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# A Wind Tunnel Investigation of Three NACA 1-Series Inlets at Mach Numbers Up to 0.92

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# **SUMMARY**

Pressure distributions on three NACA 1-series inlets have been obtained in the Langley 16-Foot Transonic Tunnel. The cowl diameter ratio (ratio of cowl highlight diameter to cowl maximum diameter) was 0.85 for all three inlets. The cowl length ratio (ratio of cowl length to cowl maximum diameter) was 1.0 for two of the inlets (NACA 1-85-100) and 0.439 for the other (NACA 1-85-43.9) inlet. One of the inlets with a cowl length ratio of 1.0 had an internal contraction ratio (ratio of highlight area to throat area) of 1.009 and the other had a contraction ratio of 1.250. The inlet with a cowl length ratio of 0.439 also had an internal contraction ratio of 1.250. All three inlets had longitudinal rows of static pressure orifices on the top and bottom external cowl surfaces. The inlet with a contraction ratio of 1.009 also had a row of static pressure orifices on the side of the cowl (external surface). The two inlets with a contraction ratio of 1.250 had a longitudinal row of static pressure orifices on the diffuser surface.

The NACA 1-85-100 inlets were tested in the Mach number range from 0.79 to 0.92 and the NACA 1-85-43.9 inlet was tested in the Mach number range from 0.60 to 0.92. Inlet mass-flow ratios ranged from 0.27 to 0.96 depending on inlet configuration and freestream Mach number. Angle of attack was varied within the range -3° to 3.1° at selected Mach numbers and mass-flow ratios. The Reynolds number of the test varied with Mach number from 3.2x10<sup>6</sup> to 4.2x10<sup>6</sup> per foot.

# INTRODUCTION

Engine installation on jet-powered subsonic transport aircraft generally results in each engine being wrapped separately in a nacelle that is essentially symmetric (in external contour) about the axis of the engine rotating components. The nacelle is pylon mounted (displaced from the airframe) so that during cruise flight at least the forward portion of the nacelle will pass through air that has not been significantly disturbed by the passage of any main airframe components. Such installations permit some decoupling of nacelle design from airframe design in that substantial development of at least the inlet portion of the nacelle can be done independently. This independence of inlet geometry from airframe geometry makes the pitot-type subsonic inlet data base available in the literature directly useable for many aircraft applications.

Inlets for turbojet and turbofan powered subsonic aircraft must provide high quality flow to the engine fan and compressor, produce low external drag, be low in weight and have noise characteristics acceptable to the community. High quality flow for the engine is provided by designing the internal flow lines (cowl lip, throat contour, and diffuser) for separation-free flow. Based on internal flow considerations, cowl length and weight are minimized by making the inlet throat radius as large as possible and by designing the diffuser contour so that the diffusion angle is close to the maximum for separation-free flow while allowing some margin at the most adverse operating conditions. For commercial applications it is also important to consider noise suppression during diffuser design since this may have some effect on how short the cowl portion of the nacelle can be. The external drag is minimized, based on external flow considerations, by making the maximum cowl diameter and length as small as

possible while still obtaining the desired drag divergence Mach number and spillage critical mass-flow ratio.

Many of the pitot-type subsonic transport nacelle forebodies (cowls) used in the past have been based (at least in part) on the NACA 1-series contour which was developed in the 1940's. The NACA 1-series contour has a relatively small leading edge radius (external to the highlight) and because of this has good high speed spillage drag characteristics. However, high speed external performance of the NACA 1-series contour must often be compromised by increasing the leading edge radius to achieve acceptable internal performance at low speed and static crosswind conditions. The NACA 1-series contour was developed concentrating on the inlet external performance with the assumption that throat and diffuser shape would be essentially a separate design endeavor. Most of the published experimental data obtained on NACA 1-series inlets is contained in references 1 to 10.

Evolutionary changes in transport aircraft speeds, engine cycle and mass flow needs, and advances in analytical and computational techniques applicable to inlet forebody design and analysis have produced the need for some expansion of the experimental data base. To this end, three inlet models having the same cowl highlight diameter have been investigated to obtain pressure data on the inlet forebody exterior and lip over a range of mass-flow ratios. Two of the inlets had an NACA 1-85-100 external contour but had different internal lip contours and internal contraction ratios. One of these inlets had a contraction ratio of 1.009 and has been tested previously over a limited range of mass-flow ratios (refs. 9 and 10). The other NACA 1-85-100 inlet had a contraction ratio of 1.250 and therefore had a different internal lip shape and throat diameter. The third inlet had an NACA 1-85-43.9 contour and a contraction ratio of 1.250. The two inlets with 1.250 contraction ratio had identical internal surface contours so that the effect of the 53.1 percent change in external cowl length on the surface pressure distributions could be determined. The difference in inlet lip contour and contraction ratio between the two NACA 1-85-100 inlets will show the effect, if any, of the internal contour change on the external surface pressure distributions.

The investigation was conducted in the Langley Research Center 16-Foot Transonic Tunnel at Mach numbers ranging from 0.60 to 0.92, mass-flow ratios from 0.27 to 0.96, and at angles of attack within the range from -3° to 3.1° at selected mass-flow ratios and Mach numbers. Cowl external static pressures were measured in rows on the top and bottom surfaces of the inlets (in the plane of vertical symmetry). The NACA 1-85-100 inlet with a contraction ratio of 1.009 also had a longitudinal row of cowl external static pressure orifices on the side of the inlet. Diffuser wall static pressures were measured in the two inlets with a contraction ratio of 1.250.

## **SYMBOLS**

Symbols in parenthesis are used in computer generated tables.

A area normal to model centerline, in<sup>2</sup>

 $C_{\mathbf{p}}$ (CP) local pressure coefficient,  $(p-p_0)/q_0$ D<sub>max</sub> maximum diameter of model, 18.0 in. inlet internal diameter at end of lip radius (see Table I), in. d L (L) length of cowl from lip (highlight) to start of cylindrical portion of model,in., see fig. 1 mass-flow ratio based on highlight area,  $1/(\rho A_h V_0) \rho_r V_r dA$ mfr freestream Mach number M local static pressure, psi р freestream static pressure, psi Po freestream dynamic pressure, psi  $q_0$ pressure probe radial distance from model centerline, in.  $R_{\mathbf{p}}$ radial distance from model centerline to duct outer wall, 8.40 in.  $\bar{R_{\mathbf{w}}}$ maximum external cowl radius. in. (RMAX) (R/RMAX) nondimensionalized radius, in percent, from centerline of model to cowl or diffuser surface, RMAX = 9.0 in. freestream Reynolds number, per foot  $R_0$ lip radius internal to highlight for NACA 1-series inlet (see Table I). r V velocity, ft/sec x/L (X/L) nondimensionalized distance, in percent, from cowl lip measured longitudinally (aft) with negative values indicating locations on the internal surface (X)longitudinal distance measured aft of the cowl lip (highlight), in. X radial distance at RMAX minus inlet highlight radius (see Table I), in. Y radial distance minus inlet highlight radius (see Table I), in. y angle of attack with respect to forebody centerline, deg α density slug/ft<sup>3</sup> ρ meridian angle, measured from top of model in clockwise direction when looking upstream, deg

# Subscripts:

h highlight, most forward point on cowl lip

max maximum

r axial mass-flow rake measuring station in duct

0 freestream condition

## **MODELS**

A complete model test installation consisted of an inlet cowl and cylindrical section which were supported by a force balance, and an afterbody (also cylindrical) which was supported by the sting upon which a remote controlled mass-flow throttle plug was mounted. A simplified cross-sectional sketch of the model assembly is shown in figure 1 and a photograph of a typical model installation in the wind tunnel test section is shown in figure 2.

The basic nondimensionalized NACA 1-series outer profile ordinates, as presented for a given lip radius of 0.025Y in reference 1, are reproduced in table I. The NACA 1-85-100 inlet with an internal contraction ratio of 1.009 (table II) was used in the investigations of references 9 and 10. The second NACA 1-85-100 cowl had the same external profile, but had a different lip radius and an internal contraction ratio of 1.250 (table III). The third inlet (table IV) also had an internal contraction ratio of 1.250 but had a shorter cowl profile (NACA 1-85-43.9). This third inlet was designed to have the same overall assembled model length by including a section of constant (external) diameter at the end of the cowl profile. The internal contours (including the diffuser) of the two inlets with a 1.250 contraction ratio were identical.

Total model length was 52.0 inches (fig. 1) with the forward 27.50 inches, which included the cowl, supported by four struts that connected to a force-balance mounted centerbody. The aft 24.50 inches (cylindrical in external shape) of the model was supported by four struts attached to the support sting. A 0.10 inch gap between the forward and aft portions of the model was spanned by a free floating flexible strip to inhibit flow leakage. Three of the four struts supporting the forward portion of the model were instrumented with pressure (fig. 3) probes to measure the internal mass flow. These struts were also used to route the tubes from the inlet surface static-pressure orifices to differential pressure-scanning units mounted in the nose of the centerbody. All pressure tubes associated with the aft portion of the model were routed through the four rear support struts; into the sting; and out through the tunnel support system to another differential pressure-scanning unit.

The mass-flow throttle plug was driven by an internally housed remote controlled electric motor and had a travel capability of about 10 inches (fig. 1). The open area at the exit of the model (normal to the centerline of the model) could be varied from 27.5 in<sup>2</sup> to 244.9 in<sup>2</sup> (plug in its two extreme positions).

# WIND TUNNEL

The investigation was conducted in the Langley Research Center 16-Foot Transonic Tunnel which is a single-return atmospheric wind tunnel with continuous air exchange. The test section is octagonal in shape with 15.5 feet between opposite walls (equivalent in area to a circle 16 feet in diameter) and has axial slots at the wall vertices. The total width of the eight slots in the vicinity of the model is approximately 3.7 percent of the test section perimeter. The extreme limits of solid blockage of the model in the test section is between 0.88 percent for the hypothetical case of no flow through the model and 0.79 percent for the case of the throttle plug only (the throttle plug in its most rearward position). The tunnel sting support system pivots in such a manner that the model remains on or near the test section centerline through the angle of attack range. Details of the operation of the tunnel and its flow qualities are presented in references 11 to 13.

#### TESTS AND METHODS

Each inlet was tested at Mach numbers up to 0.92 at an angle of attack of  $0^{\circ}$  and over a nominal angle of attack range (less than  $3.1^{\circ}$ ) at selected Mach numbers and mass-flow ratios. Freestream Reynolds number per foot varied with Mach number from  $3.2 \times 10^6$  to  $4.2 \times 10^6$  (fig. 4). All the data presented herein are for artificially fixed boundary layer transition on the internal and external surfaces of the model. Boundary-layer transition on the external surface of the model was fixed by applying a 0.10 inch wide circumferential strip of number 120 silicon carbide particles 0.6 inch aft (streamwise) of the cowl lip. Boundary-layer transition was fixed on the internal flow surface of the model by applying a 0.10 inch wide circumferential strip of number 120 silicon carbide particles at the geometric throat of each inlet.

Angle of attack was computed by correcting the measured angle of attack of the support system for deflection of the sting and force balance due to aerodynamic forces and moments and for tunnel stream angularity. Although the test was conducted with the model mounted on a force balance, the data from it will not be presented since the balance was damaged during the test. Duct mass flow was calculated from the freestream total temperature, rake area-weighted stagnation pressures, and static pressures from the rake, centerbody surface, and duct wall.

No corrections have been made to the pressure data for test section wall interference effects. The presence and geometry of the mass-flow plug will have an effect on the afterbody external flow field. Therefore, the afterbody pressure data presented in the pressure tabulations should be considered qualitative, especially for pressures near the model aft end. The effect of the mass-flow plug should be the greatest for cases with large mass-flow ratios where the internal flow exits the afterbody before passing over the front face of the mass-flow plug and therefore has not been turned back streamwise by the internal afterbody surface.

## PRESENTATION OF RESULTS

The results of this investigation are presented primarily in tabular form as local internal and external pressure coefficients in tables V to VII. The surface pressure coefficients are tabulated against nondimensionalized orifice location (X/L) where L is the length of the NACA cowl portion of the model. The ratio X/L is presented in percentage form in the tables. A negative value of X/L indicates the orifice is located on the internal surface (downstream of the highlight) of the inlet. The pressure coefficients are presented for either two or three meridian angles (PHI) depending on the number of rows of orifices on the configuration. Inlet mass-flow ratio and angle of attack are given at the top of each table. In addition, some data are presented graphically (figs. 5 to 11) to illustrate the variation of pressure coefficient with X/L over the lip and cowl portion of the model over a range of Mach numbers, mass-flow ratios, and angles of attack. Some graphical data are presented in figures 12 to 15 for the two inlets with a contraction ratio of 1.250 to show the effect of mass-flow ratio and angle of attack on the lip and diffuser pressure coefficient distributions.

Summaries of the tabular and graphical data presented are contained in the following three listings. The listing for each cowl includes nominal test condition information and table and figure numbers for the pressure coefficient data.

NACA 1-85-100 with contraction ratio 1.009

		1	Pressure c	oefficients
М	mfr	α,deg	Table	Figure
0.79	0.57 .64	0	V(a)	5(a) 5(a)
	.71 .77 .85	<b>\</b>	↓	5(a) 5(a)
0.84	0.57	-3.0 -2.0	V(b)	6(a)
		-1.0 0 1.0		5(b),6(a),7(a)
		2.0 3.0		6(a),7(a)
	.64 .71	0		5(b)
	.78   	-3.1 -2.1		6(b)
		-1.1 0 1.0		5(b),6(b),7(b)
	↓	2.0 3.0		6(b),7(b)
	.95	-3.1 -2.1		6(c)
		-1.1 -0.1 1.0		5(b),6(c),7(c)
	<b> </b>	2.0 3.0	↓	6(c),7(c)
0.87	0.57	-2.0	V(c)	6(d)
	- ↓	0 2.1		5(c),6(d),7(d) 6(d),7(d)
	.63	0		5(a), 7(a) 5(c)
	.70	Ĺĺ		5(0)
V	.78	▼		5(c)
0.89	0.57	-2.1	V(d)	6(e)
	- ↓	0 2.1		5(d),6(e),7(e)
	.62			6(e),7(e) 5(d)
	.71	0		3(4)
↓	.77 .96	-0.1	- ↓	5(d)
0.92	0.57	0	V(e)	5(d) 5(e)
	.63	ΙÌΙ		5(e)
	.71			
<b>↓</b>	.77 .96	. ↓	- ↓	5(e)
	.30			5(e)

NACA 1-85-43.9 with contraction ratio 1.250

		Pressure	e coefficien	ts			Pressur	e coefficien	ts
М	mfr	a,deg	Table	Figure	М	mfr	α,deg	Table	Figure
0.60	0.28 .31 .40 .50 \$\infty\$	1.0 2.0 3.0 0	VI(a)	14(a) 8(a) 8(a),9(a),14(a),15(a) 9(a),15(a) 15(a) 14(a)	0.82	0.27 .30 .40 .49 .54 .61 .68 .74	o •	VI(h)	14(h) 14(h) 14(h) 14(h) 14(h)
0.64	.69 .69 .75 .82 .82 .93 0.27	2.0 0 0 2.0 0	VI(b)	8(a).9(b).15(b) 9(b).15(b) 14(a) 8(a).9(c).14(a).15(c) 9(c).15(c)	0.84	0.27 .30 .39 .49	1.0 2.0 3.1	VI(i)	14(i) 8(d) 8(d),9(f),14(i),15(f) 9(f),15(f) 15(f)
<b>1</b>	.40 .50 .55 .62 .68 .75	•		14(b) 14(b) 14(b) 14(b)		.61 .67 	1.0 2.0 3.1 0		14(i) 8(d).9(g).14(i).15(g) 9(g).15(g) 15(g) 14(i) 8(d).9(h).14(i).15(h)
0.69	0.28 .30 .40 .49 .49 .55 .61 .68	2.0	VI(c)	14(c) 8(b) 8(b),9(d),14(c),15(d) 9(d),15(d) 14(c) 8(b) 14(c)	0.87	.83 .84 .81 0.27 .31 .39 .50 .49	1.0 2.0 3.0 0 2.0 0	VI(j)	9(h), 15(h) 15(h) 14(j) 8(e) 8(e), 9(i), 14(j), 15(i) 9(i), 15(i)
0.72	.81 0.30 .40 .49 .54	0	VI(d) VI(e)	8(b),14(c) 14(d) 14(e)	0.89	.61 .68 .68 .74 .83 0.27	20 0 0	VI(k)	14(j) 8(e),9(j),14(j),15(j) 9(j),15(j) 14(j) 8(e),14(j) 14(k)
0.77	.31 .40 .49 .54 .61 .68 .74 .80	•	VI(f)	14(e) 14(e) 14(e) 14(e) 14(f)		.32 .39 .49 .49 .54 .61 .68 .74	2.1		8(f) 8(f),9(k),14(k),15(k) 9(k),15(k) 14(k) 8(f),14(k) 14(k) 8(f)914(k)
	.30 .40 .48 .54 .61 .68 .74			14(f) 14(f) 14(f) 14(f)	0.92	0.27 .32 .40 .49	1.0 2.0 3.1	VI(I)	14(I) 8(g) 8(g),9(I),14(I),15(I) 9(I),15(I) 15(I)
0.79	0.27 .30 .39 .49 .49 .54 .61 .68 .74	2.0	VI(g)	14(g)  8(c) 8(c),9(e),14(g),15(e) 9(e),15(e)  14(g) 8(c),14(g) 14(g) 8(c),14(g) 8(c),14(g)		.61 .68 .68 .74 .82 .82	2.1 0 0 2.0		14(1) 8(g),9(m),14(1),15(m) 9(m),15(m) 14(1) 8(g),9(n),14(1),15(n) 9(n),15(n)

NACA 1-85-100 with contraction ratio 1.250

	***************************************	<del></del>	Pressure c	oefficients
М	mfr	α,deg	Table	Figure
0.79	0.61 .67 ↓ .74	0 -2.0 0 2.1 0	VII(a)	10(a),12(a) 11(a) 10(a),11(a),12(a) 11(a) 10(a),12(a)
0.84	0.49	-2.1	VII(b	11(b)
		-1.0 0 1.0		10(b),11(b),12(b),13(a)
	.55	2.0 3.1 0		11(b),13(a) 13(a)
	.61 .67 I	0 -2.1 -1.0		10(b),12(b) 11(c)
		0 1.0		10(b),11(c),12(b),13(b)
		2.0		11(c),13(b)
	.74	3.1 0		13(b) 12(b)
	.83	-2.1		12(b) 11(d)
	.83 .84 .83	-1.1 O 1.1		10(b),11(d),12(b),13(c)
<b>1</b>	<b>↓</b>	2.0 3.1	<b>+</b>	11(d),13(c) 13(c)
0.87	0.49	-2.0 0	VII(c)	11(e)
	.55	2.1 0		10(c),11(e),12(c),13(d) 11(e),13(d)
	.61	Ĭ		10(c),12(c)
↓	.67 .73	↓	↓	10(c),12(c) 10(c),12(c)
0.89	0.49	-2.1	VII(d)	11(f)
	1	0		10(d),11(f),12(d),13(e)
	.55	2.0 0		11(f),13(e)
	.61	ı ĭ l		10(d),12(d)
	.67			10(d),12(d)
↓	.73 .81		<b>\rightarrow</b>	12(d) 10(d),12(d)
0.92	0.49	0	VII(e)	10(e),12(e)
	.55			10(a) 10(a)
	.61 .67			10(e),12(e) 10(e),12(e)
	.73	1	1	12(e)
<b>V</b>	.81	▼	▼	10(e),12(e)

# **RESULTS**

This investigation was conducted primarily to obtain cowl pressure distributions under conditions that isolate the cowl from the influence of a boattailed afterbody flow field. Therefore a considerable portion of the model aft of the cowl was cylindrical in shape equal in diameter to the cowl maximum diameter (figure 1). This test apparatus was used in the investigation of

reference 10 for high mass flows through the model. However, the geometry of the throttle plug used in that investigation was not capable of reducing the afterbody exit area enough over the range of plug travel to obtain low mass flows for the NACA 1-85-43.9 cowl, which should have significantly better performance at low mass-flow ratios at the lower Mach numbers. That is, it should have a lower critical mass-flow ratio which is a measure of cowl performance when operating below the compressibility drag-rise condition. At a given Mach number, drag changes only gradually as inlet mass flow is decreased until a critical mass flow is reached where drag abruptly increases. The drag increase results from flow separation caused by shocks or strong pressure gradients resulting from flow separation around the initial cowl lip curvature. Conversely the term lower critical Mach number would indicate the Mach number at which an abrupt drag increase results for a given mass-flow ratio as Mach number is decreased.

To expand the mass flow range capability of this apparatus to encompass lower mass flow rates, the throttle plug geometry was altered so that it was blunter and had a larger maximum diameter. Comparisons made in reference 10 of the results of references 9 (last 14 inches of afterbody boattailed) and 10 (cylindrical afterbody) at high mass-flow ratios indicate no significant effects fed forward from the exit plume/mass-flow plug combination to the cowl pressure distributions over the range of test Mach numbers.

## **Cowl Pressure Distributions**

At 0° angle of attack.- NACA 1-series cowls that are designed for moderate or high subsonic Mach numbers often have high negative pressure peaks near the lip at low Mach numbers and low mass-flow ratios because of the relatively sharp cowl lip. This often results in flow separation on the forward portion of the cowl when the pressure can not recover from the peak. The pressure distributions of reference 9 for the NACA 1-85-100 inlet with a contraction ratio of 1.009 show that flow separation occurred on the cowl at a mass-flow ratio of 0.56 for Mach numbers of 0.4, 0.6, and 0.7. However at a Mach number of 0.79, which was the lowest test Mach number for that inlet in the present investigation, flow separation did not occur (fig. 5(a)) at that mass-flow ratio. Larger contraction ratios of 1.046 and 1.093 (reference 9) did not significantly affect flow separation on the forward portion of the cowl under the aforementioned conditions. At higher Mach numbers where flow separation did not occur on the forward portion of the cowl, larger contraction ratio had only small effects on the cowl pressure distributions. However, these small effects did result in some decrease in cowl critical Mach number at a given mass-flow ratio (see ref. 9) for a contraction ratio of 1.093.

The NACA 1-85-43.9 inlet, which because of its blunter lip profile is capable of better performance at lower Mach numbers than the NACA 1-85-100 inlets was tested at lower Mach numbers and lower mass-flow ratios. This inlet did not encounter flow separation at  $0^{\circ}$  angle of attack on the forward portion of the cowl at the lowest Mach numbers and mass-flow ratios tested (fig. 8) which indicates that it had lower critical Mach numbers relative to the NACA 1-85-100 inlets. Three non-NACA 1-series inlets (X/L = 0.337, 0.439, and 0.547), whose external

contour changes with length were made in the same manner as the NACA 1-series inlets, were tested on the same apparatus described herein and the pressure coefficients are reported in reference 14. Those data showed the same improvements in performance at the lower Mach numbers and lower mass-flow ratios for the blunter lip profiles.

At small angles of attack.- The NACA 1-85-100 inlets were tested at angles of attack within the range from -3.0° to 3.1° at selected Mach numbers and massflow ratios (figs. 6 and 11). As would be expected, at low mass-flow ratios an increase in angle of attack caused an increase in the severity of the negative pressure peaks on the cowl upper surface and shifted the onset of strong recompression aft (see fig. 6(e) for example). At the high mass-flow ratios an increase in angle of attack decreased the extent of positive pressure on the forward portion of the cowl upper surface (see fig. 6(c) for example). The NACA 1-85-43.9 inlet was tested only at positive angles of attack so the row of pressure orifices on the bottom of the cowl can be considered to represent the equivalent negative angle of attack and are included in figure 9 for that purpose. The effects of angle of attack on the forward pressure peaks on this inlet were similar to those encountered on the NACA 1-85-100 inlets. This inlet was tested at angle of attack at lower Mach numbers than the others since it has more potential for good performance in the lower Mach number range. At a Mach number of 0.69 (fig. 9(d)) there appears to be flow separation near the cowl upper surface leading edge at 2.0° angle of attack. This can be seen by comparing the extent of constant pressure coefficient at the peak relative to that at 0° angle of attack for the top and bottom rows of pressure orifices.

At small angles of sideslip. The NACA 1-85-100 inlet with a contraction ratio of 1.009 had a row of external pressure orifices on the side of the cowl at a meridian angle of 90°. Because of the inlet axial symmetry this row of orifices can be considered to represent the top of an inlet at 0° angle of attack that moves in sideslip when the model is moved in what has been defined as the angle of attack direction in this investigation. To determine the effect of sideslip on the pressure distributions, data from this row of orifices are presented in figure 7 for the maximum positive angle of attack at each Mach number. The data indicate a negligible effect of sideslip over the small angle range of this test.

#### **Diffuser Pressure Distributions**

The variation of pressure coefficient (internal to the highlight) with  $X/D_{max}$  for various mass-flow ratios for the two inlets with a contraction ratio of 1.250 is shown in figures 12 ( $\alpha$  = 0°) and 13 (small  $\alpha$ 's) for the NACA 1-85-100 cowl and in figures 14 ( $\alpha$  = 0°) and 15 (small  $\alpha$ 's) for the NACA 1-85-43.9 cowl.

At 0° angle of attack.- An illustration of the effect of changing mass-flow ratio at a Mach number of 0.60 on the location of the stagnation point on the inlet lip of the NACA 1-85-43.9 inlet can be seen in the pressure coefficients of table VI(a). As expected the stagnation point was farthest inside the inlet on the contraction surface (at an X/L of -5.13 percent) at the lowest mass-flow ratio of 0.28. The

stagnation point moved forward on the contraction surface with increasing mass flow until it reached the highlight (X/L = 0) at the maximum mass-flow ratio of 0.93.

The pressure distributions of figure 14 (or figure 12) indicate that the lowest internal pressure occurred approximately at the geometric throat ( $\rm X/D_{max} = 0.113$ ) for all mass-flow ratios up through a Mach number of 0.77. At a Mach number of 0.79 a shock occurred at the throat at a mass-flow ratio of 0.80. Above a Mach number of 0.79 the shock moved downstream to an  $\rm X/D_{max}$  of about 0.18 where the lowest pressure also occurred.

The effect of changes in external cowl shape on the pressure distributions internal to the highlight at 0° angle of attack was negligible as can be seen by comparing the data of figure 12 (NACA 1-85-100) with data at the appropriate Mach number and mass-flow conditions in figure 14 (NACA 1-85-43.9). The inlets both had a contraction ratio of 1.250 and identical diffuser geometry.

At small angles of attack. The effect of angle of attack on the pressure distributions internal to the highlight is shown in tables VI and VII and figures 13 and 15 for the two different external cowl shapes. In general the effect of angle of attack is as would be expected. For example, examination of the pressure coefficients of tables VI and VII show that as angle of attack was increased for a given mass-flow ratio, the stagnation point of the incoming stream tube on the upper lip moved slightly farther into the contraction section while on the lower lip (the windward side) of the inlet the streamtube stagnation point moved slightly closer to the highlight.

# **CONCLUDING REMARKS**

An investigation has been conducted over a range of subsonic speeds to determine pressure distributions on three isolated inlets having NACA 1-series cowl profiles. Two had NACA 1-85-100 cowls that differed only in internal contraction ratio (1.009 and 1.250). The third inlet had an NACA 1-85-43.9 cowl and had a contraction ratio of 1.250. Angle of attack was varied over a small range at selected Mach numbers and mass-flow ratios for each inlet.

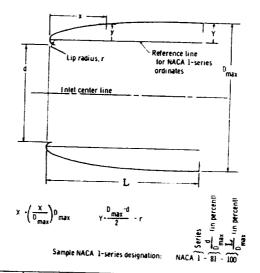
At low Mach numbers and low mass-flow ratios, the NACA 1-85-100 inlets encountered flow separation over the forward portion of the cowl surface that was not significantly affected by the variation in contraction ratio. However the critical Mach number at a given mass-flow ratio was decreased somewhat by the increase in contraction ratio. The NACA 1-85-43.9 inlet did not encounter flow separation at the lowest mass-flow ratios since its blunter lip profile was more conducive to better performance at lower Mach numbers. At an angle of attack of 2.0°, the NACA 1-85-43.9 inlet did encounter separation at the lowest mass-flow ratio at the two lowest Mach numbers (0.60 and 0.69). Pressure coefficients from a row of pressure orifices on the side of the NACA 1-85-100 inlet with a contraction ratio of 1.009 showed no significant effect of angle change when the model was moved through a small range of angles of attack thus indicating insensitivity to small angles of sideslip.

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TABLE I.- NACA 1-SERIES ORDINATES
[Coordinates in percent]



	x/L	y/Y	x/L	y/Y	x/L	y/Y
	0	0	20.0	52.70	48.0	81.25
	.2	4.80	21.0	54.05	49.0	
	.4	6.63	22.0	55.37	50.0	1
1	.6	8.12	23.0	56.66	52.0	
-	.8	9.33	24.0	57.92	54.0	85.45
1	1.0	10.38	25.0	59.15	56.0	86.73
	1.5	12.72	26.0	60.35	58.0	87.95
	2.0	14.72	27.0	61.52	60.0	89.11
	2.5	16.57	28.0	62.67	62.0	90.20
1	3.0	18.31	29.0	63.79	64.0	91.23
1	3.5	19.94	30.0	64.89	66.0	92.20
1	4.0	21.48	31.0	65.97	68.0	93.11
	4.5	22.96	32.0	67.03	70.0	93.95
	5.0	24.36	33.0	68.07	72.0	94.75
	6.0	27.01	34.0	69.08	74.0	95.48
	7.0	29.47	35.0	70.08	76.0	96.16
	8.0	31.81	36.0	71.05	78.0	96.79
	9.0	34.03	37.0	72.00	80.0	97.35
	10.0	36.13	38.0	72.94	82.0	97.87
	11.0	38.15	39.0	73.85	84.0	98.33
	12.0	40.09	40.0	74.75	86.0	98.74
	13.0	41.94	41.0	75.63	88.0	99.09
	14.0	43.66	42.0	76.48	90.0	99.40
	15.0	45.30	43.0	77.32	92.0	99.65
	16.0	46.88	44.0	78.15	94.0	99.85
	17.0	48.40	45.0	78.95	96.0	99.93
	18.0	49.88	46.0	79.74	98.0	99.98
	19.0	51.31	47.0	80.50	100.0	100.00
		1	Lip radiu	s: 0.025	Y	·

TABLE II. - DESIGN ORDINATES FOR NACA 1-85-100 INLET WITH INTERNAL CONTRACTION RATIO OF 1.009

[Coordinates in percent] L = 18.00in. and RMAX = 9.00in.

External ordinates

R/RMAX	93.09 94.02 94.87 95.62 96.29 97.47 99.11 99.62	RMA	87.98 87.98 90.89 93.33
X/L	20.00 25.00 30.00 35.00 40.00 45.00 50.00 70.00 80.00 90.00	_	60.00 80.00 90.00 100.00
R/RMAX	85.36 86.33 86.33 86.36 87.22 87.22 87.51 87.80 88.04 88.51 88.51 88.69 90.64 92.00	RMA	85.00 85.42 85.87 86.22
X/L	0.0 	X/L	.18 .18 .12.50 .25.00 .35.00

TABLE III.- DESIGN ORDINATES FOR NACA 1-85-100 INLET WITH INTERNAL CONTRACTION RATIO OF 1.250

[Coordinates in percent] L = 18.00in. and RMAX = 9.00in.

							j
X/L	R/RMAX	X/L	R/RMAX	X/L	R/RMAX	X/L	R/RMAX
0.0	5	1.5	3.3	0.0	5.3	2.0	6.3
.02	85.58	23.16	93.68	.01	85.00	12.43	76.38
.08	5.	4.8	4.0	.04	4.6	2.9	6.4
.18	9.	9.9	4.3	80.	4.2	3.4	6.4
.32	6.2	8.5	4.6	.14	3.9	3.9	6.4
. 50	9.9	9.0	4.9	.23	3.5	4.6	6.5
.72	9.	2.7	5.2	.33	3.2	5.3	9.9
٥;	ω.	5.0	5.6	.45	2.8	6.0	6.7
	7.0	7.4	5.9	.59	2.4	6.9	6.8
Ψ.	7 . 3	0.0	6.3	94.	2.1	7.8	7.0
٠.		3.0	9.9	.94	1.7	8.8	7.2
7.	7.7	6.0	7.0	Π.	1.3	9.9	7.4
٥,	S. C.	9.0	7.3	۳.	1.0	1.1	7.7
7.	.2	2.0	7.6	φ.	9.0	2.5	8.0
٥.	ຜ	5.0	7.9	ο.	0.3	3.9	8.4
œ.	. 7	8.0	8.2	Ġ	9.9	5.6	8.9
∾.	0.	1.0	8.4	9.	9.5	7.3	9.4
o.	.2	4.0	8.7	٥.	9.2	9.3	0.0
۲.	٠. ت	7.0	9.9	4.	8.8	1.5	0.7
r.	œ.	0.	9.1	ō.	8.5	9.6	1.5
m.		3.0	9.2	ഹ	8.1	6.5	2.4
9.2	4.	6.0	9.4	Τ.	7.7	9.4	3.5
0.7		0.6	9.5	∞.	7.4	2.5	4.6
1.2	-	2.0	9.6	S.	7.1	6.0	5.8
2.2	L.3	Ω	9.7	3	6.9	9.8	7.1
3.4	9:	8.0	9.8	∞.	6.7	4.1	8.4
4.5		1.0	9.9	v.	9.9	8.7	9.8
5.8	٠ <u>.</u>	4.0	9.9	7	6.4	3.8	1.0
7.1	4.	7.0	9.9	ο.	6.4	9.4	2.2
18.54	7.7	0	0.0	10.59	6.3	5.6	3.0
0.0	∞.			.2	6.3	2.2	3.3
				,			

TABLE IV.- DESIGN ORDINATES FOR NACA 1-85-43.9 INLET WITH INTERNAL CONTRACTION RATIO OF 1.250

[Coordinates in percent] L = 7.897in. and RMAX = 9.00in.

External ordinates
R/RMAX
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TABLE V. PRESSURE COEFFICIENTS ON MODEL WITH NACA 1-85-100 INLET AND CONTRACTION RATIO OF 1.009

(a) M = 0.79

	ð,	පු	0.00		10131	0742	1273	72.01	2362	1007	75369	35.39																				J,	S C	0103	0.0174	0363	0531	22,60	1524	2166	2651		7616	3882																
కి	Afterbody		0.00																												٠	흁			183.30 0																									
• = 180°													<b>2</b> 5	2 3	9 9	6 5	S :	221	49	723	£	52	323	130	20	Š	88	19			<u>=</u>														3 :	⊋ 8	20	7	8	5.	84	8	2	2 2	2 ;	<u>.</u>	-	24	2	2 :
	ě		0.9345															20.2122			0.1549						0.0398					Forebody																			0.1784									
	- ;	× ×	2.5	÷	÷	Ģ	Ö	c	; <u>-</u>	: -		5.2	· -	4 -	ŕ		-	<u>.</u>	= ;	20.	₹	Š	8	20.00	80.	96	122.00	138	اة	,		<u></u>	ž		-3.12	7	-1.2	Ö.	0.0	0.0	13	: :		3;		5.75	Ţ:	0.0	2.5	150	17.50	500	40.0	00	3	90.0	0.0	80.08	800	
.06 = ♦	body	3	0.9420	0.9851	1.0240	0.6916	1.5728	-1.4910	4774	1 1660	1 2014	200	1 1367	0 5330	0.0326	2010	2000	907.0	0.1037	0.1518	0.1298	-0.1278	0.1141	-0.1117	-0.0931	-0.0419	0.0311		and a		.06 = <del>+</del>	y y	č	0.7053	0.7135	0.7182	0.7681	1.1550	0.9331	0.5572	0.4574	71.070	2000	0.230	0.200	0.2303	CD 7 TO	0.2347	0.1792	-0.1787	0.1416	0.1334	0.1132	1001	2000	2000	0.1005	0.0814	0.0291	
*	Pore	X.	5 5	1.88	-1.25	000	0.62	1.25			2 2							00.00				90.00					139.00		mfr = 0.77 and a		•	Porebody	χŢ	-3.75		86 -								71.7		3 5					20.00					3 5			22.00	
	~ E	2 5	\$ 3	0.0157	389	788	111	872	275	2	471	:																	Ē				. :	77	£ ;	327	38	8	113	137	575	8	2 2	2															_	•
•	ě																														٠	ě				30 0.0327																								
.0 <b>* </b>			183.30										•	· <u>·</u>		90	, ,			,	۰ و	ا	2	1	S		••				0	•	X/F		0 183.30																_	_	_						_	
	Forebody		0.9581									.1 2543									0.1406						0.0258					Forebody		0.70			0.769									900			0.2334	0.232	0.1815	0.1479	ф Т	-0.1185	0.10		40.1021	-0.0722	-0.0266	
	° ,	17.	-3.12	-1.88	-1.25	-0.62	0.00	0.31	0.62	1.25	2.50	3.12	4.38	8	7.50	900	5	2 2	3 5	30.00	00.04	30.00	90.00	70.00	90.00	122.00	139.00					ō	7.	6.6	3.12	88.	1.25	-0.62	000	0.31	0.62	1.25	200	1 2	7	5	3 5	2 5	3 5	25	8:	800	40.00	90:00	000	3 5	00.00	8	122.00	
180	Arrerbody X/I. CP	7		200.00 0.0111							283.30 0.3198																				A	Arrerbody	_		200.00 0.0113																									
<u>#</u>	ATTENDO X/I.	186.70	183.30	200:00	216.70	238.90	255.60	266.70	272.20	277.80	283.30		1.4145	1.3924	1.3497	1.2055	0.1553	0.1723	0 1719	9091	5.100	0.000	0.1404	0.1191	0.1267	0.0958	3.0449	3.0395			15  -		7 7	200.00	20000	200.00	210.70	238.30	255.60	266.70	272.20	277.80	283.30		14439	.2767	2777	2905	2317	2117	2113	1900	.1451	1400	.1217	1030	901	2011	.ueus	7,010
<u>#</u>	CP X/I.	0.981 6.70	183.30	1.0767 200.00	1.1010 216.70	1.1560 238.90	-0.1455 255.60	-1.7532 266.70	-1.6955 272.20	1.5944 277.80	-1.5801 283.30				5.00 -1.3497	7.50 -1.2055	15.00 -0.1553				50.00			70.00			22.00 -0.0449				15  -		7 7	0.6316 100.10		00.007 00.000	0.917 210.70	0.38.30	0.7951 255.60	-1.2975 266.70	1.2353 272.20	-1.1537 277.80	-1.0492 283.30	-0.9912				7.50 0.2905						0.00 -0.1400						
281 = + 180 March 201	XI. CP XII.	-3.75 1.0176 166.70	-3.12 1.0291 183.30	-1.88 1.0767 200.00	-1.25 1.1010 216.70	-0.62 1.1560 238.90	0.00 -0.1455 255.60	0.62 -1.7532 266.70	1.25 -1.6955 272.20	1.88 -1.5944 277.80	2.50 -1.5801 283.30	3.12 -1.4995	3.75	4.38	9:00	7.50	15.00	17.50	2000	9	8 9	8.6	80.00	00.00	80.00	90.00	122.00		α = 0°		Promphode:	XII CD	275 00216 125	0.001 0.0010 0.00	OC.001 05400 501.	00.002 80.800 80.1	0/317 5/16/0 57:1-	0.62 1.0078 238.90	0.00 0.7951 255.60	0.62 -1.2975 266.70	1.25 -1.2353 272.20	1.88 -1.1537 277.80	2.50 -1.0492 283.30	3.12 -0.9912	3.75	4.38	200	2.5	15.00	35.	06.71	00.07	40.00	20:00	00:09	2000	00.08	90.06	80.00	122 (10
281 = + 180 March 201	CP X/I CP X/I.	1,0078 -3.75 1,0176 166.70	1.0243 -3.12 1.0291 183.30	1.0653 -1.88 1.0767 200.00	1.0979 -1.25 1.1010 216.70	0.2493 -0.62 1.1560 238.90	-1.7592 0.00 -0.1455 255.60	-1.6915 0.62 -1.7532 266.70	-1.6955 272.20	-1.5427 1.88 -1.5944 277.80	-1.4899 2.50 -1.5801 283.30	-1.3621 3.12 -1.4995	-1.3260 3.75	-1.2054 4.38	-0.5817 5.00	-0.2006 7.50	-0.1640	-0.1652 17.50	-0.1565	0 1408 40 00	0.364	0.174	0.00 0.00	-0.1246 70.00	-0.1040 80.00	-0.0474 90.00	-0.0445 122.00		71 and \alpha = 0.		Promphode:	CP VI CP	OF 251 91290 371 OF 30	0.6231 0.6316 100.10	0.0000 0.0000 0.0000	00.002 85.00 95.1 500.0	0/10/17 6/16/10 6/11- /10/10	0.9798 -0.62 1.0078 238.90	-1.2940 0.00 0.7951 255.60	-1.1871 0.62 -1.2975 266.70	-1.1525 1.25 -1.2353 272.20	-1.0740 1.88 -1.1537 277.80	-0.9477 2.50 -1.0492 283.30	-0.4965 3.12 -0.9912	-0.2661 3.75	-0.3016 4.38	-0.2743 \$ 00	-0.2197 7.40	-0.2030 15.00	0.631	0.1331 17.30	-0.1460 20.00	-0.1217 40.00	-0.1231 50.00	-0.1069 60.00	-0.1086 70.00	0.001	0000	0.0356 90.00	-0.0278 122.00
<u>#</u>	XI. CP XII.	1,0078 -3.75 1,0176 166.70	1.0243 -3.12 1.0291 183.30	-1.88 1.0767 200.00	1.0979 -1.25 1.1010 216.70	0.2493 -0.62 1.1560 238.90	-1.7592 0.00 -0.1455 255.60	0.62 -1.7532 266.70	1.25 -1.6955 272.20	-1.5427 1.88 -1.5944 277.80	2.50 -1.5801 283.30	-1.3621 3.12 -1.4995	3.75	-1.2054 4.38	-0.5817 5.00	-0.2006 7.50	-0.1640	-0.1652 17.50	-0.1565	0 1408 40 00	8 9	0.174	0.00 0.00	-0.1246 70.00	-0.1040 80.00	-0.0474 90.00	-0.0445 122.00		$\mathbf{mfr} = 0.71 \text{ and } \alpha = 0^{\circ}$	900 : 1	Promphode:	CP VI CP	275 00216 125	0.6231 0.6316 100.10	0.0000 0.0000 0.0000	00.002 85.00 95.1 500.0	0/10/17 6/16/10 6/11- /10/10	0.9798 -0.62 1.0078 238.90	-1.2940 0.00 0.7951 255.60	-1.1871 0.62 -1.2975 266.70	-1.1525 1.25 -1.2353 272.20	-1.0740 1.88 -1.1537 277.80	-0.9477 2.50 -1.0492 283.30	-0.4965 3.12 -0.9912	-0.2661 3.75	-0.3016 4.38	-0.2743 \$ 00	-0.2197 7.40	-0.2030 15.00	0.631	06.71	-0.1460 20.00	-0.1217 40.00	-0.1231 50.00	-0.1069 60.00	-0.1086 70.00	0.001	0000	0.0356 90.00	-0.0278 122 DD
Porcellada Porcellada:	P X/L CP X/L CP X/l.	1 -3.75 1.0078 -3.75 1.0176 166.70	1.0243 -3.12 1.0291 183.30	-1.88 1.0653 -1.88 1.0767 200.00	-1.25 1.0979 -1.25 1.1010 216.70	0.00 0.2493 -0.62 1.1560 238.90	0.62 -1.7592 0.00 -0.1455 255.60	1.25 -1.6915 0.62 -1.7532 266.70	1.88 -1.6136 1.25 -1.6955 272.20	2.50 -1.5427 1.88 -1.5944 277.80	3.12 -1.4899 2.50 -1.5801 283.30	-1.3621 3.12 -1.4995	-1.3260 3.75	-1.2054 4.38	-0.5817 5.00	-0.2006 7.50	-0.1640	-0.1652 17.50	-0.1565	0 1408 40 00	0.364	0.174	0.00 0.00	-0.1246 70.00	-0.1040 80.00	-0.0474 90.00	-0.0445 122.00		$\mathbf{mfr} = 0.71 \text{ and } \alpha = 0^{\circ}$	900 : 1	Porehods Breehods:	P XI CP XI CD	27. 08330 37. 08330 37.	217 0 0271 217 0 0444 100.10	OC. CO. D. C.	00,002 86,000,000,000,000,000,000,000,000,000,0	07.012 67.15.0 63.1. 720.0 63.1.	0.00 0.9798 -0.62 1.0078 238.90	0.62 -1.2940 0.00 0.7951 255.60	1.25 -1.1871 0.62 -1.2975 266.70	1.88 -1.1525 1.25 -1.2353 272.20	2.50 -1.0740 1.88 -1.1537 277.80	3.12 -0.9477 2.50 -1.0492 283,30	4.38 -0.4965 3.12 -0.9912	-0.2661 3.75	-0.3016 4.38	-0.2743 \$ 00	-0.2197 7.40	-0.2030 15.00	0.631	0.1331 17.30	-0.1460 20.00	-0.1217 40.00	-0.1231 50.00	-0.1069 60.00	-0.1086 70.00	0.001	0000	0.0356 90.00	-0.0278 122 DD
♦ = 90° ♦ = 188 Afterhoods Preshoods	P X/L CP X/L CP X/l.	-0.0121 -3.75 1.0078 -3.75 1.0176 166.70	-0.0036 -3.12 1.0243 -3.12 1.0291 183.30	0.0071 -1.88 1.0653 -1.88 1.0767 200.00	0.0264 -1.25 1.0979 -1.25 1.1010 216.70	0.0621 0.00 0.2493 0.62 1.1560 238.90	0.1121 0.62 -1.7592 0.00 -0.1455 255.60	0.1660 1.25 -1.6915 0.62 -1.7532 266.70	0.2052 1.88 -1.6136 1.25 -1.6955 272.20	0.2498 2.50 -1.5427 1.88 -1.5944 277.80	0.3105 3.12 -1.4899 2.50 -1.5801 283.30	-1.3621 3.12 -1.4995	-1.3260 3.75	-1.2054 4.38	-0.5817 5.00	-0.2006 7.50	-0.1640	-0.1652 17.50	-0.1565	0 1408 40 00	0.364	0.174	0.00 0.00	-0.1246 70.00	-0.1040 80.00	-0.0474 90.00	-0.0445 122.00				Afterhody Forebody Forebody	CP X/I CP X/I CP	A 175 08330 375 08330 375	0.001 21.0 0.000 Cit. 10.000 Cit. 100.10	00.000 0000 0000 0000 0000 0000 0000 0	00.002 00.000 00.11 0000.0 00.1 00.000 00.10 00.000 00.11 00.000 00.11 00.000 00.11 00.000 00.11 00.000 00.11	0/017 6/16/0 67/1: /200/0 00/0 00000	0.266 0.00 0.9798 -0.02 1.0078 238.90	0.1405 0.62 -1.2940 0.00 0.7951 255,60	0.2042 1.25 -1.1871 0.62 -1.2975 266.70	0.2477 1.88 -1.1525 1.25 -1.2353 272.20	0.3018 2.50 -1.0740 1.88 -1.1537 277.80	0.3673 3.12 -0.9477 2.50 -1.0492 283.30	4.38 -0.4965 3.12 -0.9912	-0.2661 3.75	-0.3016 4.38	-0.2743 \$ 00	-0.2197 7.40	-0.2030 15.00	0.631	0.1331 17.30	-0.1460 20.00	-0.1217 40.00	-0.1231 50.00	-0.1069 60.00	-0.1086 70.00	0.001	0000	0.0356 90.00	JO 0778 122 00
Porcellada Porcellada:	XI CP XI CP XI CP XI	166.70 -0.0121 -3.75 1.0078 -3.75 1.0176 166.70	-0.0036 -3.12 1.0243 -3.12 1.0291 183.30	200.00 0.0071 -1.88 1.0653 -1.88 1.0767 200.00	216.70 0.0264 -1.25 1.0979 -1.25 1.1010 216.70	238.90 0.0621 0.00 0.2493 0.62 1.1560 238.90	255.60 0.1121 0.62 -1.7592 0.00 -0.1455 255.60	0.1660 1.25 -1.6915 0.62 -1.7532 266.70	272.20 0.2052 1.88 -1.6136 1.25 -1.6955 272.20	0.2498 2.50 -1.5427 1.88 -1.5944 277.80	283.30 0.3105 3.12 -1.4899 2.50 -1.5801 283.30	4.38 -1.3621 3.12 -1.4995	5.00 -1.3260 3.75	7.50 -1.2054 4.38	10.00 -0.5817 5.00	15.00 -0.2006 7.50	17.50 -0.1640 15.00	-0.1652 17.50	40.00 -0.1565 20.00	\$0.00 0.1408 40.00	00.00 826.00 00.00	00.00 F021.0 00.00 20.00 ACELO 00.00	00:00 0771:0- 00:00	80.00 -0.1246 70.00	90.00 -0.1040 80.00	-0.0474 90.00	139.00 -0.0445 122.00			000 : 1 00 = 1	Afterhody Formbody Franked:	XI. CP XI. CP XII. CP	A 16670 .00008 .3.75 08330 375 08330	18110 00111 -111 08211 0110 0110	OC.COI 0796.0 21.0 1700.0 21.0 0.000.0 00.000.00	216.70 0.0444 .1.25 0.000.0 set 7.000.0 .1.35 0.000.0	216.00 0.000 0.000 0.0000 0.0000 0.0000	236.50 0.0869 0.00 0.9798 -0.62 1.0078 238.50	255.00 0.1405 0.62 -1.2940 0.00 0.7951 255.60	200.70 0.2042 1.25 -1.1871 0.62 -1.2975 266.70	272.20 0.2477 1.88 -1.1525 1.25 -1.2353 272.20	277.80 0.3018 2.50 -1.0740 1.88 -1.1537 277.80	283.30 0.3673 3.12 -0.9477 2.50 -1.0492 283.30	4.38 -0.4965 3.12 -0.9912	5.00 -0.2661 3.75	7.50 -0.3016 4.38	10.00 -0.2743 \$00	-0.2197 7.40	17.50 -0.2030 15.00	0.631	0.71 1.53U - 0.1351 1.30 40.00 0.1484 30.00	-0.1460 20.00	20:00 -0:1217 +0:00	60.00 -0.1231 50.00	70.00 -0.1069 60.00	-0.1086 70.00	90 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	23.00 0.035	00'08 96'00 -0'03'8	-0.0278 122 DD

TABLE V. Continued

(a) Concluded

| Forebord | Forebord

TABLE V. Continued

(b) M = 0.84

		ody G	3 6	0.0100	0.0277	0.0416	0.1326	0.1910	0.2319	0.2758																ody	<b>a</b> 2	0.004	0.0191	0.0357	0.1338	0.1981	0.2430	0.3631													
	<b>\$</b> = 180°	Afterbody	18 J	183.30	200.00	07.017	255.60	266.70	272.20	283.30															= 180°	Afterbody	X/L	183.30	200:00	216.70	255.60	266.70	272.20	283.30													
	•	Forebody	2 2	1.0925	1.1271	1.148/	0.3974	-1.6325	-1.5888	-1.3453	-1.4549	-1.4358	-1.3865	1 2 300	-1.0537	-0.5073	-0.1738	-0.0628	801.0-	0110	-0.1202	-0.0907	-0.0243		+	Forebody	<u>දී</u>	1.0634	1.0977	7227	-0.0120	-1.5339	14941	1.3913	-1.3327	-1.2829	1.2398	1.1039	0.8869	-0.2358	-0.0711	-0.1205	-0.1356	0.1321	-0.1240	-0.0907	-0.0398
8		Fore	 	-3.12	88.	99	0.0	0.62	1.25	8. c 8. c	3.12	3.75	86.4	8 5	15.00	17.50	20.00	40.00	8 9	70.00	80.00	00:00	139.00			Fore	X ?	3.12	1.88	27.5	000																122.00
$\mathbf{mfr} = 0.57 \text{ and } \alpha = -2.0^{\circ}$	<b>.</b> 06	à c	2 2	1.0522	8160.1	0.3383	1.5467	-1.4799	1.4207	-1.3522	1.2196	-1.1714	92601-	-0.8305	0.2716	-0.0995	-0.1278	0.1271	50.0	0.1253	-0.1045	-0.0450	-0.0338	mfr = 0.57 and $\alpha = 0^{\circ}$	.06 = <b>0</b>	ody (	3 5	1.0520	9.0876	1.1209	1.5373	-1.4764	1.4177	1.3227	1.2036	1.1709	0.004	-0.8477	0.2159	-0.0775	-0.1212	0.1240	0.1257	<b>X</b> 2	0.0994	-0.0410	0.0325
r = 0.57 a		Forebody	3.75	-3.12	88.7	000				3.12			9, 9			20.00			800			122.00		fr = 0.57	+	Forebody	X/L	-3.12	.1.88					3.12								20.00				122.00	
Ē		÷	-0.0231	80000	0.0167	0.0851	0.1379	0.2017	0.2475	0.3810														8		Ą.	3 6	0.004	0.0171	0.0393	0.1332	0.1930	0.2374	0.3541													
	ಹಿ	Afterbody								283.30															ಹಿ	Afterbody			200.00																		
	o = o	Forebody	10119	1.0236	1.0617	1.1538	0.4565	-1.3752	-1.4561	1.2179	-1.1311	1.0306	1.0001	-0.8242	0.7440	-0.1748	-0.1415	0.1320	0.1339	-0.1238	-0.0925	0.0404	6000		• = 0°	Forebody	2 2	1.0556	1.0947	1.1213	0.1870	-1.5278	50/51	-1.3656	-1.2987	÷ 1	1.1708	-1.0255	-0.9206	-0.8419	-0.1008	0.1090	0671.0	-0.12/4	0.0907	-0.0390	-0.0225
		Fore	3.75	-3.12	88.	7.62	0:00	0.31	0.62	2.50	3.12	4.38	90.6	10.00	12.50	15.00	30.00	90.00	90.00	70.00	90:00	122.00	28.00			Fore	7 7	-3.12	1.88	C7 1.	0.00	0.31	7970	2.50	3.12	4.38	2.5	10.00	12.50	15.00	30.00	90.00	20.00	20.02	00.00	122.00	139.00
		Afterbody CT. CP		0.0158						0.3128																Afterbody	٠		0.0238																		
	<b>•</b> = 180°	<b>8</b> 5	2 5	183.30	8 9	238.90	8.6	266.70	27.7	283.30															80.	¥ Ş	3 5	183.30	200.00	38.5	89.5	2.98	3 2	8													
			• 9	=	≍ ⊼	3 23	25																		-																						
	÷	ĺ		1.1023	1.1389	6061	-0.6407	-1.6862	07507	1.5612	-1.5281			-1.3239			-0.2897	-0.0815	0.1051	-0.1010	-0.1178	-0.0892	-0.0316		•	rebody		1.0712	1.1128	1.1840	-0.2232				-1.3836	-1.3397	1.2937	-1.1699				-0.0960	0.1237	<b>10.113</b>	-0.1204	0.0876	-0.0396
3.0°	•	Forebody XA			1.1389		-0.6407	-1.6862		1.5612	-1.5281	3.75 -1.4923		7.50 -1.3239			20.00 -0.2897						139.00 -0.0316	1.0*		Forebody		1.0712		1.1840	-0.2232	66851		-1.4433		3.75 -1.3397				17.50 -0.4151							139.00 -0.0300
and α = .3.0°		Forebody	3.75 1.0872	-3.12 1.1023	-1.88 1.1389	6061	0.00 -0.6407	-1.6862	1.25 -1.0520	2.50 -1.5612	3.12 -1.5281		8.38	7.50	15.00	17.50	20:00		00.09	70.00	80.00		139.00	and α = -1.0°		•		-3.12 1.0712	1.1128	0.62	-0.2232	0.62 -1.5899	1.88 -1.4977	2.50 -1.4433	3.12	3.73	£ 53	7.50	15.00	17.50	20.00		30:00		80.00	90.00	139.00
fr = 0.67 and $\alpha$ = -3.0°		rebody Forebody	3.75 1.0872	1.0507 -3.12 1.1023	1.0929 -1.88 1.1389	0.3226 -0.62 1.1909	-1.5528 0.00 -0.6407	1.4933 0.62 -1.6862	1.464 1.89 1.4020	-1.3076 2.50 -1.5612	-1.2219 3.12 -1.5281	3.75	0.0976 4.38	0.7958 7.50	-0.2146 15.00	-0.1274 17.50	-0.1471 20.00	0.1355	0.1194 60.00	-0.1272 70.00	-0.1005 80.00	8 5	139.00	fr = 0.57 and $\alpha$ = -1.0°		rebody	10409	1.0483 -3.12 1.0712	-1.88 1.1128	0.3553 -0.62 1.1840	-1.5441 0.00 -0.2232	-1.4857 0.62 -1.5899	1.88 -1.4977	-1.3078 2.50 -1.4433	-1.2290 3.12	3.73	1.0114 5.00	0.8995 7.50	-0.2736 15.00	-0.0927 17.50	-0.1237 20.00	0.1223 40.00	0.1303	-0.1230 70.00	80.00	0.0400 90.00	-0.0288 122.00 139.00
	•06 = ♦	Forebody Forebody P XA. CP XA. CP	-3.75 1.0404 -3.75 1.0872	-3.12 1.0507 -3.12 1.1023	1.88 1.0929 -1.88 1.1389	0.3226 -0.62 1.1909	0.62 -1.5528 0.00 -0.6407	1.4933 0.62 -1.6862	7.50 11.425 1.25 1.0520	3.12 -1.3076 2.50 -1.5612	-1.2219 3.12 -1.5281	-1.1874 3.75	0.0976 4.38	0.7958 7.50	-0.2146 15.00	-0.1274 17.50	-0.1471 20.00	0.1355	0.1194 60.00	-0.1272 70.00	-0.1005 80.00	0.0432 90.00	139.00		.06 ± ♦	Forebody	2 -3.75 1.0409 -3.75	-3.12 1.0483 -3.12 1.0712	1.0942 -1.88 1.1128	0.00 0.3553 -0.62 1.1840	0.62 -1.5441 0.00 -0.2232	-1.4857 0.62 -1.5899	2.50 -1.3685 1.88 -1.4027	3.12 -1.3078 2.50 -1.4433	-1.2290 3.12	1.1809 3.75	1.0114 5.00	0.8995 7.50	-0.2736 15.00	-0.0927 17.50	-0.1237 20.00	0.1223 40.00	0.1303	-0.1230 70.00	-0.1023 80.00	0.0400 90.00	-0.0288 122.00 139.00
	•06 = <b>♦</b>	body Forebody Forebody CP XI. CP XI. CP 1	-3.75 1.0404 -3.75 1.0872	-0.0015 -3.12 1.0507 -3.12 1.1023	0.0142 -1.88 1.0929 -1.88 1.1389	0.0811 0.00 0.3226 -0.62 1.1909	0.1343 0.62 -1.5528 0.00 -0.6407	1.25 -1.4933 0.62 -1.6862	0.2422 1.88 1.4252 1.25 1.0520	0.3857 3.12 -1.3076 2.50 -1.5612	-1.2219 3.12 -1.5281	-1.1874 3.75	0.0976 4.38	0.7958 7.50	-0.2146 15.00	-0.1274 17.50	-0.1471 20.00	0.1355	0.1194 60.00	-0.1272 70.00	-0.1005 80.00	0.0432 90.00	139.00		°06 ± ♦	body Forebody	3.75 1.0479 3.75	-0.0009 -3.12 1.0483 -3.12 1.0712	-1.88 1.0942 -1.88 1.1128	0.0770 0.00 0.3553 -0.62 1.1840	0.1316 0.62 -1.5441 0.00 -0.2232	1.25 -1.4857 0.62 -1.5899	0.2973 2.50 1.3685 1.88 1.4027	0.3708 3.12 -1.3078 2.50 -1.4433	-1.2290 3.12	1.1809 3.75	1.0114 5.00	0.8995 7.50	-0.2736 15.00	-0.0927 17.50	-0.1237 20.00	0.1223 40.00	0.1303	-0.1230 70.00	-0.1023 80.00	0.0400 90.00	-0.0288 122.00 139.00
	06 = \$ 00 = \$ 00 = \$	body Forebody Forebody CP XI. CP XI. CP 1	166.70 -0.0281 -3.75 1.0404 -3.75 1.0872	183.30 -0.0015 -3.12 1.0507 -3.12 1.1023	200.00 0.0142 -1.88 1.0929 -1.88 1.1389	0.0811 0.00 0.3226 -0.62 1.1909	255.60 0.1343 0.62 -1.5528 0.00 -0.6407	266.70 0.1983 1.25 -1.4933 0.62 -1.6862	277.50 0.3042 1.88 1.4252 152 1.0520	283.30 0.3857 3.12 -1.3076 2.50 -1.5612	-1.2219 3.12 -1.5281	5.00 -1.1874 3.75	0.0976 4.38	15.00 -0.7958 7.50	17.50 -0.2146 15.00	20.00 -0.1274 17.50	-0.1471 20.00	50.00	0.1194 60.00	80.00 -0.1272 70.00	90.00 -0.1005 80.00	0.0432 90.00	0361		.06 = ♦	body Forebody	8 166.70 -0.0202 -3.75 1.0409 -3.75	183.30 -0.0009 -3.12 1.0483 -3.12 1.0712	0.0128 -1.88 1.0942 -1.88 1.1128	238.90 0.0770 0.00 0.3553 -0.62 1.1840	255.60 0.1316 0.62 -1.5441 0.00 -0.2232	0.1975 1.25 -1.4857 0.62 -1.5899	277.80 0.2973 2.50 -1.3685 1.88 -1.4077	283.30 0.3708 3.12 -1.3078 2.50 -1.4433	4.38 -1.2290 3.12	1.1809 3.75	10.00 -1.0114 5.00	15.00 -0.8995 7.50	17.50 -0.2736 15.00	20.00 -0.0927 17.50	40.00 -0.1237 20.00	0.1223 40.00	00.00 COC1.0- 00.00 00.04 00.01 0.000	-0.1230 70.00	90.00 -0.1023 80.00	0.0400 90.00	139.00 -0.0288 122.00

		c d	-0.0225	-0.0025	0.0161	0.0291	0.0767	0.1535	0.1980	10000	0.3843																				body	Ç	0.0051	0.0137	0.0310	0.0494	0.0957	0.1533	0.2206	0.2695	0.3258	0.3961																
	= 180°	Arteroody X/L C.	04.991	183.30	200:00	216.70	238.90	00.00	2,007	277.80	283.30																			\$ × 180°	Afterbody	χ	166.70	183.30	200.00	216.70	238.90	255.60	266.70	272.20	277.80	283.30																
	•	rorebody /L CP	1.0135	1.0262	1.0628	1.0921	1.1514	0.530	1 3667	1 2785	1.2494	1.1698	1.0975	1.0787	-1.0522	-0.9372	-0.1691	-0. 144 44	-0.1381	-0.1429	-0.1418	-0.1293	501105	0.1247	9	600	0.0266			*	sbody	ST. CP	0.9664	90.60	1.0200	1.0577	1.1257	0.4721	-1.3555	34	-1.2589	-1.2324	-1.1793	-1.0638	-1.0756	-1.0313	-0.9477	-0.3155	-0.1153	-0.1392	-0.1496	-0.1411	-0.1365	-0.1171	-0.1219	-0.0876	-0.0350	-0.0284
	Į	X. Z.	-3.75	-3.12	-1.88	1.25	0.62	8 9	79.0	3 2	2.50	3.12	3.75	4.38	2.00	7.50	12:00	17.50	20.00	40.00	50.00	00:09	00 02	8 9	8 8	3 5	139.00	۰			Fon	χ	-3.75	-3.12	-1.88	-1.25	-0.62	0.00	0.62	1.23		2.50	3.12	3.75	4.38	2.00	7.50	15.00	17.50	20.00	40.00	\$0.00	90.09	20.00	80.00	90.00	122.00	139.00
ıdα ≂ 2.0	<b>.</b>	c g	1.0359	1.0488	1.0925	1.1193	0.3808	1.5421	1.4880	1 3688	1.3027	12170	-1.179	-1.1008	0.9999	-0.8436	0.2174	-0.0951	-0.1252	0.1285	-0.1289	0.1239	1193	0.000	0.0400	0.042	0.00	7		.06 = ¢	ody	C C	0.9660	0.9678	1.0256	1.0461	0.7223	1.3924	.1.3256	1.2690	.1.2302	-1.1255	1.0767	-0.9978	-0.9198	-0.8555	-0.1365	-0.1293	-0.1412	0.144	-0.1342	-0.1282	-0.1169	061100	-0.0962	-0.0338	-0.0238	
mfr = 0.57 and $\alpha \approx 2.0^\circ$	.06 = <del>•</del>	Y.L CP	-3.75	-3.12	-1.88				9				200					20:00								20.00		90 - 7 Feet 90 - 3-		•	Fore	X/L CP	-3.75	-3.12	1.88	-1.25								2.00		10.00		17.50			20.00	00:09	70.00	80.00	90.06	122.00	139.00	
#a		<u>ئ</u> ۾	0.0141	86103	0.0234	.0421	.0850	6251	2,1893	2701	0.3257																	Ì			Ą.	G G	60000	0.0127	0.0280	0.0508	0.0974	0.1533	0.2189	0.2642	0.3194	0.3811																
	٠	Afferbody X/L C		183.30 0					07.002																					ኤ	Afterbo				200:00							283.30																
	• 0 = <b>•</b>	c g					1.1865			-1.0000		14020	3470	-1.3286	-1.2325	-1.1696	1.0908	-1.0117	0.1110	0.0464	0.0965	-0.1188	01130	0.0013	0.071	6000	0.020			% » •	ody	ę,	0.9642	96760	1.0354						3448	-1.2139	1.1397	1.0672	-1.0298	-0.9529	-0.8079	-0.7117	-0.1743	-0.1452	-0.1350	-0.1350	-0.1320	-0.1192	-0.0836	-0.0338	-0.0145	
		Forebody X/I. CF	3.75	-3.12			0.62			70.0				\$.00												8.77					Foreb	X/L CP	-3.75	-3.12	-1.88	-1.25								4.38								\$0.00			0006	122.00	139.00	
mfr = 0.67 and $\alpha = 1.0^\circ$	81 # 4	Forebody Forebody  P VA CP XA CP	.3.75 1.0362 -3.75 1.0283 166.70	-3.12	-1.88 1.0951 -1.88 1.0733 200.00	-1.25 1.1204 -1.25 1.1137 216.70	0.00 0.3695 -0.62 1.1694 238.90	0.62 -1.5379 0.00 0.1283	1.25 -1.4680 0.62 -1.4626 266.70	0.2.7.2 515.4.1. 52.1 17.4071 52.1	7165.1 08.1 0205.1- 05.2 7105.1. 08.6 A105.1. 51.5	0.002 202.1 0.02 0.00.1 20.0 0.002.1 0.002.1 0.000.1 0.000.1	57.E 9191 1-	1.0791 4.38	-0.9861 5.00	-0.8843 7.50	-0.2555 15.00	-0.0752 17.50	-0.1206 20.00	-0.1181 40.00	0100		0.00	0.07 821.0-		00.00	139,00 -0.03/2 122,00 -0.0393 139,00 -0.0333		mrr = 0.07 and a = 5.0	.06 = ♦	Forebody	P XI. CP XI. CP >	-3.75 1.0358 -3.75 0.9945 166.70	3.12 1.0549 -3.12 1.0068 183.30	1.88 1.0391 200.00	.1.25 1.1234 .1.25 1.0722 216.70	0.00 0.3934 -0.62 1.1376	0.62 -1.5462 0.00 0.4431 255.60	1.25 -1.4794 0.62 -1.3495 266.70	188 .1 4035 1. 251 . 272 20	2 50 -1 3846 1 88 -1 2016 277.80	11 12 C APIT CLE	4.38 .1.2050 2.12 .10501	-1.1626 3.75	-1.1113 4.38	5.00	-0.8730 7.50	17.50 -0.2419 15.00 -0.1580	-0.1394 17.50	-0.1429 20.00		0.1389 50.00	0.1310	00.00 87.01.0.	90.00 J. 100.00	-0.0477	-0.0373 122.00	
H	81 # <b>\$</b> 06 # <b>\$</b>	Forebody Forebody Afferbo	0.0014 .3.75 1.0362 .3.75 1.0283 166.70	0.0074 -3.12 1.0468 -3.12 1.0433 183.30	0.0213 -1.88 1.0951 -1.88 1.0733 200.00	0.0389 -1.25 1.1204 -1.25 1.1137 216.70	0.00 0.3695 -0.62 1.1694 238.90	0.1352 0.62 -1.5379 0.00 0.1283 255.60	0.1939 1.25 -1.4680 0.62 -1.4626 266.70	0.2345 1.56 1.4071 1.23 1.415 27.20	05.77. (1.6.1) 05.1 05.0.1. 05.1. 0.0.1.	0.550 200.1. 0.3 0.00.1. 21.0 0.00.0.	57.E 9191 1-	1.0791 4.38	-0.9861 5.00	-0.8843 7.50	-0.2555 15.00	-0.0752 17.50	-0.1206 20.00	-0.1181 40.00	0100	0009 69110-	0.00	0.07 821.0-	00.00	00.08	-0.0372 122.00 139.00				Afterbody Forebody	P XI CP XI CP XIL	0.0175 -3.75 1.0358 -3.75 0.9945 166.70	0.0168 3.12 1.0549 -3.12 1.0068 183.30	0.074 -1.88 1.0882 -1.88 1.0391 200.00	0.0444 -1.25 1.1234 -1.25 1.0722 216.70	0.3934 -0.62 1.1376 238.90	0.1340 0.62 -1.5462 0.00 0.4431 255.60	1.25 -1.4794 0.62 -1.3495 266.70	02 672 286 1. 261 251 20 20 181 1816 1	1 3846 1 88 -1 2016 277.80	0.3004 1. 02.0 APIT 1. 01.1 APR 283.30	4.38 1.3080 3.12 1.0501	-1.1626 3.75	-1.1113 4.38	-1.0037 5.00	-0.8730 7.50	-0.2419 15.00	-0.1394 17.50	-0.1429 20.00	0.1340 40.00	0.1389 50.00	01110 60.00	00.00 87.01.0.	0.1007	-0.0477	-0.0373 122.00	139.00
H	81 # 4	erbody Forebody Afferbo CP X.1. CP X.1. CP X.1.	7 166.70 0.0014 .3.75 1.0362 .3.75 1.0283 166.70	183.30 0.0074 -3.12 1.0468 -3.12 1.0433 183.30	200.00 0.0213 -1.88 1.0951 -1.88 1.0733 200.00	216.70 0.0389 -1.25 1.1204 -1.25 1.1137 216.70	238.90 0.0847 0.00 0.3695 -0.62 1.1694 238.90	255.60 0.1352 0.62 -1.5379 0.00 0.1283 255.60	266.70 0.1939 1.25 -1.4680 0.62 -1.4626 266.70	0.272.0 0.2543 1.56 1.4071 1.23 1.473 2.22.0	05.112 C1CC.1 88:1 020C.1 0C.2 0202.0	05.504 20.4.1. 05.4.4 01.05.1. 21.5 00.55.0 05.502 0.504 21.5 1.505.1. 21.5 0.505.1	500 State St	7.50 -1.0791 4.38	10.00 -0.9861 5.00	15.00 -0.8843 7.50	17.50 -0.2555 15.00	-0.0752 17.50	40.00 -0.1206 20.00	50 07 1811 0F 00 05	0005 1621 05 0009	0009 69110- 0002	00.00	00.07 8221.0- 00.09	MUM -4,0931 80.00	00.0x 6/60.0- 00.771	-0.0372 122.00 139.00			.081 = ♦ .06 = ♦	Afterbody Forebody Forebody	CP XII CP XII CP XII	8 166.70 0.0175 -3.75 1.0358 -3.75 0.9945 166.70	183.30 0.0168 3.12 1.0549 -3.12 1.0068 183.30	200.00 0.0774 -1.88 1.0391 200.00	216.70 00444 -1.25 1.1234 -1.25 1.0722 216.70	0.0859 0.00 0.3934 -0.62 1.1376 238.90	255.60 0.1340 0.62 -1.5462 0.00 0.4431 255.60	266.70 01862 1.25 -1.4794 0.62 -1.3495 266.70	05 272 2851. 251 280 1. 881 18150 05 575	277.80 02571 2.50 .1.3846 1.88 .1.2016 277.80	05.5.2. 0.5.5. 0.5.5. 0.5.5. 0.5.5. 0.5.5.5. 0.5.5.5. 0.5.5.5. 0.5.5.5. 0.5.5.5. 0.5.5.5. 0.5.5.5. 0.5.5.5. 0.5.5.5.	20.503 05.011 05.02 4.15. 4.15	\$00 -1.1626 3.75	7.50 -1.1113 4.38	-1.0037 5.00	15.00 -0.8730 7.50	17.50 -0.2419 15.00	20.00 -0.1394 17.50	40.00 -0.1429 20.00	50.00 -0.1340 40.00	00'05 681'0- 00'09	00.09 01110- 00.07	00.05 8751.05 00.08	00.08 7.001.04 00.09	122.00 -0.0477 90.00	139.00 -0.0373 122.00	139.00

TABLE V. Continued

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		Afterbody								0.3026																						Afferbody				0.0686																				
	• = 180°	Afte	ž	166.70	183.30	20000	210.70	25.35.7	266.75	272.20	277.80	283.30																			- 180 - +	Ane X	166.20	183.30	200:00	216.70	238.90	255.60	200.7	277.80	283.30															
	*	body	පි	0.8333	0.8602	0.9014	77.6	10101	1.1654	1.1760	1348	-1.10S0	-1.0718	-0.9824	-0.9640	-0.9172	-0.8642	-0.1167	-0.1557	0.1646	-0.1521	-0.1428	-0.1324	-0.1086	0.1121	-0.0747	-0.0202	-0.0163			11 -	og o	0 7740	0.7780	0.8338	0.8515	0.9246	1.0484	0.9858	0.8887	0.8743	-0.8128	0.6174	0.6998	0.2883	0.2292	0.2133	0.1647	0.1455	-0.1393	0.1295	0.1088	0.1146	76/00	-0.0224	1000
		Fore								1.23														89			122.00				5	rorebody VA	7.	-3.12	-1.88	-1.25																				
t = -3.1°			۵.	8	= :	2 3	2 3	5 5	2 2	83	573	120	86	2	<del>3</del> 2	514	<u>8</u>	<u></u>	<b>2</b>	<b>3</b>	33	S :	<b>3</b> 2	<u>.</u>	8	<u>=</u>	113		: a .1.1°																											•
and o	.06 = <b>♦</b>	Forebody								0.6093													-0.1055			-0.0317			and o	8	× -	rorebody	0.7297							0.5272										-0.1124						
mfr = 0.78 and α = -3.1°		Š	ž	-3.73	-3.12	20.7	7.1.0	3 6	- 2	1.88	2.50	3.12	4.38	200	7.50	10.00	15.00	17.50	20.00	900	20.00	00.00	90.02	80.00	8	122.00	139.00		mfr = 0.78 and α = .1.1°		2	, X	3.73	-3.12	.1.88	-1.25	0.00	0.62	C7 1	2.50	3.12	4.38	88	8 8	8 2	17.50	20.00	40.00	20.00	00:09	70.00	80.00	90.00	00.271	39.00	
ā		ğ	g G	0000	0.0200	0.0389	2000	0170	0.2464	0.2906	0.3485	0.4266																	ā		į	ۇ ئ ئ	00041	0.0263	0.0416	0.0676	0.1194	0.1776	7070	0.3494	0.4195															
	٠	Afterbody						255.60																							American	XII. C	_			216.70																				
	0 = 0							1 1869					0083	000	0687	8860	0952	6060	640	288	9824	-0.0955	2160	-0.0893	4 5	0187	90000			8	•		*						0.5250			0.2132	348	<b>1</b> 000	0.1900	142	-0.1568	1371	173	-0.1142	911	0.1070	0.0756	2 0	603	
		Forebody										2.50 0.																			Pomphody																									
		<b>124</b>	Ş	3.75		7 -	} <	000	Ö	ŏ	12	2.5	<u>.</u>	4	×	7	2	12	15.00	)   	<b>Q</b>	Š	80.00	8.00	Š	00771	139.				G	X	-3.75	-3.12	8.1-	-1.25	0.0	0.0	000	12	2.5	3.12	Ţ.	2 6	000	12.50	15.00	30.00	40.00	20:00	900	20.00	90.00	130 00	0.66	
	180°	Afterbody								272.20 0.2941																				000	Afterbody	X/L CP	166.70 0.0391			216.70 0.0710			272.20 0.3004		283.30 0.4102															
	*	ody o	පු දි	0.8090	0.5544	0.0471	10747	0.8461	1.1189	-1.0833	-1.0436	0.9399	-0.9112	0.8480	0.7876	0.8019	0.7505	-0.1948	0.2070	0.1030	6/6/10	0.1379	1001	20170	0.1169	0.0040	0.0287	0.0241		- 180	2	ှင် (၁	0.8033	0.8287	0.8587	0.8876	0.9886	1.0981	1.0553	-1.0240	9886	-0.9433	2,8013	0.00	6333	-0.1910	-0.2120	-0.1696	.1538	-0.1427	0.1314	660	0.1153	100	0.0183	
		Forebody	Z .							1 <u>2</u>			3.12						2 2			900					00.22				Porch	XL				-1.25						3.12						20.00			00.00		888		39.00	
= 0.71 and $\alpha$ = 0°	.06 m	Forebody	<b>a</b> 8	0.8019	0.0063	18360	1.0086	-1.1272	1.0601	-0.9917	-0.9895	-0.9289	0.8438	-0.7865	0.4525	-0.1746	0.1744	-0.1926	0.1508	0.1432	6.1303	0.1210	6.1163	0.0630	-0.0639 0.0000	1970.0	¥.0.0		= 0.78 and $\alpha$ = -2.1°	# OU.	a Pod	Č.	0.7452	0.7507	0.7676	0.8021	1.1851	- 10 V 04 I	0.4803	-0.5216	-0.5612	0.3717	-0.2039	0.2510	0.2002	-0.1895					0.0999			0.0156	_	
îr = 0.71	•	Fore	¥ ;	5.5	71.6-		000	0.62	1.25	88.	2.50	3.12	4.38	200	7.50	000	15.00	17.50	00.00	3 6	8 6	8 6	3 6	8 8	3 5	30.00	39.00		- 0.78 RI	•	Forehody	χľ	3.75		-1.88		_	70.0			3.12		8.5							8 8						
fa		pody	දී දී	0.0046	0.0252	0.000	0.1092	0.1700	0.2360	0.2845	0.3384	0.4031																	n T		ybody	S.	-0.0088	0.0201	0.0391	09900	0.150	0.7445	0.2921	0.3493	0.4205															
	8	Afferbody	X.	9 9	2000	216.70	238.90	255.60	266.70	272.20	277.80	283.30																		ě	Afterbody	χ	166.70	183.30	200.00	216.70	258.50	266.70	272.20	277.80	283.30															
	•	ğ S	- N	0.0000	0000	0.9647	1.0245	0.9162	-1.0925	-1.2018	-1.1092	-0.9933	-0.8395	¥ 5	-0.7843	0.5597	0.1814	0.200	6.1.4	0.1366	0.1330	130	217	10200	2000	70700	8890			•	-	å	0.6504	0.6694	0.6752	0.6618	0.6932	10.0	-0.2189	-0.1897	-0.1192	0.0808	0.00	-0.1713	-0.1513	-0.1375	-0.1139	0.1146	-0.0992	0.1021	-0.1057	7960.0	0.0708	0.000		
		Forebody	Z,					000										2 2								130.00					Forebody	Ķ				-1.25				1.25			99			12.50					200					

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	.08	Arrenbody X/I. CI	_		200:00			00.007		277.80																					<b>0</b> = 180°	Afterbody	χ		183 30		216.70	238.90	255.60	266.70	272.20	277.80	283.30																
	<b>\( \phi \)</b>	og G	0.6935	0.7158	0.7380	0.7258	0.7799	0.1800	0.4728	-0.3778	0.3481	-0.2740	-0.1998	-0.2069	-0.1977	-0.2366	17.10	102.0	0.170	1351.0	0 1166	9017	-0.1141	-0.0957	-0.1072	-0.0751	-0.0188	-0.0100			11	Forebody	ð	0.6069	0,6008	0.5850	0.5427	0.5099	1.1868	0.0351	0.0216	1200	0.0400	-0.0235	0.0139	0.0051	-0.0529	-0.0856	-0.1014	-0.1191	0.0978	-0.1055	-0.1022	-0.0942	-0.0801	0.1004	-0.0683	-0.0208	-0.0097
	,	Korebody X/I. CP	3.75	-3.12	-1.88 -1.88	1.25		30.0				3.12							3 5		3 5		8 8	00.00	80.08	0006	122.00	139.00		,		Fore	X	-3.75	215	~	- 25	-0.62	000	0.62	1.25	8	5	3.12	3.75	4.38	5.00	7.50	15.00	17.50	20.00	40.00	20.00	90.00	20.00	80.00	90:00	122.00	139.00
dα= 1.0°	. م	ğ û	0.7358	0.7534	0.7713	.7895	.1865	5,752	0.00/1	5713	222	0.2752	-0.2572	0.2840	0.2447	0.1968	1810	1404	0.1300	60.1.0	0.1166	0.1133	0.1000	0.1067	0.0839	-0.0203	0.0115			ום מ = 5.0 ספר א	06	ρφ	6	0.7345	2650	0.7635	0.7752	1.1776	0.8070	0.6275	-0.5571	0.4357	0.550	0.2988	-0.2925	-0.3103	-0.2609	-0.1975	-0.1939	-0.1456	-0.1369	-0.1249	-0.1195	9601.0	-0.1103	-0.0873	-0.0274	-0.0243	
Infr = 0.78 and $\alpha$ = 1.0°	.06 × •	K/Y										4.38						5		3 5				80.00		122.00				mr = 0.78 and a = 5.0"	06 = <b>0</b>	Foreh	X/L CP														10.00									00:06			
Ħ		à c	15200	0337	0.0473	.0725	.1242	17871	0.2530	2404	4108	3																	•			ģ	, B	00431	00415	0.0544	0.0760	0.1295	0.1897	0.2525	0 2964	0.7413	0.3041																
		Ž			200.00				200.70																						ئ	Afterbo	XI, CP	166.70				238.90				277.80																	
	<b>0</b> = <b>0</b>				0.8274				0.9399				-0.7457	-0.4168	-0.2705	02150	0.2530	0.000	2/07/0	0.1031	671.0	0.1742	-0.1232	-0.1141	-0.0740	-0.0184	-0.0057				() #	Apod	2	0.8373	0.8493	19000	0.9321	1.0286	0.8979	-1.1533	.1 2427	200	8	0.0718	1200	-0.9298	-0.8964	-0.7867	-0.3431	-0.1544	-0.1629	-0.134	-0.1338	-0.1282	-0.1161	-0.0735	-0.0185	-0.0074	
		Forebody	7 7	-3.12	-1.88	-1.25	-0.62					3 2												70.00		122.00						Porehody	X	17.	21.5			-0.62	000	0.31	0.60	2 2	5	12	4 35	200	7.50	10.00	12.50	15.00	30.00	40.00	20.00	00:09	20.00	00:06	122.00	139.00	
= 0.78 and $\alpha$ = 0°	æ = 180	rebody Foreb	07759 335 07010 16570 C	-3.12 0.7576 183.30	-1.88 0.7595 -1.88 0.7985 200.00 0.0456	0.7910 -1.25 0.7908 216.70	1.1840 -0.62 0.8285 238.90	-0.7549 0.00 1.1489 255.60	0.7294 0.62 0.7373	07.212 1080.0- 62.1 72.20	-0.5350 1.86 -0.5/7 2/7.60	0.502 0150.0 05.2 5015.0 0.503.00 0.003	0.2514	0.1018	0.2617	0.50	0.17	9 7		-0.1389	-0.1183 40.00	-0.1216 50.00	70.00 -0.1064 60.00 -0.1114	-0.1120 70.00	-0.0915 80.00	-0.0246 90.00	-0.0169 122.00			= 0.78 and $\alpha$ = 2.0°	- 180°	Pombodi	CD AT CD	07373 375 0.6568 16670 4	0.001 0.000 0.000	0.001 0/000 21.0 114.0	96.1.	08875 5250 530 1881	0.000 0.000 0.000 0.000	0.000 0	0.000	02.212 1801.0- 62.1 60.40.0-	05:117 07:170 09:1 10:170	0.502 C01.0- 0.2 APC.0-	3.12	0.200	10.00 -0.2457 5.00 -0.1324	-0.2014 7.50	0.1890 15.00		-0.1365 20.00	-0.1190 40.00	-0.1159 50.00	-0.1014 60.00	0.1089 70.00	80.00	-0.0277 90.00	-0.0204 122.00	139.00 -0.0050
mfr = 0.78 and $\alpha = 0^{\circ}$	<b>♦</b> = 180	Forebody Forebody Afterbo	XL CF XL CF XL	.3.12 0.7551 -3.12 0.7576 183.30	.1.88 0.7595 -1.88 0.7985 200.00	-1.25 0.7910 -1.25 0.7908 216.70	0.00 1.1840 -0.62 0.8285 238.90	0.62 -0.7549 0.00 1.1489 255.60	0.62 -0.7373 266.70	07.717 10.69.0 67.1 1.25 - 67.50	08:7/7 2//5.0- 08:1 06:00-0 C: C	05.502 U150.0- U5.2 2016.0- 21.5 4.18 0. 262 1. 12 0.4014	771	0.1018	0.3517	0.50	0.17	-0.1900	0.154	0.1389 20.00	-0.1183 40.00	-0.1216 50.00	0.1064	-0.1120 70.00	-0.0915 80.00	00:06	-0.0169 122.00	139.00		$\mathbf{mfr} = 0.78 \text{ and } \alpha = 2.0^{\circ}$		Donnbods Pombods	o vi co vi co vi	07 37 0554 157 0554 157 0570	0.001 00.00 0.1.0. 0.100 0.10	0.001 0/000 21.0 114.0	0.002 81/0.0 86.1. \$50.00 86.1.	0882 C529 C70 F1811 WO	09352 70801 000 0000 0000	0.000 0	0.000 0.000 301 301 301 301	07777 10100- 671 671- 691 991	05:117 07:170 09:1 10:170	0.12 -0.4544 2.50 -0.1055 405.50 5.15 605.50	27.5	0.200	-0.2457 5.00	-0.2014 7.50	0.1890 15.00	0.1401	-0.1365 20.00	-0.1190 40.00	-0.1159 50.00	-0.1014 60.00	0.1089 70.00	-0.0868 80.00	-0.0277 90.00	-0.0204 122.00	139.00
	y2 = φ = 06° = φ = 180°	erbody Forebody Afterbo	XL CF XL CF XL	0.0144 - 3.13 0.1258 - 3.12 0.7576 183.30	0.00413 -1.88 0.7595 -1.88 0.7985 200.00	0.0673 -1.25 0.7910 -1.25 0.7908 216.70	0.1174 0.00 1.1840 -0.62 0.8285 238.90	0.1766 0.62 -0.7549 0.00 1.1489 255.60	1.25 -0.7294 0.62 -0.7373 266.70	0.2932 1.88 -0.6527 1.25 -0.6961 212.20	08:7/7 2//5.0- 08:1 06:00-0 C: C	0.4124 5.12 -0.5109 2.30 -0.0510 265.30 4.18 -0.554 1.10 -0.4014	771	0.1018	0.3517	0.50	0.17	-0.1900	0.154	0.1389 20.00	-0.1183 40.00	-0.1216 50.00	0.1064	-0.1120 70.00	-0.0915 80.00	-0.0246 90.00	-0.0169 122.00	139.00		$mfr = 0.78$ and $\alpha = 2.0^\circ$		A = 100 Possible de la Possible de la Comptende la Compten la Comptende la Comptende la Comptende la Comptende la Comptend	VA CD VA CP VA	05 37	0.094 -5.15 0.1523 -5.15 0.0506 100.00	OCCEST 0/500 21.5. 1147.0 21.5.	000007 91100 90'1. 6000'0 90'1. 6000'0 00'007	05 81.6 65.90 69.0 PEST 00.0 1961.0 00.017	09 55C 7081 1 000 0508 0 050 05810 05950	00.000 F00.11 00.0 F00.00 20.0 0.1635 00.00 00.255	00 CCC 1891 0. 3C1 3083 0 881 53050 06 555	08:7/7 1801:0- 67:1 CO+CO- 99:1 /567:0 07:7/7	00:11.0 01:34.0 01:0 02:0 01:0	00:507 CC01.0: 00:7 #464.0- 21:5 070#10 06:587	4.36 -40.2634 3.12 5.00 0.3500 3.75	750 -0.2566 4.38	10,00 -0,2457 5,00	15,00 -0.2014 7.50	17.50 -0.1890 15.00	20.00 -0.1401 17.50	40.00 -0.1365 20.00	50.00 -0.1190 40.00	60.00 -0.1159 50.00	70.00 -0.1014 60.00	80.00 -0.1089 70.00	00:08 8980:0- 00:06	122.00 -0.0277 90.00	139.00 -0.0204 122.00	139.00
	<b>♦</b> = 180	Afterbody Forebody Afterbo	XIL CP XIL CF XIL CF XIL CF XIL	100.70 0.0144 - 2.12 0.1254 - 2.12 0.755 100.70	0.00413 -1.88 0.7595 -1.88 0.7985 200.00	216.70 0.0673 -1.25 0.7910 -1.25 0.7908 216.70	238.90 0.1174 0.00 1.1840 -0.62 0.8285 238.90	255.60 0.1766 0.62 -0.7549 0.00 1.1489 255.60	266.70 0.2483 1.25 -0.7294 0.62 -0.7373 266.70	277.20 0.2932 1.88 -0.6527 1.25 -0.6961 272.20	277.80 U.3488 2.30 -0.3330 1.36 -0.3772 277.00	0.4124 5.12 -0.5109 2.30 -0.0510 265.30 4.18 -0.554 1.10 -0.4014	27.5 \$15.0° W.S	7.50 .0.30.8 4.38	000 5050	05.0 1667.0 00.01	OC:1 9761:0- OC:1 9767:0-	0.51 - 0.571	20.00 -0.1544 17.50	0.1389 20.00	-0.1080 -0.1183 40.00	-0.1253 60.00 -0.1216 50.00	-0.1034 70.00 -0.1064 60.00	-0.1120 70.00	-0.0815 90.00 -0.0915 80.00	-0.0181 122.00 -0.0246 90.00	-0.0069 122.00	139.00		$mfr = 0.78$ and $\alpha = 2.0^{\circ}$	- 4 - 00	The Description Prompted to	stoody rurenody rurenowy are in	OF AND OF	0.3105 100.00 0.000 0.025 0.025 0.000 0.000 0.000	00'000 01'00'0 21'00 114'00 71'00 66'1 1778'0 1778'0 1778'0 66'1 1778'0 66'1 1778'0 66'1 1778'0	0.87.36 200.00 0.0463 -1.86 0.7034 -1.86 0.00.00 2315 200.00	05 81.6 65.90 69.0 PEST 00.0 1961.0 00.017	(A) 75 1000 2000 COLUMN 1020 1021 1020 COLUMN 1020 COL	00.000 F00.11 00.0 F00.00 20.0 0.1635 00.00 00.255	00 CCC 1891 0. 301 3083 0 881 C300 00 CCC 3001	07:717 1001:0- C7:1 C0+C0- 99:1 /C67:0 07:717 C911:1-	00:117 07170, 00:1 MONTO 00:0 00:00 00:00 00:00	41,9435 283,30 0,4026 3.12 -0,4344 2.30 -0,1033 203,30	-0.8808 4.36 -0.2634 3.12	0.200	-0.7300 10.00 -0.2457 5.00	-0.2991 15.00 -0.2014 7.50	17.50 -0.1890 15.00	.0.1482 20.00 -0.1401 17.50	J. 1744 40.00 -0.1365 20.00	-0.1329 50.00 -0.1190 40.00	01168 60.00 -0.1159 50.00	00.05	0000 - 01089 70.00	00.051 90.00 -0.0868 80.00	00000 122.00 -0.0277 90.00	JO 00046 122.00	139.00

