70
8 - /	1.59E+09	9.84%	3.40E+07	10.82%	9.10E+05	21.09%	5.89E+06	19.59%	21.36	0.57	04.00
6 - 8	2.22E+09	11.23%	4.64E+07	12.47%	1.12E+06	23.08%	8 ODF TOF	24 27%	00.13		
9 - 10	5.03E+09	14.37%	1.04E+08	16.14%	2.07F+06	26 74%	1 66E+07	0/ 17.12	20.32		00.0 00.0
10 - 11	5.57E+09	17.86%	1 17F+08	20 20%	2 22E 106	20 6 6 9V		24.12%	80'NZ	0.41	3.28
11 - 12	5 235-00	01 4 40/		500070	2,225	20.00%	1.04540/	28.16%	21.00	0.40	2.95
4 7 7 7	0.201-00	Z1.14%	1.13E+08	24.29%	2.08E+06	34.33%	1.38E+07	31.04%	21.50	0.40	2.63
12 - 13	0./ZE+U9	25.34%	1.44E+08	29.41%	2.38E+06	38.54%	1.62E+07	34.43%	21.48	0.35	241
13 - 14	3.03E+09	27.24%	7.27E+07	32.00%	9.63E+05	40.24%	2.00E+06	34.84%	23.98	0.32	0.66
- 15 	3.03E+09	29.14%	7.27E+07	34.58%	9.62E+05	41.95%	1.99E+06	35 26%	23 08	0.20	00.00
15 - 16	3.04E+09	31.04%	7.28E+07	37.16%	9.65E+05	43.65%	2.02E+06	35 68%	23.06	0.02	00.0
16 - 17	1.01E+10	37.35%	1.79E+08	43.52%	2 98F106	AR 0.2%	0 245.07	10 500			
17 - 18	2.89F+10	55 44%	A A7E LOD		001100	0/ 76.0F		40.28%	17.80	0.30	2.33
18 - 10		002020		00.09%	0.3/E+00	63.72%	8.01E+07	57.34%	16.15	0.29	2.77
	4.000+10	%/6.00	/./1E+08	87.48%	1.41E+07	88.59%	1.39E+08	86.49%	15.82	0.29	2.86
13 - 20	2.246+10	100.00%	3.53E+08	100.00%	6.46E+06	100.00%	6.45E+07	100.00%	15.73	0.29	2.88
Global Total	1.60E+11		2,82F+09		5 GELUT		1 701 .00				
					0.001701		4./0E+U8		1 / .63	0.35	2.99

