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# Derivation of Midinfrared (5–25 $\mu$ m) Optical Constants of Some Silicates and Palagonite

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The midinfrared 2000-400 cm<sup>-1</sup> (5-25  $\mu$ m) optical constants (real (n) and imaginary (k) indices of refraction) are presented for: (1) pyrophyllite; (2) kaolinite; (3) serpentine; (4) montmorillonite; (5) saponite; (6) palagonite; and (7) orthopyroxene. Comparison of the values derived here with those previously presented for serpentine, montmorillonite, and palagonite is generally quite good and discrepancies between values are probably due to either chemical differences between the actual samples or different techniques used to derive the values. For montmorillonite, saponite, and palagonite we were able to derive optical constants in the region of the  $H_2O$ -bending fundamental near 6  $\mu$ m. We find that if a pellet of pure material can be produced with a mirror-like surface then the optical constants of clays and other noncohesive materials can be readily derived. © 1991 Academic Press, Inc.

#### 1. INTRODUCTION

Recent reports concerning the midinfrared reflectance properties of silicates (Salisbury et al. 1987, Salisbury and Walter 1989, Walter and Salisbury 1989) coupled with recent observations of the Earth (e.g., Bartholomew et al. 1989) and other planets (Potter and Morgan 1981, Tyler et al. 1988, Roush et al. 1989, Pollack et al. 1990, Lucey et al. 1989) in the midinfrared and the planned Thermal Emission Spectrometer scheduled as an instrument to be included on the Mars observer all illustrate the increasing interest in the optical properties of materials in the midinfrared and their direct application to remote sensing obser-

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vations of other planetary surfaces. As the laboratory and observational data increase they will ultimately be modeled to aid in the understanding of the composition and mineralogy of the surface and atmospheric constituents on these bodies. In order to facilitate such quantitative analyses, knowledge regarding the optical constants (real (n) and imaginary (k) indices of refraction) of a wide variety of pertinent materials is required. Examples of the application of such quantitative analyses to the interpretation of Martian surface and atmospheric constituents, based on the optical constants of minerals, are presented in Aronson and Emslie (1975), Toon et al. (1977), and Pollack et al. (1990).

Optical constants can be readily derived from polished surfaces of cohesive materials using standard geological thin sectioning and polishing techniques. The midinfrared optical constants of only a few specific silicate minerals are available in the literature [e.g., quartz, Spitzer and Kleinman (1961); muscovite and garnet, Aronson and Strong (1975); serpentine and chlorite, Mooney and Knacke (1985); and montmorillonite, Toon et al. (1977)]. Additionally, optical constants have been determined for a number of specific rock types including silicates (e.g., Pollack et al. 1973, Aronson and Strong 1975) and limestone (Querry et al. 1978). Recently optical constants for palagonite, typically a poorly characterized mineralogical assemblage resulting from the alteration of basaltic glass, were presented for a limited wavelength range (Crisp and Bartholomew 1989). The optical constants of many nonsilicate materials are available [e.g., terrestrial atmospheric aerosols, Toon et al. (1976); graphite, Draine (1985),

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Twitty and Weinman (1971); organic materials, Khare *et al.* (1984), Twitty and Weinman (1971); low temperature condensates, Irvine and Pollack (1968), Roux *et al.* (1979), Sill *et al.* (1980), Warren (1984, 1986), Masterson and Khanna (1990)].

Due to their physical particle size clays and other materials, such as palagonite, can not be prepared using standard geological preparation techniques. Yet in some cases, such as for Mars, these are the materials of perhaps the greatest interest. Here we present a method for the derivation of the optical constants for these less cohesive materials.

#### 2. DERIVATION OF MATHEMATICAL RELATIONSHIPS

In general, we wish to derive the optical constants, i.e., the real, n, and imaginary, k, indices of refraction, of a material as a function of wavelength from a measurement obtained in the laboratory. One technique commonly employed is dispersion analysis (Pollack *et al.* 1973, Aronson and Strong 1975, Toon *et al.* 1976, Querry *et al.* 1978, Mooney and Knacke 1985) which describes n and k as the contributions due to a sum of classical oscillators and relates them via Fresnel's equations for nonnormal incidence, to the measured near-normal reflectivity. Nonlinear least squares techniques can then be used to minimize the differences between the observed and the calculated reflectivities.

# 2.1. Dispersion Analysis

In dispersion analysis n and k are described in terms the summation of the contributions due to a set of classical oscillators (Spitzer and Kleinman 1961, Pollack *et al.* 1973, Aronson and Strong 1975, Toon *et al.* 1976, Querry *et al.* 1978, Mooney and Knacke 1985) and are expressed as:

$$n^{2} - k^{2} = \varepsilon_{\infty} + \sum_{i=1}^{n} \frac{4\pi\rho_{i}\lambda^{2}(\lambda^{2} - \lambda_{i}^{2})}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2}\lambda^{2}}$$
(1)

and

$$nk = \sum_{i=1}^{n} \frac{2\pi\rho_i \lambda^3 \Gamma_i}{(\lambda_i^2 - \lambda^2)^2 + \Gamma_i^2 \lambda^2},$$
 (2)

where each oscillator is described by its characteristic strength  $4\pi\rho_i$ , width  $\Gamma_i$ , and wavelength  $\lambda_i$ . The high frequency dielectric constant is  $\varepsilon_{\infty}$ . Let the right hand side of Eqs. (1) and (2) be represented by A and B, respectively, so  $n^2 - k^2 = A$  and  $k^2 = B^2/n^2$ . Substituting for  $k^2$  yields  $n^2 - B^2/n^2 = A$ . Finding the lowest common de-

nominator, rearranging, and combining all terms on the left gives  $n^4 - An^2 - B^2 = 0$ . Let  $z = n^2$  and this becomes  $z^2 - Az - B^2 = 0$ , which is quadratic in z. Applying the quadratic formula gives  $z = (A \pm \sqrt{A^2 + 4B^2})/2$  or simplifying and resubstituting for z gives  $n^2 = (A \pm \sqrt{A^2 + 4B^2})/2$ . Hence,  $n = \sqrt{(A \pm \sqrt{A^2 + 4B^2})/2}$ . Which results in

$$k = \frac{B}{n} = \frac{B}{\sqrt{\frac{A + \sqrt{A^2 + 4B^2}}{2}}}.$$
 (3)

Replacing A and B yields

$$n = \frac{1}{\sqrt{2}} \left\{ \varepsilon_{\infty} + \sum_{i=1}^{n} \frac{4\pi\rho_{i}\lambda^{2}(\lambda^{2} - \lambda_{i}^{2})}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2}\lambda^{2}} \\ \pm \left[ \left( \varepsilon_{\infty} + \sum_{i=1}^{n} \frac{4\pi\rho_{i}\lambda^{2}(\lambda^{2} - \lambda_{i}^{2})}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2}\lambda^{2}} \right)^{2} + \left( 4 \sum_{i=1}^{n} \frac{2\pi\rho_{i}\lambda^{3}\Gamma_{i}}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2}\lambda^{2}} \right)^{2} \right]^{1/2} \right\}^{1/2}$$
(4)

and

$$k = \frac{\sum_{i=1}^{n} \frac{4\pi \rho_{i} \lambda^{3} \Gamma_{i}}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2} \lambda^{2}}}{2\sqrt{2}} \left\{ \varepsilon_{\infty} + \sum_{i=1}^{n} \frac{4\pi \rho_{i} \lambda^{2} (\lambda^{2} - \lambda_{i}^{2})}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2} \lambda^{2}} \\ \pm \left[ \left( \varepsilon_{\infty} + \sum_{i=1}^{n} \frac{4\pi \rho_{i} \lambda^{2} (\lambda^{2} - \lambda_{i}^{2})}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2} \lambda^{2}} \right)^{2} + \left( 4 \sum_{i=1}^{n} \frac{2\pi \rho_{i} \lambda^{3} \Gamma_{i}}{(\lambda^{2} - \lambda_{i}^{2})^{2} + \Gamma_{i}^{2} \lambda^{2}} \right)^{2} \right]^{1/2} \right\}^{-1/2}.$$

Thus, *n* and *k* are given in terms of the oscillator parameters  $\rho_i$ ,  $\Gamma_i$ , and  $\lambda_i$ .

#### 2.2. Fresnel Reflectance

Both *n* and *k* can be related to the measured reflectivity at normal incidence  $(R_n)$  via Fresnel's equation

$$R_{\rm n} = \frac{(n-1)^2 + k^2}{(n+1)^2 + k^2}.$$
 (6)

For nonnormal incidence, the intensity and polarization of the light reflected and refracted by the surface can be computed from the Fresnel reflection coefficients,  $|r_{\perp}|^2$ and  $|r_{\parallel}|^2$ , which represent the reflected intensity of the light resolved perpendicular and parallel to the plane of the incident radiation, respectively. The total reflected intensity which can be calculated  $(R_{calc})$  is defined by

$$R_{\text{calc}} = \frac{1}{2} \{ |r_{\perp}|^2 + |r_{\parallel}|^2 \}.$$
 (7)

following Hansen and Travis (1974) and defining i to be the angle of the incident light relative to the surface normal, yields

$$|r_{\perp}|^{2} = \frac{(\sin(90 - i) - u)^{2} + v^{2}}{(\sin(90 - i) + u)^{2} + v^{2}}$$
(8)

and

 $|r_{\|}|^{2}$ 

$$= \frac{[(n^2 - k^2)\sin(90 - i) - u]^2 + (2nk\sin(90 - i) - v)^2}{[(n^2 - k^2)\sin(90 - i) + u]^2 + (2nk\sin(90 - i) + v)^2}$$
(9)

where

$$u = \left\{ \frac{n^2 - k^2 - \cos^2(90 - i)}{+ [(n^2 - k^2 - \cos^2(90 - i))^2 + 4n^2k^2]^{1/2}}{2} \right\}^{1/2}$$
(10)

and

$$v = \left\{ \frac{-(n^2 - k^2 - \cos^2(90 - i))}{+ [(n^2 - k^2 - \cos^2(90 - i))^2 + 4n^2k^2]^{1/2}}{2} \right\}^{1/2} .$$
 (11)

Hence if the reflectance of a sample can be measured in the laboratory ( $R_{meas}$ ), nonlinear least squares techniques (Bevington 1969) can be used to derive the optimal values of *n* and *k* by minimizing the differences between  $R_{meas}$ and  $R_{calc}$ . In our analyses we require that: (1)  $\rho_i$ ,  $\Gamma_i$ ,  $\lambda_i$  all to have values greater than zero; (2)  $\lambda_i$  falls within the range of our observations, i.e., 5  $\mu m \le \lambda_i \le 25 \mu m$ ; and (3) the differences between observed and calculated reflectivities are minimized, i.e., that  $\chi^2$  is a minimum.

In our fitting procedure we first chose the number of oscillators based upon the number of obvious peaks in the reflectivity spectrum.  $\varepsilon_{\infty}$  is estimated from values of the real index of refraction,  $\varepsilon_{\infty} = n_{vis}^2$ , measured in the visible for the appropriate minerals (Deer *et al.* 1966). In order to assess the effect of both  $n_{vis}$  and the total number of oscillators on our analysis we vary these parameters and use  $\chi^2$  to evaluate the best fit.

# 2.3. Estimate of Associated Errors

Toon *et al.* (1976) provide an excellent discussion on the relative errors associated with derivation of n and k

via dispersion analysis. They conclude that  $\Delta n/n$  is a few percent due to errors in the measured reflectivity. In respect to k, if 0.01 < k < 1, i.e., in the strong bands, then comparison of values derived from dispersion analysis and Kramers-Kronig analysis agree to within a few percent (Toon *et al.* 1976).

At frequencies higher than 2000 cm<sup>-1</sup> (wavelengths  $< 5 \,\mu$ m) the assumption that Fresnel reflectivity is the dominant source of reflected light becomes increasingly invalid due to the decrease in the imaginary index of refraction which results in an increasing contribution of multiply scattered light. As a result, optical constants were derived for only the 2000-400 cm<sup>-1</sup> (5-25  $\mu$ m) region by our analyses here.

In order to provide an estimate of the errors from our analysis procedure optical constants from several resultant fits, which contain the same number of oscillators but various  $n_{vis}$ , were averaged together. These errors can be associated with the derived optical constants, as well as, the oscillator parameters and are included in our following presentation.

#### 3. EXPERIMENTAL

#### 3.1. Mineral Samples

This study was initially conceived in order to aid in the interpretation of Martian surface and atmospheric aerosol mineralogy. The interpretation of remotely sensed data often requires a choice from among a number of fundamental variables. From the perspective of interpreting Mars surface mineralogy we believe that a wider range of surface evolution/modification processes would be implicated by structural rather than compositional variability. Hence we chose to pursue this as the main variable in our study.

The minerals included are biased toward samples which represent hydrated and hydroxylated silicates. These include: (1) the Al and Mg end members of the 1:1 layer lattice silicates, kaolinite and serpentine, respectively; (2) an Al-bearing 2:1 layer lattice silicate, pyrophyllite; (3) the Mg and Al smectite clays saponite and montmorillonite, respectively; and (4) a palagonite, typically a poorly characterized alteration product of basaltic glass. The kaolinite and montmorillonite clay samples were obtained from the Clay Mineral Society (CMS) and independent chemical analyses and structural characterization are presented by Van Olphen and Fripiat (1979). The saponite, also a CMS sample, has been chemically and structurally characterized by Post (1984). The serpentine was kindly provided by Dr. James Gooding and is a serpentinite from San Luis Obispo, California. Based on its X-ray diffraction (XRD) pattern and differential thermal analysis this sample appears to be  $\geq 95\%$  by weight serpentine (J.

Sample	SiO2	$Al_2O_3$	TiO2	Fe2O3	FeO	MnO	MgO	CaO	Na <sub>2</sub> O	K <sub>2</sub> O	$P_{2}O_{5}$	LOI®	Total	Pressure
Kaolinite	44.1	39.3	1.66	0.17	≤0.01	0.02	0.11	0.07	0.07	0.10	0.06	14.8	100.6	3.72
Serpentine														
This Study	38.2	1.11	0.04	4.68	3.7	0.12	37.2	0.64	0.04	0.01	0.02	14.5	100.6	6.89
Mooney & Knacke	40.2	1.31	0.06	c	3.26	0.03	40.1	0.02	<b>≤0</b> .02	≤0.02	n.a.	15.1	100.0	n.a.
Pyrophyllite	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	n.a.	6.89
Montmorillonite														
This Study	55.0	17.2	0.15	3.62	≤0.01	0.02	2.42	1.21	1.41	0.54	0.05	16.9	98.6	6.89
Toon et al.														
219B	63.2	20.6	0.21	3.98	d	0.00	2.14	1.01	2.23	0.26	0.01	5.67	99.31	n.a.
222B	53.1	20.2	0.91	9.90	d	0.21	1.21	0.84	0.18	1.16	0.13	11.9	99.8	n.a.
Saponite <sup>e</sup>	49.6	4.42	0.77	0.80	< 0.01	0.04	22.9	4.18	1.82	1.21	0.11	13.8	99.8	≈0.5
Palagonite	30.7	23.0	4.11	14.6	1.0	0.21	0.87	2.05	0.61	0.47	1.13	21.4	100.4	6.89
Orthopyroxene <sup>f</sup>	55.3	0.12	0.05	c	9.38	0.15	32.80	0.45	0.00	0.02	0.01	<b>2</b> .00	100.3	6.89

TABLE I Chemical Analyses of Samples

Note. n.a., not available.

<sup>a</sup> Lost on ignition, indicative of volatiles.

<sup>b</sup> Pressure, in kbar, to which the pure pellet was pressed in the KBr die.