TABLE V. Continued

(b) Continued

266.70 0.2343 277.80 0.2344 283.30 0.3876	9000 1.25 2.25 3.12 4.38 5.00 15.00 15.00 15.00 15.00 15.00 10.00	3.75 O.048 3.17 O.048 3.17 O.0084 3.18 O.3316 0.00 O.9074 0.00 O.9074 0.00 O.9074 0.00 O.9074 0.00 O.9076 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090 0.0090	No. 2 (1972)  No	# C # X C Z C # C 2 C 1 C 2 C C 2 C 2 C 2 C 2 C 2 C 2 C	Afferbody  2	ody CP CP 0.0028 0.0054 0.00643 0.1343 0.1335 0.2352 0.3382	For XL XL XL 3.75 3.75 3.17 3.18 5.18 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.0	Prevebody 7L CP	\$ 7 = 2 % K K K K K K K K K K K K K K K K K K	Afterbody KL. CP 66.70 0.0047 88.30 0.0316 90.00 0.0318 16.70 0.0780 88.90 0.1250 88.90 0.1250 77.20 0.2733 77.80 0.3267 88.30 0.3870	Pore X/L3.75 -3.12 -4.88 -1.18 -1	Portbody CL CP CT	Form XII. 3.175 - 3.17	Perebody 1. CP   Presebody 1. CP   CP   CP   CP   CP   CP   CP   CP	## = 180° Afterbody Afterbody Afterbody Afterbody Afterbody A 166.70 0.00 0.00 0.00 0.00 0.00 0.00 0.00	004 0.0501 0.0501 0.0501 0.0501 0.0501 0.0501 0.0501 0.0501 0.0501 0.0501 0.0501
mfr Afterbody XII. CP 165.70 0.0078 183.90 0.0319 216.70 0.0760 228.90 0.1244 228.90 0.1244 226.70 0.2387 265.70 0.2387 277.20 0.2387 277.20 0.2387 277.20 0.3288	•	0.95 and α = -1.1?  Porebody  Forebody  3.75 0.0686 3.75 0.0087 3.12 0.0287 0.00 0.0889 0.00 0.0889 0.00 0.0889 0.00 0.0889 0.00 0.0889 0.00 0.0889 0.00 0.0889 0.00 0.0889 0.00 0.00	Forebody XI. CP XI. CP 3.75 0.2141 0.2061 0.		<b>1. 1. 1. 1. 1. 1. 1. 1. 1</b>	ody CP 0.0402 0.0429 0.05381 0.07381 0.1274 0.1377 0.2463 0.3361 0.3931	For X X X X X X X X X X X X X X X X X X X	Porebody 7. C. P. P. C. P. P. C. P. C. P. P.	* 0* After After X/L 166.70 183.30 218.30 2285.60 2265.70 277.80 283.30	body CP 0.0227 0.0337 0.0373 0.0737 0.1789 0.1789 0.2383	Fore 10.85 (1) 11.50 (1) 1		************	4 = 4  2.7. CP  3.7. CP  3.8. 0.126  3.9 0.126  3.9 0.126  3.9 0.126  3.9 0.126  3.9 0.126  3.9 0.126  3.9 0.126  3.9 0.126	→ = 180°  Afterbody  Afterbody	ody CO24 0.0054 0.0056 0.0056 0.0056 0.0057 0.0057 0.0057 0.0057 0.0057

		و د و	0.0115	0348	0.0540	1248	0.1780	.2388	0.2843	3318	0.3965																																																
	°.	Afferbody X/L C				238.90			272.20 (		283.30 (																																																
	.081 = <b>\( \phi \)</b>					-0.8022						0.000	0.000	0101	0.1820	57100	2 2	-0.0463	1710	0.0716	0927	-0.0943	0827	-0.0993	-0.0694	EVIO	-0.0032																																
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2.0°		<sup>2</sup> X	4	ė,	÷·	<del>,</del>	Ö	Ö	-	-	~ `	٠, د	ri <b>≺</b>	·	· -	· <u>·</u>	2 2		3 :	₹ :	8	8	2	8	8	5	2 6																																
= 0.95 and $\alpha \approx 2.0^\circ$	.06 = \$	S G	-0.0570	0.0259	-0.3240	0.8964	0.4247	0.2457	0.1954	0.1199	0.1015	0.0884	0.0314	0.0102	0.047	0.0867	0000	0.0963	460.0	0.1039	0.0922	-0.1012	-0.0897	0.0647	-0.0097	6000	C#377																																
= 0.95 a	•	Y.7. CP	3.75	-3.12	-1.88	000	0.62	1.25	1.88	2.50	3.12	8. 8 8. 8	3 5	9 6	8 5	2 5	2 2	40.00	9.0	800	00.09	9000	80.00	0006	122.00	00 00.1	97.60																																
相			<u> </u>	<u>\$</u>	573	8 8	6	161	653	868	0.3820																																																
		Afterbody K/I. CP				0.0906																																																					
	ر ه	Ž 5				238.90																																																					
		Forebody 7. CP	0.2791	0.3035	0.2524	0.1/84	1.1632	0.2442	0.0902	-0.0296	20.0494	77000	100	0.102	2 2 4	0.1480	0 1 10 1	2 2	<b>X</b>	0.1156	-0.1038	\$ 0	-0.0916	-0.0610	-0.0209	0.0117	100																																
		York	-3.75	-3.12	-1.88	C 29 G	000	0.31	0.62	1.25	2.50	3.12	9 8	8 5	3 5	2 5	2 2	20.02	30.00	90.0	\$0.00	00:09	00.00	0000	122.00	0000	39.00																																
		× 9.	168	3337	3543	57/1	1780	2417	2856	3337	970																			<u>.</u>	e E	0056	0341		0360	1//0	1242	1769	2418	787	3340	4006	4000																
		Rerbody				0.0723					30 0.3970																			fterbody		.70 0.0056			00000 000						0.000																		
	.= 180°	ĝ	166.70	183.30	200.00	238.90	255.60	266.70	272.20	277.80	283.30			. •	* 0		~ •	0.6	7	•	0	•	_	_	000				180		χ	166.70	183 30	0000	200.00	710.70	238.90	255.60	266.70	06 676	27.7.60	262.20	763.30	*	rys	· =	• 6	. 4				÷ v	0 1	₹ '	-	2	.2	23	11
	)SI = +	Afterbo X/I.	166.70		200.00		255.60	266.70	272.20	277.80	283.30	0.1660	0.141	0.1487	0.1004	50500	11600	-0.0/45	-0.0782		-0.0830		-0.0771	-0.0901	.0.0588	2000	0.0041		¥ = 0		χ		183 30	0000		710.70	238.90	255.60	266.70	04 677 773 70	0.277 11850	0.3464 303.30	0.562 05950									-0.0003			0.0681				
	)SI = +	Afterbo X/I	0.1976 166.70	-0.1798 183.30	-0.4261 200.00	238.90	1,0200 255.60	0.4940 266.70	0.3329 272.20	0.2443 277.80	283.30					15 00 0.0503		17.50 -0.0/45			50,00 -0.0830				90.00 0.0588		139,00 -0.0041		¥ = 0	rebody	CP X/L	166.70	-0.5723 183.30	00'000 00000	00.002 06/1.0-	-0.8918 216.70	-0.9642 238.90	0.9312 255.60	0.6619 266.70	04 677 773 70	0.277 11850	0.3464 303.30	0.562 05950	3.12 0.2894								40,00 -0.0003			70.00 -0.0681				139.00 -0.0037
α = 1.0°	₩ = 180	Forebody Afterbo	3.75 -0.1976 166.70	-3.12 -0.1798 183.30	-1.88 -0.4261 200.00	-0.67 -0.8619 216.70	0.00 1.0200 255.60	0.62 0.4940 266.70	1.25 0.3329 272.20	1.88 0.2443 277.80	2.50 0.1780 283.30	3.12	3.73	4.38	3.00	3 2	8.5	00.70	20.00	40.00	20.00	90:00	20.00	80.00	00'06	9000	139.00	I a = 3.0°	¥: = ◆ · · ·	Forebody	X/L CP X/L	-3.75 -0.5046 166.70	08 181 16229 - 51 1.	00'001 67100 7110	00.002 00.7/30 200.00	07'917 8168'0- 67'1-	-0.62 -0.9642 238.90	0.00 0.9312 255.60	0.62 0.6619 266.70	175 04817 270	08.777 1187.0 52.1	02.112 2.11.00	00:007 00:00 00:7	3.12	25.4	, e	9	2 2	9 5	0000	70.07	90.00	20.00	80.00	20.00	80:00	90.06	122.00	139.00
.95 and α = 1.0°	₩ = 180	rebody Forebody Afferbo CP X/I. CP X/I.	0.0544 -3.75 -0.1976 166.70	-0.0104 -3.12 -0.1798 183.30	-0.3674 -1.88 -0.4261 200.00	0.5302 -0.25 -0.6078 216.70	0.4217 0.00 1.0200 255.60	0.2460 0.62 0.4940 266.70	0.2116 1.25 0.3329 272.20	0.1192 1.88 0.2443 277.80	0.1142 2.50 0.1780 283.30	0.0877 3.12	0.0298	0.0240 4.38	0.0372 3.00	0.0074 15.00	00.03 14	0000	-0.0962 20:00	-0.0824 40.00	-0.0893 50.00	-0.0840 60.00	-0.0893 70.00	00.08	00048 90.00	00000	139.00	$3.95 \text{ and } \alpha = 3.0^{\circ}$	¥: = ◆ · · ·	rebody Forebody	CP X/L CP X/L	0.0596 -3.75 -0.5046 166.70	01 181 1677 0 - CLE. F191 0-	00'000 0000 0000 000	-0.315/ -1.88 -0.790 200.00	0.4987 -1.25 -0.8918 216./0	0.8808 -0.62 -0.9642 238.90	0.3835 0.00 0.9312 255.60	0.2912 0.62 0.6619 266.70	0.077 778 0.4817 77.00	08.777 1187.0 57.1 2741.0	0.000 3460 036 0000	0.1410 0.50 0.00 0.00 0	0.0340	0.000	00.5	0.0746 7.50	0.00	0.0873	0000	00007	0.0982 40.00	00.00	00000	0.0908	00.08 80.00	-0.0216 90.00	-0.0151 122.00	139.00
mfr = 0.95 and α = 1.0°	₩ = 180	Afterbo X/I.	0.0544 -3.75 0.1976 166.70	-0.0104 -3.12 -0.1798 183.30	-0.3674 -1.88 -0.4261 200.00	-0.67 -0.8619 216.70	0.4217 0.00 1.0200 255.60	0.2460 0.62 0.4940 266.70	0.2116 1.25 0.3329 272.20	0.1192 1.88 0.2443 277.80	2.50 0.1780 283.30	0.0877 3.12	3.73	0.0240	0.0372 3.00	3 2	00.03 14	00.70	-0.0962 20:00	-0.0824 40.00	20.00	-0.0840 60.00	-0.0893 70.00	00.08	00'06	00000	139.00	mfr = 0.95 and $\alpha = 3.0^{\circ}$	¥: = ◆ · · ·	rebody Forebody	CP X/L CP X/L	-3.75 -0.5046 166.70	01 181 1677 0 - CLE. F191 0-	00'000 0000 0000 000	-0.315/ -1.88 -0.790 200.00	0.4987 -1.25 -0.8918 216./0	0.00 0.8808 -0.62 -0.9642 238.90	0.62 0.3835 0.00 0.9312 255.60	1.25 0.2912 0.62 0.6619 266.70	00 01 00 0 10 0 00 1	05:212 (185:0 C2:1 25:1:0 00:1	00.712 F100.0 08.1 00.00.0 00.2	00.002 00.00 00.2 01.410 21.5 00.000 01.6 00.000 01.8	3.12	0.000	00.5	0.0746 7.50	0.00	9 5	0000	00007	90.00	00.00	00000	0.0908	00.08 80.00	-0.0216 90.00	122.00	139.00
mfr = 0.95 and $\alpha$ = 1.0°	φ = 90°	Forebody Forebody Afterbo	7 3.75 -0.0544 3.75 -0.1976 166.70	-3.12 -0.0104 -3.12 -0.1798 183.30	1.88 -0.3674 -1.88 -0.4261 200.00	0.5302 -0.25 -0.6078 216.70	0.62 0.4217 0.00 1.0200 255.60	1.25 0.2460 0.62 0.4940 266.70	1.88 0.2116 1.25 0.3329 272.20	2.50 0.1192 1.88 0.2443 277.80	0.1142 2.50 0.1780 283.30	0.0877 3.12	0.0298	0.0240 4.38	0.0372 3.00	0.0074 15.00	00.03 14	0000	-0.0962 20:00	-0.0824 40.00	-0.0893 50.00	-0.0840 60.00	-0.0893 70.00	00.08	00048 90.00	00000	139.00	mfr = 0.95 and $\alpha = 3.0^\circ$	81 = ♦	Forebody Forebody	X/L CP X/L CP X/L	0.0596 -3.75 -0.5046 166.70	08181 16720- 518. 11910- 518.	00'000 0000 0000 000	0.000 0.000 0.000	07.01.2 -0.4987 -1.25 -0.8918 216.70	0.00 0.8808 -0.62 -0.9642 238.90	0.62 0.3835 0.00 0.9312 255.60	1.25 0.2912 0.62 0.6619 266.70	00 01 040 01 04810 081	08.777 1187.0 57.1 2741.0	00.712 F100.0 08.1 00.00.0 00.2	00.002 00.00 00.2 01.410 21.5 00.000 01.6 00.000 01.8	0.0340	0.000	00.5	0.0746 7.50	0.00	0.0873	0000	00007	0.0982 40.00	00.00	00000	0.0908	00.08 80.00	-0.0216 90.00	-0.0151 122.00	139.00
	06 = <b>♦</b> = 180	rbody Forebody Forebody Afferbo	-3.75 -0.0544 -3.75 -0.1976 166.70	0.0420 -3.12 -0.0104 -3.12 -0.1798 183.30	0.0560 -1.88 -0.3674 -1.88 -0.4261 200.00	0.0805 -1.25 -0.5302 -1.25 -0.6078 216.70	0.1807 0.62 0.4217 0.00 1.0200 255.60	0.2414 1.25 0.2460 0.62 0.4940 266.70	0.2809 1.88 0.2116 1.25 0.3329 272.20	0.3264 2.50 0.1192 1.88 0.2443 277.80	0.3817 3.12 0.1142 2.50 0.1780 283.30	0.0877 3.12	0.0298	0.0240 4.38	0.0372 3.00	0.0074 15.00	00.03 14	0000	-0.0962 20:00	-0.0824 40.00	-0.0893 50.00	-0.0840 60.00	-0.0893 70.00	00.08	00048 90.00	00000	139.00	$\mathbf{mfr} = 0.95 \text{ and } \alpha = 3.0^{\circ}$	81 = ♦	Afterbody Forebody Forebody	CP XI CP XI CP XIL	0.0590 3.75 0.0596 3.75 0.5046 166.70	0181 1873 0- 51 E. F1910- 51 F. F8730	00'001 62160 001 2160 216 66600	0.002 041.0- 88.1- 1.515 1.1-88 1.1- 8.0000	0.0864 -1.25 -0.4987 -1.25 -0.8918 216./0	0.1355 0.00 0.8808 -0.62 -0.9642 238.90	0.62 0.3835 0.00 0.9312 255.60	0.2514 1.25 0.2912 0.62 0.6619 266.70	00000 00000 00000	05:212 (185:0 C2:1 25:1:0 08:1	00.212 2.20 0.023 1.88 0.3874 2.12.00 00.000	06.682 06.60 06.2 01.410 21.6 0616.0 06.60 0 06.8	0.0340	0.000	00.5	0.0746 7.50	0.00	0.0873	0000	00007	0.0982 40.00	00.00	00000	0.0908	00.08 80.00	-0.0216 90.00	-0.0151 122.00	139.00
	φ = 90°	Afterbody Forebody Porebody Afterbo	166.70 0.0337 -3.75 -0.0544 -3.75 -0.1976 166.70	183.30 0.0420 -3.12 -0.0104 -3.12 -0.1798 183.30	200.00 0.0560 -1.88 -0.3674 -1.88 -0.4261 200.00	216.70 0.0805 -1.25 -0.502 -1.25 -0.6078 216.70 0.0805 -0.0078 216.70	255.60 0.1807 0.62 0.4217 0.00 1.0200 255.60	266.70 0.2414 1.25 0.2460 0.62 0.4940 266.70	272.20 0.2809 1.88 0.2116 1.25 0.3329 272.20	277.80 0.3264 2.50 0.1192 1.88 0.2443 277.80	283.30 0.3817 3.12 0.1142 2.50 0.1780 283.30	4.38 0.0877 3.12	5.00 0.000 0.000	80.9 0920.0- 00.7	0000 27000-0001	0.000 0000	00.C1 +140.0- 0C.11	OC/1 O680 D-0007	40.00 -0.0962 20.00	50.00 -0.0824 40.00	60.00 -0.0893 50.00	70.00 -0.0840 60.00	80.00 -0.0893 70.00	00'08 8690'0- 00'08	122.00 -0.0148 90.00	23000 00000	00.221 (20.00- 0.005)	mfr = 0.95 and $\alpha = 3.0^\circ$	881 ≡ ♦	Afterbody Forebody Forebody	XI. CP XII. CP XII. CP XII.	166.70 0.0590 -3.75 0.0596 -3.75 -0.5046 166.70	0. 181 1677 0. 51 F. F191 0. 51 F. F730 0. 181	00'001 0710'0 11'0' 0110'0 11'0' 01'00'0 00'00'	200.00 0.0053 -1.88 -0.5157 -1.88 -0.707	216.70 0.0864 -1.25 -0.4987 -1.25 -0.8918 216.70	238.90 0.1355 0.00 0.8808 -0.62 -0.9642 238.90	255.60 0.1935 0.62 0.3835 0.00 0.9312 255.60	266.70 0.2514 1.25 0.2912 0.62 0.6619 266.70	00 CCC C1870 3C1 CPV10 881 0C0C0 0CCC	05.272 (184.0 C2.1 2441.0 00.1 (102.0 02.272 03.272	00:112 F100:0 00:1 00:00:0 00:1 70ECO 01:100	00,002 00,00 00,2 01,410 1,50 00,000 00,002	4.38 0.0340 5.12	7 \$0 -0 0393	003 50000-0001	15.00 -0.0746 7.50	12.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	05.61 618000 00000	0000 0000	0007 14000 0004	20:00 -0:0987 40:00	00.00	00.00 10.0967	80:00 -0:0908 70:00	00:08 0890:0-00:06	122.00 -0.0216 90.00	139.00 -0.0151 122.00	139.00
	06 = <b>♦</b> = 180	rbody Forebody Forebody Afferbo	0.1833 166.70 0.0337 -3.75 -0.0544 -3.75 -0.1976 166.70	0.1941 183.30 0.00420 -3.12 -0.0104 -3.12 -0.1798 183.30	0.0507 200.00 0.0560 -1.88 -0.3674 -1.88 -0.4261 200.00	-0.2129 216.70 0.0803 -1.25 -0.5302 -1.25 -0.6078 216.70 0.0803 -1.25 -0.5302 -1.25 -0.6078 216.70	1.1362 255.60 0.1807 0.62 0.4217 0.00 1.0200 255.60	0.4822 266.70 0.2414 1.25 0.2460 0.62 0.4940 266.70	0.2019 272.20 0.2809 1.88 0.2116 1.25 0.3329 272.20	0.1489 277.80 0.3264 2.50 0.1192 1.88 0.2443 277.80	0.0706 283.30 0.3817 3.12 0.1142 2.50 0.1780 283.30	0.0895 4.38 0.0877 3.12	0.0390 0.0350 0.0350 0.0350 0.0350	95.4 0420.0 0003	0.0372 3.00	0031 62000- 00.01	00.01 #150.0- 00.11	067.1 0680.0- 00002 7.0000	-0.1145	-0.0965 50.00 -0.0824 40.00	-0.1011 60.00 -0.0893 50.00	-0.0840 60.00	-0.0893 70.00	OU 08 80 00 O O O O O	0000 00000 00000	0.000	139.00	mfr = 0.95 and $\alpha = 3.0^{\circ}$	881 ≡ ♦	Afterbody Forebody Forebody	CP X/L CP X/L CP X/L CP X/L	0.0590 -3.75 0.0596 -3.75 -0.5046 166.70	08 181 1677 0. 51 F. F191 O. 51 F. F83 30 OF F81 5725 O	00'000 0000 001 00100 0010 0000 00000 00000 00000	0.3908 200,00 0.0053 -1.88 -0.3157 -1.88 200,00	0.3188 216.70 0.0864 -1.25 -0.4987 -1.25 -0.8918 216.70	0.2367 238.90 0.1355 0.00 0.8808 -0.62 -0.9642 238.90	0.1935 0.62 0.3835 0.00 0.9312 255.60	0.0738 266.70 0.2514 1.25 0.2932 0.62 0.6619 266.70	00 22	02:717 1194'0 C7'1 7441'0 08'1 610'0 07'7/7 4100'0-	00.114 F100.0 08.1 00.00,0 00.1 210.0 00.114 00.00.0-	06:007 06:00 06:7 01:410 71:0 06:007 75:01:00	4.38 0.0340 5.12	81.7 1000 000 1 1800 0 1901 0	00.5 70.00 00.01 71.00 71.00	05.7 97.00 -0.0746 7.50	0051 5750 0.571	0.0873	0.00	00.04 1900 00.04	-0.1202 30.00 -0.0982 40.00	0.00 0.000 0.000	0.1120	-0.1091 80.00 -0.0908 70.00	-0.0604 90.00 -0.0680 80.00	122.00 -0.0216 90.00	-0.0021 139.00 -0.0151 122.00	139.00

TABLE V. Continued

(c) M = 0.87

		g G	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	6000	77100	0.070	6000	0.0710	0.176	0.461	0.4063	75750	0.367																		1	3 6	0.0152	0.003	00400	0.0560	0.1078	0.1698	0.2399	0.2888	0.3470	0.4145															
	\$ = 180°	Affert	777	182.70	200	3.67	230.00	255.60	26.73	373 30	777.80	367.30	06.502																	<b>★</b> 180°	Afterbody	X.	02.99	183.30	20000	216.70	238.90	255.60	266.70	272.20	277.80	283.30															
		Forebody	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	1000	1001	130	1,011	0.000	1 4786	13601	1,267	1,000	070711	1745		102	08101	0 0 7 1 4	447.0	1000	0000	0000	0100	0.013	701	0.0867	0.000	-0.0283		*	1	De la company	000	1014	0460	1.0806	1.1435	0.4945	-1.2989	-1.2622	-1.1892	-1.1614	1.1390	0268	-1.0087	87/60	570K.0-	2077.0	0.2570	0.1145	77.0	90.10	-0.1138	-0.1260	-0.0892	-0.0328	.0.0247
	ı	For	7. r	5 5	71.6	8 2	3.5	0.00	3 6	7 7	7.7	8 5	3 12	1 7	7 70	8 8	5	3 8	2 2	200	9	8 5	8 9	8 6	8 8	8 8	3.6	139.00			2	X/I	3.75	3.12	88	27	-0.62	000	0.62	1.25		2.50	3.12	3.75		8 5	8 5	3 5	8 8	40	9	900	20.00	80.00	90:00	122.00	139.00
ndα=0°	.06	ğ é	2 5	250	100	32.1	0.4601	1.4371	1,187.1	1 3377	1,357	77.77	1.1386	1001		0107	0.8355	0.747.0	0.0840	7900	0.000	0.00	1010	0.106	9000	1980	10000	6000	nd a = 0°	ě	2	3 6	0.9847	0.9946	10408	1.0728	0.7758	1.2839	-1.2549	1.1835	1.1494	1.0834	1.0027	0.9682	0.8709	0.8109	0.7332	0.0000	0.000	21.0	0.1280	9517	0.1195	0.0952	0.0380	0.0210	
mfr = 0.57 and $\alpha$ = 0°	.06 = <del>•</del>	Fore	N.	2.5	1 80			3 6				2 5							2000			9			8 8		130.00		mfr = 0.63 and α	**************************************	Porehody	X				1.25			1.25			3.12			8: :		30.51					0002					
Ē	,	<b>a</b> 6	<b>1</b> 8	91100	9000	10800	7000	0.623	23161	0090	2126	3814	7.70																Ī		÷	3 6	00100	0.0232	47101	0.0621	3.1113	1171.0	3.2390	1.2837	0.3399	0.4051															
		Afterbody	7VF			01.410						06.772																		2	Afterhody	X/1				216.70						283.30 (															
	<b>0</b> = <b>0</b>		֓֞֜֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓					21010				1 2081		1363	9011	, W.	9560	1000	5.494	61210	570	200	92010	01140	0.0828	0.0354	0.000			e •	2								-1.2507			1.1281	26	1.0282	19861	0.9240	0.6300	0.730.7	11200	9660	0 1205	0.1272	-0.1262	-0.0864	0.0299	-0.0132	
	,	rorebody	7 7	22	1 86	200							2 5									9			9		305				Foreh	XA. CP	3.75	-3.12	88											F 6											
	,	Arterbody	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	0000	0.0207	0000	0.000	0.153	200	3986	0.570	0 3500	2000																		Afterhody	d	-0.0213	0.0025	0.0228	0.0395	0.0865	0.1468	0.2182	0.2694	0.3303	0.4079															
	• = 180°	V V	7 7	183.30	20000	316.70	228.00	255.60	26.50	272.30	277.80	28.3 20	N.C.																	Φ = 180°	4	X7.	166.70	183.30	200.00	216.70	238.90	255.60	266.70	272.20	277.80	283.30															
		Forebody	֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	100	3 2	1667	8	0.2514	0903	4066	1.4436	1 3003	147	1 3377	1.000	1 2760	1 1674	0000	19060	0.066	41700	0.0358	0.0740	0.0848	1901 0	9000	0000	-0.0287		ě	Pode	CD.	1.0253	1.0425	1.0742	1.1070	1.164	0.3618	1.3404	-1.2783	-1.2102	1.1699	963	-1.0519	02001	0.909.0	07000	0.000	0100	-0.1236	308	0.1276	-0.1115	-0.1231	-0.0883	-0.0346	-0.0171
ô	í	5	7 6	2 5	7 6	8 2	3 0	8	90		2 2	. C	3 2	3.75	7 38	9	5	20 21	17.50	2000	9	9	8	900	900	8	12.0	139.00	ዾ		Pos	X	3.75	3.12	1.88	-1.25	-0.62	0.00	0.62	2	88	2.50	3.12	3.75	<b>4</b> . 4	8.5	2 5	3 5	900	40.00	20 00	000	00.00	80.00	90.00	122.00	139.00
nd α = -2.		g G	. 35 2	8	1 1084	1 1340	97770	14367	200	22.	764	1 2 2 8 1	1383	1003	1010	1000	0.8474	1877.0	0.1059	20,000	9000	1001 0	1711	0.1733	9900	0.0428	0000		= 0.57 and $\alpha$ = 2.0°	- 00 <sub>e</sub>	4	2	10548	1.0672	1.1063	1.1340	0.4261	1.4490	-1.3872	-1.3195	1.2726	-1.2410	1.1551	0061	00701	1060	0.6336	901	1000	-0.1034	-0.1168	-0.1138	-0.1233	-0960	-0.0387	-0.0294	
mfr = 0.67 and $\alpha$ = -2.0°	•	Forebody	7 7	2 5	7 6	2	3 6						. 4			0001	200		20.00		2003	9	200	80.00	8	122 00	30.00		r = 0.57 a	4	Porehody	X	-3.75	3.12	1.88												3 5	2 5	8 9	20.00	0000	0000	80.00	00:06	122.00	139,00	
ā		<b>a</b> 6	ָבָּי בָּבְּי	0.004	91000	00000	9000	1477	02160	0.2636	1227	0.3086	2000																Ħ		2	e C	0.0179	0.0183	0.0292	0.0479	0.0962	0.1519	0.2095	0.2508	0.2946	0.3487															
		Arterbody	_									281.00																		,	Afterhody	X.	_									283.30															
	e) = 0	<b>.</b> 6	_											25060	0.0517	0.8780	07.07.0	7104	0.6534	0.000	19110-	101	1261	80110	0.0891	00313	00.00	•		ے اا	Forehody	? B	_						_			-1.4236	3863	1.3002	1,07.1	67/17-	000	0.0740	0.2712	-0.0383	07500	0.0770	-0.0935	-0.0805	0.0335	-0.0193	
	•	rorebody	ַ כ	: :	: :	: -		֏	; <b>-</b>	: -	-	: -		: ē		; =		, c	, ,																																			~			

		ody	CP	0.0241	0.0354	0.0550	0.0740	0.1307	0.1971	0.2682	0.3204	0.3771	0.4428																
	.081	Afterb	X/L CP	166.70	183.30	200.00	216.70	238.90	255.60	266.70	272.20	277.80	283.30																
	• = 180°	body	G C											-0.5525	-0.2900	-0.3834	-0.3067	-0.2425	-0.2297	-0.2022	-0.1516	0.1441	-0.1348	-0.1218	-0.1016	-0.1036	0.0670	-0.0232	-0.0147
		Fore	ž	-3.75	-3.12	<b>88</b> .	-1.25	-0.62	0.00	0.62	1.25	88.	2.50	3.12	3.75	4.38	2.00	7.50	15.00	17.50	20.00	40.00	20.00	90.00	70.00	80.00	90.00	122.00	139.00
ndα=0°	.06	ody	G G	0.7485	0.7421	0.7890	0.7943	<u>1</u>	0.7411	0.6539	-0.5665	-0.5899	-0.3611	-0.3972	-0.2810	-0.2937	-0.2618	-0.1888	-0.1987	-0.1456	-0.1359	-0.1226	-0.1173	-0.1047	-0.1095	-0.0854	-0.0132	-0.0061	
mfr = 0.78 and $\alpha = 0^{\circ}$	n 👄	Fore	X/L CP	-3.75	-3.12	-1.88	-1.25	0.00	0.62	1.25	1.88	2.50	3.12	4.38	200	7.50	10.00	15.00	17.50	20.00	40.00	20.00	90.00	00:00	80.00	00.00	122.00	139.00	
E		χģχ	G C	0.0212	0.0367	0.0560	0.0814	0.1359	0.1990	0.2692	0.3137	0.3681	0.4309																
	0	Afterbo		166.70	183.30	200.00	216.70	238.90	255.60	266.70	272.20	277.80	283.30																
	°0 = �	body	5	0.7610	0.7803	0.8125	0.8106	0.9021	1.1829	-0.7015	-0.7681	-0.7011	-0.5741	-0.4071	-0.5211	-0.2684	-0.3119	-0.2484	-0.2376	-0.2011	-0.1545	-0.1230	-0.1218	-0.1126	-0.1088	-0.0792	-0.0180	-0.0020	
		Fore	χľ	-3.75	-3.12	-1.88	-1.25	-0.62	0.00	0.31	0.62	1.25	2.50	3.12	4.38	200	7.50	10.00	12.50	15.00	30.00	40.00	20.00	90.00	70.00	00:06	122.00	139.00	
		dy Afterbody	χζ	166.70	183.30	200.00	9531 216.70 0.0683	238.90	255.60	266.70	272.20	277.80	283.30	2003	7535	7859	7642	7320	1405	1216	1543	1533	1433	1345	1141	1200	.0827	.0245	.0207
	. 180°	Forebody Afterbody	χζ	166.70	183.30	200.00	216.70	238.90	255.60	266.70	272.20	277.80	283.30	3.12 -0.8607	3.75 -0.7535	4.38 -0.7859	5.00 -0.7642	7.50 -0.7320	15.00 -0.1405	17.50 -0.1216	20.00 -0.1543	40.00 -0.1533	50.00 -0.1433	60.00 -0.1345	70.00 -0.1141	80.00 -0.1200	90.00 -0.0827	22.00 -0.0245	39.00 -0.0207
if $r = 0.70$ and $\alpha = 0^\circ$	•	Forebody	CP X/L	-3.75 0.8857 166.70	-3.12 0.8924 183.30	-1.88 0.9360 200.00	-1.25 0.9531 216.70	-0.62 1.0268 238.90	0.00 0.9177 255.60	-1.0183 0.62 -1.0467 266.70	1.25 -0.9921 272.20	-0.9280 1.88 -1.0039 277.80	-0.8154 2.50 -0.9430 283.30	-0.8028 3.12 -0.8607	-0.7185	-0.6793	-0.5881	-0.1315		-0.1501	-0.1451	-0.1296	-0.1315	-0.1166	-0.1173	-0.0873	-0.0237	-0.0167	139.00 -0.0207
mfr = 0.70 and $\alpha$ = 0°	.06 = ♦	Forebody Forebody	XI CP XIL CP XIL	.3.75 0.8818 -3.75 0.8857 166.70	-3.12 0.8733 -3.12 0.8924 183.30	-1.88 0.9319 -1.88 0.9360 200.00	-1.25 0.9433 -1.25 0.9531 216.70	0.00 1.0700 -0.62 1.0268 238.90	0.62 -1.0389 0.00 0.9177 255.60	1.25 -1.0183 0.62 -1.0467 266.70	1.88 -0.9618 1.25 -0.9921 272.20	2.50 -0.9280 1.88 -1.0039 277.80	3.12 -0.8154 2.50 -0.9430 283.30	4.38 0.8028 3.12 -0.8607	-0.7185	-0.6793	-0.5881	-0.1315	-0.1833	-0.1501	-0.1451	-0.1296	-0.1315	-0.1166	-0.1173	-0.0873	-0.0237	-0.0167	139.00 -0.0207
	.06 = ♦	fterbody Forebody Forebody	L CP X/L CP X/L CP X/L	.70 0.0158 .3.75 0.8818 .3.75 0.8857 166.70	.30 0.0306 .3.12 0.8733 .3.12 0.8924 183.30	.00 0.0477 -1.88 0.9319 -1.88 0.9360 200.00	.70 0.0728 -1.25 0.9433 -1.25 0.9531 216.70	.90 0.1243 0.00 1.0700 -0.62 1.0268 238.90	.60 0.1887 0.62 -1.0389 0.00 0.9177 255.60	.70 0.2598 1.25 -1.0183 0.62 -1.0467 266.70	.20 0.3054 1.88 -0.9618 1.25 -0.9921 272.20	.80 0.3608 2.50 -0.9280 1.88 -1.0039 277.80	(30 0.4255 3.12 -0.8154 2.50 -0.9430 283.30	4.38 -0.8028 3.12 -0.8607	5.00 -0.7185	7.50 -0.6793	10.00 -0.5881	15.00 -0.1315	17.50 -0.1833	20.00 -0.1501	40.00 -0.1451	\$0.00 -0.1296	60.00 -0.1315	70.00 -0.1166	80.00 -0.1173	90.00 -0.0873	122.00 -0.0237	139.00 -0.0167	_
	.06 = ♦	fterbody Forebody Forebody	XI CP XIL CP XIL	.70 0.0158 .3.75 0.8818 .3.75 0.8857 166.70	.30 0.0306 .3.12 0.8733 .3.12 0.8924 183.30	.00 0.0477 -1.88 0.9319 -1.88 0.9360 200.00	.70 0.0728 -1.25 0.9433 -1.25 0.9531 216.70	.90 0.1243 0.00 1.0700 -0.62 1.0268 238.90	.60 0.1887 0.62 -1.0389 0.00 0.9177 255.60	.70 0.2598 1.25 -1.0183 0.62 -1.0467 266.70	.20 0.3054 1.88 -0.9618 1.25 -0.9921 272.20	.80 0.3608 2.50 -0.9280 1.88 -1.0039 277.80	(30 0.4255 3.12 -0.8154 2.50 -0.9430 283.30	4.38 -0.8028 3.12 -0.8607	5.00 -0.7185	7.50 -0.6793	10.00 -0.5881	15.00 -0.1315	17.50 -0.1833	20.00 -0.1501	40.00 -0.1451	\$0.00 -0.1296	60.00 -0.1315	70.00 -0.1166	80.00 -0.1173	90.00 -0.0873	122.00 -0.0237	139.00 -0.0167	_

TABLE V. Continued

(d) M = 0.89

		A 6	12100	0.0214	0.0395	0.0607	0.1094	07.70	0.2399	0.3457	0.4115																			od v	e e	00100	0.0284	0.0484	0.0715	0.1720	0 1883	70070	0.110	71150	0.3701	0.4333																
	180°	Afterbody		183.30																									000	Afterbody	//	2 2	181.30	20000	07.91.6	238.00	0755	366.30	373.30	07.717	06.712	783.30																
	<b>\( = 180^{\)}</b>	à à	103	1.0869	1.1259	1.1501	1.2004	0.0840	1 3008	1.2630	-1.2212	-1.1676	-1.1179	.1.1013	1.0595	-0.9517	-0.7989	-0.7284	-0.5825	101.6	00.00	0.000	900	7000	6.00	-0.0/31	-0.0237		• 180°	Apod	2	10134	10182	080	1024	8	07170	1026	9	8	1.120	0760	1.0354	2000	9560	0.8235	0.000	0.6341	1470.0	-0.5124	-0.0319	0.0826	-0.1026	-0.0989	-0.1173	-0.0812	-0.0254	-0.0100
		Forebody X/I.																									139.00			Fore	X.	,	3.15																								122.00	22.50
nd α = 0°	<b>.</b>	ğ d	980	10794	1.1190	1.150	0.4794	200	7677	1.2048	3	1.0599	1.0543	0.9657	0.9088	0.7869	0.7080	0.5778	0.0962	0.0342	0.0682	0.0807	0000	0.020	1000	0.020	<b>X</b>	ndα=0°	ů	odv	, <u>a</u>		10138	10,83	8	8922 0	306	2991	201	/717	0160	1900	0.9339	0.5401	707.0	-0.6742	96090	0.0670	0.3300	00.00	0.0730	66600	0.0993	0.1092	0.0881	0.0225	0.0161	
$mfr = 0.57 \text{ and } \alpha = 0^{\circ}$	•	Y. CP	27.	3.12										7.50						20.00						8777		mfr = 0.62 and α ≈ 0°	- 4	Forebody	X.	1 .			-1.25						2 5			3 5		15.00			3 6						90.06			
ā		a a	0074	0.0202	.0355	2650	92.5	97.7	0830	13391	404																	B		4	<u>۾</u>	72.00	10278	8990	0.0718	1245	1876	1961	300	500	190	0074																
	٠	ê																											2	Afterbo	XI.				216.70																							
	% = 0°	y od	7.0	1.0862					1.3684				1.0776	-1.0567	9026:0-	-0.9103	0.8482	-0.8039	-0.5845	-0.0853	-0.0312	0.0586	7700	0.0717	100	0.020	0.0140		ئ * *	ypoc	2												1970.1	0.0380	-0.8319	-0.7953	-0.7387	0.000	0.100	C.4131	-0.0333	-0.0793	0.1012	0.10	-0.0809	-0.0261	-0.0103	
		Korebody	27.5	-3.12	-1.88	-1.25	70.0		0.62			3.12									20.00		20.02		3 5					Fore	XA. CP		-3.12											5		10.00			8 6			50.00			00.06			
	- 180°	Afterbody X/I. CP	166.70 0.0353																										- 180	Afterbody	XII.	7	183.30 0.0135		216.70 0.0549						367 30 0.3340																	
	26 28		166.70	183.30		216.70		255.00		277.80	283.30		-1.2518	-1.2304	6961'1-	-1.1088	-0.9605	-0.8534	-0.7208	-0.2653	-0.0349	19000	0.030	-0.0%	0.0000	2000	-0.0203		A = 180°		XI.	02.991	183,30		216.70	238.90		07.84	04 444	07.717	06.11.50	763.30	0.0073	57(C)	-0.9026	-0.8163	25.00	0.5420	0.1808	0.0004	90600	0.1034	0.1150	-0.1058	-0.1207	0.0868	-0.0274	•
٠	26 28	Yorebody Afferbody	166.70	183.30	1.1492 200.00	1.1792 216.70	08367 1717.1	05552 +07770- 07 347 - CE891	-1,4200 272.20	.1.3710 277.80	-1.3240 283.30	-1.2773		4.38 -1.2304									3000 -0.0390				139.00 -0.0203	.1°	°081 ∺ <del>*</del>		CP XII.	07.991	1.0552 183.30	1.0874 200.00	216.70	1.1761 238.90	0.4118 255.60	OF AAC 7555 1.	04 444 0441 1	07.717 0711.1	01.114 /211.11	06.682 00.0.1	174 .00721					0000 0000			40.00 -0.0908			70.00 -0.1058			122.00 -0.0274	
nd α = -2.1°	<b>8</b> 1 = <b>♦</b>	Korebody XA. CP	6 -3.75 1.1008 196.70	-3.12 1.1157 183.30	1.1492 200.00	-1.25 1.1792 216.70	08367 17171	0.62 1.4433 344.30	-1,4200 272.20	1.88 -1.3710 277.80	2.50 -1.3240 283.30	3.12 -1.2773	3.75	4.38	2.00		15.00	17.50	20.00	40.00	20.00	90.00		8 9		200	139.00	and $\alpha = 2.1^{\circ}$		Forebody	XU. CP XVI.	07.761 10401 27.5	-3.12 1.0552 183.30	-1.88 1.0874 200.00	-1.25 1.1144 216.70	-0.62 1.1761 238.90	0.4118 255.60	OF AAC FCCC L. CAO	04 444 0441 1	07:717 07:111, 67:1	01.114 /211.11	06.682 0010.1: 06.2	3.12	36	200		15.00	5 2		9007	8 6	90.00	80.00	00.02		90.00	122.00	
r = 0.57 and α = .2.1°	<b>8</b> 1 = <b>♦</b>	Forebody X/I. CP	1.0706 -3.75 1.1008 166.70	-3.12 1.1157 183.30	1.1212 -1.88 1.1492 200.00	1.1525 -1.25 1.1792 216.70	0.5054 1.11.1 2.05- 7.55.90	1.3573 0.00 1.4433 344.30	1.25 -1.4200 272.20	-1.2007 1.88 -1.3710 277.80	-1.1441 2.50 -1.3240 283.30	-1.0720 3.12 -1.2773	-1.0324 3.75	-0.9646 4.38	-0.9011 5.00	-0.7836 7.50	-0.7166 15.00	-0.5678 17.50	-0.1023 20.00	-0.0520 40.00	-0.0763 50.00	00009 00000	0.00	0.0316 80.00	00.00	0.0322 30.00	00'661	= 0.57 and a	\$ 1800 € # ± 1800	Forebody	CP X/I CP X/I.	0,590 1 275 1 300 1	1.0784 -3.12 1.0552 183.30	1.1259 -1.88 1.0874 200.00	-1.25 1.1144 216.70	0.5006 -0.62 1.1761 238.90	0.00 0.4118 255.60	OF AAC	06 676 0671 1. 361	07:717 07:111, 67:1 66-7:1.	00:112 1:11:1 00:1	06.681 00.01: 06.2 \$161.1:	21.0	36	-0.8929 5.00	7.50	-0.6823 15.00	05.21	0000	00.02	-0.0364 40.00	00000 20000	0.0847 60.00	0.1020 70.00	0.0861 80.00	0.0292	0.0231 122.00	
mfr = 0.67 and $\alpha$ = -2.1°	281 = ♦	Forebody Forebody P X/I CP X/I CP I	3 -3.75 1.0706 -3.75 1.1008 166.70	-3.12 1.0792 -3.12 1.1157 183.30	1.1212 -1.88 1.1492 200.00	-1.25 1.1525 -1.25 1.1792 216.70	0.5054 1.11.1 2.05- 7.55.90	00.562 #022.0° 00.0 1/56.1° 20.0 00.586 66861 680	-1.2503 1.25 -1.4200 272.20	2.50 -1.2007 1.88 -1.3710 277.80	3,12 -1,1441 2,50 -1,3240 283,30	4.38 -1.0720 3.12 -1.2773	-1.0324 3.75	-0.9646 4.38	-0.9011 5.00	-0.7836 7.50	-0.7166 15.00	-0.5678 17.50	-0.1023 20.00	-0.0520 40.00	-0.0763 50.00	00009 00000	0.00	0.0316 80.00	00.00	0.0322 30.00	00'661	0.57 and a		Forebody Forebody	P X/I. CP X/I. CP X/I.	07 301 1040 1 37 F. A	-3.12 1.0784 -3.12 1.0552 183.30	-1.88 1.1259 -1.88 1.0874 200.00	1.25 1.1510 -1.25 1.1144 216.70	0.00 0.5006 -0.62 1.1761 238.90	1354 0.00 0.4118 255.60	05 AAC 5555 5 50 AVE 1. 251	06.676 0671 1. 361 3886 1.	07:717 07:11:1 60:1 C60:1 03:C	08:117 (511:1: 98:1 7841:1: 05:7 06:186 770:1 03:0 7131:1 51:5	00.001 00.001 00.2 PICI.1- 21.0	21.0	0.6677	-0.8929 5.00	0.7889 7.50	-0.6823 15.00	05.21	0000	00.02	-0.0364 40.00	00.00	0.0847 60.00	0.1020 70.00	0.0861 80.00	0.0292	0.0231 122.00	
•	81 = ♦ .06 = ♦	body Forebody Forebody CP X/I. CP 1	3.75 1.0706 -3.75 1.1008 166.70	0.0134 -3.12 1.0792 -3.12 1.1157 183.30	-1.88 1.1212 -1.88 1.1492 200.00	0.0558 -1.25 1.1525 -1.25 1.1792 216.70	0.302 1212.1 230.4 40.00 0.00	00.002 #033.0° 00.0 1/00.1° 40.0 00.00.0 00.00.0 00.00.0 00.00.0 00.00.	1.88 -1.2503 1.25 -1.4200 272.20	0.3469 2.50 -1.2007 1.88 -1.3710 277.80	3,12 -1,1441 2,50 -1,3240 283,30	4.38 -1.0720 3.12 -1.2773	-1.0324 3.75	-0.9646 4.38	-0.9011 5.00	-0.7836 7.50	-0.7166 15.00	-0.5678 17.50	-0.1023 20.00	-0.0520 40.00	-0.0763 50.00	00009 00000	0.00	0.0316 80.00	00.00	0.0322 30.00	00'661	= 0.57 and a	ED #	Afterbody Forebody Forebody	CP XA, CP XA, CP XA.	07.951 MAG 37.E. 83601 37.E.	0.0353 -3.12 1.0784 -3.12 1.0552 183.30	0.0453 -1.88 1.1259 -1.88 1.0874 200.00	0.0649 -1.25 1.1510 -1.25 1.1144 216.70	0.1135 0.00 0.5006 -0.62 1.1761 238.90	04 255 81140 000 A251 1. CAO 81710	07.33c 7.0c 1. 030 320c 1. 3c 1 13c 0	0,000 0	02.21.2 0211.1 02.1 CCP2.1 00.1 03.0 CCCC.0	08:117 (511:1: 98:1 7841:1: 05:7 06:186 770:1 03:0 7131:1 51:5	06.585 00.0.1: 06.2 FIGURE 28.5.0 0.000 00.1: 00.00 00.1: 00.00	21.0	0.6677	-0.8929 5.00	0.7889 7.50	-0.6823 15.00	05.21	0000	00.02	-0.0364 40.00	00.00	0.0847 60.00	0.1020 70.00	0.0861 80.00	0.0292	0.0231 122.00	
•	φ = 0°	body Forebody Forebody CP X/I. CP 1	2 166.70 -0.0153 -3.75 1,0706 -3.75 1,1008 166.70	183.30 0.0134 -3.12 1.0792 -3.12 1.1157 183.30	200.00 0.0296 -1.88 1.1212 -1.88 1.1492 200.00	216.70 0.0558 -1.25 1.1525 -1.25 1.1792 216.70	258.50 0.1045 0.00 0.3094 -0.62 1.2121 238.50	0.106.2 -0.25.00	272.20 0.2861 1.88 -1.2503 1.25 -1.4200 272.20	277.80 0.3469 2.50 -1.2007 1.88 -1.3710 277.80	283.30 0.4224 3.12 -1.1441 2.50 -1.3240 283.30	4.38 -1.0720 3.12 -1.2773	-1.0324 3.75	7.50 -0.9646 4.38	10:00 -0:9011 5:00	15.00 -0.7836 7.50	-0.7166 15.00	20.00 -0.5678 17.50	40.00 -0.1023 20.00	50.00 -0.0520 40.00	0000 -0.0763 50.00	00.00 00.00 00.00	0.00	00.08 8180 0- 00.00	00.00	0.00 0.001	00.221 102.03- 00.921	= 0.57 and a		Afterbody Forebody	YA, CP XA, CP XA, CP XA.	07.331 MARCH 27.E. 88801 27.E. 8810.0 07.831 FL	183.30 0.0353 -3.12 1.0784 -3.12 1.0552 183.30	200,00 0.0453 -1.88 1.1259 -1.88 1.0874 200,00	0.0649 -1.25 1.1510 -1.25 1.1144 216.70	238.90 0.1135 0.00 0.5006 -0.62 1.1761 238.90	255 60 01718 0.62 J. 1354 0.00 0.4118 255 60	OC 350	0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0	05-217 021111, C2:1 CCE2:1 00:1 00:12:0 05:217	00117	00,001 00,001 00,2 P10,11- 21,0 00,000 00,001	21.0	7.40 -0.9672 4.38	10.00 -0.8929 5.00	15.00 -0.7889 7.50	17.50 -0.6823 15.00	05 (1 5975 0 00 0 0	A000 0.004 30.00	00.01 +201.0- 00.04	00.05 P.00.05 O.05	00.00 01/0.0- 00.00	70.00 0.0847 60.00	80.00 -0.1020	0008 1980 0006	0.0292	139,00 -0.0231 122,00	

$mfr = 0.77 \text{ and } \alpha = .0.1^{\circ}$	\$1 = \$0.00 m m m m m m m m m m m m m m m m m m	Forebody Afterbody Forebody Afterbody X/I CP	0.8016 166.70 0.0222 .3.75 0.7825 .3.75 0.7979 166.70	0.7893 183.30 0.0410 -3.12 0.7887 -3.12 0.8084 183.30	0.8292 200.00 0.0601 -1.88 0.8187 -1.88 0.8324 200.00	0.9111 238.90 0.1496 0.00 1.2018 -0.62	1.1444 255.60 0.2157 0.62 -0.7188 0.00 1.1439 255.60	-0.7117 200.70 0.2877 1.25 -0.0000 0.02 -0.0913 200.70 -0.7833 272.20 0.3341 1.88 -0.6456 1.25 -0.6469 272.20	0.6814 277.80 0.3882 2.50 -0.6183 1.88 -0.6434 277.80	0.4540 3.12 -0.5572 2.50 -0.6167 283.30	-0.5101 4.38 -0.4776 3.12 -0.5107 5.00 -0.4312 3.75	-0.4527 7.50 -0.2725 4.38	-0.3984 10.00 -0.1951 5.00	0.2494 15.00 -0.2414 7.50	0.50 - 0.505 -	-0.1629 40.00 -0.1444 20.00	-0.1361 50.00 -0.1293 40.00	-0.1314 60.00 -0.1240 50.00	0.1274 70.00 -0.1145 60.00	00.07 - 0.11.25 - 0.00 - 0.11.29 - 0.00 - 0.0	-0.0143 122.00 -0.0165 90.00	0.0009 139.00 -0.0035 122.00	139.00																								
mfr = 0.71 and $\alpha$ = $0^\circ$	φ = 90° φ = 180	body Forebody Forebody	0.6 501 50.0 57 5. 10.0 57 5. 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50 10.0 07.50 51.50	183.30 0.0416 -3.12 0.9077 -3.12 0.9133 183.30	0.9500 200.00 0.0606 -1.88 0.9307 -1.88 0.9494 200.00	1.1079 -0.62	0.9626 255.60 0.2100 0.62 0.9626 0.00 0.8967 255.60	-0.9091 266.70 0.2818 1.25 -0.9325 0.62 -0.9768 266.70 1.75 -0.9091 266.70 1.75 -0.9778 277.70	-0.9426 277.80 0.3819 2.50 -0.8565 1.88 -0.8814 277.80	-0.8291 283.30 0.4443 3.12 -0.8212 2.50 -0.8676 283.30	0.7317 4.38 -0.6846 3.12	-0.756 5.00 -0.6402 4.38	-0.6543 10.00 -0.5767	-0.6106 15.00 -0.4929 7.50		-0.3032 -0.3034 -0.1245 -0.1041 -0.1041 -0.1041 -0.1041	-0.1218 50.00 -0.1311 40.00	-0.1310 60.00 -0.1342 50.00	0.1334 70.00 -0.1167 60.00	0.0211 70.00	-0.0187 122.00 -0.0227	-0.0079 122.00	00'661	$\mathbf{mir} = 0.96 \text{ and } \alpha = 0^\circ$	==	Afterbody Forebody Forebody	CP XI CP XII CP XII CP XII	0.0360 -3.75 0.0235 -3.75 0.1362 166.70	-0.1910 200.00 0.0701 -1.88 -0.3400 -1.88 -0.2229 200.00	0.1004 -1.25 -0.5191 -1.25 -0.3893 216.70	-0.7443 238.90 0.1541 0.00 0.9328 -0.62 -0.8213 238.90	1.25 0.3056	0.4290 272.20 0.3189 1.88 0.1997 1.25 0.2842 272.20	0.2123 277.80 0.3652 2.50 0.1590 1.88 0.2262 277.80	0.1541 283.30 0.4224 3.12 0.1350 2.32 0.1491	5.00 0.0573	0.0527 7.50 -0.0511 4.38	7.50 -0.0372 10.00 -0.0447 5.00 0.0497	-0.0840 17.50 -0.0922 15.00	-0.0764 20.00 -0.0892 17.50	-0.1096 40.00 -0.0908 20.00	-0.0849 50.00 -0.1001 40.00	0.0950 50.00	0.1003 80.00 -0.0884 70.00	-0.0548 90.00 -0.0659 80.00	-0.0060 122.00 -0.0034 90.00	0.0114 139.00

TABLE V. Continued

(e) M = 0.92

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	Afterbody	2 G		0.0641																					ş		0.0560		0.1655																	
- 1800	¥	X,	183.30	200.00	238.90	255.60	266.70	07.777	283.30	:														.081 = <b>\$</b>	¥ ;	166.70	183.30	200.00	238.90	255.60	266.70	277.80	283.30													
		<b>a</b> 8	1.0424	1.0818	1.1722	0.5343	1.1261	2 2 2	10322	0.9690	0.9128	0.8721	0.80%	-0.6706	-0.5844	0.5161	0.4189	0.0410	0.0515	0.0926	0.0639	0.0119		-	g g	0.8123	0.8180	0.8466	86160	1.1614	0.6301	0.5543	0.5863	0.5576	0.4104	0.4734	0.4835	0.3720	0.1806	0.1247	0.1496	0.1480	0.1434	-0.1200	0.1205	2013
	Forebody	χ.	3.12					2 2													8 22				Forebody		-3.12																	00.00		
)   		• <u>-</u>	<b></b>	<b>-</b> ₹	. 82	=	£ ;	ಕ ಕ														_	α = 0°			*	23	2 5	2 2	¥																
900	Forebody	ਰੂ ਹੁੰ		1.071								0.7756					5.0814			_	00003		77 and	06 ± ф	rebody	Ū		0.8270				0.5655								-0.1453				-0.1146	C.00.0	35.
906 = 40	¥	7 7	-3.12	1.88	0.0	0.62	1.25	2.50	3.12	4.38	5.00	1.50	15.00	17.50	20.00	40.00	8.00	20.07	80.00	00.00	139.00		$\mathbf{mfr} = 0.77 \text{ and } \alpha = 0^{\circ}$	Ĭ	e s	-3.75	-3.12	25.1.25	0.00	0.62	1.25	2.50	3.12	4.38	8 8	2 5	15.00	17.50	20.00	40.00	\$0.00	90.00	70.00	80.00	20.00	77.00
•	ģ	C 6	0.0377	0.0547	0.1446	0.2112	0.2829	0.3846	0.4493														•		<b>≱</b> €	0.0341	0.0529	0.07.0	1682	.2394	0.3131	4141	0.4767													
	Afterbody	2 K 2 8																							Afterbody		183.30																			
0 +	•		1.0418						1.0155 2		0.8811	20 EX	-0.7322	-0.6924	6287	0.4909	96.0	-0.0334	0642	3562	0.0010			°0 = +	_		0.8134							0.4306	577	310	<b>2</b>	-0.3832	-0.2678	536	352	382	316	0.1232	701	51100
	죭	3.75 2.75 2.75		1.88		000						7.50													Forebody			1.25		000				3.12 0.4		2.00										
		<b>×</b> 7	ψ.	7 7	9	0 (	2 6	· —	2	e .	4 4		2	12	25	3 2	3 8	8	0.0	8 5	139.00				<b>-</b> ≽	ļ 🛒	ų.	7 -	<b>ợ</b>	oʻ,	<b>=</b>	· -	2.	ю·	4.0	, L	<u>.</u>	12.50	15.	30.00	40.00	ŝ	90.00	0.05 0.09	22.	
°C.	Rerbo			216.70 0.0712		255.60 0.1919																		= 180°	Afferbody X/I. CP		183.30 0.0481						283.30 0.4756													
∞.			•																														~									<u> </u>	<u>s</u> :	27	. g	00100
¢ = 180°		_	9001		1.2143	0.0958	-1.2298	-1.1948	-1.1278	-1.0992	-1.0403	9686.0-	-0.9128	0.7441	0.6775	0.5/30	-0.4064	.0.0348	-0.0247	0.0454	0.010	-0.0081			90 <b>g</b>	0.9115	0.9306	0.9809	1.0654	0.9429	0.8445			-0.7276	0.0863	0.6548	-0.6356	-0.5102	-0.4287	0.2242	0.079	0	0.12	غ خ خ	00	•
90	rebody	_	1.1006	508					2.50 -1.1278																Y/I. CP	-3.75 0.9115	-3.12 0.9306	-1.25 0.9809	-0.62 1.0654	0.00 0.9429	1.25 -0.8445		0.8084	3.12 -0.7276		5.00 -0.6548							60.00 -0.1289	20.00 20.00 20.00	00:00	
•	Forebody	-3.75 1.0897	-3.12 1.1006	-1.25 1.1605	-0.62	0.00	1.25	<b>88</b>	2.50	3.12	3.75	5.00	7.50	15.00	17.50	9.07	20.00	00:09	70.00	800	122.00		1 a = 0°			3.75	-3.12	1.25	-0.62	000	1.25	1.88 -0.7731	2.50 -0.8084	3.12	5, 5 5, 5	\$.00	7.50	15.00	17.50	20.00	40.00	20.00	90.00	8.08	00:06	200
<b>♦</b> = 90° <b>♦</b> = 18	rebody Forebody	1.0847 -3.75 1.0897	1.0954 -3.12 1.1006	1.1622 -1.25 1.1605	0.5484 -0.62	-1.2859 0.00	-1.1762 1.25	-1.1347 1.88	-1.0813 2.50	1.0079 3.12	-0.9787 3.75	-0.8316 5.00	-0.7406 7.50	0.6761 15.00	0.5573 17.50	-0.3052 40.00	-0.0351 50.00	-0.0204 60.00	-0.0402 70.00	00:08	-0.0032 122.00		$0.71 \text{ and } \alpha = 0^{\circ}$		CP	0.9147 -3.75	0.9228 -3.12	0.9732 -1.25	1.0915 -0.62	00.00	-0.7880 1.25	-0.8041 1.88 -0.7731	-0.7476 2.50 -0.8084	0.6808 3.12	-0.0022	-0.5436 5.00	-0.4730 7.50	-0.4260 15.00	-0.1240 17.50	0.0632 20.00	-0.1110 40.00	-0.1228 50.00	-0.1145 60.00	0.1170 70.00	0006 0000	00000
•	rebody Forebody	1.0847 -3.75 1.0897	-3.12 1.1006	1.1622 -1.25 1.1605	0.5484 -0.62	-1.2859 0.00	-1.1762 1.25	-1.1347 1.88	-1.0813 2.50	1.0079 3.12	-0.9787 3.75	5.00	-0.7406 7.50	0.6761 15.00	0.5573 17.50	-0.3052 40.00	-0.0351 50.00	-0.0204 60.00	-0.0402 70.00	00:08	122.00		$\mathbf{mfr} = 0.71 \text{ and } \alpha = 0^{\circ}$		rorebody rorebody XI. CP XI. CP	0.9147 -3.75	-3.12	0.9732 -1.25	1.0915 -0.62	000	-0.7880 1.25	-0.8041 1.88 -0.7731	-0.7476 2.50 -0.8084	0.6808 3.12	-0.0022	-0.5436 5.00	-0.4730 7.50	-0.4260 15.00	-0.1240 17.50	0.0632 20.00	-0.1110 40.00	-0.1228 50.00	-0.1145 60.00	8.08	0006 0000	00000
<b>♦</b> •06 = <b>♦</b>	Forebody Forebody	-3.75 1.0847 -3.75 1.0897	1.0954 -3.12 1.1006	-1.25 1.1622 -1.25 1.1605	0.00 0.5484 -0.62	0.62 -1.2859 0.00	1.23 -1.2211 0.02	2.50 -1.1347 1.88	3.12 -1.0813 2.50	1.0079 3.12	-0.9787 3.75	-0.8316 5.00	-0.7406 7.50	0.6761 15.00	0.5573 17.50	-0.3052 40.00	-0.0351 50.00	-0.0204 60.00	-0.0402 70.00	00:08	-0.0032 122.00			06 = +	P XI, CP	-3.75 0.9147 -3.75	-3.12 0.9228 -3.12	-1.25 0.9732 -1.25	1.0915 -0.62	1.25 0.8401 0.00	1.88 -0.7880 1.25	2.50 -0.8041 1.88 -0.7731	3.12 -0.7476 2.50 -0.8084	0.6808 3.12	-0.0022	-0.5436 5.00	-0.4730 7.50	-0.4260 15.00	-0.1240 17.50	0.0632 20.00	-0.1110 40.00	-0.1228 50.00	-0.1145 60.00	0.1170 70.00	0006 0000	00000
• • • • • • • • • • • • • • • • • • •	body Forebody Forebody	-3.75 1.0847 -3.75 1.0897	0.0335 -3.12 1.0954 -3.12 1.1006	0.0746 -1.25 1.1622 -1.25 1.1605	0.1281 0.00 0.5484 -0.62	0.1910 0.62 -1.2859 0.00	0.3071 1.88 -1.1762 1.25	2.50 -1.1347 1.88	0.4272 3.12 -1.0813 2.50	1.0079 3.12	-0.9787 3.75	-0.8316 5.00	-0.7406 7.50	0.6761 15.00	0.5573 17.50	-0.3052 40.00	-0.0351 50.00	-0.0204 60.00	-0.0402 70.00	00:08	-0.0032 122.00			06 = ♦	CP X/I. CP	0.0301 -3.75 0.9147 -3.75	0.0472 -3.12 0.9228 -3.12	-1.25 0.9732 -1.25	0.1576 0.00 1.0915 -0.62	0.2279 0.62 -0.9094 0.00	0.3490 1.88 -0.7880 1.25	2.50 -0.8041 1.88 -0.7731	0.4665 3.12 -0.7476 2.50 -0.8084	0.6808 3.12	-0.0022	-0.5436 5.00	-0.4730 7.50	-0.4260 15.00	-0.1240 17.50	0.0632 20.00	-0.1110 40.00	-0.1228 50.00	-0.1145 60.00	0.1170 70.00	0006 0000	00000
<b>♦</b> = 0 <sub>0</sub> = <b>♦</b>	body Forebody Forebody	166.70 0.0189 -3.75 1.0847 -3.75 1.0897	0.0335 -3.12 1.0954 -3.12 1.1006	216.70 0.0746 -1.25 1.1622 -1.25 1.1605	238.90 0.1281 0.00 0.5484 0.62	255.60 0.1910 0.62 -1.2859 0.00	272.20 0.3071 1.88 -1.1762 1.25	277.80 0.3633 2.50 -1.1347 1.88	0.4272 3.12 -1.0813 2.50	4.38 -1.0079 3.12	5.00 -0.9787 3.75	10.00 -0.8316 5.00	15.00 -0.7406 7.50	17.50 -0.6761 15.00	20.00 -0.5573 17.50	-0.3052 40.00	60.00 -0.0351 50.00	70.00 +020.0 -0.000	80.00 -0.0402 70.00	00:08	139.00 -0.0032 122.00			06 пф 0 пф	CP X/I. CP	166.70 0.0301 -3.75 0.9147 -3.75	0.0472 -3.12 0.9228 -3.12	216.70 0.0946 -1.25 0.9732 -1.25	238.90 0.1576 0.00 1.0915 -0.62	0.2279 0.62 -0.9094 0.00	272.20 0.3490 1.88 -0.7880 1.25	277.80 0.4035 2.50 -0.8041 1.88 -0.7731	283.30 0.4665 3.12 -0.7476 2.50 -0.8084	0.6808 3.12	7.50 -0.0022 3.73	10:00 -0:5436 5:00	15.00 -0.4730 7.50	17.50 -0.4260 15.00	20.00 -0.1240 17.50	40.00 -0.0632 20.00	50.00 -0.1110 40.00	60.00 -0.1228 50.00	70.00 -0.1145 60.00	0.1170 70.00	122.00 -0.0130 90.00	0000 00001

TABLE V. Concluded

(e) Concluded mfr = 0.96 and  $\alpha = 0^{\circ}$ 

	•	.0.		٠	8		•	.081	
Por	Forebody	After	pody	Fore	pody	Pon	ebody	After	pody
χ	G	P X/L CP	පි	ž	X/L CP	×	XIL CP	CP X/L CP	පි
-3.75	0.1537	166.70	0.0465	-3.75	0.1226	-3.75	0.1251	166.70	0.0525
-3.12	0.1621	183.30	0.0632	-3.12	0.0472	-3.12	0.1304	183.30	0.0663
-1.88	-0.2652	200:00	0.0824	-1.88	-0.5843	-1.88	-0.1657	200.00	0.0894
-1.25	-0.4062	216.70	0.1135	-1.25	-0.6922	-1.25	-0.5397	216.70	0.1129
-0.62	-0.7739	238.90	0.1725	00.00	0.9918	-0.62	-0.8487	238.90	0.1689
0.00	1.1245	255.60	0.2355	0.62	0.4270	0.00	1.1260	255.60	0.2346
0.31	0.5952	266.70	0.2994	1.25	0.3112	0.62	0.4886	266.70	0.3025
0.62	0.4180	272.20	0.3411	1.88	0.1971	1.25	0.2947	272.20	0.3463
1.25	0.3193	277.80	0.3886	2.50	0.1198	1.88	0.2420	277.80	0.3959
2.50	0.1434	283.30	0.4455	3.12	0.1649	2.50	0.1713	283.30	0.4531
3.12	0.1711			4.38	0.1099	3.12	0.1864		
4.38	0.1003			2.00	0.0846	3.75	0.1239		
5.00	0.0615			7.50	-0.0107	4.38	0.1031		
7.50	-0.0258			10.00	-0.0462	200	0.1068		
10.00	-0.0393			15.00	1650.0	7.50	0.0212		
12.50	-0.0882			17.50	-0.1092	15.00	-0.1001		
15.00	-0.0579			20.00	-0.1017	17.50	-0.1297		
30.00	0.1140			40.00	-0.1129	20.00	-0.1135		
40.00	-0.0984			20.00	-0.1107	40.00	-0.1122		
50.00	-0.1161			90.00	-0.1102	20.00	-0.1213		
90.00	0.13			20.00	-0.0989	90.00	-0.1122		
70.00	-0.0996			80.00	-0.1011	70.00	-0.0923		
90.00	-0.0660			90.00	1770.0-	80.00	-0.1070		
122.00	0.0020			122.00	-0.0030	90.00	-0.0643		
39,00	0.0196			139.00	0.0122	122.00	0.0001		
						139.00	0.0062		

FABLEVI. PRESSURE COEFFICIENTS ON MODEL WITH NACA 1-85-43.9 INLET AND CONTRACTIONRATIO OF 1.250

Afterbody VL CP 1.16 - 0.038 13 - 0.035 1 - 0.032 1 - 0.0213 0.0177 0.0348 0.0544 X/L 343.16 384.14 419.13 457.12 595.77 545.76 571.08 583.74 596.41 
 Korebody

 XIL
 CP

 ANL
 CP

 -1874
 0.991

 -2557
 0.8441

 -205
 0.8441

 -205
 0.04691

 0.00
 0.4691

 0.01
 2.0920

 0.03
 2.103

 1.25
 2.0807

 1.88
 2.103

 2.0
 1.858

 4.3
 1.728

 5.0
 1.728

 6.2
 1.738

 6.2
 1.738

 6.2
 1.339

 100
 1.1419

 11.50
 6.6947

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 0.6941

 17.50
 0.4011

 600
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 900
 0.3404

 10000
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 44185
 0.0724
 mfr = 0.40 and  $\alpha = 0^{\circ}$ Afterbody
Afterbody
AL CP
116 0.00433
13 0.00400
2 0.00346
7 0.00240
0.0033
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0.0033 XAL 3943.16 394.14 419.13 457.12 595.77 545.76 583.74 596.41 
 Korebody

 X/L
 CP

 LBA4
 OP909

 -171.29
 0.9936

 -171.29
 0.9937

 -170.34
 0.9783

 -160.34
 0.9713

 -180.34
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 -38.31
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 -2.1421

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 0.5225

 0.57
 -1.2732

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 0.9284

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 0.0000

 0.04
 0.0328

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 1. Afterbody
X/L CP
343.16 -0.0358
344.14 -0.0358
384.14 -0.0358
897.77 -0.0468
597.77 -0.0468
587.78 -0.0468
583.74 -0.0136
596.07 -0.0258 
 Forebody
 A

 XI
 CP
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 XII
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 XII

 -1874
 10318
 343

 -18657
 1,0136
 344

 -1567
 0.9613
 419

 -1027
 1,0138
 343

 -1028
 0.9607
 547

 -1021
 0.0738
 545

 0.01
 0.7238
 545

 0.12
 1,1443
 571

 0.23
 1,1989
 58

 1.23
 1,1302
 43

 4.3
 1,1302
 43

 4.3
 1,1369
 58

 5.0
 1,2364
 43

 100
 1,1245
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 1,1286
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 <tr (a) M = 0.60mfr = 0.31 and  $\alpha = 0^{\circ}$ Afterbody
X/I. CP
343.16 -0.0530
384.14 -0.0523
384.14 -0.0497
457.12 -0.0465
545.76 -0.0417
571.08 -0.0311
571.08 -0.0311
571.08 -0.0311
571.08 -0.0311
571.08 -0.0311 
 Korebody

 XL
 CP

 XL
 CP

 183.11
 10342

 152.31
 10312

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 41.83
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 1.18362

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 0.3882

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 1.2654

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 1.15362

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 1.6547

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 1.4561

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 0.4245

 241.85
 Afterbody
71. CP
71. CP
71. CP
71. 4. 6.00541
71. 0.00573
72. 0.0057
73. 0.0057
74. 0.0057
75. 0.0058
76. 0.0059
77. 0.0059
78. 0.0059
79. 0.0059
79. 0.0059
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79. 0.0059
79. 0.0059
79. 0.0059
79. 0.0059
79. 0.0059 XGE 343.16 384.14 419.13 457.12 507.77 545.76 571.08 583.74 596.41 Forebody A

X/L CP X/I

-18.74 1.0403 34.1

-106.57 1.10243 384.4

-25.67 0.9507 419.4

-10.7 1.0866 457

-2.07 1.0866 457

-2.07 0.9293 547

-2.08 1.11541 591

-2.09 1.11541 591

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-2.1 mfr = 0.28 and α = 0° Afterbody
X/L CP
344.16 -0.0010
344.14 -0.0594
419.13 -0.0537
457.12 -0.0537
547.76 -0.0536
571.08 -0.0451
588.74 -0.0455
596.41 -0.0455 
 Korebody

 XL
 CP

 AZL
 CP

 187.4
 L036

 -10.53.11
 1.0377

 -10.54
 1.0294

 -10.29
 1.0129

 -90.39
 1.0120

 -8.80
 0.984

 -4.18
 0.984

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 1.007

 -5.13
 1.007

 -6.13
 1.021

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 1.020

 -6.24
 0.228

 -6.35
 1.986

 -7.17
 1.020

 -7.20
 1.034

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 1.034

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 1.034

 -7.20
 1.041

 -7.20
 1.020<

TABLE VI. Continued

(a) Continued

		vodv	Ç	-0.0379	0.0257	0.0240	-0.0054	0.0132	\$ 50 00 00 00 00 00 00 00 00 00 00 00 00 0	0.1228	0.1948																																	
	<u>چ</u>	Afterbody	χ		419.13			545.76	583.74	596.41	609.07																																	
	φ = 180°	· •	Ç.	0.9269	0.6215		1.0830	0.1435	16107	-1.5612	-1.3269	-1.1872	0.8666	-0.7526	0.7064	-0.6615	-0.6694	.6159	-0.6025	0.5990	0.5655	0.7238	0.4105	0.3583	0.3413	-0.3278	-0.3084	-0.2814	-0.2268	0.1728	/6Cm													
α = 2.0°		Forehody	χΓ		-106.57 U				15.0				3.13									200								90.01														
$\mathbf{mfr} = 0.50 \text{ and } \alpha = 2.0^{\circ}$								<b>*</b> 9	2. 3	: 3	92											•					_	-	_	- (	•													
mfr = 0		Afterbody	S		0.0304				0.0329																																			
	°0 •		χĽ		419.13				583.74						_		_									_	_		_				_		۰		_		•	٠.	_			_
	•	Forebody	C	0.9361	0.9324	0.9147	0.8824	0.8490	0.7744	0.7322	0.7183	0.7119	0.7183	0.8934	1.0479	1.0855	1.0719	0.9185	0.7128	7.4617	2.0331	2 2004					-1.7828	-1.5846	-1.4457	1.1442	1000	-0.8716	-0.7730	-0.7146	0.6596	-0.4859	-0.4413	-0.4182	-0.3912	0.3560	0.3560	-0.2061	-0.0677	-0.0579
		Por	×	-187.47	-155.11	-130.84	-106.57	90.39	-78.03	41.85	-33.76	-25.67	-23.11	-10.27	-5.13	3.34	-2.05	96.0	4.0	90.0	0.31	0.03	2 8	2.50	3.13	3.75	4.37	5.00	6.25	7.50	10.00	12.50	15.00	17.50	20.02	40.00	90.00	90.00	70.00	80.00	20.00	1000	241.85	279.84
		ş	G.	0.0370	-0.0397	-0.0269	.0082	0.0088	0.0462	0.1155	0.1844																																	
		Afterbody	χŢ		384.14 -0 419.13 -0				583.74 0		0 09:01																																	
	. 18∩°	) · >			0.6496 41						_	98	161	0.8089	272	-0.7046	713	-0.6848	-0.6789	3 5	0.0460	477	0.4195	-0.3706	-0.3794	241	-0.3436	-0.2783	-0.2447	0.1689	ì													
e 1.0°		Forebody	C					0.00 -0.0138	063 -1.3160				3.13 -1.0191								13:00																							
0 and a		-	7	-187.47	-100.57	-10.27	-2.05	o c	jc	· <del>-</del>	_	7	mi m	í <del>v</del>	,	ý	7	œ	9	2 :	2 2	÷ 5	3 8	S	8	2	28	8	100.00	10.00	147													
$\mathbf{mfr} = 0.50 \text{ and } \alpha = 1.0^{\circ}$		Afterbody	Ç	-0.0445	0.0381	-0.0328	-0.0173	0.0008	0.0230	0.0856	0.1395																																	
	یو		χΓ	343.16	419.13	457.12	507.77	545.76	583.74	596.41	609.07																																	
	•	Forebody	Ĉ	0.9350	0.9376	0.9141	0.8843	0.8504	0.7714	0.7228	0.7014	0.6826	0.6997	0.8693	1.0217	1.0797	1.0847	0.9525	0.7710	0.3040	3,3500	2,1075	-2.2385	-2.0751	2.0231	-1.5316	.1.3892	-1.3981	1.0891	0.8778	0.8491	-0.7780	-0.7256	0.0666	\$ C C C	0.4774	-0.4278	0.4144	-0.3883	0.3576	0.3232	0.2061	0.0459	-0.0335
		Pore	X	-187.47	-155.11	130.84	106.57	90.39	-58.03	41.85	-33.76	-25.67	-23.11	-10.27	-5.13	3.34	-2.05	90.00	4.0	300	150	20.0	88	2.50	3.13	3.75	4.37	5.00	6.25	7.50	10.01	12.50	15.00	17.50	30.05	40.00	90.00	00:00	00.07	80.08	8.00	10.00	241.85	279.84
		>	. و	222	-0.0168	-0.0147	045	0.0227	0.032	66	0.1707																																	
		Afterbody	XI. CP																																									
	A = 180°	1	^		58 419.13		_	81 545.76				8 :	<u>-</u> 8	. 26	2	93	16	5	5 :	≏ :	2 5	3 6	3 89	. 20	*	9	8	58	22	92 :	5													
8	•	Forehody	CP		7 0.6658				3 -2.2251				3 -1.6317					5 -0.7815			0.0903									0.1956	_													
mfr = 0.50 and α ≈ 0°		Š.	ž	-187.47	-100.57	-10.27	-2.05	0.00	0.51	1.25	1.88	2.50	3.13	4.37	2.00	6.25	7.50	8.75	10.00	12.50	15.00	00.00	30.05	2000	00:09	70.00	80.00	90.06	100.00	10.00	741.0													
nfr = 0.5		Afterbody	ದಿ	-0.0307	0.0222	-0.0147	-0.0035	0.0189	0.0419	0.0980	0.1734																																	
-	9		ž	343.16	419.13	457.12	507.77	545.76	581.74	596.41	609.07																																	
	() -C	•	ට්	0.9328	0.9370	0.9129	0.8773	0.8443	0.7580	0.7077	0.6870	0.6640	0.6711	0.8391	1.0039	1.0713	1.0855	0.9928	0.8172	79170	0.101.	2 1503	2.0709	-1.8876	1.5740	-1.1662	-1.0762	-0.9462	-0.9031	0.8207	787.0	0.7579	0.7129	-0.6569	0.5992	0.4453	-0.4271	-0.4038	-0.3518	0.3544	6,516	0.237	0.0675	-0.0595
		Forebody	χ	-187.47	155.11			90.39	-78.03	41.85	-33.76	-25.67	-23.11		-5.13	-3.34	-2.05	-0.90			0.31			2.50						2.50					20.00		20.00	00:09	70.00	80.00	8.8	11000	241.85	279.84
							-																																					

TABLE VI. Continued

(a) Continued

		Š	<u></u>	-0.0253	0.0253	-0.0130	0.0089	0.0367	0.0772	0.1109	0.1120	0014																																	
mfr = 0.63 and α = 0°	2	Afterbody	χ		384.14			545.76	871.08	583.74	500 US																																		
	- 180	ě .	දී	_	0.7461					1.1270			-0.8704	-0.7079	-0.6757	-0.6243	5558	-0.6207	8	0.5984	0.3830	0.4705	-0.4682	-0.4004	-0.3509	-0.3498	-0.3274	-0.3150	-0.2797	-0.2237	0.1724														
		Porehody	XL					_		1.00										0001									_	_															
			×	-187.47	-25.67	-10.27	-5	0	0 (	-	_	. 7			4	•	•		**	2 2	2 2		20	æ	S	8	5	8	8	00.00	74185														
		Afterbody	Ç	-0.0258	0.0210	0.0061	0.0190	0.0479	0.0895	0.1203	0.743																																		
	٤		χľ	343.16	419.14	457.12	507.77	545.76	\$71.08	506.41	609.07																																		
	4		ಕ	0.8382	0.8335	0.8016	0.7451	0.6891	0.6225	0.3419	0.4068	0.3479	0.3402	0.3803	0.5629	0.7975	0.9335	1.0521	1080	1.0151	0.8027	1.3959	1.1759	-1.0301	0.9533	-0.8388	-0.7561	-0.7048	0.6473	0.6190	0.001	0.6038	0.5750	-0.5422	0.4814	0.4483	-0.3753	-0.3573	-0.3482	-0.3362	-0.3111	-0.2799	0.2201	0.0544	0.0470
		Forebody	ΧĽ	-187.47	-171.29				-74.21											\$ 8						3.13				6.23						20.02					80.00			110.00	
				Ţ.																																								- (	4 74
$\mathbf{mfr} = 0.66 \text{ and } \alpha = 0^{\circ}$		Afterbody	ට්	-0.0286	-0.0280	-0.0143	0.0033	0.0241	0.0593	0 1397	0.2048																																		
	<b>*</b> = 180°	Afte	χľ	343.16	419.13	457.12	77.70	245.76	571.08	506.41	609.07																																		
		ody	S.	0.8939	0.5370	0.7263	1.0874	0.1232	661.1	16478	1.6297	1.3250	-0.9981	0.8583	0.8313	0.795	2607.0	0.73%	0.7011	0.6807	0.5996	-0.5673	-0.5109	-0.4397	-0.3780	-0.3586	-0.3427	-0.3227	-0.2957	0.2263	0.0583														
		Forebody	χΓ	-187.47	-25.67	-10.27	-2.05	0.00	0.31		1.88					90.5			5 5											0000															
						249	32	<u>\$</u>	¥ 2	t = 1	215																																		
		Afterbody		16 -0.0393					28 0.0534 24 0.0534																																				
	% #		×	943.16	, •	•			50.178		_	<b>.</b>	_	<b>.</b>	<b>.</b>	<b>.</b> ~						~	•	•	_	<b>.</b>		~ .		• •		•	_				_	_	_	_		_			
		Forebody		0.8926					0.7307						0.7363	1 0363	000	.0869	300	0.011	-1.3078	-1.9612	-1.7168			-1.0005	0.916			0.7167	-0.7261	-0.6906	-0.6651	0.6438	7/860	0.4614	-0.4117	-0.3893	-0.3667	0.3498	-0.3297	-0.2938	0.2341	0.00	-0.0546
		Fo	Χď	-187.47	-155.11	-130.84	106.57	80.5	-74.21	41.85	-33.76	-25.67	-23.11	-17.97	77:01-			20.7-	77	000	0.31	0.63	1.25	.88	2.50	3.13	3.75	4.37	2.00	2.50	8.75	10.00	12.50	2.00	20.00	30.00	40.00	20.00	90.00	20.00	80.00	800	8 9	241.85	279.84
		Ą	G	-0.0342	-0.0181	-0.0175	6000	0020	0.0380	0.1263	0.1994																																		
mfr = 0.50 and $\alpha$ = 3.0°		er.		343.16 -0				245.76																																					
	081 = 0			0.9275 34 0.8717 38							_	-0.9096	<b>3</b>	5 36	0.6333	34.5	0 6680	, <u>5</u>	: 2	510	22	ž	727	£	S :	<b>8</b>	= :	i i	2 2	3 3	185														
		퉏						_	0.63 - 1.3011						4.37 -0.0333														27/7:0	_															
			2	-187.47	-25.67	-10.27	4	<b>5</b> 6	9 0		-	7	m i	ró.	•	ni vo	•	~ o	9 5	12	15	17.50	20.00	30.06	80.05	<b>S</b> 8	20.00	80.8	8 8	10.00	241.85														
		Afterbody	c <sub>P</sub>	0.0422	0.0401	-0.0277	0.0052	0.0104	0.0368	0.0796	0.1258																																		
	క		ž	343.16	419.13	457.12	507.77	25.70	581.74	596.41	609.07																																		
	e0 = <b>♦</b>		CP CP	0.9353	0.9322	0.9143	0.8822	0.8301	0.7785	0.7438	0.7366	0.7165	0.7449	0.7/09	407470	1.0895	020	0.8788	5,0990	0.6260	-2.1944	-2.3558	-2.1336	-2.2865	-2.1043	-2.0749	-2.0326	1.8510	1,8430	-1.4659	-1.3849	1.1859	#O#O:-	1906.7	-0.80%	-0.5750	-0.4955	-0.4577	-0.4247	-0.3895	0.3575	0.3203	-0.2077	-0.0672	0.0560
		Forebody		-187.47	-155.11	-130.84	-106.57	-50.50 - 1.50 - 1.50						17.97		7												. 6.37						932							00.00				_
					•	•	•																																			-	_	~ ~	.4