G-6

	Altitude Band (km)	Fuel (ko/vear)	cum fuel (%)	NOx (kg/year)	cum NOx (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOX)	EI(HC)	EI(CO)
ļ									•			
	0 - 1	2.11E+09	2.52%	3.11E+07	2.12%	2.55E+06	8.81%	2.39E+07	9.75%	14.77	1.21	11.35
	1 - 2	7.76E+08	3.45%	1.67E+07	3.25%	4.30E+05	10.30%	2.71E+06	10.85%	21.54	0.55	3.50
	2 - 3	7.76E+08	4.38%	1.67E+07	4.39%	4.30E+05	11.79%	2.71E+06	11.96%		0.55	3.50
	3 - 4	7.76E+08	5.30%	1.67E+07	5.53%	4.30E+05	13.27%	2.71E+06	13.06%	21.54	0.55	3.50
	4 - 5	7.76E+08	6.23%	1.67E+07	6.67%	4.30E+05	14.76%	2.71E+06	14.17%	21.54	0.55	3.50
	5 - 6	7.76E+08	7.16%	1.67E+07	7.80%	4.30E+05	16.25%	2.71E+06	15.27%	21.54	0.55	3.50
	6 - 7	7.76E+08	8.09%	1.67E+07	8.94%	4.30E+05	17.74%	2.71E+06	16.38%	21.54		3.50
	7 - 8	7.76E+08	9.02%	1.67E+07	10.08%	4.30E+05	19.22%	2.71E+06	17.48%			
-	6 - 8	1.15E+09	10.39%	2.41E+07	11.72%	5.56E+05	21.15%	3.90E+06	19.07%	21.06		
	9 - 10	2.48E+09	13.35%	5.24E+07	15.29%	9.88E+05	24.56%	7.04E+06	21.94%			
_	10 - 11	2.80E+09	16.70%	5.97E+07	19.35%	1.09E+06	28.32%	7.56E+06	25.03%			
	11 - 12	2.90E+09	20.17%	6.24E+07	23.60%	1.11E+06	32.17%	7.35E+06	28.02%			
	12 - 13	3.82E+09	24.74%	8.15E+07	29.14%	1.33E+06	36.78%	9.46E+06	31.88%			
	13 - 14	1.51E+09	26.55%	3.64E+07	31.62%	4.76E+05	38.42%	9.38E+05	32.26%	24.02	0.31	0.62
	14 - 15	1.51E+09	28.37%	3.64E+07	34.09%	4.76E+05	40.07%	9.38E+05	32.65%	_		
	15 - 16	1.52E+09	30.18%	3.65E+07	36.58%	4.78E+05	41.72%	9.54E+05	33.03%	23.99		
	16 - 17	7.01E+09	38.57%	1.19E+08	44.71%	2.05E+06	48.81%	1.77E+07	40.25%	17.04		2.53
	17 - 18	1.75E+10	59.46%	2.79E+08	63.67%	5.04E+06	66.25%	4.92E+07	60.32%	15.96		2.82
	18 - 19	2.53E+10	89.76%	3.99E+08	90.84%	7.30E+06	91.48%	7.27E+07	89.96%	15.76		
	19 - 20	8.56E+09	100.00%	1.35E+08	100.00%	2.47E+06	100.00%	2.46E+07	100.00%	15.73	0.29	2.88
	Global Total	8.36E+10		1.47E+09		2.89E+07		2.45E+08		17.58	0.35	2.94

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Appendix H. Altitude Distribution of Emissions for Year 2015 subsonic fleets

This appendix contains the tables which summarize the different Year 2015 subsonic emission scenarios occurring with fleets of 0, 500, and 1000 Mach 2.4 HSCTs. For each of the scenarios considered, the fuel burned and emissions (NOx, CO, and hydrocarbons) were summed over latitude and longitude and tabulated as a function of altitude in 1 km altitude increments (the resolution of the data set).

Cumulative fractions of fuel burned and emissions were calculated from the ground up to provide a simple way to evaluate how the emissions were distributed vertically. In addition, the effective emission index for each altitude band was calculated and tabulated.

The global total of fuel burned and emissions were calculated and listed at the bottom of each table. Also, included is the effective emission index for NOx, CO, and hydrocarbons, globally averaged over all locations and altitudes.

For the charts shown, the notation 1.00E+08 is equivalent to 1.00×10^8 . The emissions are in units of kilograms per year and the emission indices have units of grams of emissions per kilogram of fuel burned.

US Standard Atmosphere (1976) pressures and temperatures were used in the calculations. These altitudes correspond to the geopotential (pressure) altitudes of the US Standard Atmosphere grid. Table H-1. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic passenger fleet, assuming 500 Mach 2.4 HSCTs are flying on the universal network.