<sup>c</sup> As FeO.

<sup>d</sup> As Fe<sub>2</sub>O<sub>3</sub>.

<sup>e</sup> Analysis from Bruckenthal (1987).

<sup>f</sup> Analysis from Singer (1981).

Gooding, personal communication 1991). The pyrophyllite used here has been characterized by Clark et al. (1990) as being "spectrally pure." Based on its X-ray diffraction pattern, the palagonite is a sample of an X-ray amorphous weathering product of basaltic glass collected at several locations on the upper slopes of Mauna Kea on the island of Hawaii (Roush 1987). The palagonite sample was separated from the bulk soil sample by liquid particle suspension in methanol. Subsequent transmission electron microscopy of this sample indicates that it is mostly amorphous as more than 75-80% of the grains sampled did not produce an electron diffraction pattern (Roush and Blake 1991). The remaining grains which did diffract electrons exhibited patterns which were consistent with smectite clays (Roush and Blake 1991). Chemical analyses for the samples are provided in Table I.

As our research progressed it became obvious we needed to assess the effects of our nonstandard sample preparation (see following section). In order to facilitate our understanding we included an orthopyroxene because, as discussed below, it represents a material which could be prepared using standard thin sectioning and polishing techniques and as a powdered pellet. The pyroxene used here was obtained from Ward's Scientific and is an enstatite from a locale near Bamle, Norway. A chemical analysis from Singer (1981) is also included in Table I.

## 3.2. Sample Preparation

Most of the silicates included in this study are clays which are not amenable to standard polishing techniques. In order to obtain a suitable sample of these less cohesive materials for the laboratory measurements a standard KBr pellet die was used and a pellet of the pure sample was prepared. The powders were previously separated by dry sieving and roughly 200 mg of the finest grain size fraction  $(\leq 38 \,\mu\text{m})$  were placed in the KBr die. The die was placed in a hydraulic press and the pressure increased to a maximum of roughly 0.5 to 7 kbar on the 12-mm die, depending upon the sample (see Table I), and held at that pressure for 5 min. For all clays and the palagonite this produced a pellet with highly reflective surfaces at visible wavelengths (average surface roughness  $0.7 \pm 0.4 \mu m$ ). In contrast, the sole pyroxene prepared by this technique exhibited a matte-like surface (surface roughness  $\approx 5 \,\mu$ m). Inspection of this sample, with a binocular microscope, revealed a pellet which had abundant fine grains of pyroxene adhered to it. In order to semiquantitatively assess the variation of derived optical constants as a function of surface roughness a sample of the pyroxene was also prepared by polishing a large slab of pyroxene to produce a mirror-like surface (surface roughness  $\leq 1 \mu m$ ).

#### 3.3. Laboratory Measurements and Analyses

The reflectivities of all samples were determined by placing them at the focus of a standard near-normal reflectance attachment located in a Nicolet 7199 Fourier transform spectrometer. A schematic diagram illustrating this device is presented in Fig. 1. The Fourier transform of the signal measured from each sample was ratioed to the Fourier transform of the signal obtained from a first



FIG. 1. Schematic diagram of optical path within the spectrometer. For all observations here  $i = e = 20^{\circ}$ .

surface aluminum mirror which was conservatively assumed to have a reflectance of 0.96 at all wavelengths. Data were collected from 4000 to 400 cm<sup>-1</sup> (2.5–25  $\mu$ m) with a constant spectral resolution of 4 cm<sup>-1</sup>; however, as discussed above the dispersion analysis was performed only in the 2000–400 cm<sup>-1</sup> (5.0-25  $\mu$ m) region. The measured reflectivities of all samples are presented in Figs. 2a, 3a, 4a, 5a, 6a, 7a, and 8a.

Table II lists the final dispersion parameters and associated errors for each sample of this study. We find that the value of  $n_{vis}$  for all samples is less than those listed for visible wavelengths (Deer et al. 1966). This is due to our analysis covering a finite wavelength region, and the value of  $n_{vis}$  listed here is really applicable to the value of n at 5  $\mu$ m, not visible wavelengths. This is consistent with previous studies of silicates where both visible and infrared optical constants have been derived (e.g., Pollack et al. 1973, Mooney and Knacke 1985). The refractive indices (n and k) which provided best comparison to the laboratory reflectance data, as defined by minimizing the sum of the square of the differences between the calculated observed reflectances, were determined. The imaginary indices of refraction (n) are presented for the samples in graph form in Figs. 2b, 3b, 4b, 5b, 6b, 7b, and 8b and are also tabulated in the appendix. The real indices of refraction (k) are presented for the samples in graph form in Figs. 2c, 3c, 4c, 5c, 6c, 7c, and 8c and are also tabulated in the appendix.

#### 4. DISCUSSION

#### 4.1. Effect of the Physical Nature of the Surface

As seen in Fig. 2a, the reflectivity of the pyroxene polished slab is roughly three to four times the reflectivity of the pyroxene pure pellet. A comparison of the two surfaces, using a binocular microscope, reveals that the polished slab has a smooth mirror-like surface, whereas the pressed pellet has a rough matte-like surface with obvious fine grains of pyroxene present. We conclude that the polished slab is smooth on the scale of the wavelength, whereas the pellet is rough. The rougher surface results in less Fresnel reflectivity and greater multiply scattered light with the net result being a decrease of the measured reflectance due to the distinctly different physical nature of the two surfaces.

Comparison of the derived oscillator parameters for the



FIG. 2. Measured reflectance of orthopyroxene samples (a). Data points (+) with error bars represent an average of two measurements of the polished slab and the solid line the calculated fit to these data. Triangles  $(\nabla)$  represent the measured reflectance of the pressed pellet and the dashed line a calculated fit to these data. Derived imaginary (b) and real (c) indices of refraction of orthopyroxenes. The solid and dashed line represent the values derived for the polished slab and powdered pellet, respectively.



FIG. 3. Measured (points with error bars) and calculated (solid line) reflectances of kaolinite (a). Imaginary (b) and real (c) indices of refraction derived for kaolinite.

powder and the slab given in Table II immediately shows that one additional oscillator was required to fit the data for the powder. Also  $n_{vis}$  derived for the powder is much less than for the slab. The slab  $n_{vis}$  is slightly less than, but consistent with, values listed in the visible (Deer *et al.* 1966). In general, central wavelengths are shorter, widths are broader, and strengths are less when oscillator parameters for the powder are compared to those of the slab. Figures 2b and 2c illustrate the difference between the derived optical constants of these pyroxene samples. The actual values are tabulated as a function of wave-



FIG. 4. Measured (points with error bars) and calculated (solid line) reflectances of serpentine (a). Imaginary (b) and real (c) indices of refraction derived for serpentine.

length in the appendix. In general, the slab k is a factor of 2 to 4 greater than that derived from the powdered pellet, and occasionally in the more intense features greater by a factor of 10. In general, the derived n of both samples agree to within a factor of 2, but again occasionally deviate by slightly more than 2. These results imply that pellets which have a matte finish are not suited for derivation of the optical constants of the materials, and in order to arrive at the closest estimate of n and k, a sample with a mirror-like surface is required.

In contrast to the pyroxene, the pressed pellets of all



FIG. 5. Measured (points with error bars) and calculated (solid line) reflectances of pyrophyllite (a). Imaginary (b) and real (c) indices of refraction derived for pyrophyllite.

the other samples exhibited mirror-like surfaces similar to the polished slab of orthopyroxene. Hence, we feel that the values derived and presented here represent a close estimate to the optical constants of these materials. This is especially true at those frequencies (wavelengths) where  $k \ge 10^{-2}$ .

# 4.2. Optical Constants in the Region of Adsorbed Water Absorption

Due to extensive isomorphous substitution within their crystalline structure smectite clays readily accommodate



FIG. 6. Measured (points with error bars) and calculated (solid line) reflectances of montmorillonite (a). Imaginary (b) and real (c) indices of refraction derived for montmorillonite.

exchangeable water molecules between basal tetrahedral layers. As such one would expect the spectral signature of such water to be similar to free molecules, and in transmission and diffuse reflectance spectra of smectites absorptions near 6  $\mu$ m are observed (e.g., Salisbury *et al.*1987). In the current study we were able to distinguish a distinctive reflectivity peak near 6  $\mu$ m for both smectites and the palagonite. Although the structural location of the water in palagonite remains uncertain it appears to survive extremes of heating (Bruckenthal 1987). A comparison of the reflectivity of pyrophyllite, a material whose structure





FIG. 7. Measured (points with error bars) and calculated (solid line) reflectances of saponite (a). Imaginary (b) and real (c) indices of refraction derived for saponite.

FIG. 8. Measured (points with error bars) and calculated (solid line) reflectances of palagonite (a). Imaginary (b) and real (c) indices of refraction derived for palagonite.

TABLE II Oscillator Parameters for Silicates

Oscillator	wavelength ( $\mu$ m)	width	strength	Oscillator	wavelength $(\mu m)$	width	strength
	Orthopyrozene, Sla	$b, n_{vis} = 1.6250 \pm$	:0.0108	12	13.7890±0.0005	0.4261±0.0079	0.0031±0.0000
1	9.0524±0.0077	$0.2872 \pm 0.0188$	$0.0006 \pm 0.0001$	13	14.4380±0.0014	$0.3328 \pm 0.0009$	$0.0026 \pm 0.0000$
2	9.3302±0.0019	$0.3531 \pm 0.0094$	$0.0042 \pm 0.0002$	14	$15.2680 \pm 0.0010$	0.4311±0.0109	$0.0014 \pm 0.0000$
3	9.6021±0.0008	$0.2219 \pm 0.0018$	$0.0035 \pm 0.0001$	15	16.9380±0.0005	$1.0319 \pm 0.0058$	$0.0038 \pm 0.0001$
4	9.9373±0.0004	$0.2116 \pm 0.0009$	$0.0025 \pm 0.0000$	16	17.7750±0.0005	$0.4897 \pm 0.0018$	$0.0041 \pm 0.0001$
5	$10.2140 \pm 0.0005$	$0.2528 \pm 0.0003$	$0.0056 \pm 0.0001$	17	18.4930±0.0009	$0.7099 \pm 0.0054$	$0.0093 \pm 0.0002$
6	$10.5370 \pm 0.0005$	$0.3243 \pm 0.0004$	$0.0091 \pm 0.0001$	18	$20.1280 \pm 0.0111$	$0.6864 \pm 0.0042$	$0.0367 \pm 0.0038$
7	$10.8230 \pm 0.0005$	$0.2070 \pm 0.0005$	0.0084±0.0000	19	20.4970±0.0266	$0.5703 \pm 0.0271$	$0.0281 \pm 0.0024$
8	$11.1260 \pm 0.0000$	$0.1925 \pm 0.0006$	0.0028±0.0000	20	$20.8830 \pm 0.0324$	$0.5346 \pm 0.0307$	$0.0164 \pm 0.0017$
9	$11.3820 \pm 0.0011$	$0.2231 \pm 0.0015$	$0.0094 \pm 0.0001$	21	$21.3210 \pm 0.0350$	$0.4748 \pm 0.0325$	$0.0083 \pm 0.0011$
10	$11.6460 \pm 0.0004$	$0.0932 \pm 0.0013$	$0.0029 \pm 0.0000$	22	$21.8080 \pm 0.0088$	$0.6984 \pm 0.1219$	$0.0203 \pm 0.0047$
11	$11.5190 \pm 0.0010$	$0.1590 \pm 0.0005$	0.0072±0.0001	23	26.6700±0.2729	$2.0060 \pm 0.1244$	$0.1264 \pm 0.0185$