TABLE VI. Continued

(a) Continued

			2	æ :	3 2	27	<b>#</b> 5	6 6	77	<u></u>																													
		f		-0.0108		0.0327		0.1491																															
	<b>081 = 0</b>		343.16	384.14	457.12	507.77	8.3.2	583.74	596.41	609.07																													
2	**	Forebody	0.7121	0.5655	0.0695	0.8400	0.7993	-0.3652	-0.4571	0.4471	-0.3689	-0.3387	0.3025	0.3185	-0.3105	-0.3634	0.3727	0.3891	-0.3645	0.3340	0.3181	0.3094	0.2947	0.2806	0.1968	-0.1482	\$1\$0.0 P.0\$18												
nd a = (		Fore	.187.47	.106.57	-10.27	-2.05	8 6	0.63	1.25	2.50	3.13	3.75	4.37	6.25	7.50	8.75	2 00 00	15.00	17.50	20.00	800	00:09	20.00	80.00	100.00	110.00	241.83												
mfr = 0.75 and α = 0°		<b>₽</b> ;	_	0.0082	0.0163	0.0444	0.0795	0.1577	0.2007	0.2645																													
Ē		Ę.		384.14 -0.1			571.08			609.07 0.																													
	را <sub>ي</sub> ۱۱ 💠	•		0.7168 38			0.4750 34			-0.0232 60 -0.1369	-0.1640	-0.1433	0.0788	0.6382	0.8541	1.0486	0.7929	-0.0901	986	-0.4058	618	98	9	397	324	288	086	808	\$69	-0.3777	205	-0.3271	017	0.3007	0.2804	-0.2580	0.1949	0.0434	342
		존							41.85 0.0				-10.27 0.0				4.0 4.0 5.0				2.50			5.00		_	5.75			17.50 -0.3			_	80.00		_	00:00		279.84 -0.0342
		_,	J87.47	171.29	130.84	5	-74.21	. <b>8</b> 5	7	£ 2	-23	-13	۹,	, 4,	-7	φ,	9 0		0		7	6	<b>.</b>	4 4	. •		<b>*</b> 5	2 2	2	2 2	3 8	4	S	88	₹ 8	8	20 :	241	279
		ody G	-0.0267	-0.0213	-0.0079	0.0172	0.0461	0.1236	0.1692	0.2451																													
	6	Afterbody	343.16	384.14	457.12	507.77	571.08	583.74	596.41	609.07																													
	= 180°	dy 5	0.7721	0.6523	0.2151	0.8572	0.0994	-0.3245	-0.4245	-0.4353 -0.3891	-0.3580	-0.2994	0.3115	0.2905	0.3112	0.3363	0.3242	0.3319	-0.3089	0.3047	0.2882	-0.2947	0.2776	-0.2475	-0.2003	0.1478	-0.0 <del>4</del> 04												
mfr = 0.69 and $\alpha = 2.0^{\circ}$		Forebody		-106.57			3.6			7 7 7 8 8 7 8							200			9000				00:06	_		. 62.142												
0.69 and		<b>.</b>			81	0.0348	0.1140	0.1487	879	457																													
mfr =		Afterbody		14 -0.0117						07 0.2457																													
	.0 = <b>0</b>	<b>&lt;</b> 5		384.14	-		571.08			609.07					_			_	_						_				_					<b>.</b>					
	Ĭ	Porebody	0.7766	0.7786	0.7330	0.664	0.5430	0.4147	0.3057	0.2659	0.1921	0.2181	0.4387	0.8600	0.9943	1.0525	0.3393	-0.8438	1.3211	-1.2652	0.9569	-0.9132	0.7804	0.7652	-0.6583	0.6431	0.0703	0.6079	-0.6359	0.5288	424	-0.4378	0.3846	0.3982	-0.3598	-0.2856	-0.2533	-0.0874	-0.0806
		-										_			0			•	•									•	7	7 7	Υ .	٣	•			_	88	3 22	279.84
		S.	187.47	-171.29	-130.84	106.57	-74.21	-58.03	41.83	-33.76			-10.27				\$ 6			1.25	2.50		3.75	, 3 8 8 8 8	6.25	7.50				17.50					80.00	90.00	100.00	241.85	23
		,			•	•															2.50		3.75		6.25										80.00	20:06	00 :	241.	27
		erbody	-0.0176	0.0197	-0.0047	0.0215	0.0875	0.1234	0.1675	0.2377											2.50		3.75		6.25										80.00	20:06	001	241.	27
	• = 180°	Afterbody	343.16 -0.0176	384.14 -0.0197	457.12 -0.0047	507.77 0.0215	571.08 0.0875	583.74 0.1234	596.41 0.1675	609.07 0.2377	-23.11	16.71.	10.27	3.6°	-2.05	0.00	4 <del>4</del> .0	0.31	690	1.25		3.13		5.00		7.50	10.00								80.00	30'06	1001	241.	27
α = 0°	• = 180°	rebody Afterbody	0.7715 343.16 -0.0176	0.6591 384.14 -0.0197	0.3426 457.12 -0.0047	0.9763 507.77 0.0215	-0.3644 \$71.08 0.0875	-0.8543 583.74 0.1234	-0.8258 596.41 0.1675	-0.7321 609.07 0.2377 -0.6602	-0.5930	-0.5224	-0.5335 -10.27	-0.4683	-0.4910 -2.05	-0.4999	-0.4679	-0.4443 0.31	-0.4200	0.3981 1.25	-0.3325	-0.3319 3.13	-0.3159	-0.2698 5.00	-0.2083	7.50	6.73								80.00	30'06	001	241.	27
.69 and α = 0°	• = 180°	Afterbody	-187.47 0.7715 343.16 -0.0176	-106.57 0.6591 384.14 -0.0197	10.27 0.3426 457.12 -0.0047	2.05 0.9763 507.77 0.0215	0.00 0.004 545.76 0.0473 0.31 -0.3644 571.08 0.0875	0.63 -0.8543 583.74 0.1234	1.25 -0.8258 596.41 0.1675	609.07 0.2377	-0.5930	-0.5224	10.27	-0.4683	-0.4910 -2.05	-0.4999	-0.4679	0.31	-0.4200	0.3981 1.25	-0.3325	-0.3319 3.13	-0.3159	5.00	-0.2083	7.50	6.73								80.00	30'06	001	241.	77
mfr = 0.69 and $\alpha$ = 0°	φ = 180°	Forebody Afterbody	-0.0235 -187.47 0.7715 343.16 -0.0176	-0.0165 -106.57 0.6591 384.14 -0.0197	0.0081 .10.27 0.3426 457.12 .0.0047	0.0312 -2.05 0.9763 507.77 0.0215	0.1111 0.31 -0.3644 571.08 0.0875	0.1427 0.63 -0.8543 583.74 0.1234	0.1889 1.25 -0.8258 596.41 0.1675	0.2522 1.88 -0.7321 609.07 0.2377 2.50 -0.6602	-0.5930	-0.5224	-0.5335 -10.27	-0.4683	-0.4910 -2.05	-0.4999	-0.4679	-0.4443 0.31	-0.4200	0.3981 1.25	-0.3325	-0.3319 3.13	-0.3159	-0.2698 5.00	-0.2083	7.50	6.73								00'08	20'06	001	241.	27
mfr = 0.69 and $\alpha$ = 0°		Afterbody Forebody Afterbody	-0.0235 -187.47 0.7115 343.16 -0.0176	-106.57 0.6591 384.14 -0.0197	0.0081 -10.27 0.3426 457.12 -0.0047	0.0312 -2.05 0.9763 507.77 0.0215	0.00 0.004 545.76 0.0473 0.31 -0.3644 571.08 0.0875	0.1427 0.63 -0.8543 583.74 0.1234	0.1889 1.25 -0.8258 596.41 0.1675	1.88 -0.7321 609.07 0.2377 2.50 -0.6602	-0.5930	-0.5224	-0.5335 -10.27	-0.4683	-0.4910 -2.05	-0.4999	-0.4679	-0.4443 0.31	-0.4200	0.3981 1.25	-0.3325	-0.3319 3.13	-0.3159	-0.2698 5.00	-0.2083	7.50	6.73								80.00	20'06	001	241,	27
$\mathbf{mfr} = 0.69 \text{ and } \alpha = 0^{\circ}$	Φ = 0° Φ = 180°	Afterbody Forebody Afterbody	343.16 -0.0235 -187.47 0.7715 343.16 -0.0176	-0.0165 -106.57 0.6591 384.14 -0.0197	457.12 0.0081 -10.27 0.3426 457.12 -0.0047	507.77 0.0312 -2.05 0.9763 507.77 0.0215	0.1111 0.31 -0.3644 571.08 0.0875	583.74 0.1427 0.63 -0.8543 583.74 0.1234	596.41 0.1889 1.25 -0.8258 596.41 0.1675	0.2522 1.88 -0.7321 609.07 0.2377 2.50 -0.6602	3.13 -0.5930 -23.11	3.75 -0.5224	-0.5335 -10.27	6.25 -0.4683 -3.34	7.50 -0.4910 -2.05	8.75 -0.4999 -0.90	-0.4679	15.00 -0.4443 0.31	17.50 -0.4200 0.63	0.3981 1.25	50,00 -0,3325	60.00 -0.3319 3.13	70.00 -0.3159	-0.2698 5.00	100.00 -0.2083	110.00 -0.1621 7.50	6.73	12.50	15.00		3000	40.00	80.00				-0.2081		-0.0411
mfr = 0.69 and $\alpha$ = 0.		rebody Afterbody Forebody	0.7769 343.16 -0.0235 -187.47 0.7715 343.16 -0.0176	384.14 -0.0165 -106.57 0.6591 384.14 -0.0197	0.7280 457.12 0.0081 -10.27 0.3426 457.12 -0.0047	0.6580 507.77 0.0312 -2.05 0.9763 507.77 0.0215	0.5036 571.08 0.1111 0.31 0.3644 571.08 0.0875	0.3932 583.74 0.1427 0.63 -0.8543 583.74 0.1234	0.2744 596.41 0.1889 1.25 -0.8258 596.41 0.1675	609.07 0.2522 1.88 -0.7321 609.07 0.2377 2.50 -0.6602	0.0952 3.13 -0.5930 -23.11	0.1332 3.75 -0.5224 -17.97	4.37 -0.5335 -10.27	0.8156 6.25 -0.4683 -3.34	0.9626 7.50 -0.4910 -2.05	1.0812 8.75 -0.4999 -0.90	12.50 - 0.4946 0.00	0.4199 15.00 -0.4443 0.31	-0.8051 17.50 -0.4200 0.63	0.8146 20.00 -0.3981 1.25	50,00 -0,3325	-0.5797 60.00 -0.3319 3.13	-0.5529 70.00 -0.3159	90.00 -0.2698 5.00	-0.4882 100.00 -0.2083	-0.4625 110.00 -0.1621 7.50	-0.4972 241.83 -0.0088 6.73	0.4609	0.4602	17.50	-0.3603	40.00	-0.3322	00'09	-0.2981	-0.2686		-0.0461	

TABLE VI. Continued

(a) Concluded

		_	. a.	723	S :	2 2	9	7.	149	111	187	128																																					
		Afterbody	S			3 0.0162																																											
	. 180°	₹ }	×	343.16	384.14	419.13	507.77	545.76	\$71.08	583.74	596.41	609.07																																					
ይ	-8	Forebody	Ç	0.3544	0.0998	11861-	0.2085	1.0807	0.7355	0.4665	0.2830	0.2351	0.1701	0.1372	0.1105	0.0603	0.0530	0.0281	-0.0255	-0.0481	-0.0882	-0.1271	-0.1720	-0.1472	-0.1850	-0.2022	-0.2482	-0.2471	-0.2482	-0.2376	-0.2140	0.1644	-0.1242	0.0264															
nd a = (		For	ž	-187.47	-106.57	10.27	2.05	000	0.31	0.63	1.25	88.T	2.50	3.13	3.75	4.37	2.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	20.00	00:09	00.00	80.00	90.00	00:00	10.00	241.85															
mfr = 0.93 and α = 0°		γþα	ಕ್ಕಿ	-0.0015	0.0050	0.0135	69500	0.0901	0.1302	0.1571	0.1919	0.2412																																					
Ħ		Afterbody	XL			457.12					596.41																																						
	0 = <b>0</b>	·				0.2448 4		_					-1.9629	-1.8752	-1.5723	-0.9781	-0.3823	-0.0989	0.2779	0.7175	0.9164	1.0814	0.6862	0.4820	2448	0.1986	1745	0.0653	1120	38	464	0.0027	¥77	0.1148	-0.1274	070	5 2	78	0.2014	-0.2285	-0.2376	-0.2415	-0.2512	-0.2378	0.2203	0.1603	0.1248	0.0270	1
		Forebody				130.84													-2.05 0.			0.00						3.13 0.0							10.00												10.00		
				<b>≈</b>	÷ :	÷÷	9.	ġ,		÷	4	÷	.5	-5	7	<del>-</del>	•	•	•	•	•																	- ~	e en	4	•	•	<b>Γ</b>	<b>æ</b>	<b>5</b> .	5	= 7	7 .	ì
		Afterbody	S	-0.0123	-0.0086	0.0149	0.0416	0.0752	0.1200	0.1575	0.2002	0.2696																																					
	.08		χſΓ	343.16	4. 5	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																					
٠.	<b>*</b> = 180°	body	ŝ	0.6261	0.4459	0.4142	0.4971	1.0459	0.5896	0.3060	0.1443	0.0613	0.0582	0.0477	0.0511	0.0254	-0.0066	-0.0005	-0.0891	-0.1031	-0.1091	0.1656	-0.1833	-0.1780	-0.1686	0.1963	-0.2381	-0.2475	-0.2446	-0.2404	-0.2216	0.1721	0.1262	0.0308															
dα=2.0		Forebody	Ķ	-187.47	-106.57	10.27	-2.05	000	0.31	0.63	1.25	1.88	2.50	3.13											20:00						90.00	00:001	110.00	241.85															
$mfr = 0.82$ and $\alpha = 2.0^{\circ}$		φ		_	0.0021	0.0240	0.0522	0923	0.1376	8691.0	0.2104	0.2680																																					
mfr		Afterbody			384.14							609.07 0.																																					
	0) = <b>(</b>		×										×	~	2	=	22	æ	23	S	œ	9	52	2	æ	œ	92	<u>0</u>	7	æ	1	× :	æ :	<b>.</b>	n =	: 5		9	ي و	<u></u>	92	y	90	<b>~</b> :	٤,	2 ¥	2 5	- 9	,
		Forebody			0.6333																						-0.4066			-0.4296					0.4181										0.200	0.1993	0.040	9800	
		F	χ	-187.47	(7.17)	130.84	106.57	.90.39	-74.21	-58.03	41.85	-33.76	-25.67	23.11	.17.97	-10.27	-5.13	ξ. Σ.	-2.05	<b>6</b> 9	<b>4</b> .	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	S. 3	6.25	7.50	8.73	10.00	20.51	17.50	20.00	30.00	40.00	20.00	90.09	20.00	80.00	800	0001	241.85	270.84	
		χģχ	G G	-0.0063	0.004	0.0114	10431	.0785	1240	.1590	.2068	.2684																																					
		Afterbody		343.16				545.76 0.			596.41 0.	0.609																																					
	<b>0</b> 81 = <b>0</b>	d,		0.6306						_	_	_	0.1690	18	0.1690	1620	2205	201	2365	2650	2566	2992	-0.3016	2933	2761	-0.2708	-0.2933	-0.2862	-0.2797	0.2614	0.2389	0.1832	0.1406	-0.0.39 <b>y</b>															
α = 0°		der		187.47 0																						9 9 9				_	_	_		41.85 .0.															
mfr = 0.82 and $\alpha = 0^\circ$										3	13	=									_	_	_	_	~	•	•	•	_	<b>x</b> c +	σ ;	2 :	= ?	77															
af.		Afterbody		6 -0.0138						0.164		172.0 7																																					
	• = 0 <sub>•</sub>	₹		343.16								1 609.07	_			_	_	•	~	~-	_	_	_	_	_	_	_		_	_		_							_		_								
		Forebody		0.6306					0.2111	0.0250	-0.1933	-0.3111	0.4833	0.5324	-0.4963	0.2140	<u>2</u>	0.4179	0.6782	0.9552	0.070	0.0	0.2190	0.0760	0.135	0.1954	0.161	0.191	0.1433	-0.175	0.219	0.209	0.2311	01870	0.3016	0.3215	0.2648	-0.2905	-0.2810	-0.2868	-0.2889	0.278	-0.2791	0.2669	2.0	0 1407	0.0415	9100	
		For	×	-187.47	67.17.	130.84	-106.57	-90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	17.97	-10.27	-5.13	¥.	-2.05	06.0	4.	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	2.00	6.25		6/.6	12.50	15.00	17.50	20.00	30.00	40.00	20.00	90.00	00.00	00.00	8.6	0001	241.85	270.84	:

TABLE VI. Continued

(b) M = 0.64

		Ņ	G C	-0.0384	-0.0337	-0.0351	-0.0257	-0.0119	0.0155	0.0430	0.0653	0.1230																																						
		ą.	Z X																																															
	<b>•</b> = 180°				•							0 609.07	_	oc -	<u>.</u>	7 .	0	4	_	6	•	4	9	<b>50</b>	•	_	6	4	6	4	9	•	7	8																
.0	•	Forebody		0.9772																						-0.5641								-0.0805																
and a		Fo	X	-187.47	-25.67	-10.27	-2.05	00'0	0.31	0.63	1.25	1.88	2.30	3.13	5.75	15.4	200	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20:00	30.00	\$0.00	90.09	70.00	80.00	90.00	100	110.00	241.85																
mfr = 0.40 and $\alpha$ = 0°		ody	CP CP	-0.0384	-0.0351	-0.0294	-0.0181	-0.0081	0.0203	0.0397	0.0534	0.1126																																						
E	ዿ	Afterbody	X.		419.13	457.12	507.77	545.76	80.178	583.74	296.41	609.07																																						
	<b>⊕</b> = 0		<u>ئ</u> و	2710.1	6600.1	0.9964	0.9783	0.9565	0.9361	0.9059	0.8827	0.8753	0.8003	0.8785	0.000	666	1.0962	1.1067	1.0710	0.8824	0.6719	-0.4912	-1.9067	-2.1579	2.0734	-2.0220	-2.1130	-1.9343	-1.9436	-1.7910	-1.7667	-1.6009	-1.5309	-1.3829	-1.3148	-1.0427	-0.9244	-0.8335	-0.8227	-0.5460	-0.4985	-0.4532	-0.4256	-0.3807	-0.3729	0.3366	0.2731	-0.2062	-0.0860	
		Forebody	֓֞֞֞֝֟֝֟֝֟֝֟֝֟֝֟֞֟֝֟֟֝֟֟֟ ֓֞֓֞֓֞֓֞֓֞֓֞֞֓֓֞֞֓֓֞֞֓֓֞֞֓֓֞֞֓֓֞												16:1				-502						1.25	1.88			3.75																				279.84	
													•	-		•																																- ,		
		Afterbody	CP	-0.0523	-0.0461	0.0490	-0.0437	-0.0395	-0.0262	-0.0091	-0.0024	0.0456																																						
	180°	Afr	X,	384.14	419.13	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																						
٠.	= 180°	Forebody	CP.	1.0324	0.9842	1.0754	0.9784	-0.6322	-1.7982	1.8164	-1.4740	-1.3291	*	1.3324	1.2141	6907.1-	-1.4719	-1.2578	-1.2857	1.4943	-1.3146	-1.3478	-1.2252	-1.2536	-1.2294	-0.9853	-0.4920	-0.4223	-0.3835	-0.3164	-0.2938	-0.2508	-0.2183	-0.0762																
mfr = 0.30 and $\alpha = 0$ °		Fore	Z :	-106.57	-25.67	-10.27	-2.05	0.00	0.31	0.63	1.25	1.88	OC 7	3.13	C .	4.3/	200	6.25	7.50	8.75	0.00	12.50	15.00	17.50	20.00	30.00	20.00	00:00	00.00	80.00	00:06	100.00	110.00	241.85																
■ 0.30 ₽		dy.	a 5	0.0532	-0.0547	0.0499	-0.0433	-0.0466	0.0404	0.0195	-0.0238	0.0085																																						
n F		ter d	, K									006.01																																						
	• = 0 •								_				<b>X</b> :	Ŧ :	7 2	9 ;	<b>.</b>	-1	<b>2</b>	88	₹ Ş	53	88	758	128	174	192	17.	113	159	80	182	£	187	83	<u>€</u>	<b>9</b> 2	8	<b>2</b>	<u>2</u>	<u>8</u>	214	9	8 1 8	8	92	532	197	3 2	1
		ě	2 S		1.0502										70107													13 -1.4271	75 -1.4613			25 -1.4482																_	5 -0.0812	
		<u> </u>	×	-171.29	-155.11	-130.84	-106.57	.90.39	-74.21	-58.03	41.85	-33.76	10:57-	-23.11	/6/1-	2	2	4.6.	-2.05	96.O	<b>4</b> 0	00:0	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	8.00	6.25	7.50	8.75	10:00	12.50	15.00	17.50	20:00	30.00	90.0	20.00	90.09	900	80.08	00.06	00:001	110.00	241.85	
		ody	<u>د</u> و	0.0558	-0.0534	-0.0558	-0.0477	.0.0591	-0.0458	-0.0340	1620.0	0.0049																																						
	٠	Afterbody	֓֞֞֞֝֞֞֞֞֝֞֞֞֝֟֞֝֟֞֝֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞									20.609																																						
	<b>*</b> 180°	dy.	و										601.1	1.0681	/0C0:1-	2000	1.1220	-1.1322	-1.0827	-1.1273	-1.0648	-1.1078	1498	-1.3340	-1.1346	.1.1420	-0.7799	-0.6461	-0.4427	<u>¥</u>	-0.3030	-0.2345	-0.2047	-0.0837																
l α = 0°		ě	XI																			12.50				30.00			70.00				_	41.85 -0																
mfr = 0.27 and $\alpha$ = 0°								£	œ	=	2	2													•			•	•	_	•	=	-	ż																
F.		er b	<b>6</b>									7 -0.0132																																						
	.0 <b>=</b> 0	7	¥ 5								_	.009							_	~.	_	_	~	۰,	_	<u>.</u>	_	_	_	<u>.</u>	~	_	_	-	•	_	~	_	~	_	<b>~</b>	×	_	_	_	_				
	•	Forebody	<b>a</b> 8		_	_		_																					1.7623			-1.6194																	-0.0925	
		For	Z Š	-171.29	-155.11	-130.84	106.57	-90.39	-74.21	-58.03	41.85	-33.76	10.62-	-23.11	1671-	/701-	51.5	-3.34	-2.05	0 <del>.</del> 0	-0. 4	0.00	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	\$.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	40.00	20.00	00.09	70.00	80:00	0006	00001	0001	241.85	

TABLE VI. Continued

(b) Continued

				٥	2 1	t t		=	2	0	9.	۰																																		
		Afterbody	පි	-0.0179	-0.0189	0.00	0.0243	0.056	0.100	0.1410	0.188	0.2576																																		
	.08		χ̈	343.16	384.14	457.12	507.77	\$45.76	\$71.08	583.74	596.41	609.07																																		
e	<b>•</b> = 180°	Forebody	G	0.8618	0.7750	0.6080	1.0734	0.4057	-0.6392	-1.2343	-1.363S	-1.3110	-1.1414	-0.8919	-0.7285	0.6810	0.6707	8/700	0.6523	0000	0.030	0755 0	0.5047	-0.4921	-0.4100	-0.3765	-0.3566	-0.3435	-0.3247	-0.2980	0.2263	0.1739	0.0430													
nd a = 0		Fore	X/L	-187.47	-106.57	-10.27	-2.05	0.00	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37			2.5				17.50				00:09	0.00	80.00	00:06	000	110.00	9													
mfr = 0.62 and $\alpha$ = 0°		ş	ę.	-0.0236	0.0163	0.0058	0.0309	0.0646	0.1101	0.1429	0.1875	0.2586																																		
8		Afterbody			384.14							609.07 0																																		
	0 = <b>+</b>				0.8677							-	0.3898	0.3819	0.4160	0.6063	0.8379	0.5037	1.0740	920	0.2986	7435	-1.3891	960	717	138	90	1678	0.7014	7257	0.0318	505	-0.6309	192	-0.5856	-0.5026	950	0.4189	0.3967	0.3/84	0.3487	-0.3192	-0.2896	-0.2254	-0.1757	-0.0501
		Porebody			20 17.75	_								-23.11 0.			5.13		607		000						3.13 -0.5					875 C				17.50 -0.5		30.00				_				241.85 -0.0 279.84 -0.0
				<b>.</b>	7	: <del>:</del>	OI.	ð,	Ŀ		4	d.			<del>,</del> .	<del>-</del>	•		• •		_								•				=	<u> </u>		-	≈ :	<b>ल</b> ₹	7 3	* 3	5 F	* **	8	<u>8</u>	Ξ	27.2
		Afterbody	ŝ	-0.0256	0.0273	-0.0175	0.0010	0.0281	0.0703	0.1059	0.1487	0.2189																																		
	<b>•</b> = 180°	Afte	χ	343.16	41013	457.12	507.77	545.76	\$71.08	583.74	596.4	609.07																																		
ం	•	Forebody	g G	0.9124	0.5681	0.7467	1.1026	0.1310	-1.0979	-1.6909	1.8099	-1.6645	-1.7351	1.6042	0440	0.8230	20,0	25.0	0.730	1367 0	0.7034	0.6629	-0.5963	-0.5659	-0.4574	-0.4066	-0.3851	0.362	0.3442	0.3029		0.053														
and a =		For	X	-187.47	-25.67	-10.27	-2.05	0.00	0.31	0.63	1.25	88.	2.50	3.13	3.73	15.	30.0	3 5	2, 2	9	12.50	15.00	17.50	20.00	30.00	20.00	90.00	00.00	80.00	8.00	8 8	241.85														
mfr = 0.55 and $\alpha$ = $0^\circ$		ody	වු	0.0308	0.0180	-0.0080	0.0162	0.0451	0.0869	0.1192	0.1591	0.2284																																		
£		Afterbody		343.16				545.76	571.08	583.74	596.41	609.07																																		
	.0 = <b>+</b>	yþo	<b>a</b>	0.9171	0.9138	0.8882	0.8468	0.8030					1000	0.500	0.3869	0.7337	1.0486	7	9020	9480	0.1335	-1.1479	-1.6908	-1.8649	7484	-1.6015	-1.4188	0.9222	0.8871	0.0179	0.7323	-0.7701	-0.7215	-0.7065	-0.6475	0.6033	0.3480	0.4027	1004	3820	-0.3673	-0.3424	-0.3026	0.2380	0.1890	0.0531
		Forebody		187.47											7671-														75.4							17.50 -0					_	_	Ė			241.85 -0 279.84 -0
						•	•																																						- '	* ~
		Afterbody				-0.0247			0.0466		٠,	0.1915																																		
	= 180°	¥		384 14							280.4	609.07																																		
ی		Forebody		0.800								21861															0.4026		0.3491	0.510	A 1986	0.0662														
) and α		چ ا	ž ;	106.57	-25.67	-10.27	-2.05	0.00	0.31	0.63	27	88.1	2.30	5.1.5	4 27	5 8	6.25	2.50	8.75	10.00	12.50	15.00	17.50	20:00	30.00	800	900	90.00	90.00	100	8001	241.85														
mfr = 0.50 and $\alpha$ = 0°		body	C.	0.0389	-0.0256	-0.0204	0.0014	0.0209	0.0609	0.0846	0.1222	4.67.0																																		
-	ب س و	Afterbody	¥ ;	384 14	419.13	457.12	207.77	545.76	571.08	583.74	4.08	0.60																																		
	•	yody	a 5	0.9524	0.9482	0.9329	0.8970	0.8649	0.8267	0.779	0.7303	0.7112	0.0070	0.0720	0.8596	100	1084	1.1042	1.0162	0.8621	-0.1270	.1 4899	-1.9780	2.1340	1.9467	856.	96.5	0.00	1,3630	ACO. 0	0.7794	0.8206	0.7705	-0.7382	0.7010	0.0189	92050	0.4557	0.4242	0.4029	-0.3779	-0.3534	0.3161	0.2532	0.1909	0.0601
	,	Forebody	X X			-130.84		_				35.70	23.11	17.07			100	-2.05									5.13									00.00			20.00					800	_	279.84
				. '	•	•	•																																					-	,	

TABLE VI. Continued

(b) Concluded

		ody	C C	0000	0.0121	0.0250	0.0582	0.0987	0.1495	0.1914	0.2346	0.3037																																						
		Afterbody	X	184 14	419,13	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																						
	= 180°	¥	CP				0.7021	_	_		_		-0.2129	-0.2030	1840	-0.2079	2134	1861	2480	2641	22.2	3000	3173	2821	2942	2821	5885	3010	-0.2926	-0.2826	2585	-0.1893	-0.1457	-0.0362																
°0 = x		ě				Ť								3.13				6.25 -0.														_																		
an fr = 0.81 and α = 0°		_	X	106.57	-25.67	-10.27	-2.05	Ó	Ó	Ö			7	<b>с</b> і	ei	4	٧i	۰	7	œ	9	12.50	2.	17.50	20	8	80	9	70.00	80	8	100.00	110.00	241.85																
fr = 0.8		ody	<u>د</u> و	0000	0.0116	0.0278	0.0601	0.1020	0.1519	0.1861	0.2285	0.2937																																						
Ħ	•	Afterbody	XI.	384 14	419.13	457.12	507.77	545.76	80.178	583.74	596.41	609.07																																						
	0 = <b>+</b>	ģ	CP CP	0,000	0.6437	0.5863	0.4852	0.3687	0.2391	0.0424	-0.1837	0.3105	0.4967	-0.5424	-0.4999	1751	1884	4703	7115	0686	740	0.9197	.2936	.0550	.0811	1767	182	2116	266	1855	2225	-0.2312	2545	-0.2671	.3281	3193	3258	3002	.2944	2946	-0.2955	.2988	-0.2894	.2937	-0.2779	2484	-0.1903	.1431	-0.0362	-0.0252
		룓	X					_			41.85 -0																		3.75 -0				7.50 -0		0.00			17.50 -0		30.00		_	_			90.06			241.85 -0	
			~	62 121	155.11	÷	ē	Š.	ř.	Ϋ́	4	ri i	i,	-7	<del>`</del>	÷	70	•	•	7	7	•	•	_						•					=	-	-	_	Ñ	æ	4	er,	Z.	~	æ	Φ.	2	Ē	74	27
		ody	C.	0000	0.0000	0.0135	0.0486	0.0880	0.1416	0.1815	0.2256	0.2973																																						
		Afterbody	XL									609.07																																						
	<b>\$= 180</b> °		CP		•			_	_				0.4359	-0.4482	-0.3674	-0.3845	674	631	-0.3653	116	189	218	857	<u>2</u>	354	203	276	250	-0.3150	-0.2878	684	-0.2041	0.1580	-0.0384																
% = 0°		훋			•			_											_												_		_																	
mfr = 0.75 and $\alpha$ = 0°		_	XL	75 901	-25.67	-10.27	7	ō	0	o	_		7	•	6	4	S	•	7	•	2	12	21		20	æ	S	8	2	8	8	100.00	011	241.85																
ofr = 0.		Afterbody	C.	0.000	0.0079	0.0240	0.0548	0.0951	0.1459	0.1838	0.2294	0.2954																																						
-		After	XIL	384 14	419.13	457.12	507.77	545.76	\$71.08	583.74	596.41	2009																																						
	<b>0=</b>	ą,	CP.	0.7417	0.7296	0.6830	0.6002	0.5096	0.4040	0.2613	0.0965	0.0010	0.1339	0.1449	-0.1192	0.0854	0.4784	0.6669	.8564	1.0662	1.1074	0.8310	00063	-0.3675	-0.4043	3936	3945	3968	-0.3596	3187	0.4080	-0.3420	3415	3954	3880	3838	-0.4169	-0.3754	0.3647	-0.3410	3334	0.3280	-0.3197	0.3119	0.2961	-0.2634	2005	0.1569	-0.0389	-0.0263
		휻	XL			_										-10.27 (		-3.34				000													10:00			17.50			40.00					90:06			241.85 4	
			=	-		÷	÷	Ψ.	•	7,	7	•		٠,٠	•	•																											_				-	-	7	7
		body	C C	0.0131	0.0045	0.0116	0.0397	0.0744	0.1243	0.1667	0.2090	0.2842																																						
		Afterbody	ZZ.	384 14	419.13	457.12	507.77	545.76	\$71.08	583.74	596.41	609.07																																						
	<b>+</b> = 180°	dy	C.P.	0.6906	0.1727	0.4073	9966	0.5695	-0.3735	-0.8610	-0.8643	-0.7978	0.7600	-0.6259	-0.5902	-0.5526	-0.4747	-0.5130	.5036	.5400	.4763	-0.5067	.4905	-0.4585	-0.4349	3761	-0.3604	3388	0.3273	0.3084	-0.2733	-0.2124	0.1610	-0.0517																
l α = 0°		Ē	XIT					_																									10.00																	
mfr = 0.68 and $\alpha = 0^{\circ}$						•		2	0	9	90	•													•		••	•	•	_	•	=	_	7																
- La		Afterbody	d C								0.2118																																							
	°0 = 0	4	X	384 14	419.13	457.12	507.77	545.76	\$71.08	\$83.74	596.41	609.07																																						
		<u>~</u>	CP CP	0.8046	0.7976	0.7603	0.6922	0.6195	0.5402	0.4274	0.3090	0.2504	0.1607	0.1428	0.1727	0.3690	0.6575	0.8276	0.9713	1.0737	1.0633	0.6060	0.4558	-0.7969	-0.8714	-0.7482	-0.6269	-0.6106	-0.5542	0.5570	0.5719	-0.5225	0.4735	-0.5672	-0.5188	0.5020	-0.5097	0.4684	0.4519	-0.3622	-0.3902	0.344	-0.3688	-0.3220	-0.3324	-0.2759	0.2405	0.1594	-0.0786	-0.0676
		ğ		-	•	0	0	0	_	Ψ.	_	_	_																		•																			
		퉏	XL					_								-10.27	-5.13	-3.34	-2.05	060	ó. 4	0.00	0.31	0.63	1.25	88.1	2.50	3.13								12.50	15.00	17.50	20.00	30.00	40.00	20.00	00:09	70.00	80.00			_	241.85	279.84

TABLE VI. Continued

(c) M = 0.69

Martin   M			φ	g.	-0.0348	-0.0408	0.0344	-0.0203	-0.0065	0.0239	0.0543	0.0864	0.1417																																				
### Color   Co																																																	
Mathematical Continue   Math		• = 180°			_								-	375	ğ	498	474	555	335	246	762	2	230	707	<u>6</u>	832	25	537	315	87.0	£ .	<b>3</b>	23	<u> </u>															
Market   M	, a 0°		orebod						•																																								
### Colin and e = 0	o pue o		-	Ş	-187	2.5	10	-2.0	õ	Ö	ò		-	7	e,	'n.	*	<u> </u>	9	~	ϗ	Ē	12	. <u>.</u>	7.	20.	Š	S.	Š	10.	<u>.</u>	8	00	110.5															
### Control Co	mfr = 0.		rbody	Ç	0.0468	000	-0.0314	-0.0198	-0.0018	0.0243	0.0466	0.0761	0.1310																																				
### 187   ### 18		8	Afte	XVL	343.16	419.13	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																				
### Particle   19   19   19   19   19   19   19   1		*	Apox	CP	1.0305	1 0292	020	0.9973	0.9784	0.9583	0.9289	0.9087	0.8952	868	0.830	0.9264	0202	1203	1302	9880	0.9195	0.7231	0.3383	1.6581	-2.0216	-5.1799	-2.2014	-2.1486	-2.1377	-2.0469	-2.0676	06667	1,7724	1,605.1	207	1.3761	-0.8866	0.7383	-0.5318	0.4917	-0.4725	0.4525	0.4209	0.4050	0.3614	0.3324	0.2563	0.2119	0.0579
### 100 mt			Fore	X	-187.47	-155.11	130.84	-106.57	-90.39	.74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	10.27	5.13	<b>1</b>	-2.05																										_	_		
### 100 mt			_	۵.	<b>2</b> 5	9 9	9	182	178	8	36	182	56																																				
### Color of the			Rerbody																																														
### Color of the c		= 180°	*											<b>.</b>	۰.	φ,	۰.	<u> </u>	7	<u> </u>	_	•	•	~	<b>5</b>	_	•		~	•	•																		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	٠,	•	ş																														777	0.075															
## Fig. 1.028 and $\alpha = 0^{\circ}$ Afterbody Atlantody Forebody Atlantody Forebody Atlantody Atlant	) and α		2	X	187.47	-25.67	-10.27	-2.05	0.00	0.31	0.63	1.25	1.88	2.50	3.13	3.75	15.4	805	70	S	8.75	000	12.50	15.00	17.50	20.00	90.00	800	900	20.00	80.00	8 8	0000	241.85															
## Fig. 1.028 and $\alpha = 0^{\circ}$ Afterbody Atlantody Forebody Atlantody Forebody Atlantody Atlant	nfr = 0.3(		body	පි	0.0542	0.0529	-0.0516	-0.0405	0.044	-0.0273	-0.0205	0.0003	0.0280																																				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-	°	After	ž	343.16	419.13	457.12	207.77	545.76	\$71.08	583.74	596.41	609.07																																				
## 0.28 and \$\alpha = 0.9\$  ## 10.7  ##		•	ody	G.	91.071	1.0727	1.0640	1.0523	1.0439	1.0326	1.0172	1.0059	1.0043	0000	5210.1	1.0311	6	1.1245	2	1.0141	0.7887	0.5307	0.6095	1.5482	1.5503	2020	1.4361	96	1.5037	1.5163	1.5389	2/04:1	1.3230	14407	4168	1.4122	1.3642	1.2849	1.2471	1.0318	0.7920	0.6040	704	3.4147	3549	3143	12.7UI	0.0862	0.0724
## 0.28 and \alpha = 0°.  ## 0.7  Afterbody Forebody Afterb  X.L CP X.L CP X.L CP X.L  39. 343.16 0.0054 1.08.37 1.0801 343.16 1.08.37 1.08.38 149.13 1.09.39 149.39			Foreb	ž	-187.47	-155.11	130.84	-106.57	-90.39	-74.21			-33.76	/9.67-		1671-	-10.27																																
## 0.28 and \alpha = 0°.  ## 0.7  Afterbody Forebody Afterb  X.L CP X.L CP X.L CP X.L  39. 343.16 0.0054 1.08.37 1.0801 343.16 1.08.37 1.08.38 149.13 1.09.39 149.39			^	<u>a</u> ;	514	505	539	<b>548</b>	161	<del>(</del> 15	373	313	28																																				
## 0.28 and \(\alpha = 0^{\text{T}}\)  ## 10^{\text{T}}  Afterbody Forebody  X.L CP X.L CP  39. 343.16 0.0034 1877 1.0801 347 1.0801			Literbod			7	-	7	7	7	7	7	_																																				
## C		180						_						<b>8</b>	e :	2 3	RS	æ :	<del>.</del> :	2 9	2:	2 :	<b>s</b> t:	₹ :	<u>∽</u> :	9:	<b>s</b> t :	= 5	₽:	= :	= 9	2 2	: =	- =															
mfr = 0.28 and  Afterbody  X/L CP X  X/L CP X  X/L CP X  343.16 -0.0544 -183  11 545.71 -0.0514 -2.0  12 55.77 -0.0514 -2.0  13 55.77 -0.0514 -2.0  14 55.77 -0.0514 -2.0  15 55.77 -0.0514 -2.0  16 55.77 -0.0514 -2.0  17 55.71 -0.0514 -2.0  18 55.77 -0.	<b>ی</b>	Ť	ě																																														
After a second and	8 and a		Œ,	¥ ;	187.4	-25.6	-10.2	-2.0	0.0	03	9.0	1.2	ec :	C7 :	- :	7.5	? •	0.5	7.0	Z. C	8.	00 9	621	15.0	17.5	20.0	9. 9	20.0	0.00	20.00	90.0	200	100	241.8															
After a second and	nfr = 0.2		body	පු දි	0.0548	-0.0539	-0.0527	-0.0514	-0.0484	0.0415	-0.0360	0.0279	-0.0026																																				
	_		Affei	ZZ.	383.16	419.13	457.12	507.77	545.76	571.08	583.74	596.4	609.07																																				
			ģ	<b>a</b> 5	8 2	1.0776	1.0747	1.0642	1.0541	1.0457	1.0323	1.0277	1.0263	1.0343	\$780°1	1.0008	. 1013	200	5650.1	0.9443	0.6800	0.4284	0.0890	1.7333	1.9107	06697	/7897		1.7324	2	(00/	9139	¥685	0.9136	11011	0.9225	1.1896	-08 -28	1.1333	1.0674	0.9960	0.8272	0.7500	0.5967	0.5307	0.3806	0.5524	0.1235	0.1116
Fort XL			Foreb	אָל גל	171.70	-155.11	-130.84	-106.57	-90.39	-74.21	-58.03	183	33.76	75.07	-23.11	11.97	77.01.	5.5																															279.84

TABLE VI. Continued

(c) Continued

		Afterbody	CP	-0.0195	0.0101	-0.0067	0.0224	0.0578	0.1023	0.1433	0.765	0.0																																	
	80.	Afte	ΧĽ	343.16	419.13	457.12	507.77	\$45.76	\$71.08	585.74	6000	6.00																																	
	<b>\$</b> = 180°	Forebody	Ç	0.9409	0.6188	0.7947	1.1220	0.2127	-0.9275	87751	7676	1.6723	-1.6215	1.6590	1.6230	-1.4745	0.7247	0.6776	0.0758	0.0833	0.7133	-0.6322	-0.5835	-0.4836	-0.4198	-0.4001	-0.3831	-0.3529	0.3138	1300	0.0467														
ndα=0		Fore	χŢ	-187.47	-25.67	.10.27	-2.05	000	0.31	0.63 1.25	88 1	2.50	3.13	3.75	4.37	2.00	6.25	7.50	8.75	0001	2 2	17.50	20.00	30.00	20.00	00:09	20.00	80.00	0006	00.00	241.85														
mfr = 0.55 and α = 0°		ģ	c <sub>B</sub>	-0.0251	0.0131	-0.0007	0.0279	0.0617	0.1104	0.1438	0.000	1																																	
ā		Afterbody		343.16						506.41																																			
	<b>0</b> = <b>0</b>	ď,		0.9458	•					0.677			0.6141	0.6419	0.7833	0.9873	1.0813	1.1273	1.0897	0.9794	1 0864	-1.5284	-1.8345	.1.7831	-1.6358	-1.6240	-1.6017	-1.4055	-1.0942	0.8870	0.7244	-0.7004	-0.7063	-0.6699	0.6133	-0.5549	0.4369	-0.4193	-0.3894	3868	0.3439	0.3108	-0.1952	-0.0501	0.0383
		Forebody		-187.47				_		58.03										\$ 5										67.0						20.02					00.00				279.84
							•		<u>-</u>	e 9	. ×	2																																	
		Afterbody		6 -0.0357				90:0308		0.1120																																			
	• = 180°	₹		343.16						506.4			•		•	0 :	<b>.</b>	· ·	. م		٠.	, 0	4	•	7	_	7	e .		4 4															
2.0°	٠	Forebody		0.9763						27.47.34										0.6431										0.1844															
and α =		ĕ	ጟ	-187.47	.25.67	-10.27	-2.05	0.00	0.3	0.03	2 2	2.50	3.13	3.75	4.37	2.00	57.0	2.5	57.5	000	00.31	17.50	20.00	30.00	90.00	90.00	20.00	80.00	20.06	9001	241.85														
mfr = 0.49 and α = 2.0°		Afterbody	Ç	0.0276	-0.0225	-0.0105	0.0129	0.0449	0.0870	0.1548	0.3042	203.0																																	
-	.0 = 0		ž	343.16	419.13	457.12	507.77	545.76	571.08	506.41	6000	2.03																																	
	•	Forebody	C	0.9788	0.9788	0.9596	0.9358	0.8982	0.8656	0.8220	0.7763	0.7674	0.7745	0.8045	0.9359	1.0772	907	1.1132	0.9844	0.8058	903	-1.8882	-2.0780	-2.1003	2.0902	-2.0826	-2.0134	-1.9802	1.9331	1.8850	1.7647	1.7341	-1.6164	-0.8551	0.6126	0.3042	0.4859	-0.4509	-0.4303	-0.4101	0.3706	0.3288	0.2081	-0.0592	-0.0479
		For	χ	-187.47	-155.11	130.84	-106.57	-90.39	-74.21	-58.03 4 85	37.55	-25.67	-23.11	17.97	-10.27	-5.13	¥. ;	-2.05	<b>3</b> 6	<b>4</b> 5	3 5	0.63	1.25	1.88	2.50	3.13	3.75	4.37	5.00	67.6	8.75	10.00	12.50	12:00	17.50	20.02	40.00	\$0.00	90.00	70.00	80.08	00.00	10.00	241.85	279.84
		ody	C.	-0.0239	-0.0222	-0.0154	690000	0.0326	0.0720	0.1110	0.033	7.77																																	
	90	Afterbody		343.16			507.77	545.76	571.08	506.41	60000	6.00																																	
	<b>4</b> = 180°	ody	C.	108670	0.7298	0.8939	1.1295	0.0487	1.1908	07270	1.0405	-1.9525	-1.8500	-1.8443	-1.8053	1.7755	1000	-1.3753	0.8103	0.6811	0.0303	0.6166	-0.5862	-0.5017	-0.4273	-0.4117	0.3904	-0.3578	0.3143	0.2300	0.0550														
mfr = 0.49 and α = 0°		Forebody	χ	-187.47	-25.67	-10.27	-2.05			0.63										900			20.00				000	80:00	80.00	00:00	241.85														
. • 0.49 в		d,	_	-0.0334	0.0214	-0.0107	0.0133	0.0399	0.0836	0.1153	0.1268	0077																																	
ja		Afterbody			419.13 -0					583.74 0																																			
	0 = 0	·	_	0.9756 3v						0.8122 5			0.7336	0.7643	0.8996	1.0436	8	1.1270	9478	0.8928	1003	-1.7452	-1.9783	-1.9593	-1.8385	-1.8064	-1.7929	-1.7342	1.6932	-1.6058	-0.2720	-0.8244	-0.6559	-0.6628	-0.6267	0.5826	-0.4529	0.4212	-0.4062	-0.3847	0.3616	0.3141	6961 0-	0.0580	0.0460
		Forebody			155.11 0.5					-58.03 0.3											3 -					3.13 -1.				6.25						20.00 -0.				70.00		9 9 8 8 8 8			_
			_	<b>=</b> :		: =	9-	6.	۲.	ک ن	7 "		7	7	7	•	•	•	•	•												-	_	_	1		. 4	•7	J		~ (	=	: =	- 7	

TABLE VI. Continued

(c) Continued

				۰	6	₹,	n a		, <u> </u>	. ~	7	9																																				
		Afterbody	ි පි	-0.0076	-0.0029	0.000	0.0195	0.00	0.1621	0.2092	0.2592	0.329																																				
	°081	Afte	X	343.16	384.14	419.13	45/.12	45.76	571.08	583.74	596.41	609.07																																				
٠	<b>6</b> = 180°	pod	ů	0.7631	0.6246	-0.1032	0.077	0.8272	0.0465	0.3411	-0.4603	0.4304	-0.4927	-0.3588	0.3802	-0.3573	0.361	200	430	1906	04780	-0.4317	4018	0.3456	0.3283	-0.3381	-0.3311	03180	-0.3026	-0.2712	0.2048	-0.1500	-0.0297															
nd a = 0		Forebody	χĽ	-187.47	106.57	-25.67	7707	000	0.31	0.63	1.25	1.88	2.50				200							20.00					80.00	90.00	100.00	110.00	241.85															
mfr = 0.74 and $\alpha$ = 0°		ły	<u>ت</u>			0.0269	00710	0.1087	1549	0.1948	0.2456	0.3126																																				
Į.		Afterbody				419.13						0.609																																				
	°0 *		_	_		0.7366 41		_					-0.0780	-0.1346	-0.1079	513	0.3286	0 0003		1,1253	469	-0.0882	596	-0.5026	174	-0.3779	817	910	910	911	784	509	374	716	7 70 7	<b>S</b> S	2	223	3	282	80	353	ž	20	31	218	<b>8</b>	163
		Forebody			_	130 84 0.7									17.97 -0.1		2.0		0.0				0.63 -0.3				3.13 -0.3			5.00 -0.4	6.25 -0.3			10.00 -0.3917					40.00 -0.3440							00 -0.1618		84 -0.0263
			×	-	Ę	5. 5.		×	4.	85-	₹	÷.	ξ.;	-23	÷ •	? •	? "	, 17	, 4	, 4		0	•	_		7	Ē.	•	•	•	•	7	•	2 5	2 2	: :	: 2	8	ŧ	S	8	2	86	8	100:00	1000	241.83	279.
		Afterbody	පි	-0.0059	-0.0055	0.0082	0.0536	0.0964	0.1542	0.1936	0.2484	0.3203																																				
	.08	After	χ	343.16	384.14	419.13	507.77	545.76	571.08	583.74	596.41	609.07																																				
	• = 180°	oody	c	0.8283	0.7216	0.4235	1.0212	0.6249	-0.2880	-0.8296	-0.8753	0.778	-0.6576	-0.6352	62724	1000	0 5153	5 5448	0.5437	0.5083	-0.5348	-0.5092	-0.4865	-0.4198	-0.3914	-0.3593	0.3579	-0.3371	-0.3187	-0.2790	-0.2166		0.0315															
mfr = 0.68 and $\alpha$ = 0°		Porebody	χ	-187.47	106.57	-10.27	-2.05	000	0.31	0.63					5.73														_	_	_	_	241.85															
■ 0.68 a		۵			0.0076	0.0198	0.0528	0.0956	<u>\$</u>	1885	0.2381	890																																				
nf.		Afterbody			384.14							0.609																																				
	0) = <b>0</b>		•										8 5	3 5	1 7	. E	. Se	356	721	25	<b>9</b>	19	<b>8</b>	<b>2</b>	4	78	<b>2</b>	22	₩.	Ş	2	<b>3</b> 1	2 8	3 3	2	12	78	38	3	22	85	92	<b>:</b>	5 5	<b>2</b> 2 52 52	<b>3</b>	7 :	2
		훋			25 0.8313								2661.0						7201.1 06		_	31 -0.4119			1.88 -0.8142				37 -0.5648				0.5568												•	· 	2003	
		_	×	-187.47	27.17.1.	130.84	-106.57	.90.39	-74.2	.58.03	4.85	55.70	10.62	17.07	-10 27	-5.13	25.65	-2.05	06.0	44.0	Ö	0.31	ŏ	-	-	7	eri i	3.75	₹ .	Ň	6.25	S. 5	ró <u>č</u>	12.50	15.00	17.50	70.	30.00	<del>Q</del>	20.00	3	8 9	<b>S</b>	80.8	0000	110.00	1907	7.2.7
		ody	පි	0.000	0.000	0.0135	0.0447	0.0794	0.1290	0.1743	0.2239	0.6933																																				
	.0°	Afterbody			41013						596.41																																					
	• = 180°	od,	a 5	0.8910	0.4357	0.6442	1.0907	0.4402	-0.6087	-1.2474	1.4831	6764.1	1 2844	0.000	-0.7187	0.7011	-0.6229	0.6589	-0.6595	0.6433	0.6466	0.6215	0.5495	2.5202	0.4293	0.3859	-0.3831	0.3042	0.3397	0.3015	0.2335	76/10																
<b>d</b> α = 0°		Forebody		18/.4/							·							7.50		000		12:00					90:00					0000																
$mfr = 0.61 \text{ and } \alpha = 0^{\circ}$		<b>&gt;</b>					0.0482	0.0845	<b>3</b>	743	777	974																				- '	•															
uf.		Ě		343.10 -0.0133							27770 14.																																					
	• 0 •	i			•	Ì					1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00			2	5	3	73	61	71	8	8	<b>5</b> :	<u> </u>	<b>=</b> ∶	F) :	ء ج	⊋ :	<b>.</b> :	Ŧ :	× .	e :	3 8	3 8	33	33	93	21	7	28	<b>6</b> 5 5	<b>3</b> 3	٠ : د	<b>.</b> 2	3 2	2 2	3 X	3 %	2
	•	Š		0.8928							55 0.3318									1.0508							3 -1.2040					02000										62529						
		*	X :	121.70	-155.11	130.84	-106.57	8	-74.21	50.86-	5 E	25.67	-23.11	-17.97	-10.27	-5.13	4.5	-2.6	96.0	Ġ.	J.O	0.31	0.63	1.25	86.	77	5.15	3	15.4	30.0	6.25	JC., 9	10.00	12.50	15.00	17.50	20.0	30.00	900	20.00	90.0	80.0	80.00	20.00	1000	2418	270.84	

TABLE VI. Continued

(c) Concluded

 mt = 0.81 and  $\alpha = 0^{\circ}$  

 Forebody
 Afterbody
 After

TABLE VI. Continued

(d) M = 0.72

		ż	) D	-0.0231	-0.0252	0.0154	0.0156	0.0450	0.0903	0.1283	0.1736	0.2479																																				
		Afterbody	X.			419.13 -0					596.41 0	0 609.01																																				
	<b>♦</b> = 180°	} • •	<b>2</b> 6	- 1		0.7397					-1.8312 5		-1.8543	-1.8119	-1.7585	-1.7388	1. 7002	2010	1.4633	0.01	-1.4010	1,011	0.50	0.5417	-0.4974	-0.4477	-0.4269	0.4043	0.3749	-0.3326	-0.2573	-0.1988	-0.0597															
°0 ⊌ 0		Porebody	X			.0.22-0.0		0.00			1.25 -1.						3.5		÷ - ₹ :		999		2 2 2			20.00							241.85 -0.0															
mfr = 0.49 and $\alpha = 0^{\circ}$											9									•					. ~	. •		. ~	60	•	2	=	24															
- fa		Afterbody	b			2 0.01/4					1 0.1756	7 0.2462																																				
	0 = 4	\ \	×			457.13						1 609.07	3	<b>90</b>		۰.	۷ -		<b>4 6</b>		- ·							•	_	7	0	•	~	•	_	<b>.</b>	~ .	<b>.</b>	•									
		Forebody	Ç			0.9804	_								0.7821				10404					-1.8378								-1.5116							0.4940									
		P.	χ	-187.47	171.29	13084	-106.57	-90.39	-74.2	-58.03	41.85	-33.76	-25.67	-23.11	76.71	7701-	2.5	200	60.7	277	\$ 6	250	063	1.25	88	2.50	3.13	3.75	4.37	5.00	6.25	7.50	8.75	10.00	12.50	15.00	05.71	20.02	30.05	3 5	8.6	20.00	8 6	8 6	100.00	1000	24185	279.84
		Apoc	පි	-0.0366	-0.0395	-0.0342	-0.0175	0.0000	0.0297	0.0586	0.0953	0.1555																																				
	8	Afterbody	χ		384.14	457.12			571.08	583.74	596.41	609.07																																				
	<b>9</b> = 180°	ğ	g.	1.0436	1.0108				-1.4358	-1.8707			-2.0522	-2.0112	0686	1001	1880	1 8233	7786	17305	263	¥065	-1.1374	-0.8544	-0.4101	-0.4375	-0.4281	-0.4051	-0.3776	-0.3363	-0.2658	-0.2142	0.0640															
<b>d</b> α = 0°		Forebody	χΓ		106.57			,	0.31						. 61.6											\$0.00	00:00	70.00	80.00	90.00	_	_	41.85															
mfr = 0.40 and $\alpha = 0$ °		•	. م				8	0.0122	0.0435	0.0638	0.1018	178																			_	_	7															
Į.		Afterbody	L CP		384.14 -0.0391							.07 0.157																																				
	• = 0 •		×									97 609.07	8 8	2 5	÷ 8	3 3		3	3 3		3 25	. 5	72	33	82	53	3	20	7	<del>2</del>	33	51	e :	<b>8</b> . 2	8 8	c s	٤ ٧	3 3	3 \$	: ×	2 2	8	22	11	: 8:	:22	8	25
		Forebody			00401									0.90/3					_					25 -2.0233										00 1.7329											•	Ċ		
		124	ΧΓ	187.47	(7.17)	130.84	-106.57	-90.39	-74.21	-58.03	41.85	33.76	-25.67	11.62-	70.01.	13.5	7.	20.05	06.0	440	000	0.31	0.63	1.25	88.1	2.50	3.13	3.75	4.37	5.0	6.25	2.50	8.75	00.01	25.5		2.00	20.05	8.6	Ş	00'09	20.00	80.00	00:06	100	110.00	241.85	279.84
		Afterbody	ŝ	-0.0455	9000	-0.0496	-0.0459	-0.0422	-0.0239	-0.0080	0.0127	0.0501																																				
	<b>80</b> e	After	ž	343.16	41013	457.12	507.77	545.76	871.08	583.74	596.41	609.07																																				
	= 180°	ody	G C	1.0824	1000	1.1062	1.0258	-0.4333	-1.4822	-1.5726	-1.4178	-1.4325	-1.4881	1704	14189	1 3953	-1.4532	-1.3001	13700	-1.4020	-1.3016	-1.3034	-1.2866	-1.2514	·1.1068	-0.6896	0.5801	-0.4170	-0.3751	-0.3216	0.2678	0.2314	-0.0698															
mfr = 0.30 and $\alpha = 0^{\circ}$		Forebody	χľ	187.47	75.67	-10.27	-2.05							27.5																_	_		. 68.142															
- 0.30 a		¥		-0.0585		0.0491	-0.0422	-0.0410	-0.0300	-0.0223	0.0000	0.0282																																				
F		Afterbody		343.16 -0.0						_		009.07																																				
	% # <b>♦</b>			1.0829								20101	1.0182	0670.1	96	1.1339	1.1075	1.0275	0.8013	638	0.5426	\$	119	393	461	250	012	297	389	896	629	086	ę s	3,50	3 5	784	178	. 795	90	189	86\$	172	375	282	733	582	577	889
		Forebody						_					0.1 /0.22-									0.31 -1.4994			1.88 -1.4461		3.13 -1.4012			5.00 -1.3968			8.75	10.00		2875 1. 02.71		30.00 -1.0667				70.00 -0.4472		90.00 -0.3282	00.2733	_	.85 -0.0773	.84 -0.0688
			×	-187.47	1551.	130.84	-106.57	ķ	-74	Š,	₹ :	3, 5	9 5	7 -	: =	γ,	, ti	7	9	Ŷ	0	C	0	_	-	2		3	4	\$	<b>1</b>	- 0	<b>*</b>	2 2	: <u>*</u>	2 2	: 2	2	<b>\$</b>	8	8	70.	80	8	100.00	110.00	241.85	279.84

TABLE VI. Continued

(d) Concluded

			nfr = 0.54	mfr = 0.54 and α = 0°			
,	H .	ಹಿ		ı	u		٠
Fore	Forebody	Affei	Afterbody	For	Forebody	After V	Afterbody
-187.47	0.9620	343.16	-0.0231	-187.47	0.9565	343.16	-0.0190
-171.29	0.9600	384.14	0.0190	-106.57	0.8963	384.14	0610.0
-155.11	0.9580	419.13	-0.0101	-25.67	0.6472	419.13	-0.0060
-130.84	0.9341	457.12	0.0066	-10.27	0.8195	457.12	-0.0007
-106.57	0.8974	507.77	0.0334	-2.05	1.1320	507.77	0.0253
-90.39	0.8571	545.76	0.0700	000	0.2203	545.76	0.0615
-74.21	0.8140	571.08	0.1189	0.31	0.8566	571.08	0.1152
-58:03	0.73	583.74	0.1575	0.63	-1.4653	583.74	0.1575
25.25	0.700	500.4	0.2042	C7:1	1 7214	500.4	0.2831
-25.67	0.6342	6.00	0.4.7.0	2.50	1.5867	0.00	
-23.11	0.6405			3.13	-1.6325		
-17.97	0.6710			3.75	-1.5407		
-10.27	0.8106			4.37	-1.5287		
-5.13	0.9958			2:00	-1.4826		
-3.34	1.0905			6.25	-1.4634		
-2.05	1.1305			7.50	-1.2997		
8; 9;	1.0975			8.75	-0.7859		
4 5	0696			00:01	-0.8859		
000	0.1897			12.50	1699.0		
5 5	1,787			9.51	0.0131		
0.03	1.450/			20.00	6.00/2		
8	.1 7262			3.05	0.27		
2.50	1.5934			20.00	-0.4368		
3.13	-1.5778			90.09	-0.4071		
3.75	-1.5008			70.00	-0.3904		
4.37	-1.4632			80.00	-0.3593		
2.00	-1.3722			00:06	-0.3176		
6.25	-1.4271			100,00	-0.2436		
7.50	-1.2896			110.00	0.1893		
8.75	0.6690			241.85	0.0444		
2 2	0.0040						
15.00	0.6548						
17.50	-0.6053						
20.00	-0.5576						
30.00	-0.4811						
40.00	-0.4472						
90.00	0.4166						
90.00	0.4049						
8.00	0.3834						
8 8	1 1 1						
000	0.2455						
110.00	0.1938						
241.85	0.0548						
279.84	-0.0421						

TABLE VI. Continued

(e) M = 0.74

		į	දිරි	-0.0310	0.0360	-0.0271	1600	0.0135	0.0466	0747	0.1125	0.1742																																	
		American	5																																										
	<b>4</b> = 180°			_	384.14						396.41				_	_		_	_			_			_	_																			
°,	4	Forehody	g S	0.05	0.010	1.0428	1.109	-0.1081	1329	1.74	1.8330	910	8	-1.8634	-1.7965	1.797.1	-1.7456	-1.7179	-1.6510	1.6424	1 500	-1.4959	-1.4502	-0.4627	-0.4066	-0.4100	0.4040	0.3781	0.2634	-0.2010	-0.0628														
$mfr = 0.40 \text{ and } \alpha = 0^{\circ}$		No.	×	187.47	15 on 1	-10.27	-2.05	0.00	0.31	0.63	C7:	2.50	3.13	3.75	4.37	5.00	6.25	7.50	8.75	10.00	8	17.50	20.00	30.00	20.00	00:00	00.02	80.00	100.00	110.00	241.85														
<b>=</b> 0.40 a		2	ر ئ	0.0415	1310	0.0201	-0.0017	0.0181	0.0544	0.0809	9117	<u>*</u>																																	
mfr		Afterbody	;																																										
	% = 0,		×	343.16					571.08			_	_	_	•	<b>.</b>	_	<b>.</b>	٠.		. ~	_	_						_	_	_			_	_										
		Forebody	ට්	1.0551	1.0532	1.0433	1.0234	1.0020	0.9817	8660	0.010	0.9184	0.9223	0.9545	1.0389	1.1325	1.1460	1.1133	0.963	0.7614	1.416	1.7378	1.8768	1.9026	1.893)	-1.8803	000	1.8050	-1.7578	1.6870	- 6493	1.6313	4006	-1.4457	-1.4240	-0.4893	-0.3665	-0.4119	0.4115	404	0.375	0.3551	0.2368	0.0647	-0.0516
		For	×	-187.47	-155.11	-130.84	106.57	90.39	14.21	-58.03	11.56	25.67	-23.11	-17.97	-10.27	-5.13	÷.	-2.05	Ş ;	\$ 6	0.31	0.63	1.25	88.	2.50	3.13	6.73	8	6.25	7.50	8.73	2 2	15.00	17.50	20.00	30.00	40.00	20.00	80.00	20.00	8 8	3.6	1000	241.85	279.84
				- 9	. 0	=	<b>4</b>	ve y		20		,																																	
		Afterbody		0.0397	0.0470	0.0521	0.0	-0.0366	0770.0	0000	0.900																																		
	08	Ą	X	38.15	419.13	457.12	507.77	55.78	50.1.08	596.41	609																																		
	<b>081 = </b>	ody	G .	1.0720	1.0253	1.1157	1.0378	0.3529	0146.1	7 (1) 7	2.0713	-2.0599	-2.0210	1.9804	-1.9775	9996	1.9331	0606.1	1.6369	-1.7136	1.7132	-1.6509	-1.6117	0.8986	9 5	77450	0.355	-0.3235	0.2643	0.2103	0.0757														
mfr = 0.31 and $\alpha$ = 0°		Foreb	X/L CP	-106.57	-25.67	-10.27		80.5										S. 5		12.50						90.06			į	0001															
0.31 an							æ ·	4 4	, ,	· -													•				_		=	= ;	*														
mfr -		Afterbody		0.0525	-0.0501	-0.0474	0.040	0.0334	0.000	0.0121	0.0536																																		
	90 = <del>0</del>	ΨV	X	384.14	419.13	457.12	507.77	545.76	58174	5964	609.07																																		
	*	ody	<u>د</u> د	1.0931	1.0927	9980.	1.0740	1.0649	1 0175	1.0272	1.0172	1.0275	1.0305	1.0558	1.1162	1.1412	8 2	277	0.5885	0.4899	-1.6261	1.8986	-2.0380	7.0587	2 0100	2.0346	-1.9725	1.9694	-1.9189	1.8829	1.8818	1.7708	1.7021	-1.6651	.5948	-0.9133	2000	40.3307	0.3420	0350	0.3211	0.2641	0.2151	-0.080.0	7.0734
		Forebody	XI	171.29	-155.11	130.84	-106.57	26.39	-58.03	41.85	-33.76	-25.67	-23.11	17.97	-10.27		30.0							8 5			4.37			7.50		12.50						300		0000					279.84
			7	7	<del>-</del>	7	_		,	•	•		•	•	•																						•	,	, ,-	- 02		. 5	=	77	22
		body	CP CP	0.0491	-0.0452	-0.0495	4 6 6	-0.0483	0.0219	-0.0114	0.0271																																		
		Afterbody	X/L				307.77				609.07																																		
	• = 180°	Į,	CP				0.44600				_	-1,4037	-1.3973	-1.4192	45.7	1.4206	1 3714	-1.3232	-1.3525	-1.3340	-1.3111	-1.3146	1.2492	5 7081	564	0.5631	-0.4719	-0.3918	0.3243	0.2761	600														
,0 × D		ě					50.2-								15.4															_															
mfr = 0.27 and $\alpha = 0^{\circ}$		,	X/L	106.57	-25.67	-10.27	7 0	• •	0	_	-	2	mi e	mi •	4	-i ve		i ec	2	12		:	8.6	8.8	9	8	80.00	00.00	00'001	24   85															
ifr = 0.5		pody	CP 050	-0.0507	-0.0499	0.0429	9190	0.0464	-0.0394	-0.0285	0.0069																																		
=		Afferbody	7 5 K	384.14	419.13	457.12	77.705	\$71.08	583.74	596.41	206:02																																		
	0		,,,		•	•	. •	. •1	-1	-,	~								_	_	_																								
	.0 = <b>\( \phi \)</b>	<u>.</u>	<u> </u>	1018	1026	\$ 50	786	969	388	)542	342	8650	£ 5	26.5	, ,	2	ğ	ş	26	<u>₹</u>	22	4 5	2 8	3 6	47	355	63	037	1	9 6	5	616	3	8 8	3	2	3 5	\$	023	Š	718	116	731	23	802
	٠	٥	X/L CP -187.47 1.1018		_	-130.84 1.0965			-58.03 1.0588			_		17.97 1.0842			-2.05 0.9908					0.03 -1.3141		2.50 -1.5539					7.50				15.00 -1.2361	20 -1.1088	20.00						_		_		279.84 -0.0802

TABLE VI. Continued

(e) Continued

		ody	ch Ch	0.0028	0.0082	0.0195	0.0361	0.1594	0.2043	0.2561	0.3290																																			
	ይ	Afterbody		384.14	419.13	457.12	77.100	571.08	583.74	596.41	20.609																																			
	⇒ = 180°	dy		0.8367			0811.1					-1.2989	-1.2516	6//1.1	0.8676	0.8875	i i	0.5995	-0.6363	-0.6786	-0.7006	5785	0.5418	0.4459	0.4096	4023	-0.3747	0.3501	0.303	-0.1791	-0.0389															
α = 0°		훋		-106.57 0.			-2.03							 									20:00					80.00	_	Ĺ																
mfr = 0.61 and $\alpha = 0^{\circ}$						•												_	΄ =	: =	=	_	~	æ. ₁	<b>∞</b> , ∶	<b>25</b> i	<b>κ</b> δ	ž đ	. 5	Ξ	24															
mfr = 0		Afterbody	<b>a</b> 8	-0.0024	0.0078	0.0234	0.0588	0.1583	0.2000	0.2506	0.3223																																			
	.0 = <b>0</b>	Affe	Z X	384 10	419.13	457.12	507.77	571.08	583.74	596.41	609.07																																			
	•	pody	<u>د</u> و	0.9220	0.9182	0.8903	0.8397	0.7290	0.6488	0.5624	0.5279	0.4703	0.4655	0.5098	2000	0.5010	911	8	1.0835	0.4462	-0.6065	-1.1479	-1.3860	-1.3334	1.2500	-1.1951	-1.1375	1.0094	06200	0.5490	-0.7014	-0.6546	-0.6930	-0.6522	-0.5890	0.5529	0.4037	0.4074	-0.3983	-0.3807	-0.3537	-0.3069	0.2384	-0.1750	0.0447	-0.0339
		Forebody	X/E	-187.47	-155.11	-130.84	-106.57	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	16.71	7701-		5	60.0	4	000	0.31	0.63	1.25		5.50	3.13	5.7	£ \$	2,5	7.50	8.75	10:00	12.50	15.00	17.50	20.02	80.08	9 9	0000	70.00	80.00	00:06	00.00	0.00	241.85	77.84
			_ ;	> <b>3</b>	11	<b>=</b> :	2 8	2 2	4	_	8																																			
		Afterbody		-0.010/ 4 -0.0146			7 0.0365				7 0.2999																																			
	\$\phi = 180^c			384.16	-		7.702				609.07			_						_	_		_																							
<b>.</b>	÷	Forebody	G G	0.9784	0.0649	0.8395	1.1437	0.2702	1.3061	-1.5722	-1.5962	-1.6123	-1.5727	0000	7007.	0.000	1 3430	1 2912	.1.2282	66601	-0.6043	0.5447	-0.5020	-0.4856	0.4403	-0.4226	-0.3932	0.3682	0.345	-0.1860	-0.0501															
and a =		For	χŢ	187.47	-25.67	-10.27	2.05	200	0.63	1.25	1.88	2.50	3.13	3.13		3,00	3 5	7.8	10.00	12.50	15.00	17.50	20.00	30.00	50.00	90.00	00.02	80.08	100.00	110.00	241.85															
mfr = 0.54 and $\alpha = 0^{\circ}$		ody	G 5	0.0224	0.0045	0.0103	0.0400	0.0786	0.1729	0.2200	0.2941																																			
ā		Afterbody		384 14	•		77.105		583.74	596.41	20.609																																			
	• = 0 <sub>•</sub>	À		0.9750	•	•	0.9103		_		Ī	0.6675	90990	0.0993	1 5	C#70"	1464	1071	92260	0.2036	-0.9086	-1.3655	-1.6275	-1.6141	- 5945	-1.5207	-1.4987	1.4599	0070	3048	-1.2979	-1.1519	-0.6155	0.5419	2. S.	-0.5365 0.4864	0.4804	0.4768	0.4140	-0.3984	-0.3641	-0.3216	-0.2469	-0.1892	0.0488	0.0410
		Forebody		-187.47 0.			-106.57 0.							671		2.5												5.00				10.00				900										. 79.84
			~ :	-1.	. 5	£.	۽ ڊ	, ,	. <b>4</b> 5	4	ė.		·	7 -	•	•			•													_	_	_	- '	7 (		, ,	, •	1	•	5	2	= ;	7. 5	7
		Afterbody	<b>a</b> 5	0.0130	-0.0076	-0.0033	0.0263	0.0018	0.1499	0.1967	0.2653																																			
	°0.		X.	38.10	419.13	457.12	507.77	571.08	583.74	596.41	609.07																																			
	<b>4</b> = 180°	ody	G.	0.9907	0.7577	0.9079	1.1438	1.0425	1.4754	-1.7110	-1.7224	-1.7300	-1.6715	-1.0035	-1.0328	1.5836	55.5	14403	1 1733	1.3246	-1.2827	-0.7631	-0.7061	-0.4622	0.4523	0.4289	0.4130	0.3806	0.5555	0.2013	-0.0611															
d a = 0°		Forebody		106.57				3 2								90.4												8.8		_																
mfr = 0.49 and $\alpha = 0^{\circ}$		_					325	\$ <del>§</del>	218	61.6	653																																			
Ħ.		Afterbody		16 -0.0252				0.0004																																						
			X	343.6	419.13	457.12	507.77	6.5	583.74	596.4	609.07																																			
	,0 # •			<b>3</b> 3	وب	=	<u>ب</u>	2 5	: =	<b>*</b>	200	2	õ	2 2	2 9	28 2		3 %	3 3	92	12	8	5	\$	2	2	-	÷ 5		3 2	2	82	5	8	= :	<b>X</b> :	<b>=</b> 5	3 8	3 92	83	98	7	42	5	23	7
	.0 <b>**</b> •	Forebody		187.47 1.0034				74.21 0.9197								5.13 1.0608										3.13 -1.6852		4.37 -1.5845		7.50 -1.4673					17.50 -0.9111		30.00 -0.4681					_		_		279.84 -0.0521

TABLE VI. Continued

(e) Concluded

		2	2 6	0.0075	0.0107	0.0399	0.0808	0.1310	0.1918	0.2362	0.1579																																	
		Afterhody	XI.		384.14 0.				571.08 0.																																			
	180°	1	Î				_						12	2 5	2 2	2 2	2	20	٤	22	2 :	2 5	2 5	. =		. <u>se</u>		9	so :	٠,	,													
<u>ی</u>	•	Forehody	Ö		0.5516				0.3121					0.1870							0.3652				-0.3280					0.1500														
and a		Pe	, ¥	-187.47	.106.57	10.27	-2.0\$	000	0.31	0.03	88	2.50	3.13	5.75	5 5	625	7.50	8.75	10.00	12.50	15.00	2.5	20.00	2000	90.09	70.00	80.00	90.00	00:00	74184														
mfr = 0.80 and $\alpha = 0^{\circ}$		Apor	ð	0.0013	0.0103	0.0442	0.0835	0.1291	0.1902	0.2271	0.34																																	
8	٤.	Afterbody	χ	343.16	384.14	457.12	507.77	545.76	571.08	596.41	609.07																																	
	0 #		<u>မ</u>	0.7221	0.7255	0.6530	0.5522	0.4403	0.3112	0.1211	-0.2828	-0.5775	0.5822	0.5132	0.3391	0.5989	0.7799	1.0528	1.1349	0.9567	0.2997	0.1403	01570	0.1402	-0.2307	-0.1937	-0.1700	.2265	-0.2865	1817.	0.2957	-0.3790	-0.3504	0.3606	0.3468	0.3233	0.3187	-0.3333	-0.3247	-0.3072	-0.2773	-0.1985	7947	-0.0213
		Forebody	X/L		0 62.171-				58.03					7 601.							0.31			250						2 2					20.00							00:00		
				7	<del>,</del> ,	· <del>·</del>	÷	-	•	. 1		**																									•		-	-	· ;	= =	- 2	21
		Afterbody	පි	0.0034	0.0070	0.0346	0.0756	0.1270	0.1839	0.2837	0.3535																																	
	e 180°		Χď	343.16	419.13	457.12	507.77	545.76	571.08	596.41	609.07																																	
٠	•		g.	0.7988	0.0633	0.2141	0.9451	0.8274	0.04/6	-0.5391	-0.4511	-0.5201	-0.4029	1205	-0.3375	-0.3548	-0.3764	-0.4178	-0.4217	0.4765	0.4446	0.4021	0.3582	-0.3626	-0.3613	0.3341	-0.3233	-0.2827	0.2150	0.1370														
nd a = 0		Forebody	χĽ	-187.47	-106.57	-10.27	-2.05	000	15.0			2.50	3.13								200	200	30.00	20.00	90.00				000															
$mfr = 0.74 \text{ and } \alpha = 0^{\circ}$		*	۵,		0.0030	0.0358	0.0767	0.1239	0.1824	0.2760	0.3434																																	
mfr		Afterbody	C.																																									
	00 #		×		9 584.14				581.08		55 609.07	<b>22</b>	= 5	: 5	: 12	9	2	92	œ:	2 5	: ¥	2 2	: :=	13	=		_	= :	2 =		4	<b>1</b>	'n	v.	0 5	. 2		5	•	0.5	n -	<del>.</del> -		
		Forebody	g.		0.08030				3 0.333				1 -0.0741						1.1406		10/0/07								0.403							03800					0.2923			
		Ĕ	X	-187.47	-171.29	130.84	-106.57	S. 35	58.03	41.85	-33.76	-25.67	-23.11	10.27	-5.13	3.34	-2.05	96. 9	40.0	800	15.0	1.25	88.1	2.50	3.13	3.75	4.37	8.8	0.20	8.75	10.00	12.50	15.00	17.50	20.02	000	20.00	90.00	90.0	80.00	80.05	10.00	241.85	279.84
		Ą	පු	0.0007	0.0027	0.0311	0.0696	3.5	2238	1772	3476																																	
		Afterbo		343.16 0.				0.00			0 20.609																																	
	<b>\$</b> = 180°			0.8532 34				0.0901			_	-0.7553	0.7213	-0.5666	-0.5357	-0.5050	386	-0.5729	0.5301	0.5745	710	-0.4806	-0.4086	-0.3853	-0.3935	-0.3899	-0.3405	0.3004	6 9	503														
α = 0°		Ę					203						3.13 -0.7						00.01					50.00 -0.3				80.08 80.08																
mfr = 0.68 and α = 0°				187.47							_			. 4	•		_	∞ ;	2 5	2 2	2 2	50	8	8	8	2	æ ₹	3 8	3 =	241														
= fr = 0		Afterbody		0.0086		0.0346	0.0673				0.3371																																	
	• = 0°		ž	343.16	419.13	457.12	507.77	571.70	583.74	596.41	609.07																																	
		Forebody	CP	0.8622	0.8334	0.8171	0.7530	0.0788	0.4938	0.3763	0.3101	0.2216	0.2000	0.4683	0.7225	0.9010	1.0407	1.1367	1.1187	0.10.0	0.8016	-0.8975	-0.8166	-0.6973	0.6504	0.6347	0.5640	0.5705	0.4984	-0.5598	-0.5617	-0.5026	-0.5508	0.4938	0.4071	0.4092	-0.3802	0.3871	-0.3659	0.3476	-0.3031	-0.1626	-0.0493	0.0313
		For	χŢ	187.47	-155.11	-130.84	.106.57	24.2	-58.03	41.85	-33.76	-25.67	11.67	-10.27	-5.13	3,3	-2.05	06.0	<b>3</b> 5	3 5	0.63	1.25	88.1	2.50	3.13	3.75	4.37	300	3 5	8.75	10.00	12.50	15.00	200	30.05	40.00	20.00	90.00	00.00	00.08	0000	10.00	241.85	279.84

TABLE VI. Continued

(f) M = 0.77

		ody	දි	-0.0323	0.033	0.0193	-0.0021	0.0243	0.0606	0.0919	0.1333	0.1933																																					
	٠,	Afterbody		343.16					571.08	583.74	596.41	200																																					
	\$\phi = 180°	d,		1.0658				9090:0-	-1.2262	-1.6215	-1.7410	-1.7855	-1.7897	-1.7683	-1.7414	-1.7128	-1.6997	-1.6310	1.6011	-1.5569	5267	-1.4776	-1.4586	-1.4301	-1.3834	-1.2443	-0.3113	-0.3460	-0.3675	-0.3588	-0.3275	0.2585	-0.1975	0.0615															
g = 0°		Forebody		-187.47 1.				0.00	0.31																								_	241.85 -0															
mfr = 0.40 and $\alpha = 0^{\circ}$							,				_	_									-	_	_	_	7	•	•	۰	1	•	•	2	=	24															
mfr = 0		Afterbody	CP	0.039			0.0016	0.0303	0.0688	0.0979	0.134	0.1940																																					
	,() = <b>(</b>	Aff	×	343.16	41913	457.12	507.77	\$45.76	\$71.08	583.74	\$96.41	609.07																																					
	•	body	CP	1.0676	1 0658	1.0545	1.0373	1.0172	0.9967	0.9711	0.9489	0.9390	0.9373	9410	0.9674	1.0579	1.1405	1.1539	1.1220	0.9761	0.7858	-0.1518	-1.3010	-1.6049	-1.7504	-1.7772	-1.7581	-1.7544	-1.7320	-1.7129	-1.6589	-1.6148	-1.5590	-1.5450	-1.5311	-1.4572	9.14	1041	1760	0.110	0.171	0.3606	0.3860	0.3641	0.3300	-0.2543	-0.1997	-0.0636	-0.0524
		Forebody	X	-187.47	67:171	-130.84	.106.57	90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	-11.97	-10.27	-5.13	3.34	-2.05	0.90	Ó.	0.00	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	200	6.25	7.50	8.75	000	12.50	3.5	2 6	30.02	8 9	5	8 9	0002	80.00	0006	0000	110.00	241.85	279.84
				5 5	2 2	: =	8	25	25	=	72	<b>3</b>																																					
		Afterbody		5 -0.0457								7 0.0784																																					
	= 180°		^	343.16		-		-				609.07											_																										
<b>6</b>	*	Forebody	CP	1.1026	1.0453	1.1270	1.0466	-0.3160	-1.4304	-1.7695	-1.9153	-1.9568	1.9670	1.9274	-1.8769	-1.8424	-1.8483	-1.8153	-1.7912	-1.7557	-1.7279	-1.6324				-1.3547	-0.5923	-0.3572	-0.2736	-0.2894	-0.2869	-0.2385	-0.1931	-0.0697															
end a		For	χŢ	-187.47	75.67	-10.27	-2.05	0.00	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	2.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	20.00	90.00	70.00	80.00	90.00	100.00	110.00	241.85															
mfr = 0.30 and a = 0°		ody	C.	0.0524	0.0496	-0.0397	0.0341	-0.0233	0800:0	0.0107	0.0331	0.0807																																					
E	•	Afterbody		943.16			507.77		80.178	583.74	596.41	609.07																																					
	0 =	A	_		101	•		32707	٠.	٠.		_	1.0429	1.0466	0000	1.1274	1.1531	1.1268	1.0515	0.8400	0.6241	-0.4042	-1.5336	-1.773	÷	-1.9339	-1.9261	-1.9232	-1.8852	-1.8664	-1.8520	-1.8068	-1.7574	-1.7405	-1.7147	-1.6485	1.0017	5,05.1	0626.1-	5057	0.4554	10.0	1012	0.2948	0.2927	2401	-0.1986	0.0788	0.0680
		Forebody		-187.47 1.		. –	_	_	_	_													0.31			F 88.											200												
				<u>~</u> :	? *	. <del>.</del>	0.	ġ	i.	÷	7	£.	7	7	<del>-</del>	_	•	•	•	•	•														_				•	, ,	•	. •	, ,			` ~	Ξ	74	2
		body		-0.0450	0.0314	-0.0521	-0.0439	-0.0432	-0.0290	-0.0167	0.0075	0.0507																																					
	<b>.</b> 0	After		343.16	384.14	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																					
	= 180°	ody	G.	1.1159	10756	1.1422	1.0312	-0.3327	-1.4830	1.7695	-1.9375	-1.9799	-1.9672	-1.9222	-1.8975	1.9020	-1.8988	-1.8512	1.8497	-1.7677	1.7491	-1.7004	-1.6422	-1.6360	-1.5102	1321	-0.5392	0.4196	-0.2827	-0.2600	-0.2761	-0.2155	-0.1752	-0.0730															
g = D		Forebody	χΓ	-187.47	75.67	10.27	-2.05	000	0.31	0.63											10.00										00.06	_	_	241.85															
mfr = 0.27 and α = 0*			_				432	417	320	216	037	365																																					
E E		Afterbody	G.		14 -0.0540				08 -0.0320		·	07 0.036																																					
	°0 = 0		XZ		1,04,14			7 545.76				8 609.07	<i>u</i>	<u>o</u> .	_	7	<b>T</b>	=	<b></b>	2	8	₽:	<b>*</b>		5	2	9.	1	=	2	×	2	=	=	2	<u>o</u>	<b>.</b> .	6. 9	9 4	2 5	5 5	3 2	2 00	. 4	· ×	₹ ≂	: ×2	11	22
		Forebody	Ç		611.1				1.0814												0.5903	0.4629	_		5 -1.933				5 -1.9421										1,3388						_	_			
		F	ΧĽ	-187.47	67:1/1:	130.84	-106.57	90.39	.74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	-10.27	-5.13	-3.34	-2.05	0.0	4.0	000	0.31	0.63	1.25	1.88	2.50	3.13	3.7.	4.37	2.00	6.25	7.50	8.7.	10.00	12.50	15.00	00.7	20.02	90.00	20.05	8 8	20.05	80.00	8	10000	110.00	241.84	279.84