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Altitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOX (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOX)	EI(NOX) EI(HC) EI(CO)	EI(CO)
0 - 1	2.61E+10	11.78%	2.50E+08	12.20%	3.06F+07	32 80%	3 40F+08	%PP 68	0 56	1 17	12 00
1 - 2	6.95E+09	14.91%	8.75E+07	16.47%	6.37E+06	39.62%	6.03F+07	38.20%	-	0 00	8.67 8.67
2 - 3	6.09E+09	17.65%	7.48E+07	20.12%	5.44E+06	45.44%	5.13E+07	43.10%	12.29	0.89	0.07 8 43
3 - 4	7.81E+09	21.17%	1.05E+08	25.22%	4.94E+06	50.72%	4.52E+07	47.43%	-	0.63	5.79
4 - 5	6.68E+09	24.18%	8.18E+07	29.21%	5.47E+06	56.58%	4.71E+07	51.93%	•	0.82	7.06
5 - 6	6.11E+09	26.93%	7.26E+07	32.76%	4.52E+06	61.42%	4.72E+07	56.44%	11.89	0.74	7.73
6 - 7	5.19E+09	29.26%	5.98E+07	35.68%	3.63E+06	65.31%	4.05E+07	60.30%	11.53	0.70	7.80
7 - 8	5.52E+09	31.75%	6.09E+07	38.65%	3.99E+06	69.58%	4.37E+07	64.48%	11.03	0.72	7.93
8-9	6.13E+09	34.51%	6.54E+07	41.84%	4.23E+06	74.11%	4.58E+07	68.86%	10.67	0.69	7.48
9 - 10	6.73E+09	37.54%	6.67E+07	45.09%	4.17E+06	78.57%	4.39E+07	73.05%	9.91	0.62	6.52
10 - 11	4.32E+10	57.02%	3.39E+08	61.62%	6.44E+06	85.47%	9.47E+07	82.10%	7.83	0.15	2.19
11 - 12	9.54E+10	100.00%	7.86E+08	100.00%	1.36E+07	100.00%	1.87E+08	100.00%	8.24	0.14	1.96
Global Total	2.22E+11		2.05E+09		9.34F+07		1 05F+09		0 23	040	4 7 A

Table H-2. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic passenger fleet assuming 1000 Mach 2.4 HSCTs are flying on the universal network.

Altitude Band	Fuel	cum fuel	NOX	cum NOX	ЧĊ	cum HC	00	cum CO	EI(NOX)	EI(HC) EI(CO)	EI(CO)
(km)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	,		
0 - 1	2.48E+10	12.61%	2.32E+08	12.83%	2.92E+07	33.56%	3.27E+08	33.46%	9.32	1.18	13.18
1 - 2	6.66E+09	15.99%	8.24E+07	17.40%	6.11E+06	40.57%	5.81E+07	39.39%	12.36	0.92	8.71
2 - 3	5.83E+09	18.95%	7.03E+07	21.29%	5.19E+06	46.54%	4.93E+07	44.43%	12.05	0.89	8.46
3 - 4	7.41E+09	22.72%	9.71E+07	26.68%	4.72E+06	51.95%	4.34E+07	48.86%	13.10	0.64	5.85
4 - 5	6.40E+09	25.97%	7.70E+07	30.95%	5.25E+06	57.97%	4.52E+07	53.49%	12.03	-	7.07
5 - 6	5.84E+09	28.93%	6.81E+07	34.72%	4.29E+06	62.90%	4.53E+07	58.12%	11.67	Ĩ	7.76
6 - 7	4.93E+09	31.43%	5.55E+07	37.80%	3.41E+06	66.82%	3.89E+07	62.09%	11.26	-	7.88
7 - 8	5.24E+09	34.09%	5.64E+07	40.93%	3.75E+06	71.13%	4.19E+07	66.37%	10.77	-	8.00
8 - 9	5.81E+09	37.04%	6.05E+07	44.29%	3.96E+06	75.68%	4.38E+07	70.85%	10.43	-	7.54
9 - 10	6.31E+09	40.25%	6.13E+07	47.68%	3.90E+06	80.15%	4.18E+07	75.12%	9.71	-	6.62
10 - 11	3.89E+10	29.99%	2.97E+08	64.17%	5.84E+06	86.86%	8.77E+07	84.09%	7.65	-	2.26
11 - 12	7.88E+10	100.00%	6.46E+08	100.00%	1.14E+07	100.00%	1.56E+08	100.00%	8.20	-	1.98
Global Total 1.97E+11	1.97E+11		1.80E+09		8.71E+07		9.78F+08		916	0.44	4 07

Table H-3. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic passenger fleet assuming no HSCTs are flying on the universal network.