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Oscillator	wavelength (um)	width	et rengt h	Oscillator	mayolongth (up)		-4
					wavelength (µm)	width	strength
0	rthopyroxene, Powa	ler, $n_{vis} = 1.3200$	)±0.0127		Pyrophyllite, n.	$v_{is} = 1.3550 \pm 0.0$	040
1	$9.0591 \pm 0.0250$	$0.6709 \pm 0.1253$	$0.0022 \pm 0.0006$	1	$8.8448 \pm 0.0040$	0.1497±0.0041	$0.0013 \pm 0.0000$
2	9.3089±0.0101	$0.5565 \pm 0.0324$	$0.0041 \pm 0.0001$	2	$8.9163 \pm 0.0014$	$0.0698 \pm 0.0030$	$0.0012 \pm 0.0001$
3	9.6497±0.0017	$0.3538 \pm 0.0068$	$0.0015 \pm 0.0001$	3	$9.1628 \pm 0.0005$	0.1372±0.0005	$0.0021 \pm 0.0001$
4	9.9272±0.0013	$0.2167 \pm 0.0104$	$0.0007 \pm 0.0001$	4	$9.3058 \pm 0.0014$	$0.2164 \pm 0.0027$	$0.0124 \pm 0.0001$
5	$10.2290 \pm 0.0030$	$0.2346 \pm 0.0022$	$0.0018 \pm 0.0000$	5	$10.4900 \pm 0.0008$	$0.1761 \pm 0.0010$	$0.0020 \pm 0.0000$
6	$10.4830 \pm 0.0029$	0.3737±0.0058	$0.0033 \pm 0.0001$	6	$8.7311 \pm 0.0054$	$0.4135 \pm 0.0067$	$0.0020 \pm 0.0001$
7	$10.7490 \pm 0.0048$	$0.2506 \pm 0.0154$	$0.0012 \pm 0.0001$	7	$11.7240 \pm 0.0000$	$0.1499 \pm 0.0025$	$0.0002 \pm 0.0000$
8	$11.0800 \pm 0.0072$	0.0757±0.0446	$0.0001 \pm 0.0000$	8	11.9680±0.0000	$0.1199 \pm 0.0011$	$0.0004 \pm 0.0000$
9	$11.4220 \pm 0.0130$	$0.2796 \pm 0.0640$	$0.0012 \pm 0.0002$	9	$11.2080 \pm 0.0826$	$3.7121 \pm 0.1461$	$0.0077 \pm 0.0002$
10	$11.3130 \pm 0.0189$	$0.2823 \pm 0.0634$	$0.0012 \pm 0.0002$	10	$12.2850 \pm 0.0005$	$0.1761 \pm 0.0141$	$0.0002 \pm 0.0000$
11	$11.5750 \pm 0.0069$	$0.2286 \pm 0.0262$	$0.0006 \pm 0.0000$	11	$16.0570 \pm 0.0018$	$0.6447 \pm 0.0113$	$0.0005 \pm 0.0000$
12	$13.6690 \pm 0.0228$	$0.8135 \pm 0.2908$	0.0007±0.0002	12	17.0970±0.0005	$0.7746 \pm 0.0003$	0.0029+0.0000
13	$14.4930 \pm 0.0033$	$0.3691 \pm 0.0183$	$0.0009 \pm 0.0001$	13	$18.5260 \pm 0.0039$	$0.9515 \pm 0.0014$	0.0312+0.0003
14	$15.3960 \pm 0.0013$	$0.4211 \pm 0.0208$	0.0007±0.0000	14	$19.2070 \pm 0.0026$	$0.2852 \pm 0.0039$	0.0012±0.0000
15	$16.9480 \pm 0.0007$	$1.0682 \pm 0.0312$	$0.0025 \pm 0.0002$	15	$20.7050 \pm 0.0029$	0 7863+0 0017	0.0286+0.0001
16	$17.5940 \pm 0.0008$	0.9989±0.0007	$0.0038 \pm 0.0001$	16	$21.6820 \pm 0.0016$	$0.7729 \pm 0.0235$	0.0044+0.0002
17	$18.2740 \pm 0.0058$	$1.0030 \pm 0.0046$	$0.0086 \pm 0.0000$	17	$23.8390 \pm 0.0004$	$0.4701 \pm 0.0041$	0.0027+0.0000
18	$19.2790 \pm 0.0056$	$0.6767 \pm 0.0034$	$0.0060 \pm 0.0000$			0.1.01±0.0011	0.0021 20.0000
19	$19.5990 \pm 0.0130$	0.7415±0.0082	$0.0031 \pm 0.0000$		Saponite, n <sub>vis</sub>	$= 1.3134 \pm 0.003$	28
20	$19.9660 \pm 0.0162$	$0.9321 \pm 0.0363$	$0.0024 \pm 0.0002$	1	6.1708+0.0154	0 1916+0 1081	0 0001+0 0001
21	$21.6290 \pm 0.0161$	$1.0250 \pm 0.0287$	$0.0027 \pm 0.0002$	2	9 1474+0 0002	$0.3675 \pm 0.0035$	0.000110.0001
22	$22.1170 \pm 0.0112$	$0.7108 \pm 0.0249$	$0.0019 \pm 0.0001$	3	$9.8531 \pm 0.0021$	$0.0010\pm0.0000$ 0.4814+0.0017	0.0163±0.0000
23	$23.8240 \pm 0.0004$	$0.0381 \pm 0.0094$	$0.0003 \pm 0.0000$	4	$136500 \pm 0.0369$	$3.1476 \pm 0.0871$	0.0032±0.0000
24	24.7670±0.0028	$0.3594 \pm 0.0484$	$0.0010 \pm 0.0001$	5	$15,1570\pm0.0014$	0.6703+0.0025	0.0032±0.0000
				6	$20.1070 \pm 0.0063$	2 3999+0 0092	0.0169+0.0000
	Kaolinite, n <sub>vi</sub>	$= 1.4400 \pm 0.010$	8	7	$21.4140 \pm 0.0034$	1 4703+0 0117	0.0103±0.0004
1	8 9326+0 0004	0 1632+0 0000	0.0000 1.0.0000	8	$22.3200 \pm 0.0036$	0.5615+0.0106	0.0004±0.0003
2	0.002010.0004	$0.1032 \pm 0.0009$	0.0009±0.0000	-		0.00101010100	0.0010100001
3	9 9143-0 0024	0.2193±0.0001	0.0100±0.0000		Montmorillonite n	$a_{\rm ref} = 1.4050 \pm 0$	0050
4	10 6350 +0 0008	0.1330±0.0049	$0.0007 \pm 0.0003$				0000
5	10 8200 + 0 0005	$0.1900 \pm 0.0041$ 0.1977 $\pm 0.0000$	$0.0021 \pm 0.0000$	1	$6.1251 \pm 0.0004$	$0.0558 \pm 0.0018$	$0.0001 \pm 0.0000$
6	$10.0200 \pm 0.0000$	$0.1677 \pm 0.0029$	0.0018±0.0000	2	$8.7293 \pm 0.0015$	$0.3944 \pm 0.0078$	$0.0007 \pm 0.0000$
7	$12.6050 \pm 0.0013$	0.1030±0.0003	0.0032±0.0001	3	$8.9212 \pm 0.0007$	$0.2563 \pm 0.0013$	$0.0018 \pm 0.0000$
8	13 3200+0.0008	0.2911±0.0020	0.0000±0.0000	4	$9.5429 \pm 0.0011$	$0.3056 \pm 0.0010$	$0.0136 \pm 0.0005$
ŏ	14 7470±0 0129	0.0015.10.0004	0.0000±0.0001	5	9.7748±0.0021	$0.3198 \pm 0.0082$	$0.0103 \pm 0.0004$
10	15 5010+0.0037	0.9213±0.0294	0.0024±0.0001	6	$10.8660 \pm 0.0006$	$0.2866 \pm 0.0098$	$0.0012 \pm 0.0001$
11	16 8860±0.0007	$1.5651\pm0.0024$	0.0008±0.0000	7	$11.3240 \pm 0.0015$	$0.3367 \pm 0.0053$	$0.0007 \pm 0.0000$
12	$17.9890 \pm 0.0100$	1.0001±0.0107	0.0080±0.0005	8	$11.7390 \pm 0.0010$	$0.1965 \pm 0.0066$	$0.0002 \pm 0.0000$
13	18 5560+0 0000	0.5889±0.0209	0.0197±0.0002	9	$12.6210 \pm 0.0010$	$0.3401 \pm 0.0005$	$0.0004 \pm 0.0000$
14	21.2710+0.0066	0.3652±0.0084	0.0224±0.0001	10	$14.3020 \pm 0.0053$	$0.3290 \pm 0.0524$	$0.0001 \pm 0.0000$
15	23 2230+0 0028	0.1014±0.0045	0.0243±0.0000	11	$16.8460 \pm 0.0025$	$2.4263 \pm 0.0281$	$0.0082 \pm 0.0002$
	20.2200.20.0020	0.330010.0042	0.0100±0.0001	12	$18.3180 \pm 0.0006$	$1.4641 \pm 0.0066$	$0.0114 \pm 0.0001$
	Serpentine, n <sub>vi</sub>	$= 1.4000 \pm 0.01$	58	13	18.9800±0.0030	$0.7182 \pm 0.0035$	$0.0118 \pm 0.0000$
1	9 2634-0 0060	0 2202 + 0 0204	0.0010 1.0.0001	14	$20.9160 \pm 0.0025$	$0.8305 \pm 0.0012$	$0.0097 \pm 0.0001$
2	9.2034 10.0009	0.5302±0.0204	0.0010±0.0001	15	$21.4010 \pm 0.0030$	$0.8047 \pm 0.0075$	$0.0219 \pm 0.0002$
3	10 2480 ±0.0032	0.3163±0.0102	0.0040±0.0000		Palagonite, n	$= 1.5077 \pm 0.003$	0
4	10 4840-0 0074	0.2001 ±0.02/0	0.000510.0001				
5	16 2320-0 0187	1 7456-0 0070	0.0000 ± 0.0004	1	0.0961±0.0032	$0.3309 \pm 0.0148$	$0.0005 \pm 0.0000$
6	18 0870+0 0004		0.0209±0.0005	2	9.8177±0.0024	$1.2525 \pm 0.0029$	$0.0218 \pm 0.0001$
7	20.0010.20.0004	1.1000±0.0160	0.0042±0.0001	3	$10.9110 \pm 0.0015$	$0.9340 \pm 0.0145$	$0.0025 \pm 0.0001$
8	21 0080 +0 0097		0.0004±0.0001	4	$14.3460 \pm 0.0228$	$4.0665 \pm 0.1040$	$0.0079 \pm 0.0003$
ğ	22 3150+0 0411	2 2162±0.0333	0.0090±0.0004	5	$18.4430 \pm 0.0072$	$5.3360 \pm 0.0311$	$0.0617 \pm 0.0003$
10	22.8470+0.0100	0 5539±0 0775	0.0010±0.0000	8	21.4100±0.0095	1.4590±0.0659	$0.0058 \pm 0.0006$
		0.000220.0110	0.0090±0.0004	7	$23.1830 \pm 0.0250$	$3.4204 \pm 0.2421$	$0.0178 \pm 0.0017$

TABLE II—Continued

does not accommodate exchangeable water, to the reflectivities of the smectites and the palagonite is shown in Fig. 9. Our analyses of these "water-bearing" samples included a single oscillator to describe these features and our results are the first, to our knowledge, to provide optical constants of such materials.

# 4.3. Comparison to Previous Studies

Montmorillonite. A comparison of our determined optical constants, n and k, of montmorillonite to the tabulated values of two samples of montmorillonite presented by Toon *et al.* (1977) is shown in Figs. 10a and 10b. As seen



FIG. 9. Measured reflectivities of (a) pyrophyllite, (b) montmorillonite, (c) saponite, and (d) palagonite in the region of adsorbed water absorption.

in these figures the values from the two studies generally agree quite well, although there are some discrepancies. We believe these discrepancies can be explained by differences in sample composition, methods of defining a "best fit" to the reflectivity data, and wavelength coverage of the reflectivity data.

The chemical analyses of the two montmorillonites of Toon *et al.* (1977) are included in Table I. There are obvious differences in the abundances of silicon, iron, magnesium, and sodium between the three samples. As discussed by Farmer (1974) and Russell (1987) the Si-O stretching vibrations near 10  $\mu$ m are only weakly coupled with other vibrations of the structure of montmorillonites, hence variations of silica content will not strongly influence these features until the structure is significantly altered. On the other hand the Si-O bending vibrations between 17 and 50  $\mu$ m are strongly coupled with vibrations of the octahedral cations. As a result, the features at 19 and 21  $\mu$ m can be strongly influenced by iron and magnesium substitution. The octahedral cation-OH bending vibrations occur between 10.5 and 16  $\mu$ m, thus features in this region will also be strongly affected by compositional differences within the octahedral sites.

Toon *et al.*(1977) derived optical constants from measurements which included the 25- to 40- $\mu$ m wavelength region. The possibility of additional features at these wavelengths which are not included in the current study is quite real. The existence of any features beyond 400 cm<sup>-1</sup> (25  $\mu$ m) would most strongly affect the longest wavelength features observed in the current study. In their analyses Toon *et al.*(1977) estimated when the best comparison between the measured and calculated re-



FIG. 10. Comparison of the (a) imaginary and (b) and real indices of refraction of montmorillonite derived in this study (solid line) to those previously presented by Toon *et al.*(1977) (dashed line 222B, dotted line 219B).

flectance occurred (O. B. Toon, personal communication 1988) rather than formally minimizing the differences between the two values.

Serpentine. A comparison of our derived values of n and k for serpentine with those of Mooney and Knacke (1985) is presented in Figs. 11a and 11b, respectively. The agreement between the values is generally quite good, although there are some discrepancies. As for the montmorillonite above, we believe these discrepancies can be explained by differences in sample composition, sample preparation, and dispersion analysis techniques. The chemical analysis of the serpentine used by Mooney and Knacke (1985) is included in Table I. There are obvious differences in the abundances of silicon, iron, and magnesium between the two samples. The compositional variation in iron and magnesium would be expected to most strongly affect bands in the 15- to  $25-\mu m$  wavelength region (Farmer 1974, Russell 1987). If we speculate that some of the ferric iron is substituting for silicon in the tetrahedral layer, then this could explain the apparent shift in the maxima of the real index near 10.5  $\mu$ m.

The sample of Mooney and Knacke (1985) was a polished slab of serpentine while the current study used a pressed pellet. As discussed above for the orthopyroxene, if the pellet has a matte-like surface the derived values of k will be underestimated and the values of n only approximate. This is in agreement with the differences seen in Fig. 4b. Even though the pellet appeared mirror-like upon inspection with the binocular microscope, we can not rule out the possibility that differences in the physical nature of the two surfaces can explain the discrepencies in the derived optical constants. In their analysis Mooney and Knacke (1985) were able to include data for the 400-200  $cm^{-1}$  (25–50  $\mu$ m) region while we could not. As discussed above for the montmorillonite, the existence of any features in this region would most strongly affect the longest wavelength features seen in the current study.

*Palagonite*. Crisp and Bartholomew (1989) presented the imaginary index of refraction of a palagonite in the 1250–500 cm<sup>-1</sup> (8–20  $\mu$ m) region for both the hydrated and the dehydrated samples. A comparison of their results with ours is given in Fig. 12. In this case the values we derived for the palagonite generally fall between the two



FIG. 11. Comparison of the (a) imaginary and (b) real indices of refraction of serpentine derived in this study (solid line) to those previously presented by Mooney and Knacke (1985) (dashed line).



FIG. 12. Comparison of the imaginary index of refraction of palagonite derived in this study (solid line) to those previously presented by Crisp and Bartholomew (1989) for "wet" (dashed line) and "dry" (dotted line) palagonite.

values derived by Crisp and Bartholomew (1989). Some discrepancies still exist, particularly at the longer wavelengths, but this may be due to differences in sample composition, as well as the derivation of values by distinctly different techniques. Crisp and Bartholomew (1989) used transmission measurements, Beer's Law, and assumed the real index of refraction was constant in order to derive the imaginary index of palagonite.

# 5. CONCLUSIONS

Here we present the real (n) and imaginary (k) indices of refraction of kaolinite, serpentine, montmorillonite, saponite, palagonite, and orthopyroxene as determined by dispersion analysis. We found that comparison of the values derived here for serpentine, montmorillonite, and palagonite to values previously presented were generally consistent. The discrepancies which did exist for these comparisons can be explained by either different sample compositions, sample preparation, or analysis techniques. Comparison of the optical constants derived for both a polished slab and pressed pellet of orthopyroxene led us to conclude that when possible, a polished surface is preferable to a pressed pellet for derivation of optical constants. However, when the physical characteristics of a material preclude preparation of a polished surface the results presented here indicate that if a mirror-like surface is produced, then optical constants can be derived from a pressed pellet of the pure material. Thus, the techniques presented here appear to provide a mechanism for deriving optical constants of clays and other noncohesive materials which may be of interest for interpretation of planetary surface composition.