TABLE VI. Continued

(f) Continued

		4	à à	-0.0075	-0.0012	0.0123	16200	0.0024	00910	0.2169	0.2733	0.3450																																		
	8	7. ************************************	X/I.			419.13	21.12	26.76	821.08	583.74	596.41	0.609																																		
			Š	0.9327			1366					-1.2914	.3487	2207	-1.1445	0630	2000	3	0.7458	3	-0.6103	-0.7330	7037	-0.5581	-0.4742	0.4329	0.4254	-0.392	0.3692	0.343	-0.1779	0.0413														
°0 = 0		Powebod	9			0 19:57-								3.13										20.00 -0.				90.00			_															
mfr = 0.61 and α = 0°			Î				•													=		=	_	₹.	æ ;	<b>e</b> r (	8 7	< a	ž ð		Ξ	24														
in in		Afterhody	ට්	•		0.0142					0.2662	0.3345																																		
	ع		χ	343.16	384.14	457.13	507.77	545.76	\$71.08	583.74	596.41	609.07																																		
	•	Forebody	වී	0.9345	0.9363	0.9276	0.8510	0.7998	0.7423	0.6596	0.5832	0.5442	0.4800	0.4899	0,000	0.00K7	1.0264	1.1276	1.1505	1.0835	0.4236	-0.5197	-1.0713	-1.3288	. 2021	126921	4907.1-	0.70	-1.0282	-0.8067	-0.9042	-0.6308	0.6687	0.000	0.6551	-0.5651	-0.4780	0.4522	-0.4310	0.4194	-0.4023	-0.3655	-0.3217	0.2344	200	-0.0352
		Por	ΧĽ	187.47	62.171-	13084	106.57	90.39	.74.21	-58.03	£.83	-33.76	/0.62-	17.07	7001.	1	33	.205	-0.90	4.0	000	0.31	0.63	27	8 6	25.5	27.5	6.72	9	6.25	7.50	8.75	00.0	2 2	17.50	20.00	30.00	40.00	20.00	90.09	20.00	80.00	90.06	0000	241.85	279.84
				£ :	2 :	9 2	22	98	57	8	=	22																																		
		Afterbody	2		0.0079							7 0.3175																																		
	<b>4</b> = 180°		^		384.14							609.07				_		_	_	_	_																									
.0	•	Forebody			0.9247	0.8474	1.1535	0.3088	-0.7289	-1.2481	1.4720	1.4885		4088	-1.3639	-1.3168	1.2972	-1.2074	1.2029	1.1137	1.1364	100		0.4974	0.4470	0.446	0.4177	0.3818	0.3376	-0.2505	-0.1862	0.0486														
and a =		Fo	ž	-187.47	75.67	10.27	-2.05	000	0.31	0.63	1.25		2.12	3.75	4.37	5.00	6.25	7.50	8.75	10.00	12.50	92.5	2.50	20.02	8 8	8.00	2000	80.00	8 06	100.00	110,00	241.85														
$\mathbf{mfr} = 0.54 \text{ and } \alpha = 0^{\circ}$		ody	S.	-0.0135	0000	0.0152	0.0484	0.0928	0.1487	0.1878	0.2370	50.5																																		
Ē	•	Afterbody		343.16	•							/0.500																																		
	9	-		0.9878 3								0.7071	0.6746	0.7137	0.8544	0,7070	1.1064	1513	1163	1.0058	2448	0.8158	5/17	1,306/	1 4433	3	-1.3915	-1.3254	1.3563	1.2637	-1.2005	1.2020	-1.0800	-1.0470	-1.0121	-0.9221	0.4084	0.4489	2.42	0.4330	0.4132	0.3843	0.3337	0.1870	0.0498	-0.0429
		Forebody		-187.47 0.				_			51.45					-5.13			_		_	F 0			5.50							27.8						40.00		90.00 90.00						
			_		57.	÷	9	œ.	Ļ.	ė,	4	ijĠ	7	· <del>`.</del>	Ŧ	7/	•	٠,٠	Τ	Ψ.	•		-	-			,	•	•,	•	-		2 2	23	11	2	8 9	₹ ;	3	8 8	2 8	8 8	0000	10.00	241	279.84
		Afterbody	g.	0.0146	0.0064	0.0007	0.0299	0.0693	0.1198	0.10	0.12.0	0.4636																																		
		After		343.16	419.13	457.12	507.77	545.76	571.08	583.74	14.000	00300																																		
	= 180°	ody	c C	0.0140	0.7736	0.9326	1.1540	0.1868	0.9405	51/57	1 4039	-1.6113	-1.6085	-1.5333	-1.5311	-1.4802	-1.4160	1.3799	3303	500	5757	1 2100	2017	0.3631	-0.4356	-0.4385	-0.4166	-0.3789	0.3387	0.2545	0.1929	57507														
<b>d</b> α=0°		Forebody	X.	-187.47				_																30.00						_	000	_														
mfr = 0.48 and $\alpha = 0^{\circ}$							8	8 :	25 52	8 5	3 2	2																		_	- '	•														
n F		erb		0.0238	·				38 0.1255																																					
	•0 = <b>•</b>			384.14	•				571.08				3	_	7	_	_		٠.	^ <del>-</del>	o -			,	~			•			<b>.</b> -		_	•	_	_										_
		죨		1.0142	_				0.899				0.7793								0.1203										1.3/48				1.1801	-1.1424	0.3636	0.4216	0.4016	0.4187	0.1870	0.3356	0.2547	-0.1981	-0.0564	-0.0416
		S.	אָל ג	-171.29	-155.11	-130.84	-106.57	90.39	17.4/	41.85	33.76	-25.67	-23.11	17.97	-10.27	-5.13	<b>1</b>	2.05	3.5	\$ 5	3 5	0.63	1.25	88.	2.50	3.13	3.75	4.37	2.00	6.25	05.7	0000	12.50	15.00	17.50	2002	8 8	9 9	8 6	900	80.00	9006	00001	110.00	241.85	279.84

TABLE VI. Continued

(f) Concluded

		۰.	42	19	9 9	£ 63	120	0.2044	<u>\$</u>	34	121																																			
		Afterbody	_			0.0489				0.3034																																				
	\$\rightarrow\$ 180°	¥ 5	343.16	384.14	419.13	507.77	\$45.76	\$71.08	583.74	596.41	609.07																																			
2	<b>*</b>	à à	0.7324	0.5642	0.6365	0.7975	0.9892	0.3160	0.0291	0.2059	-0.2155	-0.2352	-0.1368	<b>₹</b>	9	0.1969	0.563	10777	0.2857	0.3477	-0.3701	-0.3490	-0.3453	-0.3374	-0.3428	-0.3378	Q.	0.3163	-0.2853	-0.2088	0.1401															
<b>nd</b> α = (	1	Forebody VA	-187.47	-106.57	-25.67	-10.27	00:0	0.31	0.63	1.25	.88	2.50	3.13	5.13	5	9.0	9 6	3,5	10.00	12.50	15.00	17.50	20.00	30.00	20.00	00:00	000	80.00	0006	00:001	241.85															
mfr = 0.80 and $\alpha = 0^{\circ}$		<u>ء</u> ۾			0.0265	0.0915	0.1416	0.1999	0.2432	0.2944	0.3602																																			
mfr		Afterbody							_		009:07 0:3																																			
	0 = <b>0</b>	Ī	. ~	_								<u>ج</u> ج	9 3	5 X	07	\$ 6	3 2	5 5	: 8	5	8	10	\$	TI.	7.7	22	. 67	62	8 8	2 5	7 6	2 2	980	49	8	25	3 8	2 2	0 14	28		33.5	8	851	16	켮
		Forebody	_			0.5651									07800					0.9673				8 -0.1677		3 -0.2022		7 -0.1967			0.1120					0 -0.3437		0.3230		0 -0.3378			_	_	5 -0.0291	-0.020
		Fo	-187.47	.171.29	-155.11	190.84	-90.39	-74.21	-58.0	41.85	-33.76	.25.67	-23.11	1671-	17:01-		200	9 0	4	000	0.3	0.63	1.25	1.88	2.5	3.13	3.75	4.37	200	6.25	00.7	0001	12.50	15.00	17.5	20.00	9	3 5	20.0	20.05	80.08	00.06	100.00	110.00	241.8	279.84
		ğ g	0.0075	10100	0.0258	0.0404	0.1337	0.1979	0.2430	0.2990	0.3707																																			
		Afterbody	_			71.76					0.609																																			
	<b>4</b> = 180°		4	_		0.216/	_	-				-0.4309	0.4499	-0.3573	-0.3433	0.3943	0.3170	3 00	0.4193	0.4805	-0.4669	-0.4169	<u>166</u>	-0.3784	704	-0.3706	20	-0.3317	0.2941	-0.2177	0.1396	ì														
v = 0°		ē														300																														
74 and (		\$	-187.47	-106.57	-25.67	-10.27	, ¢	Ó	o	-	_	7	eri (	· ·	•	אימ	<b>.</b>		9 9	12	15	17	50	8	S	8	2	<b>&amp;</b> ∶	8 9	100.00	241.85															
mfr = 0.74 and $\alpha$ = 0°		Afferbody	0000	0.0108	0.0220	0.044	0.1359	0.1956	0.2374	0.2900	0.3576																																			
	్ట	Y Y	343.16	384.14	419.13	507.12	545.76	571.08	583.74	596.41	609.07																																			
	% = 0°	ģ ģ	0.8137	0.8162	0.8071	0.7624	0.5924	0.4980	0.3560	0.1877	0.0915	-0.0312	0.0468	0.000	17471	0.110.0	0.77	1 1340	1981	0.8191	0.0392	-0.4279	-0.4717	-0.4342	0.3158	-0.4890	0.3592	-0.3926	-0.3798	0.3779	0.3827	-0.4228	-0.4857	-0.4896	-0.4460	0.4180	0.3897	0.2007	0.3733	5.363	0.3378	0.2886	-0.2202	-0.1613	-0.0361	0.0245
		Forebody	187.47	171.29	155.11	106.54	-90.39	-74.21	-58.03	41.85	-33.76	_			770	5.5	5 5	90.5	4	000				1.88							) ) (			15.00		20.00		3 8				90.06	100.00	110.00	241.85	279.84
				•				_	•	0	4																																			
		Afterbody				0.035.5		0.1911		0	0.3654																																			
	<b>\$</b> = 180°	¥ 5	343.16	384.14	419.13	457.12	545.76	571.08	583.74	596.41	609.07																																			
్డి	*	Forebody	0.864	0.7569	0.2279	1 0429	0.7204	-0.1416	-0.6537	-0.8111	-0.9375	-0.6772	-0.7102	-0.6102	0.0023	-0.5382 0.4863	200	0.5360	9229	0.5821	-0.6003	-0.5027	-0.4799	-0.4150	0.4051	-0.3894	-0.3832	0.350	-0.3208	0.2265	0.1740															
and α = 0°		For	187.47	-106.57	-25.67	.2.05	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	15.5	3 5	770	9 6	9 9	12.50	15.00	17.50	20:00	30.00	90.00	90.09	00.00	80.00	90.00	00.00	241 85	64.16														
mfr = 0.68 and α		Ą.	1900	0.0047	0.0137	0.0358	0.1247	0.1848	0.2296	0.2811	0.3505																																			
đ		Afterbody	•			457.12 0 507.77 0					0.609																																			
	0 = <b>6</b>			_		0.8303 45						0.2332	0.2204	0.2559	0.4589	ŝ	507	1.0300	1202	0.6850	-0.2259	-0.7487	<u> </u>	738	212	-0.6483	360	685	\$	241	0.4880	E	137	-0.6239	-0.5221	8	0.4334	2 3	-0.4030	0.3741	1000	0.3134	0.2341	-0.1603	0.0418	1327
		Forebody	_													13 0.7653								88 -0.7738			75 -0.6399																			84 -0.0327
		۲ کے د	187.47	-171.29	-155 11	20.5	90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	10.71	5.13	7 6	007	Ý	Ö	o	0.63	-	1.88	2	۴.	e.	4	ń	6.25	05.7	ē	12.50	15.	17.50	2	g ş	<b>?</b> ?	ž š	20.05	80.08	8006	100.00	110.00	241.85	279.84

TABLE VI. Continued

(g) M = 0.79

		à	3 6	-0.0270	0.0288	0.019	0.0043	0.0327	0.0754	0.1089	0.1531	26																																			
		Afterbody	X.																																												
	A = 180°	9	^	_				_		583.74				~	•	_	٠.	_	_		•	_	_		_	_				_																	
ం	•	*	GL CP	1.077	20.0	1.0686	1.1312	-0.0113	<u>.</u>	1.5104		1.6889	1 6602	1.6463	-1.6179	-1.5957	-1.5452	-1.4871	-1.4788	-1.4342	-1.3836	-1.3769	-1.3574	1.3052	-1.1810	0.4674	-0.2822	-0.2978	-0.2978	0.2834	0.2297	90.0															
$\mathbf{mfr} = 0.40 \text{ and } \alpha = 0^{\circ}$		Por	χ	-187.47	78.67	10.27	-2.05	0.00	0.31	0.63	9	2.50	3.13	3.75	4.37	8.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	\$0.00	90.09	70.00	80.00	8	00:00	341.00															
. 0.40 a			. 0.		8 C	2 2	139	ŝ	8	2 3	£ 9	}																																			
Į.		Afterbody	Ç	6 -0.0345						0.1135																																					
	٥	` <b>*</b>	X	343.16	419.13	457.12	507.77	545.76	571.08	585.74	5000																																				
	•	•	දී	1.0793	6,70	1.0677	1.0480	1.0297	01101	0.9853	0.000	0.9487	0.9507	0.9789	1.0702	1.1502	1.1627	1.1381	0.9978	0.8177	0.0949	-1.1910	-1.4984	-1.6355	-1.6656	-1.6564	-1.6390	1.640	1.5941	1.5735	5333	4500	44	-1.4052	-1.3526	-1.3245	-1.3110	-1.1767	-1.0711	0.5476	-0.2885	0.2810	0.36.0	0.2019	0 1840	0.0629	0.0517
		Forebody	ž	-187.47	-155.11	130.84	-106.57	-90.39	-74.21	-58.03	71.76	-25.67	-23.11	-17.97	-10.27	5.13	3.34	-2.05	0.00	÷.0.	0.00	0.31	0.63	1.25	1.88			3.75			67.0			12.50				30.00				90.02		3.62			
				•			•																																					_	-		-
		Afterbody	Ğ	-0.0374	0.0389	0.0418	-0.0335	-0.0217	0.000	0.0234	0.1087																																				
	్డ		χŢ	343.16	419.13	457.12	507.77	545.76	371.08	596.41	60007																																				
	<b>6</b> = 180°	ķ	C.	1.1155			0090'1	-0.2627	4615.1	1 7800	1 8319	1.8404	-1.8157	-1.7757	-1.7535	-1.7232	-1.7013	-1.6683	1.6453	-1.6087	-1.5531	-1.5257	-1.5070	4549	-1.3024	-1.1092	-0.5869	-0.4276	-0.2659	0.2078	0.1450	0.0677															
α = 0°		Forebody		187.47				_													12.50 -1.				30.00 -																						
30 and										_					•	•	Ĭ	-	•	2	22	\$2	2	2	<b>∺</b> ∶	S	8	2	S 8	3 5	3 5	241															
mfr = 0.30 and $\alpha = 0^{\circ}$		Afterbody	පි	0.0489	0.0435	-0.0378	-0.0274	0.0130	0.000	0.020	0.1072																																				
-	°		ž	343.16	419.13	457.12	507.77	545.76	50.1.08	596.4	609 07																																				
	0= 0		c.	1.1163	1156	01111	7660	0888	0600	10551	1.0521	1.0596	1.0612	0810	1.1388	1.1631	1.1390	1.0626	0.8656	0.6316	0.3529	1.4257	.0467	06	1.8013	-1.8035	-1.7992	-1.778	1.7720	2/6/1-	-1 6552	1.6410	-1.6113	-1.5222	-1.5164	-1.4780	1.4542	7,294	-1.1585	-1.0/83	70007	0.3321	-0.2078	0.1848	-0.1576	-0.0714	-0.0627
		Forebody		187.47	_			60.35																					4.37									900						_			
			^	÷ ;	155.11	-130.84	-106.57	Ş, è		4	4	7,	7	÷	÷	٠,	``	٠,٠	7	Ψ.	_	_	•	-	_ '			-, -	4 •	, ,	,		2	12	2	= ;	20	₹ \$	₹ \$	2 2	3 5	2 2	8 8	100.00	110.00	241.85	279.84
		ď	Сb	-0.0451	-0.0437	-0.0483	0.0447	0.0415	0.0203	0.0187	0.0632																																				
		9		343.16				93.79																																							
	= 180°				_							92	20	91	36	38	<u>.</u>	<b>2</b> 2	33	۱ ۶	25	3 :	3	<b>\$</b> 8	3 8	3 8	8:	2;	<u> </u>	3 2	52	4															
%		퉏		7 1.1272				0 -0.3463						5 -1.8116				0 -1.7278				1.5662					0.000		0.5151			·															
a pue /		ě.	×	-187.47	-25.67	-10.27	-2.03	900	190	1.25	.88	2.50	3.13	3.75	4.37	S.00	6.25	8.	8.75	10.00	22.50	5	00.71	20.0	30.00	90.00	8 8	8 6	80.08	200	110.00	241.85															
mfr = 0.27 and α = 0°		òdy	a.	0.0505	-0.0483	-0.0426	0.0368	0.0036	000	0.0162	0.0628																																				
ā		Afterbody		38.36				243.70																																							
	°0 = 0				_						_	78	8	8	3	22	<b>5</b> 5	6	₹ 9	<b>3</b> 3	/ 2	<b>≘</b> ;	2 8	2 8	Ş		3 5	2 8	87.8	3 5	; <b>;</b>	62	יי	67	33	£ 8	2 8	3 %	3 2	2 2	; e	. S	\$	7	8	03	24
		ğ		7 1.1250 9 1.1250	_		7																				D7#67:		37028								-1.4882						_	_	Ĺ		-0.072
		Ē	ž	-187.47	-155.11	-130.84	-106.57	74.21	58.03	41.85	-33.76	-25.67	-23.11	-17.9	-10.27	5.13	r.	-2.05	<b>S</b> C :	<del>2</del> 2	30.0	15.0	0.03	7	8 6	( , ·	2.1.5		, e	2,5	7.50	8.75	10.00	12.5	15.0	06.71	00.02	8.08	9 5	8 8	000	80.00	00:06	100.00	110.00	241.85	279.84

TABLE VI. Continued

(g) Continued

		ybo	Cb	0.0048	0.0184	0.0317	0.0693	0.1192	0.2310	0.2883	0.3618																																				
		Afterbody		343.16				545.76																																							
	<b>6</b> = 180°											449	155	25	<del>2</del>	342	191	8	9	<b>6</b>	<del>\$</del>	465	820	985	738	8	<del>2</del> 5	<u>z</u> :	857	0.3290	96	4 5	ş														
°0 "		Ę		7 0.9471				0.5344										50 -0.8500					50 -0.6850							_		0.1774	_														
l and α		<u> </u>	χŢ	187.47	-25.67	-10.27	-2.05	800	190	1.25	1.88	2.50	3.13	3.75	4.37	200	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	20.00	90.00	000	80.00	80.5	000	110.00	741														
mfr = 0.61 and α = 0°		ody	CP	0.0067	0.0131	0.0328	0.0740	0.1231	0.7263	0.2804	0.3532																																				
8	۰	Afterbody		343.16	419.13	457.12	507.77	545.76	\$81.74	596.41	20,609																																				
	°0 = •	ģ.		0.9504				0.8161				0.4979	0.4936	0.5348	0.6973	0.9269	1.0484	1.1326	1.1637	1.1048	5018	-0.4691	9519	-1.1803	-1.2071	-1.1379	-1.1203	-1.0006	-1.0066	1.0133	84.8	4 5	0.8580	-0.6986	-0.6874	-0.6573	-0.6004	0.4744	-0.4676	0. 440	-0.4316	-0.4182	0.3873	0.3310	-0.1763	-0.0402	0.0311
		Forebody		-187.47 0.				90.39																								P 9					20.00 -0		90.04 0				90.08				
			^	÷ 5	÷	¥.	9	<b>ማ</b> ተ		, <b>4</b>	, ė	?	?	<del>-</del>	Ŧ	•		•	•	1													_	_	_	_	7	m	4	•	•		* 0	` =	:=	. 72	72
		ybod	C	0.0049	0.0084	0.0199	0.0518	0.1011	0.000	0.2617	0.3354																																				
	s.	Afterbody		343.16		457.12	507.77	545.76	571.06	596.41	70.609																																				
	<b>•</b> = 180°	dy		0.9964				0.3835				-1.3884	-1.3495	-1.3386	-1.3066	-1.2924	-1.2053	1.1734	-1.1509	-1.1066	-1.0903	-1.0473	1.0604	1.0091	4088	-0.4450	0.4462	-0.4287	-0.3909	0.3475	-0.2528	0.1856	0.0455														
ر الا		Forebody		-187.47 0.				0.00																20:00									.41.85 -U														
mfr = 0.54 and $\alpha \approx 0^\circ$						•														-	_	_	_	~	•	•	•		•	5	≌	= ?	7														
mf		Afterbody	C	0.0143	0.0037	0.0213		0.1040	0.000	0.2010	0.3228																																				
	.0 <b>#</b>		ž	343.16	419.13	457.12	507.77	545.76	27.1.00	596.41	609.07																																				
	•	Forebody	C	0.9977	0.9928	0.9744	0.9385	0.8969	0.838	0.7485	0.7231	0.6894	0.6894	0.7283	0.8615	1.0339	1.10	1.00	1.1284	1.0160	0.2856	-0.7672	-1.1774	-1.3829	-1.4077	-1.3744	-1.3517	-1.3237	-1.3018	-1.2660	-1.1806	-1.1357	1.1473	1.0570	-1.0783	-0.9968	1.0040	0.4010	-0.3974	-0.4225	0.4431	0.4319	-0.3953	0.350	0.2304	0.0476	-0.0410
		Fore	ž	-187.47	-155.11	-130.84	-106.57	90.39	17.57	28.03	33.76	-25.67	-23.11	-17.97	-10.27	-5.13	3,34	-2.05	8	<u>4</u>	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	200	6.25	8, 1	× 5	12.50	15.00	17.50	20.00	30.00	40.00	20.00	00.00	00.00	80.00	9.00	900	241.85	279.84
				<u>ش</u> ،	4 a⊊	<b>Q</b>	₽	<b>5</b> 9	2 2	. 4	=																																				
		Afterbody		0.0093					6761.0																																						
	= 180°		ΧΓ	343.16	419.13			545.76																																							
ం	•	Forebody	Ç	1.0276	0.7905	0.9362	1.1666	0.2309	40.8439	1.4911	1.4955	-1.5134	-1.4872	-1.4636	-1.4140	.1.3978	-1.3320	-1.2887	-1.2747	-1.2265	-1.1819	-1.1875	-1.1811	-1.1221	-0.8945	-0.3534	-0.4095	-0.4175	-0.3908	0.3442	-0.256	0.1924	-0.0524														
= υ pue		For	ž	187.47	25.67	.10.27	-2.05	0.00	5.0	1.03	88	2.50	3.13	3.75	4.37	5.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	20.00	90.09	0.00	80.00	800	100.00	110.00	241.85														
mfr = 0.49 and $\alpha$ = 0°		ф	C.	-0.0175	-0.00114	0.0152	0.0462	0.0868	0.1422	0.1789	0.2955																																				
Ę II		Afterbody			419.13 - 0					585.74 U																																					
	0 = 0	-			1.0302 38			0.9498 54		0.8755			0.7881	0.8274	0.9517	1.0821	1.1467	1.1617	1.0988	0.9576	0.1476	-0.9183	1.3119	-1.4949	-1.5042	-1.4839		-1.4382	-1.4144	-1.4024	-1.3616	820	1.2524	1 2119	1.1978	-1.1254	-1.1400	-0.9470	-0.3851	-0.3473	-0.3959	-0.4099	-0.3997	-0.3434 0.3636	0.2625	0.1884	0.0445
		Forebody																	0.00			0.31 -0.9										7.50 -1.2			15.00		20.00					70.00 -0.4			00:00		
		124	×	-187.47	-155.11	130.84	106.57	90.39	17.47	-58.03	-33.76	-25.67	-23.11	-17.97	-10.27	Αż	ΨÝ	-5.	Ġ.	Ģ	0	0	0			7		eri	4	5.	ø	1	eo g	3 2	: 5	17	20	8	€	30	8	2	ဆွ ဆ	⊀ 5	₹ 5	7 7	27.2

TABLE VI. Continued

(g) Concluded

			å ç	22 0.01 27	0.0193	0.0380	10000	0.1552	0.220	72674	0.3216	0.3904																																		
			Afferbody		_	419.13					596.41																																			
		- 180°	à g	0.7442	0.5804	0.7652	0.8178	1.0272	0.3747	0.0637	-0.1585	-0.1093	-0.2118	0.1400	0.1482	-0.1359	7.1788	0.000	0.77.0	2868	0.3610	3.3789	-0.3551	-0.3293	-0.3344	-0.3447	-0.3698	3459	-0.3400	0.2888	0.1466	0.1433														
$mfr = 0.80 \text{ and } \alpha = 0^{\circ}$		2	VA CD	_		. 25.67									5.5						12.50				30.00					8.8																
= 0.80 ar		,	ě			0.0326	00010	0.1527	0.2169	0.2581	0.3090	0.3754																		•			ı													
-ţu		Amount	X/I			419.13 0.0			571.08 0.2			609.07 0.3																																		
		) 	>		_								1.7	5 ;	5 6	2 2	3 3	. 2	! 35	. 25	19	41	11	77	21	11	10	ę:	x :	\$ 2	3 2	. <u>.</u>	<u>6</u>	24	<b>1</b>	≘ :	2 :	<u> </u>		92	9.	=	<b>3</b> . 1	<b>-</b> ,	•	<b>T</b> -
		Porehode	ָרָ בְּיִבְּיִבְּיִבְּיִיבְיִיבְיִיבְיִיבְיִ			84 0.6769			21 0.3385					0.720				25 0.8172							18 -0.1321				0.1525			5 -0.3016														0.0129
		_	X	-187.47	-171.29	130.84	90	-90.39	-74.21	-58.03	41.85	-33.76	79:07	11.62	10.27	115	7.	-2.05	06:0	4.0	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	8,4	7.50	8.75	10.00	12.50	15.00	17.50	20.02	80.00	20.00	90	70.00	80.00	00:06	00:00	10.00	279.84
		Afterbody	ð	0.0132	0.0157	0.0329	0.0902	0.1477	0.2121	0.2613	0.3170	0.3868																																		
	٥		ž	343.16	384.14	457.12	507.77	545.76	571.08	\$83.74	- 56 - 4	609.07																																		
	- 180		5	0.8237	0.6928	0.2691	96260	0.8631	0.1053	-0.3570	0.4854	0.4874	5 6 7 6	0.304.0	-0.3503	0.3651	-0.3437	-0.4121	-0.4542	-0.4336	-0.4885	0.5085	-0.4408	0.4161	-0.3667	-0.3922	0.3823	0.3771	-0.3480 -0.3480	0.2230	-0.1573	-0.0249														
nd a = 0		Forebody	χ	-187.47	106.57	-10.27	-2.05	0.00				86.5						7.50	8.75								90.8				_	241.85														
mfr = 0.74 and $\alpha = 0^{\circ}$		ψ	2		0.0128	0.0495	0.0887	0.1441	660	0.2512	0.5048	0.5727																																		
見		Afterbody			419.14					_		0.60																																		
	.0 •	, -	×		0.8190 41	-							. 185	5	0.2619	916	573	ŝ	313	1.1644	8	2	28	2 3	3 9	8 5	<u> </u>	3 5	<b>.</b>	8	82	86	87	2 :	. ×	: E	: E	æ	11	86	2.5	2;	= 1	2 2	: =	<b>. 2</b>
		Porebody	XILC					_		-58.03 0.3		•		_							_				1.65 -0.4253	2.12 0.3400								3. C. 4868								0.3470				
			×	-187.47	11551-	130.84	-106.57	\$ i	-74.2	<u>چ</u>	7 -	3 %	-23.11	-17	÷	÷	Ę.	-7	9	9	0	<b>5</b> (	σ.		-i -	, ,	ń ~	•	fwi	•	7.	œ	00.01	8.5	2.5	2000	30.00	40:00	20:00	00:00	20.00	80.00		801	241.85	279.84
		Afterbody	č	0.0123	0.0274	0.0396	0.0838	0.1367	0.2042	0.2513	0.300	0.3/20																																		
	<b>80</b> °	Afte	X	343.16	419.13	457.12	507.77	545.76	571.08	585.74	2000	10.200																																		
ę.	H	Forebody	CP	0.8862	0.2599	0.4923	1.0767	0.7100	641.0	0.7159	0000	0.7940	-0.7998	-0.6451	-0.6067	-0.5082	-0.5062	0.479 10.791	0.5764	0.5758	0.6224	7 6 6 6	0.0019	0.770	0.4230	04170	0.4063	-0.3593	0.3223	-0.2311	0.1686	-0.0454														
mfr = 0.68 and $\alpha = 0^\circ$		Fore	χZ	-187.47	-25.67	-10.27	-2.05	90.0	50	20.0	8	2.50	3.13		4.37						0.72		8 8		8 5		0002			_	_	241.85														
r = 0.68 s		d,	CP CP	0.0025	0.0216	0.0417	0.0824	0.1363	040	0.2434	0.3682	•																																		
Ē		terb		343.16 -0				543.76			_																																			
	0 = <del>0</del>			0.8852 34			30 7777						0.2333	0.2611	0.4832	0.7630	02160	389	1.1380	087	55.	4/8/7	-0.8432	08280	0.5466	-0.6062	-0.5728	-0.5399	-0.6019	366	0.4414	210	-0.0106	0.6665	824	103	861	155	2 :	60 5	Ç 2	162	550	558	Š	\$0 <del>\$</del>
		ş		-187.47 0.8		-130.84 0.8														1.1 WO					2.50 -0.5			4.37 -0.5			_	8.75		15.00		20.00 -0.5103				00 -0.4269			_	_		.84 -0.0504
			~ ;	? ?	-155.11	₹.	<u> </u>	¥ 1,		, <u>4</u>		7	.7	7	÷	•••	7 '	7 (	γ °	• ب				_	7	٣	m	4	S	۰	,	** 5	2 2	5	17.	20	8	40:00	S, (	800	ē ģ	90.06	00:00	110.00	241.83	279.84

TABLE VI. Continued

(h) M = 0.82

		Ď.	CP -0.0195	-0.0233	-0.0139	5,000	69#00	0.0926	0.1278	0.1732	0.2379																																						
		Ę	343.16			71.12					0.609																																						
	<b>4</b> = 180°					_						759	220	380	3 :	913	248	36	673	<del>2</del>	-1.3089	917	265	274	163	877	25	385	-0.2753	-0.2010	-0.1570	-0.1260	-0.0510																
% •		ě	2 C		_		_	•																								_																	
0 and a		GE.	X/L	-106.57	-25.67	77:01-	000	0.31	0.63	1.25	88.	2.50	3.13	÷ ;	4.57	89	6.25	7.50	8.75	00.00	12.50	15.00	17.50	20.00	Š	20.00	90.00	70.00	80.00	90.00	100.00	110.00	241.85																
mfr = 0.40 and $\alpha$ = 0°		body	<b>CP</b>	-0.0247	-0.0167	0.0036	0.0545	0.0964	0.1299	0.1711	0.2375																																						
8		Afterbody	<b>X</b> X.	384.14	419.13	507.72	545.76	\$71.08	583.74	596.41	609.07																																						
	°0 = ◆	dy	و او د	1.0935	1.0932	0647	4	1.0261	1.0013	0.9779	0.9715	0.9677	0.9700	0.999	828	1.1630	1.1778	1.1458	1.0108	0.8347	-0.0438	-1.0987	-1.3956	-1.5329	-1.5591	-1.5278	<u>-</u> .	-1.5206	-1.5131	-1.4807	1.4235	-1.4068	-1.3751	-1.3489	- 3049	-1.2751	9007.1-	9067.1.	2671.1-	7.007	0.000	1506.0	0.4534	2102.0	2017.0	-0.1021	0.00	2000	2
		ě	X/L			130.84			-58.03																		3.13			5.00								0007											
			7	÷	÷:	7 5	ָּי <sup>ָ</sup>	• • •	٠,	7	7,	٠,٠	•	•	•																														-			• •	•
		body	CP -00332	-0.0391	-0.0353	0.0367	-0.022	0.0176	0.0418	0.0705	0.1325																																						
	å	Afterbody	7 K	384.14	419.13	457.12	£ 22.2	571.08	583.74	596.41	609.07																																						
	<b>\$ = 180</b> °	γþγ	<u>ට</u> දි	1.1122	1.0721	1,1523	0.1883	-1.2196	1.5450	-1.6759	1.7140	-1.7249	1.7084	-1.6793	1.0449	1.6364	1.6001	-1.5579	-1.5306	1.5150	-1.4686	-1.4211	-1.4161	-1.3618	-1.2323	-1.0503	-1.0105	-0.8805	-0.4347	-0.3577	-0.2086	-0.1558	-0.0515																
<b>1</b> α=0°		Forebody	X7.			10.27	_			1.25																			. 00:08	_	_	_	. 41.85																
mfr = 0.30 and $\alpha$ = 0°								1 20	∞	11	9																				_	-	7																
##		Ę	CP			80600-2				1 0.0737	7 0,1276																																						
	°0 = 0	¥	% K	384.14	419.13	457.12	545.76	571.08	583.74	596.41	609.07																		_							_	_					_					_		_
	•	Forebody	CP -	1.1311	1.1294	1.1250	1036	1.0928	1.0792	1.0707	1.0668	1.0710	1.0732	1.0965	1.1500	1.1785	1.1525	1.0916	0.8982	0.6810	-0.2816	-1.3119	-1.5472	-1.6676	-1.6952	-1.6980	-1.6785	-1.6768	-1.6530	-1.6362	-1.606S	-1.5496	-1.5475	-1.5042	1.4729	4439	400	3048	-1.2552	-1.1183	-1.0383	0.980	1756.0	0.429	0.3454	0.2111	0.000	0.000	7,000
		For	XL 747	-171.29	-155.11	13084	500.5	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	76.71-	-10.27	-5.13	7	-2.05	-0.90	6 4	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	2.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	90.05	30.05	30.05	90.00	800	90.00	00.00	10.00	20.00	73084	17.71
		_	۸. 🕳	28	.58	8 5	e 2	8 8	27	121	<del>5</del>																																						
		f	45 C			0.0400				11 0.0321	0.0840										`																												
	= 180°		X X			457.12			2 583.74		-	4	S	DO -	_	8	7	*	<b>~</b>	•	_	4	9	٥	4	2		9	_	99	9	9	22																
٩	•	Forebody	2 S	_			0.2801																								Ċ	·	6 -0.0783																
and a		Fo	XL	-106.57	-25.67	-10.27	CO.7	0.3	0.63	1.25	88.	2.50	3.13	3.75	4.37	2.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	30.00	00:09	70.07	80.00	00:06	100.00	110.0	241.85																
mfr = 0.27 and $\alpha$ = 0°		ody	CP CARO	0.0445	-0.0421	0.0365	68700	09000	90100	0.0341	0.0823																																						
ā		Afterbody	XI.				507.77			596.41	10.609																																						
	() = ()	٠	CP				1.1243					1.0960	1.104	17117	1.1618	1.1494	1.1133	1.0323	0.8077	0.5963	-0.3665	.1.3775	-1.5765	-1.7156	-1.7343	1.7500	-1.7412	-1.7220	-1.6869	-1.6787	48	-1.6052	-1.5888	-1.5642	-1.5172	-1.5022	-1.4564	-1.4238	-1.2693	1.1676	1.0815	-1,0232	0.9801	0.5121	0.3720	0.2864	j. 104	0.0832	4).07.09
		Forebody			_														0.90		0.00		0.63 -1.					3.75				7.50					17.50 -1		30.00		20.00							241.85	
			X X	171.29	-155.11	130.8	106.57	¥ 7.	. 87	7	£.	-73	7	÷	÷	-,	Ÿ	۲۰	۲	~	٦	٦	٦	_		. •	. ,		1		_	**		=	_	-	-	~	e	4	<b>σ</b>	•	- 1	DC (	<b>3</b>	2 :	= :	7 5	7

TABLE VI. Continued

(h) Continued

		ody	5	0.0066	0000	0.0396	0.0908	0.1361	0.2013	0.2512	0.3084	0.3823																																			
	2	Afterbody		343.16		457.12	11.108	\$45.76				00.60																																			
	φ = 180°	ķ	c G	0.9598	0.5200	0.7195	1.1417	0.5918	-0.3323	-0.8526	0.0800	1.1580	20017	1.0768	6220	-0.9762	18871	.8793	.7893	.8113	1917	.7583	(1322	6788	4976	889	0.4549	107	<u></u>	96.5	0.710	0.0375															
0 = 0 E		Forebody		187.47								2.05					6.25 -0	7.50											_	90.00		241.85															
$\mathbf{mfr} = 0.61 \text{ and } \alpha = 0^{\circ}$							88	٤ ;	ec .	<b>x</b> 3	2 2	=												•	•						=	. 2															
mfr.		Afterbody		0.0066				6 0.1329		_																																					
	% = 0			7 384 14				_	_	583.74				9	90	2	<b></b>	•		_	•	~	~	_	_	•					. ~		_		_			_		_	_						
		rebody		0.9637						0.6954									1.1700			-0.4872		-1.1469			0.0789			7000	0.7969	-0.8636	-0.8393	0.8072	0.7657	-0.8397	-C. 7087	0.5354	0460	-0.4623	0.4499	-0.4211	-0.3517	-0.2456	-0.1692	-0.0383	-0.0279
		Pe	X	-18/.47	-155.11	-130.84	-106.57	603	7.4/-	-58.03	2 2	.25.67	-23.11	-17.97	-10.27	-5.13	.3.3¥	-2.05	8 9	Ġ	000	0.31	0.63	1.25	1.88	R :	3.13		£ \$	20.00	7.50	8.75	00:00	12.50	200	17.50	00.07	9 9	900	90.09	70.00	80.00	90.00	100.00	110.00	241.85	279.84
		ody	<b>G</b>	-0.0025	0.0121	0.0224	0.0612	0.1103	0.1/43	0.2224	0.3552																																				
	ጷ	Afterbody	X,					545.76		596.41																																					
	<b>6</b> = 180°				•			16291					.1.2723	-1.222.1	-1.2119	-1.1821	-1.1356	-1.1135	0880	1.0511	-1.0243	282	656	2000	9009	0.3327	-0.3%22	04131	0.3530	0.2432	0.1746	0.0374															
d a = 0°		Forebody	Z Z	_				900															17.50							_	_	41.85 -0.															
mfr = 0.54 and $\alpha$ = 0°							2 5	8 5	3 9	8 =	: =													•	., •	. •	,			. =	=	77															
mfr.		ţe Ţ	<b>3</b> 5					8 0.1138																																							
	% •	<b>*</b>	XX XX					571.08			_		\$	-	<b>~</b>	9					v .		٠.		<b>.</b> .					. •		7							_	_	_	_					_
		Forebody	. C				DCCC-0										1.1297		1.1461				4								-1.0693		-1.0427		71.00		0,0						-0.3516		0.044	7.00	è
		<u> </u>	X/L	-171.29	-155.11	130.84	6.00	-74.21	58.03	41.85	-33.7	-25.67	-23.11	-17.97	-10.27	·5.13	Ę.	-2.05	<b>5</b>	<b>3</b>	3 6	50	0.03		, c	-	3.75	4	20.5	6.25	7.50	8.75	10.00	20.51	3 5	20.02	30.00	40.00	\$0.00	90.00	70.00	80.00	888	8 6	741.85	270 84	
		Afterbody	-0002	-0.0072	0.0056	0.0119	2000	0.1505	0.1970	0.2493	0.3228																																				
	.08	Affer	343.16	384.14	419.13	457.12	201.10	571.08	583 74	596.41	70.609																																				
	<b>6</b> = 180°	ody S	2 6	0.9944	0.8054	0.9607	71.0	0.7691	-1.1465	-1.3840	-1.4096	-1.3936	-1.3724	1.3530	93199	2336	55077	/1771	66.	966	0/00	200	90001	0.000	0.6816	0.3051	-0.3623	-0.3343	-0.3209	-0.2449	0.1781	0.0458															
nd a = 0°		Forebody	-187.47	-106.57	-25.67	-10.27	8 8										9 6				2 20 21		200									241.85															
mfr = 0.49 and α		<u> </u>			0.0025	0.0181	0.0078	0.1550	1945	0.2465	0.3137																																				
a f		Afferbody	۰			00 71.70					.0 09:00																																				
	•	•	2 E	_		0.9964						070	8	55	760	1,0983	1741	1 1067	9 5	Ş <u>Ş</u>	22	260	Z Z	Ž	3	519	151	113	125	552	<u> </u>	60	9 9	9	22	133	19	174	98	æ :	<u> </u>	3 5		9	38	8	
		rorebody V/I		_		_										2.5					٠				2.50 -1.38	13 -1.3619				6.25 -1.26			50 -1.1180									0.00				_	
	•	>	-187.47	-171.29	-155.11	106.57	6.06	-74.21	-58.03	41.85	-33.76	25.67	-23.11	1671-	2 •	ų.	,	4 9	9	•	0	Ö	نہ ہ		7		<u>د</u>	4,	٠,	ģ	۲.	só è	12.50	15.	-	20.	ĕ	₹	Š	90.00	5 8	8	2 2	1000	241.2	279.84	

TABLE VI. Continued

(h) Concluded

		ody	و د	0.0279	0.0477	0.0619	0.1108	0.1083	7848	0.3392	0.4064																																			
		Afterbody	X.					52.70																																						
	<b>4</b> = 180°											<b>4</b> 56	<b>3</b> 3	939	8	200	120	436	666	113	150	740	417	421	-0.3809	-0.3759	835	451	0.30/9	127	5 5 5	?														
= 0°		ā	65 5 5			,		0110.1 0						7 - U. 1398																	20170															
9 and a		<u> </u>	X	106.57	-25.67	-10.	-2.05	0.00	0.53	1.25	1.88	2.50	3.13	2.73	٤	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20	30.00	20.00	90.09	20.00	80.08	80.05	0000	241 85															
mfr = 0.80 and α = 0°		ody	<b>G</b>	0.0262	0.0418	0.0654	0.1122	0.10/0	0.2751	0.3295	0.3929																																			
B	•	Afterbody	Z Z	384,14	419.13	457.12	207 77	545.70	583.74	596.41	609.07																																			
	•0 •		a i	0.7516			0.5909	0.4811	0.3320	0.0846	-0.8572	-0.7163	-0.6580	5,47,5	0.4370	0.6525	0.8697	8060	.1663	06660	0.3408	-0.0020	.0693	-0.1139	-0.1450	-0.1792	0.1655	0.1846	061	2471	0.1980	3096	-0.3937	-0.3674	3916	0.3530	-0.3203	0.3612	-0.3918	-0.3812	-0.3622	-0.3117	0.2176	0.1453	-0.0228	0.0112
		Forebody	XI.					3421						1671							0.31 0			1.88 -							2 2				17.50							_	_			279.84
			•	;	<u>.</u>	÷	÷.	? "	7	, 4	**	'7'	.,	•	7																											-	_	- 1	Ċ.	7
		body	a 3	0.0210	0.0377	0.0522	0.1034	0.1602	0.2283	0.3363	0.4045																																			
	ప్	Afterbody	Z ;	384,14	419.13	457.12	507.77	52.70	583.74	596.41	609.07																																			
	081 = 0	dy	CP CP	0.7107	0.0194	0.2697	1.0017	0.8832	13701	0.4878	-0.5010	-0.4019	-0.3703	0.3483	0.3547	0.3163	0.1712	-0.4710	-0.4452	-0.4341	-0.5575	-0.5491	0.4770	-0.3904	0.4073	-0.4184	-0.4157	0.3789	-0.3176	-0.2257	5 C C C	0.00														
ο <b>*</b> α		Forebody	χ		·			900						6.5																	00.011															
mfr = 0.74 and $\alpha$ = 0°								9 9	R 1	2 22	2																				- (	•														
mfr =		Afterbody		0.0080				0.1626																																						
	.0 = <b>0</b>		X	384.14	419.13	457.12	507.77	545.70	59174	596.41																																				
	•	Forebody	<u>ئ</u> د	0.8447	0.8335	0.7917	0.7141	0.6248	0.3278	0.2086	0.1116	0.0079	-0.0519	0.0161	0414.0	0.8167	80.00	1.1472	1.1781	0.8606	0.1055	-0.3633	0.3470	-0.3790	-0.2907	-0.3732	-0.3385	-0.3739	0.3732	0.3749	0.3231	0.5090	0.4544	0.5590	-0.5148	0.4191	0.3809	0.4010	0.4147	0.4211	-0.3779	-0.3231	-0.2224	0.1597	0.05	-0.0151
		For	3 3	-171.29	-155.11	-130.84	106.57	90.39	4.21	41.85	-33.76	-25.67	-23.11	/6/1-	27.5		20.6	9	4.0	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	900	6.25	2 2	10.00	12.50	15.00	17.50	20.00	8 8	3 6	8 8	70.00	80.00	90.00	100.00	110.00	241.85	279.84
			_ :	<b>2</b> 23	. œ	63	1 :	2 8	3 5	3	. 8																																			
		Afterbody		4 0.0152		2 0.0463		0.1530																																						
	<b>4</b> = 180°		^ ;	384.14	•		_	545.76			_	_									~	~	<b>د</b>		•	<b>ac</b>		0	~																	
8	•	Forebody		0.7983		0.5256			0.0830						0.0007																0.139	2.0														
∎ pue		Fo	χ	-187.47	-25.67	-10.27	2.05	0.00	0.51	1.25	1.88	2.50	3.13	3.75	2 5	3,5	5	8.75	10.00	12.50	15.00	17.50	20.00	30.00	20.00	90.09	70.00	80.00	8	00:00	110.00	C0.14.7														
mfr = 0.68 and α = 0°		χqχ	G.	0.0027	0.0297	0.0508	0.0941	0.1523	0.2171	13143	0.3866																																			
Ē		Afterbody		38.16					80.172																																					
	0 #		_ ;	0.9058					0.000.0			0.2838	0.2705	0.2987	0.5202	0.000	\$2201	1,1697	1545	0.7035	0.2009	-0.5946	-0.8263	-0.8379	-0.8137	-0.6161	0.5840	-0.5530	-0.5342	-0.5250	0.4189	10,500	0.6171	-0.6376	01.6710	0.6600	0.4449	25.0	0.4437	0.4350	0.4065	-0.3285	-0.2402	-0.1634	-0.0386	-0.0242
		Forebody														3.74						0.63 -0.5	1.25 -0.8			3.13 -0.0				6.25 -0.5					17.50 -0.0		30.00		20.00					_		279.84 -0.0
		_	×	187.47	-155.11	-130.84	-106.57	-90 39	14.21	-58.03	33.76	-25.67	-23.11	-17.97	77:01-	, ,		4 9	ç	, 0	0	0	_	-	7		•	4	•	٠	,- 6	- 2	: 2	15	-	z :	¥ \$	f i	ಗ ೪	5 8	. ×	×	Σ	ĭ	24	27.

TABLE VI. Continued

(i) M = 0.84

		ody	පි	0.0133	0.0063	0.0029	0.0229	0.0594	0.1049	0.1438	0.1891	0.2547																																		
	8	Afterbody		384 14					571.08			203.07																																		
	<b>6</b> = 180°	Ą	g :	240	0.9806					_		1.4680	7764	1445	4262	-1.4043	-3.3484	3379	7667	2703	-1.2214	-1.2114	-1.1858	-1.1709	0715	-0.9176	8972	0.8098	0.8620	0.355.0	1331	-0.0362														
l α = 0°		Forebo		187.47	_							88.1									12.50 -1.		17.50				90.00					41.85														
mfr = 0.39 and $\alpha$ = 0°										4.	<b>.</b>	5								_	-	_	_	2	•	•	•		**	• =	? =	7.														
mfr =		Afterbody		4000	•			5 0.0641																																						
	°0 =	7	X.		•	•	507.77	545.76			390.41	_																																		
	•	Forebody	G C	1.106	1.1034	1.0939	1.0761	1.0581	1.0381	1.0131	2000	0.9823	0.9869	1.0128	1.0890	1.1758	1.1862	1.1568	1.0195	0.8566	0.0408	-1.0380	1.3154	-1.4438	1.4590	1430	1.4576	4340	1 3761	1 36 16	-1.3203	1.3084	-1.2718	-1.2421	1.2122	1.1833	1.101.1	0.000	-0.9281	-0.8929	-0.8705	-0.8051	-0.3352	-0.2312	0.1403	0.0374
		Por	XZ.	171.29	-155.11	-130.84	106.57	-90.39	74.21	-58.03	2 2	25.67	-23.11	17.97	-10.27	-5.13	ė,	-2.05	06:0-	0 4	000	0.31	0.63	1.25	88.7	05.7	3.15	4.37	<u> </u>	6.25	7.50	8.75	10.00	12.50	12.00	17.50	8 8	8 8	0005	00:09	00.00	80.00	00.00	00:00	241 96	279.84
		ody	<b>C</b>	-0.0308	-0.0264	-0.0291	·0.0164	0.0020	0.0308	0.000	0.0914	0.140																																		
	ዾ	Afterbody	֓֞֞֝֟֝֟֝֓֓֓֟֝֟֝֟֟ ֓֞֓֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞							583.74		10.50																																		
	<b>081 = </b>	ý						0.1575		7697			1.6090	1.5907	-1.5584	-1.5381	2011	-1.4769	4482	4172	-1.3672	320	3272	-1.2849	56.1.7	100.1	0.3078	0380	-0.5028 -0.5028	0.3990	0.3307	0.0360														
π = 0°		Forebody	X/L					_		1.05												15.00			7 ·						_	241.85 -0.														
mfr = 0.30 and α = 0°								۰,	٠,	e =	- 4	,								_	_	-	- (	7 .	~ •	n 4		· •		9	=	54														
= H		Afterbody	- C					0.0070		0.0336																																				
	ų, 0			_				_	27.1.00						_	_																														
	·	Forebody	. 5. 5.					2011	200	0.00	0.00	1.0846	1.0905	1.1112	164	1.1859	1.1619	1.0913	0.899	0.09	0.2511		7604.1-	10/01-	0007	600	.1.5748	.1.5666	-1.5338	1.5038	1.4790	1.4592	-1.4338	2	75001	1 3058	1761	-1.0783	-1.0045	0.9639	-0.9574	0.9256	0.4894	0.3521	0.0418	-0.0438
		€ ;	X/L -187.47	-171.29	.155.11	20.5	-106.57	803	7.47	28.45 84 85	31.76	-25.67	-23.11	17.97	-10.27	÷.	<b>X</b>	50.7	S :	4 5	33 3	0.5	. C.	9 8	8 5	3 .	3.75	4.37	200	6.25	7.50	8.75	900	2 2	3 5	2000	30.00	40.00	20.00	90.00	70.00	80.00	8 8	1000	241.85	279.84
		Afterbody	1689 1689	-0.0362	-0.0345	-0.0352	0.0283	0.00	0.000	0.0283	0.1074																																			
	.08	Affei	343.16	384.14	419.13	457.12	200	571.08	\$93.74	596.4	609.07																																			
	• = 180°	g g	1.1525	1.1381	1.1116	6771.1	1003	40.1979	1 4778	6865	6402	-1.6487	-1.6379	-1.6203	-1.5746	-1.5637	7667	7/101	-1.4965	600	C714.1-	9/6:-	2262	1 2007	10174	0.9886	-0.9412	-0.9405	-0.7423	-0.4118	-0.3686	-0.0321														
mfr = 0.27 and α = 0°	,	Forebody	187.47	106.57	-25.67	-10.27										90.5					00.21				900				_	00.00	_	241.85														
- 0.27 aı		× 6	•		308	5 50	85	<u> </u>	. 2	€ €	<b>\$</b>																			_	_	. •														
į.	,	Afferbody	Ÿ			12 -0.0305		•																																						
	.0 = <b>0</b>	>	_		-	70 457.12					54 609.07	_	23	<b>.</b>	ς.	= 1	2 3	2 1	3 5	2 3	ŧ 9		2 55		مِ ج	•	Į.	9	=	ž	9	90 °	y (		, .	•	2	60	6	• •	י פ	٠.	0 00	, ~	•	<b>80</b>
		rorebody	7 1.1500	_		7 1.1470								7		11811					00.25												1.4086								0.9553		_			
		2 >	-187.47	.171.29	-155.11	20.8	00.00	.74.21	58.03	41.85	-33.76	-25.67	-23.11	17.97	-10.27	5.5		9 9	9	2	3 5	690	2 2		2.50	3.13	3.75	4.37	9:00	6.25	7.50	8.75	10.00	12 00	17.50	20.00	30.00	40.00	20.00	90.00	70.0K	80.00	0000	110.00	241.85	279.84

TABLE VI. Continued

(i) Continued

		ody	<b>c</b>	-0.0088	9800.0	0.0206	16000	0.10//	0.2202	0.2784	0.3591																																				
	•	Afterbody	<b>X</b>			457.12	77.70	52.75	583.74	596.41	70.609																																				
	<b>0</b> = 180°	Į.						0.43/1				-1.2033	1.1595	1262	-1.1033	-1.0850	-1.0128	1866	675670	0.9250	0.871	8867	-0.8133	-0.6726	0.6148	-0.5388	-0.4517	-0.4257	-0.3642	-0.2570	0.1673	0.0354															
<b>=</b> 2.0°		Forebody					50.7	•		1.25 -1.										00.01									_	_		41.85															
9 and 9			X.	106.57	-25.67	10.27	7.	9 6	. 0	_	_	7	<b>.</b>	•	σ.		, ,		~ ;	2 ⊆	: :	2 52	7	×	×	3	×	×	8	≊	≌ ;	24															
mfr = 0.49 and $\alpha$ = 2.0°		Afterbody	8	0.0032	0.0126	0.0297	0.0002	0.1100	0.1998	0.2423	0.2999																																				
P	సి	Afte	¥ 5	384.14	419.13	457.12	207	\$45.76	583.74	596.41	609.07																																				
	0 = <del>0</del>	ody	<u>د</u>	1.0588	1.0539	1.0388	6000	0.9810	0.9143	0.8805	0.8666	0.8625	0.8603	0.9002	30.1	1.1423	2701.1	1.1813	0880	0.9373	1000	1 2222	-1.3826	-1.3955	-1.3806	-1.3826	-1.3645	-1.3625	-1.3262	1.304	-1.2582	1.2411	1 1866	2002	1.1506	-1.1417	-1.0810	-0.9645	-0.9510	-0.9084	-0.8652	0.4474	-0.2850	0.2014	0.000	0.0397	0.00
		Forebody	<b>X</b>	-171.29	-155.11	-130.84	-106.57	25.35	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	-10.27	5.13	<b>1</b>		_	<b>4</b> 6				88.							_		20.02										_	00.00		241.85	13.04
											_																																				
		Afterbody	a 5	-0.0032	0.0095	0.0186	0.0367	0.1083	0.2161	0.2727	0.3510																																				
	180	Afte	ž ;	384.14	419.13	457.12	207.77	43.76	583.74	596.41	609.07																																				
٠.	<b>\$</b> = 180°	body	සු දි	1.0076	0.8144	0.9518	1.1898	0.3685	1.0296	1.2475	-1.2694	1.2594	1.2234	-1.2082	-1.1/4/	-1.1578	CO11.		1.047	0.9932	0.0813	0.9984	-0.9461	-0.8505	-0.7366	-0.6673	0.6410	-0.3118	-0.2673	-0.2109	-0.1587	-0.0365															
mfr = 0.49 and $\alpha$ = $1.0^\circ$		Fore	ž	-187.47	-25.67	-10.27	-2.05	900	0.63	1.25	1.88	2.50	3.13	3.75	4.51	2,00	0.0	S. 5	S.73	8 9	15.00	2 2	20.00	30.00	\$0.00	00:09	20.00	80.00	00:00	100.00	1000	241.85															
. 0.49 ar			G CB		0.0082	0.0276	0.0061	0.1137	2064	0.2506	0.3152																																				
Ę,		Ě	XX					545.76 0.																																							
	% = 0				•	_					_	9	8	721	S 3	8 3	2 6	2 3	23	8 9	6	3 5	23	63	60	8	<b>2</b>	2	265	<u>\$</u>	787	2	<u> </u>	2 0	33	<u> </u>	152	<u>\$</u>	782	316	112	<del>5</del>	337	210	6 5	775	, 76
		Forebody		06501 6	_			0.9835								900		1.1879		0.9666		90917							00 -1.2592				1691 T 93		50 -1.1233							•				7,50.0- 68	
		2	X	171.29	-155.11	-130.84	-106.57	90.39	-58.03	4.85	-33.76	-25.67	-23.11	17.97	77.01-	5.13	\$ 6 6	-2.05	96.0	4 6	Š	šč	===	-88	2.	6	'n	4	2.00	6.25	7.50	ec i	200	200	2	20.00	30.00	40.00	20.00	00:00	70.00	80.00	90.06	100.00	30.00	241.85	
		ydy	a c	-0.0025	0.0109	0.0223	0.0608	0.1061	3.2128	0.2670	0.3384																																				
		Afterb		384.14				545.76																																							
	<b>\( = 180^\)</b>			2 00001			_	0.3391 S			-	-1.3261	-1.2897	1.2585	7407	1.2154	-1.1/89	1482	83	4.084	9.00	7488	22	204	7826	988	-0.7391	-0.3513	-0.2236	0.1694	-0.1326	-0.0390															
80 × 0		g.			_			000														962							_	_	10.00 -0.																
mfr = 0.49 and $\alpha = 0$ °				18/4/		•	•			_		,,		,	•				_	= :				ian	•	25	~	æ	5	≘	Ξ	74															
mfr = 0		Afterbody	<u>ئ</u> و	0.0103	0.0072	0.0263	0.0619	0.1108	0.10	0.2620	0.3321																																				
	% # ⊕		ጟ	38.15	419.13	457.12	507.77	545.76	583.74	596.41	609.07																																				
	٠	Forebody	<b>a</b>	1.0567	1.0538	1.0353	.0078	0.9775	0.0000	0.8615	0.8475	0.8301	0.8245	0.8578	0.9850	<u>-</u>	100	1.1882	1.1265	0.9980	0.2323	6.713	7841	1.3074	-1.2922	-1.2625	-1.2625	-1,2393	-1,2119	-1.1743	-1.1459	6660 T	6860	6807	1044	85101	0.8905	0.8436	-0.7626	-0.7650	-0.6980	-0.2744	-0.2350	-0.1969	-0.1283	0.0428	-0.0343
		Fore	Z,	187.47	-155.11	-130.84	5.57	-80.39	58.03	41.85	-33.76	-25.67	-23.11	17.97	-10.27	-5.13	4	-2.05	0.00	<b>4</b> 8	3 3	7 7	2 2	80	2.50	3.13	3.75	4.37	200	6.25	7.50	8.75	90.0	25.30	3.5	000	8 8	000	00.08	00:09	00.07	80.00	90.00	00.00	000	241.85	48.6
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TABLE VI. Continued

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		d,	a,	0.0133	0.0277	0.0468	0.0916	0.1479	2169	0.2681	2043	606																																		
		fterbo																																												
	• = 180°		• • •	384.14	•						14.0%				_	_	_			_																										
8	•	Forebody	ð į	0.8949	0.5458	0.7350	1.1557	0.6134	-0.2985	0.7795	1000	10824	0365	0.9505	0.9329	-0.9049	-0.8610	-0.7759	-0.8064	0.790	-0.7681	-0.7577	0.7251	-0.6806	0.6421	-0.5513	0.4424	0.4131	0.4509	200	0.70	-0.0337														
nd a =		For	Z :	-106.57	-25.67	-10.27	-2.05	0.00	0.31	0.63	67	2 6	3.13	3.75	4.37	200	6.25	7.50	8.75	000	12.50	15.00	17.50	20:00	30.00	20:00	00.00	90.02	80.08	3 8	300	241.85														
$mfr = 0.61 \text{ and } \alpha = 0^{\circ}$		<b>&gt;</b>	a, š	0.0110	0.0257	0.0478	90600	0.1502	162	0.2634	9 5																																			
mf		terb									0.3100																																			
	.0 *		ž,		•		_	545.76		583.74			. ~	~	_	_	~	~	_	_	_	_	_	•	_								_	_					_			_	_			
			g 5	0.9816	0.9747	0.9472	0.899	0.8300	0.7959	0.720	0.00	0.5370	0.536	0.5788	0.7398	0.9595	1.0618	1.1536	1.183	1.132	0.544	-0.356	0.8083	1.030	1.026	1.013	0.9960	20/60	0.9237	46.0	0.8228	-0.8119	-0.7931	-0.7730	0.7903	0.750	0.6555	-0.6321	-0.5846	-0.4237	-0.4427	-0.4257	-0.3956	0.2397	0.1044	0.0230
		For	X	171.29	-155.11	-130.84	-106.57	-90.39	-/4.21	-58.03	33.74	25.67	-23.11	17.97	-10.27	-5.13	3.34	-2.05	<b>6</b> 0	Ġ	0.00	0.31	0.63	52 5	E .	200	3.13	5	5.5	3 2	2.50	8.75	10.00	12.50	2.00	2000	30.00	90.0	\$0.00	90.00	20.00	80.00	8	00.00	10.00	279.84
			9	. ×	æ		9	<u>o</u> . 1	- 9	2 9	` <u>'</u>	,																																		
		Afterbody	<b>a</b> §					0.1259			90210																																			
	• = 180°	¥	¥ 5	384.14	419.13	457.12	507.77	\$45.76	80.176	583.74	6000																																			
٠.	H	body	<u>ට</u> දි	0.963	0.7263	0.8957	1.1857	2492	0.000	12.5	2316	1.2232	-1.1782	-1.1708	-1.1437	-1.1174	÷.0460	5	1.025	-0.9585	0.9589	0.9574	90960	0.8650	0.8120	0.7179	0.6574	70000	0.2910	0.7183	0.1559	-0.0377														
mfr = 0.64 and $\alpha$ = 0°		Forebody	XIL	106.57	-25.67	-10.27	-2.05	0.00	5 5	0.03	8	2.50	3.13	3.75	4.37	9:00	6.25	7.50	8.73	0.00	12.50	200	17.50	20.02	90.06	90.00	80.00		8 8	0000	110.00	241.85														
. 0.54 a		_			133	3 5	S :	8 8	3 5	7 6	989																																			
H		Ę				2 0.0354		0.1296		0.2342																																				
	.0 <b>=</b>	₹	ZZ X					545.76			609 07		_	_		_	_			_	_	_		_																						
		Forebody	<u>မ</u> ရိ	60	1.0237	1.0027	0.9672	0.9304	0.0030	0.0357	0.7559	0.7193	0.7230	0.7570	0.8861	0.0510	1398	1.1856	700	1.057	0.3849	0.393	0.9858	1.1930	677.1-	-1.1987	-1.1030	29	000	1.0529	1.0063	-0.9746	-0.9835	0.9964	0.3080	-0.9388	0.8438	0.7491	-0.7113	0.6142	-0.3850	0.3173	0.2309	01480	0.0350	-0.0280
		For	X 781.	-171.29	155.11	130.84	-100.57	50.3	60 03	41.85	-33.76	-25.67	-23.11	-17.97	-10.27	-5.13	٠ ب	-2.05	3	4	800	0.3	60.0	9 8	2 5	2.50	5. L	4 17	9	6.25	7.50	8.75	10.00	12.50	2 5	20.00	30.00	<del>4</del> 0.00	20.00	90.00	00.02	80.00	3 8	3 6	241.85	279.84
			£	20	۳.	<u>-</u> -	2 :	2 0	1 2	2 5	. Q																																			
		erp	CP CP					0.1025																																						
	<b>•</b> = 180°	V	X X	384.14	419.13	457.12	77.100	545.76	261 74	596.41	609.07																																			
<u>.</u>	*	Forebody	C C C	1.006	0.7774	0.9095	1.1833	0.5020	333	1117	.1.1423	-1.1532	-1.0938	.1.0623	1.0090	0.9936	-0.9273	0.8352	600	0.795	20,00	17/7	06.1.5	9700.0	7	7,000	5,4803	218	0.4612	0.2406	-0.1656	-0.0350														
d a = 3.		Fore	X/L	106.57	-25.67	10.27	CO.7-	900	0.63	1.25	1.88	2.50	3.13	3.75	4.37	80.	6.25	9	2.5	800	06.71	3.5	200	9 9	8 8	8 8	900	900	0006	100.00	110.00	241.85														
mfr = 0.49 and α = 3.1°		<b>-</b> 1			9 :	<b>Ž</b> 3	2 5	C %	2	2 2 2	<b>6</b>																																			
mfr =		terbo	2 6			2 0.0304		0.1072																																						
	,0 = <b>6</b>	₹;	343.16 343.16			457.12				596.4																																				
		Forebody	286	1.0573	0550	5.0415	07000	0.9840	0.9217	0.8886	0.8799	0.8736	0.8765	0.9113	1.0326	1.1528	28.	20/17	0000	0.909	0.0798		7.62.1	1 4447	1438	1.4355	1.4200	4 4	1.3972	-1.3585	-1.3304	1.3050	-1.2977	1 3622	1 2267	-1.2074	-1.1116	-1.0497	-1.0185	1904	0.6340	0.4277	12.00	0.1914	-0.0288	-0.0276
		Fon	187.47	-171.29	-155.11	190.84	00.00	74.21	58.03	41.85	-33.76	-25.67	-23.11	17.97	-10.27	5.13		50.7	2 3	\$ 8	3 5	5 6	5 2	88 1	5	113	3.75	4.37	800	6.25	7.50	8.75	000	2.5	17.50	20.00	30.00	40.00	20.00	90.00	0.00	8 8	8 8	110.00	241.85	279.84

TABLE VI. Continued

(i) Continued

		ody	CP	-0.0034	0.0340	0.0528	0.1002	0.1628	0.2354	0.2856	0.3481	0.4224																																				
	°	Afterbody		343.16	419.13	457.12	507.77	545.76	\$71.08	583.74	396.41	609.07																																				
	<b>4</b> = 180°	dy		0.9240			_	0.8954	0.1446	-0.2337	-0.3852	0.2998	3918	-0.3067	01/70	-0.5043	į	2043	2364		0.3321	707	200	0070	-0.413/	4.50G	217	0.4144		0.4422	200	0.22.0	0.0181															
x = 2.0°		Forebody		-187.47 0.				_				O 88.		3.13			900				9 9 200 200 200			200		3 8 8																						
67 and (					_	•						_								•				- ‹	7 (	•	n •		•	ю о	` =	2 =	. 2															
mfr = 0.67 and $\alpha = 2.0^{\circ}$		Afterbody	G	0.0270	0.0384	0.0611	0.1096	0.167	0.2341	0.2782	0.3291	0.3909																																				
-	% = 0°	Afte	×	343.16	419.13	457.12	507.77	545.76	\$71.08	583.74	<b>2</b> 86.4	609.07																																				
	÷		Ç	0.9260	0.9200	0.8849	0.8272	0.7653	0.6961	0.6007	0.5010	0.4498	0.5852	0.3811	0.4330	0.0470	0.5020	1401		200	1.1582	9000	0.3200	00.700	0.000	6666	9/00/1	0.9903		0.9148	0.07	2860	-0.8182	-0.7883	-0.8212	0.8048	0.8120	0.0200	0.6966	-0.6372	-0.4956	-0.3911	-0.3740	0.3317	0.2241	0.03	-0.0224	
		Forebody	ž	-187.47	-155.11	-130.84	-106.57	-90.39	-74.21	58.03	41.85	33.76	19.67	23.11	17.7	7701.	5.15		50.7	2 :	\$ 6	3 6	5.0	60.7	9 8	89.	2.5	3.13		5 6	3 4	9.0	8.75	10.00	12.50	15.00	17.50	30.05	40.00	20.00	00:00	70.00	80.00	80.06	110.00	241.85	279.84	
				9 9	) me	96	Ω.	9	=	<b>S</b>	×	=																																				
		Afterbody		0.0070								0.418																																				
	= 180°		ጟ	343.16	419.13	457.12	507.77	545.76	871.08	583.74	296.41	609.07																																				
<b>o</b> .	•	Forebody	CB	0.9243	0.2882	0.5064	1.0783	0.7864	0.0424	-0.4108	0.6419	-0.6163	0.3422	0.4981	0.007	0.5910	0.3767	0.55	0.304		40.0	200	11100	C.7419	193391	7756	0.443	0.4022		246.0	0.000	0.1525	0030															
mfr = 0.67 and α = 1.0°		For	χ	-187.47	-100.57	-10.27	-2.05	0.00	0.31	0.63	1.25	1.88	7.30	3.13	6.5	5.5	9.5	C7.0	UC. 9	0.0	8 5	3 5	3 5	2 2	20.02	30.00	3 8	8 6	9 6	8 8	20.00	8 9	241.85															
= 0.67 8		ý	C.	0.0174	0.0338	0.0588	0.1067	0.1669	0.2318	0.2776	0.3311	0.3970																																				
nf		Afterbody			19.13				571.08			00600																																				
	°0 =				0.9195 4	•		•				-	0.3525	0.3528	0.3930	0.5742	0.8333	200	101	2	1.1459	1700	10,2401	5 5	51260	677670	0.8900	0.8980	1361	6211.0	1997	0.0317	0.7172	-0.6608	-0.5922	-0.7149	0.6624	0.0000	0.6380	-0.5668	-0.4517	-0.4096	0.4386	0.3842	0.2388	0.1517	0.0359	
		Forebody												-23.11 0.			5.13		67.7		# 6 # 6				21			3.13		75.4 5.50 5.00		99			12.50 -0.		17.50							90.00	•			
			×	-187.47	155.11	-130.84	-106.57	ģ	4	Š	₹	÷,	7	ξ; :	7 5	₹ `	, .		7 '	Τ'	-	•					•			•	.,			=	=	<del></del>		5 7	4	•	. 35	Ε.	æ	55.9	2 3	- 7	27	
		pody	Ğ	0.0176	0.0396	0.0557	0.1065	0.1666	0.2364	0.2888	0.3457	0.4162																																				
	°,	Afterbody	χŢ	343.16	384.14 419.13	457.12	507.77	545.76	\$71.08	583.74	596.41	609.07																																				
	<b>081</b> = <b>4</b>	γģς	c C	0.9252	0.3258	0.5345	1.0978	0.7833	-0.0653	-0.5517	-0.7648	-0.8152	-0.8470	-0.7381	07070	-0.0173	-0.5987	0.4818	0.4/10	0.4529	0.4932	0000	Coppo Coppo	0.6265	-0.6105	-0.5677	0.4233	0.4204	0.4333	0.4936	0.3930	0.2181	1000															
<b>d</b> α = 0°		Forebody	χĽ		-25.67			_	0.31								200				800						90.06			90.08		0000																
mfr = 0.67 and α = 0°							62	£.	31	78	33	38																																				
m H		Afterbody	C		3 0.0346							0.403																																				
	• = 0°		X	• • •	2 419.13							6 609.07	•			•	~ 1		•	<b>.</b>	ec c		<b>5</b> . (	_	•	<b>o</b> .	٠,		ю.	۰.	•	<b>.</b>			5	•	oo 1	٠.	n es		. 0	٠	Q	0	٠:	<b>s</b>		
		Forebody	ට්		0.9272																1.1628			0.6097								0.3000						0.0397								0.1504		
		Po	×	-187.47	155.11	-130.84	-106.57	-90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	1671-	-10.27	-5.13	<b>\$</b> .5	-2.05	9	4.6	0.00	0.31	0.63	125	88.	2.50	3.13	5.75	4.37	J) (	67.0	S. 8	0001	12.50	15.00	17.50	20.02	8 8	900	90.09	70.00	80.00	00:06	00.001	00.011	241.62	

TABLE VI. Continued

(i) Continued

		į	è è	86100	0.0244	0422	.0553	<u> </u>	2000	301	2813	Ş	È																																		
		Attento	Ē																																												
	A = 180°	3	^		_		457.12			583.74		_		_																																	
å	•	1	CL CP	0.1135	-0.2090	-0.6982	0.0089	1 0000	0.4638	0.0725	0.109	0.1298	0.1170	0.1220	-0.0833	0.1096	-0.0929	-0.0988	-0.2012	0.2334	-0.2498	0.3399	0.3866	0.4252	0.3284	0.402	0.421	0.463	2000	0.3381	-0.2127	0.1456	0.0233														
mfr = 0.82 and $\alpha = 0^{\circ}$		Pos	<u> </u>	187.47	106.57	.25.67	10.27	900	6	0.63	1.25	88.	2.50	3.13	3.75	4.37	5.00	6.25	7.50	8.75	0.00	12.50	8.8	17.50	20.00	80.00	8 8		8 6	80.00	100.00	110.00	241.85														
0.82 a			۰.	54	<u>ج</u> ج	e :	6 F	? <b>?</b>	9	17	56	77																																			
Į.		Afterbody	ð				0/0000																																								
	°0 = 0		×	343.16	384.14	419.13	457.12	\$45.75	571.0	583.74	596.41	609.07																																			
	•	Forebody	වී	0.1338	0.0881	90.0	0.1032	0.2693	-0.3102	-0.3666	0.9037	-0.8377	-0.6870	-0.6310	-0.4259	0.0008	0.4335	0.6781	0.8760	8	1.1788	1.0153	0.5200	0.10	671.7	0 173	0.1587	1491	7	0.1986	-0.2366	-0.1848	0.3211	0.3122		0.3980	0.3874	0.3894	0.3971	-0.4261	0.4246	0.4441	0.4141	0.3310	0.2095	0.1455	0.0029
		Fore	×	-187.47	-171.29	130.11	106 57	90 39	74.21	-58.03	-41.85	-33.76	-25.67	-23.11	17.97	10.27	-5.13	£.	-2.05	8	<b>4</b> 8	80	15.0	500						808				90.02				30.00		_	00.00		_		· 		79.84
				•	•		• •																																					;	= -	- ^	
		Afterbody	ů	0.0248	0.0271	0.04	0.1127	0.1769	0.2495	0.2970	0.3532	0.4224																																			
	ಹಿ	After	Z	343.16	384.14	457.12	507.77	545.76	\$71.08	583.74	596.41	609.07																																			
	<b>4</b> = 180°	dy	e de	0.8626	0.730	3008	1.0088	0.8882	0.1640	-0.2872	-0.4237	-0.3888	-0.4341	-0.3548	3008	3215	2948	2833	0.3426		6 7	, i		(5000)	3	-0.4582	809	-0.4722	0.4363	0.3511	-0.2185	0.1497	0.0194														
α # 0°		Porebo																	φ										_	_	_	_															
74 and			×	-187.47	75.601-	?	7	0	0	0	-	-	7		Ē	4	vo v	<i>.</i>	~ 0	• 9	2 2	4 =	2 2	2000	<b>;</b>	20.00	90.00	70.00	80.00	90:00	100.00	10.00	241.83														
mfr = 0.74 and $\alpha = 0^{\circ}$		body	Ġ	0.0127	0.0238	0.0669	0.1157	0.1776	0.2442	0.2903	0.3431	0.4090																																			
-	٤.	Afterbody	XI	343.16	419.13	457.12	507.77	545.76	80.178	583.74	596.41	200600																																			
	<b>\$</b> ) = <b>\$</b>	à	e.	0.8054	0.8576	0.8153	0.7405	0.6569	0.5615	0.4238	0.2589	0.1725	0.0404	0.0120	0.0784	0.3482	0.6590	100.0	7510	1887	0.1007	1921	10.3673	722	230	-0.3044	1937	-0.3568	449	-0.3406	1832	200	100	K 8	<u>4</u>	-0.5400	-0.5178	537	-0.3988	Š,	0.4571	0.4945	0.4282	0.3030	0.1514	523	-0.0109
		Forebody															51.5				_		_									7.50													•		
			×	121.30	155.11	061	-106.57	-90.39	-74.21	85.	88.1	-33.76	.25.67	-23.11	-17.97	.10.27	ųσ	, ,	4 9	<b>,</b>	je	io	Ċ			2.	e.	<b>e</b> .	4	Š	6	- 6	xé ç	12.50	<u></u>	17.	õ	Ř	900	Š	80.00	5 5	£ 8	10.00	10.00	241.85	279.84
		ģ	<u>ئ</u>	0.0110	0.0352	.0542	<u>100</u>	0.1602	2312	0.2840	0.3462	0.4272																																			
	:	Afterbody	XI.							_		009.07																																			
	- 180												× ×	3 :	: s	2 2	: 5	. 2	2 2	<b>x</b>	90	. 20	2	=	œ.	-	٥	92	₽:	<b>T</b>	9 9	<b>⊃</b> y	2														
3.1°		ē	<u>ئ</u> د											0.1833			200				0.3218			0.3081						0.3444	0.2196	0.1303	(A)														
endα.	•	Ξ,	X.	-106.47	-25.67	-10.27	-2.05	00.0	0.31	0.63	2 8	80.0	2.50	2.1.5	5.75	2 5	2,5	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	80.00	90.09	20.00	80.00	00:06	0000	341.86	C\$: 147														
mfr = 0.67 and α = 3.1°		à l	C.	0.0335	0.0422	0.0633	0.1094	6171	0.2362	0//70	0.3279	386/																																			
Ħ	•	Arerbody	X/L								14.060																																				
	°0 = 0										_		3 7	ţ ::	3 5	2 2	: 2	*	20	æ	22	35	92	17	<b>*</b>	×	=	۰	<b>∑</b>	<b>.</b>	2 -	<del>.</del> 5		<b>*</b>	20	27 1	<u>.</u>			• 0	, -		. 0	•	00	2	•
	4	ě	CP						0.6992										1.1729						-1.1198		1.0907				0.9630							1679.0			-0.3807	0.2901	02799	-0.2179	0.1418	-0.0375	-0.0286
	ŝ	Ĭ	X. X	171.29	-155.11	-130.84	-106.5	90.39	17.47	20.00	22.67	7.55.75	) T. T.	17.07	10.77	1 5	7	-2.05	0.00	4.0	0.00	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	8.8	67.0	8.75	10.00	12.50	15.00	17.50	00.02	3 5	3 5	8 8	20.00	80.00	800	100.00	110.00	241.85	279.84

TABLE VI. Continued

(i) Concluded

		g g	-0.007	0.0147	0.0348	20000	44.	0.1872	0.2264	0.2723	0.3336																																				
		Afterbody	343.16	384.14	419.13	507.12	545 76	571.08	583.74	596.41	609.07																																				
	<b>o</b> = 180°	<b>₽</b> 6	0.0778	-0.1981	4 :	0.1617	1 1287	0.7437	0.4096	0.2630	0.1971	0.1916	1579	0.1051	11211	0.1495	.0885	0.0405	4	0.0620	1313	1017	7	1814	01177	3038	1.5585	0.000	0.3333	0000	0.1380	0.0158															
α = 3.0°		Forebody	_		•	0 70 6																		0007		90.00																					
mfr = 0.81 and $\alpha = 3.0^{\circ}$						•			4	9	5											_		•		.,		_		. =		~															
mfr = 0.		Afterbody	_			0.0030					0.3265																																				
	o = 0e	¥ Ş	343.16	384.14	419.13	45/.12	445.76				609.07																																		_		
		Forebody	0.2196	0.1582	0.0784	0.0463	0.3866	-0.3015	0.8099	-0.8303	-0.7088	-0.5600	-0.5018	0.2704	0.1632	0.5853	0.8083	0.9987	1.1588	1.1856	0.8479	0.0269	-0.4091	0.5619	7106.0-	104451	0.4929	0.6074	0.3074	0.4080	0.3810	0.4903	-0.5381	-0.5837	-0.6530	0.031	2/40.0	0.0302	0.4827	0.3795	-0.4536	-0.4522	-0.3417	0.2131	0.1400	-0.0138	
		For	-187.47	-171.29	155.11	20.55 20.55 20.55	2 20	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	-10.27	-5.13	3.34	-2.05	8 9	4	000	0.31	0.63	1.23	80.0	R :	3.13	133	15.4	3. 4	2.0	8.75	10.00	12.50	15.00	06.71	20.02	8.00	800	90.09	70.00	80.00	00:06	100.00	10.00	279.84	
		ody S	0008	0.0199	0.0376	0.0510	1000	0.1935	0.2319	0.2761	0.3370																																				
	٠	Afterbody	#3.16 #3.16	384,14	419.13	457.12	201.17	571.08	583.74	14.965	20609																																				
	<b>4 = 180°</b>	Ą ć	•	•	•	0.1047						0.0458	0.0924	0.0402	.0285	000	0370	6940	.0752	0.1291	908	12525	2276	2336	5157	13247	0.3614	2600	0.3163	02107	011387	0.0276															
α = 2.0°		Forebody		•	25.67 0											_		_			12.50			20.02			90.00																				
infr = 0.84 and $\alpha = 2.0^{\circ}$								. 2	. <del></del>	2	3																			-	-	Ä															
mfr = 0		Afterbody	0.0326				201.0																																								
	% H 0%	₹,	343.16	384.14		457.12					_								_										_					_									_	_			
	•	Forebody	0.1892	0.1286	0.0679	0.0782	0.1701	0.3027	-0.5305	-0.8517	-0.7614	-0.6021	-0.5399	-0.3173	0.107	0.5296	0.7469	0.9538	1.1320	1.1765	0.9182	0000	-0.2107	0.3650	-0.3637	-0.3202	0.3785	200.0	0.3776	2012.0	0.3136	0.460	-0.5051	-0.5124	0.5501	0.3931	2945.0	0.3313	0.4404	0.4991	-0.5066	0.4496	-0.3334	0.2244	0.144	-0.032	
		For	-187.47	-171.29	155.11	130.84	60.00	74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	-10.27	5.13	3,34	-2.05	0.0	0 4	900	0.31	0.63	1.25	88.	2.50	3.13	5.13	4.5	30.0	67.0	8.75	10:00	12.50	15.00	02.71	20.02	80.08	20.05	90.00	70.00	80.00	90.00	100.00	0001	241.83	
		yboc	0.0145	0.0229	0.0399	0.0510	1000	0.1955	0.2353	0.2791	0.3393																																				
		Afterbody	343.16 343.16	384.14	419.13	457.12	207.700	571.08	583.74	596.41	609.07																																				
	<b>•</b> = 180°	<del>\$</del> 6	0.1085	0.2080	0.7066	0.0221	0.520	0.5201	0.2287	0.0174	-0.0277	-0.0410	0.0366	0.0288	0.0249	9090.0	09900	0.1410	0.1900	-0.2054	1 2 3 3	0.3065	0.2776	0.2991	0.2954	0.3751	0.4014	100.0	0.3984	0.3347	0.1140	0.0184															
mfr = 0.83 and $\alpha = 1.0^\circ$		ę.	-187.47 (	•	•	-10.27						2.50															800		888			241.85															
0.83 an		<b>&gt;</b> 1	•		0.0406	0.0614	2 2	0.000	370	0.2765	293																																				
#		erb																																													
	<b>0= 0</b>		343.16			53 457.12		52.75			_	51	88	22	<b>%</b>	91	ē	8	33	3	58	2	<u>.</u>	<b>3</b> :	& :	53	<u>2</u> 2	7 6	256	<b>2</b> 2	19.5	9 2	162	33	88	<u> </u>	E 5	è	90.	181	90	66	169	186	95	3 8	
		ě					706170													1.1846		31 0.2473		25 -0.2354		50 -0.2423		70770- 0		8/87 G		75 -0 3976						70.590/ 0.590/					_	_		85 -0.0222 84 -0.0133	
		ŭ,	X/L	-171.29	155.11	130.84	7001	5.04.5	58.03	41.85	-33.76	-25.67	-23.11	-17.97	-10.27	-5.13	ن ک	-2.05	96.0	4.0	9	0.31	0.63	=	≃ .	~	3.13	. ·	4.37	200	67.0	8.75	01	12.50	15.	17.50	ž ž	8 6	į	8 8	2	80.00	90.00	00.00	110.00	241.85	

TABLE VI. Continued

(j) M = 0.87

			. ^	8	۲. د	<u>-</u> 2	3 8	. 2	, 2	23	6	8																																			
		Afterhody	වී		•		0.0100																																								
	φ = 180°		ž	343.16	384.14	419.13	507.72	\$45.76	571.08	583.74	596.4	609.07																																			
£.	-	Forebody	G	1.1186	2000	1.0032	1 1733	0.1419	0.8799	-1.2258	.1.3489	-1.3751	-1.3919	-1.3616	-1.3493	-1.3324	3095	-1.2745	-1.2338	1.2098	1.1854	-1.1574	1381	1,004	81000	0.8742	0.8642	0.8444	0.8484	0.8416	0.7839	-0.3511	-0.0148														
mfr = 0.39 and α ≈ 0°		Fore	χ	-187.47	-106.57	10.07	-205	000	0.31	0.63	1.25	1.88	2.50	3.13				6.25	8	8.73	000	06.21			90.05	2005	9	20 00	80.00		100:00	110.00	241.85														
- 0.39 a		A	පි		-0.0085	0.000	0.0407	0.0802	0.1275	0.1593	0.2059	0.2719																																			
nfr		Afterbody			384.14																																										
	%) #		×	_								77 609.07	=	æ	S2 :	2 5	2 :	<u>.</u>	2:5	× :	= 1	2 2	9 ==		: =	•	92	•	22	•	2	Ŀ	Q .	<b>30 4</b>	, .				-		₹		<b>.</b>	•	,	<b>.</b> .	* ~
		Forebody			2071.1		_		_											1.0367						-1.3506						_		1.1888			8								0.7497	0075.0	0.0192
		£	ž	-187.47	67.171	13084	106.57	-90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	7701-	3.5	<b>1</b>	507-	× ;	\$ 6 \$ 6	3 2	0.63	1.25	86	2.50	3.13	3.75	4.37	2.00	6.25	7.50	8.75	000	2 2	3 5	20.00	30.00	40.00	20.00	90.00	20.00	9000	80.06	00.00	241 85	279.84
		ody	c C	96000-	2010.0	00130	0.0035	0.0265	0.0618	0.0916	0.1275	0.1881																																			
	•	Afterbody		. 343.16								20000																																			
	<b>4</b> = 180°	dy		1.1527 3		•							1.5057	204	1 4644	1.4215	990	1,4006	7107	2 2	1.2823	12521	-1.2213	-1.1962	1.0990	-0.9509	-0.9125	-0.9071	-0.8985	-0.8809	0.8694	-0.4289	-0.00.0														
α = 0°		ā		187.47				_						3.13															_	_	_		_														
mfr = 0.31 and $\alpha$ = 0°												_	•		. ,			, ,		``	2 2	=	=	20	æ	×	8	2	₩.	8	2	10.00	*														
THE		Ę		0.0176							0.1233	0.1826																																			
	<b>0= 0</b>	¥	X	384 14	419.13	457.12	507.77	545.76	571.08	583.74	250.4	609.07																																			
	•	Forebody	<u>ඩ</u> දි	2 2	1.1519	1.1475	1.1361	1.1240	1.1122	1.1002	/690	1.0862	0.000	£ 1	1891	1914	1.1738	1082	0.9304	0 7308	0.1303	-1.1266	-1.3423	-1.4599	.1.4813	-1.4787	-1.4784	1.4647	1.4583	14231	1.4043	2,002	3912	1.2890	1.2579	-1.2162	-1.2092	-1.0930	-1.0124	0.9443	0.9185	0.000	0.000	0.8620	0.4233	0.0131	-0.0243
		For	¥ ;	-171 29	-155.11	-130.84	-106.57	60.30	-74.21	58.03	Q 2	35.70	10.07	17.07	-10.27	5.13	334	-2.05	06.0	4	000	0.31	0.63	1.25	88.	2.50	3.13	3.75	4.37	200	57.0	00.7	9 9	12.50	15.00	17.50	20.00	30.00	40.00	20.00	8 8	8 9	8 8	8 8	110.00	241.85	279.84
	,	ģ	<u>ا</u> و	-0.0225	-0.0196	-0.0228	-0.0150	-0.0014	0.0231	0.0480	16/0:0	Ì																																			
	:	Afterbody		384.14					5/1.08																																						
	# 180°		. 5					_				٠.	. 2	. 8	8	20	8	8	2	21	2	88	8	<b>\$</b>	82	. 38	2 2	⊋ ;	2 9	8 8	3 2	3 5	;														
°		ě	1. CP						0.31 -1.0831										75 -1.3872										0.8972																		
mfr = 0.27 and $\alpha$ = 0°	•	- ;	XVI.	-106.57	-25.67	-10.27	-2.05	000	ع د	5 -	<i>:</i>		-		4	3.5	6.25	7.50	8.75	10.00	12.50	15.00	17.	20.00	30.00	50.00	00.00	00.00	00.08	20.00	00001	241.85															
mf = 0.		Afferbody	ביים פיים פיים	-0.0231	-0.0247	0.0199	0.0092	8700.0	0.0277	0.075	0.000	7671.0																																			
	0 =	Affe	7 K	384.14	419.13	457.12	507.73	\$71.0	583.74	4 4	000																																				
	٠	ğ ç	- <del>-</del>	1.1652	1.1636	1.1595	1.1535	2	1250	1.1221	1207	1.1247	1.1307	1.1453	1.1864	1.1946	1.1612	1.0804	0.8695	0.6729	-0.2276	1.1921	-1.3853	1.5113		5359	1.5353	2020	1.3002	1 4440	.1 4716	1.4089	-1.3764	-1.3222	-1.3005	-1.2731	-1.2527	1611.1	1.037	5.0074	0.9029	0.9097	0.8947	9068.0	-0.7360	0.0116	-0.0130
	D.	rorebody	-187.47	171.29	-155.11	30.8	106.57	14.2	5803	41.85	37.75	-25.67	.23.11	-17.97											20 5								10.00					90.00		20.00					_	241.85 0	