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Altitude Band	Fuel	cum fuel	NOX	cum NOX	Я	cum HC	8	cum CO	EI(NOX) EI(HC) EI(CO)	EI(HC)	EI(CO)
(km)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)			·
0 - 1	2.73E+10	10.92%	2.67E+08	11.51%	3.18E+07	32.05%	3.49E+08	31.44%	9.78	1.17	12.79
1 - 2	7.20E+09	13.80%	9.22E+07	15.49%	6.57E+06	38.66%	6.19E+07	37.01%	-	0.91	8.60
2 - 3	6.32E+09	16.33%	7.92E+07	18.90%	5.63E+06	44.33%	5.29E+07	41.78%	-	0.89	8.38
3 - 4	8.18E+09	19.60%	1.12E+08	23.71%	5.13E+06	49.50%	4.68E+07	45.99%	13.65	0.63	5.72
4 - 5	6.92E+09	22.37%	8.61E+07	27.42%	5.67E+06	55.20%	4.87E+07	50.37%		0.82	7.03
5-6	6.35E+09	24.91%	7.68E+07	30.73%	4.73E+06	59.96%	4.87E+07	54.75%		0.74	7.67
6 - 7	5.44E+09	27.08%	6.41E+07	33.49%	3.82E+06	63.81%	4.20E+07	58.53%	11.79	0.70	7.72
7 - 8	5.78E+09	29.40%	6.52E+07	36.30%	4.21E+06	68.05%	4.53E+07	62.61%		0.73	7.84
8-9	6.42E+09	31.97%	7.00E+07	39.31%	4.47E+06	72.55%	4.75E+07	66.88%	10.90	0.70	7.40
9 - 10	7.50E+09	34.97%	7.53E+07	42.56%	4.45E+06	77.02%	4.62E+07	71.04%	10.04	0.59	6.15
10 - 11	5.04E+10	55.13%	4.04E+08	59.95%	7.30E+06	84.37%	1.06E+08	80.54%	8.01	0.14	2.09
11 - 12	1.12E+11	100.00%	9.29E+08	100.00%	1.55E+07	100.00%	2.16E+08	100.00%	8.28	0.14	1.93
Global Total	2.50E+11		2.32E+09		9.94E+07		1.11E+09		9.28	0.40	4.44