		Orthopy	roxene													
wavelength	Sh	ab	Pow	der	Kaol	inite	Serpe	ntine	Pyrop	hyllite	Montm	orillonite	Sapo	nite	Palag	onite
(in µm)	n	k	n	k	n	k	n	k	n	k	n	k	n	k	n	k
5.000	1.505	0.002	1.277	0.001	1.362	0.001	1.344	0.002	1.280	0.003	1.336	0.002	1.262	0.002	1.438	0.006
5.010	1.504	0.002	1.277	0.001	1.362	0.001	1.343	0.002	1.280	0.003	1.335	0.002	1.262	0.002	1.438	0.006
5.020	1.503	0.002	1.277	0.001	1.362	0.001	1.343	0.002	1.279	0.003	1.335	0.002	1.262	0.002	1.437	0.006
5.030	1.503	0.002	1.276	0.001	1.361	0.001	1.343	0.002	1.279	0.003	1.335	0.002	1.261	0.002	1.437	0.006
5.040	1.502	0.002	1.276	0.001	1.361	0.001	1.343	0.002	1.278	0.003	1.334	0.002	1.261	0.002	1.436	0.006
5.050	1.502	0.002	1.276	0.001	1.360	0.001	1.342	0.002	1.278	0.003	1.334	0.002	1.261	0.002	1.436	0.006
5.061	1.501	0.002	1.276	0.001	1.360	0.001	1.342	0.002	1.278	0.003	1.333	0.002	1.260	0.002	1.436	0.006
5.071	1.500	0.002	1.276	0.001	1.360	0.001	1.342	0.002	1.277	0.003	1.333	0.002	1.260	0.002	1.435	0.007
5.081	1.500	0.002	1.275	0.001	1.359	0.001	1.341	0.002	1.277	0.003	1.333	0.002	1.260	0.002	1.435	0.007
5.092	1.499	0.002	1.275	0.001	1.359	0.001	1.341	0.002	1.276	0.003	1.332	0.002	1.260	0.002	1.434	0.007
5.102	1.498	0.002	1.275	0.001	1.358	0.001	1.341	0.002	1.276	0.003	1.332	0.002	1.259	0.002	1.434	0.007
5.113	1.498	0.002	1.275	0.001	1.358	0.001	1.340	0.002	1.276	0.003	1.332	0.002	1.259	0.002	1.434	0.007
5.123	1.497	0.002	1.274	0.001	1.357	0.001	1.340	0.002	1.275	0.003	1.331	0.002	1.259	0.002	1.433	0.007
5.134	1.497	0.002	1.274	0.001	1.357	0.001	1.340	0.002	1.275	0.003	1.331	0.002	1.258	0.002	1.433	0.007
5.144	1.496	0.002	1.274	0.001	1.357	0.001	1.340	0.002	1.274	0.003	1.330	0.002	1.258	0.002	1.432	0.007
5.155	1.495	0.002	1.274	0.001	1.356	0.001	1.339	0.002	1.274	0.003	1.330	0.002	1.258	0.002	1.432	0.007
5.165	1.495	0.002	1.273	0.001	1.356	0.001	1.339	0.002	1.273	0.003	1.329	0.002	1.258	0.002	1.431	0.007
5.176	1.494	0.002	1.273	0.001	1.355	0.001	1.339	0.002	1.273	0.003	1.329	0.002	1.257	0.002	1.431	0.007
5.187	1.493	0.002	1.273	0.001	1.355	0.001	1.338	0.002	1.272	0.003	1.329	0.002	1.257	0.002	1.430	0.007
5.198	1.492	0.002	1.273	0.001	1.354	0.001	1.338	0.002	1.272	0.003	1.328	0.002	1.257	0.002	1.430	0.007
5.208	1.492	0.002	1.272	0.001	1.354	0.001	1.338	0.002	1.271	0.003	1.328	0.002	1.256	0.002	1.429	0.007
5.219	1.491	0.002	1.272	0.001	1.353	0.001	1.337	0.002	1.271	0.003	1.327	0.002	1.256	0.002	1.429	0.008
5.230	1.490	0.002	1.272	0.001	1.353	0.001	1.337	0.002	1.270	0.003	1.327	0.002	1.256	0.002	1.429	0.008
5.241	1.490	0.002	1.272	0.001	1.352	0.001	1.337	0.002	1.270	0.003	1.326	0.002	1.255	0.002	1.428	0.008
5.252	1.489	0.002	1.271	0.001	1.352	0.001	1.336	0.002	1.270	0.003	1.326	0.002	1.255	0.002	1.428	0.008
5.263	1.488	0.002	1.271	0.001	1.351	0.001	1.336	0.002	1.269	0.003	1.325	0.002	1.255	0.002	1.427	0.008
5.274	1.487	0.002	1.271	0.001	1.351	0.001	1.336	0.002	1.269	0.003	1.325	0.002	1.254	0.002	1.427	0.008
5.285	1.487	0.002	1.270	0.001	1.350	0.001	1.335	0.002	1.268	0.003	1.324	0.002	1.254	0.002	1.426	0.008
5.297	1.486	0.002	1.270	0.001	1.350	0.001	1.335	0.002	1.268	0.004	1.324	0.002	1.254	0.002	1.426	0.008
5.308	1.485	0.002	1.270	0.001	1.349	0.001	1.335	0.002	1.267	0.004	1.324	0.002	1.253	0.002	1.425	0.008
5.319	1.484	0.002	1.270	0.001	1.349	0.001	1.334	0.002	1.266	0.004	1.323	0.002	1.253	0.002	1.425	0.008

6. APPENDIX: OPTICAL CONSTANTS

-		Orthopy	roxene													
wavelength	SI	ab	Pov	wder	Kao	linite	Serp	entine	Pyrop	hyllite	Montn	norillonite	Sap	onite	Pala	gonite
<u>(in µm)</u>	<u>n</u>	<u>k</u>	n	<u>k</u>	n	<u>k</u>	n	<u>k</u>	n	<u>k</u>	n	k	n	k	n	k
5.331	1.484	0.002	1.269	0.001	1.348	0.001	1.334	0.002	1.266	0.004	1.322	0.002	1.253	0.002	1.424	0.009
5.342	1.483	0.002	1.269	0.002	1.348	0.001	1.334	0.002	1.265	0.004	1.322	0.002	1.252	0.002	1.423	0.009
0.000	1.402	0.002	1.209	0.002	1.047	0.001	1.000	0.002	1.200	0.004	1.321	0.002	1.202	0.002	1.423	0.009
5 376	1.461	0.002	1.200	0.002	1.347	0.001	1.000	0.002	1.204	0.004	1.321	0.002	1.401	0.002	1.422	0.009
5 388	1.480	0.002	1.208	0.002	1.340	0.001	1 330	0.002	1.204	0.004	1.320	0.002	1.201	0.002	1.422	0.009
5 400	1.400	0.002	1.268	0.002	1.345	0.002	1.332	0.002	1.203	0.004	1.320	0.002	1.201	0.002	1.421	0.009
5.411	1.478	0.002	1.267	0.002	1.345	0.002	1.332	0.002	1.262	0.004	1.319	0.002	1 250	0.003	1 420	0.009
5.423	1.477	0.002	1.267	0.002	1.344	0.002	1.331	0.002	1.262	0.004	1.318	0.002	1.250	0.003	1.419	0.010
5.435	1.476	0.002	1.267	0.002	1.343	0.002	1.331	0.002	1.261	0.004	1.318	0.002	1.249	0.003	1.419	0.010
5.447	1.476	0.002	1.266	0.002	1.343	0.002	1.330	0.002	1.260	0.004	1.317	0.002	1.249	0.003	1.418	0.010
5.458	1.475	0.002	1.266	0.002	1.342	0.002	1.330	0.002	1.260	0.004	1.317	0.002	1.248	0.003	1.418	0.010
5.470	1.474	0.002	1.266	0.002	1.342	0.002	1.329	0.002	1.259	0.004	1.316	0.002	1.248	0.003	1.417	0.010
5.483	1.473	0.002	1.265	0.002	1.341	0.002	1.329	0.002	1.259	0.004	1.316	0.002	1.247	0.003	1.416	0.010
5.495	1.472	0.002	1.265	0.002	1.340	0.002	1.329	0.002	1.258	0.004	1.315	0.002	1.247	0.003	1.416	0.010
5.507	1.471	0.002	1.265	0.002	1.340	0.002	1.328	0.002	1.258	0.004	1.314	0.002	1.247	0.003	1.415	0.011
0.019 E E 01	1.470	0.002	1.265	0.002	1.339	0.002	1.328	0.002	1.257	0.004	1.314	0.002	1.246	0.003	1.414	0.011
5.542	1.409	0.002	1.204	0.002	1.339	0.002	1.327	0.002	1.250	0.004	1.313	0.003	1.246	0.003	1.414	0.011
5 556	1.468	0.003	1 263	0.002	1 337	0.002	1 3 97	0.002	1.200	0.004	1.313	0.003	1.240	0.003	1.410	0.011
5.568	1.467	0.003	1.263	0.002	1.337	0.002	1.326	0.002	1.250	0.004	1.312	0.003	1.245	0.003	1.412	0.011
5.580	1.466	0.003	1.263	0.002	1.336	0.002	1.326	0.002	1.254	0.004	1.311	0.003	1.244	0.003	1.411	0.012
5.593	1.465	0.003	1.262	0.002	1.336	0.002	1.325	0.002	1.253	0.005	1.310	0.003	1.244	0.003	1.410	0.012
5.605	1.464	0.003	1.262	0.002	1.335	0.002	1.325	0.002	1.252	0.005	1.309	0.003	1.243	0.003	1.409	0.012
5.618	1.463	0.003	1.262	0.002	1.334	0.002	1.324	0.002	1.252	0.005	1.309	0.003	1.243	0.003	1.408	0.013
5.631	1.462	0.003	1.261	0.002	1.334	0.002	1.324	0.002	1.251	0.005	1.308	0.003	1.242	0.003	1.408	0.013
5.643	1.461	0.003	1.261	0.002	1.333	0.002	1.324	0.003	1.250	0.005	1.308	0.003	1.242	0.003	1.407	0.013
5.656	1.460	0.003	1.261	0.002	1.332	0.002	1.323	0.003	1.250	0.005	1.307	0.003	1.241	0.003	1.406	0.014
5.669	1.459	0.003	1.260	0.002	1.332	0.002	1.323	0.003	1.249	0.005	1.306	0.003	1.241	0.003	1.405	0.014
5.682 5.605	1.458	0.003	1.260	0.002	1.331	0.002	1.322	0.003	1.248	0.005	1.305	0.003	1.240	0.003	1.404	0.014
5 708	1.456	0.003	1.259	0.002	1.330	0.002	1.322	0.003	1.247	0.005	1.305	0.003	1.240	0.004	1.403	0.015
5 721	1.455	0.003	1 259	0.002	1 329	0.002	1.321	0.003	1.247	0.005	1.304	0.003	1.239	0.004	1.403	0.010
5.734	1.454	0.003	1.258	0.002	1.328	0.002	1.321	0.003	1.240	0.005	1 303	0.003	1.230	0.004	1.401	0.010
5.747	1.453	0.003	1.258	0.002	1.327	0.002	1.320	0.003	1.245	0.005	1.302	0.003	1 237	0.004	1 400	0.010
5.760	1.452	0.003	1.258	0.002	1.327	0.002	1.319	0.003	1.244	0.005	1.301	0.003	1.237	0.004	1.399	0.017
5.774	1.451	0.003	1.257	0.002	1.326	0.002	1.319	0.003	1.243	0.005	1.300	0.003	1.236	0.004	1.398	0.018
5.787	1.449	0.003	1.257	0.002	1.325	0.002	1.318	0.003	1.242	0.005	1.299	0.003	1.236	0.004	1.397	0.018
5.800	1.448	0.003	1.256	0.002	1.324	0.002	1.318	0.003	1.241	0.005	1.298	0.003	1.235	0.004	1.396	0.019
5.814	1.447	0.003	1.256	0.002	1.324	0.002	1.317	0.003	1.241	0.005	1.298	0.003	1.235	0.004	1.395	0.020
5.827	1.446	0.003	1.255	0.002	1.323	0.002	1.317	0.003	1.240	0.006	1.297	0.003	1.234	0.004	1.393	0.021
5.841 F of F	1.445	0.003	1.255	0.002	1.322	0.002	1.316	0.003	1.239	0.006	1.296	0.003	1.233	0.005	1.392	0.022
0.800 5.960	1.444	0.003	1.255	0.002	1.321	0.002	1.316	0.003	1.238	0.006	1.295	0.004	1.232	0.005	1.391	0.023
5.889	1.445	0.003	1.204	0.002	1.320	0.002	1.315	0.003	1.237	0.000	1.294	0.004	1.232	0.005	1.390	0.024
5.896	1 440	0.003	1 253	0.002	1.319	0.002	1 314	0.003	1.237	0.000	1.293	0.004	1.231	0.005	1.389	0.025
5.910	1.439	0.003	1.253	0.003	1.318	0.002	1.314	0.003	1.235	0.006	1.291	0.004	1.230	0.000	1 387	0.027
5.924	1.438	0.003	1.252	0.003	1.317	0.002	1.313	0.003	1.234	0.006	1.290	0.004	1.229	0.000	1.387	0.028
5.938	1.436	0.003	1.252	0.003	1.316	0.002	1.313	0.003	1.233	0.006	1.289	0.004	1.228	0.006	1.386	0.032
5.952	1.435	0.004	1.251	0.003	1.315	0.002	1.312	0.003	1.232	0.006	1.288	0.004	1.227	0.006	1.385	0.034
5.967	1.434	0.004	1.251	0.003	1.314	0.002	1.311	0.003	1.231	0.006	1.287	0.004	1.227	0.007	1.385	0.036
5.981	1.433	0.004	1.250	0.003	1.314	0.002	1.311	0.003	1.230	0.006	1.285	0.005	1.226	0.007	1.385	0.038
5.995	1.431	0.004	1.250	0.003	1.313	0.002	1.310	0.003	1.229	0.006	1.284	0.005	1.225	0.008	1.385	0.041
6.010	1.430	0.004	1.249	0.003	1.312	0.003	1.309	0.003	1.228	0.006	1.282	0.005	1.224	0.008	1.386	0.043
6 039	1.429	0.004	1.249	0.003	1.311	0.003	1.309	0.003	1.227	0.007	1.281	0.006	1.223	0.009	1.387	0.046
6 053	1 426	0.004	1.248	0.003	1.310	0.003	1.308	0.003	1.220	0.007	1.279	0.007	1.222	0.009	1.388	0.048
6.068	1.425	0.004	1.247	0.003	1.308	0.003	1.307	0.003	1 224	0.001	1.270	0.000	1.221	0.010	1.390	0.050
6.083	1.423	0.004	1.247	0.003	1.307	0.003	1.306	0.004	1.223	0.007	1.271	0.013	1.220	0.011	1.393	0.051
6.098	1.422	0.004	1.246	0.003	1.306	0.003	1.306	0.004	1.222	0.007	1.269	0.019	1.219	0.014	1.398	0.052
6.113	1.420	0.004	1.246	0.003	1.305	0.003	1.305	0.004	1.221	0.007	1.272	0.028	1.219	0.016	1.401	0.053
6.128	1.419	0.004	1.245	0.003	1.304	0.003	1.304	0.004	1.220	0.007	1.284	0.033	1.219	0.018	1.403	0.052
6.142	1.417	0.004	1.245	0.003	1.303	0.003	1.304	0.004	1.219	0.007	1.294	0.025	1.221	0.020	1.406	0.050
6.158	1.416	0.004	1.244	0.003	1.302	0.003	1.303	0.004	1.218	0.007	1.294	0.017	1.223	0.022	1.407	0.049
6.173	1.414	0.004	1.243	0.003	1.301	0.003	1.303	0.004	1.217	0.007	1.291	0.012	1.225	0.022	1.409	0.047
0.188 6.903	1.413	0.004	1.243	0.003	1.300	0.003	1.302	0.004	1.216	0.008	1.288	0.009	1.227	0.020	1.410	0.045
6 910	1.411	0.004	1.242	0.003	1.299	0.003	1.301	0.004	1.215	0.008	1.286	0.008	1.229	0.019	1.410	0.042
6 234	1.410	0.004	1.242	0.003	1.298	0.003	1 300	0.004	1.213	0.008 0.009	1.283	0.007	1.229	0.017	1.410	0.040
6.250	1.407	0.004	1 240	0.003	1.297	0.003	1.000	0.004	1.212	0.008	1.201	0.000	1.229	0.015	1.410	0.038
6.266	1.405	0.005	1.240	0.003	1.294	0.003	1.298	0.004	1.210	0.008	1.278	0.000	1.229	0.014	1.409	0.037
6.281	1.403	0.005	1.239	0.004	1.293	0.003	1.298	0.004	1.209	0.008	1.276	0.006	1.227	0.013	1.407	0.033
6.297	1.402	0.005	1.238	0.004	1.292	0.003	1.297	0.004	1.207	0.008	1.275	0.006	1.226	0.011	1.406	0.032
6.313	1.400	0.005	1.238	0.004	1.291	0.003	1.296	0.004	1.206	0.008	1.273	0.006	1.225	0.011	1.405	0.031
6.329	1.398	0.005	1.237	0.004	1.290	0.003	1.295	0.004	1.205	0.009	1.271	0.006	1.224	0.010	1.404	0.030
6.345	1.397	0.005	1.236	0.004	1.288	0.003	1.294	0.004	1.204	0.009	1.270	0.006	1.223	0.010	1.403	0.029
6.361	1.395	0.005	1.236	0.004	1.287	0.003	1.294	0.004	1.202	0.009	1.269	0.006	1.222	0.009	1.401	0.028
6.378	1.393	0.005	1.235	0.004	1.286	0.003	1.293	0.004	1.201	0.009	1.267	0.006	1.221	0.009	1.400	0.027