TABLE VI.Continued

(j) Continued

		Ą	<b>G</b>	0.0132	0.0278	0.0861	0.1435	0.2122	0.2611	0.3872																															
		直	7X. 91.18		419.13 0				583.74 0																																
	\$ = 180°											22	<u>8</u> 2	*	\$ 2	3 =	. =	28	17	<b>\$</b> \$	23	86	57	33	2 2	8 8	3	٠٥:	9												
°0°	•	rebod	9 S			1969			0.8658						65207		5 -0.9381			0.9046				0.7035					5 -0.0316												
and a		ž	XL 74747	-106.57	-25.67	-10.27	0.00	0.31	0.63	68.1	2.50	3.13	3.75	4.37	85.	9.2	8.75	10.00	12.50	15.00	20.0	30.00	80.00	888	800	90.06	100.00	110.00	241.85												
mfr = 0.54 and $\alpha = 0^{\circ}$		ody	C. P.	0.0109	0.0265	0.0877	0.1451	0.2115	0.2537	0.3006																															
E		Afterbody	Z Z Z		419.13	507.77	545.76	80.178	583.74	500.07	6.00																														
	00 =	d,	C 5			0.9822			0.8544			0.7401	0.7740	0.8892	1.0710	200	1.1723	1.0710	0.4579	0.5258	1124	-1.1402	-1.1243	-1.0722	0,000	.0233	-0.9930	-0.9546	0.9383	0.9032	-0.8973	-0.8716	-0.8591	-0.7370	-0.6876	-0.6924	0.6849	0.7149	-0.2577	-0.1169	0.0342
		죨	XII.	-		10657 0			-58.03 0						5.13					0.31			2.50						2.3 2.3			17.50 -0					00.00			_	241.85 £
			~ ~	-17	ž.	? =	Ģ		÷.	7 "	, 7	-5	7	₹	•		•	•											-		_	- (	•	. 4	•,	Ĭ		~ .	^ =	=	2 2
		body	C. C.	0.0034	0.0131	0.0245	0.1204	0.1868	0.2371	1820	9650																														
	్ర	Afterbody	¥ ¥	384.14	419.13	457.12	545.76	\$71.08	583.74	14:060	0.500																														
	<b>*</b> 180°	ď	<b>G</b> 5	1.0216	0.8127	2004	0.4931	-0.4308	0.8770	5.55	1.1274	-1.1100	1.0578	1.0141	-1.0065	0.9831	-0.8845	-0.8239	-0.8325	0.8296	-0.7794	-0.6630	-0.6017	0.6225	0.6330	0.6372	-0.5084	-0.1559	-0.0257												
α * 2.0°		ē	X/L			.205		0.31		7					500					92				00.00			_		. 241.85												
mfr = 0.49 and $\alpha$ = 2.0°						•		21	7.	3 2	3																_	-	7												
H.		Afterbody	C C			0.0381				0.6320																															
				84.14	419.13	457.12	545.76	571.08	583.74	9,00,00	8																														
	8		X, X,	28	•	-																																	<b></b>		
	% •		CP XI		-	4.0534	0.9994	0.9708	0.9326	0.6971	0.8749	0.8821	0.9197	1.0287	1.1498	<u> </u>	1.0995	0.9592	0.1877	0.7968	26.	-1.3008	1.2791	1.301	7167.1-	1.2475	-1.2248	-1.1810	1.1491	-1.1082	-1.1141	-1.1188	0.000	-0.9328	-0.8942	-0.8729	0.8827	0.8602	0.3600	-0.3307	0.0160 -0.0171
	<b>0</b> # ◆		Ċ	1.0747	1.0709	130.84 1.05.94				41.85 0.89/1					-5.13 1.1498		_				1.25 -1.2941				3.73 - 1.2912					12.50 -1.1082			20.00						100.00		241.85 -0.0160 279.84 -0.0171
	9) # <del>◆</del>		X/L CP	-171.29 1.0747	155.11 1.0709	130.84	90.39	-74.21	-58.03	41.85	-25.67																														
	ည်။ <del>စ</del>	Forebody	CP X/L CP	0.0046 -171.29 1.0747	90001 11.5211 1.0709	0.0289	0.1206 -90.39	0.1842 -74.21	0.2315 -58.03	C8.14- 4483.U	.25.67																														
		Afterbody Forebody	X/L CP	0.0046 -171.29 1.0747	419.13 0.0188 -155.11 1.0709	457.12 0.0289 -130.84 507.77 0.0691 -106.57	545.76 0.1206 -90.39	571.08 0.1842 -74.21	583.74 0.2315 -58.03	590.41 0.2844 -41.85	25.78	.23.11	76.71-	-10.27	-5.13	* 50° c	060-	0.44	000	0.31	0.63	1.88	2.50	3.13	3.73	5.00	6.25	7.50	8.75												
ь	0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 =	Afterbody Forebody	CP X/L CP	384.14 0.0046 -171.29 1.0747	419.13 0.0188 .155.11 1.0709	0.0289	545.76 0.1206 -90.39	571.08 0.1842 -74.21	583.74 0.2315 -58.03	C8.14- 4483.U	25.78	.23.11	76.71-	-10.27		* 50° c		0.44	000	0.31		1.88	2.50		3.73	5.00	6.25	7.50													
and $\alpha = 0^\circ$		Afterbody Forebody	XI CP XIL CP	1,0224 384.14 0.0046 -171.29 1.0747	0.8438 419.13 0.0188 .155.11 1.0709	457.12 0.0289 -130.84 507.77 0.0691 -106.57	0.3469 545.76 0.1206 -90.39	571.08 0.1842 -74.21	-1.0076 583.74 0.2315 -58.03	1,1956 396.41 0.2844 41.83	25.78	-1.2065 -23.11	10.1701	-1.1810 -10.27	-5.13	1607.	0.50.1	-1.0046	-0.9640 0.00	-0.9985 0.31	0.63	-0.8419	-0.7942 2.50	3.13	0.7608	-0.7529 5.00	-0.3421 6.25	7.50	8.75												
r = 0.49 and α = 0°		Forebody Afterbody Forebody	XI CP XI CP XII CP XII CP	106.57 1.0224 384.14 0.0046 -171.29 1.0747	-25.67 0.8438 419.13 0.0188 -155.11 1.0709	. 10.27 0.9887 457.12 0.0289 -130.84	0.00 0.3469 545.76 0.1206 -90.39	0.31 -0.6053 571.08 0.1842 -74.21	0.63 -1.0076 583.74 0.2315 -58.03	1.25 -1.1956 399.41 0.2844 -41.85	2.50 -1.2146 -2.5070 -2.5570 -2.567	-1.2065 -23.11	10.1701	-1.1810 -10.27	-1.1389 -5.13	1607.	0.50.1	-1.0046	-0.9640 0.00	-0.9985 0.31	1.053	-0.8419	-0.7942 2.50	0.7698	0.7608	-0.7529 5.00	-0.3421 6.25	-0.2103	8.75												
$mfr = 0.49 \text{ and } \alpha = 0^{\circ}$	⊕ = 180°	Afterbody Forebody Afterbody Forebody	CP X/L CP X/L CP X/L CP X/L CP	0.0029 -106.57 1.0224 384.14 0.0046 -171.29 1.0747	0.0143 -25.67 0.8438 419.13 0.0188 -155.11 1.0709	0.0334 - 10.27 0.9887 457.12 0.0289 - 130.84	0.1226 0.00 0.3469 545.76 0.1206 -90.39	0.1845 0.31 -0.6053 571.08 0.1842 -74.21	0.2267 0.63 -1.0076 583.74 0.2315 -58.03	0.2789 1.25 -1.1930 390.41 0.2844 -41.63	0.3467 1.86 -1.2260 005.07 0.3570 -35.70 2.50 -1.2146	-1.2065 -23.11	10.1701	-1.1810 -10.27	-1.1389 -5.13	1607.	0.50.1	-1.0046	-0.9640 0.00	-0.9985 0.31	1.053	-0.8419	-0.7942 2.50	0.7698	0.7608	-0.7529 5.00	-0.3421 6.25	-0.2103	8.75												
mfr = 0.49 and $\alpha$ = 0°		Afterbody Forebody Afterbody Forebody	XI. CP XI. CP XI. CP XII. CP XII. CP	384.14 0.0029 106.57 1.0224 384.14 0.0046 -171.29 1.0747	419.13 0.0143 -25.67 0.8438 419.13 0.0188 -155.11 1.0709	457.12 0.0334 -10.27 0.9887 457.12 0.0289 -130.84 (1.02.0.028)	545.76 0.1226 0.00 0.3469 545.76 0.1206 -90.39	571.08 0.1845 0.31 -0.6053 571.08 0.1842 -74.21	583.74 0.2267 0.63 1.0076 583.74 0.2315 58.03	596.41 0.2789 1.25 -1.1936 596.41 0.2844 -41.85	2.50 -1.2146 -0.5570 0.5570 -55.70	3.13 -1.2065 -23.11	3.75 -1.1701	4.37 -1.1810 -10.27	5.00 -1.1389 -5.13	30 L 000 1 00 L	8.75 -1.0428 -1.050	10.00 -1.0046	12.50 -0.9640 0.00	15.00 -0.9985 0.31	2000 - 45,975 - 12,95	30.00 -0.8419 1.88	50.00 -0.7942 2.50	60.00 -0.7698 3.13	70.00 -0.7008 5.75	90.00 -0.7529 5.00	100.00 -0.3421 6.25	110.00 -0.2103 7.50	241.85 -0.0273 8.75	10.00	15,00	17.50	0007	40:00	80.00	00:09	70.00	0008	00000	00011	241.85 279.84
mfr = 0.49 and $\alpha$ = 0.	⊕ = 180°	Afterbody Forebody Afterbody Forebody	CP X/L CP X/L CP X/L CP X/L CP	1.0715 384.14 0.0029 1.06.57 1.0224 384.14 0.0046 1.0727 1.0747	1.0677 419.13 0.0143 -25.67 0.8438 419.13 0.0188 -155.11 1.0709	0.0334 - 10.27 0.9887 457.12 0.0289 - 130.84	0.9949 545.76 0.1226 0.00 0.3469 545.76 0.1206 -90.39	0.9619 571.08 0.1845 0.31 -0.6053 571.08 0.1842 -74.21	0.9205 583.74 0.2267 0.63 -1.0076 583.74 0.2315 -58.03	0.8776 596.41 0.2789 1.25 -1.1956 596.41 0.2844 -41.85	0.3467 1.86 -1.2260 005.07 0.3570 -35.70 2.50 -1.2146	0.8492 3.13 -1.2065 -23.11	0.8724 3.75 -1.1701 -17.97	0.9927 4.37 -1.1810 .10.27	1.1206 5.00 -1.1389 -5.13	1607.	000- 00001- 0001-	1.0034 10.00 -1.0046 -0.44	0.2941 12.50 -0.9640 0.00	0.6717 15.00 -0.9985 0.31	2000 - 45,975 - 12,95	1.2195 30.00 -0.8419 1.88	50.00 -0.7942 2.50	-1.1965 60.00 -0.7698 3.13	70.00 -0.7008 5.75	-1.1460 80.00 -0.1741 +.37 -1.1463 90.00 -0.7529 5.00	1.0894 100.00 -0.3421 6.25	110.00 -0.2103 7.50	1.0239 241.85 -0.0273 8.75		-0.9855	.0.9737		-0.8229	-0.7583 50.00	-0.7529 60.00	0.0518	-0.7630		0.011	

TABLE VI.Continued

(j) Continued

			ģ	<u>.</u>	00212	0.0432	0.0623	0.1165	0.1777	0.2527	0.3049	0.3658	0.44.90																																		
			튵	XVI.						571.08 0			0 /0.600																																		
		<b>e</b> = 180°		200		•						-0.3782		0.3041	-0.2557	-0.2453	-0.2532	-0.2101	36	-0.3093	-0.3538	383	381	<b>3</b>	93	-0.3559	239	8	523	2 2	7 2	220	122														
x = 2.0°			ş	187 47 0.0								C				4.37 -0.2		6.25 -0.2	7.50 -0.2	8.75 -0.3					20.00 -0.4693				70.00 -0.4923	80.00 -0.5120																	
mfr = 0.68 and α = 2.0°					_											4	•	•	,	•	2	12	2	=	ຂ :	2 1	S (	38	₹ \$	8 8	0000	110.00	241.85														
mfr = 0		•	Afterbody	_				-		7252.0																																					
	;	ဦ မ	ν,					507.77		571.08					_																																
		•	Forebody	_				0.8408										1.0524	1.1556	1946	1.1533	0.6235	0.2569	0.6873	0.9457	6.0	0.6924	0.8040	0.0070	0.8570	-0.8272	-0.7205	-0.7806	0.7905	0.700	0.7665	-0.7662	-0.6656	-0.6737	-0.6678	-0.6531	-0.6603	-0.6617	0.4499	0.00	0.004	0.0203
		F	2 \$	-187.47	-171.29	1155.11	200	75.00	5.42	58.03	4185	31.76	-25.67	-23.11	-17.97	-10.27	-5.13	3.34	-2.05	8	о. <b>4</b>	000	0.31	600	9 8	8 6	2.30	2.5	4.33	200	6.25	7.50	8.75	0.00	15.0	17.50	20.00	30.00	40.00	\$0.00	90.00	000	80.00	0006	80.00	241 #5	279.84
		į	g a	0.0218	0.0280	0.0458	70000	0.1813	0.2540	0.3062	0.3622	0.4306																																			
			XII. CP			419.13 0.																																									
	7001 - 4	) e = 19()			•	0.3459							-0.7757	-0.6922	-0.5711	-0.5431	-0.4824	0.4143	-0.4207	0.4570	-0.4523	0.4910	0.301/	7080	0.564	0.5580	0.5413	0.5703	-0.5825	-0.4756	415	92	321														
% * 8		Porehodu	XI.			25.67 0.							2.50 -0.7										200								_	_	241.85 -0.0321														
mfr = 0.68 and α = 0°																•		-		~ ;	= :	2 3		~	; >=	. 5	<b>( &amp;</b>	` <b>×</b>	` <b>≈</b>	8	90	≘ ;	7														
- La		Afterbody	) d			3 0.0426																																									
	<u>و</u> = 0	` <b>\</b>	X		_	419.13						609.07		_																																	
		Forebody	්ට්		20.9634				0.7021		0.4895						0.8283		1.1028	1.1809	0.3600		0.5097	-0.7261	-0.6880	-0.5059	-0.4839	-0.5509	-0.5116	-0.5065	-0.5298	0.4685	0.4746	0.5177	-0.5746	0.6004	0.5986	0.5762	10/50	0.535	21120	5794	10.5621	-0.2219	0.1209	-0.0351	-0.0193
		P.	ž	-187.47	62.171.	130.84	-106.57	-90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	17.97	10.21		,	9 6	2 4	\$ 6	3 2	0.63	1.25	1.88	2.50	3.13	3.75	4.37	2.00	6.25	8 5	6.73	12.50	15.00	17.50	20.00	8,8	3 6	900	20.02	000	8006	0000	110.00	241.85	279.84
		ody	S.	0.0207	77700	0.0567	0.1034	0.1665	0.2374	0.2886	0.3449	0.4159																																			
	8	Afterb			384.14							20.609																																			
	<b>\$</b> = 180°				0.5673			_			_	_	\$ 000 000 000 000 000 000 000 000 000 00	0.000	0.0064	10000	80%	7484	0.7652	7082	7261	-0.7039	-0.7060	-0.6716	-0.6143	-0.6082	-0.6089	-0.5935	-0.6103	0.6039	0.2635	0.1272															
d a = 0°		Forebody		-187.47			-2.05						2.50											20.00 -0.								34185															
mfr = 0.61 and $\alpha = 0^\circ$		_				•			4.5	<u></u>	29	82									-	_	_		**	•	•	-	••	on :	2 :	7	•														
L		terb		16 0.0091								07 0.4082																																			
	% = 0				78 419.13							609.07	5 5	: =	: =		5	*	2	<b>*</b>	=	5	=	5	<b>z</b>	2		<b>1</b> 20	ο.	<u>.</u>				•	. 2	o -	, ,	, 🕶	_	_	_	~			<u>.</u>	<u>.</u>	•
		ē		17 0.9929 10 0.9935									0.000								0 0.5801		3 -0.7261								5 7386					C18815							_		_		-0.0233
		24	\$	187.47	-155.11	-130.84	-106.57	90.39	.74.21	-58.03	7	-53.70	70.62-	17.97	-10.27	5.13	75.	-2.05	96.0	<b>4</b>	000	0.31	0.63	1.25	- 88	2.5	3.13	3.75	4.37	9.0	57.0	8.75	10.00	12.50	5.00	2000	2007	40.00	\$0.00	90.00	00.00	80.00	00'06	00:00	110.00	241.85	279.84

TABLE VI. Continued

(j) Concluded

		Afterbody	දු දි	0.0267	0.0475	0.0640	0.1085	0.1571	0.2142	0.2536	0.2990	0.3564																																					
	<b>.</b> 081	Afte	X	384 16	419.13	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																					
8	<b>*</b> = 180°	Forebody	<b>a</b>	0.136	-0.5982	0.0623	0.9043	1.0201	0.4342	0.0302	-0.1628	-0.0789	0.15	0.1007	-0.1128	0.1351	0.1523	0.1014	0.191	0.2543	11570	0.3037	-0.4258	-0.4265	0.4060	0.5500	0.4269	4 3	0.4836	0.5084	-0.5095	0.2069	1010	-0.0141															
and α =		For	X	187.47	-25.67	-10.27	-2.05	0.00	0.31	0.63	1.23	88.	5.20	3.13	3.75	4.37	2.00	6.25	7.50	8.73	10.01	12.50	15.00	17.50	20.00	30.00	50.00	00.00	70.00	80.00	80.00	00:00	10.00	241.85															
mfr = 0.84 and $\alpha = 0^\circ$		body	<b>d</b> (	00100	0.0439	0.0656	0.1062	0.1581	0.2123	0.2477	0.2896	0.3447																																					
-		Afterbody	X.	343.10	419.13	457.12	507.77	545.76	571.08	583.74	<b>38</b> .4	609.07																																					
	•	Forebody	a i	0.1376	0.0011	0.0947	-0.1910	-0.2437	-0.2780	-0.3611	-0.8392	-0.7639	0.6263	0.5487	0.342	0.0870	0.4660	0.7075	0.8935	1.1245	1.1883	0.9932	0.3268	0.0543	0.1232	6780.0	0.0842	0.1000	0.1082	-0.1149	099	0.2022	-0.1852	0.2905	79670		0.4241	2674.0	1035.0	3804	0.4219	0.4402	0.4998	-0.5189	-0.5373	-0.2161	-0.1123	-0.0201	-0.0089
		Fore	אל גל	-187.47	-155.11	-130.84	-106.57	-90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	-10.27	-5.13	3.34	-2.05	9:0	⇒ 4 8	900	0.3	0.63	1.25	80.	2.50	3.13	3.75	4.37	200	6.25	DS: 7	8.75	00.0	25	3 5	2 6	20.05	8.8	900	900	20.00	80.00	90.00	100.00	110.00	241.85	279.84
		Afterbody	c <sub>b</sub>	0.0312	0.0516	0.0724	0.1266	0.1921	0.2638	0.3164	0.3725	0.4416																																					
	.08	After	χ	343.16	419.13	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																					
<u>د</u>	• = 180°	Forebody	G.	0.8784	0.0475	0.3392	1.0187	0.9150	0.2086	-0.1848	-0.4474	0.3909	-0.3975	0.3493	0.2919	0.3291	0.2578	-0.2522	0.3081	-0.3658	4 4 4	0.4069	0.4963	-0.5243	-0.5082	-0.492/	-0.4589	-0.4521	0.4916	0.5247	0.5347	-0.2333	16110	0.0165															
$mfr = 0.74 \text{ and } \alpha = 0^{\circ}$		Fore	ž	106.57	-25.67	-10.27	-2.05	0.00	0.31	0.63	1.25	88	2.50	3.13	3.75	4.37	8.8	6.25	<b>S</b>	8.73	900	12.50	13.00	17.50	20.00	30.00	20.00	90.00	0.00	80.00	8.08	00.00	110.00	241.85															
ofr = 0.74		Afterbody	<u>ئ</u>	0.0176	0.0487	0.0776	0.1275	0.1928	0.2628	0.3095	0.3647	0.4273																																					
<b>5</b>	= 0,	After	X	38.16	419.13	457.12	507.77	545.76	\$71.08	583.74	596.41	609.07																																					
	•	Forebody	C.	0.8827	0.8706	0.8286	0.7552	0.6725	0.5767	0.4368	0.2666	0.1706	0.0360	0.0213	0.0818	0.3342	0.6780	0.8545	1.0119	1.1772	7661.1	0.900	0.1375	0.3081	0.3561	5 4 5 4	0.3315	-0.3618	0.3030	-0.2768	-0.3056	0.3084	-0.2547	-0.4050	0.4226	40.4.0	0.4775	2010.0	0.4658	0.4651	0.4283	D.4625	-0.4927	-0.5236	-0.5390	-0.2676	-0.1191	-0.0191	-0.0060
		920	ž	171.79	-155.11	-130.84	-106.57	-90.39	-74.21	-58.03	41.85	-33.76	-25.67	-23.11	-17.97	10.27	-5.13	-3,34	-5.05	0.00	4 5	8	0.31	0.63	52 5	80	25.5	3.13	3.75	4.37	89	6.25	5.5	8.75	9 5	06.21	8.5	2 2	30.05	8 6	2005	8	20.00	0008	90.00	00:00	10.00	241.85	279.84

TABLE VI. Continued

(k) M = 0.89

		5	) b	0.0176	0.0085	0.0239	0.0541	0.0922	0.1453	0.1856	0.2328	0.3023																																			
		Afterhody	:		410 13			_	571.08			0.609																																			
	• 180°	1											<u>.</u>	= 2	. Y	2 5	· 5	=	. 95	9	2 ==	: ::	<b>.</b>	=	و و	90	6	50	Ŀ	7	2		7														
ھ	•	Forebody	!	1.1321	10157	1.1248	1.1842	0.1658	0.8144	-1.1398	-1.2551	-1.2931	5118	1087.1	3071			1.1683	1.13	801	1.078		1.0624		-0.9426	-0.8388	-0.8213	-0.8025	-0.8147	-0.8172	-0.8105	0.7768	0.032														
mfr = 0.89 and α = 0°		ů.	X	-187.47	78.67	-10.27	-2.05	0.00	0.31	0.63	1.25	<b>8</b> 6. 6	3 :	3.13	4 17	9	6.25	7.50	8.78	000	12.50	15.00	17.50	20.00	30.00	50.00	60.00	70.00	80.00	90.06	100.00	110.00	241.83														
- 0.89		2	å	0.0044	00116	0.0251	9950	0.0962	0.1481	0.1837	0.2306	0.2929																																			
nf.		Afterbody																																													
	e •	, ,	×	343.16	•					_		3 609.07					_	_	_	_	_	_		_	_			_	_						_	_				_	_						
		Forebody	Ç.	1.1339	1.1320	1.1224	1.1064	1.0879	00/01	1.0463	-05 <b>8</b>	1.0213	000	1 0480	1.124	96	1.2134	1.1890	1.0594	0.896	0.100	-0.866	-1.1501	-1.2623	-1.2853	-1.2785	1.2757	-1.2558	-1.2329	1.2326	<u>66</u>	11320	200	-1.0912	-1.0660	1.0493	-1.0391	0.9241	0.0000	0.8130	-0.8189	-0.7956	-0.8115	0.7916	-0.7762	4070.0	3
		For	ž	-187.47	-155.11	-130.84	-106.57	-90.39	-74.21	-58.03	41.85	33.76	79.7	17.97	-10.27	-5.13	3.34	-2.05	06.0	4	0.00	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	8.00	6.25	00.7	000	12.50	15.00	17.50	20.00	80.05 40.00	3 5	0000	70.00	80.00	<b>8</b> 0.00	00:00	10.00	24 077	417.61
						_	_				_																																				
		Afterbody	5	0.0157	0,000	0.0031	0.0239	0.0516	0.0916	0.126	0.1678	0.2321																																			
	ò		×	36.15	419.13	457.12	77.70	545.76	871.08	583.74	4.06	609.03																																			
	<b>6 =</b> 180°	Ą	<u>ئ</u>	1.1610 1.147	.0953	1.1774	1.1405	0.0035	-0.9582	-1.2634	7605	1.4083	403	3859	3602	-1.3430	-1.2998	-1.2820	-1.2551	2202	-1.1878	1766	-1.1431	-i.1166	-1.0241	<b>3</b> 62	-0.8772	0.8545	-0.8538	0.0444	0.8497	0.0475	}														
α <b>=</b> 0°		Forebody		106.57	_	_		_				20°			4.37	5.00	6.25						17.50						00.08		00.00																
32 and			~ ;	2	-7	Ŧ	•		•	•			• .		•		Ĭ	,	_	=	2	22	=	×	×	×	<b>&amp;</b> 8	2	₩ 8	× §	3 3	241															
mfr = 0.32 and α = 0°		Afterbody	<b>a</b>	0000	-0.0020	0.0046	0.0251	0.0535	0.0932	0.1234	0.101.0	0.225																																			
-	<u>۔</u>	After	Z,	384.14	419.13	457.12	207.77	545.76	571.08	583.74	19.000	0.60																																			
	0 = 0		a i	1.1617	1608	1.1543	1426	6061	/07!	1.1065	2 6	0960	6101	1.1207	1.1739	1.2086	1.1962	1.1357	0.9599	0.7818	-0.0594	.1.0339	1.2605	-1.3674	3876	-1.3873	3951	0786.1	-1.3714	8/557	705	-1.2580	-1.2363	-1.1988	1.1699	1.1584	1001	0.9427	0.8895	-0.8612	-0.8521	-0.8456	0.8472	0.8407	0.0030	0.0184	:
		를																																									_			_	
			× 5	-171.29	-155.11	130.84	-106.57	SE 26	* :	-58.03	20.14	-25.70	.23.11	-17.97	-10.27	ΑĻ	ij	-7	Ŷ	φ̈́	o	Ö	Ö		<i>-</i> - ,	7	mi r	÷, •	4 v	ń •		œ	10:00	12.50	15.00	8.6	2007	900	20,00	90:00	70.00	80.00	00.06	100	241.89	279.84	
		dy	<u>ئ</u> ق	0021	-0.0017	0000	9	0.0200	# F	18/00	1771	67/1																																			
		ferb	ی د																																												
	<b>\( \phi = 180^\circ\)</b>	•	× 5		-			7 545.76						2	3	7		_	_	~	•	~	~ .	~	٠,					. ~																	
<b>°</b> 0	•	ebody	- C	1.1657	1.1397	1.2010	60.	0.1067		4126	1457	1.4623	-1.459	-1.4352	-1.4103	38	-1.3700	-1.342	1.320	- 58	-1.258	-1.218	1.192	187	1.061	0.923	0.8881	200	08400	0.8558	0.8154	0.0632															
andα=		<u>.</u>	Z 2	-106.57	-25.67	-10.27	9.7	3 6	5.0	2.03	: ==	2.50	3.13	3.75	4.37	200	6.25	7.50	8.75	2000	12.50	15.00	17.50	20.00	800	00.00	30.05	9 6	8 8	000	110,00	241.85															
infr = 0.27 and $\alpha = 0^\circ$		<u>&gt;</u> !	<b>.</b>	0.0003	0.0039	0.0023	79000	87700	0000	926	0.1670	2																																			
mfr		Afterbody																																													
	°0 = <b>\$</b>	< ;	~ 3		•	457.12																																									
		Forebody	<u> </u>	1.1788	1.1778	1.1726	1.10/4	2021.1	3171	3	11317	1366	1.1442	1.1605	1.2017	1.2047	1.1759	0.1010	0.8909	0.6948	-0.1933	060	9069	1.4248	1.4350		14319	4174	400	-1.3635	1.3427	-1.3114	-1.2965	-1.2634	1 2065	1796	1.0467	-0.9748	-0.9242	-0.8798	-0.8759	0.8598	0.8526	0.8118	0.0599	0.0370	
		For	X/I.	171.29	155.11	130.84	100.30	.74.21	60.03	418	.33.76	-25.67	-23.11	-17.97	-10.27	5.13	3.34	50.7	06.0	40	0.00	6.3	500	9	2 5	2.70	3.75	4.17	90	6.25	7.50	8.75	10,00	12.50	8 5	2002	30.00	40.00	20.00	00:09	20.00	8 8	000	10.00	241.85	279.84	
			•																																										•	•	

TABLE VI. Continued

(k) Continued

		_	<b>.</b> 8	8	<u>s</u>	2 20	5	9/	69	20	916																																	
		Ę	<b>2</b> 0000			0.0020					0.4076																																	
	<b>•</b> = 180°	7	¥ 54 54 54 54 54 54 54 54 54 54 54 54 54	384.14	419.13	457.12	\$45.7	\$71.08	\$83.74	596.41	609.07																																	
	•	Forebody	CP	0.9993	0.7609	1 2108	0.5324	-0.3653	-0.8017	-1.0280	-1.0507	-1.0732	0.0848	0.9774	-0.9765	-0.8932	0.9000	-0.8696	-0.8415	-0.8349	0.8015	0.23	0.7181	0.6610	0.6439	-0.6568	0.6899	0.0340	0.730	0.0027														
<b>nd</b> α = 0		Fore	X/L	-106.57	-25.67	10.27	000	0.31	0.63	1.25	88.	2.50	3.13	4.37	200	6.25	7.50	8.75	900	12.50	986	2000	30.00	20.00	00.09	000	80.00	8 8	8 9	241.85														
mfr = 0.54 and $\alpha = 0^\circ$		<u>ا د</u>	G009		0.0294	0.0526	0.1610	0.2266	0.2703	0.3243	0.3959																																	
n F		erb	X7.			457.12 0.					0.609.07																																	
	<b>0</b> = <b>0</b>			_		1.0361 45						0.7633	0.7619	0.9224	1.0852	1.1623	1.2099	1.1877	1.1012	0.4612	0.4529	1 0300	019	-1.0409	1.0161	-0.9873	0.9811	0.9384	0.8909	0.864	-0.8483	-0.8591	-0.8623	204	-0.8079	0.7362	0.08/4	-0.6399	-0.6694	-0.6860	-0.7003	-0.6903	0.0094	0.0064
			X. CP										7.0 11.62-								0.31 -0.4							800 C								30.00						_	110.00	
			X/L.	-171.29	-155.11	30.85	§ 6.	-74.2	85-	₹	ę, i	5.	7 -	: =			7	٧	Υ.			, –			•	•••	•				=	=	-	=	≍ :	≠ ¥	₹ ₹	<b>.</b> 25	×	<b>∞</b>	<b>5</b>	≝ :	Ĭ ?	\$ 15
		body	<u>ئ</u> ۋ	0.0075	0.0248	0.0377	0.1392	0.2070	0.2580	0.3202	0.3984																																	
		Afterbody	¥ ¥	384.14	419.13	457.12	545.76	571.08	583.74	596.41	609.07																																	
	• <b>≈</b> 180°	ody	ر اور اور	1.0372	0.8274	0.9588	0.5035	-0.3565	-0.7713	-1.0004	-1.0389	-1.0477	55001-	0.9568	-0.9082	-0.8733	-0.8469	-0.8407	0.8101	-0.7812	0.7570	0.7450	-0.6220	-0.6008	-0.5900	0.5904	0.6388	0.0340	0.0068	0.0072														
mfr = 0.49 and α = 2.1°		Forebody	X/L	106.57	-25.67	10.27							5.5								5.00							3.8																
0.49 and		_			0.0339	0.0521	0.0917	0.1954	0.2319	137	0.3290																																	
mfr.		terb	. CP																																									
	00 =	•	XX.			457.12					1 609.07				_	_		_	_	~ .				•	<u>.</u>	•		•		. ~		~		_	an i	~ -	- ~		_	2	0	oc v	۰.	n ee
	Ĭ	Forebody	CP 1087	1.087	1.0854	1.0706	79101	0.9880	0.9497	0.9134	0.9033	0.8961	0.8995	1.0549	1.1614	1.2043	1.2065	1.1159	0.9700	0.2002	0.7480	7021	-1.216	-1.2138	-1.2086	-186	-1.1807	67/17.9	0000	-1.0772	-1.0683	-1.0525	.1.0273	-1.0460		0.9462	0.63	-0.8399	-0.8351	-0.8352	-0.8270	-0.8268	-0.5336	0.0088
		Por	X/L	-171.29	-155.11	130.25	-90.39	.74.21	-58.03	41.85	-33.76	-25.67	13.07	.10.27	.5.13	-3.34	-2.05	96.0	4	80	0.31	2,5	1.88	2.50	3.13	3.75	4.37	8 5	5.5	8.75	10.00	12.50	15.00	17.50	20.00	80.00	8 8	90.00	70.00	80.00	90:00	00.00	110.00	279.84
		d,	<b>a</b> 5	0.0167	0.0299	0.0418	1378	0.2026	0.2514	3065	13773																																	
		Afterbody	KIT KIT			457.12 0				S96.41 C	0.609																																	
	<b>4</b> = 180°		CP CP			1.0006						1304	1.1264	0814	-1.0540	-1.0137	0032	9896	-0.9478	0.9014	-0.9241	0.0133	7882	-0.7415	-0.7161	-0.7171	-0.7227	-0.7283	0.7471	0.0034														
ο # O		der	X/L C		_	-10.27	-						3.13								15.00				00:00		_	00.00																
mfr = 0.49 and α = 0°																			-	-			. ~	•	•		90	2 5	2 =	. 2	į													
mfr = (		Afterbody	CP			0.0450					0.3691																																	
	<b>.</b> 0 ≈ <b>♦</b>	¥	Z Z	384.14	419.13	457.12	545.75	\$71.08	583.74	596.41	609.07																																	
		Forebody	C C	1.0877	1.0815	1.0679	10103	0.9801	0.9390	0.9004	0.8756	0.8648	0.8655	1,000	1.1439	1.1909	1.2113	1509	1.0346	0.3473	0.6184	1 1304	1.14	-1.1242	-1.1205	-1.0957	-1.0929	-1.0700	1.0194	0.9962	-0.9807	-0.9372	-0.9312	0.934	0.9075	0.8094	0.7363	0.7305	-0.7203	-0.7382	-0.7189	-0.7618	0.7034	0.0021
		۳	X4.	-171.29	-155.11	130.84	75.00. 05.00.	74.21	-58.03	41.85	-33.76	-25.67	-23.11	10.27	513	4.5	-2.05	96.0	Ġ <b>4</b>	0.0	63		. ~	2.50	_	3.75	4.37	8 5	57.0	8.78		0	15.00	17.50	0	8 8	- 0	000	70.00	0	90.00	00'00	00.00	279.84

TABLE VI. Continued

(k) Continued

		÷	ع و	0.0405	0.0449	0.0647	2 2	0.1433	0.2867	3374	0.3918	0.4600																																		
		Attorbody	X/I.	_		419.13																																								
	1000					_							876	æ	828	3	8 .	. 5	. ×	3	. <del>.</del>	. 8	S 52	287	132	023	SOS :	12	22	àă	2 7	22														
,0 # 0°		e Formshode	CP			.6/ 0.0384					1.25 -0.3315				3.75 -0.2528		5,00 - 0,2528 5,00 0 - 0,528				50									0.000		15 -0.0022														
mfr = 0.74 and α = 0°			X		106.57	10.64-	,				_	_	.2	eri i	~; •	÷ •	ri <b>v</b>	, .	·od	9	12.50	<u> </u>	17.50	20	30.00	\$0.00	00:00	00:02	80.8	20.00	110.00	241.85														
mfr.0		Afterbody	පි	0.0279	0.0436	0.0028	0.1427	02113	0.2817	0.3286	0.3827	0.4481																																		
	ر م		XT	343.16	384.14	457.13	507.77	545.76	\$71.08	583.74	596.41	609.07																																		
	•	Forebody	ç	0.8981	0.8975	0.8469	0.7717	0.6899	0.5941	0.4581	0.2817	0.1881	0.0624	0.03/4	0.0630	0.032	0.8801	1040	1.1892	1,2126	0.9326	0.1436	-0.1929	-0.3525	-0.3240	-0.2825	0.3113	0.3032	0.1178	0.2989	0.2034	-0.3463	-0.3798	0.4291	0.4830	0.4760	0.4840	-0.4597	-0.4592	-0.4819	-0.5224	0.5425	0.5642	0.3873	0.000	0.0007
		Pon	X	-187.47	-171.29	130.84	-106 57	-90.39	-74.21	-58.03	41.85	-33.76	-25.67	11.67-	10.01	7.7	7	-2.05	060	4	0.00	0.31	0.63	1.25	1.88	2.50	3.13	0.5	9	6.25	7.50	8.75	000	200	17.50	20.00	30.00	40.00	90.00	90.00	0.00	80.00	8 8	1000	241.85	279.84
			. ه.	90	90 G	2 2	153	00	745	245	120	<u> </u>																																		
		Afterbody	X/L CP	-	14 0.0388							07 0.4514																																		
	• = 180°		*		79 384.14							11 609.07	2 3	3 5	2 ≎	: 5	2	<b>*</b>	2	8	7	9.	2	2	<b>3</b>	<b>.</b>	<b>x</b> :	. 9	2 22			0														
8		Forebody			0.8579								710077		7 -0 5787		5 -0.3546		5 -0.4130								0.5304			_	0.5387	90.0080														
mfr = 0.88 and α = 0°		-	χ	-187.47	-106.57	-10.27	-2.05	0.00	0.31	0.63	1.25	88.	7.30	175	4.37	2.00	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20:00	30.00	30.00	8 8	8 8	0006	100.00	110.00	241.83														
mfr = 0.		Afterbody	G	0.0250	0.0375	0.0806	0.1349	0.1978	0.2700	0.3166	0.3722	0.4394																																		
	<b>%</b> • •	Afte	X	343.16	410 13	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																		
	•	Forebody	CB	0.9579	0.9518	0.9179	0.8584	0.7953	0.7242	0.6235	0.5036	0.4484	0.3331	0.3954	0.5958	0.8502	0.9898	1.1186	1.2084	1.1968	0.7648	-0.0269	-0.4967	0.6333	0.6761	0.9871	0.5320	-0.4119	-0.4843	0.4403	-0.4366	0.4422	0.4/44	0.5142	0.5441	0.5401	-0.5351	0.5412	0.5435	-0.5361	0.5589	06113	0.6308	0.5558	-0.0087	-0.0050
		Fore	ž	-187.47	-171.29	130.84	-106.57	-90.39	-74.21	-58.03	56.14	35.76	73.11	17.97	-10.27	-5.13	3.34	-2.05	96.0	<b>4</b> .	000	0.31	0.63	1.23	88.	3 :	3.75	4.37	200	6.25	7.50	8.75	12.50	15.00	17.50	20.00	30.00	90.09	20.00	90,00	9 9	00.00	00:00	110.00	241.85	279.84
		_	. !	.0287	050	80	83	92	<del>,</del>	3053	<b>1</b> 8	ξ,																																		
		Afterbody		0 0			77 0.1183		•	•	1 0.3044	>																																		
	× 180			343.16	. •			30 545.76		-, .	2,000		. <u>.</u>		7	23	<u>-</u>	=	90	21	•	<b>.</b>	90.0	2. 1	P =	- 5		90	5	_	0	7														
.0 #	Ĭ	ğ		7 0.0089		_						0.00					5 -0.7587						0.6928								_	0.007														
mfr = 0.61 and α =		<u>.</u>	ָּבֶּ	187.47	-25.67	.10.27	-2.05	S 8	16.0 16.0	0.63	C7 :	2.50	3.13	3.75	4.37	2.00	6.25	7.50	8.75	10.00	12.50	15.00	17.5	80.02	2 5	9	70.00	80:00	90.00	100.00	110.00	241.85														
mfr = 0.		Afterbody	3	0.0203	0.0466	0.0749	0.1239	0.1836	15521	0.2987	0.0047	0.45.30																																		
	• = 0.	Affe	X :	384 14	419.13	457.12	77.70	545.76	271.08	583.74	600.00	6.50																																		
		Forebody	3	1.0127	8900	0.9806	0.9334	0.8863	0.830	0.7383	92190	0.5751	0.5893	0.6115	0.7808	0.9909	 	70	1.2095	1917	0.6217	0.2427	0.0413	7700.0	90780	0.8835	-0.8278	-0.7377	0.1179	0.7596	0.6311	0.0940	0.6801	0.6770	0.6689	-0.6527	# S	0.00	00/00	0.5998	-0.6385	0.6454	-0.6716	0.5961	0.0111	-0.0086
	ı	Fore	Z S	171.29	1155.11	-130.84	-106.57	6.36	17.4/-	38.03	77.55	-25.67	-23.11	17.97	-10.27	-5.13	ξ. (*)	-2.05	0.00	<b>\$</b>	8 6	500	0.03	7 8	5.5	3.13	3.75		2.00		7.50				17.50			3 5				_	_	_		279.84

TABLE VI. Continued

(k) Concluded

mfr = 0.81 and  $\alpha$  = 0°

 Forebody
 Afterbody
 Forebody
 Afterbody
 <th

TABLE VI. Continued

(1) M = 0.92

				×	۲.	n -	- ~	. ~	4	7	•	6																																			
		Afterbody	ට්	9.0555	0.0387	0.0413	0.0773	0.123	0.180	0.225	0.2759	0.345																																			
	80%	After	X	343 16	384.14	419.13	77.10	545.76	571.08	583.74	596.41	00600																																			
	<b>6</b> = 180°	yody	G	1.1431	1.1151	1.0245	1 2029	0.2292	-0.7160	-1.0567	-1.1762	1.1963	-1.1989	-1.1889	-1.1819	-1.1553	585	1.1094		10001	1006	-0.9873	0.9698	-0.9715	-0.8648	-0.7784	-0.7703	-0.7489	-0.7597	-0.7486	-0.7611	-0.7201	0.0784														
ndα≈0°		Forebody	χ	-187.47	106.57	10.62-	2.05	0.00										C7.0						20.00					_	_		110.00	241.85														
mfr = 0.40 and $\alpha = 0^\circ$		ھ				0.0372	0.0791	0.1256	0.1810	0.2205	0.2673	343																																			
fa		Afterbody			384.14 0.0					583.74 0.2		609.07 0.3																																			
	0 = <b>0</b>			_		14.29							1.0181	1.0252	1.0492	273	5508	7050	2 9	0.9386	01710	7	223	25	<b>24</b>	816	60	916	217	127	7	39	210	2 2	Š	ē	182	538	986	623	<b>184</b>	ž	E 5	2 5	ìş	3	œ Æ
		Forebody																	000			·					3.13 -1.1909					7.50 -1.0836		10.00					00 -0.7986					00 -0.7542			
		_	×	187.47	171.29	5.05	106.57	6	74.	-58.03	41.85	-33.76	-25.67	-23.11	17.97	10.27	5.13		•	Ģ		ó	Ö		_		e,		4	Š	ý	7.	oci (	12.50	200	17.50	20.00	30.00	40.00	20.00	90.09	20.00	80.00	8.8	10.00	241.85	279.84
		pody	Cb	0.0069	0.0446	0.0391	0.0510	0.0816	0.1259	0.1630	0.2052	0.2704																																			
	8	Afterbody	χŢ	343.16	384.14	457 12	17.705	545.76	571.08	583.74	596.41	609.07																																			
	<b>•</b> = 180°	od y	C	1.1752	1.1586	1 1010	1.1525	0.0614	-0.8737	-1.1754	-1.2881	-1.3165	-1.3277	-1.3133	1.2979	-1.2805	1107.1-	2007	3921	-1.1586	11153	601	-1.0763	-1.0431	-0.9649	-0.8314	0.8242	-0.8019	0.8070	0.7958	-0.7972	0.7619	0.0642														
dα = 0		Forebody	Χľ	-187.47	106.57	-10.27	-2.05										9				12.50							_			_		241.85														
mfr = 0.32 and $\alpha$ = 0°					0.0418	24500	535	0.0847	0.1278	593	003	0.2664																																			
nfr.		ţe.																																													
	• = 0°				384.14							0.609	- 1	× •	_ (	۰.	٠,	. 4	. 4		•	7	3	<b>∞</b>	7	6	<b>S</b>	۰	_	•	ο.	7 (	<b>.</b>			<b>ac</b>		_	•	•			•			_	<b>5</b>
		ě			19/11		_								1881			1542		0.8136					-1.3002		-1.3005						1.1769					-0.9661	-0.877	0.8326	0.8040	4218.0	5 70 6	0.00	-0.7716	990:0	0.0816
		P	Ž,	187.47	62.171-	300	106.57	.90.39	-74.21	-58.03	41.8	33.76	-25.67	11.67-	1671	10.27	5.15	2.05	6	9	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	8	6.25	7.50	2.3 2.5	12.50	15.00	17.50	20.00	30.00	809	20.00	90.00	00.07	80.00		110.00	241.85	279.84
		òdy	d C	0.0726	0.0472	0.0252	0.0319	0.0502	0.0823	3.1126	0.1466	1.2059																																			
		Afterbody		97.79								207.07																																			
	<b>\( \phi = 180^a</b>	ģ		8751.1								_	-1.3917	2815	1.3389	1,3331	07767	2739	2487	2241	1652	1533	1353	16601	9901	8488	8390	-0.8170	-0.8207	0.8051	0.8156	0.7736	03/4														
lα = 0°		Ę		-18/.4/													200		8.75					20.00								0.00															
Infr = 0.27 and $\alpha = 0^{\circ}$								13	7	<b>2</b>	23	٥								_	_	_	_	7	e-1	•	•	_	oco 1	σ.	≌ :	= ?	ξ.														
帛		Ę		0.0031						\$60.0 •		0.20.5																																			
	o = 0	7		36.10								965												_																							
		Forebody		1.191.1		_	_		1.1627	1.1531	1.1486	1.1480	1.1543	1.13/4	21.49	1 2 2	100	1.1089	0.9124										1.3406	1.3216	-1.2932	0607.1	35477	1.1853	-1.1685	-1.1349	-1.1176	1.0107	06160	-0.8766	0.8230	0.8103	0.8076	-0.8052	0.7684	0.0410	0.0752
		Po	Z S	4.181	(7.17)	130.84	-106.57	-90.39	-74.21	.58.03	8 1 8	97.79	.25.67	11.62-	7671	10.27	7 7	-2.05	060	4.0	000	0.31	0.63	1.25	1.88	2.50	3.13	3.75	4.37	200	6.25	S. 5	6.75	12.50	15.00	17.50	20:00	90.00	40.00	30.00	8.6	8.6	8.0	100.00	110.00	241.85	279.84

			۵	145	ē <del>[</del>	193	005	281	291	0.2833	£ ;	<u> </u>																																			
		å		0.0145																																											
	.081	Ą	ž	343.16	419.13	457.12	507.77	545.76	571.08	583.74	9864	0.600																																			
	<b>\( = 180^\)</b>	ody	CP	1000	0.8521	9696.0	1.2225	0.5245	0.3022	-0.7028	-0.9333	70807	0.9498	-0.9082	-0.8853	-0.8774	0.8343	-0.7919	0.7664	-0.7319	0.7055	0.7201	0.7516	0.710	0.886	1430	-0.5538	0.6013	-0.6251	0.6410	0.6146	0.0443															
mfr = 0.49 and $\alpha = 2.0^\circ$		Forebody	χ	-187.47	25.67	-10.27	-2.05					88.6											9.50			9	70.00	80.00	00.06	100.00	110.00	241.85															
0.49 and									<u></u>	77	£ .	6																																			
mf-		Afterbody	C		0.000							0.365																																			
	• = 0 <sub>•</sub>			_	584.14							0 609:07			~	_	_	7	4	0	_	0		n a	<b>.</b> o		. •	•	2	6	•	<b>0</b> 0 1	e c			• • <u>•</u>		<b>9</b> 2	9	Z	Ω.	<u> </u>	2 1	•	2 5	? =	:
		Forebody	Ç	1.1026	2 2	1.0870	1.0605	1.0323	1.0026	0.9659	0.9338	0.9240	0.9100	0.9443	1.0622	1.1801	1.219	1.2222	 25	960	0.2561	-0.6720	0.9642	1469	1 1458	11205	-1.1126	-1.1078	-1.0942	-1.07	1.0218	-1.0248	91001	0.0010	06960	0.9568	-0.8803	-0.8269	0.7940	-0.7802	0.7950	6.7915	0.795	0.7613	0.0000	0.000	2
		For	χŢ	-187.47	1551.	130.84	-106.57	-90.39	-74.21	-58.03	1.85	-33.76	10.02	-17.97	-10.27	-5.13	3.34	-2.05	8 9	<del>4</del>	0.0	0.31	0.63	C7:1	5.5	3.13	3.75	4.37	5.00	6.25	7.50	8.75	000	2.71	12.50	20.00	30.00	40.00	20.00	60.00	20.00	90.08	90.06	00.00	241 86	C0.1+2	•
		<u>~</u>	G.	0.0309	0.0315	0.0575	0.1019	0.1594	0.2289	0.2806	0.3409	0.4180																																			
		Afterbody	. 1		384.14 0.0							609.07																																			
	• = 180°		×										. v		04	11	35	92	56	8	<del>\$</del>	6	5 3	\$ 5	3 9	3 8	22	43	8	æ	<b>8</b> 8	56															
1.0°	•	rebody	G		0.0540							3 -1.0295								0.8250				0.704								5 0.0526															
and a *		Ē	X	.187.47	106.57	10.2	-2.05	0.00	0.31	0.6	1.25	88.	2.7	175	4.37	2.00	6.25	7.50	8.75	10.00	12.50	12:00	17.50	80.02	8.8	3 5	20.00	80.00	00.06	100:00	110.00	241.85															
mfr = 0.49 and α × 1.0°		yody	පි	0.0505	0.0444	0.0679	0.1095	0.1643	0.2258	0.2674	0.3155	0.3819																																			
Ē	<u>د</u>	Afterbody	χĽ	343.16	384.14	457.12	507.77	545.76	\$71.08	583.74	596.41	609.07																																			
	.0 = <b>6</b>	•	S.	1.1034	000	1.0845	1.0587	96707	1.0029	0.9606	0.9258	0.9126	0.8933	0.0075	10429	1.1703	1.2139	1.2234	1.1614	1.0197	0.3205	0.6182	-0.9397	-1.0983	-1.1089	600.1	10751	1 0657	-1.0356	-1.0069	0.9904	-0.9747	-0.9614	-0.9354	0.9340	0.000	0.8374	-0.7735	-0.7484	-0.7374	0.7427	0.7413	0.7466	0.7480	0.7240	0.0726	0.0471
		Forebody	Σ		171.29				-74.21				79.67									0.31				R:									00.51				50.00					_		241.85	17.04
				÷		7	Ŧ	7	`•	7	1	•			•																													_	- ,	•	•
		rbody	X/L CP	0.0408	0.0359	0.0463	0.1027	0.1585	0.2271	0.2753	0.3320	0.4043																																			
	180°	After	X	343.16	384.14	457.12	507.77	545.76	571.08	583.74	596.41	609.07																																			
	-	9	) ů	1.0973	1.0533	1.0195	1.2248	0.4231	-0.4862	-0.8706	-1.0511	-1.0742	500.5	5000	1 0098	-1.0039	-0.9457	-0.9262	-0.9025	-0.8814	-0.8433	-0.8770	-0.8627	0.8603	0.754	-C. /UIS	0.000	0.09	-0.7089	-0.7100	-0.6781	0.0588															
id α ≡ 0°		Foreh	X/L CP			10.52	2.05	000	0.31				2.50					7.50		10.00		15.00	17.50			8.8	8 6	000	800	100.00	110.00	241.85															
mfr = 0.49 and α = 0°							0.003	0.1609	262	0.2700	0.3237	0.3911																																			
n F		Afterbody	Č																																												
	وا 1	)  -	×	_		0 419.13					33 596.41	18 609.07	<b>=</b> :	8 5	ě	2	90	<b>~</b>	16	86	<b>58</b>	61	F	2	<b>9</b>	8 8	3 8	3 5	7 5	8	37		32	2	5 5	79.	9 9		8	62	35	36	4	ž	SG :	9	6
		Forebody	٥	1000	1.099	200	3	1.0261	0.9957	0.9542	0.9133	0.8981	0.879	0.880	1 0320	1.1563	1.2088	1.2251	1.169	1.0498	0.3458	0.5519	-0.8977	-1.0512	1.0759	9040	200	2010	0.9935	-0.9802	-0.9337	-0.9267	0.9092	0.9013	0.8607	0.8482	2618	-0.7258	0679 0-	-0.6829	-0.6835	-0.7056	0.7114	9669	0.6805	0.0616	0.0379
		9	3	187.47	-171.29	135.11	10.5	90.39		-58.03	41.85	-33.76	-25.67	12.07	10.77	-5.13	3.3	-2.05	0.00	0. 44.	000		69.0	1.23	88:	2.50	3.13		9	6.25	7.50	8.75	10:00	12.50	15.00	2 2	30.05	900	0000	90.00	00.07	80.00	90.00	00.00	10.00	241.85	279.84

TABLE VI. Continued

			Afterbody	AL CP						571.08 0.2779	_	596.41 0.3873																																			
		200 200 200 200 200 200 200 200 200 20		- 2							· ·		٠.	2 2	6.5	. *	2 2	2 2				×	23	20	2	~	-	63	2	<b>T</b>	<b>T</b>	<b>3</b> 7 9	· -														
9			Forebody	1024	_		_					200									-0.6427							-0.5633		_	_		0.000														
mfr = 0.61 and α ≈ 0°			¥ 5	-187.47	-106.57	-25.67	-10.27	-2.05	000	0.31	60.0	67.1	8° 5	7.		4 17	200	6.25	7.50	8.75	10:00	12.50	15.00	17.50	20.00	30.00	20.00	90.09	20.00	80.00	90.06	100.00	241 85														
mfr = 0.			Afferbody	0.0371	0.0457	0.0628	0.0876	0.1393	0.2020	0.2742	0.3213	0.4464																																			
	8	5 8	¥ Š	343.16	384.14	419.13	457.12	507.77	545.76	571.08	505.74	609.07																																			
	•		Forebody	1.0286	1.0286	1.0241	0.9974	0.9523	0.9025	0.8489	0.000	0.6565	0.6035	0.6038	0.6386	0.7948	1.0010	1.1040	1.1823	1.2145	1.1639	0.6492	-0.2052	-0.5866	-0.7955	0.8133	-0.8012	0.7922	-0.7612	-0.7102	-0.7328	0.0828	0.6575	-0.6478	-0.6339	-0.6512	-0.6547	0.6000	0.3640	0.3033	5858	0.5769	0.6190	-0.6306	0.6554	-0.6125	0.0244
		c	K FO	187.47	-171.29	-155.11	-130.84	-106.57		4.21	41.85	-33.76	25.67	-23.11	-17.97	.10.27	-5.13	¥.6	-2.05	06.O	4.0	0.00	0.31	0.63	1.25	88.	2.50	3.13	3.75	4.37	8.5	5.5	8.75	10.00	12.50	15.00	17.50	20.00	90.00	9.00	90.09	70.00	80.00	00:06	100.00	110.00	241.85
		-	à ê	0.0443	0.0400	0.0529	0.0697	0.1193	671.0	0.2513	1000	0.4313																																			
	•	A Description of the	X/I.					77.70																																							
	A = 180°		2 0	•	•	-		5 1777				_		-0.9662	9308	-0.9103	-0.9057	8533	8355	8126	-0.7728	1301	7710	-0.7653	0.7616	9060	-0.0436	93.4	-0.0432	0.6636	0.0000	0.6537	0.0465														
0 = 0°		Pomphodu	5			-25.67		507						3.13 -0		4.37 -0	_								00.02				_	90.00		_															
mfr = 0.54 and α = 0°								3 2	3 2	8 8	28	8:												•			.,	•	•	~ •	`` ≥	2 =	7.														
f i		Afterbody	ð		14 0.0388		75/00/57		78 0.7488			0.4206																																			
	.0 = <b>•</b>		×	_	_	419.13	•					Ī	2	::	9.	9.		2	<b>.</b>	m :	4 ,	۰.			•		, -			• =		. 80										_	<b>-</b>	~ .		• -	
		Forebody	G.	_		9607		Ī								_					1.1074			6.73			0.932							-0.7871				0.6701					0.6608	0.000	0.0893	0.0020	0.0451
			X,	187.47	-171.29	135.11	20.00	200	-7421	-58.03	41.85	-33.76	-25.67	-23.11	17.97	-10.27	5.13	 X	-2.05	<b>8</b>	<b>.</b>	500	6.90	136	C7:		1.3	2.5		200	6.25	7.50	8.75	0000	00.31	20.01	200	30.00	40.00	20.00	90.00	70.00	80.00	80.8	00.00	741 86	241.83
		rbody		0.0002	0.0226	0.040	100	0.1582	0.2299	0.2844	0.3460	0.4302																																			
	.08	After	χŢ	343.16	384.14	457.13	77.05	545.76	871.08	583.74	596.41	609.07																																			
	<b>\( = 180^\)</b>	ody	CP	1.0967	0.000	1000	1 2 193	0.6123	-0.2144	-0.6415	-0.8835	-0.9260	-0.9228	-0.8930	0.8597	-0.8014	0.8038	C. (.)	0.7319	7990'0	0630	13090	0.02.7	5894	-0.4975	0.4724	-0.4961	0.5124	0.560	0.5711	0.5999	-0.5806	0.0380														
mfr = 0.49 and α = 3.1°		Forebody	χŢ	-187.47	75.63												9 5		2						30.00		0009																				
. 0.49 an		<b>.</b>			00000	200	0.1135	0.164	0.2183	0.2519	0.2918	0.3482																					•														
Ė		Afterbody		343.16 0.0								0.609																																			
	• 0 •	>		1.1018	•								£ ;	2.	6 3	2 2	7 2	9 3		3 =	. 3	2	8	5	22	SS	8	\$	<del>-</del> 0	<b>4</b>	8	53	£ 8	₹ #	3	<b>9</b>	10	2	73	<del>د</del>	37	2:	2 %	3 =	: 5	: 5	<b>.</b>
		Forebody													26060 /6			2777			00 02264		63 -1.0306		88 -1.1852			1764						0.000.1		0 -1.0240						0 -0.8346		_			4 0000
		~	Χď	-187.47	-155.11	061	.106.57	-90.39	-74.21	-58.03	8.14	-33.76	70.62-	11.62-	16.71-	77.01-	2.5		060	2 4	000	0.31	0.63	1.25	8.1	2.5	3.1	3.7	4.3	5.00	6.2	7.50	× ×	12.50	15.00	17.5	20.00	30.00	40.0	20.00	0.0	00.00	90.00	100.00	10,00	241.8	279.84

TABLE VI. Continued

		yody	S C	0.0527	0.0769	0.1007	0.1610	0.2311	0.3583	0.4153	0.4801																																		
	٤	Afterbody	χ	343.16	419.13	457.12	507.77	545.76	201.00	596.41	10.609																																		
	081 = \$	. Ž		0.9147			···	0.9525				-0.2997	-0.2378	202	-0.2245	-0.1607	-0.2198	-0.2809	-0.2977	3593	-0.4088	426	-0.4275	104	0.4583	0.4691	2000	0.5335	0.582	0.5487	0.0223														
°0 ≈ α		Forebody						000					3.13 -0.	4.37									20:00			9000																			
mfr = 0.74 and $\alpha$ = 0°			×	187.47		•						,,	• `			Ĭ	•-	_	=	**	<b>=</b> :	- 1	≅ ₹	* i	<b>ж</b> ;	<b>3</b> 6	< 8	æ ð	ς Ξ	Ξ	24														
mfr = 0		Afterbody	Ç	0.0420	0.0753	0.1059	0.1631	0.2305	0 3408	0.4051	0.4694																																		
	o,0 = 0	Añe	χ	343.16	419.13	457.12	507.77	545.76	583 74	596.41	609.07																																		
	•		Cb	0.9197	0.9068	0.8660	0.7968	0.7146	0.0220	0.3157	0.2233	0.0909	0.0594	0.3873	0.7253	0.9004	1.0524	1.1987	1.2252	0.9380	0.1879	0.0993	0.3143	7107.0	-0.2081	0.2404	0.2219	0.2238	0.237	0.1955	-0.3046	0.3441	0.3782	0.4325	0.4363	0.4261	0.4421	-0.4699	-0.4647	-0.5166	-0.5340	-0.5598	0.5849	0.3037	0.0230
		Forebody	Χζ	-187.47	-155.11	-130.84	-106.57	80.3	17.5	28.4	-33.76	-25.67	-23.11	701-	-5.13	3.34	-2.05	0.00	<del>4</del> .	0.00	0.31	0.63	52 5	90.	2.50	3.13	0,70	ş 5	2,5	7.50	8.75	10.00	12.50	15.00	00.75	30.05	00.0	\$0.00	00:09	70.00	80:00	00.06	90.00	241.85	279.84
								vo a		. –	. <u>.</u>																																		
		Afterbody		0.0237				0.2186																																					
	\$ = 180°		ž	343.16	419.13	457.12	507.77	545.76			609:07																																		
٠.	*	Forebody	C	0.9714	0.3128	0.4992	1.0803	0.9765	0.5101	0.2876	-0.2003	-0.2224	-0.2024	9 9	0.1509	-0.1213	-0.1675	-0.2384	-0.2680	-0.3205	-0.3303	0.3878	-0.3786	97750	0.3678	0.4348	0.4060	0.4980	0.000	-0.5231	0.0294														
nd a = 2		For	χ	-187.47	-25.67	-10.27	-2.05	0.00	15.0	1.25	1.88	2.50	3.13	4.17	200	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.05	20.00	8 8	9.0	8 8	100.00	110.00	241.85														
$mfr = 0.68 \text{ and } \alpha = 2.1^{\circ}$		dy	c <sub>B</sub>	0.0674	27.00	0.1031	0.1569	0.2226	0.2720	0.3879	0.4487																																		
fin		Afterbody		343.16				545.76 0																																					
	.0 =						•					135	422	0.4300	559	108	1.1798	1.2286	1.1901	955	<u>\$</u>	575	8 8	2 2	752	269		5 55 5 75	200	880	639	54	920	654	9 8	268	115	976	640	277	414	557	35 55 56	26697	0.0266
		Forebody		47 0.9750				39 0.8202					0.4422												2.50 -0.7752	13 -0.7692	110.0- 6.61		82.50					00 -0.6654		000000		00 -0.5976					00 -0.6750		
		*	χ	-187.47	-155.11	-130.84	106.57	60.36	20 03	41.85	-33.76	-25.67	-23.11	-10.27	-5.13	3.34	-2.05	0.00	4.0	000	o .	o .		<u>-</u> •	~• •	mi r	· •	4. A	i •	7.	œ	.01	12.50	2000	≟ \$	20.02	900	20.00	90.09	70.00	80.00	83	100.00	24.10	279.84
		body	C.	0.0513	0.0724	0.0929	0.1517	0.2202	0.2570	0.4051	0.4737																																		
		After		343.16					501.00																																				
	081 = 0	dy.		0.9728 3				0.8407 5	_		-	-0.5958	6025	0.4675	4969	-0.3030	-0.3488	3539	-0.3739	3905	-0.4674	-0.4958	-0.4881	4914	-0.5087	0.5311	2000	0.5080	0.5783	0.5856	0.0313														
g = 0,		Forebody		187.47 0.				0.00				2.50 -0.		2	_		7.50 -0.	8.75 -0.										D 00			941.85 0														
mfr = 0.68 and α = 0°							•												-	_	_	_	7	- ·	•		- (	<b>20</b> C	`=	: =	75														
mfr =		Afterbody		0.0397				0.2181																																					
	.0 = <b>0</b>		X/L	343.16	419.13	457.12	507.77	545.76	507.74	596.41	609.07																																		
	•	Forebody	C.	0.9758	0.9692	0.9368	0.8783	0.8150	0.439	0.5258	0.4595	0.3808	0.3778	2000	0.8851	1.0105	1.1349	1.2238	1.2135	0.8135	0.0272	-0.4322	-0.5700	-0.5927	0.5435	0.5734	0.5321	0.3809	0.3043	0.3664	-0.4696	-0.4539	0.4041	-0.4603	0.4843	0.4922	0.4035	-0.5051	-0.5124	-0.5423	-0.5728	0.5960	0.6194	0.080	0.0218
		For	χΥ	-187.47	-155.11	130.84	106.57	60.3	17.47-	4.85	-33.76	-25.67	-23.11	7017	5.13	3.34	-2.05	06.0	4.0	0.00	0.31	0.63	1.25		2.50	3.13	5.73	4.37	3,5	7.50	8.75	10.00	12.50	15.00	00.71	20.00	8.8	20.00	00:09	70.00	80.00	90.00	00.001	241 85	279.84

TABLE VI. Concluded

(l) Concluded

o = 0			• = 180°	.081			•	0 =		: i	<b>a</b> 180°	90
ş	Afterbody	For	Forebody		Afterbody	For	Forebody		Afterbody	Pon	Forehody	Afterhody
χŢ	S.	χΓ	G.	χ	C <sub>P</sub>	XI	ප්	XI	ට්	, 2	ů	X Z
343.16	0.0422	-187.47	0.1319	343.16	0.0492	-187.47	0.1945	343.16	0.0649	-187.47	0.1025	343.16
Z :	0.054	106.57	0.1429	384.14	0.0520	-171.29	0.1239	384.14	0.0637	-106.57	-0.1482	384.14
457.13	0.007	10.62	0.4798	419.13	0.0703	-155.11	0.0355	419.13	0.0753	.25.67	-0.5565	419.13
200 77	0.000	200	0.000	507 77	0.0684	130.84	0.0399	457.12	86600	.10.27	0.0622	457.12
45.76	0.1931	900	1 0518	245.76	0.1280	00.00	0.1.00	17.00	0.1480	60.7.	0.8035	507.77
571.08	0.2485	0.31	0.4409	\$71.08	0.2497	74.71	0.102	27.70	0.2669	9.0	0971.1	97.79
583.74	0.2852	0.63	0.0932	\$83.74	0.2919	58.03	0 7368	\$83.74	0.202	0.51	0.0527	271.08
596.41	0.3262	1.25	-0.0381	596.41	0.3363	41.85	0630	4.4	3000	0.0	0.1671	506.74
609.07	0.3816	1.88	-0.0865	609.07	0.3926	-33.76	0.5413	609 07	0.3830		1 2	1000
		2.50	-0.1283			-25.67	-0.4073			2.50	000	0.00
		3.13	-0.0698			-23.11	-0.3498			1	0.1001	
		3.75	0.0927			1971-	0.1306			175	0 1038	
		4.37	-0.0621			-10.27	0.2555			4 33	0.0863	
		2.00	9600			-513	78690			8	0.000	
		6.25	-0.00			7	0.8371			90.4	0.000	
		7.50	0.1486			\$0.00	10101			7 6		
		8.75	-0.1738			8	1 1884			, ,	0000	
		10.00	0.2445			77	1 2164			6	9600	
		12.50	-0.2367				200			3 5	0.0629	
		15.00	-0.3394			0.31	0.2005			3 2	0.160	
		17.50	-0.3906			0.63	-0.2117			17.50	0.2171	
		20.00	-0.3655			1.25	0.3267			2000	1874	
		30.00	-0.3781			1.88	-0.3122			30.00	-0.2412	
		20.00	-0.4082			2.50	-0.2728			20.00	-0.3146	
		00:09	-0.4313			3.13	-0.2954			000	-0.3582	
		70.00	-0.4645			3.75	-0.2936			70.00	-0.4036	
		80.00	-0.5059			4.37	-0.2668			80.00	0.4638	
		00'06	-0.5282			\$,00	-0.2782			8 8	0.4875	
		100:00	-0.5686			\$29	A07704			8 8	0.107	
		110.00	0.5289			2.50	17170			8 6	0.7570	
		241.85	0.0168			8.75	30,00			241.85	0.0114	
						00'01	0.3472				2100	
						12.50	-0.4041					
						15.00	0.4779					
						17.50	-0.4682					
						20:00	-0.4981					
						30.00	-0.4875					
						40:00	-0.5175					
						20.00	-0.5336					
						00:00	-0.5238					
						70.00	-0.5379					
						80.00	-0.5849					
						00:06	-0.6068					
						100:00	0.6194					
						110.00	-0.5733					
						241.85	0.0182					

TABLE VII. PRESSURECOEFFICIENTS ONMODEL WITH NACA 1-85-100INLET AND A CONTRACTION RATIO OF 1.250

(a) M = 0.79

		юdу	G	0.0098	0.0409	0.0809	0.1357	0.2004	0.2462	0.2962	0.30																																		
	۰	Afterbody	χ	190.28	223.61	245.83	262.50	273.61	279.17	284.72	97.76																																		
	<b>6</b> = 180°	ķ		0.8910	_		_					1.3333	1 3633	1,4097	-1.1880	-1.1524	1630	-0.6398	4090	2512	1830	2174	2301	8707	0891	-0.1662	25	1360	1238	0.1032	-0.0914	0.0304	1000												
ο n α		Ę		94.32 0.1								7 67 1					5.00															90.00													
67 and			×	s, ≥	4	•		Υ .	_	_ `						•		•	,		=	₩.			4 7	h 4		. 2	(	œ	σ.	2 9	7												
mfr = 0.67 and α = 0°		Afterbody	C	0.0003	0.0244	0.0445	0.0816	0.1354	0.1961	0.2354	6687.0	0.347																																	
	್ರಿ		χŢ	173.61	206.94	223.61	245.83	262.50	273.61	279.17	71.697	290.28																																	
	.0 •		CP	0.8898	0.9121	0.9013	0.8662	0.8034	0.7431	0.6618	0.5504	0.4388	2000	0.2861	0.3332	0.5459	0.8254	0.9694	1.0982	1.1664	1.1329	0.5784	-1.5876	0810.1	7407	7.7	12701	-1.2415	-1.1996	-1.1601	-0.8708	0.4419	0.1822	0.2298	-0.2111	-0.2041	-0.1991	0.1629	-0.1467		0.1167	0.106	-0.0605	-0.0374	-0.0188
		Forebody	χŢ	54.32	-75.15	-68.05	-57.40	46.76	-39.66	-32.56	04.67	-18.36	7	10.14	7.88	4.51	-2.25	-1.46	0.00	-0.39	-0.19	0.00	0.31	0.62	C7:1	8 C	3.12	3.75	4.38	5.00	6.25	8.5	10.00	12.50	15.00	17.50	20.00	30.00	40.00	20.00	8 6	80.00	100.00	129.17	145.83
									_																																				
		Afterbody	C	0.0178	0.0463	0.0906	0.1435	0.1992	0.2374	0.2797	0.330																																		
	.08 180		χŢ	190.28	223.61	245.83	262.50	273.61	279.17	284.72	290.28																																		
<b>°</b>	081 ≃ •	body	CP	0.8918	0.8066	0.3635	0.6276	1.1327	0.4676	-1.6782	-1.7538	1.6734	700.1	1.3278	1 1743	1.3473	-1.3145	-1.2366	1.1899	-0.8520	-0.5461	-0.2743	0.1584	0.1517	2,1012	9 19 9	0 143	0.1379	-0.1237	0.1040	-0.0902	0.0508	-0.0301												
d a = .2.		Forebody	χŢ	<b>24</b> .32	46.76	-11.26	4.51	0.90	0.00	0.31	0.62	1.25	6 6	2.50	3.75	4.38	2.00	6.25	7.50	8.75	10.00	12.50	15.00	2.58	20.02	8.8	8 9	8 8	20.00	80:00	00:06	00.00	1.67												
mfr = 0.67 and $\alpha$ = .2.0°			G	0.0205	0.0013	0.0396	0.0792	0.1335	0.1949	0.2385	0.2936	0.3668																																	
mfr -		Afterbody		•																																									
	0 H		×	173.61			•		•	•	•	6 290.28	n ;	9 5		2 2		<b>1</b>		23	11	92	<b>3</b> 3	£. 5	2 9	2 1	2 2	2 2	. 2	80	23	<b>×</b> :	e e	8 8	<b>.</b> 25	ā	∞_	13	<u>~</u>	8 :	÷.	£ &	: =	: 5	**
		Forebody			0000									0.2380				0.9144					1.4663		-1.5412			2012/0- 5						0 -0.2369							0 -0.1243				
		Po	XT	-94.32	75.15	-68.05	-57.40	46.76	-39.66	-32.56	-25.46	.18.3	14.51	97:11	1 88	4.5	.2 25	- 4	96.0	-0.39	0.15	0.00	0.31	0.62	9	88.	7 .		35.3	200	6.25	7.50	8.73	12.50	15.00	17.50	20.0	30.00	40.0	20.00	90.00	8 8	10000	129.17	145.83
		•	۵,	0.0042	0.0104	721	0.1229	822	0.2261	736	0.3321																																		
		Rerbod																																											
	- 180	2			20034		_	_	_	•	8 290.28	<b>9</b> 2 !	= :	20 3	2 5	. 5	2 5	. 25	. 22	2	22	88	<b>4</b>	<b>&amp;</b> :	2:	<u>.</u>	5 5	2 8	; <del>1</del>	: 16	22	<b>4</b>	<del>2</del>												
&	•	Forebody	ភ		0.934			1.1417	_					9 -1.5826			09/21-					0 -0.2058				0.1691					Ė		7 -0.054												
and a		ĕ	χZ	94.32	46.75	-11.26	15.4	06:0-	0.00	0.31	0.62	1.25	1.88	2.50	3.12	4.28	8	6.28	7.50	8.75	10.00	12.50	15.00	17.50	20.0	90.00	8.8	8 8	2008	80.00	90.00	100:00	129.1												
$mfr = 0.61 \text{ and } \alpha = 0^{\circ}$		ě	දී	-0.0072	0.0025	0.0139	0.0724	0.1239	0.1807	0.2179	0.2646	0.3239																																	
a	•	Afterhody	XL		190.28	723.61	245.83	262.50	273.61	71.672	284.72	290.28																																	
	9. •	•			0.9515						0.6759	0.5947	0.5592	0.4981	0.4894	0.5251	2000	10433	200	1.1475	1.0780	0.4586	-1.6781	-1.7052	-1.6274	-1.5669	80.0	1.4419	1.3378	-1.2877	1.1804	-0.9998	-0.6517	0.4733	0.62.0	0.1548	0.1934	-0.1642	-0.1736	-0.1408	-0.1533	-0.1257	0.048	0.0574	0.0450
		Forehode	Z,		82.25 0.						-25.46 0					0 27.										F					6.25			30.02			20.00				80.08		90.00		145.83

TABLE VII. Continued

(a) Concluded

	9081 - 4	= 180 ************************************	•	2005	206.94	223.61	245.83	262.50	273.61	279.17		290.28		•	٥	•	,		_		•			_	_	_		_																						
్రి	•	Forehody	2	0.8251	0.8448	0.7062	-0.0243	0.2978	1.0119	0.7448	-1.3758	1.4603	1.2490	-1.2469	-1.1739	-0.9736	0.757	-0.2801	0319	0.536	0.222	0.243	0.240	-0.2491	-0.2400	<u>\$</u>	-0.187€	-0.1523	-0.1385	-0.1224	-0.1287	-0.1137	-0.1038	0.0861	-0.0460	-0.0276														
mfr = 0.74 and $\alpha \approx 0^\circ$		For	X	94.32	-82.25	46.76	-11.26	4.51	06:0-	0.00	0.31	0.62	1.25	1.88	2.50	3.12	3.75	4.38	8.	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	30.00	40.00	20.00	90.00	70.00	80.00	00:06	00:00	129.17														
mfr = 0.7		Afterbody	8	0.0039	0.0179	0.0304	0.0532	0.0954	0.1489	0.2124	0.2520	0.3056	0.3687																																					
	ر تا 4		X	173.61	190.28	206.94	223.61	245.83	262.50	273.61	279.17	284.72	290.28																																					
	•	Forebody	å	0.8220	0.8442	0.8502	0.8351	0.7893	0.7092	0.6291	0.5200	0.3730	0.2056	0.1182	0.0131	0.0570	0.0344	0.203	0.0480	2.041.3	1.0224	484	1.1633	0.7578	-1.4212	1.4071	1.2804	-: 1 <b>99</b> 1	-1.1158	-1.0254	-0.9463	-0.5590	-0.3307	-0.2407	-0.2196	-0.2459	0.2452	-0.2593	0.2348	-0.2122	Q .	6.1.0	-0.1334	-0.1237	0.1213	0.1129	0.0996	0.0499	0.0300	-0.0172
		For	X	-94.32	-82.25	-75.15	-68.05	-57.40	46.76	-39.66	-32.56	-25.46	-18.36	¥.	11.26	-10.14	1.88		C7.7.	<del>2</del> 2	S, o	<b>2</b> € 5	-0.19	000	0.31	0.62	1.25	<b>86</b>	2.50	3.12	3.75	4.38	200	6.25	7.50	8.75	10.00	12.50	13.00	17.50	20.02	3 5	90.00	20.00	90.00	00.00	80.00	00.00	129.17	145.83
	200	Afterbody	X/L CP						273.61 0.1960		284.72 0.3018	290.28 0.3765											,																											
•	<b>•</b> = 180°	Forebody	Ç	0.8914	0.9096	0.7992	0.2196	0.4369	/750.1	2007	386	-1.4333	0.5140	766771.	1.1220	0.050	0.3510	0.77.0	072.0	7 2264	0 2 2 8 7	0.22.0	07770	0.226	0.1940	000.00	00170	0.1373	0.1280	0.1209	-0.1209	-0.1083	-0.0957	0.0878	-0.0452	-0.0283														
and $\alpha=2$		Por	χ	-94.32	-82.25	46.76	-11.26	2.5	96.0	3 :	50	70.0	9 8	8 9	9 5	3.15	7 76	9 5	6.25	5	2 ×	5.5	2 5	9 5	2 2	2 2	8.8	30.00	90.00	2000	90.09	20.00	80.00	800	0000	1787														
mfr = 0.67 and $\alpha$ = 2.1°		Afterbody	පි	0.0138	0.0170	0.0263	0.0460	1990	0.1410	0.130	0.1719	0.2710	0.3136																																					
Ħ	,0 = <b>0</b>	Affei	ž	173.61	190.28	206.94	123.01	243.83	272.50	270.17	204 73	200.000	07.74																																					
	٠	Forebody	g G	0.8922	0.909	0.9126	0.9049	0.6081	0.000	0.469	0.000	0.000	0.4180	0.3868	0 1747	0.4247	0.6154	0.8917	1.0236	1.1312	1.1639	1.0986	0.4430	1.6743	1 7167	8599	2000	1 533	7676.	4664	7765-1-	4	1.3317	06571	7 1002	0.6973	04110	-0.2217	91710	-0.1478	0.1658	-0.1586	0.1409	136	08110	0.118	9900	00300	0000	2
		Po	χ	-94.32	57.78-	50.05	-08.03	04.1C	30.66	32.00	25.46	78 34	18 71	-11.26	7101	-7.88	4.51	-2.25	-1.46	06.0	0.30	010	000	0.31	0.62		8	0 60	5.5	3.12	2.5	8. 3	200	67.0	0.7	0001	12.50	15.00	05 21	20.00	30.00	40.00	20.00	00.09	20.00	900	10000	129.17	145.83	

TABLE VII. Continued

(b) M = 0.84

		_	. 3	3 2	2 2	8	\$	2	8		28																																					
		Afterbody		•	000	0.0606				0.2501																																						
	\$\phi = 180^c	Ş	X 5	206.28	223.61	245.83	262.50	273.61	279.17	284.72	290.28																																					
	# <b>⇔</b>	Forebody	<u>ئ</u>	07507	1.0127	0.8211	0.9721	1.1915	0.2688	-1.6302	-1.7129	1.6331	-1.6260	1.6104	1.5498	-1.4468	1.4346	500	3008	1.2641	1.1924	1.1496	-1.0638	0.9952	-0.9423	0.8547	-0.1520	-0.0559	1600	0.1139	9	0.08	0000	0.0436	-0.0484													
ndα=(		Fore	<b>X</b>	25.56	46.76	-11.26	4.51	0.90	000	0.31	0.62	1.25	.88	2.50	3.12	3.75	80.0	3	6.25	7.50	8.75	000	12.50	12:00	17.50	20.00	30.00	40:00	20.00	90.00	90.0	80.00	8 8	3.5	179.17													
infr = 0.49 and $\alpha = 0^{\circ}$		÷.	<u>د</u>	0.0142	0.0076	0.0259	0.0633	0.1064	.1623	.1995	0.2452	3075																																				
n T		Afferbody	ZZ.					262.50 0			284.72 0																																					
	0=0			0630									0.8460	1204	270	7492	0.9623	<del>2</del>	88	1837	69	888	629	-1.6251	-1.6724	-1.6058	5853	-1.5650	5503	80	-1.4066	3671	5167.1-	6067.1.	51/1	200	0.9853	9374	-0.8544	1837	17.70	0851	1204	1201	-0.1090	0800	0.0534	0.0457
		훋	XI.											_								61.0							3.12							12.50			20.00			_		_				45.83 -0.
			× ;	* 6	57-	<b>%</b>	ŀ	₹	ę.	-32	. <del>.</del>	<b>=</b> -	ż	₹	j.	٠,	Ψ,	7	7	Ÿ	Υ.	Υ	_	_	_	_	_				•				~ =	: -	: 24	_	- ۳	~	₹	~	Þ	7	æ	2	12	4
		body	ď	0.0040	00180	0.0519	0.0959	0.1471	0.1847	0.2336	0.2925																																					
		Afterbody	ž	190.28	223.61	245.83	262.50	273.61	279.17	284.72	290.28																																					
	• = 180°	ody	c <sub>P</sub>	1.0535	1 0138	0.8397	0.9954	1.1897	0.2149	1.6639	-1.7279	-1.6643	-1.6479	-1.6529	-1.6268	1.5630	1.4723	-1.4530	-1.3685	-1.3062	-1.2398	1.2071	-1.1216	1.0634	-1.0192	-0.7262	-0.2845	-0.0432	-0.0741	-0.1058	0.1047	0.1032	0.0851	0,00	-0.0355													
a = -1.0°		Forebody	ž	.94.32	-46.76	-11.26	4.51	-0.90	000	0.31			1.88							7.50						20.00			20:00	90:09	20.00	80.00	90.00	000	129.17													
<b>mfr = 0.49 and α = -1.0</b> °		>	و.	0.0256	-0.0083	203	0.0553	8660.0	0.1577	0.2000	0.2492	0.3124																																				
Ef.		Afterbody		•				_				290.28 0.3																																				
	0=0		~		•				•				2	4	Z,	11	<b>6</b>	S)	2	7	22	31	<b>Z</b>	æ	3,	11	72	376	22	25	53	65	4 :	3	<b>9</b> 9	2 3	3 5	2 :	. 99	<u> 4</u>	5	610	128	98	180	.47	868	36
		Forebody		1.0517									1 0.8280		4 0.8034						9 1.1375			11 -1.6130			1.5572			15 -1.4325					75 -1.1365						0.0871					Ċ		83 -0.0336
		Ē	×	¥ 32	21.25	-68.05	-57.4	-46.76	-39.6	-32.56	-25.4	-18.3	-14.81	-11.2	-10.14	-7.88	4.51	-2.25	7.	Ģ.	-0.39	Ş	9	0.31	0.62	2	3.	2.50	<u>.</u>	3.	4.38	). S	6.25	<del>.</del> .	8.73		15.	2	20.00	9	9	20.00	90.00	90.	80.00	100.00	129.17	145.83
		ody	G.	0.0064	0.0157	0.0569	0.0959	0.1454	0.1794	0.2196	0.2755																																					
	۰	Afterbody	χŢ	190.28	1916	245.83	262.50	273.61	71.61.2	284.72	290.28																																					
	<b>081 = </b>	dy	c b		7697							1.6955	·1.6862	-1.6889	-1.6816	.6443	-1.5778	5312	-1.4418	.3761	.3234	1.2924	1959	.1639	6690	-0.9398	-0.4033	-0.1465	.0555	-0.0876	1000	.0975	6060	0.0497	0.0415													
t = -2.1°		Forebody		94.32		11.26		_							3.12 -1				6.25 -1											00:00			_	00.00														
mfr = 0.49 and $\alpha$ = -2.1°				•							22	21																-						_	-													
mfr = 0.		Afterbody			8 -0.0093							8 0.326																																				
	°0 = <b>0</b>	¥		3 173.61									2	_	Ca.	3	2	0	-	7	\$	<b>.</b>	•		90	.0	90	_	۰	1	5	<b>3</b> 7	2		<u>.</u>	2 '	2 9	<u>.</u>	5 2			· •		ور	2	<u>~</u>	28	13
	,	Forebody	C	1.0533	1.0589	1.0580	1.039	1.0094	0.9790	0.9435	0.8945	0.846	0.8292	0.7951	0.8002	0.823	0.9312	1.0860	1.1561	1.1862			0.3420	1.5748	-1.6188								1.1662				0.000								_	_	Ċ	
		For	X/L	.94.32	-82.25	68.05	-57.40	-46.76	-39.66	-32.56	-25.46	-18.36	-14.81	-11.26	-10.14	-7.88	4.51	-2.25	1.46	-0.90	-0.39	-0.19	0.0	0.31	0.62	1.25	1.88	2.50	3.12	3.75	4.38	8:00	6.25	7.50	8.75	3 9	05.21	3 5	20.00	30.02	40.00	9	0000	70,00	80.00	100.00	129.17	145.83