Table H-4. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic cargo fleet

Altitude Band Fuel cum fuel NOx cum NO (km) (kg/year) (%) (kg/year) (%) 0 -1 4.24E+08 7.52% 4.04E+06 8.23 1 -2 1.04E+08 7.52% 4.04E+06 8.23 1 -2 1.04E+08 7.52% 1.33E+06 10.94 2 -3 1.02E+08 11.16% 1.36E+06 17.34 2 -3 1.02E+08 13.46% 1.78E+06 19.68 3 -4 1.30E+08 13.46% 1.15E+06 20.36 4 -5 9.27E+07 15.10% 1.15E+06 24.36 5 -6 9.62E+07 16.81% 1.15E+06 24.36 7 -8 1.05E+08 20.39% 1.15E+06 26.72 8 -9 1.12E+08 20.39% 1.17E+06 26.11 9 10 1.11E+08 24.33% 1.10E+06 31.36 9 10								
1 4.24E+08 7.52% 4.04E+06 2 1.04E+08 9.35% 1.33E+06 1 3 1.02E+08 11.16% 1.36E+06 1 4 1.30E+08 13.46% 1.78E+06 1 5 9.27E+07 15.10% 1.15E+06 1 6 9.62E+07 16.81% 1.15E+06 2 7 9.69E+07 16.81% 1.15E+06 2 8 1.05E+08 20.39% 1.15E+06 2 9 69E+07 18.52% 1.15E+06 2 9 10.11E+08 20.39% 1.15E+06 2 9 10 1.15E+08 20.39% 1.16E+06 2 9 10 23.36% 1.16E+06 3 10 1.11E+08 24.33% 1.10E+06 3	cui	HC (ka/vear)	cum HC (%)	CO (ka/vear)	cum CO (%)	EI(NOX) EI(HC) EI(CO)	EI(HC)	EI(CO)
1 4.24E+08 7.52% 4.04E+06 1 2 1.04E+08 9.35% 1.33E+06 1 3 1.02E+08 11.16% 1.36E+06 1 4 1.30E+08 13.46% 1.78E+06 1 5 9.27E+07 15.10% 1.15E+06 1 6 9.62E+07 16.81% 1.15E+06 2 7 9.69E+07 18.52% 1.15E+06 2 8 1.05E+08 20.39% 1.15E+06 2 9 105E+08 20.39% 1.15E+06 2 10 1.11E+08 22.36% 1.17E+06 2 10 1.11E+08 24.33% 1.10E+06 3		1-16-1	7-17					
2 1.04E+08 9.35% 1.33E+06 3 1.02E+08 11.16% 1.36E+06 4 1.30E+08 13.46% 1.78E+06 5 9.27E+07 15.10% 1.15E+06 6 9.62E+07 16.81% 1.15E+06 7 9.69E+07 18.52% 1.15E+06 8 1.05E+08 20.39% 1.15E+06 9 0.112E+08 20.39% 1.15E+06 9 1.12E+08 20.39% 1.17E+06 9 1.11E+08 24.33% 1.10E+06 10 1.11E+08 24.33% 1.10E+06	:+06 8.23%	1.05E+06	29.38%	7.36E+06	26.59%	9.52	2.47	17.35
3 1.02E+08 11.16% 1.36E+06 4 1.30E+08 13.46% 1.78E+06 5 9.27E+07 15.10% 1.15E+06 6 9.62E+07 16.81% 1.15E+06 7 9.69E+07 18.52% 1.15E+06 8 1.05E+08 20.39% 1.15E+06 9 1.12E+08 20.39% 1.15E+06 9 1.12E+08 20.39% 1.17E+06 10 1.11E+08 24.33% 1.10E+06 11 6.54E+08 35.92% 5.71E+06	+06 10.94%	1.84E+05	34.54%	1.24E+06	31.07%	12.81	1.77	11.97
4 1.30E+08 13.46% 1.78E+06 5 9.27E+07 15.10% 1.15E+06 6 9.62E+07 16.81% 1.15E+06 7 9.69E+07 18.52% 1.15E+06 8 1.05E+08 20.39% 1.15E+06 9 1.12E+08 20.39% 1.17E+06 9 1.11E+08 22.36% 1.10E+06 10 1.11E+08 24.33% 1.10E+06	:+06 13.72%	1.95E+05	40.00%	1.26E+06	35.64%	13.32	1.90	12.36
5 9.27E+07 15.10% 1.15E+06 6 9.62E+07 16.81% 1.15E+06 7 9.69E+07 18.52% 1.15E+06 8 1.05E+08 20.39% 1.15E+06 9 1.12E+08 20.39% 1.15E+06 9 1.12E+08 20.39% 1.17E+06 10 1.11E+08 24.33% 1.10E+06 11 6.54E+08 35.92% 5.71E+06	+06 17.34%	1.64E+05	44.61%	1.12E+06	39.69%	13.71	1.27	8.65
6 9.62E+07 16.81% 1.15E+06 7 9.69E+07 18.52% 1.15E+06 8 1.05E+08 20.39% 1.15E+06 9 1.12E+08 20.39% 1.17E+06 10 1.11E+08 24.33% 1.10E+06 11 6.54E+08 35.92% 5.71E+06	+06 19.68%	1.71E+05	49.41%	1.14E+06	43.81%	12.36	1.84	12.30
7 9.69E+07 18.52% 1.15E+06 8 1.05E+08 20.39% 1.15E+06 9 1.12E+08 22.36% 1.17E+06 10 1.11E+08 24.33% 1.10E+06 11 6.54E+08 35.92% 5.71E+06	+06 22.03%	1.78E+05	54.39%	1.17E+06	48.03%	11.99	1.85	12.16
8 1.05E+08 20.39% 1.15E+06 9 1.12E+08 22.36% 1.17E+06 10 1.11E+08 24.33% 1.10E+06 11 6.54E+08 35.92% 5.71E+06	+06 24.36%	1.76E+05	59.33%	1.13E+06	52.13%	11.83	1.82	11.70
9 1.12E+08 22.36% 1.17E+06 10 1.11E+08 24.33% 1.10E+06 11 6.54E+08 35.92% 5.71E+06	+06 26.72%	1.93E+05	64.76%	1.22E+06	56.53%	10.97	1.84	11.59
10 1.11E+08 24.33% 1.10E+06 11 6.54E+08 35.92% 5.71E+06	+06 29.11%	1.91E+05	70.12%	1.19E+06	60.84%	10.52	1.71	10.68
11 6.54E+08 35.92% 5.71E+06	+06 31.36%	2.00E+05	75.75%	1.20E+06	65.19%	9.94	1.81	10.86
	+06 42.99%	2.38E+05	82.43%	1.94E+06	72.21%	8.72	0.36	2.97
11 - 12 3.62E+09 100.00% 2.80E+07 100.00	:+07 100.00%	6.26E+05	100.00%	7.69E+06	100.00%	7.73	0.17	2.13
Giobal Total 5.64E+09 4.91E+07	E+07	3.56E+06		2.77E+07		8.69	0.63	4.90