6. APPENDIX—Continued

# ROUSH, POLLACK, AND ORENBERG

6. APPENDIX—Continued

	Orthopyroxene				•.			Duran		Montm	millonito	Sano	nito	Palar	onite	
wavelength (in µm)	Sla n	ub k	Pow n	der k	Kaoli n	k k	n	htine k	r yropi n	k	n	k	n	k	n	k
6.394	1.391	0.005	1.234	0.004	1.285	0.003	1.292	0.004	1.199	0.009	1.266	0.006	1.220	0.009	1.398	0.027
6.410	1.390	0.005	1.234	0.004	1.283	0.004	1.291	0.005	1.198	0.009	1.264	0.006	1.219	0.008	1.397	0.026
6.427 6.443	1.388	0.005	1.233	0.004	1.282	0.004	1.291	0.005	1.195	0.009	1.261	0.006	1.217	0.008	1.394	0.025
6.460	1.384	0.005	1.231	0.004	1.279	0.004	1.289	0.005	1.194	0.010	1.260	0.006	1.216	0.008	1.393	0.025
6.477	1.382	0.005	1.231	0.004	1.278	0.004	1.288	0.005	1.192	0.010	1.258	0.006	1.215	0.008	1.391	0.025
6.494	1.380	0.006	1.230	0.004	1.277	0.004	1.287	0.005	1.191	0.010	1.257	0.000	1.214	0.007	1.388	0.025
6.527	1.376	0.000	1.228	0.005	1.274	0.004	1.285	0.005	1.188	0.010	1.254	0.006	1.212	0.007	1.387	0.024
6.544	1.374	0.006	1.227	0.005	1.272	0.004	1.284	0.005	1.186	0.010	1.253	0.006	1.211	0.007	1.385	0.024
6.562	1.372	0.006	1.227	0.005	1.271	0.004	1.283	0.005	1.184	0.011	1.251	0.008	1.210	0.007	1.384	0.024
6.596	1.368	0.000	1.225	0.005	1.268	0.004	1.282	0.005	1.181	0.011	1.248	0.007	1.208	0.007	1.381	0.024
6.614	1.365	0.006	1.224	0.005	1.266	0.004	1.281	0.005	1.179	0.011	1.246	0.007	1.207	0.007	1.379	0.024
6.631	1.363	0.006	1.223	0.005	1.265	0.004	1.280	0.005	1.176	0.011	1.245	0.007	1.200	0.007	1.376	0.024
6.667	1.351	0.000	1.222	0.005	1.263	0.004	1.278	0.006	1.174	0.012	1.241	0.007	1.203	0.007	1.375	0.025
6.685	1.357	0.007	1.221	0.005	1.260	0.005	1.277	0.006	1.172	0.012	1.240	0.007	1.202	0.008	1.373	0.025
6.702	1.354	0.007	1.220	0.005	1.258	0.005	1.276	0.006	1.170	0.012	1.238	0.007	1.201	0.008	1.372	0.025
6.739	1.332	0.007	1.219	0.006	1.255	0.005	1.273	0.006	1.166	0.013	1.234	0.008	1.199	0.008	1.369	0.025
6.757	1.347	0.007	1.217	0.006	1.253	0.005	1.272	0.006	1.164	0.013	1.232	0.008	1.197	0.008	1.367	0.026
6.775	1.344	0.007	1.216	0.006	1.251	0.005	1.271	0.006	1.162	0.013	1.231	0.008	1.190	0.008	1.300	0.026
6.793 6.812	1.342	0.007	1.215	0.006	1.249	0.005	1.269	0.000	1.158	0.013	1.227	0.008	1.194	0.008	1.363	0.026
6.831	1.337	0.008	1.213	0.006	1.245	0.005	1.268	0.006	1.156	0.014	1.225	0.008	1.193	0.008	1.361	0.027
6.849	1.334	0.008	1.212	0.006	1.244	0.005	1.267	0.006	1.153	0.014	1.223	0.009	1.191	0.008	1.359	0.027
6.868 6.887	1.331	0.008	1.211	0.005	1.242	0.005	1.200	0.007	1.131	0.014	1.219	0.009	1.189	0.008	1.356	0.028
6.906	1.326	0.008	1.208	0.007	1.237	0.006	1.263	0.007	1.146	0.015	1.217	0.009	1.188	0.009	1.355	0.028
6.925	1.323	0.008	1.207	0.007	1.235	0.006	1.262	0.007	1.144	0.015	1.214	0.009	1.186	0.009	1.353	0.028
6.944 6.964	1.320	0.008	1.206	0.007	1.233	0.006	1.251	0.007	1.142	0.015	1.212	0.010	1.185	0.009	1.349	0.029
6.983	1.314	0.009	1.200	0.007	1.229	0.006	1.258	0.007	1.136	0.016	1.208	0.010	1.182	0.009	1.348	0.030
7.003	1.311	0.009	1.202	0.007	1.227	0.006	1.257	0.007	1.134	0.016	1.205	0.010	1.181	0.009	1.346	0.030
7.023	1.308	0.009	1.201	0.008	1.224	0.006	1.255	0.008	1.131	0.017	1.203	0.010	1.179	0.009	1.344	0.031
7.042	1.301	0.009	1.198	0.008	1.220	0.006	1.253	0.008	1.125	0.017	1.198	0.011	1.176	0.010	1.340	0.031
7.082	1.298	0.010	1.197	0.008	1.217	0.007	1.251	0.008	1.122	0.018	1.195	0.011	1.175	0.010	1.339	0.032
7.102	1.295	0.010	1.196	0.008	1.215	0.007	1.250	0.008	1.120	0.018	1.193	0.011	1.173	0.010	1.337	0.033
7.143	1.288	0.010	1.193	0.009	1.210	0.007	1.247	0.008	1.113	0.019	1.187	0.012	1.170	0.011	1.333	0.034
7.163	1.284	0.010	1.191	0.009	1.207	0.007	1.245	0.009	1.110	0.020	1.185	0.012	1.168	0.011	1.331	0.034
7.184	1.281	0.011	1.190	0.009	1.204	0.007	1.244	0.009	1.107	0.020	1.182	0.013	1.167	0.011	1.329	0.035
7.225	1.273	0.011	1.187	0.010	1.199	0.008	1.240	0.009	1.100	0.021	1.176	0.013	1.163	0.011	1.325	0.036
7.246	1.270	0.011	1.185	0.010	1.196	0.008	1.239	0.009	1.096	0.021	1.173	0.014	1.161	0.012	1.323	0.037
7.267	1.265	0.012	1.183	0.010	1.193	0.008	1.237	0.009	1.092	0.022	1.169	0.014	1.100	0.012	1.321	0.037
7.310	1.257	0.012	1.182	0.011	1.187	0.008	1.234	0.010	1.085	0.023	1.163	0.015	1.156	0.012	1.316	0.039
7.331	1.253	0.012	1.178	0.011	1.183	0.009	1.232	0.010	1.081	0.024	1.159	0.015	1.154	0.013	1.314	0.040
7.353	1.249	0.013	1.176	0.011	1.180	0.009	1.230	0.010	1.070	0.024	1.150	0.015	1.152	0.013	1.312	0.041
7.396	1.245	0.013	1.174	0.012	1.173	0.009	1.226	0.011	1.068	0.026	1.148	0.016	1.148	0.013	1.307	0.042
7.418	1.235	0.014	1.171	0.012	1.170	0.010	1.224	0.011	1.063	0.027	1.145	0.017	1.146	0.014	1.304	0.043
7.440	1.231	0.014	1.168	0.013	1.166	0.010	1.222	0.011	1.058	0.027	1.141	0.017	1.143	0.014	1.302	0.044
7.403 7.485	1.220	0.014	1.164	0.013	1.159	0.010	1.218	0.012	1.048	0.029	1.132	0.018	1.139	0.015	1.297	0.046
7.508	1.216	0.015	1.162	0.014	1.155	0.011	1.216	0.012	1.043	0.030	1.128	0.019	1.137	0.015	1.294	0.047
7.530	1.211	0.016	1.160	0.014	1.151	0.011	1.214	0.012	1.038	0.031	1.124	0.020	1.134	0.016	1.292	0.048
7.503	1.205	0.010	1.155	0.015	1.147	0.012	1.209	0.012	1.032	0.033	1.114	0.021	1.129	0.016	1.286	0.050
7.599	1.194	0.017	1.153	0.016	1.138	0.012	1.207	0.013	1.020	0.034	1.109	0.022	1.127	0.017	1.283	0.052
7.622	1.189	0.018	1.150	0.016	1.133	0.012	1.205	0.013	1.014	0.035	1.104	0.023	1.124	0.017	1.280	0.053
7.645 7.669	1.183	0.018	1.148	0.017	1.129	0.013	1.202	0.014	1.000	0.037	1.094	0.023	1.119	0.018	1.274	0.054
7.692	1.170	0.019	1.142	0.018	1.119	0.013	1.197	0.014	0.993	0.039	1.088	0.025	1.116	0.019	1.271	0.057
7.716	1.164	0.020	1.140	0.019	1.114	0.014	1.195	0.015	0.986	0.041	1.082	0.026	1.113	0.019	1.268	0.058
7.740	1.157	0.020	1.137	0.020	1.109	0.014	1.192	0.015	0.978	0.043	1.076	0.027 0.028	1.110	0.020	1.265	0.060
7.788	1.151	0.021	1.134	0.020	1.098	0.015	1.186	0.016	0.961	0.046	1.063	0.029	1.103	0.021	1.258	0.063
7.813	1.136	0.022	1.127	0.022	1.092	0.016	1.184	0.016	0.952	0.049	1.056	0.031	1.100	0.022	1.255	0.065
7.837	1.129	0.023	1.124	0.023	1.086	0.016	1.181	0.017	0.943	0.051	1.049	0.032	1.097	0.022	1.251	0.067
7.862	1.121	0.024	1.120	0.024	1.073	0.017	1.178	0.017	0.933	0.056	1.042	0.034	1.089	0.023	1.244	0.009
7.911	1.105	0.026	1.113	0.026	1.066	0.018	1.171	0.018	0.912	0.059	1.026	0.037	1.086	0.025	1.240	0.073
7.937	1.097	0.027	1.110	0.027	1.059	0.019	1.168	0.019	0.900	0.062	1.018	0.039	1.082	0.026	1.236	0.075
7.962	1.088	0.028	1.105	0.028	1.052	0.020	1.104	0.019	v.000	0.003	1.009	0.041	1.010	0.020	1.202	0.017

	Orthop	roxene			6. AI	PPEN		-Con	tinuec	t					
SI	ab	Pow	der	Kaol	inite	Serpe	ntine	Pyrop	hyllite	Montm	orillonite	Sapo	onite	Palag	ronite
	k	n	k	n	k	n	k	n .	k	n	k	n	k	n	k
79	0.029	1.101	0.030	1.045	0.021	1.161	0.020	0.875	0.069	1.000	0.043	1.074	0.027	1.228	0.080
69	0.030	1.097	0.031	1.037	0.021	1.157	0.020	0.861	0.074	0.990	0.045	1.069	0.028	1.224	0.082
59	0.032	1.093	0.033	1.029	0.022	1.153	0.021	0.847	0.078	0.980	0.048	1.065	0.029	1.219	0.085
49	0.033	1.088	0.034	1.020	0.023	1.150	0.022	0.831	0.084	0.969	0.050	1.060	0.031	1.215	0.088
38	0.035	1.083	0.036	1.011	0.024	1.146	0.023	0.814	0.090	0.957	0.053	1.055	0.032	1.211	0.091
27	0.036	1.078	0.038	1.002	0.026	1.141	0.023	0.797	0.097	0.945	0.057	1.050	0.033	1.206	0.094
16	0.038	1.073	0.040	0.992	0.027	1.137	0.024	0.777	0.105	0.933	0.061	1.045	0.034	1.201	0.097
04	0.040	1.068	0.042	0.981	0.028	1.133	0.025	0.757	0.114	0.919	0.065	1.040	0.036	1.196	0.100
91	0.042	1.062	0.045	0.971	0.030	1.128	0.026	0.735	0.125	0.905	0.070	1.034	0.037	1.191	0.104
78	0.044	1.056	0.048	0.959	0.031	1.123	0.027	0.711	0.137	0.890	0.075	1.028	0.039	1.186	0.108
c .	0.047	1 050	0.050	0.047	0.012	1 1 1 0	0.000	0.005	0.150	0.074	0.001	1 000	0.041		