TABLE VII. Continued

				. 6	S :	8 12	<b>₹</b>	89	<b>8</b>	23	6																																		
		Afterhody	2	•	0.0050		0.1041																																						
	1900		X	190.28	206.94	245.83	262.50	273.61	279.17	284.72	290.28																																		
<u>.</u>	•	Forehody	ð	1.0485	1.0588	0.7668	0.9055	1.1872	0.4136	-1.5558	-1.6255	1.3100	1.4387	-1.3263	-1.2473	-1,2077	-1.1755	-1.1159	-1.0124	0.961	200	0.8170	-0.2692	-0.1598	-0.1094	-0.1278	-0.1366	-0.1418	-0.1300	-0.1171	0.0980	0.0393													
mfr = 0.49 and α = 3.1°		Fore	Ž	-94.32	-82.25	-11.26	4.51	06.0	0.00	0.31	79.0	67.1	2.50	3.12	3.75	4.38	2.00	6.25	5	8.75	8 5					40.00	20.00	90.00	20.00	80.00	8 8	129 17													
0.49 an		٠	් දී	0.0073	0.0093	0.0299	0.0572	0.0881	0.1200	0.1486	0.1719	117																																	
mfr.		Afterbody				_		_																																					
	9		X			_					2007		. ~		<b>a</b> .	•	œ						•	<b>.</b>	<b>.</b>	-	~	_	_	_			_	_	_	_	_								
		Porebody	පී	1.0518	1.0587	1.0581				0.9521						1.0264	1.1368	= :	5	1.0741		-0.9283	-0.745	-0.804	-0.8615	0.848	-0.883	-0.8323	-0.8877	0.8051	0.8457	-0.8589	-0.8818	0.8759	0.8640	0.8310	0.8294	0.6903	0.4899	4.4.7 C.74.74	0.466	-0.1455	0.0526	-0.0271	-0.0256
		Po	X	-94.32	25.15	-68.05	-57.40	46.76	-39.66	-32.56	18.36	14.81	-11.26	-10.14	-7.88	4.51	-2.25	-1.46 6	2 2	\$ 9 7 0	2	0.3	0.62	1.25	1.88	2.50	3.12	3.75	4.38	8	6.25	8.75	10.00	12.50	15.00	17.50	20.02	90.00	8 8	8 8	900	80.00	100.00	129.17	145.83
		<b>^</b>	۵.	0.0079	0.0070	0.0575	0.1059	0.1640	Ξ ;	553	707																																		
		Afterbody	C C	1						78 0.2055																																			
	= 180°		×	7 190.28		_	_			700.70		. ~	. ~	•	on.	~		٠,					_	_	~:	_	_	_																	
2.0°	٠	Forebody	G.	1.0527	1.0112	0.7886			0.3838									96.1.1		0.000	D 8867	-0.8279		-0.4193	-0.087	0.1019	-0.1203	-0.1287	0.1221	4.0.114	0.036	0.043													
≖ pud α =		F.	XT	24.32	46.76	-11.26	4.51	0.90	000	0.51	1 25	86.	2.50	3.12	3.75	4.38	2.00	\$7.0	0.0	0.0	12.50	15.00	17.50	20.00	30.00	40.00	20:00	90.00	20.00	0000	8 8	129.17													
mfr = 0.49 and $\alpha$ = 2.0°		ody	C.	0.0037	0.0117	90000	0.0638	0.1059	0.1500	6781.0	0 2754																																		
ŧ		Afterbody		173.61				_	273.61																																				
	e0 ⊕			1.0538					0.9800				0.8578	0.8644	0.9047	0810.1	<b>2</b>	100	1000	777	0.1501	823	329	757	269	8	421	<b>Ž</b>	354	3 3	256	202	998	08.	<b>2</b> 9	75	2 4	2 2	3 8	<u> </u>		52	181	4	89
		ě			_																	•								0.4935 W			0 -1.2866		911.149									·	3 -0.0368
		_	×	-94.32	-75.15	-68.05	.57.40	46.76	39.00	25.46	18.36	-14.81	-11.26	-10.14	7.88	2 5	77.	9 0	0.0	Þ	000	0.31	Õ	_	.88		ണ്	3.75	8.4	3000	7.50	8.75	10.00	12.50	8.5	5.7	3 6	80.05	909	900	20.00	80.00	100.00	129.17	145.6
		ody	CP	0.0055	0.0208	0.0563	0.1015	0.1599	1507.0	3253																																			
	۰	Afterbody		190.28			262.50			290.28																																			
	<b>6</b> = 180°			1.0433		_		2 0840			_	-1.5820	-1.5602	-1.4870	20	9 8	2 5	884	3	8	832	-0.9487	553	¥ :	296	24.5	187	<b>5</b> 8	-0.1279	, 6	189	459													
r = 1.0°		Forebody		.94.32 L(		11.26 0.7		2						3.12 -1.4		2 2		3.5		1000					30.00			0000																	
mfr = 0.49 and α = 1.0°			^			•	Ψ,					_	7	-	,,,	•	~ <b>4</b>	, ,		, ⊆	12	21	-	2 :	8 8	₹ :	S. S	8 8	2 8	3 8	100.00	129													
nfr = 0.		Afterbody	රි	90000	0.0058	0.0268	0.0626	50.0	0.1339	0.2347	0.2904																																		
-	°0 =	Affe	ž	13.61	206.94	223.61	245.83	05.202	279.17	284.72	290.28																																		
	•	body	S	1.0452	1.0603	1.0574	1.041	80103	0.9629	0.9057	0.8579	0.8447	0.8275	0.8403	0.8952	1363	1.1202	1843	100	0.9629	0.1955	-1.6577	-1.7012	-1.0003	1.6371	C010.1-	86/57-	-1.3333	1.4640	1 1787	-1.3026	-1.2526	1.2113	-1.1233	1860.1-	0.9380	7.02.0	-0.0513	-0.0748	0.1046	0.1176	-0.1091	0.0551	0.0451	0.0374
		Forebody	ž	\$ .54 .32 .82 .83	-75.15	-68.05	-57.40	97.0	32.66	25.46	-18.36		-11.26					9		-0.19					200									2.50				00.0		_	00:00	_	_	_	145.83
																																												-	

TABLE VII. Continued

		dy	G G	0.0294	0.0441	0.1075	0.1699	2318	0.2725	3173	0.3660																																		
	s.	Afterbody			200.94						280.78																																		
	= 180°	ody			7856.0					_	1.5477	-1.4848	2886	2007	03661	-1.1887	1.1580	-1.1053	-1.0592	1.0154	-0.9994	0.9184	0.8696	-0.3882	0.1988	0.0883	308	0.1356	-0.1242	-0.1064	-0.0879	0.0443	-0.0277												
lα=-2.1°		Forebody	χ	-94.32	82.25	11.26	4.51	06.0-					89.7									12.50				8 6		900		_	90.00	100.00	129.17												
mfr = 0.67 and α = -2.1°		φ	c.	-0.0127	0.0120	0.0564	0.1005	0.1579	0.2271	0.2729	0.3293	0.4027																																	
fi -	•	Afterbody			300.28							290.28																																	
	0) = <del>0</del>		_		0.9356							0.4482	0.3834	0.3034	71010	0.4814	0.7659	0.9280	1.064	1.1823	1.1796	0.7543	1.2697	1.2829	7507	1,000	09990	0.9311	0.8913	-0.8580	-0.5533	-0.3924	0.1449	0.1.504	0.2020	0.1903	-0.1820	-0.1512	-0.1357	-0.1258	0.1249	0.1130	0.00	0.0261	0.0072
		Porebody			-82.25				-39.66		-25.46			97.1										0.62		28.5								8 9								00.00			145.83
			_	8	2 5	3 8	2 8	37	<b>3</b>	<b>8</b>	<u>-6</u>																																		
		Afterbody	L CP		0.0310						28 0.3691																																		
	.081 = 0		^	_	30 206.94						144 290.28	91	2 5	2 6	\$ 8	202	83	22	323	60	354	916	18	733	<u> </u>	<u> </u>	2 5	2 2	23	91	935	492	376												
°0 #		Forebody	r Cb		82.25 0.9850			_	_					250 -1.3633						8.75 -0.9909	10.00 0.9354	12.50 -0.8616				30.00 -0.1109				_	_	00:00 -0:0492	.17 -0.0376												
mfr = 0.61 and $\alpha = 0^{\circ}$		_	χ	·	•						-		- '	7 .		. 4	•	٥	7	•	2	12	51	= ;	2 5	₹ ₹	2 \$	₹ 5€	2	8	8	9	52												
mfr • (		Afterbody	පි		0.0150							8 0.3614																																	
	°0 = 0	¥	ž	_	190.28	•						290.28				_	_	_	_	_				_						_	•	<b>~</b>	•	•					_		yo.	•	n -		. •
		Forebody	S		0.9823									0.5435							1.1171					1.3067						0 -1.0266			0.6563					_	_	0.1264			
		F	X	-94.32	-82.25	68.05	-57.40	46.76	-39.66	32.56	-25.46	-18.36	14.81	-11.26	10.14	7	22.6	+	06.0	-0.39	Q.	0.0	0.31	0.62	1.25	88.7	200		4.38	200	6.25	7.50	8.75	10.00	0.21	2.0	2000	90.00	40:00	20.00	00.00	20.00	80.00	120.17	145.83
		Apoc	ಕ್ಷ	0.0040	0.0214	7,770.0	0.1250	0.1850	0.2270	0.2747	0.3386																																		
	•08	Afterl	X/L CP	190.28	206.94	10.622	262.50	273.61	279.17	284.72	290.28																																		
٠	o = 180°	Forebody	ට්	1.0200	1.0299	0.9670	0.8879	1.1862	0.3683	1.5641	-1.6419	-1.5487	-1.5221	-1.4951	-1.4524	13000	3675	62.1	38	-1.0613	-1.0360	-0.9460	-0.8792	0.8234	0.4669	0.0764	6160	561.60	0.1289	-0.1115	-0.1012	-0.0491	0.0410												
nadα = 0		Fore	ž	94.32	-82.25	40.70	15.4	06.0	000	0.31	0.62	1.25	<b>8</b> 8.	2.50	315		8 5	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	9000	3 6	8 8	8 6	80.00	00:06	100.00	129.17												
mfr = 0.55 and α = 0*		À	ð	-0.0116	0.0014	0.0154	00773	0.1290	0.1853	0.2230	0.2706	0.3303																																	
a	ٷ	Afterbody	X		190.28	200.5	245.83	262.50	273.61	279.17	284.72	290.28																																	
	e U.		ð	1.0185	1.0284	1.0323	000	0.9653	0.9297	0.8830	0.8245	0.7673	0.7405	0.7048	0.7059	0.1372	0.000	1303	1.1821	1.1551	1.0498	0.3835	1.5341	-1.5840	1.4986	1.4776	¥.	-1.4162	1 2884	-1.2634	.1.1820	-1.0979	-1.0437	1.0167	0.9498	0.8923	0.5507	0.0711	0.1007	-0.1105	-0.1392	-0.1285	0.1122	7100.0	-0.0314
		Forehody	X	-94.32	-82.25	-75.15	-08.05	4 5	39.66	-32.56	-25.46	-18.36	-14.81	-11.26	-10.14	88/-	7 6	146	6	0.39	-0.19	000	0.31	0.62	1.25	88.	05.2	3.12	6.73	2.00	6.25	7.50	8.75	10:00	12.50	8 5	0000	30.05	000	20.00	90.00	00.00	80.00	130.00	145.83

TABLE VII. Continued

			ž č	66000	0.0302	0.0583	26.7	0.2312	.2825	0.3399	0.4119																																		
			Arterbody VA CD				0 05 09				290.28 0																																		
			•	_	•							0 9	2 5	. 9	2 95	2	ō.	-			ŗ		4.	٠.					'n	۲		Ψ,	<b>.</b>												
.0		•	d Dogar	-		0.8375							1303									0.1347						-0.128	-0.118	0.100	-0.083	0.038	47.021												
and a =		ā	X.	¥.	-82.25	5.5	4	06.0	000	0.31	0.62	1.25	1.88	3.15	3.75	4.38	2.00	6.25	7.50	8.75	00.00	12.50	3.00	2 6	9 9	000	80.00	90	70.00	80.00	90.00	00.00	172.11												
mfr = 0.67 and α = 1.0°		÷	2 0	0.0119	0.0155	0.0295	6101	0.1609	1,2262	2682	3155	0.3739																																	
Ę		Acharbada	X/L			206.94	_		273.61 (		284.72																																		
	•	• •		_		0.9436	_	_	_			0.4940 0.450x	0.1800	0.3726	232	131	796	232	339	1.1907		757	70	<b>.</b>	3	8	93	£03	120	132	E :	\ 0 0	2 2	53	97	<b>6</b>	9	z	Z :	g :	<b>.</b>	77 82	2 6	: \$2	28
		Powohody	S S																			0.5757									5 -1.0477								0.1264		0.1241				3 -0.0128
		-	X	-94.32	-82.25	50.89	-57.40	46.76	-39.66	-32.56	-23.40	9839	1 26	-10.14	-7.88	15.4	-2.25	1.46	06.0	0.39	(C) (C)	90.0	690	1 25	1.88	2.5	3.12	3.75	£	2.00	6.25	00.90	10.0	12.50	15.00	17.50	20.00	900	90.0	20.0	8.6		10000	129.17	145.83
		Š	දී දී	0.0212	0.0365	0.1031	1638	0.2302	15791	0.3334	101																																		
		Afterbody	XL		206.94	_				284.72 0																																			
	• 180°			_								<u> </u>	2	83	£	<u>.</u>	2	£ :	<b>•</b> ;	8 9	7 8	Q =	: 4	53	57	13	86	53	8	<b>2</b> !	S 8	. <b>*</b>													
.0 = 1		Forebody	3		25 0.9422		-	_		13/20						1.0401						0 -0.1811		0 -0.0929							0.0907														
7 and o		2	` <b>X</b>	.94.32	82.25	-11.26	4.51	06.0	000	0.51	70.0	7 8	2.50	3.12	3.75	4.38	90.	6.25	<b>3</b> . 5	8.73	8 5	15.00	17.50	20.00	30.00	40.00	20.00	90.09	00.07	80.00	900	129.17													
mfr = 0.67 and α = 0°		pody	පි	0.0055	0.0199	0.0572	0.1031	0.1624	0.2288	0.1268	0 2804	6.30																																	
-	؞	Afterbody	χΥ	173.61	200.28	223.61	245.83	262.50	273.61	284 72	2002	270.40																																	
	0 =		5	0.9241	0.9409	0.9337	0.8997	0.8344	0.7750	0.0994	0.4870	0.4351	0.3406	0.3201	0.3812	0.5817	8487	900	2011.1	1589	0.6587	-1.3814	.1.3938	-1.3587	-1.2779	1.1867	-1.1515	1229	20.5	- 15 S	0.900	8783	-0.8185	0.6809	-0.2149	0.1387	3	-C.1443	0.1347	148	-0.1217	-0.1088	0.0543	0.0328	0.0127
		Forebody		94.32				46.76										9 6												200						17.50		3 6				_	_	_	
			^	ه به	, i	: <b>-</b>	Ϋ́	₹ ?	÷ +	7	1 =	÷	7	ĭ	٠,٠	٠,	7	, ,	, `	7 4			J	_	_	7	•		•	~ 4	~	•	01	≃ :	≏ :	2 5	3 5	2 \$	3 5	8 8	2	<b>8</b>	<u>8</u>	129.17	145
		body	CF CF	0.0252	0.0569	0.1066	0.1663	0.2351	0.279	0.3862																																			
	క	After	ž	190.28	223.61	245.83	262.50	273.61	784 77	290.28																																			
	<b>081 = </b>	dy	CP	0.9243	0.8371	0.3622		1.1316		4963	14160	-1.3388	-1.2641	-1.2309	96	52	£ 5	0.0838	9C0C	000	0.8545	-0.3524	2627	0957	0.1290	1333	-0.1353	-0.1327	1571	5000	0.0444	-0.0256													
* 0.67 and α = -1.0°		Forebody	χΓ		46.76			- 6 66 67														15.00					20.00			3 5															
.67 and					'	٠														_	_	-	_	~	<b>₽</b> ₹	₹	× ;	<b>3</b> 6 (	< δ	8	101	129													
mfr = 0		Afterbody		0.0071		0.0562		0.1600	0.2238	0.3278	0.397																																		
	.0 = <b>0</b>	Αħ	ž	173.61	206.94	223.61	245.83	262.50	71 07.0	284.72	290.28																																		
		Forebody	ဦ	0.9213	0.9439	0.9331	0.8964	0.8360	0.6947	0.5914	0.4609	0.4082	0.3184	0.2978	0.3345	1666.0	0.000	000	708	1.1786	0.6911	-1.3375	1.3434	-1.2639	1925	-1.1188	/660.1-	-1.0169	0.903	0.9052	-0.7635	-0.7530	-0.2976	0.1487	100	0.130	0 1490	0.1385	-0.1247	-0.1331	-0.1212	0.1030	0.0485	0.0306	-0.0124
		Fore	ž	52.32 52.32 52.32	-75.15	-68.05	-57.40	9 9	.12.56	-25.46	-18.36	-14.81	-11.26	-10.14	887	,	97	06	30	0.19	000	0.31								6.25				15.00		2000									. 68.64

TABLE VII. Continued

		body	S.	0.0276	0.0613	0.1160	0.1779	0.2975	0.3515	0.4171																																	
		Afterbody	χZ	190.28	223.61	245.83	262.50	279.17	284.72	290.28																																	
	<b>•</b> = 180°	d,	c <sub>b</sub>	0.8566	0.7449	0.0002	0.3357	0.7762	-1.2196	-1.2854	-1.1687	7780	70000	0000	-0.9072	-0.8304	2168	27735	1468	1309	2077	0.1803	0.1763	1582	1264	-0.1272	9.1176	0.1003	0.0848	0.0206													
g = 0°		Forebody		94.32 0			15.4.5						5.30								2021			888																			
mfr = 0.74 and $\alpha = 0^{\circ}$					•	•					œ												•••	, , ,			•		- 3														
mfr .		Afterbody					0.1153				0.4058																																
	• = 0 <sub>•</sub>	7	ΧŢ	13.61	206.94	223.6	245.83			284.72	290.28															_		_				_	_						_	_	_		_
	•	Forebody	CB	0.8544	0.8813	0.8666	0.8226	0.6659	0.5564	0.4141	0.2450	0.1586	0.035	0000	0.3123	0.6679	0.8739	1.0327	1.1736	188	1 2380	1.2299	-1.1849	-1.0825	0.0586	0.8940	-0.8825	-0.8320	0.7401	0.2042	-0.1576	-0.1829	-0.1937	-0.1832	0.1860	0.1526	0.136	-0.1303	-0.1187	-0.1047	-0.0450	0.0206	7007
		Por	X/L	£ 5	75.15	-68.05	-57.40	30.66	-32.56	-25.46	-18.36	18.4	97.11.	1 88	4.51	-2.25	-1.46	06:0	-0.39	61.0	3 6	0.62	1.25	88.5	2.5	3.75	4.38	200	6.25	8.75	10.00	12.50	15.00	17.50	20.00	30.00		90.09	70.00	80.00	100:00	129.17	145.83
		_	۸.	<b>*</b> 5	32	60	93	è 9	: :=	223																																	
		Afterbody		28 0.0114			50 0.1603																																				
	\$ = 180°			206.28			5 262.50		_	_	₹ .	. 2			•	4	0	7	5	<b>y</b> n i	<b>.</b>	. =	=	<u> </u>	9 9	ۍ و	12	<b>5</b>	= 0	2													
3.1°	٠	Forebody		0.9212			0.4235					-1.0022									0.7770				0.1158			_	0.0921														
mfr = 0.67 and $\alpha = 3.1^{\circ}$		Po	X/I	-94.32	46.76	-11.26	15.4	200	0.31	0.62	1.25	88.	2.50	37.6	38.3	5.00	6.25	7.50	8.75	10.00	2.31	17.50	20.00	30.00	9 9	80.09	70.00	80.00	90.08	129.17													
= 0.67		ф	CP	0.0381	0.0424	0.0645	0.1136	0.1079	0.2623	0.2994	0.3452																																
-		2																																									
ā	_	Afterbody		173.61	206.94	223.61	245.83	00707	279.17	284.72	290.28																																
#a	°0 = Φ		XT					•				.4831	:4445	100	7023	.9553	.0739	.1605	1841	1084	74619 4038	.5487	.5224	.4422	3466	3193	.2676	1.2340	1.1959	0841	81901	3,9936	3.9552	0.6474	0.4059	0.0683	0.100/	0.1130	0.1146	0.1090	0.0568	0.0294	0.0190
nfa.	°0 = Φ		CP X/L	0.9216	0.9431	0.9326	99680	0.8390	0.7073	0.6147	0.5177			0.14 0.4434					-0.39 1.1841							3.75 -1.3193			6.25 -1.1959						•		40.00 -0.100/					29.17 -0.0294	
n f	°0 = <del>0</del>		CP X/L		0.9431	0.9326	99680	•	0.7073	0.6147	0.5177			10.14 0.4434							0.00 0.4619												15.00 -0.9552				40.00 -0.100/				100.00 -0.0568		145.83 -0.0190
mfr	°0 = <del>0</del>	body Forebody	CP X/L CP X/L	0.9216	.75.15 0.9431	-68.05 0.9326	99680	30.66 0.2915	-32.56 0.7073	-25.46 0.6147	0.5177																																
r) a		Afterbody Forebody	CP X/L CP X/L	-94.32 0.9216	0.0525 -75.15 0.9431	0.0999 -68.05 0.9326	0.1587 -57.40 0.8966	30.66 0.2915	0.3393 -32.56 0.7073	-25.46 0.6147	0.5177																																
	Φ = 180° Φ = 0°	Afterbody Forebody	XI, CP XIL CP XIL	0.0117 -94.32 0.9216 1	223.61 0.0525 -75.15 0.9431	245.83 0.0999 -68.05 0.9326	262.50 0.1587 -57.40 0.8966	0.2254 40.70 0.8550	284.72 0.3393 -32.56 0.7073	290.28 0.4148 -25,46 0.6147	-18.36 0.5177	-14.81	-11.26		12.4	-2.25	-1.46	06:0-	-0.39	-0.19		0.62	1.25		0.50	3.75	4.38	2:00		8.75	00'01												
		Afterbody Forebody	CP X/L CP X/L CP X/L	0.9204 190.28 0.0117 -94.32 0.9216 1	0.8329 223.61 0.0525 -75.15 0.9431	0.2738 245.83 0.0999 -68.05 0.9326	0.4757 262.50 0.1587 -57.40 0.8966	73.51 0.2594 40.70 51.055	-1.2351 284.72 0.3393 -32.56 0.7073	-1.3346 290.28 0.4148 -25.46 0.6147	-1.2037 -18.36 0.5177	-1.1518	-1.0435	-10.14 	-1.08 -1.08 -1.08	-0.8450	0.6978	-0.2349 -0.90	-0.1898	-0.1335 -0.19	0.00	0.62	-0.1716 1.25	88.1	0.1347	-0.1324 -0.1324 -0.1347	-0.1217 4.38	-0.1003 5.00	-0.0910 6.25	8.75	10.00												
		Forebody Afterbody Forebody	X/L CP X/I, CP X/L CP X/L	94,32 0,9204 190,28 0,0117 -94,32 0,9216 1	-82.25 0.9359 200.54 0.0331 -62.25 0.5512 -62.25 0.5512 -62.25 0.9431 3	11.26 0.2738 245.83 0.0999 -68.05 0.9326	4.51 0.4757 262.50 0.1587 -57.40 0.8966	. 0.50 1.07/4 2/3.61 0.2294 -40.70 0.8390 .	0.31 -1.2351 284.72 0.3393 -32.56 0.7073	0.62 -1.3346 290.28 0.4148 -25.46 0.6147	1.25 -1.2037 -18.36 0.5177	-1.1518	-1.0435	0.9234	5,565/3 5,8810 5,8810	-0.8450	0.6978	-0.2349 -0.90	-0.1898	-0.1335 -0.19	0.00	-0.1823	-0.1716 1.25	-0.1557	0.1347	-0.1324 -0.1324 -0.1347	-0.1217 4.38	-0.1003 5.00	-0.0910 6.25	0000	10.00												
mfr = 0.67 and α = 2.0°		Forebody Afterbody Forebody	CP X/L CP X/L, CP X/L CP X/L	0.0274 -94.32 0.9204 190.28 0.0117 -94.32 0.9216 1	0.0200 -82.23 0.9339 200.34 0.0531 -82.23 0.3312 0.0500 0.0400 0.0528 -75.15 0.9431	0.0659 -11.26 0.2738 245.83 0.0999 -68.05 0.9326	0.1133 -4.51 0.4757 262.50 0.1587 -57.40 0.8966	0.1690 -0.90 1.0774 273.61 0.2634 -40.70 0.8530	0.2675 0.31 -1.2351 284.72 0.3393 -32.56 0.7073	0,3099 0.62 -1.3346 290.28 0.4148 -25.46 0.6147	0.3540 1.25 -1.2037 -18.36 0.5177	-1.1518	-1.0435	0.9234	5,565/3 5,8810 5,8810	-0.8450	0.6978	-0.2349 -0.90	-0.1898	-0.1335 -0.19	0.00	-0.1823	-0.1716 1.25	-0.1557	0.1347	-0.1324 -0.1324 -0.1347	-0.1217 4.38	-0.1003 5.00	-0.0910 6.25	0000	10.00												
		Afterbody Forebody Afterbody Forebody	XI CP XI CP XII CP XII CP XII	173.61 0.0274 -94.32 0.9204 190.28 0.0117 -94.32 0.9216 1	190,28 0.0260 -82.25 0.9339 200,34 0.0331 -82.25 0.9431 3 206,94 0.0407 -46,76 0.8320 223.61 0.0525 -75.15 0.9431 3	223.61 0.0659 -11.26 0.2738 245.83 0.0999 -68.05 0.9326	245.83 0.1133 -4.51 0.4757 262.50 0.1587 -57.40 0.8966	262.50 0.1690 -0.90 1.07/4 27.561 0.2294 -40.70 0.85390 .	279.17 0.2675 0.31 -1.2351 284.72 0.3393 -32.56 0.7073	284,72 0,3099 0,62 -1,3346 290,28 0,4148 -25,46 0,6147	290.28 0.3540 1.25 -1.2037 -18.36 0.5177	1.88 -1.1518	2.50 -1.0435 -11.26	3.12 -0.9234 -10.14	5.73 -4.8870 5.54 4.38 -1.8810 4.51	5.00 -0.8450	6.25 -0.6978 -1.46	7.50 -0.2349 -0.90	8.75 -0.1898 -0.39	10:00 -0.1335	12.50 -0.2071 0.00	17.50 -0.1823 0.62	20.00 -0.1716 1.25	30.00 -0.1557	40,00 -0,1547 2.50	50.50 -0.1524 5.1.2 AD DD -0.1524 3.75	70.00 -0.1217 4.38	80.00 -0.1003 5.00	90.00 -0.0910 6.25	00:00 10:0000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:0000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:0000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000 10:000	00'01	12.50	15.00	17.50	20.00	3000	D()()*	0000	0002	00'08	00'001	129.17	145.83
	• 180°	Afterbody Forebody Afterbody Forebody	CP X/L CP X/L CP X/L CP X/L CP X/L	0.9200 173.61 0.0274 -94.32 0.9204 190.28 0.0117 -94.32 0.9216 1	0.0200 -82.23 0.9339 200.34 0.0531 -82.23 0.3312 0.0500 0.0400 0.0528 -75.15 0.9431	0.9348 223.61 0.0659 .11.26 0.2738 245.83 0.0999 .68.05 0.9326	0.8974 245.83 0.1133 -4.51 0.4757 262.50 0.1587 -57.40 0.8966	0.1690 -0.90 1.0774 273.61 0.2634 -40.70 0.8530	0.705 0.356 0.305 0.30 0.30 0.305 2.8572 0.3393 0.32.56 0.3073	0.6016 284.72 0.3099 0.62 -1.3346 290.28 0.4148 -25.46 0.6147	0.5022 290.28 0.3540 1.25 -1.2037 -18.36 0.5177	0.4621 1.88 -1.1518 -14.81	0.4020 2.50 -1.0435 -11.26	3.12 -0.3891 -10.14	5,565/3 5,8810 5,8810	5.00 -0.8450 -2.25	6.25 -0.6978 -1.46	1.1436 7.50 -0.2349 -0.90	1.1841 8.75 -0.1898 -0.39	1.1273 10.00 -0.1335 -0.19	0.5423 12.50 -0.2071 0.00	-0.1823	-1,4542 20.00 -0.1716 1.25	-1.3969 30.00 -0.1557 1.88	40,00 -0,1947 2,50	-0.1324 -0.1324 -0.1347	1,2027 70,00 -0,1217 4.38	-1.1590 80.00 -0.1003 5.00	90.00 -0.0910 6.25	0000 00000 71001 71001 7000 7000 7000 7	0001	0.9161	-0.8108	0.3751	-0.1436	-0.0852	-0.1239		30000	00'08	000001	-0.0348	-0,0193

TABLE VII. Continued

			<u>&gt;</u> (	200	0.0427	0.0578	0.0975	0.1443	0.2002	0.2406	0.2400	ş																																		
			Ę			_																																								
		\$\psi\$ 180°	₹;	7 % 180 %	•			262.50		264.17	•	7.04																																		
క		÷,	Forebody	02670	0.1649	0.1798	-0.6738	0.0403	0.5020	1 0368	1 0037	99160	-0.8053	-0.6746	0.2838	-0.1817	969	-0.1628	-0.2213	-0.2180	-0.2086	0.2287	0.2498	0.710	96.0	2	0 1777	181	981	0.1092	-0.0925	-0.0814	-0.0375	0.0190												
mfr = 0.84 and α = 0*		•	For	3 5	-82.25	46.76	-11.26	٠ • •	2 5	3 6	9	125	8	2.50	3.12	3.75	4.38	200	6.25	7.50	8. 7 2. 3	000	2 20	3 5	200	8 6	40.00	\$	9	20.00	80.00	00:06	00.00	129.17												
- 0.84			à é	0.0123	0.0244	0.0351	0.034	0.100	0,000	0.2330	0.2743	0.3291																																		
Ę			Anterbody	_		206.94 0.																																								
	;	° 0	*	-										47	11	35	Z :	<del>.</del> .	<b>*</b> 2	e :	= 3	2 2	2 %	2 12	2 5	. *	. 24	=	•	2	ē.	<b>x</b> .	0 (			. ,		_	3	<b>.</b>	•	•	_	•	α.	0 40
		Pomphada	urebody	2 0.2486		5 0.1654			•										0.6924		1.1381		1 000				0.7562					-0.1864		0.727.0			0.1907			-0.1314	-0.1216	9	0.112	000	0.0419	9000
		Ď	X X	94.32	-82.25	75.15	.43.40	4	30.	-32.56	-25.4	-18.36	-14.81	-11.26	101	7.88	7	57.7	÷ .	× 2	\$ 6 6	9 6	0.00	0 62	1.25	86	2.50	3.12	3.75	4.38	2.00	6.25	S. 5	6.0	12.50	15.00	17.50	20.00	30.00	40.00	\$0.00	00:00	90.00	80.00	00.00	145.83
			à ô	0.0291	0.0414	0.0578	0.0378	0.2019	0.2437	0.2857	0.3414																																			
		Afterbody	XI			223.61 0.0					290.28 0.3																																			
	9081	181	*	_							•	11	6:	<b>=</b>	₽.		2 5	= 9	7 4		ž g	, c	٠	<b>*</b>	<u>ښ</u>	•	2	•	•	0	~ .	~ <		•												
<u>.</u>		prehody	S C			5 -0.1869					2 -1.1733					0.747			7 0 1017		0.173		0.2331		-0.173			_				0.0872	0.000													
≖ υ pue		p.	X	-94.32	82.28	46.76	4.51	06:0	00.0	0.31	0.62	1.25	1.88	2.50	3.15	2.72	2	30.4	5 5	2 X	10.00	2	15.00	17.50	20.00	30.00	40.00	20.00	90.00	20.00	80.00	800	120.00													
mfr = 0.83 and α = -1.1°		odv	ဦ	0.0004	0.0197	0.0574	0.0975	0.1412	0.1943	0.2276	0.2687	0.3270																																		
a f	•	Afterbody	ΧĽ	173.61	190.28	223.61	245.83	262.50	273.61	279.17	284.72	82.062																																		
	°0 = •	ģ	S.	0.2733	0.1833						•	•	0.8583	0.6310	50118	0.4200	95170	2590	0.8775	46	1.1853	0.9362	-0.8906	-0.9149	-0.7610	-0.6242	1736	-0.1859	273	-0.2165	3 2	201770-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	0.1977	875	-0.1935	0.2052	-0.1652	-0.1605	<b>Ž</b> :	0.1145	<b>6</b> 19	90119	š	3	202	86
		Forebody			92.25		Ċ					_			10.14								•			.88 .0				8.38																į.
			^	خب د	ri i	. æ	ķ	₹	ř	÷	7	<b>≃</b>	÷ :	<del>-</del> :	÷ '	7	.,	' ¬	, Ψ	۲	Υ .	0	0	0	-	_	7	m	•	4	n •	• -	- 90	01	12	15	12	2	30.00	8.08	90.00	20.02	800	0000	129.17	145.83
		yody	G	0.0359	0.04/9	0.1077	0.1574	0.2105	0.2502	0.2902	0.3419																																			
	8	Afterbody	χĽ	190.28	273.61	245.83	262.50	13.61	279.17	284.72	290.28																																			
	• = 180°	ďy	СЪ	0.2959	0.207			_	0.8074	1.1693		-1.1530	600	0.0636	99.5	-0.8576	8501	8349	6210	1585	-0.1654	1891	2116	1854	-0.1902	1702	0.1451	-0.1422	-0.1281	0.004	0.020	0.0347	0.0178													
t = -2.1°		훋		94.32	·									2.70									15.00 -0.							30.00		0000	-													
mfr = 0.83 and $\alpha$ = -2.1°						•							•	•		•	٠.	Ī	•	_	=	=	=	= :	χ;	<b>≍</b> ∶	¥ S	× \$	8 8	2 8	\$ \$	9	129													
ıfr = 0.8		Afterbody	පි	0.0038	0.0353	0.0563	0.0980	0.1403	0.1928	0.2282	0.707.0	0.5202																																		
8	<b>0</b> = <b>0</b>	V	ž	173.61	206.94	223.61	245.83	262.50	19.617	279.17	77.407	270.78																																		
		Forebody	<u>a</u>	0.2653	0.0781	0.0091	0.0553	0.1967	0.2828	0.3296	03750	0.7770	0.000.0	0.6535	-0.4525	-0.0864	0.3658	0.6103	0.8248	1.0862	1.1820	0.9724	0.8110	0.0117	-0.5028	200	200	0.1967	0.1002	0.1470	-0.1368	0.1447	0.1549	0.1618	0.1707	0.1374	0.1372	1219	19010	0.1046	0.1057	-0.0997	0.0948	-0.0428	-0.0213	0.0023
		Fore	<b>X</b>	82.25	-75.15	-68.05	57.40	46.76	8.6	-32.50	04.62-	14.81	36	-10 14					06:0-	-0.39		0.00					2.50							000			200					_	_	_		45.83
																																												_	_	-

TABLE VII. Continued

(b) Concluded

		od y	200	0.0382	0.0495	61600	2/5170	0.1587	03370	0.3344																																					
		Afterbody	190.28	206.94	223.61	245.83	00.207	19:6/7	707.17	200.000																																					
	$\phi = 180^{\circ}$	ody (	2086	0.1420	0.1985	-0.8053	755.0	10419	1.0419	0.4048	0.2391	-0.1318	0.0829	-0.0555	-0.0475	0.0921	0.0493	0.080.0	0.0619	0.0779	-0.0977	0.1401	0.1379	0.1224	0.0903	0.092	0.0960	0.0951	0.1084	0.0958	0.0844	0.0781	0250.0	7													
mfr = 0.83 and α = 3.1°		Ę						2 2 2 3 4															15.00		20.00								B. 651	11.63.1													
0.83 япс		<b>~</b> 1	100 100 100 100 100 100 100 100 100 10				2 2	0.1380	3 :	0.2414	0.3264																																				
nf.		Ę	_					_																																							
	ى ت 0.	,		_		123.61			11.000		• • •		158	303	161	703	163	156	)26	758	874	812	538	<b>2</b>	128	Š	083	274	<b>5</b>	975	212	976	286	780	72	684	-0.1445	119	-0.1576	-0.1487	£	-0.1310	-0.1206	96600	0.0440	111	0.0084
		ᅙ	1. C.					76 -0.1675		26 05.2983					-7.88 -0.2497	4.51 0.1703		-1.46 0.81			-0.19 1.1874						2.50 -1.1083				5.00		7.50 -0.7	00 -0.5087		15.00 -0.1684								_			45.83 -0.0
		-	X	-82.25	-75.15	-68.05	-57.40	9,00	ć.	-32.36	55 8T	14.81	-11.26	-10.14	7	7	-5	-	9	9	9	0	•	•	-	_	7		<b>~</b>	4	<b>~</b>	<b>v</b>	- •	. 5	17	15	17	20	×	4	×	8	2	<b>≈</b> ∶	<u>ĕ</u> ;	<u>~</u>	<u> </u>
		oody	40 20 20 20 20 20 20 20 20 20 20 20 20 20	0.0378	0.0504	0.0924	0.1407	0.1954	0.2357	0.2763	0.000																																				
	0.	Afterbody	X/L	206.94	223.61	245.83	262.50	273.61	11.617	284.72	7.00																																				
	<b>6</b> = 180°	ody	CP 0.7750	0.1116	0.1814	0.7517	0.0741	0.8426	26.6	0.7237	0.7074	0.2219	-0.1785	-0.1438	0.1744	-0.1877	-0.1191	-0.1561	-0.1280	-0.1438	-0.1483	0.1645	-0.1475	-0.1269	-0.1202	-0.1228	-0.1055	-0.1022	-0.1099	-O.1014	0.0889	0.0819	0.0343	-0.0183													
d a = 2.0°		Forebody	<b>X X</b>						_	0.31						_			_										00:09	00.00	80.00	00.00	00:00	11.67													
mfr = 0.83 and $\alpha$ = 2.0°		ð	CP CP	0.0348	0.0448	0.0651	\$	0.1553	0.2054	0.2403	0.2203	667																																			
mfr .		ě.		190.28 0.0						279.17 0.2																																					
	°0 =				.,	•					•		9	787	616	796	<b>50</b>	191	60	533	887	152	925	918	238	292	66	303	423	949	324	225	677	ž ¥	3 3	915	-0.1925	951	620	-0.1403	-0.1295	319	-0.1191	963	0.0451	0.0249	0.0114
		ş	X/L CP							56 -0.3321							-2.25 0.5605	-1.46 0,7761	_								2.50 -0.9899			4.38 -0.9049	.00 -0.8324			8.75 -0.0797	12.50 -0.2066		17.50 -0.1										45.83 -0.0
		_	¥ 5	-82.25	-75.15	-68.05	-57.40	46.76	39.00	-32.56	25.91	-16.30	-11.26	-10.14	1.	4	-5	7	9	9	7	0	0	0	_	_	7	•	•	•	•	•		~ ~	: =	: =	-	×	×	4	፟፠	35	×	æ	≊	22	4
		body	<b>c</b>	0.0405	0.0538	0.0947	0.1426	0.1992	0.2367	0.2803	0.3397																																				
	.08	Afterbody	X.	206.94	223.61	245.83	262.50	273.61	279.17	284.72	750.78																																				
٠	• = 180	ody	CP CP	0.1456	-0.1802	-0.7103	-0.0249	0.8876	0.9408	-0.9282	2000	0.7128	1861	1991	-0.2015	-0.2057	-0.1997	-0.1976	-0.1997	-0.1919	-0.1813	-0.2199	0.1850	-0.1581	-0.1552	-0.1187	-0.1154	-0.1161	-0.1110	-0.1077	-0.0948	-0.0768	-0.0363	0.0137													
dα = 1.1		Forebody	¥ 5	-82.25	46.76	-11.26	4.5	0.0	0.00	0.31	70.0	57.1	2.50	112	3.75	4.38	5.00	6.25	55.	8.75	10.00	12.50	15.00	17.50	20:00	30.00	40.00	20.00	00:09	20.00	80.00	00:06	00:00	129.17													
infr = 0.83 and $\alpha$ = 1.1°		Į,	CP CP	0.0272	0422	0.0628	1047	0.1502	2048	0.2384	0.2793	3314																																			
n fr		Afterbody		190.28				_			284.72 0.																																				
	ار ا	٠		0.2307 19				•		_		0.26635 25	0.5500	0.524 0.524	0.3447	0.0022	0.5506	0.7380	0.9658	99	1.1913	0.8469	1.0677	-1.1385	9939	-0.9606	-0.9160	8230	8266	8544	-0.7745	4423	1664	0.2214	0.2321	0.2377	00000	\$601	1516	-0.1335	1254	-0.1281	-0.1158	-0.0976	-0.0419	0.0217	0.0098
		Forebody		34.32 0.2 82.35 0.2								18.36 -0.8																			5.00 -0.3			8.73			25.0			40.00					_	Ċ	45.83 -0.
			* ;	, S	4	ő	ç	4	Ť	ij	7	7 ·	7	<del>.</del> =	•	1		1	7	7	٣	_	_	_						•				-			_	٠,	٠,٠	. 4	٠,	•	_	æ	2	7	7

TABLE VII. Continued

(c) M = 0.87

			ģ	0000	0.0128	0.0273	0.0669	0.1197	0.1834	0.2305	0.2839	0.3363																																		
			Afterbody	190.28		13.61	245.83	262.50	273.61	279.17	700 30	97.70																																		
		.081 • = 180			_		_			0.4251 2			98	143	171	617	214	832	<b>8</b>	431	821	972	823	035	268	315	25	515	œ ;	2	7 20	) (2)	3	127												
= 2.1°		٠	Ž											50 -1.4143													0.1620					0.0003														
and a		•	- 5	2 2	-82.25	46.76	=	4.51	<b>3</b> .000 €	000	640	125	80	2.50	3.12	3.75	4.38	2.00	6.25	7.50	8.75	10.00	12.5	15.00	17.5	20.0	30.00	40.06	20.00	90.00	80.08	0.06	100.00	179.1												
mfr = 0.49 and α = 2.1°		+	Ď Č	0.0057	0.0064	0.0196	0.0363	0.0762	1611.0	70/10	0.2444	0.3004																																		
ā			Arterbody X/I. CD	13.61	190.28	206.94	223.61	243.83	05.20	10.672	284.72	290.28																																		
		5 = -		_				7 0901					_	0.8699	0.8702	0.9104	1.0219	505	204	8	966	578	192	-1.6055	<b>3</b>	91.0	3 5	ž S	966	8 8	88	24	786	8 S	3	ŧ =	2 2	2	12	61	2	<del>2</del>	~	₹ (	2 5	3 8
		4110	rorebody X/I. CP																										96661- 21			5 -1.3446				1017									· .	3 -0.0390
			· ×	-94.32	-82.25	-75.15	98.03	, 4	30.64	32.56	-25.46	-18.36	-14.81	-11.26	-10.14	-7.88	4 .S	-2.25	÷	Ġ	-0.36	61.0	ŏ	0.31	0.62	671	= ;	, .	3.12	4.38	\$.00	6.25	7.50	8.75	900	2.50	17.50	20.00	30.00	40.00	20.00	90.00	20.00	80.00	9	145.83
		3	) C	0.0040	0.0172	0.0301	6/07	01760	2 2	0.2704	0.3329																																			
		Afterh	X/L CP		_	19.577																																								
	- 4	2		_								23	95	23	8	77	_ 9	2 5	<b>2</b>	6	<b>3</b> 2 :	<u>∞</u> ;	2 8	3 2	- ·	2 5	: 25	2 25	2 2	: 2	82	9	<u>6</u>													
8		prepad	CP			0 1.0209			_	·											-1.1166			0.9809			0.000		0.0736		_	_		0.039												
9 and a		<u> </u>	×	-94.32	-82.25	11.76	4	06:0	000	0.31	0.62	1.25	œ:	2.50	3.12	5.5	8.5	2 6	67.0	. SC	8.75	10.00	2.2	3 5	200	9 9	8 04	0005	9000	70.07	80.00	90.00	00.001	17871												
mfr = 0.49 and α α 0°		ybo	Ç	0.0118	0.0014	0.0124	0.0745	0.1196	0.1766	0.2165	0.2656	0.3268																																		
=	۰	Afterbody	X/L	173.61	90.28	23.61	245.83	262.50	73.61	279.17	284.72	90.28																																		
	<b>.</b> 0= <b>.</b>		<u>, e</u> ,	0650	•				•			_	0.8602	0.8442	0.8428	0.000	25.0	3 2	200		16	3 8	10000	1072	1.5108	11.6	873	202	266	273	£2	8	6 6	52	155	67.	ž	156	61	537	2 5		£ 3	2 S	23	5
		Porebody		94.32																											0 -1.2879		701.1.						0.6019		0.0420				Ċ	•
			×	sţ s	7 7		.57.40	-46.76	-39.66	-32.56	25 46	18.36	20. 5	97.1.	1.01.	96.7	2 2	44.	2 6	2 6	200	9 6	3.5	690	125	-	7	m	3.75	₹	Š	6.25	5. 5.	10.00	12.50	15.0	17.5	20.00	00	40.00	80.08	3.05	80.00	100.00	129.17	145.83
		ody	S.	0.0118	0.020	0.0674	0.1159	.1693	7,2062	0.2496	3040																																			
	•	Afterbody		190.28							290.28																																			
	¢ = 180°			7690.1				1.1996 2		•	•	<b>Z</b> 8	290	55	724		31	3	ŝ	: 5	1 88	£	<b>1</b>	: E	98	3	5	62	72	75	8 3	60	3 8	;												
= -2.0°		퉏				_						AC/C   - C2			725 1. 57								.1.0849						0 -0.0272			0.0657														
and a		_	Ş	94.32	46.76	-11.26	4.5	06.0	000	0.31	0.62	57.1		113	3.75	4	200	6.25	7.50	8 75	90	12.50	15.0	17.50	20.00	30.00	40.00	20.0	90.00	70.0	80.0	8 8	129.1													
mfr = 0.49 and $\alpha$ = .2.0°		body	C	0.0207	0.0130	0.0291	0.0706	0.1195	0.1824	0.2265	0.2828	0.3351																																		
E		Afterbody	χĽ	19.05	206.94	223.61	245.83	262.50	273.61	279.17	284.72	27.047																																		
	°0 = 0	ģ	<u>د</u>	0741	.0785	10704	1.0527				0.5050	7000.0	0.8130	8075	0.8289	0.9320	10801	1508	1843	1479	1.0507	0.3969	-1.4542	-1.5195	-1.4332	<b>4171</b>	1.4047	3435	-1.2533	2232	137	1.0461	-0.9931	-0.9561	-0.8594	-0.8133	0.7514	907/70	0.1922	0.0806	0.1244	137	057	-0.0509	554	H54
		ě		82.25	_					-32.56 0.											0.19								3.75 -1.2													_	_	_	Ċ	83 -0.0454
		-	× ;	¥ 8	-75	-68	-51	4	30	32	9 :	91	=	10.14	.7	Ą	-5.	÷	Ŷ	Ģ	Ģ	Ö	0	Ö		-	2.	æ,	es .	₹ 3	ń,		8.75	10.00	12.50	15.00		20.02	8 6	9	9000	70.00	80.00	100.00	129.1	145.8

TABLE VII. Continued

		d,	CP CP	0.0425	0.1156	0.1779	0.2987	0.3543	0.4215																														
		ŧ	X/L		245.83 0.				70.78																														
	os1 = ¢									ŧ =	55	0 :	9 =	<b>* *</b>	3.	22	8 2	<b>*</b> *	2 2	24	e e	s s	SS	45	11	S a	. 52	13											
°.	•	흔	CP		0.3556	0.5884				1.1761			0.0410						0.6972				0.1255			0.1055													
and a		Po	¥ \$	-82.25	-11.26	2.5	000	0.31	70:0	1.88	2.50	3.12	5.73	200	6.25	7.50	8.75	2000	15.00	17.50	20.00	30.04 40.04	\$0.00	60.00	70.00	80.08	100.00	129.17											
mfr = 0.67 and $\alpha \approx 0^\circ$		ody	<u>ئ</u> و	0.0261	0.0677	0.1179	0.2490	0.2919	0.3430	0.404																													
E	۰	Afterbody	Z :		223.61	245.83	273.61	279.17	284.72	87.067																													
	<b>0</b> = <b>0</b>	Ą	CP 02.20		0.9554	0.9119			111970	0.4537	0.3567	0.3503	0.4050	0.8624	1.0176	1.1272	1.2027	///11	1.2934	-1.3160	-1.2750	-1.1910	-1.0563	-1.0232	-0.9904	0.9694	-0.8509	-0.8261	-0.8086	0.6619	0.3154	-0.1355	-0.0884	-0.1183	-0.1215	-0.1325	0.1243	0.0550	-0.0280
		Forebody	XT		68.05 0	57.40				14.81			82.7				0.39					2.05				2.00				2.20								_	29.17 - ( 45.83 - (
			- 6	, eò	, <b>4</b>	٠, ن	r	Ψ,	7.		7	7																						•	-,			-	
		Afterbody	<b>G</b>	0.0365	0.1018	0.1636	0.2784	0.3295	0.389.9																														
	<b>.</b>		XI.	206.94	245.83	262.50	279.17	284.72	230.78																														
	<b>4</b> = 180°	ody	CB	1.0027	0.5490	0.7503	0.5630	-1.4007	-1.4500	-1.3639	-1.2689	-1.2182	1.1457	1.0561	-0.9997	-0.9651	-0.9220	4.87.54	0.7685	-0.7470	0.6406	0000	-0.1091	-0.1238	-0.1191	0.1030	0.0436	-0.0264											
mfr = 0.61 and $\alpha$ = 0°		Forebody	<b>X</b> 5		11.26		000			57.1		3.12						000				8 8				90.08		129.17											
0.61 an				11.	9 28	<u> </u>	9 98	90	S	ŝ																													
mf.		Afterbody	800		14 0.0316 11 0.0552		0.2286			5086.U 85																													
	و = 0		X		223.61					290.28						_	<b>~</b> .		~ ~		•	~ ~				m :		<u>د</u>	_	٥.		•	**		<b>.</b>	~ .	~ -		0 4
	Ĭ	Forebody	<u>د</u>	0.9997	0.9959	0.9658	0.8710	0.8117	0.7315	0.6169	0.5662	0.5562	0.5959	0.9872			1.2018	1.1415				-1.2932		-1.1443	-1.1054	-1.0563	-0.9639	-0.9295	0.8947	0.8170	047	0.7034					0.1242		0.0260
		For	χ	-82.25	-75.15 -68.05	-57.40	39.66	32.56	25.46	۶ 🖘	8	7	<b>90</b> -							7													0	60.0	50.03	80.00	5 5	100.00	129.17
									7	8.36	-11.26	-10.14	7.88	-2.25	1.46	-0.90	-0.39	Q 6	0.00	0.62	1.25	1.88	3.12	3.75	4.38	8.5	7.50	8.75	10.00	12.50	17.50	20.00	30.00	<b>\$</b>	• •				
		>	<u>a</u> :	267	422 851	394	450	096		÷. 4.	Ŧ	-10	8.7-	-2.2	1.46	06:0-	-0.39	0.19	0.31	9.0	1.25	1.88	3.12	3.75	4.38	5.00	7.50	8.75	10.00	12.50	17.50	20.00	30.0	\$	• ,				
		fterbody	L CP		.61 0.0422 .83 0.0851	_	17 0.2450		0.3573	8. <del>1.</del>	÷	-10	7.8	22.	97:1-	06:0-	-0.39	61.9	00.0	9.0	1.25	1.88	3.12	3.75	4.38	5.80	7.50	8.75	10.00	12.50	05.21	20.00	30.0	<b>Ş</b>					
	* 180°		Z Z	206.94	223.61	262.50	279.17	284.72	290.28 0.3573																				10:00	12.30	05.21	20:00	30.0	9					
°0,	* 180	}	CP X/L	1.0421 206.94	0.9819 223.61	0.8960 262.50	0.3934 279.17	-1.4734 284.72	-1.5606 290.28 0.3573	-1.4512 -1 4483	1.4098	-1.3618	-1.2793	1861.	-1.1495	-1.0615	-1.0271	-0.9413	-0.808U -0.8494	6,117	-0.7504	0.1968	-0.0638	0.1042	-0.1106	-0.1063	0.0498	-0.0532	10.00	12.50	05 21	20.00	30.00	<b>3</b>					
$s$ and $\alpha = 0^{\circ}$	• 180°	Forebody Afterbody	CP X/L	1.0421 206.94	223.61	0.8960 262.50	279.17	-1.4734 284.72	-1.5606 290.28 0.3573		1.4098	-1.3618		1811-	-1.1495	-1.0615	-1.0271	-0.9413		6,117	-0.7504		-0.0638	0.1042	-0.1106	-0.1063	0.0498		10.00	12.50	05 Z1	20.00	300	07					
fr = 0.55 and α = 0°	.081 * •	Forebody	XI CP XIL	-82.25 1.0421 206.94	0.9819 223.61	4.51 0.8960 262.50	0.00 0.3934 279.17	0.31 -1.4734 284.72	0.62 -1.5606 290.28 0.3573	-1.4512 -1 4483	1.4098	-1.3618	-1.2793	1861.	-1.1495	-1.0615	-1.0271	-0.9413	-0.808U -0.8494	6,117	-0.7504	0.1968	-0.0638	0.1042	-0.1106	-0.1063	0.0498	-0.0532	10,00	12.30	05.21	20,00	300	9					
mfr = 0.55 and $\alpha=0^\circ$	•	Afterbody Forebody	CP X/L CP X/L	0.0083 -82.25 1.0421 206.94	-46.76 0.9819 223.61 -11.26 0.7225 245.83	0.0871 4.51 0.8960 262.50	0.00 0.3934 279.17	0.2430 0.31 -1.4734 284.72	0.2918 0.62 -1.5606 290.28 0.3573	1.25 -1.4512	1.4098	-1.3618	-1.2793	1861.	-1.1495	-1.0615	-1.0271	-0.9413	-0.808U -0.8494	6,117	-0.7504	0.1968	-0.0638	0.1042	-0.1106	-0.1063	0.0498	-0.0532	00'01	12.50	05.61	20.00	30.0	9					
$mfr = 0.55 \text{ and } \alpha = 0^{\circ}$	°0 = 0	Afterbody Forebody	XAL CP XAL CP XAL	150.28 0.0083 -82.25 1.0421 206.94	206.94 0.0215 -46.76 0.9819 223.61 223.61 0.0432 -11.26 0.7225 245.83	245.83 0.0871 4.51 0.8960 262.50	262.50 0.1410 -0.50 1.2011 275.01 273.61 0.2017 0.00 0.3934 279.17	279.17 0.2430 0.31 -1.4734 284.72	284.72 0.2918 0.62 -1.5606 290.28 0.3573	290,28 0.3509 1.25 -1.4512 1.88 -1.4483	2.50 -1.4098	3.12 -1.3618	3.75 -1.2793	1867.1. 00.5	6.25 -1.1495	7.50 -1.0615	1720.1- 27.8	10.00 -0.9413	12.50 -0.8680	17.50 -0.771	20.00 -0.7504	30.00 -0.1968	50,00 -0.0638	60.00 -0.1042	70.00 -0.1106	80.00 -0.1063	0060.0- 00.000 0060.0- 00.000	129.17 -0.0532								0.1285	0.1117	0.0651	0.0607 0.0424
mfr = 0.55 and $\alpha$ = 0.	• 0 #	Afterbody Forebody	CP X/L CP X/L CP X/L	1.0355 173.01 -0.0035 -54.52 1.0355 190.28 1.0354 190.28 0.0083 -82.25 1.0421 206.94	206.94 0.0215 -46.76 0.9819 223.61 223.61 0.0432 -11.26 0.7225 245.83	1.0188 245.83 0.0871 4.51 0.8960 262.50	0.9789 262.50 0.1410 -0.90 1.2011 275.61 0.94202 273.61 0.2017 0.00 0.1934 279.17	0.8990 279.17 0.2430 0.31 -1.4734 284.72	0.8440 284.72 0.2918 0.62 1.5606 290.28 0.3573	0.3509 1.25 -1.4512 1.88 -1.4483	0.7296 2.50 -1.4098	0.7342 3.12 -1.3618	0.7463 3.75 -1.2793	1867.1. 00.5	1.1296 6.25 -1.1495	1.1726 7.50 -1.0615	1.1536 8.75 -1.0271	1.0545 10.00 -0.9413	0.3974 12.50 -0.8680 -1.4800 -1.4800	1.4970 0.717	-1.4250 20.00 -0.7504	0.1968	-1.3305 50.00 -0.0638	-1.2580 60.00 -0.1042	-1.2249 70.00 -0.1106	-1.1806 80.00 -0.1063	0.0498	1,0107 129.17 -0.0532	-0.9649	12.50 -0.9073 12.50	ት ነ ያለው ነ		-0.2316	-0.0666	-0.0655		70.00 -0.1117		

TABLE VII. Continued

(c) Concluded

mfr = 0.73 and  $\alpha$  = 0\*

| Forebardy | Afferbordy | Aff

TABLE VII. Continued

(d) M = 0.89

			- 24	33	2 22	8	æ :	2 6	e 45																														
		Afterbody	C C C		0.0382		0.2058		0.3849																														
	<b>\$= 180°</b>	Ť	X/K	206.94	245.83	262.50	273.61	11.6/2	290.28																														
å	**	Forebody	<b>9</b> 5	00010	0.8241	0.9663	1.2136	0.4498	1.4758	-1.3842	1.3579	1.3213	1.1779	-1.1276	-1.1126	1.0483	0.9390	-0.8838	0.8185	0.7363	-0.6820	0.5600	0.0596	-0.0616	0.0679	0.0706	-0.0150	-0.0324											
ıd α = 2.0		Fore	<b>Σ</b> ξ	-82.25	979	4.51	0.90	3 5	0.62	1.25	1.88	2.50	3.75	4.38	8	6.25 7.50	8.75	10.00	12.50	17.50	20.00	90.9	20.00	00:09	0.00	80.00	100.00	129.17											
mfr = 0.49 and $\alpha$ = 2.0°		ďy	CP OCP	0.0229	0.0276	0.0878	0.1365	0.1914	0.2270	0.3278																													
mfr		Afterbo			206.94		_		284.72																														
	<b>0</b> = <b>0</b>		CP	_	1.0911				0.9880 2		6106.0	0.8946	0.937	1.0457	1.1624	1.2050	1.1158	0.9687	0.2433	1.5417	-1.4762	-1.4775	4476	-1.4301	1.3744	-1.3310	-1.2015	-1.1735	1.138/	-1.0313	-0.9635	0.9321	-0.7829	-0.0/13	-0.0277	0.0092	-0.0133	0.0130	-0.0266
		ě	XX.	_	1.1 21.25				.25.46 O.			-11.26 0.				9 <del>. 4</del>			0.00				3.12						9001					3 9 9				20.00	
			<b>^</b> a	, sej	4	نممن	4	پښو		7	-	7 -	•	•	•	•		•																•	, -		:	= =	-
		Afterbody	CP CP	0.0289	0.0392	0.1366	0.2002	0.2449	0.3607																														
	.08		X/L	206.94	223.61	262.50	273.61	279.17	284.72																														
	<b>081</b> = <b>\$</b>	ody	CP.	11601	1.0446	1.0060	1.2137	0.3430	1.5203	-1.4479	-1.4287	-1.4189	31,40	1.2423	-1.2289	1.1540	-1.0372	1.0194	0.9458	-0.8269	-0.8135	16791	0.0770	-0.0172	-0.0252	0.0412	0.0055	-0.0242											
ıd α = ()°		Forebody	X.E	-82.25	46.76	15.4	-0.90	000	0.31	1.25						6.25	37.8	10.00	12.50	17.50	20.00	30.00	20.05	90.00	70.00	80.08	100.00	129.17											
mfr = 0.49 and $\alpha = 0^{\circ}$		<u>~</u>	<u>د</u>	0.0093	0.0230	0.0867	0.1397	0.2006	0.2417	0.3526																													
nf		Afterbody		,	_	_		273.61 0.7																															
	°0 = 0	•	X	8	206.94						•	<b></b>								4 6		<b>Q</b> ;	8 =	<b>.</b>	= :	2 2	2 2	<b>5</b> 2	<b>.</b>		_				, <b>%</b>	03	<b>S</b>		\$ \$
					<b>60</b> V									· •	2	<b>X</b> :	2 2	2 2	= :											- 60	8	8	5	<b>30</b> 7				4 4	
		ebody	<b>d</b>	00601	1.0933	1.070	1.0426	10.1	0.9811	0.8968			0.8666			1.2004				-1.4584			1387			62121				-0.8883		-0.8029		0.5881				0.0242	
		Forebody	X/L CP		-75.15 1.0933				32.56 0.98				10.14 0.866				0.90 1.2145			0.51 -1.458			31.50 -1.38			5.00 -1.21				15.00 -0.888		20:00 -0:8029		40.00 -0.588				100.00 -0.024	
		Forebody	X	0252 -82.25	-75.15	-57.40	46.76	-39.66	32.56	-18.36																													
		Afterbody Forebody	CP XAL	0.0252 -82.25	0.0387 -75.15	0.1315 -57.40	0.1893 -46.76	0.2278 -39.66	0.2737 .32.56	-18.36																													
	.08( # <del>*</del>	Afterbody Forebody	XIL CP XIL	7 206,94 0.0252 -82.25	223.61 0.0387 -75.15	262.50 0.0793 -06.03	273.61 0.1893 46.76	279.17 0.2278 -39.66	284.72 0.2737 .32.56	-18.36	.14.81	-11.26	10.14	4.51	-2.25	-1.46	06.0 95.0	61.0-	0.00	0.51	125	888.1	2.30	3.75	4.38	5.00	7.50	8.75											
m .2.1°		Afterbody Forebody	CP X/L CP X/L	1.0827 206.94 0.0252 -82.25	1.0441 223.61 0.0387 -75.15	0.8882 245.83 0.0793 -06.03 1 0431 262 50 0.1315 -57.40	1.2111 273.61 0.1893 -46.76	0.2306 279.17 0.2278 -39.66	-1,4966 284.72 0.2737 -32.56	-1.4976 -18.36	-1.4951 -14.81	-1.4876 -11.26	-1.4955	-1,4128 -4.51	-1.3311	-1.2785 -1.46	0.5027	71.1345 71.1345	0.00	-1.0127 0.31	0.9196	1.88	0.6605 2.50	0.0351	0.0068 4.38	0.0112 5.00	7.020.0	-0.0251 8.75											
9 and α = ·2.1°		Afterbody Forebody	X/L CP X/L CP X/L	-94.52 1,0826 190.26 0,0164 -74.52 -82.25 -82.25	-46.76 1.0441 223.61 0.0387 -75.15	-11.26 0.8882 243.63 0.0793 -06.03 -451 1.0431 262.50 0.1315 -57.40	-0.90 1.2111 273.61 0.1893 -46.76	0.00 0.2306 279.17 0.2278 -39.66	0.31 -1,4966 284.72 0.2737 -32.56	1.25 -1.4976 -18.36	1.88 -1.4951	-11.26	-1.4955	-1,4128 -4.51	-1.3311	-1.46	0.5027	71.1345 71.1345	0.00	-1.0127 0.31	0.9196	1.88	0.6605 2.50	0.0351	0.0068 4.38	5.00	7.020.0	8.75											
nfr = 0.49 and \alpha = .2.1°		Forebody Afterbody Forebody	CP X/L CP X/L CP X/L	0.0027 -82.25 1.0897 206.94 0.0252 -82.25	0.0165 -46.76 1.0441 223.61 0.0387 -75.15	0,0409 -11,26 0,8882 245,83 0,0793 -66,03	0.1400 -0.90 1.2111 273.61 0.1893 -46.76	0.2015 0.00 0.2306 279.17 0.2278 -39.66	0.2475 0.31 -1.4966 284.72 0.2737 -32.56	0.3731 1.25 -1.4976 -1.836	1.88 -1.4951	-1.4876 -11.26	-1.4955	-1,4128 -4.51	-1.3311	-1.2785 -1.46	0.5027	71.1345 71.1345	0.00	-1.0127 0.31	0.9196	1.88	0.6605 2.50	0.0351	0.0068 4.38	0.0112 5.00	7.020.0	-0.0251 8.75											
mfr = 0.49 and a = .2.1°		Afterbody Forebody Afterbody Forebody	CP X/L CP X/L CP X/L	-94.52 1,0826 190.26 0,0164 -74.52 -82.25 -82.25	0.0165 -46.76 1.0441 223.61 0.0387 -75.15	-11.26 0.8882 243.63 0.0793 -06.03 -451 1.0431 262.50 0.1315 -57.40	262.50 0.1400 -0.90 1.2111 273.61 0.1893 -46.76	273.61 0.2015 0.00 0.2306 279.17 0.2278 -39.66	279.17 0.2475 0.31 -1.4966 284.72 0.2737 -32.56	290.28 0.3731 1.25 -1.4976 -18.36	1.88 -1.4951	2.50 -1.4876 -11.26	3.12 -1.4955 -10.14	4.38 -1.4128 -4.51	5.00 -1.3311 -2.25	6.25 -1.2785 -1.46	7.50 - 1.2027 9.04 - 2121 1. 37.8	6.0. 211.1. 67.8 10.00 11.1945	12.50 -1.0729 0.00	15.00 -1.0127 0.31	20.00 -0.9196 1.25	30.00 -0.7911	40.00 -0.6603 2.50	60.00 -0.0351 3.75	70.00 0.0068 4.38	80.00 -0.0112 5.00	52.0 20.000 00.0001	129.17 -0.0251 8.75	900	00'71 00'81	17.50	20.00	3000	8.3	0009	00'01	8000	10000	145.83
mfr = 0.49 and $\alpha$ = .2.1°	<b>6</b> ≈ 180°	Afterbody Forebody Afterbody Forebody	XI CP XI CP XI CP XI	0.0027 -82.25 1.0897 206.94 0.0252 -82.25	1 206.94 0.0165 -46.76 1.0441 223.61 0.0387 -75.15	0,0409 -11,26 0,8882 245,83 0,0793 -66,03	262.50 0.1400 -0.90 1.2111 273.61 0.1893 -46.76	273.61 0.2015 0.00 0.2306 279.17 0.2278 -39.66	0.2475 0.31 -1.4966 284.72 0.2737 -32.56	290.28 0.3731 1.25 -1.4976 -18.36	1.88 -1.4951	2.50 -1.4876 -11.26	-1.4955	4.38 -1.4128 -4.51	5.00 -1.3311 -2.25	6.25 -1.2785 -1.46	0.5027	6.0. 211.1. 67.8 10.00 11.1945	12.50 -1.0729 0.00	-1.0127 0.31	20.00 -0.9196 1.25	30.00 -0.7911	40.00 -0.6603 2.50	60.00 -0.0351 3.75	70.00 0.0068 4.38	80.00 -0.0112 5.00	7.020.0	129.17 -0.0251 8.75	900		17.50	20.00	3000	8.3		00'01	8000	10000	
mfr = 0.49 and α = .2.1°	<b>6</b> ≈ 180°	Afterbody Forebody Afterbody Forebody	CP XI CP XI CP XI CP XI	173.6  -0.0213 -94.32 1.0626 190.26 0.0164 -77.32	1.0923 206.94 0.0165 -46.76 1.0441 223.61 0.0387 -75.15	1.0855 223.61 0.0409 -11.26 0.8882 243.53 0.0793 -06.03 1.0865 243.63 0.01315 -57.40	1,0396 262.50 0.1400 -0.90 1,2111 273.61 0,1893 -46.76	1.0126 273.61 0.2015 0.00 0.2306 279.17 0.2278 -39.66	279.17 0.2475 0.31 -1.4966 284.72 0.2737 -32.56	0.8744 290.28 0.3731 1.25 -1.4976	0.8558	0.8292 2.50 -1.4876 -11.26	3.12 -1.4955 -10.14	0.9545 4.38 -1.4128 4.51	5.00 -1.3311 -2.25	1.1637 6.25 -1.2785 -1.46	1.2028 7.50 -1.2027 -0.50	1.0674 10.00 1.1345 1.019	12.50 -1.0729 0.00	-1.3769 15.00 -1.0127 0.51 1.4316 17.60 0.9708 0.62	1.3528 20.00 -0.9196 1.25	-1.3347 30.00 -0.7911	40.00 -0.6603 2.50	3.75	-1.1393 70.00 0.0068 4.38	-1.1042 80.00 -0.0112 5.00	52.0 20.000 00.0001	0.9416 129.17 -0.0251 8.75	900	-0.8162 6.2840	17.50	-0.7003	-0.5564	-0.1977	0009	-0.0822	00.08	0.0318	145.83

TABLE VII. Continued

			ģ	0.0342	0.0546	0.0759	50 20	0.2710	0.3222	0.3783	0.4404																																	
			Afterbody		_		262.83				200.28																																	
		- 180	,					_	_					~	_		_	_						_																				
ૄ		•	Forebody	0.9574	0.970	0.8712	0.5729	1.1427	0.7113	-1.2051	-1.2711	188	103	1.010	-0.9734	-0.9296	0.00	0.814	0.7830	70/0	0.668	-0.6301	-0.5839	0.5606	0.0673	0.0739	0 1242	0.1163	-0.1017	-0.0850	0.0364	0.0173												
mfr = 0.67 and α = 0°	; !	1	5	94.32	-82.25	46.76	4.5	0.90	00:00	0.31	0.62	C7:1	2 50	3.12	3.75	4.38	8.8	6.25	2.50	0 0	12.50	15.00	17.50	20.00	80.00	§ \$	8 9	00.07	80.00	90.00	00:00	71.67												
0.67			_ a	. 98	8	4 5	2 %	67	82	<b>X</b> :	80	Ę.																																
į			Arrerbody A. CD			0.0314					0.3658																																	
		ီ =	X	13.61	190.28	2225	245.83	262.50	273.61	279.17	284.72	* 70.4																																
			9 6	0.9557	0.9688	0.9626	0.9287	0.8691	0.8137	0.7362	0.6310	0.4673	0.3911	0.3710	0.4244	0.6085	0.8806	1.0281	2 2 4	161	0.6975	1.2092	1.2321	9/11	10477	0.9949	-0.9718	0.9279	0.9053	0.8499	0.8196	0.7488	0.6969	0.6662	0.6245	0.5593	0.0707	00000	0.1204	8	1023	0.0463	0.0186	0.0048
		Donobad	X.	32	82.25	68.05	57.40	46.76	39.66	32.56	25.40	14.81	-11.26					<del>2</del> 2	2 2 2 7								3.75				05.7 7.8						_							145.83 -(
												·	•	•																			_	_				•	n •		- 000	2	2	7
		į	ğ	0.0291	0.0486	0.1203	0.1830	0.2532	0.3011	0.5541	0.4133																																	
	9	Afterbade	ž	190.28	\$ 190.2	245.83	262.50	273.61	279.17	284.72	97:70																																	
	•	- A	<b>.</b>	,	2 2010.1					•		790	824	96	929	ž ž	ž S	žž	2	319	532	<b>2</b> 5	r S	2 5	60	20	86	82	<b>3</b> :	2 9	2 8													
80 #		Forehody								7 1.3147						5670.1.0			5 -0.8561									0.0982	_	0.0815														
1 and		-	×	-94.32	, ¥	-11.26	4.51	96 9	000	600	1.25	1.88	2.50	3.12	3.73	8 8	2.6	5.5	8.75	10.00	12.50	2.80	2 0	3000	0.04	20.0	90.00	00.00	80.00	20.00	129.17													
$\mathbf{mfr} = 0.61 \text{ and } \alpha = 0^{\circ}$		, po	C.	0.0103	92100	0.0642	0.1194	0.1839	0.2507	0.3460	0.4068																																	
8		Afterbody	ΧT	13.61	20.5	23.61	245.83	_	71.070		290.28																																	
	- -	; •		1.0024				_				172	2	<b>≅</b> §	2 9	3 3	3 50	9	74	0/	29	8 2	<u> </u>	4	51	56	53	<b>8</b> : :	5 Z	s a	: 23	2	. و	<b>x</b> :	æ :	2 2	3 E	. 15	65	<b>9</b> .	13	2	<b>m</b> :	<u>-</u>
		podeno							0.8941						2600.0					1.1470		8587.1-							19860						0.6738			-0.0557	-0.0959	-0.0926	-0.0933	-0.0489	0.0303	-0.0137
		<u> </u>	χ	94.32 26.32 26.32	.75.15	-68.05	-57.40	0.04	3.55	-25.46	-18.36	-14.81	-11.26	-10.14	8 7	.2.28	94.	0.00	-0.39	0.19	000	0.5	125	1.88	2.50	3.12	3.75	4.38 86.5	9.5	3 5	8.75	10.00	12.50	15.00	30.00	200	900	50.00	90.09	70.00	80.00	00:00	129.17	145.83
			۵.	20 Z	132	570	89	⊋ 8	8 6	11																																		
		Afterbody		8 0.0205					2 0.3201																																			
	• 180°		χ	206.28	223.6	245.83	262.5	10.672	284.72	290.28																																		
٠,	•	Forebody	Cb	1.0575	0.9986	0.7443	0.9119	0.4599	-1.3880	-1.4593	-1.3682	3464	1.3160	3	1574	-1.1185	-1.0541	-0.9839	-0.9517	0.9119	0.8188	0.7513	0.7190	-0.6167	-0.3107	-0.0231	-0.0238	0.0380	0.0770	-0.0328	-0.0250													
ad a = (		Fore	ž	94.32 82.25	46.76	-11.26	2 5	8 8	0.31	0.62	1.25	88.	2.50	3.75	4.38	2.00	6.25	7.50	8.75	00.00	25.21	17.50	20.00	30.00	40.00	20.00	90.00	9 6	90.06	00:00	29.17													
20 20 20			_ :	= *	47	82	37	3 2	. <b>.</b>	92	2																			_	-													
•		•	8	0.00 0.0174	0.0347	0.0582	0.1037	0.27	0.2645	0.3126	0.37																																	
mfr = 0.55 and $\alpha = 0^\circ$		erb							_																																			
mfr = 0	80	erb		190.28			245.83	273.61	279.17	284.72	290.28																																	
mfr = 0	°0 = ◆	Afterb	Z :		206.94	223.61	0.0016 245.83				•••	0.1179	0.7405	0.7853	0.9086	1.0871	1.1685	1.2114	1.1848	0940	1.3781	1.4215	1.3477	1.3180	1.2914	1.2685	1.1921	1.136	1.0358	1.0012	0.9494	17560	0.8008	7566	3,7290	0.6103	3.4145	3.0306	0.0438	1,0031	1.0782	0150.0	00130	7
nfr = 0		rebody Afterbo	Z :	1.0527 190.28	1.0570 206.94	1.0543 223.61		0.9613	0.9151	0.8597	0.8052		10.14 0.7405				-1.46 1.1685			0.19 1.0940				1.88 -1.3180			3.75 -1.1921 4.38 -1.1384	500 - 1067				1750 - 0.9371	15.00 -0.8008			30.00 -0.6103		_			80.00 -0.0782		145.83 -0.0130	