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Appendix I. 3-Dimensional Scenario Data Format

The three dimensional emission scenario data files calculated by Boeing were delivered to NASA Langley electronically in a slightly different format than that used previously (Ref. 1). In addition to fuel and emissions, the total miles flown within in a cell is also provided. The format is now:

i, j, k; fuel(lb/day); NOx(lb/day); CO(lb/day); HC(lb/day); distance (nautical miles/day)

Only non-zero values are included in the ASCII data files.

<u>Altitude:</u>

Index k means emissions in the band from altitude k to k+1 i.e. index 19 is emissions in the 19-20 km band Values run from 0 to 22

Latitude:

Index i means emissions in the band from latitude i to i+1 values run from 0 to 179

For i<=89 northern hemisphere index 0 is emissions from equator to 1 degree N

For i>=90 southern hemisphere index 90 is emissions from equator to 1 degree S index 179 is emissions from 89S-90S

- Longitude: Wrap all the way around the globe.
- Index j means emissions in the longitude band j to j+1 values run from 0 to 359

For j<=179 east of prime meridian index 0 is emissions from 0-1E index 179 is emissions from 179E-180E

For j>=180 west of prime meridian index 180 is emissions from -180W - -179W index 359 is emissions from -1W - 0

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This report describes the development of a three-dimensional database of aircraft fuel burn and emissions (fuel burned,NOx, CO, and hydrocarbons) from projected fleets of high speed civil transports (HSCTs) on a universal airline network. Inventories for 500 and 1000 HSCT fleets, as well as the concurrent subsonic fleets, were calculated.						
The objective of this work was to evaluate the changes in geographical distribution of the HSCT emissions as the fleet size grew from 500 to 1000 HSCTs. For this work, a new expanded HSCT network was used and flights projected using a market penetration analysis rather than assuming equal penetration as was done in the earlier studies. Emission inventories on this network were calculated for both Mach 2.0 and Mach 2.4 HSCT fleets with NOx cruise emission indices of approximately 5 and 15 grams NOx/kilogram fuel.						
These emissions inventories are available for use by atmospheric scientists conducting the Atmospheric Effects of Stratospheric Aircraft (AESA) modeling studies. Fuel burned and emissions of nitrogen oxides (NOx as NO2), carbon monoxide, and hydrocarbons have been calculated on a 1 degree latitude x 1 degree longitude x 1 kilometer altitude grid and delivered to NASA as electronic files.						
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