(m.g.m)         p.         k         n <n< th="">         k         n</n<>	wavelength	Sl	ab	Pow	/der	Kaol	inite	Serpe	entine	Pyrop	hyllite	Montr	orillonite	Sapo	onite	Palag	gonite
7.887         1.679         0.629         1.610         0.030         1.030         0.031         1.037         0.027         1.280         0.038         1.036         0.027         1.280         0.038         1.035         0.027         1.280         0.038         0.033         0.030         0.032         0.135         0.030         0.033         0.030         0.033         0.030         0.033         0.030         0.033         0.030         0.033         0.030         0.033         0.030         0.033         0.030         0.033         0.033         0.030         0.033         0.033         0.030         0.033         0.031         0.031         0.033         0.031         0.031         0.031         0.031         0.033         0.031         0.031 <th< td=""><td>(in µm)</td><td>n</td><td><u>k</u></td><td>n</td><td>k</td><td>n</td><td>k</td><td>n</td><td>k</td><td>n</td><td>k</td><td>n</td><td>k</td><td>n</td><td>k</td><td>n</td><td>k</td></th<>	(in µm)	n	<u>k</u>	n	k	n	k	n	k	n	k	n	k	n	k	n	k
8.013         1.689         0.032         1.047         0.031         1.047         0.031         1.047         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.045         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.031         1.046         0.041         1.046         0.041         1.046         0.041         1.046         0.041         1.046         0.041         1.046         0.041         1.046         0.041         1.046         0.041         1.046         0.041         1.046 <th< td=""><td>7.987</td><td>1.079</td><td>0.029</td><td>1.101</td><td>0.030</td><td>1.045</td><td>0.021</td><td>1.161</td><td>0.020</td><td>0.875</td><td>0.069</td><td>1.000</td><td>0.043</td><td>1.074</td><td>0.027</td><td>1.228</td><td>0.080</td></th<>	7.987	1.079	0.029	1.101	0.030	1.045	0.021	1.161	0.020	0.875	0.069	1.000	0.043	1.074	0.027	1.228	0.080
BAGE         ICAD         DUAL         LUGB         DUAL         LUGB         DUAL         LUGB         DUAL         LUGB         DUAL         LUGB         DUAL         DUAL <thdual< th="">         DUAL         DUAL         <thd< td=""><td>8.013</td><td>1.069</td><td>0.030</td><td>1.097</td><td>0.031</td><td>1.037</td><td>0.021</td><td>1.157</td><td>0.020</td><td>0.861</td><td>0.074</td><td>0.990</td><td>0.045</td><td>1.069</td><td>0.028</td><td>1.224</td><td>0.082</td></thd<></thdual<>	8.013	1.069	0.030	1.097	0.031	1.037	0.021	1.157	0.020	0.861	0.074	0.990	0.045	1.069	0.028	1.224	0.082
BOR         103         0.03         103         0.0	8.039	1.059	0.032	1.093	0.033	1.029	0.022	1.153	0.021	0.847	0.078	0.980	0.048	1.060	0.029	1.219	0.085
8.117         1.027         0.038         1.078         0.038         0.078         0.047         0.077         0.145         0.077         0.045         0.077         0.045         0.077         0.045         0.077         0.045         0.077         0.045         0.077         0.045         0.038 <th< td=""><td>8.091</td><td>1.038</td><td>0.035</td><td>1.083</td><td>0.036</td><td>1.011</td><td>0.024</td><td>1.146</td><td>0.022</td><td>0.814</td><td>0.090</td><td>0.957</td><td>0.053</td><td>1.055</td><td>0.032</td><td>1.211</td><td>0.091</td></th<>	8.091	1.038	0.035	1.083	0.036	1.011	0.024	1.146	0.022	0.814	0.090	0.957	0.053	1.055	0.032	1.211	0.091
8.143       1016       0.040       1.087       0.040       0.087       0.087       0.133       0.027       0.135       0.027       0.037       0.040       0.085       0.038       1.196       0.100         8.170       1.004       0.040       0.040       0.040       0.040       0.055       0.017       0.125       0.025       0.055       0.017       0.125       0.026       0.025       0.026       0.035       0.031       1.186       0.028       0.031       0.031       0.05       0.017       0.117       0.157       0.017       0.118       0.018       0.031       0.037       0.118       0.026       0.027       0.120       0.051       0.017       0.116       0.041       1.170       0.117       0.155       0.085       0.060       0.027       0.021       0.085       0.060       0.021       0.021       0.051       0.014       0.015       0.051       0.016       0.027       0.041       0.025       0.041       0.0	8.117	1.027	0.036	1.078	0.038	1.002	0.026	1.141	0.023	0.797	0.097	0.945	0.057	1.050	0.033	1.206	0.094
8.170         100         0.042         0.085         0.042         0.085         0.042         0.085         0.042         0.085         0.045         0.071         0.084         0.007         1.186         0.108           8.274         0.574         0.054         0.055	8.143	1.016	0.038	1.073	0.040	0.992	0.027	1.137	0.024	0.777	0.105	0.933	0.061	1.045	0.034	1.201	0.097
8/17         0.94         0.94         0.93         0.13         0.13         0.90         0.14         0.90         0.14         0.90         0.91         0.13         0.15         0.90         0.91         0.13         0.14 <th< td=""><td>8.170</td><td>1.004</td><td>0.040</td><td>1.068</td><td>0.042</td><td>0.981</td><td>0.028</td><td>1.133</td><td>0.025</td><td>0.757</td><td>0.114</td><td>0.919</td><td>0.065</td><td>1.040</td><td>0.036</td><td>1.196</td><td>0.100</td></th<>	8.170	1.004	0.040	1.068	0.042	0.981	0.028	1.133	0.025	0.757	0.114	0.919	0.065	1.040	0.036	1.196	0.100
8.275         0.584         0.647         0.613         1.118         0.013         0.112         0.024         0.634         1.162         0.013         1.162         0.013         1.162         0.013         1.162         0.013         1.162         0.013         1.162         0.014         1.160         0.116         0.054         0.055         0.054         0.054 <th< td=""><td>8.197</td><td>0.991</td><td>0.042</td><td>1.062</td><td>0.045</td><td>0.971</td><td>0.030</td><td>1.128</td><td>0.026</td><td>0.735</td><td>0.125</td><td>0.905</td><td>0.070</td><td>1.034</td><td>0.037</td><td>1.191</td><td>0.104</td></th<>	8.197	0.991	0.042	1.062	0.045	0.971	0.030	1.128	0.026	0.735	0.125	0.905	0.070	1.034	0.037	1.191	0.104
8276         0390         0.651         0394         0395         113         0.029         0.675         0.176         0.187         0.088         0.096         0.049         1.176         0.117         0.117         0.117         0.117         0.117         0.117         0.118           8.330         0.918         0.665         1.007         0.065         0.980         0.641         1.017         0.017         0.161         1.007         0.017         0.118         0.138         0.988         0.981 <td>8 251</td> <td>0.978</td> <td>0.044</td> <td>1.050</td> <td>0.048</td> <td>0.959</td> <td>0.031</td> <td>1.123</td> <td>0.027</td> <td>0.685</td> <td>0.157</td> <td>0.890</td> <td>0.075</td> <td>1.028</td> <td>0.039</td> <td>1.180</td> <td>0.108</td>	8 251	0.978	0.044	1.050	0.048	0.959	0.031	1.123	0.027	0.685	0.157	0.890	0.075	1.028	0.039	1.180	0.108
8.36       9.94       0.65       1.00       0.05       1.00       0.05       0.10       0.05       1.00       0.05       1.00       0.05       1.00       0.05       1.00       0.05       1.00       0.05       1.10       0.15       0.16       0.16       0.05       0.17       0.16       0.14       0.05       0.17       0.05       0.17       0.05       0.17       0.05       0.17       0.05       0.16       0.16       0.15	8.278	0.950	0.050	1.043	0.054	0.934	0.035	1.113	0.029	0.657	0.170	0.856	0.088	1.016	0.043	1.176	0.116
8.33         0.918         0.056         1.000         0.066         1.027         0.016         1.007         0.016         1.007         0.016         1.007         0.016         1.007         0.016         1.007         0.016         1.007         0.016         1.007         0.016         1.017         0.116         0.123         0.838         0.066         1.014         0.016         0.837         0.848         0.818         0.016         0.108         0.027         0.108         0.027         0.105         1.117         0.148           8.440         0.843         0.074         0.857         0.054         1.077         0.038         0.470         0.038         0.470         0.038         0.470         0.038         0.470         0.044         0.440         0.441         0.440         0.41	8.306	0.934	0.053	1.037	0.057	0.921	0.038	1.108	0.030	0.627	0.192	0.838	0.096	1.009	0.045	1.170	0.121
8.380         0.890         0.090         0.090         1.097         0.033         0.844         0.280         0.777         0.116         0.985         0.050         1.158         0.133         0.138         0.138         0.116         0.985         0.055         1.158         0.133         0.158         0.141         0.055         0.156         0.157         0.158         0.158         0.164         0.055         0.158         0.156         0.157         0.055         0.171         0.056         0.051 <th< td=""><td>8.333</td><td>0.918</td><td>0.056</td><td>1.030</td><td>0.061</td><td>0.906</td><td>0.040</td><td>1.102</td><td>0.032</td><td>0.596</td><td>0.218</td><td>0.818</td><td>0.105</td><td>1.002</td><td>0.047</td><td>1.164</td><td>0.125</td></th<>	8.333	0.918	0.056	1.030	0.061	0.906	0.040	1.102	0.032	0.596	0.218	0.818	0.105	1.002	0.047	1.164	0.125
a.s.a.g         b.s.a.g         b.s.a.g <t< td=""><td>8.361</td><td>0.901</td><td>0.060</td><td>1.022</td><td>0.065</td><td>0.891</td><td>0.043</td><td>1.097</td><td>0.033</td><td>0.564</td><td>0.250</td><td>0.797</td><td>0.116</td><td>0.995</td><td>0.050</td><td>1.159</td><td>0.131</td></t<>	8.361	0.901	0.060	1.022	0.065	0.891	0.043	1.097	0.033	0.564	0.250	0.797	0.116	0.995	0.050	1.159	0.131
8446         0.843         0.747         0.938         0.747         0.038         0.747         0.038         0.747         0.038         0.748         0.068         0.711         0.056         0.711         0.056         0.711         0.056         0.711         0.056         0.711         0.056         0.711         0.056         0.711         0.056         0.041         0.743         0.044         0.044         0.044         0.044         0.044         0.044         0.045         0.650         0.621         0.282         0.922         0.056         0.101         0.102         0.110         0.102         0.110         0.120         0.110         0.120         0.101         0.120         0.101         0.120         0.110         0.102         0.101         0.120         0.102         0.105         0.577         0.484         0.757         0.478         0.886         0.100         0.108         0.121         0.102         0.55         0.577         0.484         0.871         0.552         0.577         0.478         0.885         0.108         0.108         0.128         0.108         0.128         0.108         0.128         0.108         0.128         0.108         0.128         0.110         0.183         0	0.309 8 417	0.863	0.004	1.014	0.076	0.874	0.040	1.091	0.034	0.532	0.289	0.774	0.129	0.987	0.052	1.103	0.130
8.475         0.822         0.080         0.890         0.881         0.662         1.071         0.440         0.450         0.451         0.450         0.452         0.462         0.450         0.462         0.440         0.450         0.642         0.440         0.450         0.642         0.440         0.450         0.645         0.741         0.650         0.672         0.220         0.675         0.118         0.743         0.070         0.120         0.040         0.444         0.474         0.550         0.681         0.616         0.621         0.230         0.646         0.453         0.650         0.621         0.375         0.486         0.377         0.448         0.101         0.102         0.104         0.102         0.550         0.650         0.621         0.575         0.448         0.577         0.448         0.575         0.448         0.571         0.448         0.502         0.441         0.120         0.550         0.651         0.671         0.551         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680         0.680 <th< td=""><td>8.446</td><td>0.843</td><td>0.074</td><td>0.998</td><td>0.081</td><td>0.837</td><td>0.054</td><td>1.078</td><td>0.038</td><td>0.478</td><td>0.391</td><td>0.725</td><td>0.163</td><td>0.970</td><td>0.058</td><td>1.141</td><td>0.148</td></th<>	8.446	0.843	0.074	0.998	0.081	0.837	0.054	1.078	0.038	0.478	0.391	0.725	0.163	0.970	0.058	1.141	0.148
8.502         0.798         0.087         0.980         0.080         0.910         0.061         0.064         0.447         0.822         0.044         0.942         0.071         0.112         0.116         0.112         0.116         0.117         0.116         0.117         0.116         0.117         0.116         0.117         0.116         0.117         0.116         0.117         0.116         0.117         0.116         0.117         0.116         0.117         0.117         0.117         0.117         0.117         0.117         0.117         0.117         0.116         0.117         0.117         0.117         0.118         0.118         0.117         0.118         0.118         0.118         0.117         0.118         0.118         0.117         0.118         0.118         0.117         0.118         0.118         0.117         0.118         0.118         0.117         0.118         0.118         0.111         0.111         0.117         0.118         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.111         0.1111         0.111         0.111 <t< td=""><td>8.475</td><td>0.822</td><td>0.080</td><td>0.989</td><td>0.088</td><td>0.817</td><td>0.059</td><td>1.071</td><td>0.040</td><td>0.459</td><td>0.451</td><td>0.699</td><td>0.185</td><td>0.962</td><td>0.062</td><td>1.135</td><td>0.154</td></t<>	8.475	0.822	0.080	0.989	0.088	0.817	0.059	1.071	0.040	0.459	0.451	0.699	0.185	0.962	0.062	1.135	0.154
8.562         0.773         0.085         0.970         0.104         0.770         0.071         1.056         0.044         0.244         0.242         0.942         0.771         1.105         0.113         0.171         0.111         0.111         0.113         0.171         0.011         0.040         0.045         0.050         0.242         0.942         0.971         0.180         0.185         0.661         0.102         0.181         0.175         0.980         0.080         0.100         0.191         0.185         0.611         0.102         0.144         0.107         0.147         0.980         0.340         0.377         0.980         0.501         0.445         0.377         0.426         0.880         0.108         0.214           8.711         0.657         0.270         0.890         0.220         0.990         0.530         0.577         0.580         0.880         0.108         0.811         1.105         0.250         0.830         0.270         0.530         0.581         0.811         1.105         0.520         0.880         0.18         0.810         0.113         0.721         0.810         0.181         0.816         0.113         0.721         0.810         0.811         0.18	8.503	0.798	0.087	0.980	0.095	0.794	0.064	1.064	0.042	0.449	0.516	0.672	0.212	0.952	0.066	1.128	0.161
8.861         0.147         0.19         0.19         0.049         0.483         0.040         0.282         0.292         0.292         0.292         0.292         0.193         0.110         0.116         0	8.532	0.773	0.095	0.970	0.104	0.770	0.071	1.056	0.044	0.447	0.582	0.645	0.244	0.942	0.070	1.122	0.169
0.648         0.130         0.641         0.130         0.640         0.101         1.031         0.642         0.844         0.782         0.845         0.375         0.476         0.866         0.092         1.030         0.845           8.561         0.616         0.500         0.149         0.661         0.140         0.101         1.022         0.550         0.845         0.877         0.476         0.866         0.022         0.810         0.888         0.101         0.888         0.101         0.888         0.101         0.888         0.101         0.857         0.127         0.570         0.476         0.888         0.181         0.570         0.581         0.847         0.581         0.847         0.551         0.857         0.121         0.163         0.562         0.877         0.131         0.162         0.625         0.887         0.181         0.502         0.564         0.879         0.181         0.151         0.563         0.877         0.574         0.880         0.181         0.502         0.877         0.574         0.883         0.181         0.570         0.524         0.877         0.575         0.171         1.051         0.563         0.877         0.783         0.774         0.7	8.002	0.747	0.105	0.961	0.113	0.743	0.079	1.048	0.040	0.455	0.000	0.621	0.282	0.932	0.075	1.115	0.177
8.651         0.652         0.147         0.330         0.149         0.443         0.119         1.022         0.055         0.577         0.478         0.886         0.002         1.085         0.214           8.711         0.577         0.150         0.911         0.182         0.550         0.174         1.002         0.063         0.543         0.977         0.576         0.588         0.086         0.018         1.082         0.223           8.712         0.450         0.230         0.661         0.670         0.984         1.044         1.682         0.237           8.722         0.496         0.271         0.886         0.237         0.436         0.774         0.731         1.043         1.682         0.234           8.830         0.497         0.886         0.330         0.426         0.633         0.427         0.571         0.484         0.430         0.171         1.010         8.26         0.774         0.730         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.784         0.774         0.734	8.621	0.686	0.130	0.941	0.124	0.680	0.102	1.031	0.052	0.484	0.782	0.585	0.375	0.920	0.086	1.108	0.185