TABLE VII. Continued

(d) Concluded

Mathematical Ma			E	mfr = 0.73 and $\alpha = 0^{\circ}$	grd α ≠ 0	ڡ					<b>u</b>	mfr = 0.81 and $\alpha = 0^{\circ}$	nda=0	Q.		
Change by Marche by March		•	ం			-				•				-	.08	
CATA         NAL         CAP         NAL         CAP <th>Foreb</th> <th>ody</th> <th></th> <th>body</th> <th>Fore</th> <th>body</th> <th>After</th> <th>body</th> <th>Fore</th> <th>body</th> <th>After</th> <th>body</th> <th>Fore</th> <th>body</th> <th>After</th> <th>body</th>	Foreb	ody		body	Fore	body	After	body	Fore	body	After	body	Fore	body	After	body
0.9181         19.02         0.044         4.91         0.0581         1.92         0.020         4.92         0.020         4.92         0.020         4.92         0.020         4.92         0.020         4.92         0.020         4.92         0.020         4.92         0.020         4.02         0.020         4.02         0.020         4.02         0.020         4.02         0.020         4.02         0.020         2.02         0.020         0.020         4.02         0.020         2.02         0.020         4.02         0.020         2.02         0.020         2.02         0.020         2.02         0.020		S.	χ	9	χ	<u>8</u>	χĽ	å	ጟ	Ç	ž	පි	χ	c G	χľ	දු
0.0112   0.0		0.8976	13.61	0.0274	-94.32	0.9007	190.28	0.0424	94.32	0.2853	173.61	0.0212	-94.32	0.2729	190.28	0.0416
0.04279         2.04289         2.04289         4.04289 <t< td=""><td></td><td>0.9183</td><td>190.28</td><td>0.0418</td><td>82.25</td><td>0.9191</td><td>206.92</td><td>81900</td><td>-82.25</td><td>0.1964</td><td>190.28</td><td>0.0385</td><td>-82.25</td><td>0.1573</td><td>206.92</td><td>0.0617</td></t<>		0.9183	190.28	0.0418	82.25	0.9191	206.92	81900	-82.25	0.1964	190.28	0.0385	-82.25	0.1573	206.92	0.0617
0.0651         3.453         0.146         4.13         0.3873         0.113         3.25         0.111         4.74         0.0971         3.25         0.111         4.75         0.0971         3.25         0.111         4.75         0.0971         3.25         0.111         4.75         0.0971         3.25         0.011         4.75         0.0971         3.25         0.0971         3.25         0.0971         3.25         0.0971         3.25         0.0971         3.75         0.0971         3.75         0.0971         3.75         0.0971         3.75         0.0972         0.0972         0.0972         3.75         0.0972<		67760	773.61	0.0370	1 26	0.0038	245.83	0.0602	50.80	0.0756	223.61	00700	7.17	0.5411	245 83	0.07.0
0.7930         3625         0.2121         0.896         1677         0.184         0.467         0.107         0.184         0.990 <th< td=""><td></td><td>0.8652</td><td>245.83</td><td>0 1445</td><td>4 5</td><td>0.3875</td><td>262.50</td><td>0.2112</td><td>-57.40</td><td>-0.0977</td><td>245.83</td><td>0.1241</td><td>4</td><td>0.1338</td><td>262.50</td><td>0.1746</td></th<>		0.8652	245.83	0 1445	4 5	0.3875	262.50	0.2112	-57.40	-0.0977	245.83	0.1241	4	0.1338	262.50	0.1746
0.0756         7.154         0.2342         0.2145         0.1343         0.010         0.7382         2.944         0.011		0.7930	262.50	0.2121	060	1.0774	273.61	0.2861	46.76	-0.1607	262.50	0.1768	060	0.9720	273.61	0.2336
0.0144         2.924         0.234 <t< td=""><td>39 66-</td><td>0.7206</td><td>273.61</td><td>0.2842</td><td>000</td><td>0.7885</td><td>279.17</td><td>0.3381</td><td>-39.66</td><td>-0.2132</td><td>273.61</td><td>0.2333</td><td>0.00</td><td>0.9328</td><td>279.17</td><td>0.2747</td></t<>	39 66-	0.7206	273.61	0.2842	000	0.7885	279.17	0.3381	-39.66	-0.2132	273.61	0.2333	0.00	0.9328	279.17	0.2747
0.0133         20.028         0.4474         2.464         0.4151         2.645         0.4312         0.645         0.6411         2.645         0.4412         0.6411         2.645         0.6411         0.6412         0.6411         0.6412         0.6411         0.6412         0.6411         0.6412         0.6411         0.6412	-32.56	0.6184	279.17	0.3287	0.31	-1.0678	284.72	0.3932	-32.56	-0.2197	279.17	0.2697	0.31	-0.8864	284.72	0.3189
0.1313         290.28         0.4452         1.123         -102344         -118.4         -0.4412         -0.8717         -11.26         -0.4716         -0.4712         -0.8717         -0.87	-25.46	0.4768	284.72	0.3822	0.62	1.1617	290.28	0.4574	-25.46	-0.4315	284.72	0.3123	0.62	-0.9811	290.28	0.3756
0.0224         1.88         0.0652         -1.81         0.0632         1.88         0.0532         1.88         0.0532         1.88         0.0532         1.89         0.014         0.0442         1.12         0.0402         1.12         0.0402         1.12         0.0402         1.12         0.0402         1.12         0.0402         1.12         0.0402         4.38         0.0232         4.31         0.0202         4.32         0.0202         4.32         0.0202         4.31         0.0202         0.0202         0.0202         4.31         0.0202	-18.36	0.3133	290.28	0.4452	1.25	1.0234			.18.36	-0.7416	290.28	0.3678	1.25	-0.8714		
0.0956         3.12         0.4940         -1.15         0.4475         2.50           0.1946         3.12         0.8876         -1.014         -0.425         3.13           0.1147         3.13         0.8275         -7.88         -0.2329         3.13           0.1147         3.13         0.8275         -7.88         -0.2329         3.13           0.1247         3.10         0.7786         -2.24         0.1279         3.13           0.1029         3.13         -0.8831         -0.299         1.1704         8.13           0.1029         1.2040         8.13         -0.589         0.09         0.99         1.20           0.8027         1.2040         0.5445         0.17         0.20         0.39         1.20           0.8028         1.2040         0.5445         0.09         0.99         1.20           0.8027         0.5938         0.01         0.31         0.99         1.20           0.1037         0.00         0.1143         0.21         0.24         1.20           0.1037         0.00         0.1143         0.124         1.20         0.00           0.8274         0.00         0.1143         0.124	14.81	0.2324			1.88	-0.9652			-14.81	-0.6832			1.88	0.8445		
0.0556         3.12         0.8850         -10.14         0.4423         3.12           0.4056         4.31         0.3259         3.13         1.175         4.31         0.1756         3.13         0.455         3.13         0.455         3.13         0.455         3.13         0.455         3.13         0.455         3.13         0.455         4.31         0.1756         4.31         0.1756         4.31         0.1756         4.31         0.1756         4.31         0.1756         4.32         3.13         0.50	-11.26	0.1077			2.50	-0.9190			-11.26	-0.4762			2.50	-0.7235		
0.1447         1.15 0.2279         -0.229         -1.239         4.38           0.4096         4.38 - 0.7966         -4.51 0.1295         4.38           0.7323         5.05         -0.6885         -1.25 0.5279         5.00           0.9071         6.25 0.6885         -1.25 0.00         0.399         1.704         4.38         4.39         1.704         8.73         4.38         4.38         4.39         1.704         8.73         4.30         6.20         1.30         4.38         4.38         4.39         1.704         8.73         4.30         4.38         4.30	-10.14	0.0956			3.12	-0.8650			10.14	-0.4425			3.12	-0.6582		
0.4496         4.38         4.7966         -4.51         0.1295         4.38           0.733         5.00         0.7796         -2.279         5.00           0.733         6.20         0.7796         -2.279         6.29           0.9701         6.20         -0.7893         -1.46         0.7897         6.20           0.9702         8.73         -0.6823         -0.99         0.9995         7.50           1.1004         8.73         -0.6823         -0.99         1.1704         8.73           1.1004         1.20         -0.898         -0.19         1.1704         8.73           1.1007         1.00         -0.996         -0.19         1.1704         8.73           1.0007         -0.874         1.25         -0.597         1.20         1.20           -0.937         -0.00         -0.184         0.00         0.9192         1.20         0.00           -0.8374         -0.00         -0.123         0.133         0.439         1.00         0.00           -0.7547         -0.00         -0.123         0.133         0.439         0.00         0.123         0.00         0.00         0.00         0.00         0.00         0.00	-7.88	0.1547			3.75	-0.8275			7.88	-0.2329			3.75	0.6411		
0.7723         0.7786         -2.25         0.5279         5.00           0.9071         6.23         -0.6833         -1.46         0.7897         6.25           1.02040         8.73         -0.6933         -0.49         0.7897         7.50           1.12040         8.73         -0.6933         -0.49         1.70         1.70           1.12040         1.2044         8.73         -0.493         1.170         1.00           0.8242         1.20         -0.5313         0.00         0.90         1.20           -1.0874         1.50         -0.5171         0.02         0.90         1.25           -1.0874         5.00         -0.184         0.29         1.79         1.70           -0.5877         5.00         -0.184         0.29         1.79         1.70           -0.5874         5.00         -0.184         0.79         0.79         1.70           -0.787         5.00         -0.184         0.79         0.79         1.70           -0.787         5.00         0.184         0.79         0.79         1.70           -0.787         5.00         0.184         0.79         0.73         1.70           -0.784<	4.51	0.4096			4.38	-0.7966			4.51	0.1295			4.38	-0.5687		
0.9971         6.25         d.6885         -1-46         0.7897         6.25           1.0829         7.30         0.6923         -1.794         7.50           1.2040         8.73         0.6923         -0.99         1.50           1.2040         8.73         0.6928         -0.99         1.50           1.2040         1.500         0.5445         -0.99         1.75           1.0874         1.500         0.5348         0.09         1.50           1.0874         1.500         0.5344         0.99         1.50           1.0874         1.500         0.1345         0.99         1.50           0.9877         4.00         0.1345         1.23         0.944         17.50           0.8876         4.00         0.1345         1.22         0.934         17.50           0.8876         4.00         0.1345         1.22         0.043         0.00           0.8876         4.00         0.1345         1.22         0.742         0.00           0.7941         8.00         0.1035         0.1345         0.044         0.00           0.7341         8.00         0.1038         0.244         0.00         0.00 <t< td=""><td>-2.25</td><td>0.7323</td><td></td><td></td><td>2.00</td><td>-0.7796</td><td></td><td></td><td>-2.25</td><td>0.5279</td><td></td><td></td><td>2.00</td><td>-0.5665</td><td></td><td></td></t<>	-2.25	0.7323			2.00	-0.7796			-2.25	0.5279			2.00	-0.5665		
1,0829         7,30         0,6923         0,999         7,50           1,2040         8.73         -0,690         0,999         7,50           1,2040         18,73         -0,636         0,919         1,174         8,73           1,210         1,210         -0,5313         0,00         0,919         1,250           1,0824         1,250         -0,5313         0,00         0,919         17.50           -1,0824         1,500         -0,5313         0,00         0,919         17.50           -1,0874         1,500         -0,224         1,25         -0,944         17.50           -0,8274         4,00         -0,1345         2,20         -0,944         17.50           -0,8274         5,00         -0,1345         2,20         -0,744         17.50           -0,8274         5,00         -0,1345         2,20         -0,744         17.50           -0,8274         5,00         -0,1345         2,20         -0,744         17.50           -0,645         1,00         -0,1345         2,20         -0,343         2,00           -0,645         1,00         -0,1345         2,20         -0,343         2,00           -0,6	-1.46	0.9071			6.25	-0.6885			-1.46	0.7897			6.25	-0.5687		
1.2040         8.73         6.6560         6.39         1.1704         8.73           1.2109         1.2109         0.3445         0.09         0.19         10.00           0.8876         1.200         0.5445         0.09         12.50         10.00           1.0874         1.500         0.5313         0.09         12.50         10.00           1.0874         1.500         0.5313         0.09         12.50         12.50           1.0875         0.00         0.224         1.25         0.8944         17.50           0.9592         0.00         0.224         1.25         0.8944         17.50           0.9592         0.00         0.1345         0.8944         17.50         17.50           0.8876         0.00         0.1345         0.1345         0.7342         17.50         17.50           0.8874         0.00         0.1345         0.1345         0.7342         0.7342         17.50         17.60         17.50         17.50         17.60         17.50         17.60         17.60         17.60         17.60         17.60         17.60         17.60         17.60         17.60         17.60         17.60         17.60         17.60 <td< td=""><td>06:0-</td><td>1.0829</td><td></td><td></td><td>7.50</td><td>-0.6923</td><td></td><td></td><td>06:0-</td><td>0.9695</td><td></td><td></td><td>7.50</td><td>0.4109</td><td></td><td></td></td<>	06:0-	1.0829			7.50	-0.6923			06:0-	0.9695			7.50	0.4109		
12109         1000         0.5445         0.19         12101         1000         0.5445         0.10         12.90         1	-0.39	1.2040			8.75	0.6360			-0.39	1.1704			8.75	-0.1170		
0.8026         12.50         4.5098         0.00         0.9109         12.50           -1.0824         15.00         -0.5313         0.631         0.9091         15.00           -1.0873         15.00         -0.5313         0.631         0.9091         15.00           -1.0873         15.00         -0.2244         1.25         -0.944         15.00           -0.9522         30.00         -0.1345         2.20         0.944         15.00           -0.8274         50.00         -0.1345         2.20         0.744         20.00           -0.8274         50.00         -0.1345         2.20         0.7542         20.00           -0.7547         70.00         -0.1347         2.20         0.7542         20.00           -0.7547         70.00         -0.1349         4.38         0.0640         6.00           -0.7547         70.00         -0.0346         8.00         0.4349         8.00           -0.6458         10.00         -0.0346         8.00         0.4349         8.00           -0.6459         10.00         -0.0346         8.00         0.4349         8.00           -0.6450         10.00         -0.0346         8.00         0.	-0.19	1.2109			10.00	-0.5445			61.0	1.2121			10,00	-0.2671		
1,0824         15.00         d.5313         0.901         0.901         15.00           1,0076         1,1087         0.5171         0.02         0.9474         17.50           1,0076         0.186         0.5171         0.02         0.9474         17.50           0,9592         30.00         0.1186         0.186         2.90         17.50           0,9876         40.00         0.1345         2.90         0.7992         30.00           0,8876         40.00         0.1345         3.75         0.640         9.00           0,8877         80.00         0.128         3.75         0.640         9.00           0,7947         80.00         0.128         9.00         0.688         8.00           0,7348         80.00         0.688         6.25         0.5421         9.00           0,7341         90.00         0.6898         6.25         0.5439         9.00           0,6455         100.00         0.0336         8.23         0.5449         9.00           0,6456         100.00         0.0336         8.03         0.449         9.00           0,5434         100.00         0.0349         1.240         1.240         1.240 <td>0.00</td> <td>0.8026</td> <td></td> <td></td> <td>12.50</td> <td>-0.5098</td> <td></td> <td></td> <td>000</td> <td>0.9109</td> <td></td> <td></td> <td>12.50</td> <td>-0.2184</td> <td></td> <td></td>	0.00	0.8026			12.50	-0.5098			000	0.9109			12.50	-0.2184		
-1,0676         17.50         -0.5171         0.62         -0.9474         17.50           -1,0973         2,000         -0.2924         1.28         -0.836         20.00           -0,9876         3,000         -0.1345         2.50         -0.7342         20.00           -0,8876         40.00         -0.1345         2.50         -0.7342         20.00           -0,8877         60.00         -0.1347         3.75         -0.6440         60.00           -0,8877         70.00         -0.1397         3.75         -0.6440         60.00           -0,7341         90.00         -0.1397         3.75         -0.6440         60.00           -0,7341         90.00         -0.1397         3.50         -0.7342         70.00           -0,6456         10,00         -0.0394         8.00         -0.449         100.00           -0,641         -0.641         10,00         -0.3944         112.0         -0.1449         112.0           -0,444         -0.544         -0.640         -0.1449         112.0         -0.1449         112.0           -0.113         -0.541         -0.044         -0.1449         112.0         -0.1449         112.0           -0.113	0.31	-1.0824			15.00	-0.5313			0.31	1606.0-			15.00	-0.2428		
-1.0373         30.00         -0.2924         1.25         -0.8136         20.00           -0.9592         30.00         -0.1186         1.28         -0.7990         30.00           -0.8876         40.00         -0.1186         2.29         4.7990         30.00           -0.8877         40.00         -0.1238         2.20         -0.7942         40.00           -0.7947         70.00         -0.1238         4.38         -0.6640         60.00           -0.7947         70.00         -0.1238         4.38         -0.6640         60.00           -0.7948         80.00         -0.1038         4.38         -0.6640         60.00           -0.7949         80.00         -0.1038         7.50         -0.6440         70.00           -0.6456         100.00         -0.0386         7.50         -0.5898         80.00           -0.6413         -0.6456         100.00         -0.0386         8.75         -0.541         80.00           -0.6411         -0.6411         -0.0040         -0.0386         7.50         -0.144         10.00           -0.5416         -0.5414         10.00         -0.1840         11.241         11.241         11.241         11.241	0.62	-1.0676			17.50	-0.5171			0.62	0.9474			17.50	-0.1803		
0.9592         30.00         0.1186         1.88         0.7990         30.00           0.8876         40.00         0.1343         2.50         0.7392         40.00           0.8877         40.00         0.1343         2.50         0.7392         40.00           0.7947         70.00         0.138         3.75         0.6440         60.00           0.7947         70.00         0.1238         4.38         70.00         60.00           0.7947         70.00         0.0898         6.25         0.3813         70.00           0.7947         10.00         0.0898         6.25         0.3813         70.00           0.7947         10.00         0.0898         6.25         0.3819         80.00           0.6456         10.00         0.0898         6.25         0.4349         100.00           0.6451         10.00         0.0849         100.00         0.1840         17.01           0.6453         10.00         0.0849         17.00         0.1840         17.01           0.5434         10.00         0.1840         0.1840         17.01         0.1840           0.113         0.113         0.1840         0.1840         0.1840		-1.0373			20.00	-0.2924			1.25	-0.8336			20.00	-0.1810		
0.8876         40.00         0.1345         2.50         0.1792         40.00           0.8274         50.00         0.1352         3.12         0.1742         90.00           0.8274         60.00         0.1352         3.12         0.0543         90.00           0.8273         60.00         0.1238         3.12         0.0549         90.00           0.7391         80.00         0.1083         5.00         0.5838         70.00           0.7391         90.00         0.0386         6.23         0.4349         70.00           0.6455         100.00         0.0336         8.73         0.5440         100.00           0.6413         100.00         0.0336         8.73         0.5440         100.00           0.5444         100.00         0.0344         10.00         0.0344         10.00         0.0344           0.5444         10.00         1.20.17         0.0004         1.136         0.0144         1.127         0.0144           0.320         1.320         1.20.17         0.0004         1.136         0.0144         1.127         0.0144           0.131         1.320         1.320         0.1340         0.1340         1.1284         1.12		-0.9592			30.00	-0.1186			1.88	-0.7990			30.00	-0.1611		
0.8274         50.00         -0.1222         3.12         -0.7242         50.00           -0.8277         60.00         -0.1397         3.13         -0.7242         50.00           -0.7947         70.00         -0.1397         4.38         -0.6640         6.00           -0.7947         70.00         -0.1993         4.38         -0.6640         6.00           -0.7341         80.00         -0.1093         5.00         -0.5831         70.00           -0.6456         100.00         -0.0386         6.23         -0.5443         100.00         -0.3804         172.17           -0.6413         -0.6413         1.20.17         -0.0094         8.75         -0.5449         100.00         -0.3804         172.17           -0.5434         -0.5434         1.50         -0.1441         11.50         -0.1441         11.50         -0.1441         11.50         -0.1441         11.50         -0.1442         11.50         -0.1442         11.50         -0.1442         11.50         -0.1459         11.50         -0.1459         11.50         -0.1445         11.50         -0.1459         11.50         -0.1459         11.50         -0.1459         11.50         -0.1459         11.50         -0.1459	2.50	-0.8876			40:00	-0.1345			2.50	-0.7592			40.00	0.1473		
0.0927         0.000         0.1397         3.75         0.6640         6.00           0.7947         7000         0.1238         4.38         0.6640         6.00           0.7948         800         0.1238         5.00         0.5838         700           0.7951         800         0.0898         6.25         0.5421         80.00           0.7351         1000         0.0336         7.59         0.4349         1000           0.6436         1000         0.0336         8.00         0.4349         1000           0.6437         1000         0.0439         8.00         0.1941         122.17           0.5436         1000         0.0304         1120         17.00         1.0304         17.00           0.5434         1000         1.240         1.240         1.240         1.221         1.221           0.5434         1.380         1.150         0.1142         1.150         0.1142         1.150         0.1142         1.150           0.1137         1.380         1.150         0.1145         1.150         0.1145         1.150         1.156         1.156         1.156         1.156         1.156         1.156         1.156         1.156 </td <td>3.12</td> <td>-0.8274</td> <td></td> <td></td> <td>20.00</td> <td>-0.1252</td> <td></td> <td></td> <td>3.12</td> <td>-0.7242</td> <td></td> <td></td> <td>\$0.00</td> <td>-0.1389</td> <td></td> <td></td>	3.12	-0.8274			20.00	-0.1252			3.12	-0.7242			\$0.00	-0.1389		
0.7947         70.00         0.1238         4.38         0.5835         70.00           0.7381         80.00         -0.1095         5.00         -0.5898         80.00           0.7391         80.00         -0.0396         6.23         -0.5491         80.00           0.6455         100.00         -0.0336         7.50         -0.449         90.00           0.6553         100.00         -0.034         8.73         -0.544         100.00           0.5344         100.00         -0.304         10.30         -0.304         129.17           0.5444         10.00         1.50         -0.1941         17.01         -0.304           0.5444         1.50         1.50         -0.1941         17.50         -0.1941           0.5444         1.50         1.50         -0.1941         17.50         -0.1843           0.5444         1.50         1.50         -0.1843         -0.1442         17.50         -0.1843           0.1320         1.13         1.00         -0.1843         -0.1442         1.044         1.044         1.044         1.044         1.044         1.044         1.044         1.044         1.044         1.044         1.044         1.044 <td< td=""><td>3.75</td><td>-0.8027</td><td></td><td></td><td>90.00</td><td>-0.1397</td><td></td><td></td><td>3.75</td><td>0.6640</td><td></td><td></td><td>90.00</td><td>-0.1393</td><td></td><td></td></td<>	3.75	-0.8027			90.00	-0.1397			3.75	0.6640			90.00	-0.1393		
0.7678         80.00         0.1095         5.00         0.5898         80.00           0.7391         90.00         0.0898         6.23         0.5421         90.00           0.6455         10.000         0.0384         7.30         0.449         100.00           0.6413         129.17         -0.094         8.75         -0.540         100.00           0.6413         1.29.17         -0.094         8.75         -0.540         129.17           0.6413         1.20.20         1.20.20         -0.194         129.17           0.5424         1.20.20         -0.194         129.17         129.17           0.5434         1.20.20         -0.194         129.17         129.17           0.544         1.20.20         -0.143         117.50         -0.142         129.17           0.1113         1.20.20         -0.145         117.50         -0.145         117.50         114.59           0.113         0.113         0.0145         0.0145         117.50         11.26         117.50         11.26         117.50         11.26         117.50         11.26         117.50         11.26         11.26         11.26         11.26         11.26         11.26         11.26<	4.38	-0.7947			70.00	-0.1238			4.38	-0.5835			70.00	-0.1261		
0.7391         90.00         0.0888         6.23         0.5421         90.00           0.6456         100.00         -0.0336         7.50         -0.5449         100.00           0.6453         129.01         -0.5349         100.00         -0.0341         100.00           0.6413         12.50         -0.1340         172.17         -0.1041         172.17           0.5454         12.30         -0.1941         17.50         -0.1941         172.17           0.5460         -0.546         0.1042         17.50         -0.142         17.50         -0.142           0.113         -0.130         -0.1890         -0.1890         -0.1890         -0.145         -0.1890         -0.145         -0.1890         -0.1991         -0.1991         -0.1992         -0.1992         -0.1992         -0.1992         -0.1992         -0.1992         -0.1992         -0.1992         -0.1	2.00	-0.7678			80.00	-0.1095			5.00	-0.5898			80.00	-0.1080		
0.6456         100.00         -0.6346         7.59         100.00           0.6553         129.17         -0.094         8.73         -0.5140         129.17           0.6413         0.0544         10.00         -0.304         129.17         -1.00           0.5434         10.50         -0.1843         12.50         -0.1843         -0.20         -0.1843           0.3516         2.0320         -0.1843         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1842         -0.20         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266         -0.1266	6.25	-0.7391			90:06	-0.0898			6.25	-0.5421			90.00	-0.0916		
0.6655         129.17         -0.0094         8.75         -0.5140         129.17         -0.0041           0.6613         0.5336         10.00         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         129.17         -0.3904         -0.242         129.17         -0.3904         -0.1459         -0.145	7.50	-0.6456			100:00	-0.0336			7.50	-0.4349			100.00	-0.0368		
0.001413 10.00 0.4534 12.50 0.5434 15.50 0.5414 17.50 0.5417 17.50 0.1317 17.50 0.137 17.50 0.137 17.50 0.137 17.50 0.108 17.50 0.000 0.0004 17.50 0.0004 17.5	8.75	-0.6555			129.17	0.009			8.75	-0.5140			129.17	-0.0148		
0.5336 12.50 0.5434 12.50 0.5436 17.50 0.113 17.50 0.113 17.50 0.137 2.50 0.137 2.50 0.137 2.50 0.137 2.50 0.137 0.00 0.108 80.00 0.004 17.50 0.001	10.00	0.6413							10.00	0.3904						
0.544 15.00 0.5516 17.50 0.113 20.00 0.1137 20.00 0.137 20.00 0.127 20.00 0.127 20.00 0.127 20.00 0.127 20.00 0.0047 17.50 0.0014 1.50 0.0014 1.50 0.0	12.50	-0.5536							12.50	0.1941						
0.5616 17.50 0.5217 2.00 0.1113 3.00 0.1317 3.00 0.1379 6.00 0.1379 6.00 0.1379 6.00 0.1379 6.00 0.008 8.00 0.008 8.00 0.008 8.00 0.008 8.00 0.008 17.50 0.001	15.00	0.5434							15.00	-0.1843						
0.3820 2000 0.1113 3000 0.1371 4000 0.1379 5000 0.1379 6000 0.1088 8000 0.008 8000 0.008 8000	17.50	-0.5616							17.50	-0.2142						
40.1113 30.00 40.137 40.00 40.137 50.00 40.127 70.00 40.108 80.00 40.0427 109.00 40.0014 145.83	20:00	-0.3820							20.00	0.1890						
-0.1317 +0.00 -0.1327 -0.00 -0.1227 -0.00 -0.0427 -0.001 -0.0014 +0.838	30.00	-0.1113							30.00	-0.1576						
-0.1397 5000 -0.1379 6000 -0.1287 70.00 -0.0427 80.00 -0.043 1129.17	40.00	-0.1317							40.00	-0.1459						
0.01379 60.00 0.1088 70.00 0.0427 70.00 0.0427 80.00 0.0131 129.17	20:00	-0.1307							\$0.00	-0.1286						
-0.1227 7000 -0.108 8000 -0.0427 100.00 -0.0131 129.17	90:00	-0.1379							90.00	-0.1351						
-0.1088 80.00 -0.0427 100.00 -0.0131 129.17	70.00	-0.1227							70.00	-0.1191						
-0.0427 100.00 -0.0131 1294 145.83 0.0014 145.83	80.00	-0.1088							80.00	0.1076						
-0.0131 129.17 0.0014 145.83	100:00	-0.0427							100.00	-0.0395						
0.0014	129.17	-0.0131							129.17	-0.0199						
	145.83	0.0014							145.83	-0.0047						

TABLE VII. Continued

(e) M = 0.92

			ody S	0038 038	0.0592	0.0805	0.1355	0.2044	20/770	0.3251	7777																																				
		ం	Afterbody	190.28	206.94	223.61	245.83	262.50	10.677	284.77	200.28																																				
		¢ = 180°	ğ ç	.02 <b>I</b> S	1.0323	0.9559	0.6018	0.7942				-1.2129	-1.1415	-1.1078	0445	906	9638	9323	8724	.8302	7829	7876	-0.7018	6964	.6612	9009	5101	4337	-0.1713	-0.0267	0314	-0.0547	0534	0.0018	900												
ည်း ဗ			ş			46.76 (		15.4								3.75 -0		5.00															_														
mfr=0.61 and α = 0°								7 6	2 2	t &	8	<b>2</b> 2											_	_	_		• 1	•	•	٠	,	<b>o</b> c	σ ;	2 5	:												
i i			Afferbody							7 0.3190																																					
	;	გ # <b>ტ</b>	×				10777					2 290.28	3	6	_	~	_	_	_	<u>~</u>	<b>.</b>	_	_	_	_	•				_		_					_										
			rorebody				8070	_			0.7733												0.6121							-1.0103	-0.9805	0.9459	70,670	0.8039	0.7834	-0.7257	-0.6820	-0.6761	-0.6217	0.5464	-0.4556	-0.2347	-0.0248	-0.0385	0.0518	-0.0286	0.0038
		ŝ	X	-94.32	-82.25	-75.15	98.03	46.76	-39.66	-32.56	-25.46	-18.36	-14.81	-11.26	-10.14	-7.88	15.4	-2.25	1.46	0.0	-0.39	0.19	000	0.31	0.62	1.25	1.88	7.30	3.12	3.75	4.38	900	0.20	8.78	10.00	12.50	15.00	17.50	20.00	30.00	40.00	20.00	90.00	20.00	80.00	00:00	145.83
		į	à ô	0.0330	0.0492	0.0665	1800	0.2490	0.2947	0.3460	0.4092																																				
		A Monthad				223.61 0					290.28 0.																																				
	0001					1.0156 22						-1.2783	-1.2649	-1.2371	-1.1927	-1.1355	1.0894	1.0487	-1.0049	233	033	8	0.7922	5.24	ž ž	9 5	è	1 20	3 5	2 5	2 2	\$ :		191													
α <b>*</b> 0°		Forebode				96.76		_	0.00														12.50 -0.7		1600 0000	00.00	30.00 -0.3987			70.00 -0.1879	0.00			•													
mfr = 0.55 and α = 0°				·	•						_	_		7	-	m	•	'n	•	_	œ :	2 :	2 :	2 5	2 8	3 5	3 5	₽ 5	7 9	8 8	5 8	9.00	0000	129.17													
mfr .		erbody	S CP		0.0302				0.2480	0.2907	25.	0.4000																																			
	ت ل	¥	ž	173.61	190.28	223.61	245.83	262.50	273.61	719.17	284.72	290.28																																			
	•	Forebody	Ç	1.0661	1.0/12	1.0700	1.0488	1.0123	0.9806	0.9360	0.8774	0.8237	0.8039	0.7742	0.7705	0.779	2076:0	7887	7001.1	7717"	. 1913	1,60.1	1 2761	6017.1	1 2838	1 2380	12146	202	001	8	0330	1.0020	-0.9341	-0.8673	-0.8577	-0.8069	0.7747	0.7095	0.093	0.3803	0.5249	7	000	9 6	0.00	0.0216	-0.0107
		For	X	-94.32	51.25	-68.05	-57.40	46.76	-39.66	-32.56	04.67	98.3		97 17	101	997.	7	77.	£ 5	2 2	\$ 5 5 5	2 6	3 5	690	72	88	2 5	12	1 2	25. 4	98	6.25	7.50	8.75	10.00	12.50	15.00	17.50	20.00	90.00	900	3 5	90.02	8 8	8 6	129.17	145.83
		ž	· <u>P</u> .	0.0278	0.0402	013	0.1593	0.2258	0.2702	0.3241	6																																				
		Afterboo		190.28 0.0			_			284.72 0.3																																					
	• = 180°		_									8 5		2 8	3 8	2 3	3 %	3 \$	1 8	2 2	6 2	3 2		23	7	17	22	22	2	: ==	2	<u>.</u>	0	2													
2 * 0°		Forebody		32 1.0980		Ī				31 -1.3635		1.23 - 1.3035					307T U				00000		0.8285									_	_	7 -0.0013													
mfr = 0.49 and α = 0°			Χď	-94.32	46.76	-11.26	4.	96.0	ë (	0.31	5 -			2.5	37.6	4.38	9	\$2.8	5 2	2. 8	10.00	2 2	15.00	12	20.00	30.00	40.00	\$0.00	90.09	00.07	80.00	90.00	100.00	129.17													
mfr = 0.		Afterbody	S	0.0168	0.0417	0.0584	0.1034	0.1602	0.2234	0.2006	0 3004	0.3800																																			
	<sub>0</sub> 0 = <b>0</b>	Afte	ž	173.61	206.92	223.61	245.83	262.50	10.572	284.77	300.000	97.04																																			
		Forebody	පි	1.1042	1.1074	1.1021	1.0869	1.0568	C100.1	7/66.0	0000	0.8974	0.8794	0.8884	0.0037	0810	1.1552	1.2002	1.2210	1647	1.0447	0.3562	-1.3691	-1.3945	-1.3463	-1.3307	-1.3139	-1.2975	-1.2396	-1.1821	1.1501	-1,1004	-1.0261	60.67	200	0.8913	2000	0.7668	0.6338	-0.5587	-0.4960	0.4344	-0.0471	0.0079	0.0250	90000	-0.0052
		For	X,	-82.25	-75.15	-68.05	-57.40	46.76	33.00	25.46	55	-14.81	-11.26	10.14	7.88	4.5	-2.25	1.46	06:0	-0.39	0.19	000	0.31	0.62	1.25										8 5		921									·	145.83

TABLE VII. Concluded

(e) Concluded

		ody	S S	0.0471	0.0871	0.1350	0.1925	0.2948	0.3376	0.3950																															
	•	Afterbody	χŗ	190.28	223.61	245.83	262.50	71.672	284.72	290.28																															
	<b>•</b> = 180°	d,		0.2853			69760			-0.9276	0.8349	-0.775	1009	-0.5477	-0.5416	-0.5427	0.5585	1977	-0.3939	3695	3705	0.2170	-0.1557	-0.1526	-0.1378	0.1493	0.1134	-0.0864	0.0299	0.0045											
α = 0°		Forebody		94.32 0	•	Ċ	2 6					88.						00.	_							00.00			_	29.17											
$\mathbf{mfr} = 0.81 \text{ and } \alpha = 0^{\circ}$					•	•	8 2	3 8	7	8	62																		_	_											
mfr =		Afterbody		0.0315			3 0.1390			2 0.3309																															
	°0 = 0			173.61		223.61					290.28				•	•	<b>.</b>	•			••	٠.	. •	,	•	<b></b>	·		2		4 04	- 4	0	7		× ×	. 00	. 0	4	en 0	• <b>v</b> ç
	•	Forebody	G.	0.2840	0.1173	0.0476	0.0367	0.1870	0.1906	-0.3432	-0.6895	0.6113	0.4138	0.1954	0.1862	0.569	0.796		1.2259			0.8947					0.5901					-0.3774				0.1488		_			0.0106
		For	χŢ	94.32	-75.15	-68.05	-57.40	30.5	-32.56	-25.46	-18.36	14.8	10.14	-7.88	4.51	-2.25	-1.46	9 6	0.0 0.0	0.00	0.31	0.62	88.	2.50	3.12	3.75	5.00	6.25	7.50	8.75	2.00	15.00	17.50	20.00	30.00	80.05	00.09	70.00	80.00	0000	145.83
		*	<u>в</u>	0.0508	0.0965	0.1593	0.2318	0.3607	991	0.4803																															
		Afterbody		190.28 0.0			262.50 0.7	_																																	
	<b>•</b> = 180°		×	- (							8 .	55	£ \$	4	8	8	32	2 :	, <u>s</u>	*	83	2 2	21	\$	69	<del>.</del> .		. 02	203	30											
% •	•	orebody	G.	2 0.9167			0.4412						0 -0.8393				25 -0.6532		0.5416			50 -0.4407				00 -0.1241			_	17 -0.0030											
mfr = 0.73 and α = 0°		1	X	-94.32	46.76	-11.26	15.5	8 6	0.31	0.62	1.25	<b>86</b>	2.50	3.75	4.38	200	6.25	7.50	0001	12.50	15.00	17.50	Š	<del>6</del>	20.00	90.00	80.08	0006	100.00	129.											
٠,			۵.	0.0271	0.0688	0.1008	0.1608	0.7318	0.3523	0.4047	0.4659																														
ofr = 0		body	Ç	000	9	0	_																																		
mfr = 0	ం	Afterbody		173.61 0.0			245.83		279.17	284.72	290.28																														
mfr = 0	°0 *		XI	13.61		223.61		72.50				0.2492	0.1480	0.1858	0.4181	0.7483	0.9350	1.0708	1.2147	0.8304	-0.9914	-1.0233	-0.8878	-0.8484	-0.7950	-0.7712	0.7421	-0.6559	-0.6391	-0.6253	0.4087	-0.5026	-0.5015	-0.4592	-0.0762	-0.0773	0.1287	-0.1265	-0.1032	0.0344	0.0100
mfr = 0	°0 * •		CP X/L	173.61	0.9392 206.94	0.9269 223.61	245.83	0.207 0.7361	0.6390	0.5042	0.3407		11.26 0.1480						0.39 1.2147			0.62 -1.0233		2.50 -0.8484			4.38 -0.7421 4.00 -0.7337				10.00 -0.5712						60.00 -0.1287				145.83 0.0100
mfr = 0	°0 ×		CP X/L	-94.32 0.9171 173.61	-75.15 0.9392 206.94	-68.05 0.9269 223.61	-57.40 0.8860 245.83	-40.70 0.8110 202.50	-32.56 0.6390	-25.46 0.5042	-18.36 0.3407																														•
mfr = 0	°() × 🗢	Forebody	X/L CP X/L	0.0468 -94.32 0.9171 173.61	0.0916 -75.15 0.9392 206.94	0.1511 -68.05 0.9269 223.61	0.2212 -57.40 0.8860 245.83	0.2908 -40.70 0.8110 202.50	0.4025 -32.56 0.6390	0.4650 -25.46 0.5042	-18.36 0.3407																														•
mfr = 0		Afterbody Forebody	X/L CP X/L	-94.32 0.9171 173.61	0.0916 -75.15 0.9392 206.94	0.1511 -68.05 0.9269 223.61	0.2212 -57.40 0.8860 245.83	-40.70 0.8110 202.50	0.4025 -32.56 0.6390	0.4650 -25.46 0.5042	-18.36 0.3407									00:0	0.31																				•
	on = 1800 on = 1800 on = 1800	Afterbody Forebody	XL CP XL CP XL	190.28 0.0468 -94.32 0.9171 173.61	0.0916 -75.15 0.9392 206.94	245.83 0.1511 -68.05 0.9269 223.61	262.50 0.2212 -57.40 0.8860 245.83	0.2968 40.70 0.8110 202.50	3 284.72 0.4025 -32.56 0.6390	290.28 0.4650 -25.46 0.5042	-18.36 0.3407	14.81		20.5		-2.25	-1.46		6.39	00:0	0.31		1.88		3.12	3.75		6.25	7.50												•
		Afterbody Forebody	XL CP XL CP XL	0.9722 190.28 0.0468 -94.32 0.9171 173.61	223.61 0.0916 -75.15 0.9392 206.94	0.3892 245.83 0.1511 -68.05 0.9269 223.61	0.6472 262.50 0.2212 -57.40 0.8860 245.83	\$ 2/3.61 0.2968 -46.70 0.8110 202.30	1,1198 284,72 0.4025 -32.56 0.6390	1.1887 290.28 0.4650 -25.46 0.5042	-1.1188 -0.3407	-1.0260	-11.26	-0.9455	-0.8449	-0.8180	-0.7657 -1.46	-0.7380	6.39	0.6576 0.00	-0.6229 0.31	0.62	0.4699	-0.1822 2.50	-0.0381	-0.0708	86.4	-0.0830 6.25	-0.0229	-0.0075											•
		Forebody Afterbody Forebody	XI CP XI CP X/I CP XII	94.32 0.9722 190.28 0.0468 -94.32 0.9171 173.61	-87.25 0.9800 200.94 0.0612 -82.25 0.5553 150.26 -46.76 0.8904 223.61 0.0916 -75.15 0.9392 206.94	-11.26 0.3892 245.83 0.1511 -68.05 0.9269 223.61	4.51 0.6472 262.50 0.2212 -57.40 0.8860 245.83	4.90 1.1563 2/3.61 0.2968 46.70 0.8110 262.50	0.31 -1.1198 284.72 0.4025 -32.56 0.6390	0.62 -1.1887 290.28 0.4650 -25.46 0.5042	1.25 -1.1188 -18.36 0.3407	-1.0260	0.9614 -11.26	-0.9455	-0.8449	-0.8180	-0.7657 -1.46	-0.7380	-0.7115 -0.39	0.6576 0.00	-0.6229 0.31	0.62	0.4699	-0.1822 2.50	-0.0381	-0.0708	0.0894 4.38	-0.0830 6.25	-0.0229	-0.0075											•
mfr = 0.67 and a = 0°	• iii 1800°	Afterhody Forebody Afterbody Forebody	CP XI CP XI CP XII CP XII	0.0306 -94.32 0.9722 190.28 0.0468 -94.32 0.9171 173.61	0.0462 -82.25 0.9866 200.94 0.0672 -82.25 0.9553 190.26 0.0645 -46.76 0.8904 223.61 0.0916 -75.15 0.9392 206.94	0.0943 -11.26 0.3892 245.83 0.1511 -68.05 0.9269 223.61	0.1523 4.51 0.6472 262.50 0.2212 .57.40 0.8860 245.83	0,2215 - 40,90 1,1563 2/3,61 0,2968 -46,70 0,6110 202,50	0.3354 0.31 -1.1198 284.72 0.4025 -32.56 0.6390	0.3916 0.62 1.1887 290.28 0.4650 -25.46 0.5042	0.4532 1.25 -1.1188 -1.836 0.3407	-1.0260	0.9614 -11.26	-0.9455	-0.8449	-0.8180	-0.7657 -1.46	-0.7380	-0.7115 -0.39	0.6576 0.00	-0.6229 0.31	0.62	0.4699	-0.1822 2.50	-0.0381	-0.0708	0.0894 4.38	-0.0830 6.25	-0.0229	-0.0075											•
		Afterhody Forebody Afterbody Forebody	XI CP XI CP XI CP XII CP XII	173.61 0.0306 -94.32 0.9722 190.28 0.0468 -94.32 0.9171 173.61	190.28 0.1462 -82.25 0.9866 200.34 0.0672 -82.25 0.5555 170.26 206.94 0.0645 -46.76 0.8904 223.61 0.0916 -75.15 0.9392 206.94	223.61 0.0943 -11.26 0.3892 245.83 0.1511 -68.05 0.9269 223.61	245.83 0.1523 4.51 0.6472 262.50 0.2212 -57.40 0.8860 245.83	262.50 0.2215 -0.90 1.1563 273.61 0.2968 -46.76 0.8110 202.50	279 17 0.3394 0.31 -1.1198 284.72 0.4025 -32.56 0.6390	284.72 0.3916 0.62 -1.1887 290.28 0.4650 -25.46 0.5042	290.28 0.4532 1.25 -1.1188 -1.836 0.3407	1.88 -1.0260 -14.81	2.50 -0.9614 -11.26	7.75 - 0.9453 7.75 - 0.9664 - 2.88	4.38 -0.8449	5.00 -0.8180 -2.25	6.25 -0.7657 -1.46	7.50 -0.7380 -0.90	8.75 - 0.7115 - 0.39	12.50 -0.6576 0.00	15.00 -0.6229 0.31	17.50 -0.5789 0.62	88'T 6698'O 00'07	40.00 -0.1822 2.50	50.00 -0.0381 3.12	60.00 -0.0708 3.75	70,00 -0,0894 4.38	90.00 -0.0830 6.25	100.00 -0.0229 7.50	129.17 -0.0075 8.75	00.01	0031	17.50	20:00	3000	803	0009	0002	00'08	00'001	145.83
	- De 1900	Afterhody Forebody Afterbody Forebody	XI CP XI CP XI CP XII CP XII	0.9712 173.61 0.0306 -94.32 0.9722 190.28 0.0468 -94.32 0.9171 173.61	0.0462 -82.25 0.9866 200.94 0.0672 -82.25 0.9553 190.26 0.0645 -46.76 0.8904 223.61 0.0916 -75.15 0.9392 206.94	0.9803 223.61 0.0943 -11.26 0.3892 245.83 0.1511 -68.05 0.9269 223.61	0.9467 245.83 0.1523 4.51 0.6472 262.50 0.2212 57.40 0.8860 245.83	0.8873 262.50 0.2215 40.90 1.1363 273.61 0.2968 46.76 0.8110 202.30	0.3354 0.31 -1.1198 284.72 0.4025 -32.56 0.6390	0.6515 284.72 0.3916 0.62 1.1887 290.28 0.4650 -25.46 0.5042	0.5440 290.28 0.4532 1.25 -1.1188 -18.36 0.3407	0.4962 1.88 -1.0260 -14.81	0.4087 2.50 -0.9614 -11.26	-0.9455	0.0413 4.38 -0.8449 4.51	5 0.8920 5.00 -0.8180 -2.25	1.0416 6.25 -0.7657 -1.46	1.1510 7.50 -0.7380 -0.50	-0.7115 -0.39	0.7113 12.50 -0.6576 0.00	.1.1362 15.00 -0.6229 0.31	-1.1464 17.50 -0.5789 0.62	88'1 669P 0 0 0 0 t 0 101'1-	-0.9884 40.00 -0.1822 2.50	-0.9178 50.00 -0.0381 3.12	60.00 -0.0708 3.75	-0.8496 70.00 -0.0894 4.38	-0.0400 -0.0001 -0.000	100.00 -0.0229 7.50	-0.7264 129.17 -0.0075 8.75	0.6774		-0,6092	-0.5695 20.00	-0.4532	-0.3526		70007	-0.0882	0.0368	•

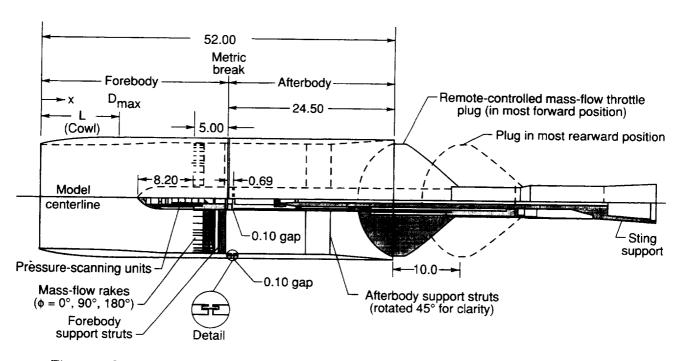


Figure 1. Simplified cross-sectional sketch of complete model. Linear dimensions are in inches.

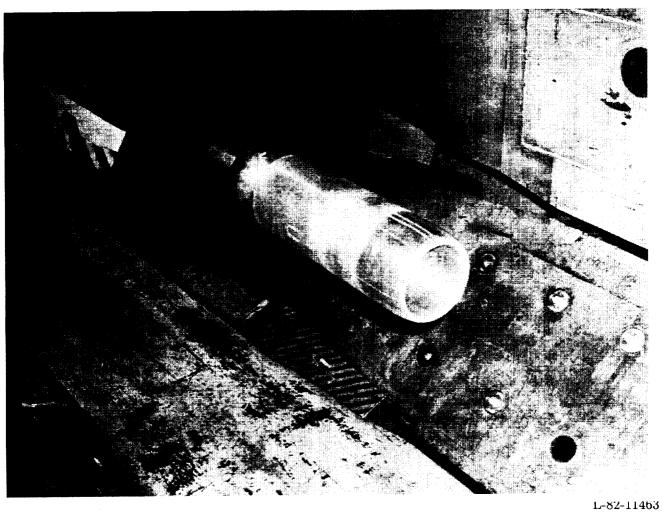


Figure 2. Complete model installed in 16-Foot Transonic Tunnel test section.

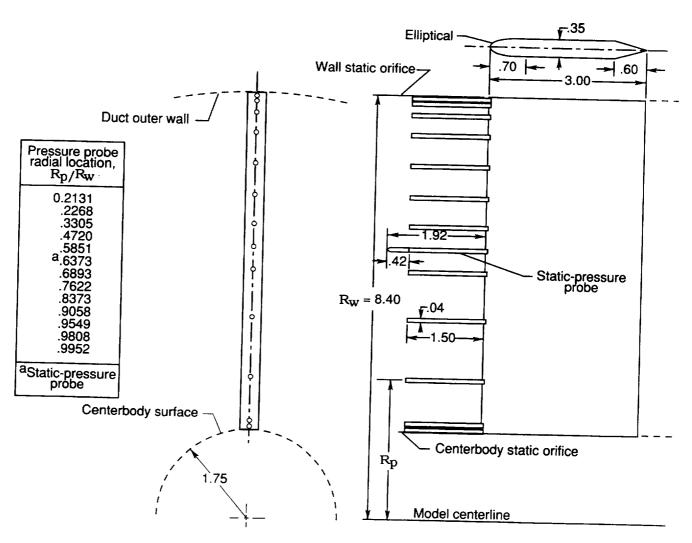


Figure 3. Pressure instrumentation (on struts at  $\phi=0^{\circ}, 90^{\circ}, \text{ and } 180^{\circ}$ ) used to obtain data for mass-flow computations. Linear dimensions are in inches.

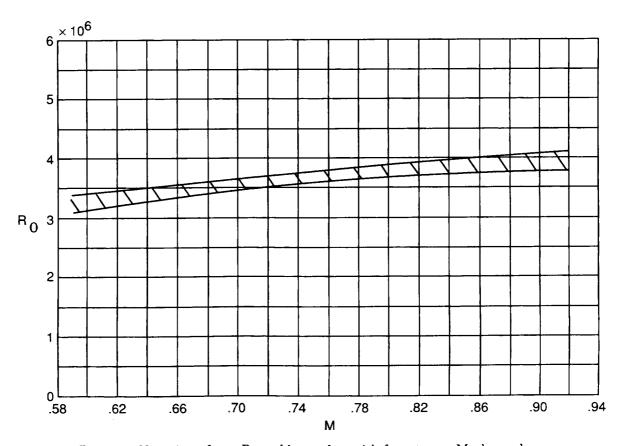


Figure 4. Variation of test Reynolds number with free-stream Mach number.

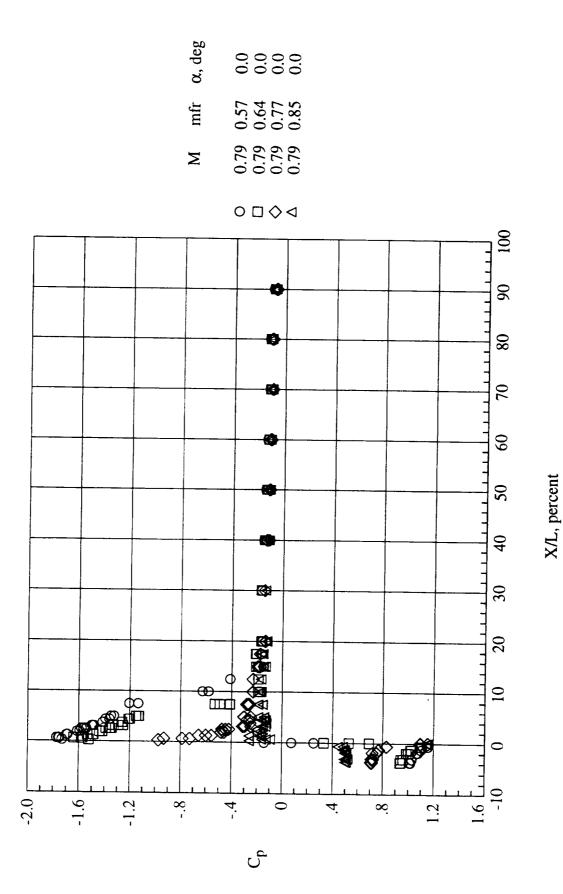
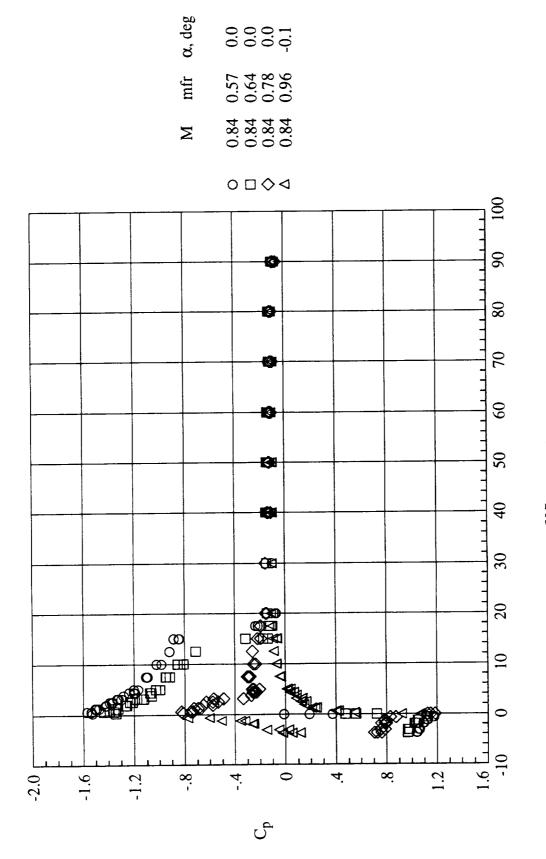


Figure 5.- Pressure coefficient variation with X/L for the NACA 1-85-100 inlet with a contraction ratio of 1.009 for several mass-flow ratios at  $lpha=0^\circ$  . Data combined from  $\hbar=0^\circ$  400 and 1800 maridians

(a) M = 0.79.



X/L, percent

(b) M = 0.84. Figure 5.- Continued.

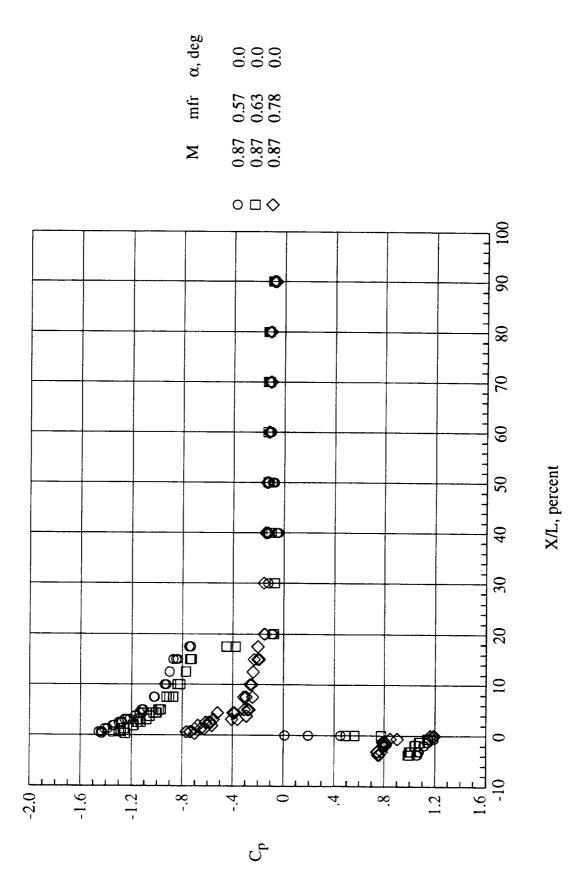
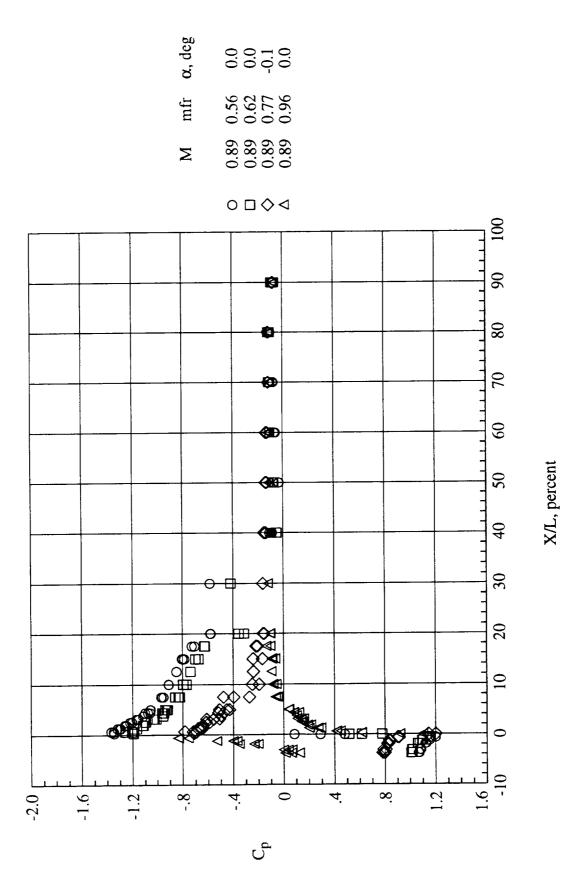


Figure 5.- Continued.

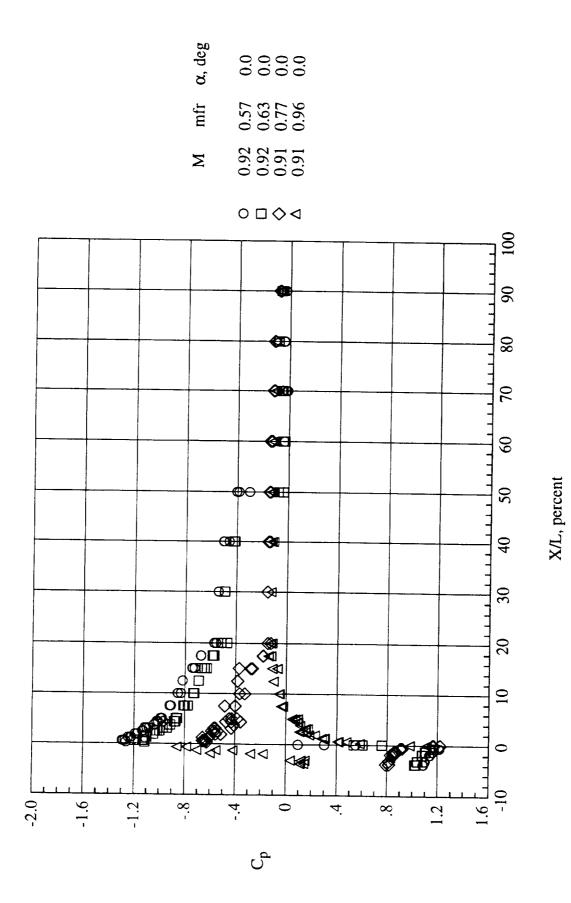
(c) M = 0.87.

100



(d) M = 0.89. Figure 5.- Continued.

101



(e) M = 0.92.

Figure 5.- Concluded.

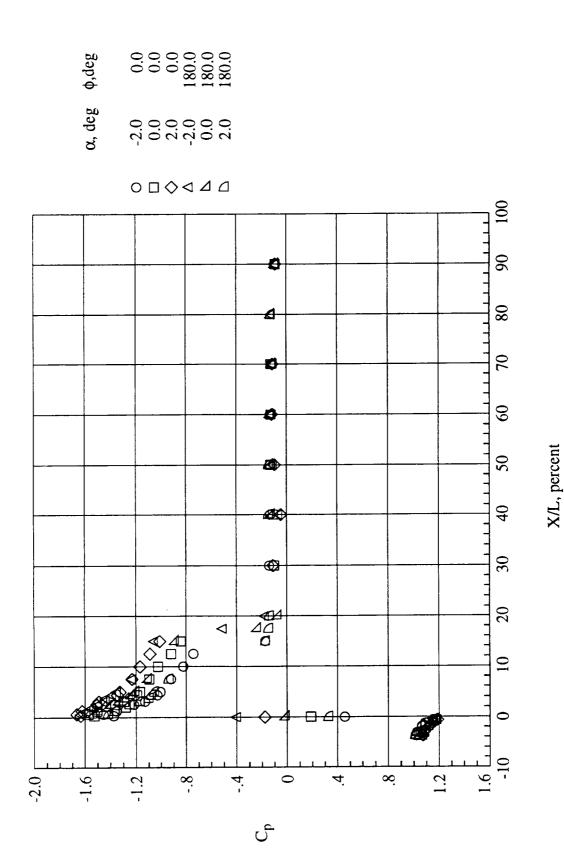
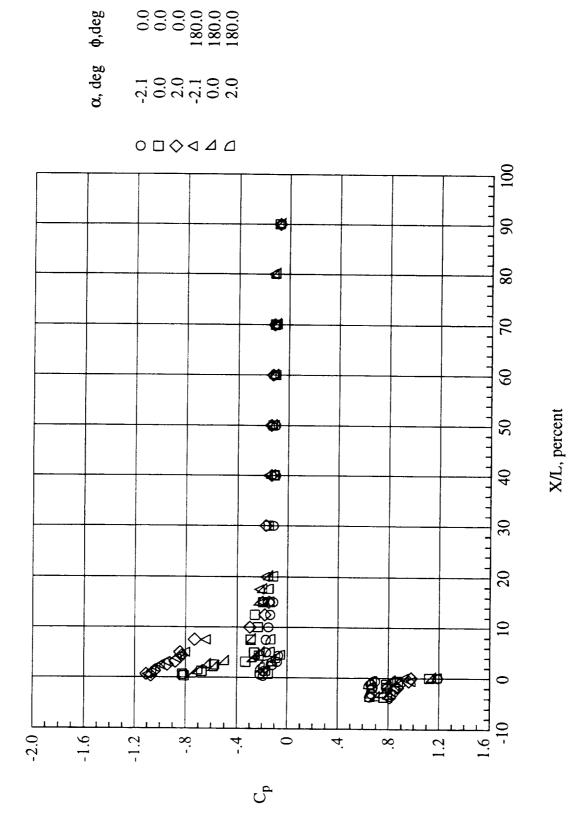


Figure 6.- Pressure coefficient variation with X/L along the  $\phi = 0^{\circ}$ , and 180° meridians for the NACA 1-85-100 inlet with a contraction ratio of 1.009 at several angles of attack.

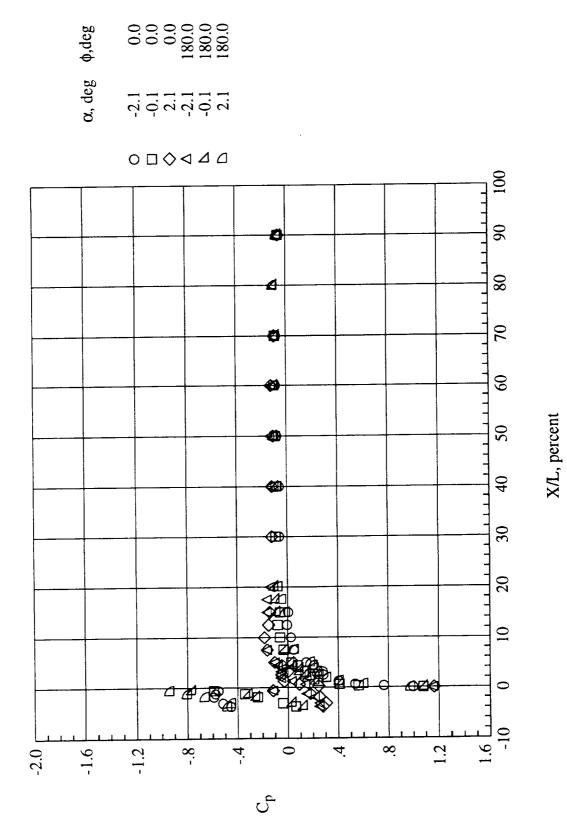
(a) M = 0.84 and mfr = 0.57.



(b) M = 0.84 and mfr = 0.78.

Figure 6.- Continued.

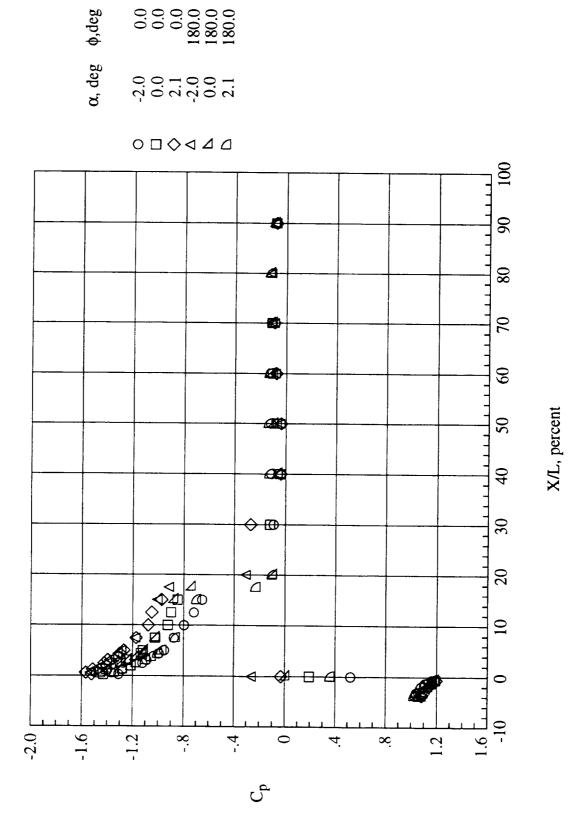
104



(c) M = 0.84 and mfr = 0.95.

Figure 6.- Continued.

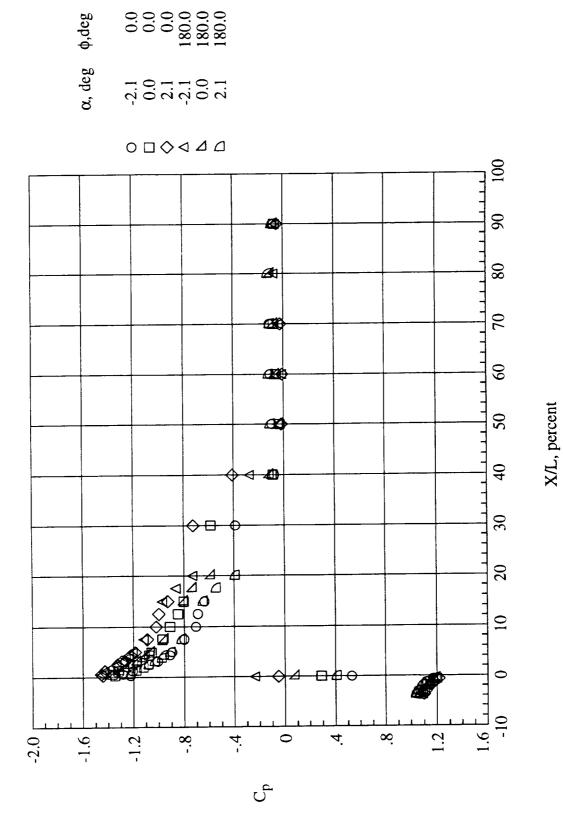
105



(d) M = 0.87 and mfr = 0.57.

Figure 6.- Continued.

106



(e) M = 0.89 and mfr = 0.57.

Figure 6.- Concluded.

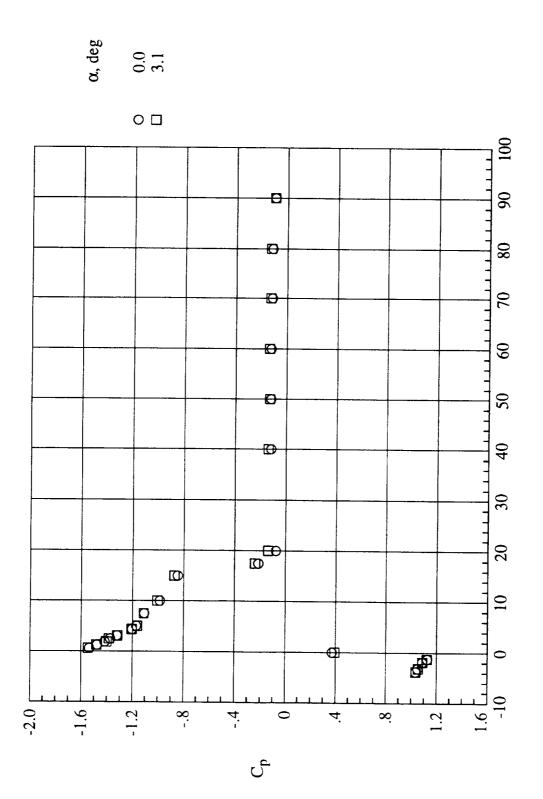
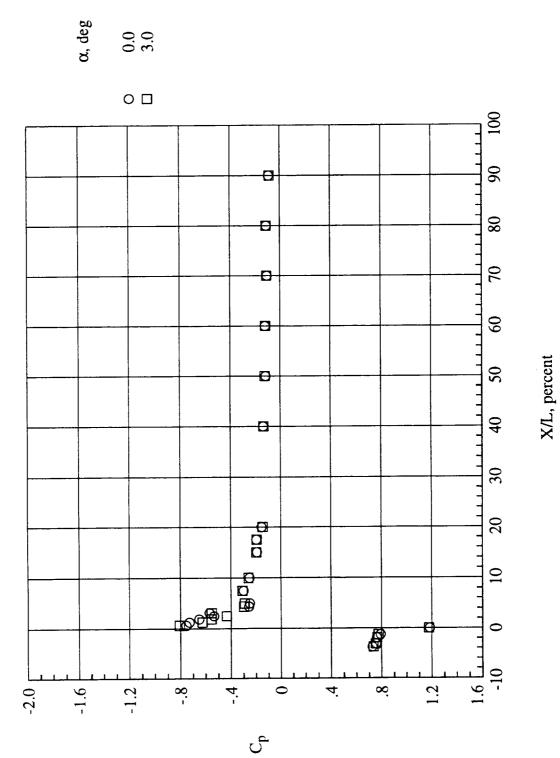


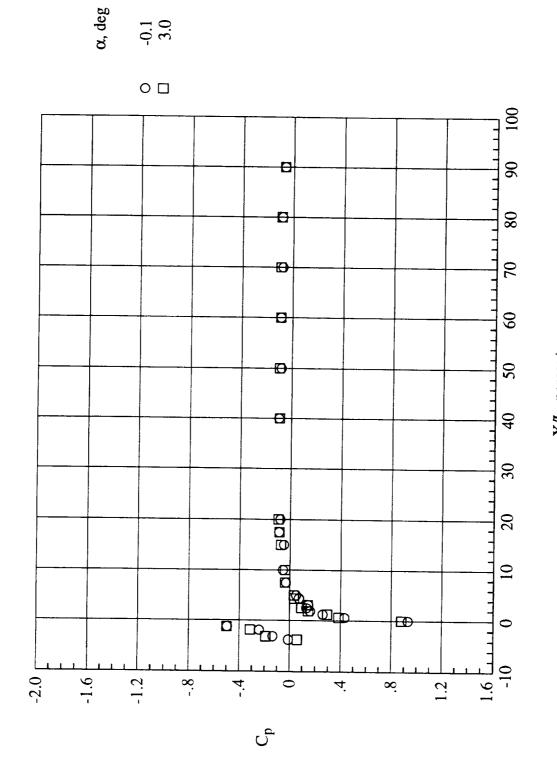
Figure 7.- Pressure coefficient variation with X/L along the  $\phi = 90^\circ$  meridian for the NACA 1-85-100 inlet with a

(a) M = 0.84 and mfr = 0.57.

X/L, percent

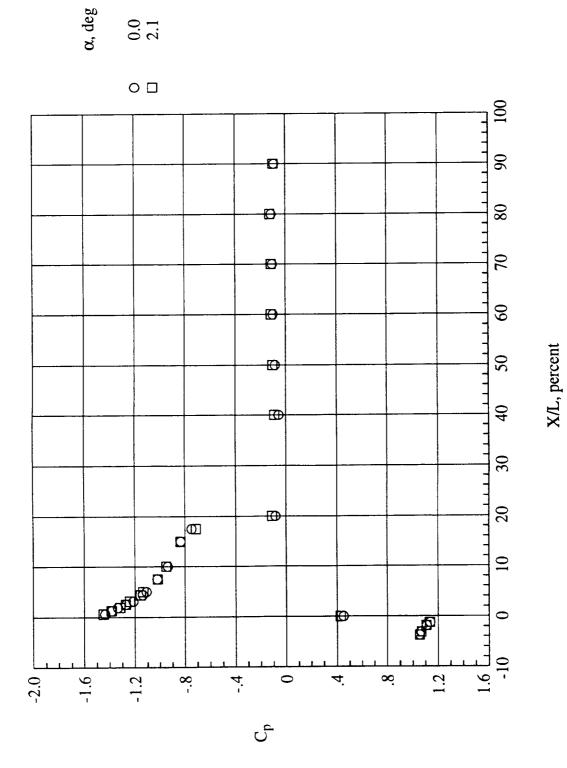


(b) M = 0.84 and mfr = 0.78.Figure 7.- Continued.

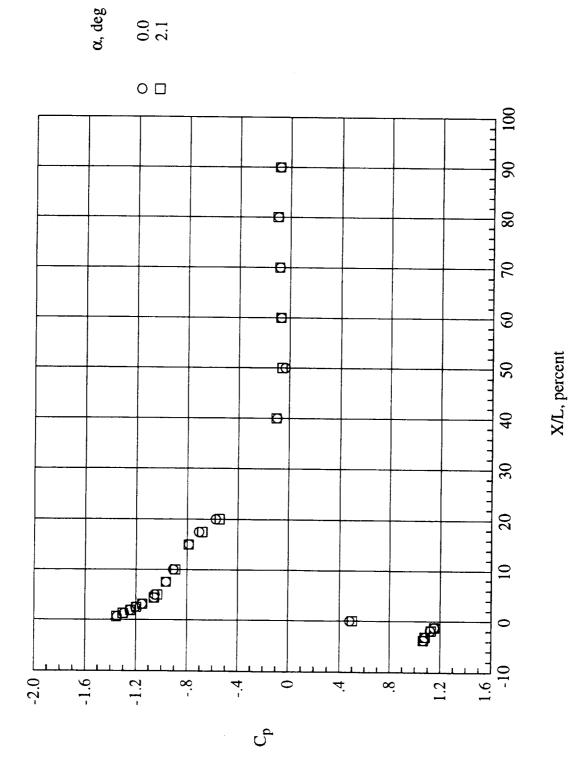


(c) M = 0.84 and mfr = 0.95.

110



(d) M = 0.87 and mfr = 0.57. Figure 7.- Continued.



(e) M = 0.89 and mfr = 0.57. Figure 7.- Concluded.

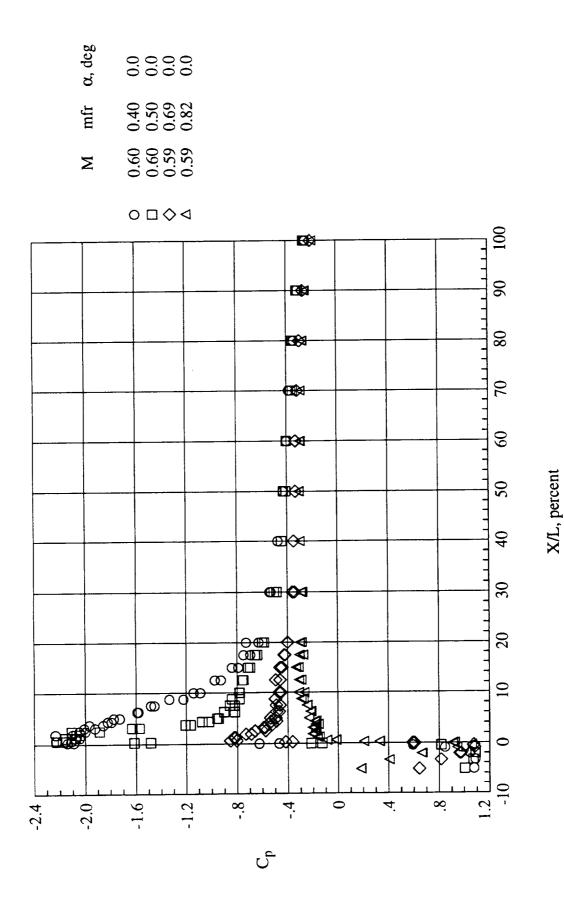


Figure 8.- Pressure coefficient variation with X/L for the NACA 1-85-43.9 inlet with a contraction ratio of 1.250 for several mass-flow ratios at  $\alpha = 0^{\circ}$ . Data combined from  $\phi = 0^{\circ}$  and  $180^{\circ}$  meridians.

(a) M = 0.60.

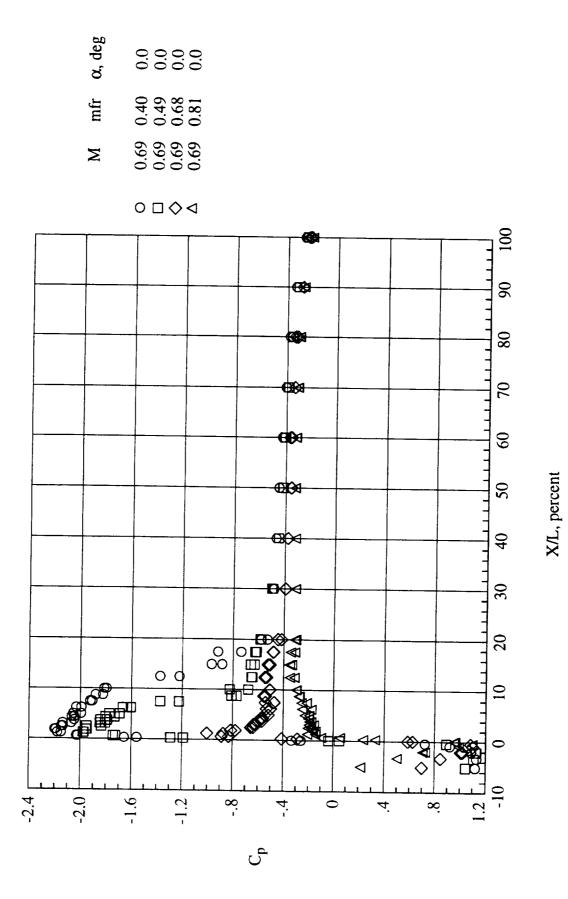
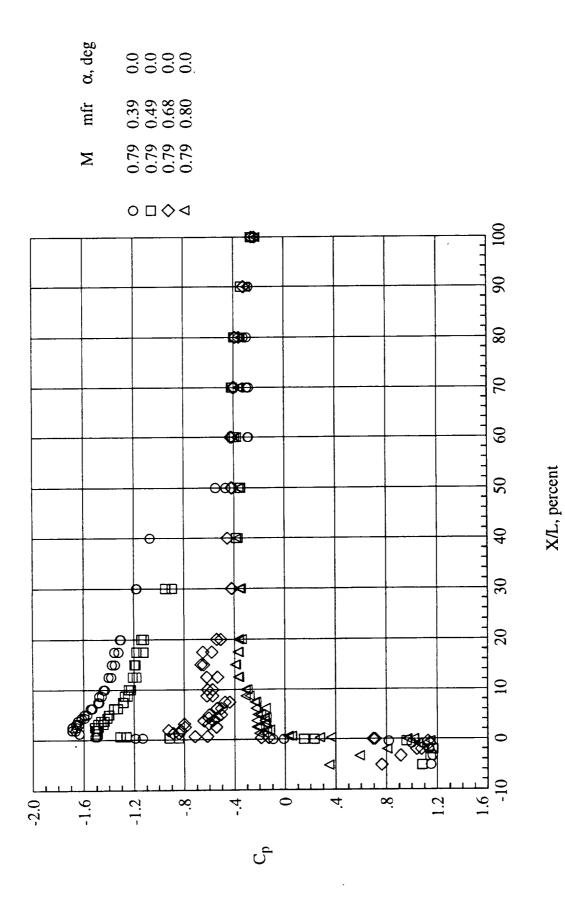


Figure 8.- Continued.

(b) M = 0.69.

114



(c) M = 0.79.

Figure 8.- Continued.

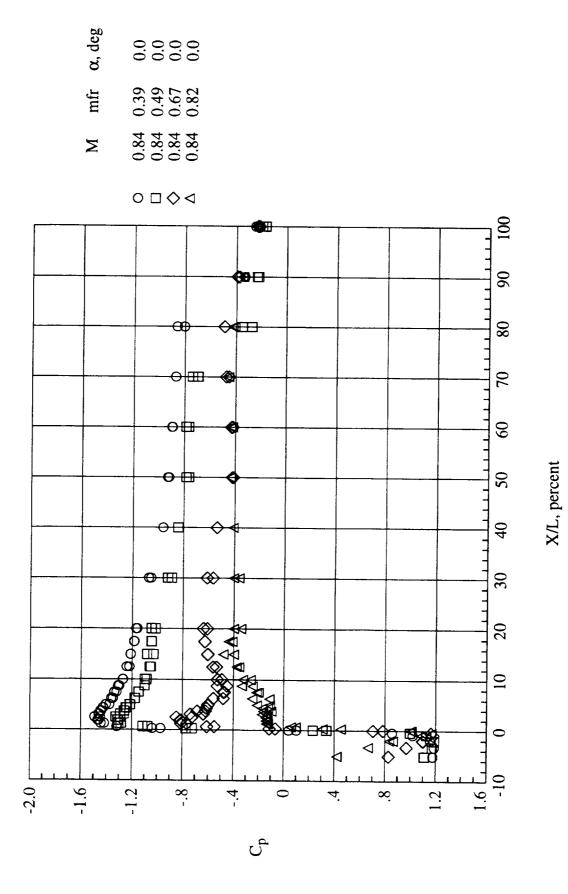
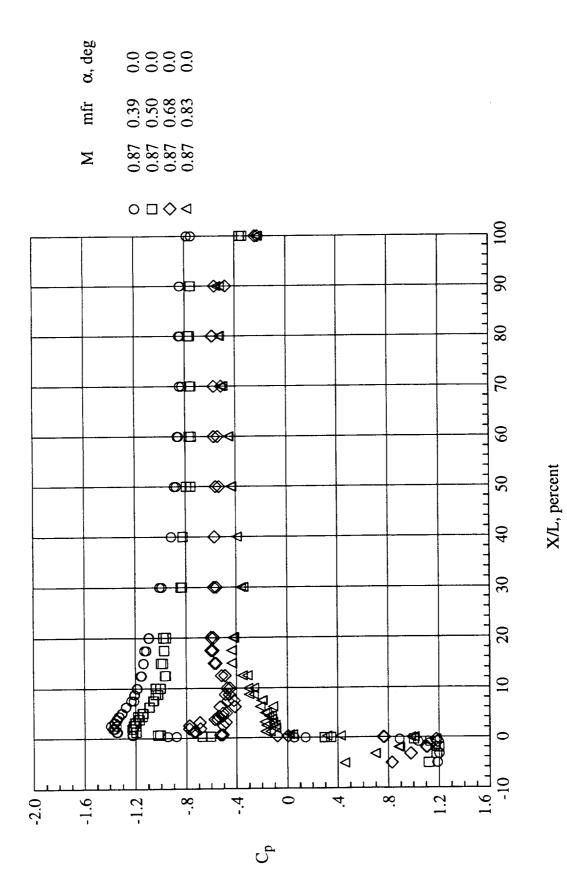


Figure 8.- Continued.

(d) M = 0.84.

116



(e) M = 0.87. Figure 8.- Continued.

117

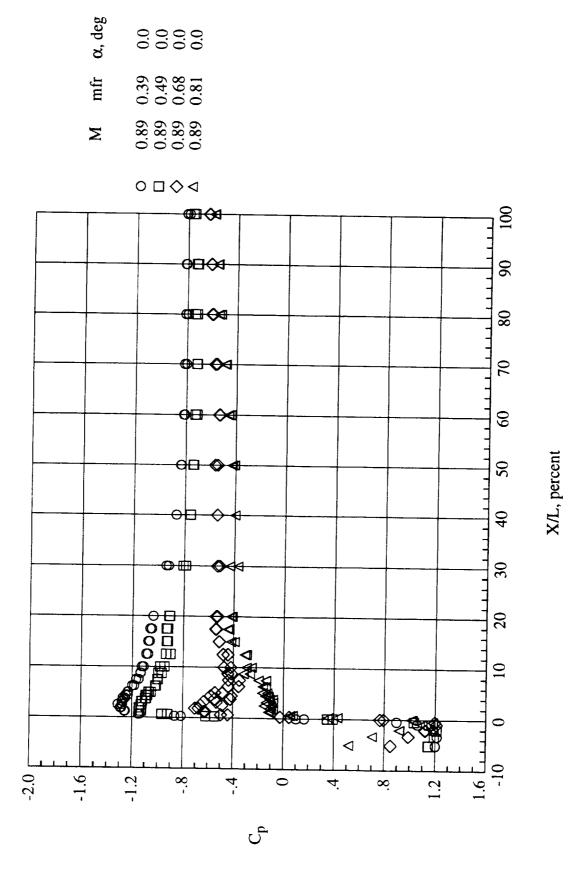
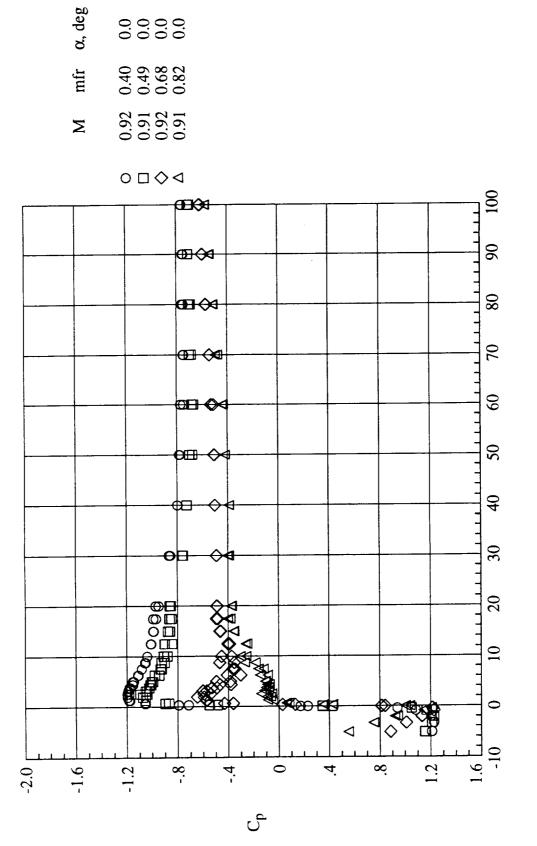


Figure 8.- Continued.

(f) M = 0.89.

118



X/L, percent

(g) M = 0.92.

Figure 8.- Concluded.

119

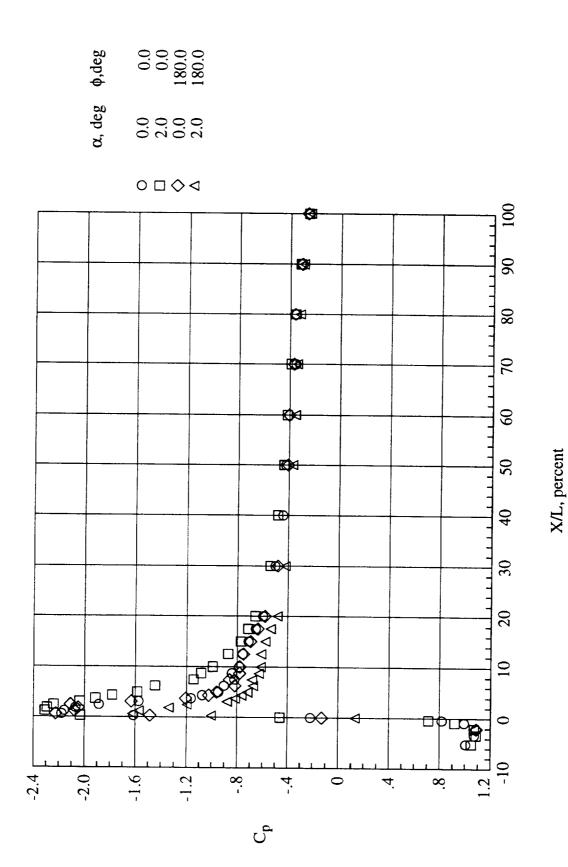
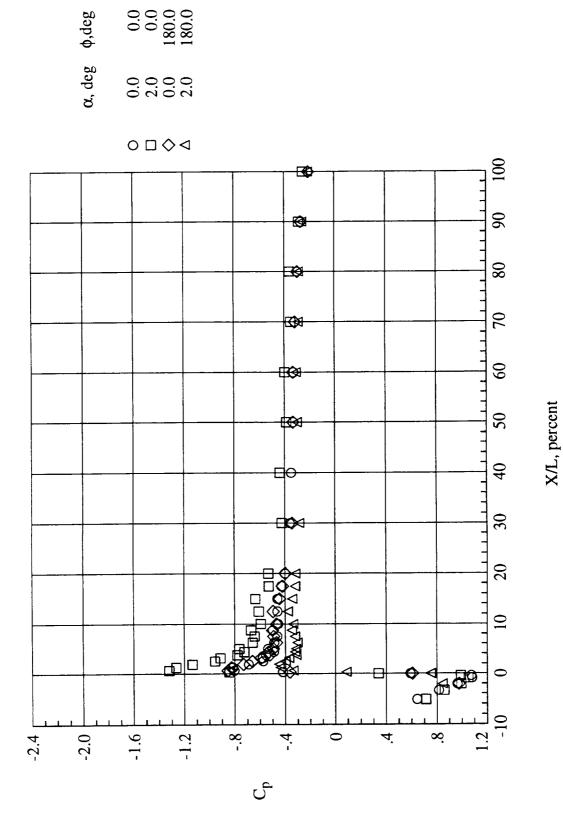


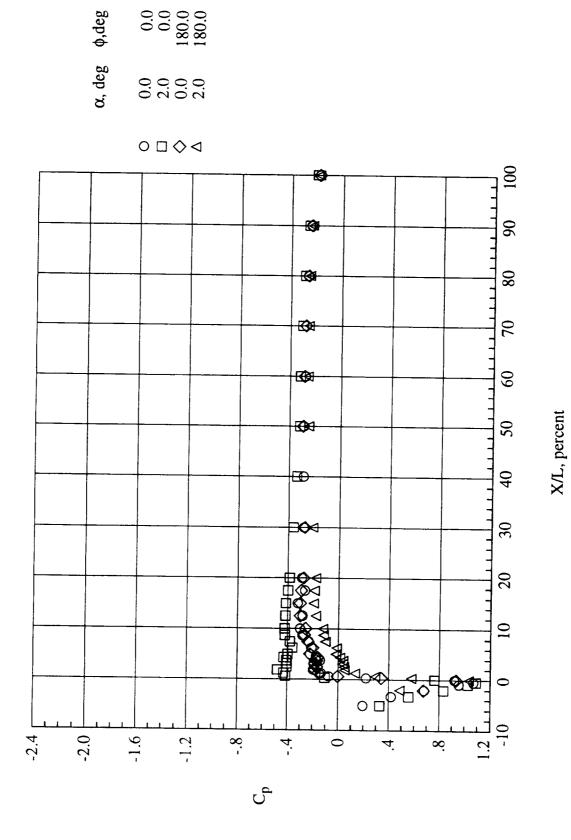
Figure 9.- Pressure coefficient variation with X/L along the  $\phi = 0^{\circ}$ , and 180° meridians for the NACA 1-85-43.9 inlet with a contraction ratio of 1.250 at two anoles of attack

(a) M = 0.60 and mfr = 0.50.



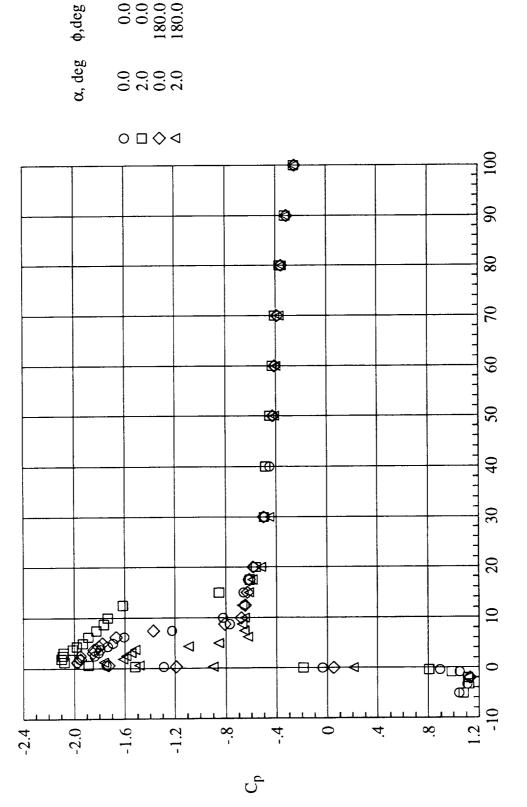
(b) M = 0.59 and mfr = 0.69.

121



(c) M = 0.59 and mfr = 0.82.

122

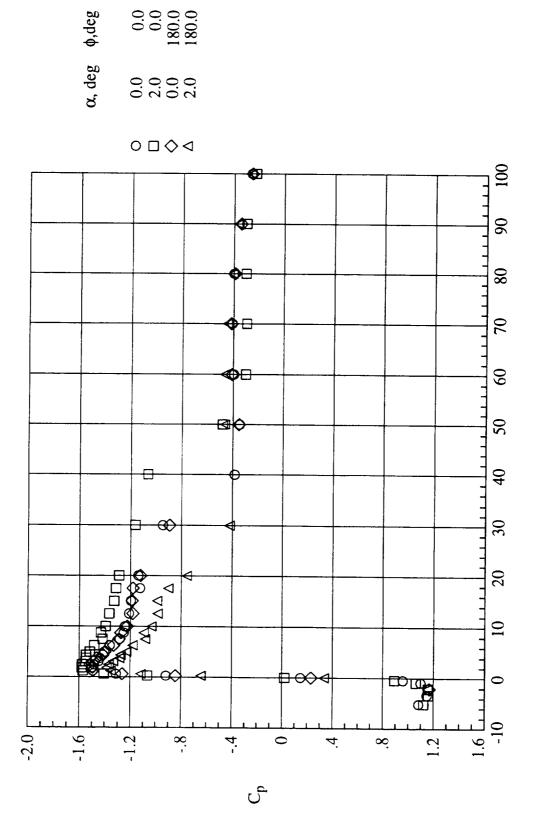


0.0 0.0 180.0 180.0

(d) M = 0.69 and mfr = 0.49.

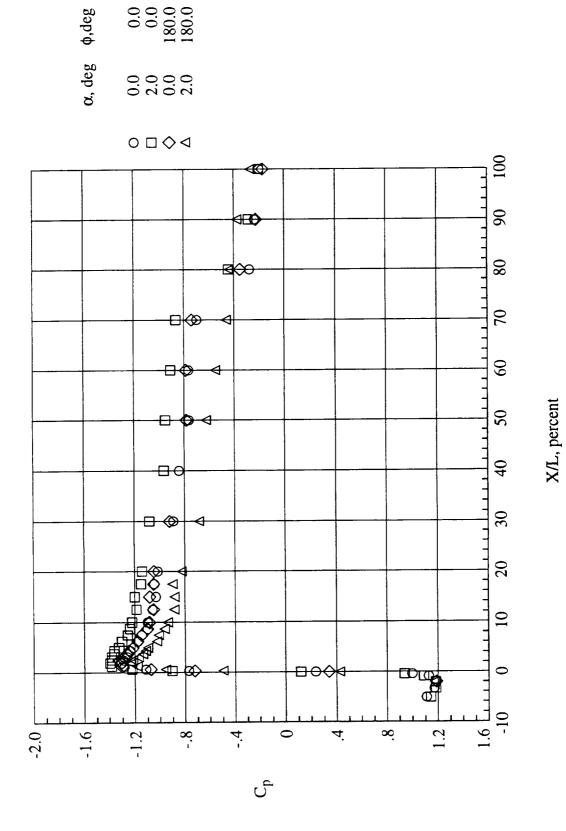
X/L, percent

123



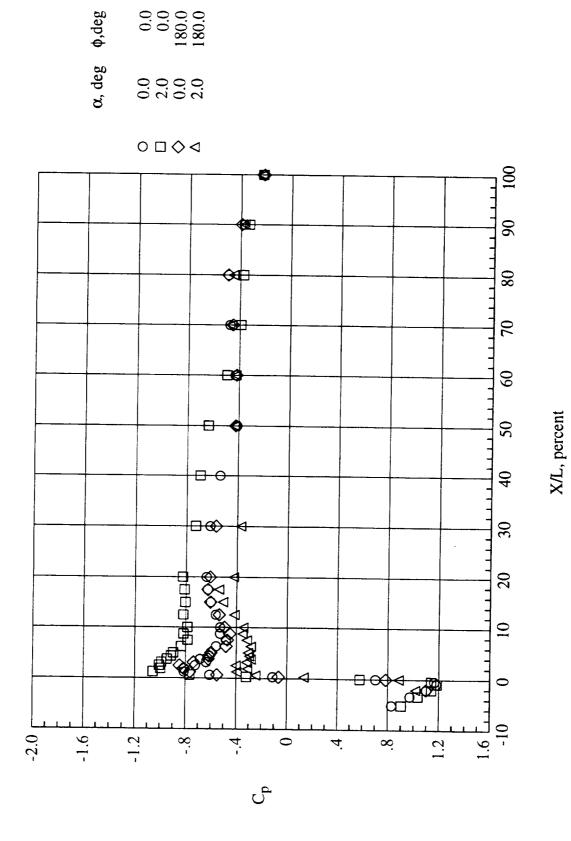
(e) M = 0.79 and mfr = 0.49.