8.681         0.616         0.169         0.220         0.165         0.610         1.042         1.012         0.050         0.230         0.530         0.868         0.106         1.082         0.221           8.711         0.537         0.229         0.920         0.506         0.220         0.901         0.671         0.583         0.853         0.118         1.052         0.233           8.741         0.537         0.229         0.850         0.227         0.430         0.477         0.730         0.661         0.623         0.811         1.162         0.483           8.830         0.450         0.886         0.277         0.430         0.477         0.875         0.178         0.785         0.177         0.733         0.777         0.738         0.775         0.778         0.785         0.177         0.730         0.767         0.189         1.040         0.551         0.551         0.875         0.141         0.571         0.747         0.734         0.551         0.433         0.795         0.421         0.116         0.551         0.875         0.141         0.595         0.841         0.717         0.734         0.521         0.323         0.401         0.333         0.363	8.651	0.652	0.147	0.930	0.149	0.643	0.119	1.022	0.055	0.507	0.845	0.577	0.426	0.896	0.092	1.095	0.204
8.711         0.577         0.195         0.911         0.182         0.555         0.174         1.002         0.063         0.563         0.979         0.573         0.580         0.868         0.108         1.022         0.523           8.772         0.466         0.271         0.885         0.223         0.461         0.270         0.799         0.73         0.649         1.126         0.620         0.681         0.827         0.128         0.77         0.791         0.731         1.206         0.523         0.686         0.034         0.143         1.626         0.274           8.845         0.410         0.456         0.386         0.386         0.397         0.586         0.390         0.586         0.771         1.70         0.734         0.767         0.198         1.646         0.310         0.288         1.037         0.341         0.322         0.410         0.328         0.374         0.325         0.827         0.131         1.105         1.388         0.771         0.734         0.224         1.041         0.328           8.991         0.440         0.575         0.666         0.480         0.575         0.414         0.575         0.414         0.532         1.410	8.681	0.616	0.169	0.920	0.165	0.601	0.142	1.012	0.059	0.534	0.907	0.575	0.478	0.883	0.100	1.088	0.214
8/71       0.537       0.229       0.902       0.201       0.506       0.220       0.991       0.077       0.598       1.044       0.587       0.833       0.118       1.075       0.237         8.830       0.459       0.324       0.886       0.237       0.433       0.374       0.997       0.731       1.206       0.623       0.742       0.837       0.143       1.062       0.548         8.840       0.420       0.586       0.587       0.567       0.568       0.992       0.771       0.780       0.785       0.171       1.051       0.548         8.857       0.402       0.528       0.669       0.528       0.992       0.114       1.371       1.130       0.326       0.777       0.750       0.224       1.041       0.328         8.951       0.440       0.667       0.669       0.688       0.804       0.844       0.779       0.767       0.750       0.224       1.041       0.325         9025       0.411       0.780       0.881       0.848       0.804       0.848       0.824       0.779       0.677       0.730       0.341       0.333       0.333       0.343       0.368       0.461       0.571       0.561	8.711	0.577	0.195	0.911	0.182	0.555	0.174	1.002	0.063	0.563	0.972	0.579	0.530	0.868	0.108	1.082	0.225
8/12         0.446         0.211         0.889         0.223         0.443         0.324         0.947         0.073         0.128         0.041         0.833         0.129         1.069         0.220         0.243         0.341         0.045         0.839         1.224         0.663         0.671         0.671         0.672         0.683         0.124         0.663         0.774         0.785         0.774         0.785         0.774         0.750         0.224         1.031         0.33         0.826         0.774         0.750         0.224         1.031         0.333         0.826         0.774         0.750         0.224         1.031         0.333         0.826         0.774         0.750         0.224         1.031         0.343         0.826         0.774         0.750         0.224         1.031         0.333         0.824         0.760         0.767         0.761         0.325         1.034         0.385         1.210         0.866         0.844         0.380         0.835         1.210         0.866         0.844         0.380         0.835         1.210         0.866         0.844         0.380         0.330         0.313         0.333         0.312         0.303         0.312         0.303         0	8.741	0.537	0.229	0.902	0.201	0.506	0.220	0.991	0.067	0.598	1.044	0.587	0.582	0.853	0.118	1.075	0.237
0.200         0.429         0.327         0.436         0.475         0.984         0.085         0.839         1.224         0.635         0.742         0.836         0.171         1.051         0.166         0.718           8.885         0.410         0.466         0.886         0.300         0.479         0.572         0.940         0.928         1.288         0.716         0.786         0.777         0.793         0.767         0.189         1.046         0.310           8.929         0.406         0.599         0.889         0.329         0.582         0.181         1.151         1.386         0.877         0.774         0.750         0.224         1.041         0.323           8.931         0.440         0.667         0.886         0.882         0.818         0.824         0.779         0.677         0.750         0.224         1.041         0.353         0.333         0.388         0.848         0.818         0.824         0.497         0.877         0.397         0.303         0.333         0.888         0.414         0.971         0.768         0.722         0.391         0.333         0.333         0.320         0.588         0.389         1.382         0.581         0.593	8.803	0.490	0.271	0.890	0.223	0.401	0.287	0.979	0.073	0.049	1.120	0.601	0.030	0.837	0.129	1.069	0.250
8.885         0.410         0.456         0.886         0.300         0.479         0.572         0.940         0.928         1.288         0.716         0.728         0.171         1.551         0.528           8.897         0.406         0.539         0.886         0.320         0.567         0.568         0.920         0.114         1.377         1.130         0.826         0.774         0.750         0.224         1.031           8.961         0.440         0.667         0.939         0.685         0.478         0.537         0.875         1.144         0.377         0.774         0.724         0.716         0.324         1.031         0.334         0.385         0.418         0.885         0.428         0.885         0.424         0.332         0.410         0.88         0.824         0.774         0.716         0.322         0.281         0.441         0.481         0.885         1.210         0.724         0.718         0.716         0.322         0.810         0.331         0.51         0.505         1.050         0.503         0.481         0.350         0.351         0.56         0.503         0.581         0.585         0.585         0.585         0.585         0.585         0.585	8.834	0.429	0.387	0.886	0.247	0.436	0.475	0.954	0.075	0.839	1.254	0.663	0.031	0.803	0.143	1.002	0.204
8.897       0.402       0.528       0.896       0.359       0.667       0.628       0.999       1.14       1.377       1.30       0.826       0.737       0.738       0.765       0.224       1.041       0.328         8.961       0.420       0.667       0.286       0.578       0.899       0.148       1.021       0.366       0.444       0.864       0.737       0.734       0.254       1.031       0.364         8.993       0.443       0.728       0.221       0.413       0.666       0.844       0.881       0.881       0.844       0.716       0.322       1.033       0.384         9.058       0.447       0.825       0.580       0.446       0.881       1.249       0.681       0.718       0.716       0.322       1.033       0.433         9.018       0.586       0.810       0.440       0.310       0.520       0.532       0.521       1.625       1.626       0.301       1.046       0.533       0.322       0.681       0.824       1.104       0.711       0.534       1.046       0.533       0.325       1.621       1.626       0.630       0.311       0.557       0.341       1.528       0.635       0.641       1.711 <td>8.865</td> <td>0.410</td> <td>0.456</td> <td>0.886</td> <td>0.300</td> <td>0.479</td> <td>0.572</td> <td>0.940</td> <td>0.094</td> <td>0.928</td> <td>1.288</td> <td>0.716</td> <td>0.780</td> <td>0.785</td> <td>0.177</td> <td>1.051</td> <td>0.294</td>	8.865	0.410	0.456	0.886	0.300	0.479	0.572	0.940	0.094	0.928	1.288	0.716	0.780	0.785	0.177	1.051	0.294
8292       0.466       0.599       0.896       0.628       0.902       0.114       1.317       1.130       0.826       0.774       0.734       0.224       1.041       0.327         8.993       0.442       0.728       0.927       0.413       0.685       0.444       0.935       0.776       0.726       0.724       0.288       1.033       0.388         9.055       0.471       0.780       0.825       0.939       0.462       0.516       0.886       0.881       0.881       0.841       0.776       0.722       0.288       1.033       0.888       9.058       0.467       0.885       0.461       0.884       0.484       0.413       0.884       0.835       1.212       0.724       0.718       0.722       0.372       1.035       0.443       0.484       0.431       0.484       0.433       0.441       0.486       0.444       0.437       0.431       0.444       0.446       0.440       0.446       0.440       0.446       0.440       0.446       0.440       0.441       0.446       0.441       0.446       0.441       0.446       0.441       0.446       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.44	8.897	0.402	0.528	0.889	0.329	0.567	0.636	0.925	0.103	1.105	1.368	0.777	0.793	0.767	0.198	1.046	0.310
8.993         0.420         0.0667         0.991         0.138         0.892         0.128         1.210         0.866         0.844         0.737         0.734         0.254         1.037         0.374         0.374         0.137         0.134         0.254         1.037         0.374         0.375         0.258         1.034         0.386         0.844         0.750         0.722         0.877         0.716         0.322         1.033         0.386           9.058         0.477         0.858         0.984         0.484         0.831         0.522         1.055         0.828         0.212         0.774         0.718         0.716         0.322         1.033         0.332         0.348         0.161         0.780         0.722         0.397         0.333         0.44         0.438         0.444         0.430         0.432         0.433         0.443         0.443         0.443         0.443         0.443         0.444         0.446         0.444         0.446         0.434         0.446         0.444         0.444         0.444         0.444         0.444         0.444         0.444         0.444         0.446         0.445           9.120         0.160         1.075         0.360         0.322 </td <td>8.929</td> <td>0.406</td> <td>0.599</td> <td>0.896</td> <td>0.358</td> <td>0.669</td> <td>0.628</td> <td>0.909</td> <td>0.114</td> <td>1.377</td> <td>1.130</td> <td>0.826</td> <td>0.774</td> <td>0.750</td> <td>0.224</td> <td>1.041</td> <td>0.328</td>	8.929	0.406	0.599	0.896	0.358	0.669	0.628	0.909	0.114	1.377	1.130	0.826	0.774	0.750	0.224	1.041	0.328
0.743         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.740         0.741         0.741         0.741 <td< td=""><td>8.901</td><td>0.420</td><td>0.667</td><td>0.907</td><td>0.386</td><td>0.718</td><td>0.553</td><td>0.892</td><td>0.128</td><td>1.210</td><td>0.866</td><td>0.844</td><td>0.737</td><td>0.734</td><td>0.254</td><td>1.037</td><td>0.347</td></td<>	8.901	0.420	0.667	0.907	0.386	0.718	0.553	0.892	0.128	1.210	0.866	0.844	0.737	0.734	0.254	1.037	0.347
9.058         0.497         0.825         0.959         0.462         0.514         0.466         0.841         0.188         0.835         1.212         0.724         0.718         0.716         0.362         1.032         0.430           9.051         0.518         0.968         0.944         0.431         0.520         0.823         0.216         0.830         0.161         0.722         0.370         0.611         0.810         0.825         1.055         0.630         0.831         0.741         0.446         0.400         0.830         0.351         0.660         0.331         0.741         0.446         0.400         0.529         0.329         1.289         1.683         0.609         1.139         0.738         0.481         1.050         0.530           9.259         0.728         1.061         0.542         0.300         0.320         1.122         0.830         1.651         1.631         0.432         1.101         0.531         0.726         0.565         0.661         1.134         0.537         0.341         1.230         0.131         0.731         0.343         1.231         1.411         0.633         1.421         0.111         0.636         1.144         0.636         1.144 </td <td>9.025</td> <td>0.443</td> <td>0.780</td> <td>0.939</td> <td>0.413</td> <td>0.606</td> <td>0.448</td> <td>0.858</td> <td>0.144</td> <td>0.868</td> <td>1.020</td> <td>0.779</td> <td>0.697</td> <td>0.716</td> <td>0.200</td> <td>1.034</td> <td>0.307</td>	9.025	0.443	0.780	0.939	0.413	0.606	0.448	0.858	0.144	0.868	1.020	0.779	0.697	0.716	0.200	1.034	0.307
9.091       0.518       0.868       0.841       0.424       0.434       0.411       0.632       0.631       0.611       0.678       0.722       0.927       1.033       0.433         9.158       0.566       0.970       1.034       0.520       0.332       0.708       0.819       0.252       1.055       1.663       0.661       0.732       0.425       1.046       1.646       1.671       0.588       1.031       0.743       0.463       1.046       0.442       0.446       0.442       0.446       0.446       0.446       0.446       0.446       0.446       0.430       0.325       1.466       1.671       0.788       1.031       0.734       0.446       0.441       0.549       0.529       0.726       0.505       1.050       0.500       0.778       0.661       1.673       0.687       1.253       0.726       0.505       1.050       0.500       0.532       1.673       0.681       1.419       0.687       0.582       1.093       0.581       0.531       2.532       1.121       0.681       0.613       0.582       1.095       0.561       0.562       1.091       0.551       0.562       1.091       0.551       0.562       1.051       0.562       1	9.058	0.497	0.825	0.959	0.462	0.514	0.466	0.841	0.188	0.835	1.212	0.724	0.718	0.716	0.362	1.032	0.410
9.124       0.538       0.916       1.007       0.503       0.371       0.611       0.819       0.225       1.055       1.663       0.630       0.841       0.732       0.425       1.036       0.460       0.448         9.158       0.566       0.701       1.045       0.533       0.312       0.809       0.830       0.325       1.616       1.633       0.605       1.034       0.443       1.046       0.507         9.259       0.660       1.075       1.099       0.542       0.300       1.12       0.830       0.366       1.841       1.752       0.634       1.372       0.711       0.583       1.095       0.555       0.650       5.050         9.228       0.799       1.120       1.186       0.537       0.340       1.231       0.891       0.351       2.532       1.414       0.684       1.372       0.711       0.538       1.095       0.613       1.334       0.681       1.041       0.681       1.047       0.682       1.065       1.53       1.836       0.683       1.063       1.650       1.838       1.633       0.681       0.661       1.061       1.663       0.551       1.652       0.551       0.560       0.551       1.553 </td <td>9.091</td> <td>0.518</td> <td>0.868</td> <td>0.981</td> <td>0.484</td> <td>0.431</td> <td>0.525</td> <td>0.828</td> <td>0.218</td> <td>0.894</td> <td>1.419</td> <td>0.671</td> <td>0.768</td> <td>0.722</td> <td>0.397</td> <td>1.033</td> <td>0.433</td>	9.091	0.518	0.868	0.981	0.484	0.431	0.525	0.828	0.218	0.894	1.419	0.671	0.768	0.722	0.397	1.033	0.433
9.188       0.566       0.970       1.032       0.708       0.819       0.289       1.289       1.683       0.065       0.931       0.741       0.446       1.040       0.482         9.129       0.605       1.026       1.055       1.053       0.312       0.473       0.661       1.013       0.738       0.441       1.040       0.537         9.259       0.788       1.109       1.134       0.544       0.303       0.112       0.885       0.366       1.631       1.637       0.664       1.077       0.582       1.095       0.563         9.254       0.799       1.120       0.431       1.222       0.890       0.362       2.421       1.431       0.574       1.444       0.567       0.582       1.095       0.613         9.383       0.866       1.017       1.188       0.577       0.340       1.233       0.351       2.516       0.850       0.982       1.631       0.568       0.688       1.131       0.665       0.688       1.133       0.665       0.688       1.135       0.666       0.589       1.140       0.512       1.537       0.561       0.562       1.990       0.561       0.562       1.991       0.563       1.282 </td <td>9.124</td> <td>0.538</td> <td>0.916</td> <td>1.007</td> <td>0.503</td> <td>0.370</td> <td>0.611</td> <td>0.819</td> <td>0.252</td> <td>1.055</td> <td>1.602</td> <td>0.630</td> <td>0.841</td> <td>0.732</td> <td>0.425</td> <td>1.035</td> <td>0.457</td>	9.124	0.538	0.916	1.007	0.503	0.370	0.611	0.819	0.252	1.055	1.602	0.630	0.841	0.732	0.425	1.035	0.457