X/L, percent

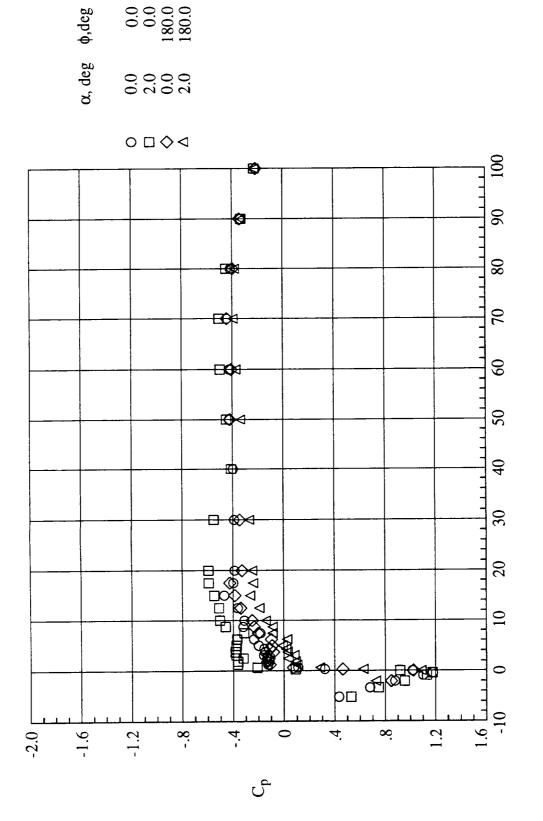


(f) M = 0.84 and mfr = 0.49.

125

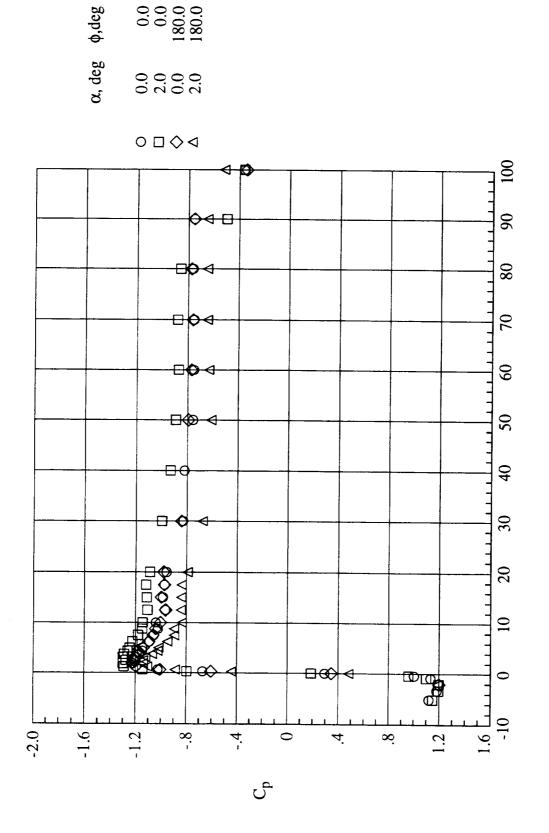


(g) M = 0.84 and mfr = 0.67. Figure 9.- Continued.



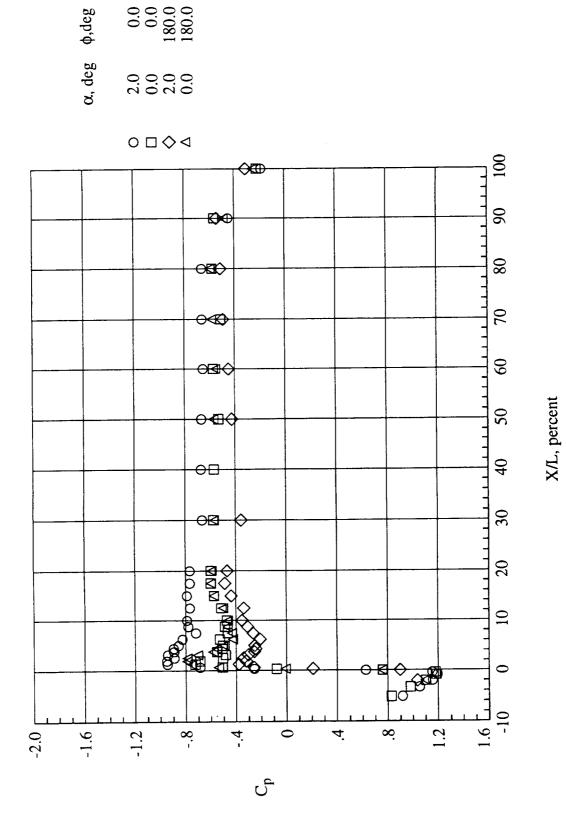
X/L, percent

(h) M = 0.84 and mfr = 0.83. Figure 9.- Continued.



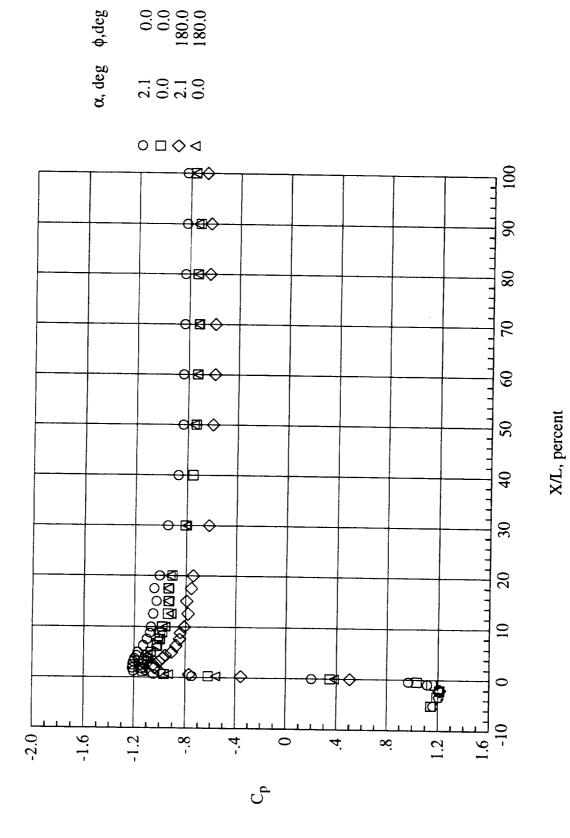
X/L, percent (i) M = 0.87 and mfr = 0.49.

128



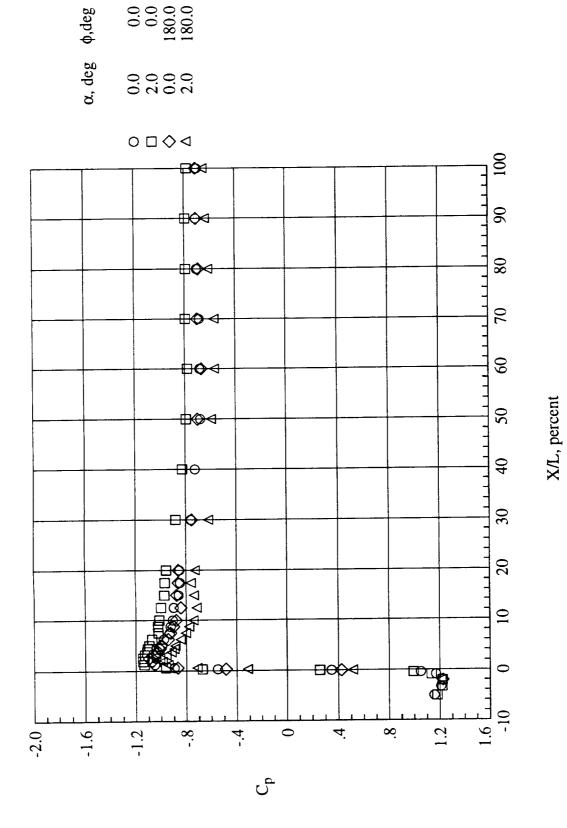
(j) M = 0.87 and mfr = 0.67.

129

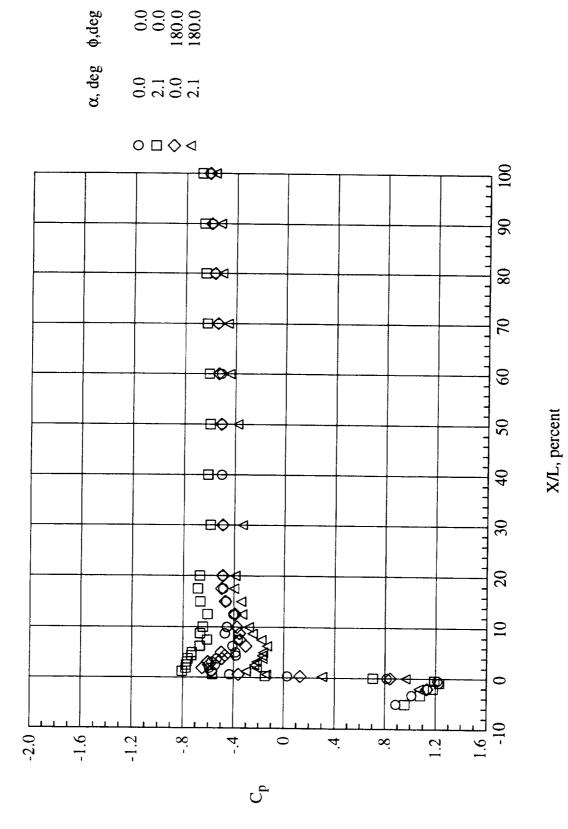


(k) M = 0.89 and mfr = 0.49.

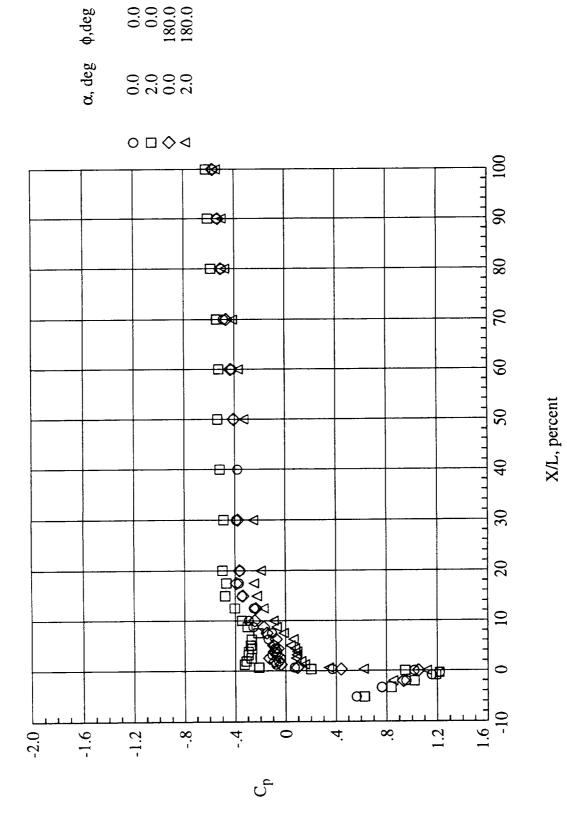
130



(1) M = 0.92 and mfr = 0.49.



(m) M = 0.92 and mfr = 0.68. Figure 9.- Continued.



(n) M = 0.92 and mfr = 0.82. Figure 9.- Concluded.

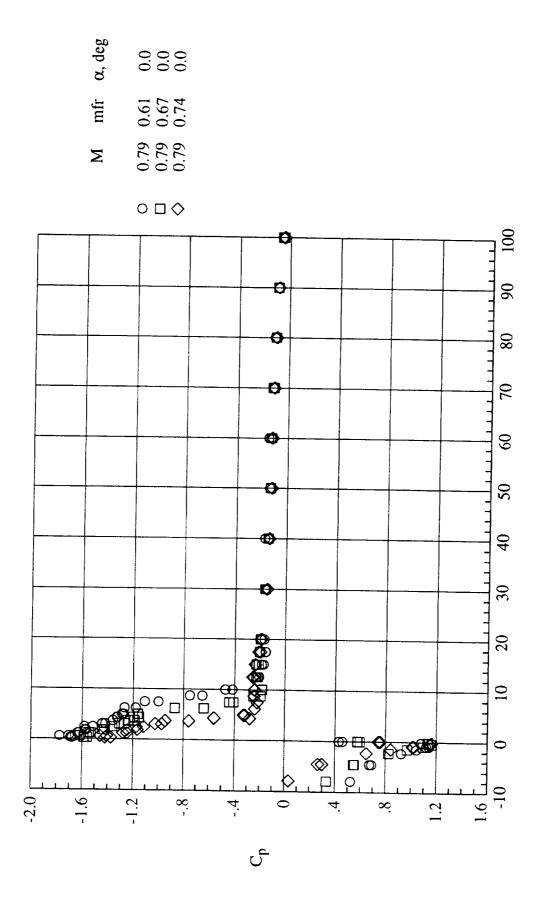


Figure 10.- Pressure coefficient variation with X/L for the NACA 1-85-100 inlet with a contraction ratio of 1.250 for several mass-flow ratios at  $lpha=0^\circ$  . Data combined from  $\hbar=0^\circ$  and 180° maridians

(a) M = 0.79.

X/L, percent

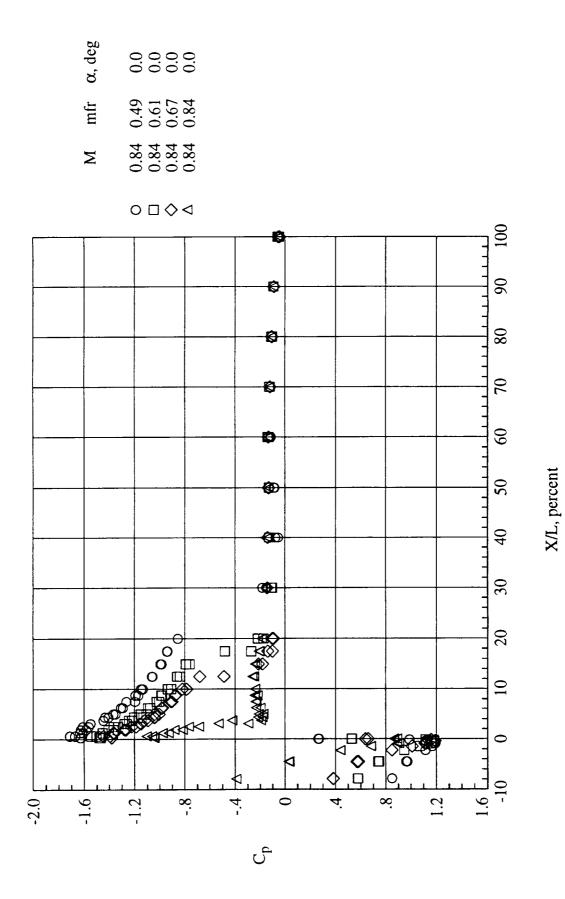


Figure 10.- Continued.

(b) M = 0.84.

135

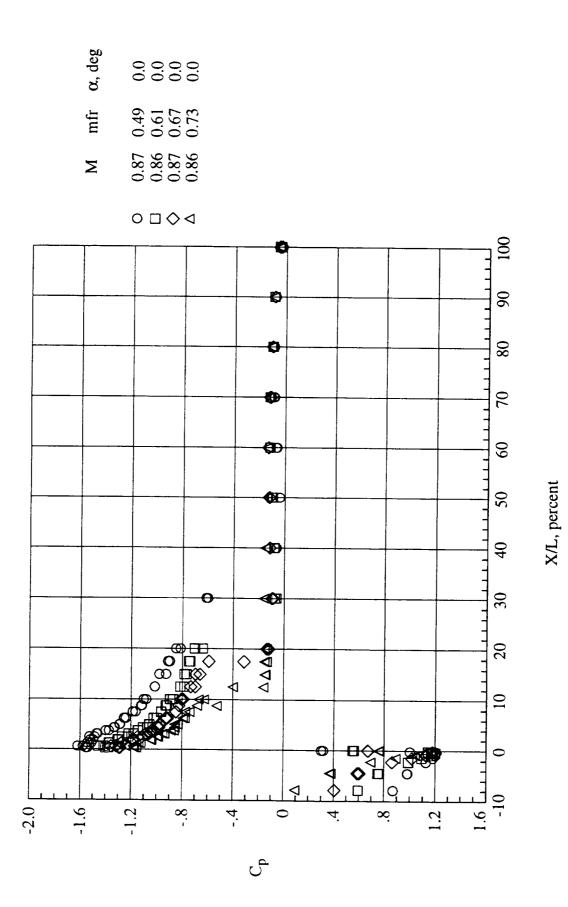


Figure 10.- Continued.

(c) M = 0.87.

136

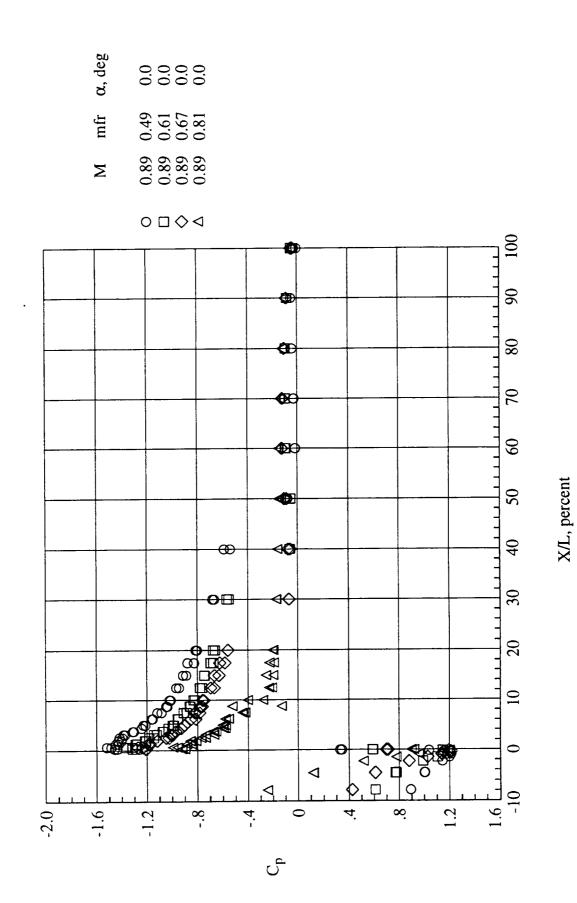
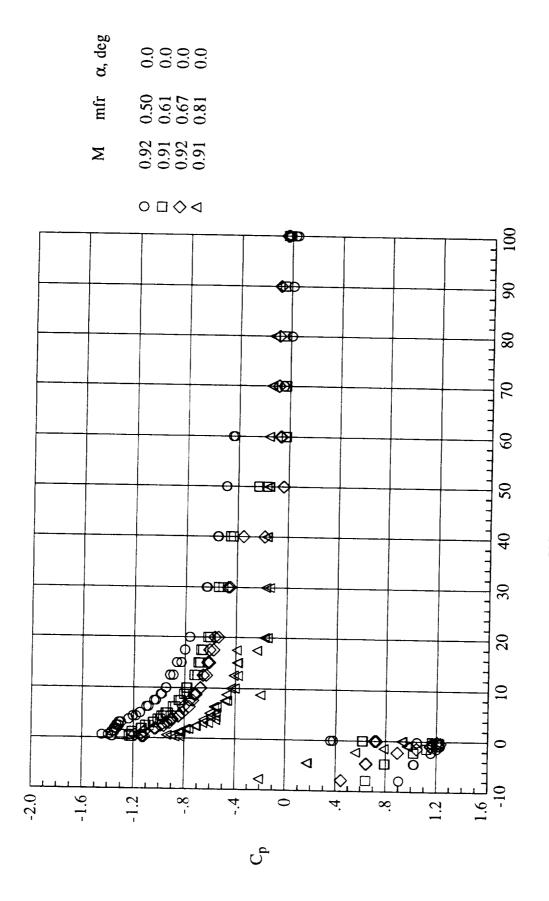


Figure 10.- Continued. (d) M = 0.89.



(e) M = 0.92.

Figure 10.- Concluded.

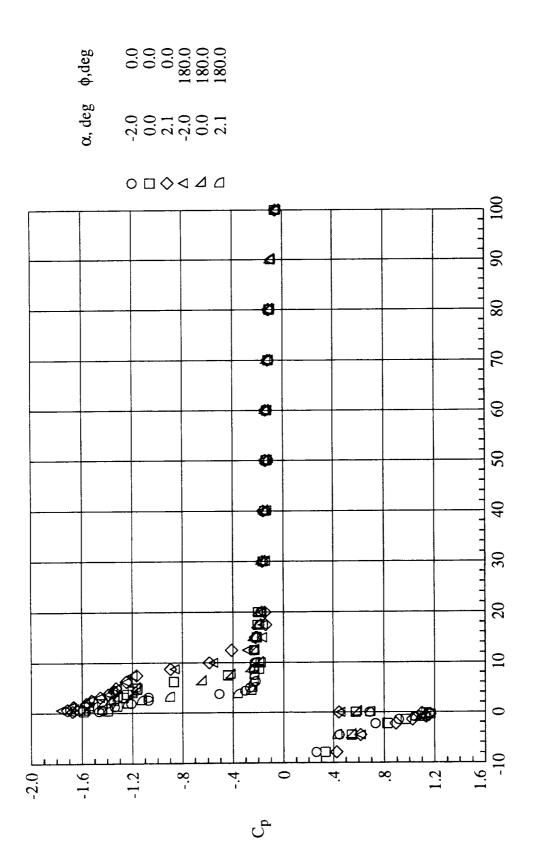
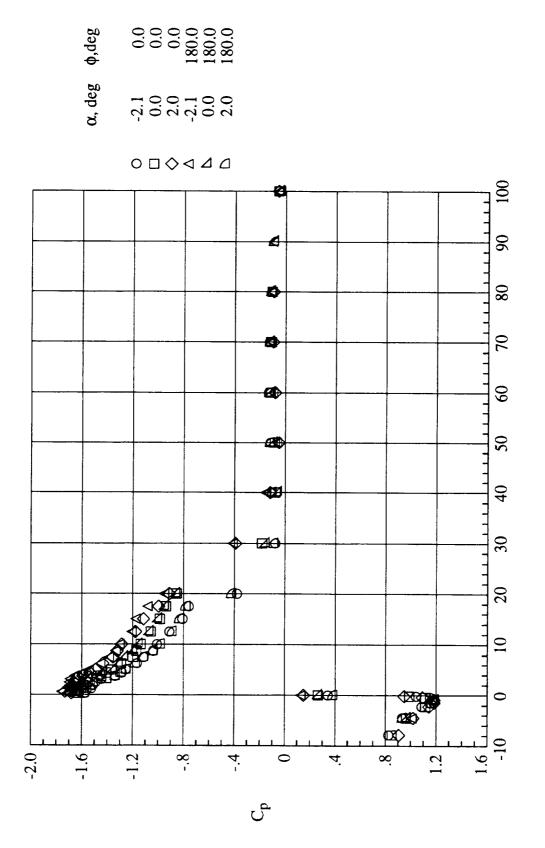


Figure 11.- Pressure coefficient variation with X/L along the  $\phi = 0^{\circ}$ , and 180° meridians for the NACA 1-85-100 inlet with a contraction ratio of 1.250 at several angles of attack.

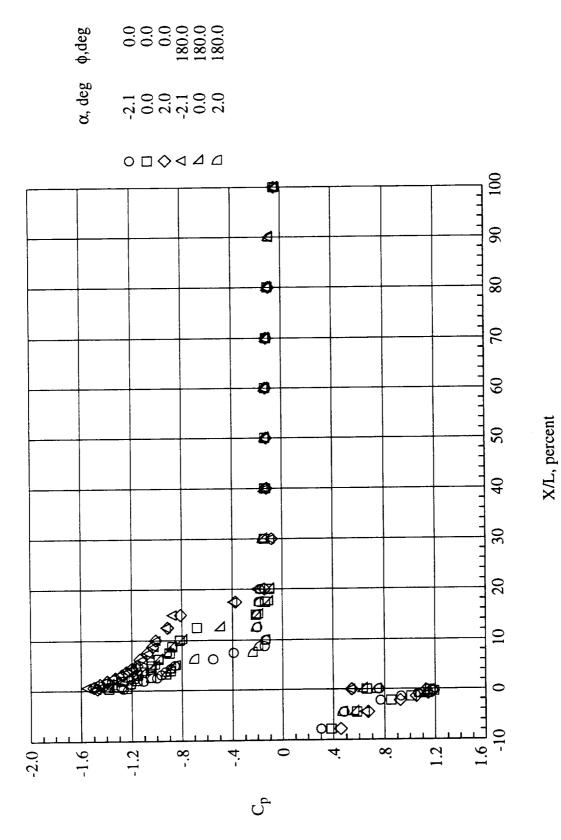
(a) M = 0.79 and mfr = 0.67.

X/L, percent

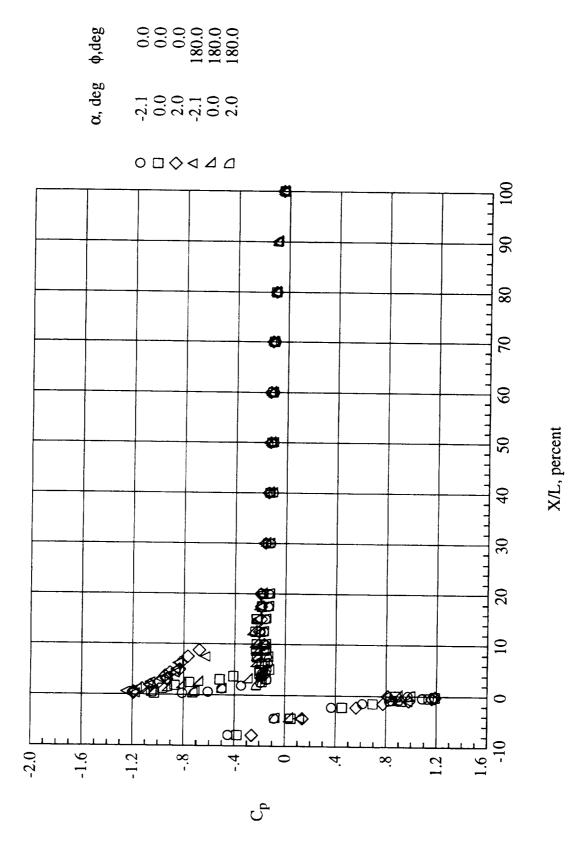


(b) M = 0.84 and mfr = 0.49.

140

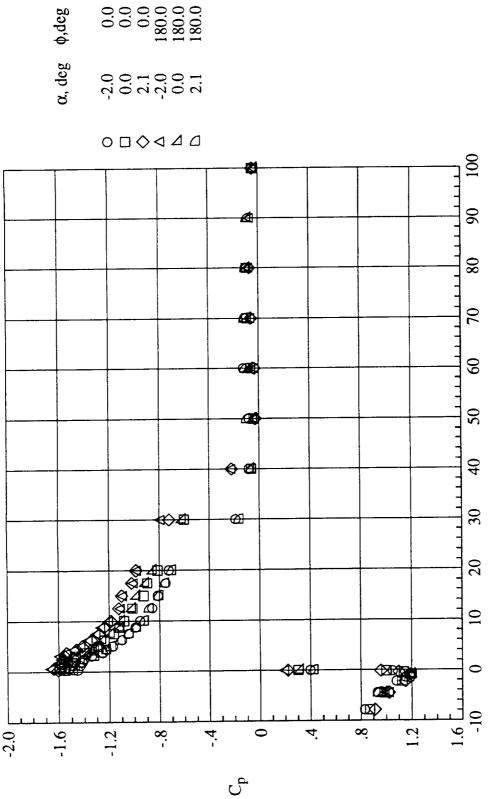


(c) M = 0.84 and mfr = 0.67. Figure 11.- Continued.

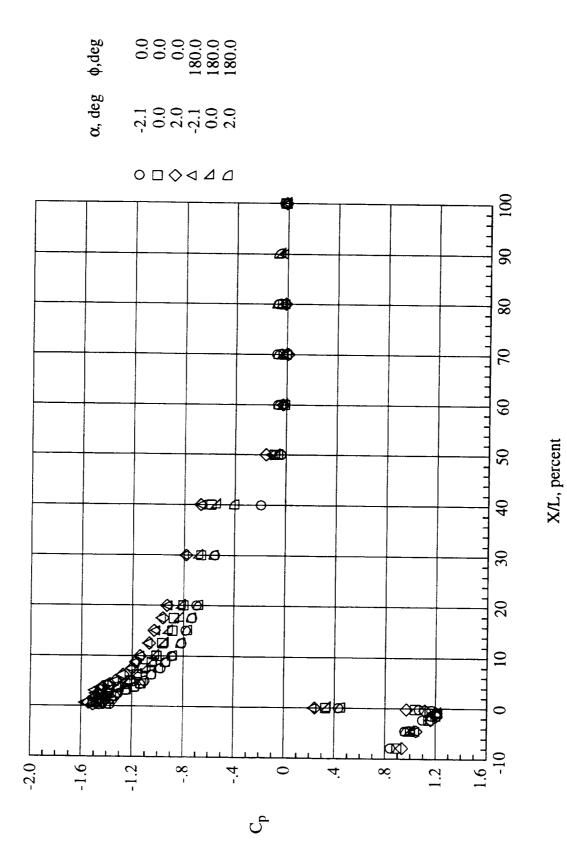


(d) M = 0.84 and mfr = 0.83.

142



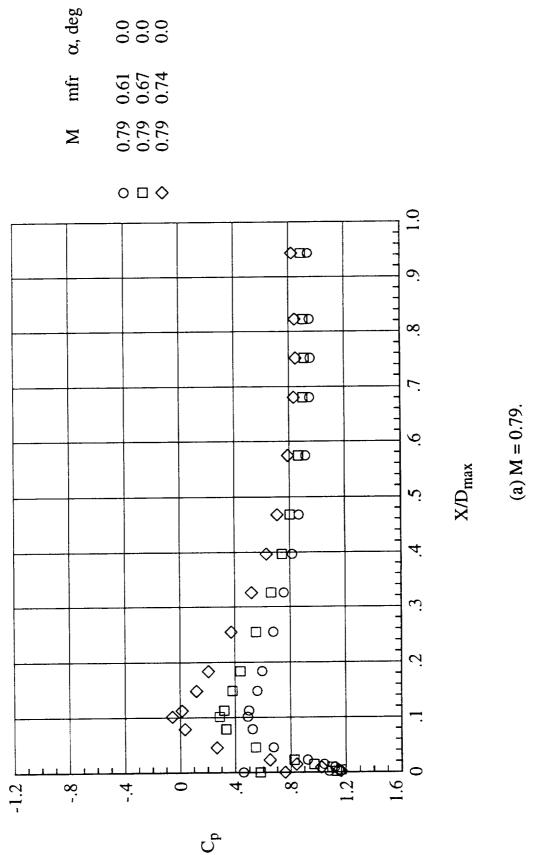
(e) M = 0.87 and mfr = 0.49. X/L, percent



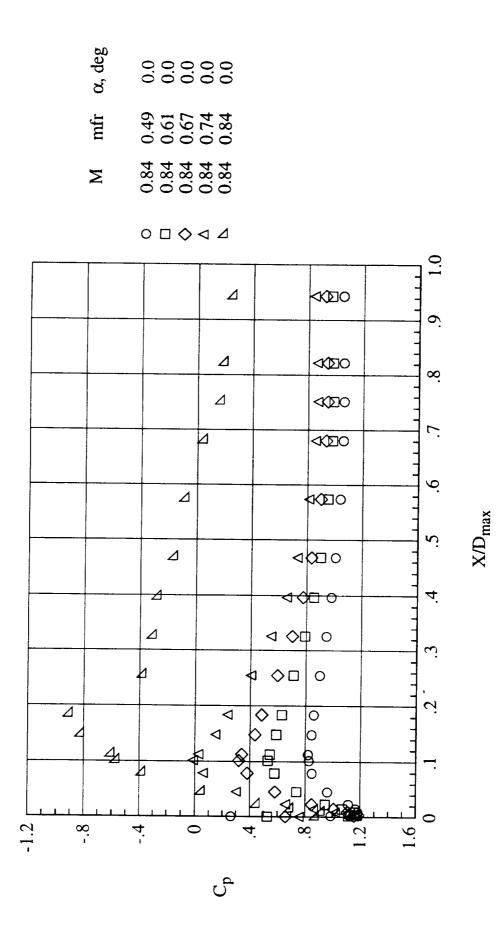
(f) M = 0.89 and mfr = 0.49.

Figure 11.- Concluded.

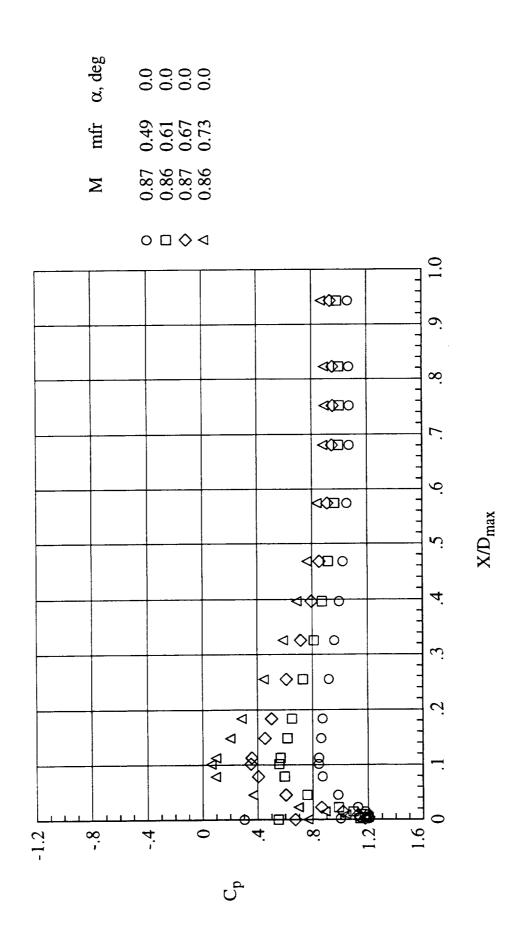
144



NACA 1-85-100 inlet with a contraction ratio of 1.25 for several mass-flow ratios at  $\alpha = 0^{\circ}$ . Figure 12.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the

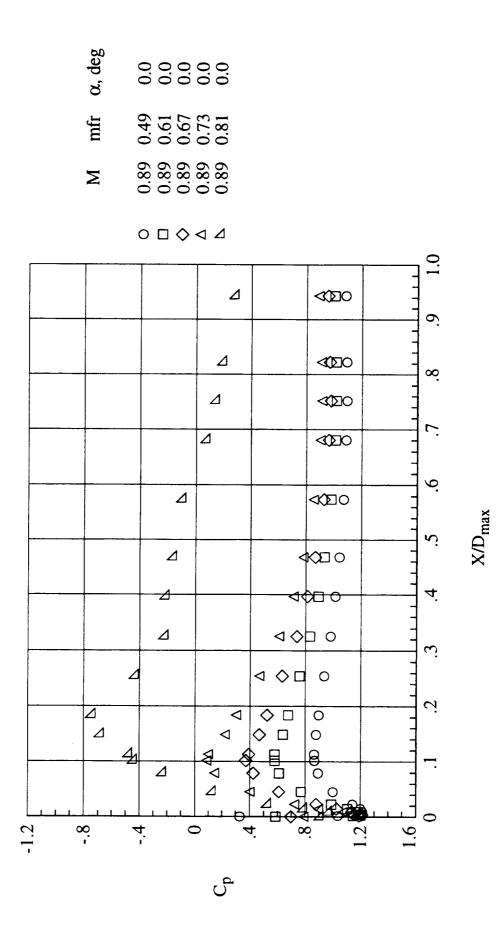


(b) M = 0.84. Figure 12.- Continued.



(c) M = 0.87. Figure 12.- Continued.

147



(d) M = 0.89. Figure 12.- Continued.

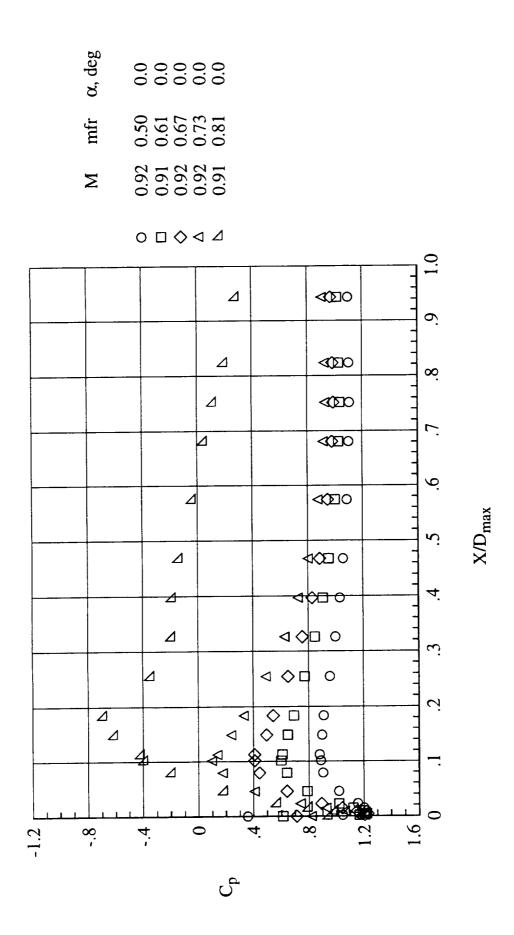
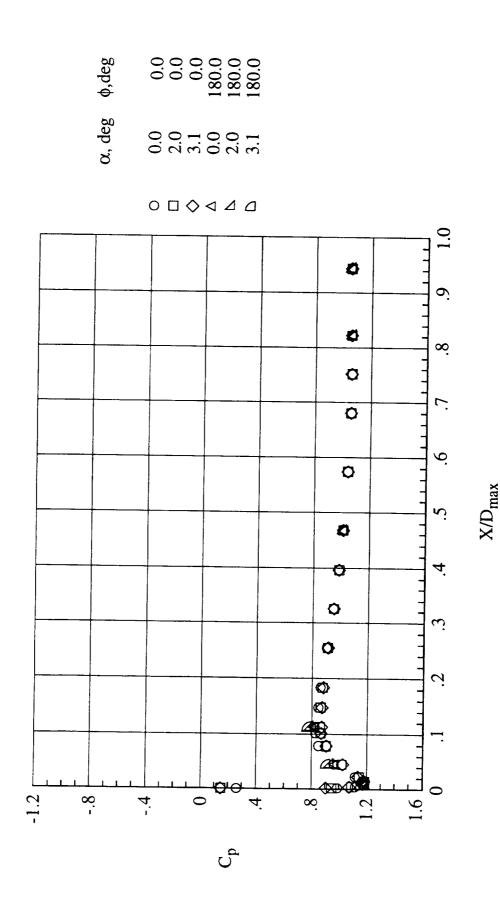


Figure 12.- Concluded.

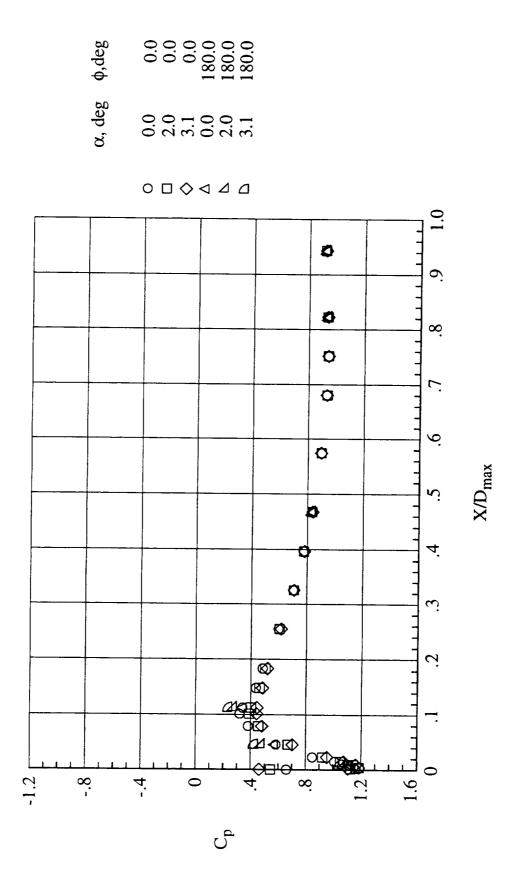
(e) M = 0.92.

149



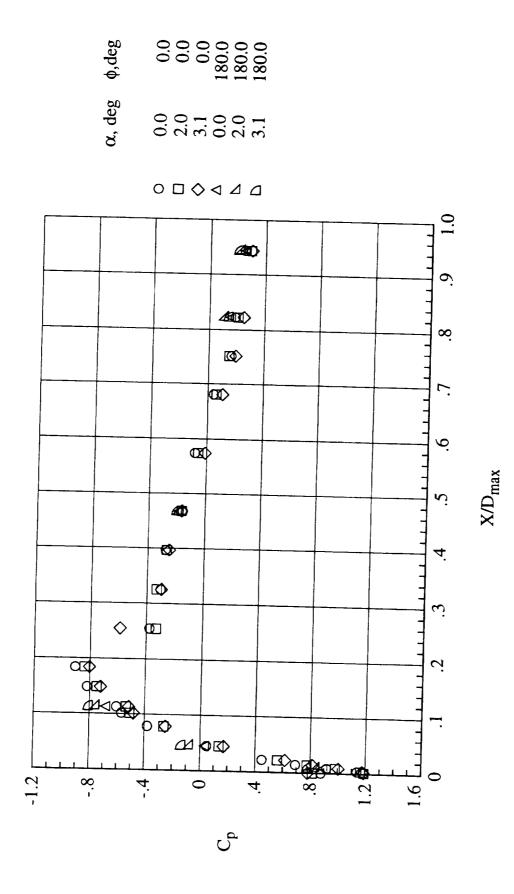
NACA 1-85-100 inlet with a contraction ratio of 1.25 for several mass-flow ratios and angles of attack. Figure 13.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the

(a) M = 0.84 and mfr = 0.49.



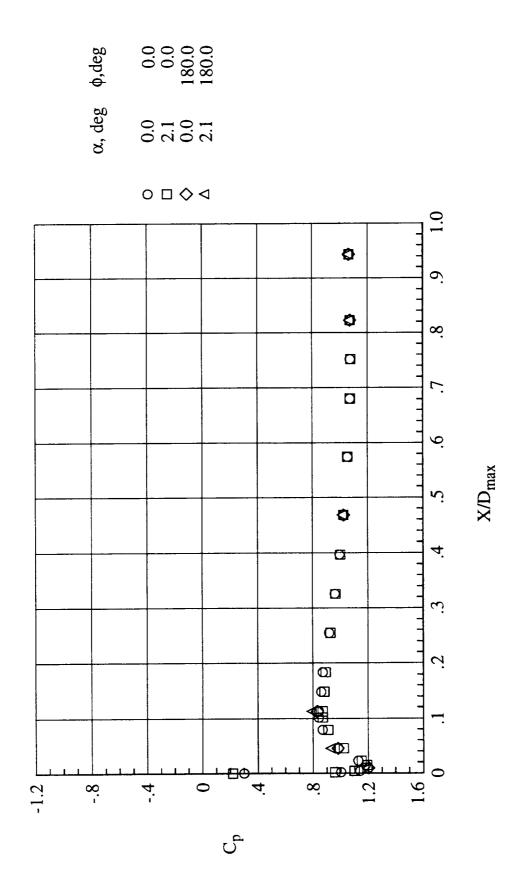
(b) M = 0.84 and mfr = 0.67.

151



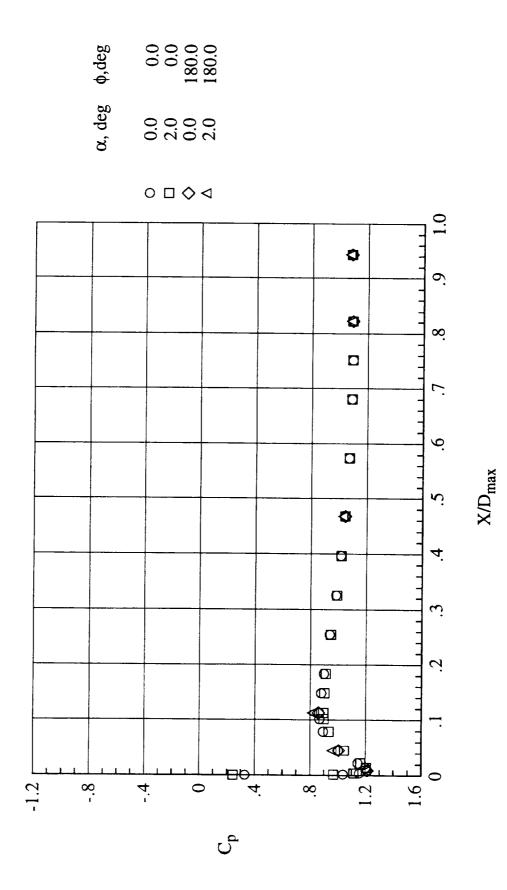
(c) M = 0.84 and mfr = 0.84.

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(d) M = 0.87 and mfr = 0.49.

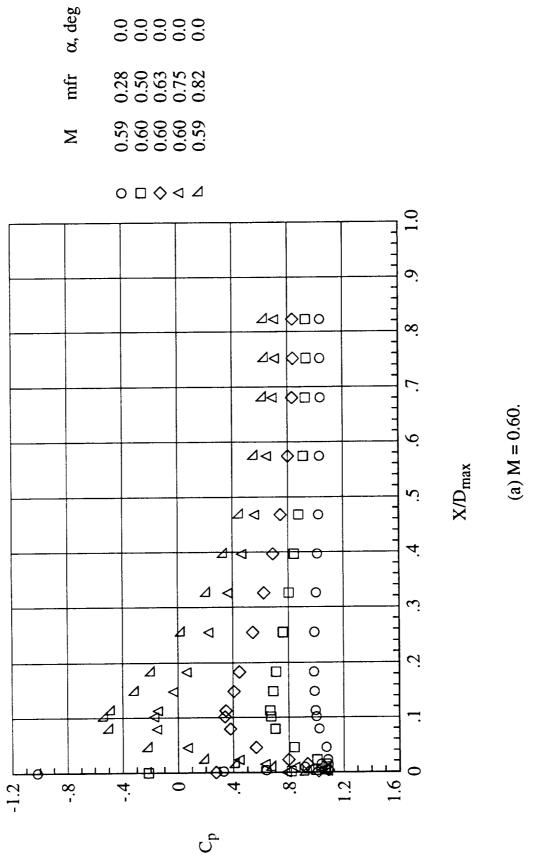
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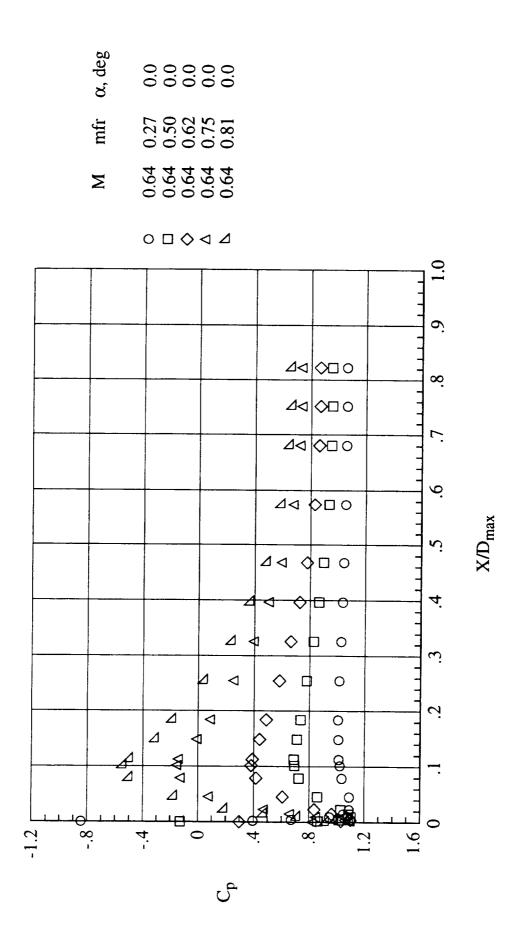
(e) M = 0.89 and mfr = 0.49.

Figure 13.- Concluded.

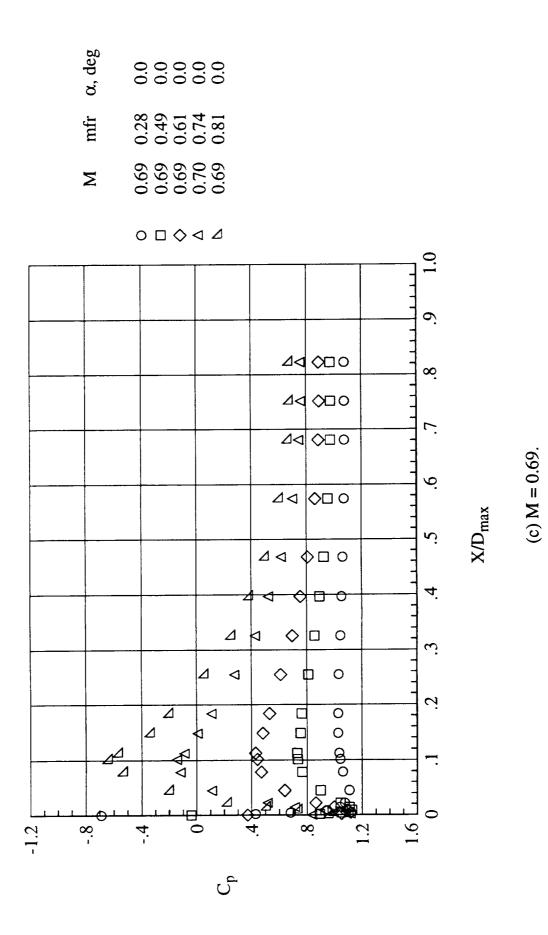
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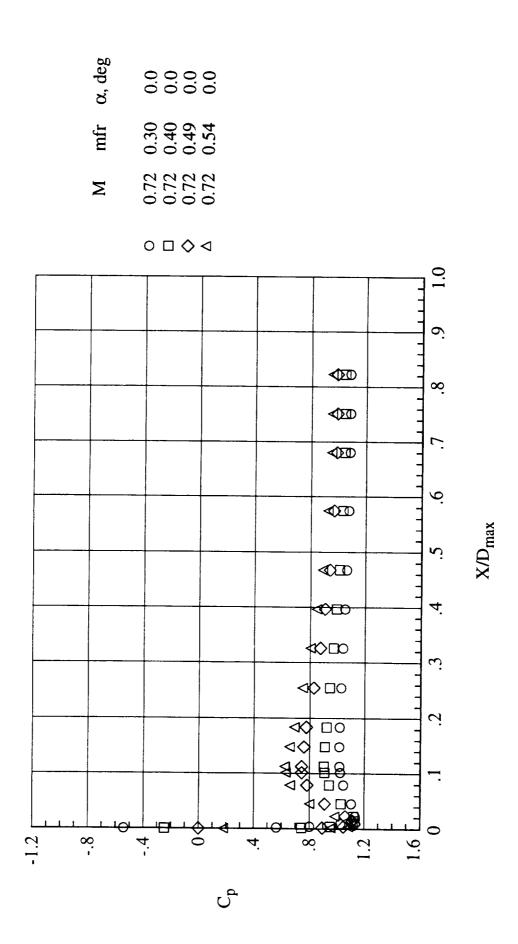
NACA 1-85-43.9 inlet with a contraction ratio of 1.25 for several mass-flow ratios at  $\alpha = 0^{\circ}$ . Figure 14.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the



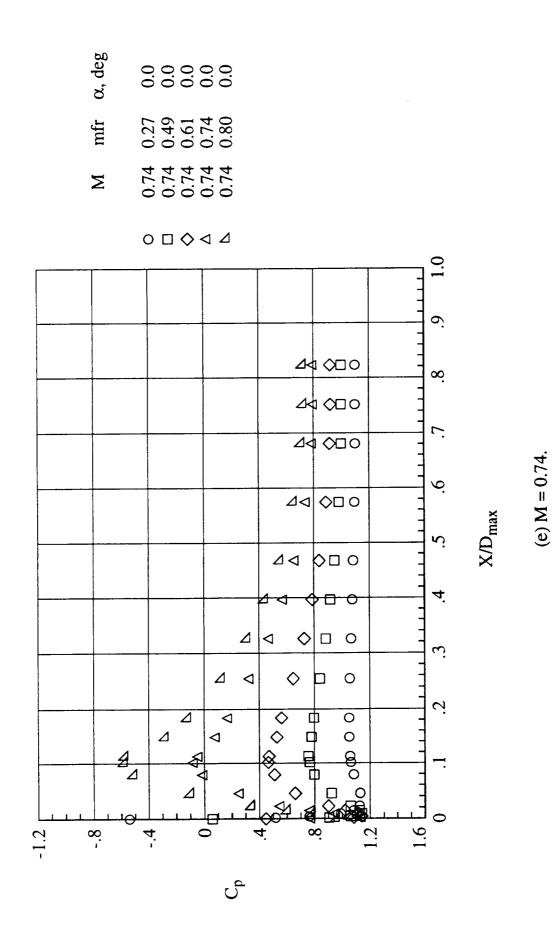
(b) M = 0.64.



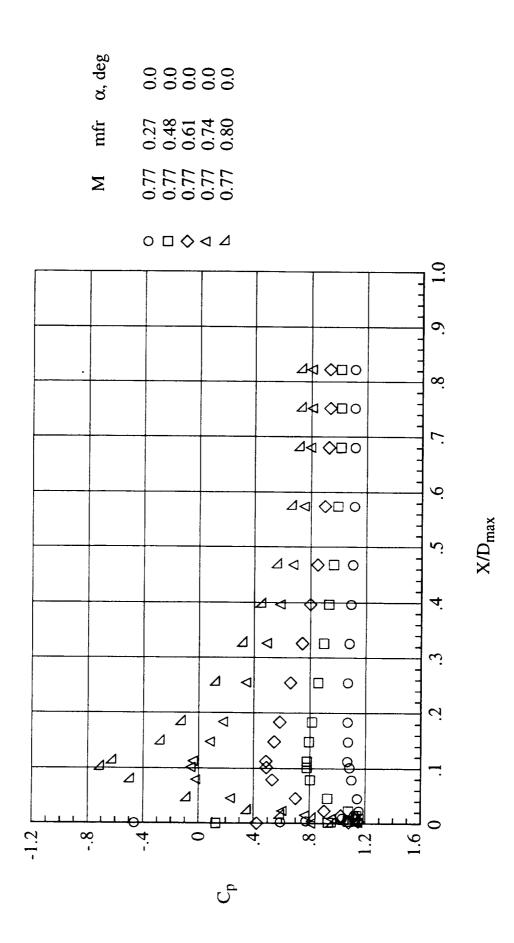
157



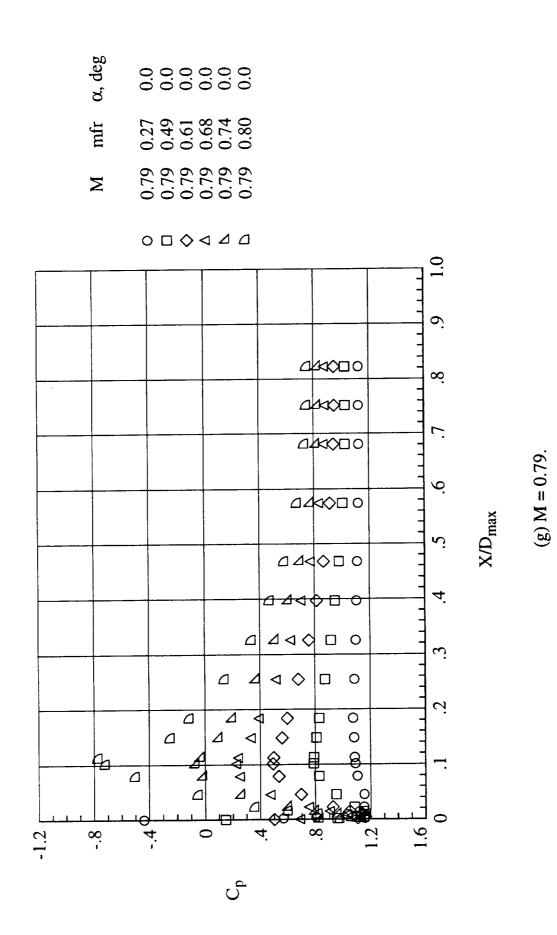
(d) M = 0.72.



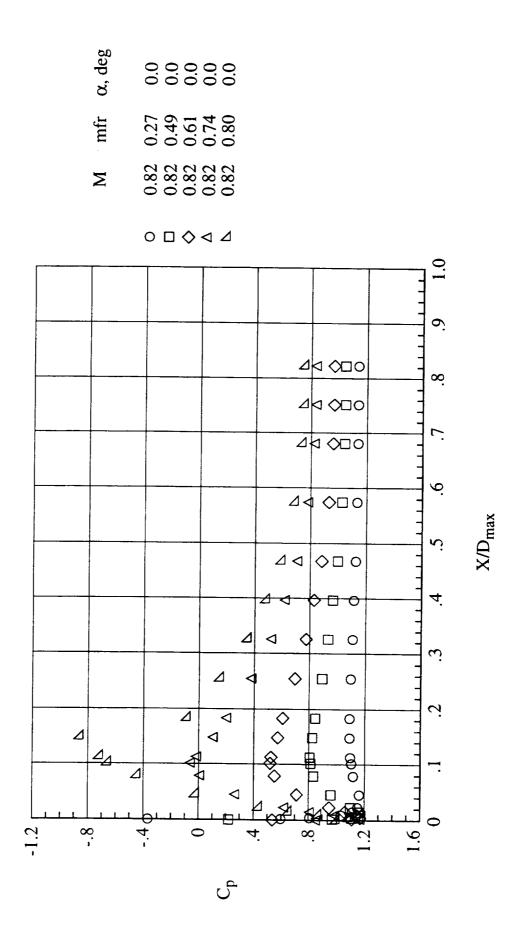
159



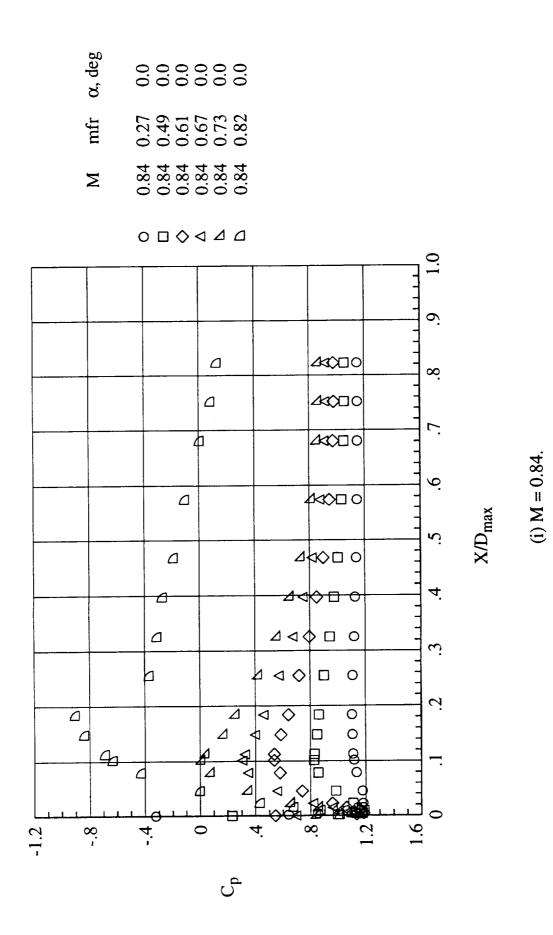
(f) M = 0.77.



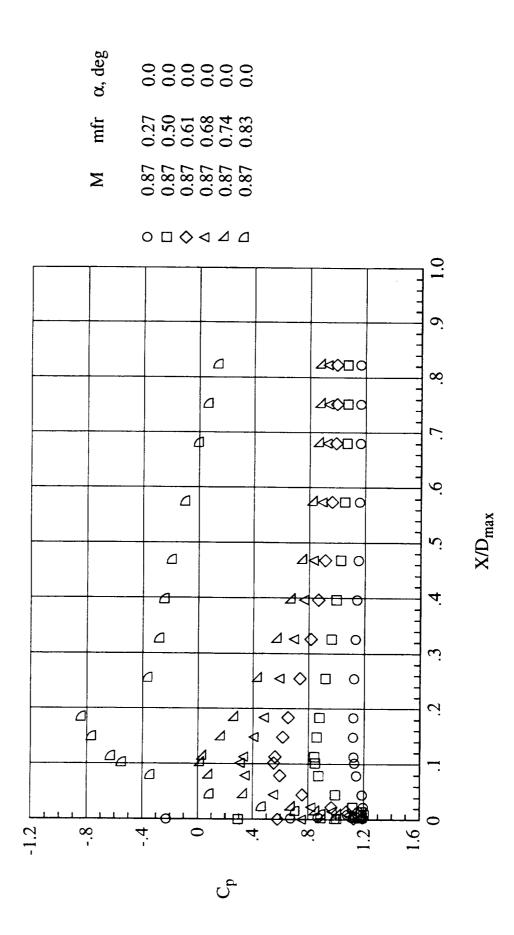
161



(h) M = 0.82.

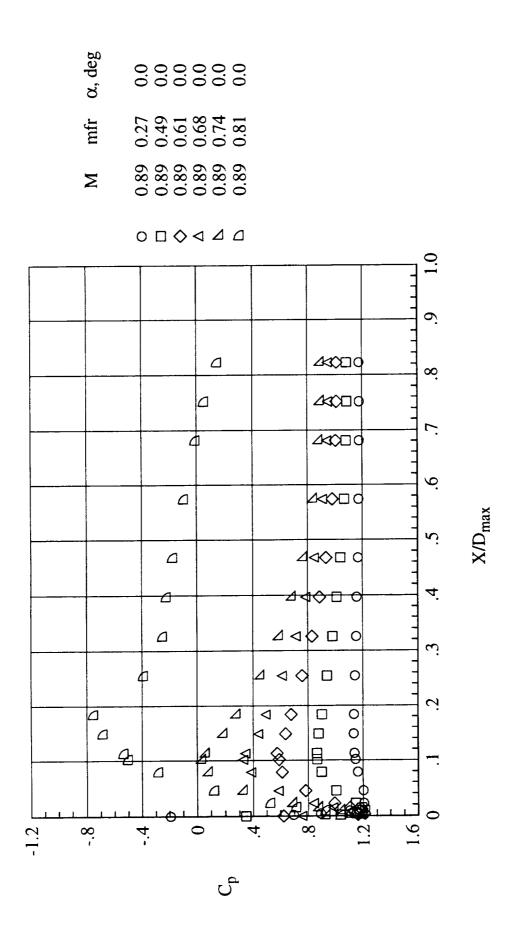


163



(j) M = 0.87.

164



(k) M = 0.89.

165

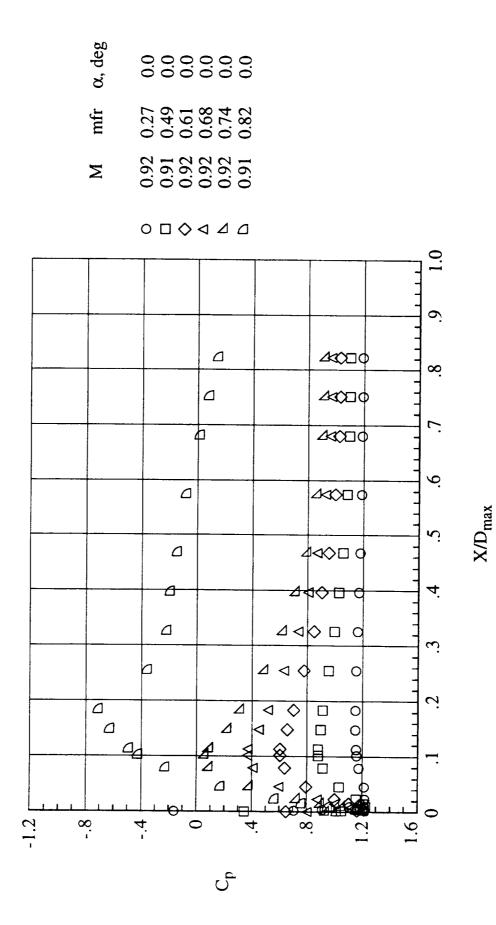
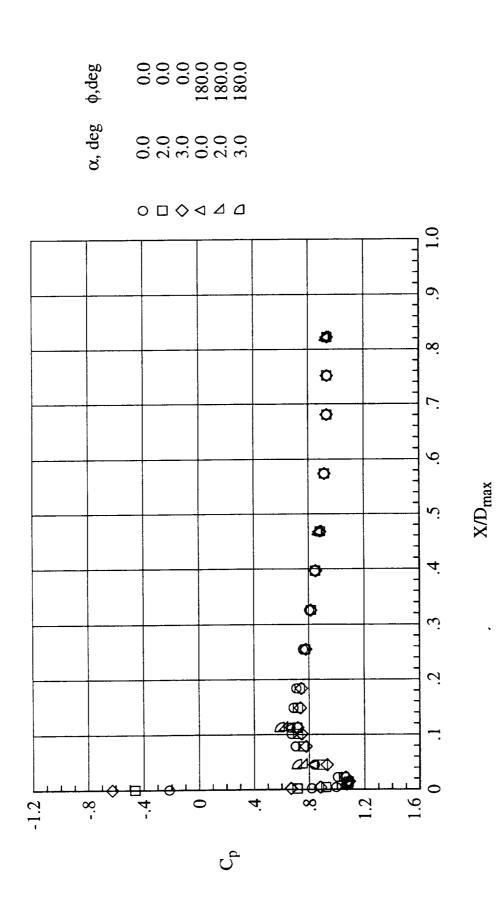


Figure 14.- Concluded.

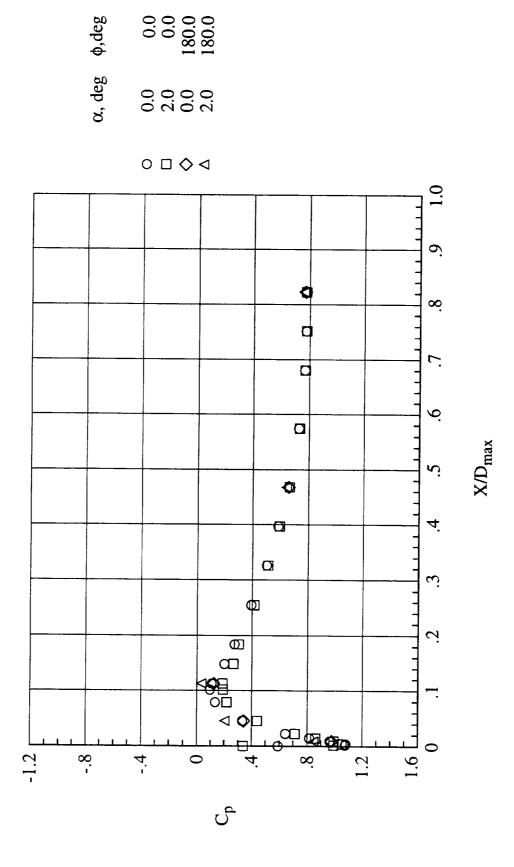
(1) M = 0.92.

166



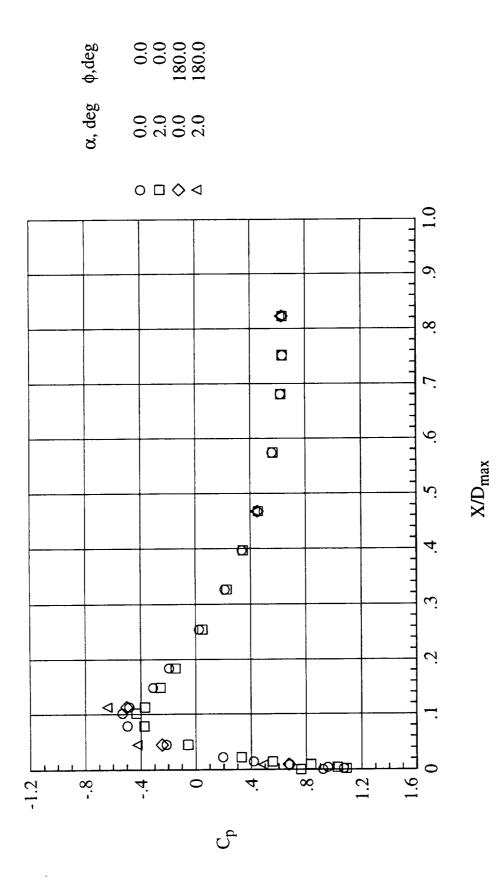
NACA 1-85-43.9 inlet with a contraction ratio of 1.25 for several mass-flow ratios and angles of attack. Figure 15.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the

(a) M = 0.60 and mfr = 0.50.

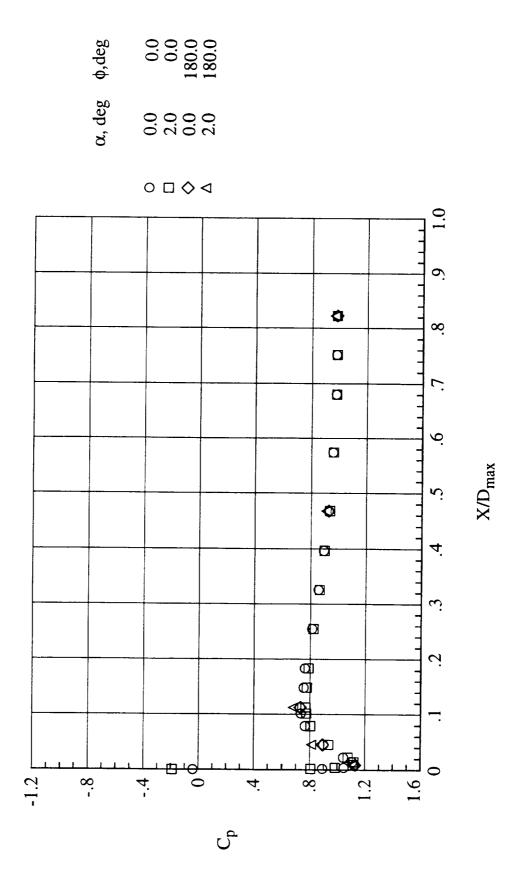


(b) M = 0.60 and mfr = 0.69.

168

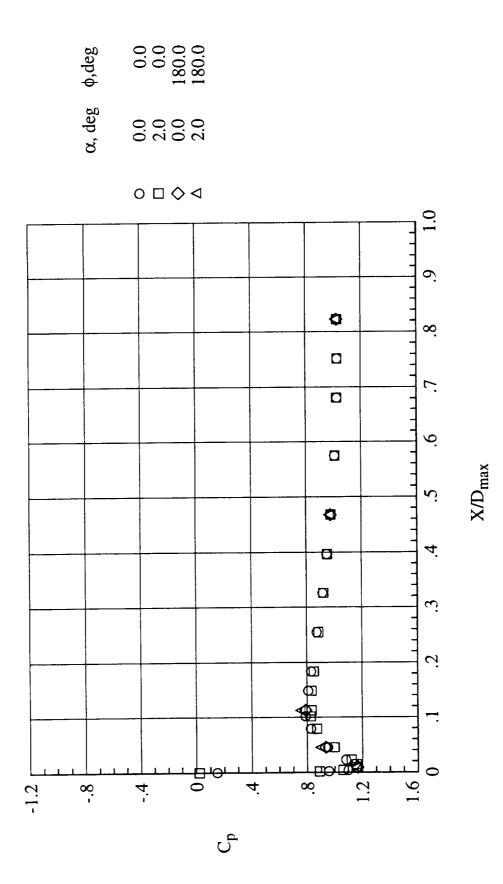


(c) M = 0.60 and mfr = 0.82.



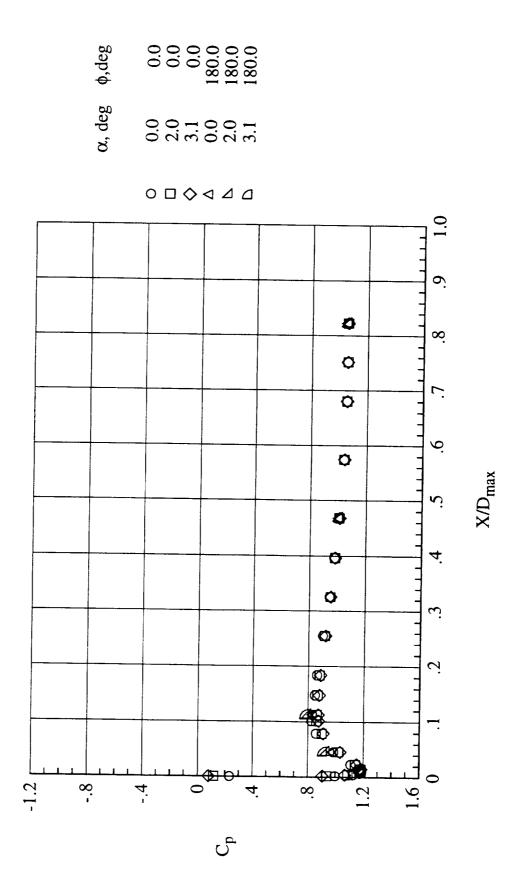
(d) M = 0.69 and mfr = 0.49.

170

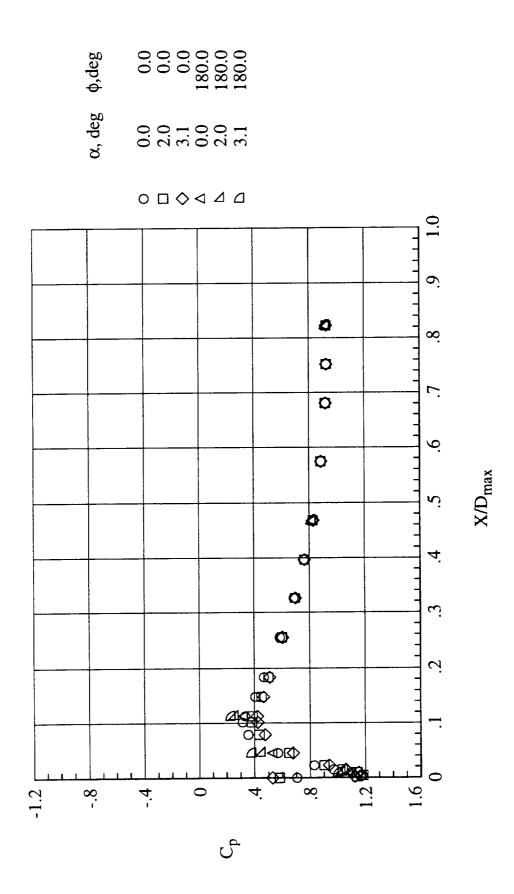


(e) M = 0.79 and mfr = 0.49.

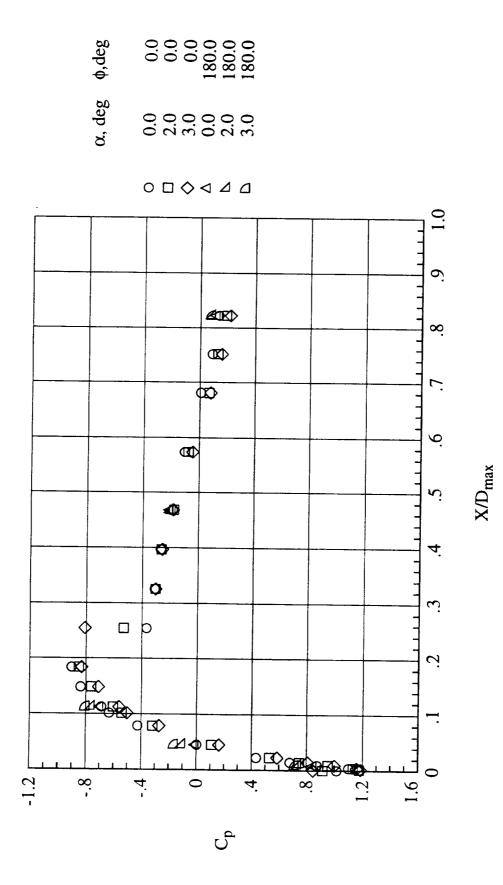
171



(f) M = 0.84 and mfr = 0.49.

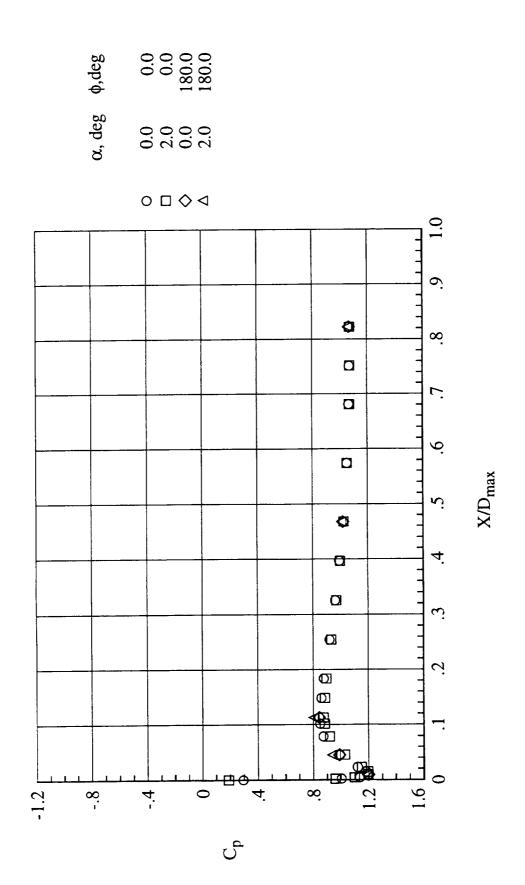


(g) M = 0.84 and mfr = 0.67.



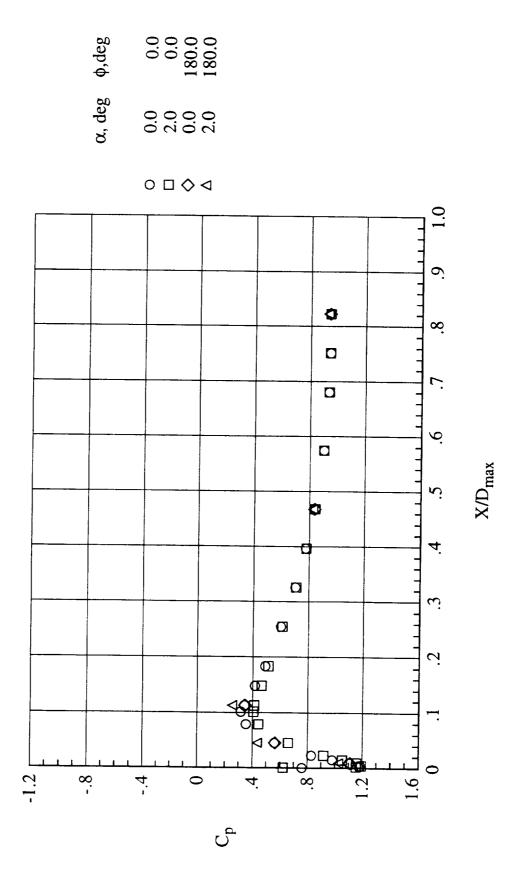
(h) M = 0.84 and mfr = 0.81.

174



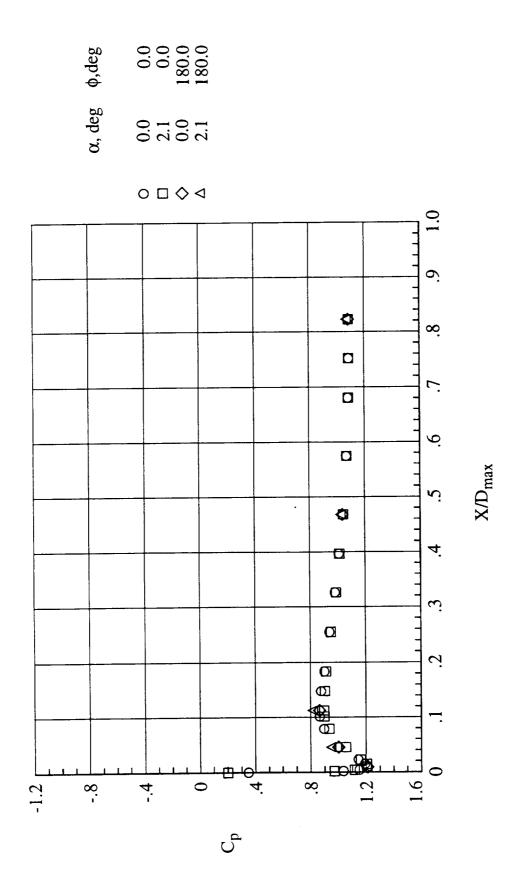
(i) M = 0.87 and mfr = 0.49.

175

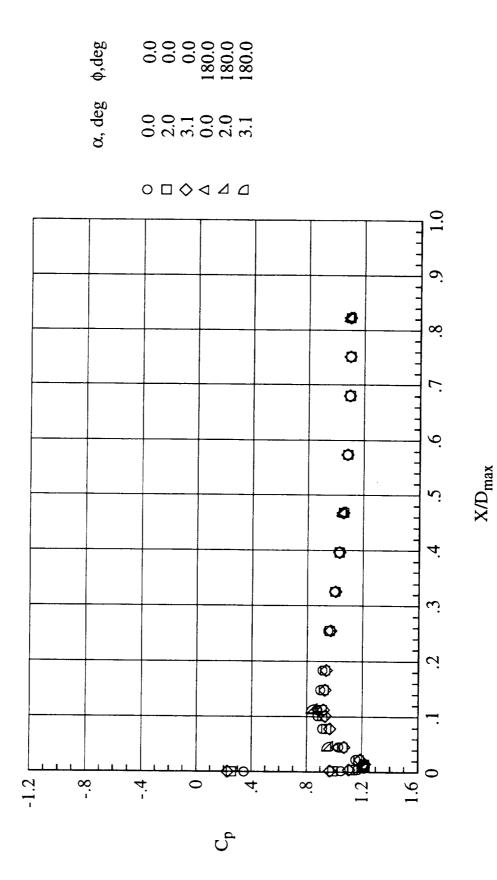


(j) M = 0.87 and mfr = 0.68.

176

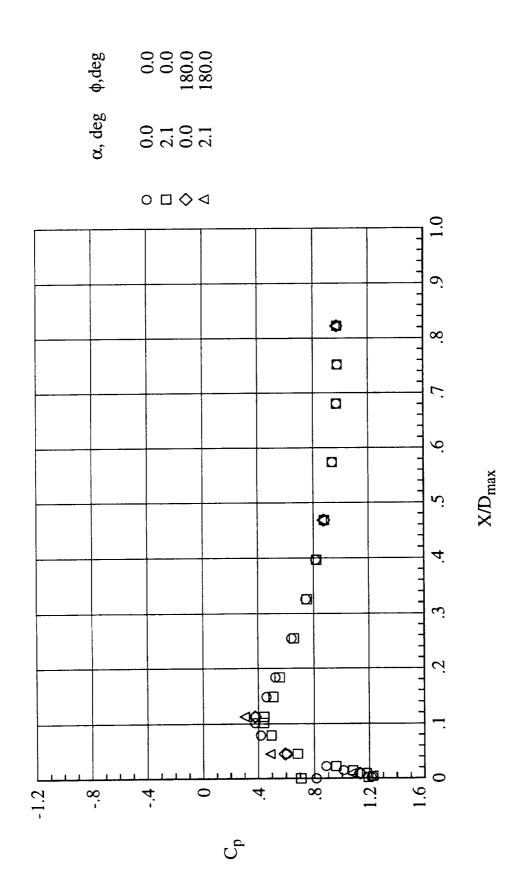


(k) M = 0.89 and mfr = 0.49.



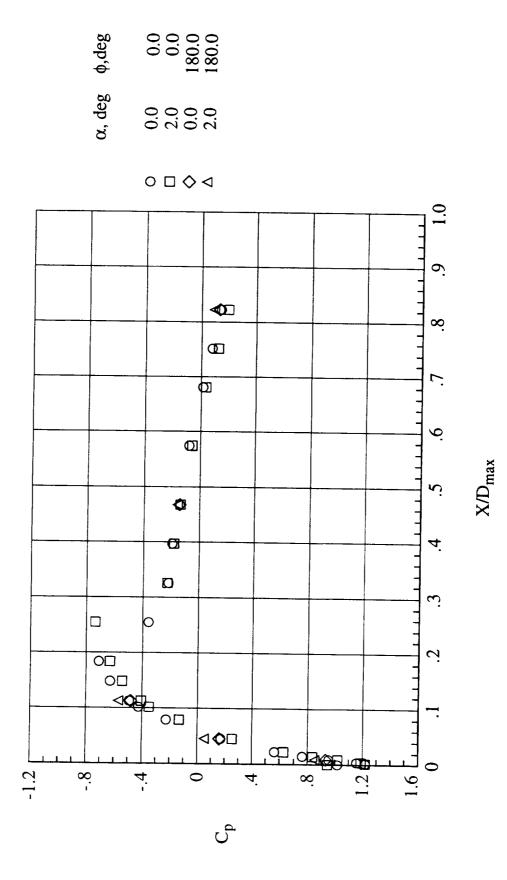
(1) M = 0.91 and mfr = 0.49.

178



(m) M = 0.92 and mfr = 0.68.

179



(n) M = 0.92 and mfr = 0.82.

Figure 15.- Concluded.

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## Form Approved REPORT DOCUMENTATION PAGE OMB No. 0704-0188 Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503. 1. AGENCY USE ONLY (Leave blank) 2. REPORT DATE 3. REPORT TYPE AND DATES COVERED November 1996 **Technical Memorandum** 4. TITLE AND SUBTITLE 5. FUNDING NUMBERS A Wind Tunnel Investigation of Three NACA 1-Series Inlets at Mach 538-05-13-01 Numbers Up to 0.92 6. AUTHOR(S) Richard J. Re and William K. Abeyounis 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) 8. PERFORMING ORGANIZATION REPORT NUMBER NASA Langley Research Center Hampton, VA 23681-0001 9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING / MONITORING AGENCY REPORT NUMBER National Aeronautics and Space Administration NASA TM-110300 Washington, DC 20546-0001 11. SUPPLEMENTARY NOTES 12a. DISTRIBUTION / AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 02 13. ABSTRACT (Maximum 200 words) Pressure distributions on three NACA 1-Series inlets have been obtained in the Langley 16-Foot Transonic Tunnel. The cowl diameter ratio (ratio of cowl highlight diameter to cowl maximum diameter) was 0.85 for all three inlets. The cowl length ratio (ratio of cowl length to cowl maximum diameter) was 1.0 for two of the inlets (NACA 1-85-100) and 0.439 for the other (NACA 1-85-43.9) inlet. One of the inlets with a cowl length ratio of 1.0 had an internal contraction ratio (ratio highlight area to throat area) of 1.009 and the other two inlets had a contraction ratio of 1.250. All three inlets had longitudinal rows of static pressure orifices on the top and bottom external cowl surfaces. The two inlets with a contraction ratio of 1.250 had a longitudinal row of static pressure orifices on the diffuser surface. 14. SUBJECT TERMS 15. NUMBER OF PAGES NACA 1-series inlets 181 inlets 16. PRICE CODE Axisymmetric inlets A09

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17. SECURITY CLASSIFICATION

18. SECURITY CLASSIFICATION

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20. LIMITATION OF ABSTRACT