9.191         0.005         1.026         1.026         1.026         1.039         1.039         1.039         1.039         1.043         0.443         1.045         1.045           9.255         0.660         1.075         1.099         0.242         0.305         0.101         0.352         1.610         1.039         0.139         0.133         0.433         0.463         1.054         0.534           9.254         0.768         1.109         1.138         0.527         0.340         1.22         0.830         0.366         2.163         1.673         0.844         1.372         0.711         0.538         1.079         0.586           9.328         0.860         1.107         1.198         0.527         0.340         1.231         0.351         2.516         0.851         1.617         0.667         0.686         1.191         0.633         1.135         0.636         1.133         0.364         1.131         0.365         0.516         1.135         0.364         1.135         0.364         1.135         0.364         1.135         0.364         1.135         0.364         1.135         0.364         1.135         0.364         1.135         0.364         1.275         0.374	9.158	0.566	0.970	1.034	0.520	0.332	0.708	0.819	0.289	1.289	1.683	0.605	0.931	0.741	0.446	1.040	0.482
0.259         0.728         1.109         1.133         0.544         0.303         0.511         0.105         0.136         1.136         0.139         0.726         0.505         1.066         0.569           9.259         0.778         1.109         1.134         0.537         0.320         1.223         0.889         0.366         2.133         0.737         0.538         1.079         0.586           9.328         0.866         1.071         1.980         0.527         0.340         1.233         0.890         0.351         2.516         0.851         1.617         0.687         0.636         1.114         0.638           9.363         0.896         1.081         1.222         0.510         0.370         1.351         0.831         0.351         2.516         0.851         1.617         0.687         0.636         1.114         0.638         1.063         1.335         0.683         1.061         0.832         0.631         1.335         0.683         0.668         1.135         0.668         0.691         1.335         0.663         0.666         1.60         0.569         1.383         0.615         0.424         0.631         1.335         0.618         1.383         0.711	9.191 9.225	0.660	1.020	1.005	0.533	0.312	0.809	0.830	0.325	1.400	1.071	0.598	1.031	0.743	0.463	1.046	0.507
9.294       0.799       1.120       1.168       0.539       0.320       1.122       0.893       0.366       2.163       1.673       0.684       1.372       0.711       0.538       1.079       0.566         9.328       0.896       1.017       1.198       0.527       0.340       1.233       0.899       0.351       2.522       1.121       0.851       1.617       0.687       0.686       1.114       0.633       0.351       2.512       1.121       0.681       1.617       0.687       0.685       0.681       1.114       0.633       0.676       1.116       0.683       0.611       1.633       1.836       0.693       0.766       1.160       0.664       0.710       0.840       1.866       0.671       0.840       1.186       0.711       0.840       1.186       0.711       0.840       1.186       0.711       0.840       1.186       0.711       0.840       1.186       0.711       0.840       1.186       0.711       0.840       1.186       0.711       0.840       1.735       0.821       1.331       1.815       0.711       0.840       1.735       0.821       1.331       1.815       0.711       0.840       1.735       0.821       1.735       0	9.259	0.728	1.109	1.134	0.544	0.308	1.015	0.875	0.366	1.848	1.752	0.637	1.253	0.726	0.505	1.065	0.534
9.363       0.860       1.07       1.18       0.527       0.340       1.23       0.890       0.358       2.423       1.210       0.551       0.687       0.682       1.031       0.687       0.687       0.682       1.031       0.687       0.687       0.682       1.035       0.686       0.631       0.550       1.53       1.617       0.687       0.636       0.114       0.568         9.434       0.893       1.063       1.248       0.470       0.460       1.615       0.848       0.361       2.441       0.500       1.353       1.836       0.693       0.766       1.160       0.689         9.470       0.887       1.069       1.251       0.460       0.549       1.765       0.821       0.381       2.349       0.500       1.365       1.888       0.711       0.840       1.880       0.772       0.532       2.176       0.410       1.823       1.815       0.744       0.995       1.248       0.757         9.561       1.124       1.266       0.451       1.622       2.764       0.561       1.321       1.42       1.746       1.330       0.773       1.351       8.431       0.773       1.351       8.431       0.773       1.281	9.294	0.799	1.120	1.168	0.539	0.320	1.122	0.893	0.366	2.163	1.673	0.684	1.372	0.711	0.538	1.079	0.586
9.363       0.864       1.081       1.222       0.510       0.370       1.351       0.891       0.351       2.516       0.850       0.982       1.735       0.665       0.698       1.114       0.663         9.399       0.904       1.053       1.243       0.491       0.411       1.478       0.873       0.351       2.516       0.850       0.982       1.735       0.665       0.693       0.766       1.60       0.668         9.470       0.887       1.091       1.251       0.460       0.549       1.755       0.821       0.381       2.344       0.509       1.355       1.898       0.711       0.916       1.216       0.727         9.542       0.992       1.216       1.256       0.451       0.825       2.099       0.772       0.453       2.175       0.341       1.823       1.815       0.784       0.995       1.248       0.784       0.995       1.248       0.771       0.280       1.252       0.786       1.679       0.842       1.073       1.282       0.756         9.653       1.215       1.124       1.281       0.448       1.397       2.757       0.561       1.989       1.242       1.679       0.842       1.578 <td>9.328</td> <td>0.860</td> <td>1.107</td> <td>1.198</td> <td>0.527</td> <td>0.340</td> <td>1.233</td> <td>0.899</td> <td>0.358</td> <td>2.423</td> <td>1.431</td> <td>0.754</td> <td>1.494</td> <td>0.697</td> <td>0.582</td> <td>1.095</td> <td>0.613</td>	9.328	0.860	1.107	1.198	0.527	0.340	1.233	0.899	0.358	2.423	1.431	0.754	1.494	0.697	0.582	1.095	0.613
9.399         0.494         1.059         1.239         0.411         1.478         0.873         0.351         2.516         0.850         0.153         1.356         0.683         0.766         0.663           9.470         0.887         1.099         1.251         0.460         0.549         1.765         0.848         0.361         2.349         0.509         1.355         1.836         0.693         0.761         0.840         0.707           9.542         0.992         1.216         1.256         0.451         0.822         0.907         0.772         0.453         2.175         0.411         1.825         0.744         0.996         1.216         0.726         0.453         2.175         0.411         1.825         0.744         0.995         1.248         0.997         1.248         0.772         0.453         1.182         0.842         0.907         1.248         0.907         1.235         0.774           9.653         1.214         1.248         0.436         1.331         2.342         0.767         0.621         1.978         0.223         1.216         1.235         0.737           9.653         1.242         0.861         1.337         0.777         0.564	9.363	0.896	1.081	1.222	0.510	0.370	1.351	0.891	0.351	2.532	1.121	0.851	1.617	0.687	0.636	1.114	0.638
9.474       0.685       1.003       1.246       0.469       1.615       0.810       0.414       0.603       1.135       1.135       1.135       0.683       0.693       0.766       1.160       0.686         9.470       0.887       1.099       1.251       0.460       1.615       0.821       0.381       2.349       0.509       1.355       1.898       0.711       0.840       0.982       1.248       0.724         9.542       0.992       1.216       1.256       0.451       0.662       2.63       0.756       0.503       2.101       0.290       1.886       1.679       0.842       1.073       1.282       0.757         9.615       1.215       1.124       1.286       0.448       1.397       2.374       0.750       0.560       2.036       0.252       2.078       1.538       0.917       1.149       1.318       0.768         9.651       1.155       0.821       1.397       0.374       0.800       0.774       1.879       0.184       2.259       1.309       1.235       1.315       1.431       0.797         9.650       1.635       0.800       0.744       1.879       0.164       2.551       1.324       1.504	9.399	0.904	1.059	1.239	0.491	0.411	1.478	0.873	0.351	2.516	0.850	0.982	1.735	0.685	0.698	1.135	0.663
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.470	0.893	1.005	1.246	0.473	0.469	1.015	0.848	0.301	2.441	0.650	1.103	1.830	0.693	0.700	1.160	0.080
9.542       0.992       1.216       1.256       0.451       0.825       2.099       0.772       0.453       2.175       0.341       1.823       1.815       0.784       0.995       1.248       0.744         9.578       1.114       1.214       1.266       0.451       1.062       2.263       0.756       0.503       2.101       0.290       1.866       1.679       0.842       1.073       1.282       0.757         9.615       1.215       1.124       1.281       0.448       1.397       2.374       0.750       0.560       2.036       0.252       2.076       1.432       1.009       1.128       1.355       0.774         9.653       1.228       0.391       1.299       0.436       1.812       2.420       0.771       0.6621       1.978       0.202       2.126       1.432       1.009       1.218       1.315       0.474         9.690       1.155       0.892       1.309       0.372       2.304       1.436       0.840       0.741       1.879       0.184       2.259       1.309       1.243       1.341       0.770         9.766       0.931       0.901       1.293       0.372       2.055       1.396       0.843 <td>9.506</td> <td>0.913</td> <td>1.161</td> <td>1.253</td> <td>0.452</td> <td>0.662</td> <td>1.927</td> <td>0.795</td> <td>0.412</td> <td>2.258</td> <td>0.411</td> <td>1.601</td> <td>1.895</td> <td>0.741</td> <td>0.916</td> <td>1.216</td> <td>0.727</td>	9.506	0.913	1.161	1.253	0.452	0.662	1.927	0.795	0.412	2.258	0.411	1.601	1.895	0.741	0.916	1.216	0.727
9.578       1.114       1.214       1.226       0.451       1.062       2.263       0.756       0.503       2.101       0.290       1.986       1.679       0.842       1.073       1.228       0.757         9.615       1.215       1.124       1.281       0.448       1.397       2.374       0.750       0.560       2.036       0.223       2.126       1.432       1.009       1.218       1.318       0.764         9.650       1.155       0.892       1.309       0.414       2.184       2.100       0.771       0.664       1.926       0.201       2.177       1.366       1.122       1.276       1.333       0.777         9.728       1.042       0.861       1.307       0.302       2.304       1.436       0.840       0.784       1.879       0.184       2.259       1.309       1.223       1.315       1.431       0.775         9.728       0.931       0.901       1.293       0.372       2.304       1.346       0.840       0.784       1.837       0.171       2.365       1.221       1.400       1.327       1.468       0.769       9.482       0.841       1.53       1.344       1.560       0.770       9.381       0.160 <td>9.542</td> <td>0.992</td> <td>1.216</td> <td>1.256</td> <td>0.451</td> <td>0.825</td> <td>2.099</td> <td>0.772</td> <td>0.453</td> <td>2.175</td> <td>0.341</td> <td>1.823</td> <td>1.815</td> <td>0.784</td> <td>0.995</td> <td>1.248</td> <td>0.744</td>	9.542	0.992	1.216	1.256	0.451	0.825	2.099	0.772	0.453	2.175	0.341	1.823	1.815	0.784	0.995	1.248	0.744
9.815       1.215       1.124       1.281       0.448       1.397       2.374       0.750       0.560       2.036       0.252       2.078       1.538       0.917       1.149       1.318       0.768         9.653       1.228       0.991       1.299       0.436       1.813       2.342       0.754       0.621       1.978       0.223       2.126       1.432       1.009       1.218       1.355       0.777         9.690       1.155       0.882       1.307       0.300       2.350       1.736       0.800       0.744       1.879       0.184       2.259       1.309       1.253       1.315       1.431       0.775         9.766       0.931       0.901       1.293       0.372       2.304       1.436       0.843       1.798       0.160       2.458       1.084       1.533       1.304       1.564       0.770         9.842       0.847       1.271       1.255       0.307       2.158       1.311       0.889       0.837       1.730       0.162       2.564       0.921       1.570       0.730       9.2452       1.588       0.994       0.897       1.730       0.142       2.464       0.623       1.917       1.032       1.599<	9.578	1.114	1.214	1.266	0.451	1.062	2.263	0.756	0.503	2.101	0.290	1.986	1.679	0.842	1.073	1.282	0.757
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.615	1.215	1.124	1.281	0.448	1.397	2.374	0.750	0.560	2.036	0.252	2.078	1.538	0.917	1.149	1.318	0.768
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	9.690	1.220	0.991	1.299	0.430	2 184	2.342	0.734	0.621	1.978	0.223	2.120	1.452	1.009	1.218	1.300	0.777
9.766       0.931       0.901       1.293       0.372       2.304       1.436       0.840       0.798       1.837       0.171       2.365       1.221       1.400       1.327       1.468       0.770         9.804       0.857       0.999       1.271       0.367       2.158       1.311       0.889       0.843       1.798       0.160       2.458       1.084       1.553       1.304       1.504       0.760         9.842       0.847       1.125       1.252       0.377       2.065       1.396       0.942       0.876       1.730       0.160       2.458       1.084       1.533       1.534       1.534       0.747         9.881       0.908       1.237       1.265       0.409       2.592       1.582       0.994       0.897       1.730       0.146       2.501       0.633       1.917       1.023       1.599       0.711         9.901       1.079       1.237       1.277       0.395       2.840       0.979       1.077       0.920       1.668       0.142       2.464       0.632       1.917       1.032       1.599       0.711         9.960       1.079       1.237       1.247       0.364       2.349       0.430 <td>9.728</td> <td>1.042</td> <td>0.861</td> <td>1.307</td> <td>0.390</td> <td>2.350</td> <td>1.736</td> <td>0.800</td> <td>0.744</td> <td>1.879</td> <td>0.184</td> <td>2.259</td> <td>1.309</td> <td>1.253</td> <td>1.315</td> <td>1.431</td> <td>0.775</td>	9.728	1.042	0.861	1.307	0.390	2.350	1.736	0.800	0.744	1.879	0.184	2.259	1.309	1.253	1.315	1.431	0.775
9.804       0.857       0.999       1.271       0.367       2.158       1.311       0.889       0.843       1.798       0.160       2.458       1.084       1.553       1.304       1.504       0.760         9.842       0.847       1.125       1.252       0.377       2.065       1.396       0.942       0.876       1.763       0.152       2.504       0.919       1.699       1.243       1.538       0.747         9.881       0.908       1.236       1.249       0.399       2.522       1.582       0.994       0.897       1.730       0.146       2.501       0.759       1.824       1.149       1.570       0.730       0.747         9.921       1.013       1.277       1.265       0.409       2.692       1.442       1.040       0.910       1.698       0.142       2.464       0.623       1.917       1.032       1.599       0.711         9.960       1.079       1.237       1.277       0.395       2.840       0.979       1.077       0.920       1.668       0.138       2.349       0.430       2.003       0.788       1.647       0.666         10.040       0.994       1.239       1.242       1.333       0.348 <td>9.766</td> <td>0.931</td> <td>0.901</td> <td>1.293</td> <td>0.372</td> <td>2.304</td> <td>1.436</td> <td>0.840</td> <td>0.798</td> <td>1.837</td> <td>0.171</td> <td>2.365</td> <td>1.221</td> <td>1.400</td> <td>1.327</td> <td>1.468</td> <td>0.770</td>	9.766	0.931	0.901	1.293	0.372	2.304	1.436	0.840	0.798	1.837	0.171	2.365	1.221	1.400	1.327	1.468	0.770
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.804	0.857	0.999	1.271	0.367	2.158	1.311	0.889	0.843	1.798	0.160	2.458	1.084	1.553	1.304	1.504	0.760
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	9.842	0.847	1.125	1.252	0.377	2.065	1.396	0.942	0.876	1.763	0.152	2.504	0.919	1.699	1.243	1.538	0.747
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	9.881	0.908	1.230	1.249	0.399	2.252	1.582	0.994	0.897	1.730	0.140	2.501	0.759	1.824	1.149	1.570	0.730
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	9.960	1.079	1.237	1.205	0.395	2.840	0.979	1.077	0.920	1.669	0.139	2.409	0.514	1.975	0.908	1.599	0.111
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.000	1.054	1.199	1.260	0.376	2.714	0.640	1.107	0.935	1.640	0.138	2.349	0.430	2.003	0.788	1.647	0.666
$            \begin{array}{ccccccccccccccccccccccccc$	10.040	0.994	1.239	1.224	0.378	2.544	0.454	1.135	0.959	1.612	0.138	2.289	0.364	2.006	0.679	1.666	0.641
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.081	0.977	1.348	1.185	0.411	2.393	0.348	1.171	0.992	1.585	0.140	2.232	0.313	1.994	0.584	1.682	0.616
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.121	1.037	1.473	1.166	0.475	2.266	0.284	1.220	1.030	1.557	0.144	2.179	0.272	1.972	0.504	1.694	0.591
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.103	1.335	1.539	1.190	0.614	2.107 2.062	0.243	1.280	1.003	1.528	0.150	2.129	0.240	1.944 1.914	0.438 0.389	1.703	0.566
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.246	1.429	1.434	1.360	0.607	1.975	0.198	1.441	1.086	1.464	0.176	2.042	0.193	1.883	0.336	1.713	0.519
$            \begin{array}{ccccccccccccccccccccccccc$	10.288	1.413	1.332	1.408	0.561	1.894	0.189	1.514	1.079	1.428	0.202	2.003	0.176	1.853	0.297	1.715	0.498
$            \begin{array}{ccccccccccccccccccccccccc$	10.331	1.339	1.310	1.413	0.529	1.817	0.188	1.582	1.075	1.390	0.246	1.966	0.162	1.824	0.265	1.714	0.478
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.373	1.284	1.373	1.414	0.528	1.740	0.195	1.661	1.079	1.359	0.322	1.932	0.151	1.796	0.237	1.713	0.460
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.417	1.295	1.480	1.435	0.542	1.001	0.215	1.769	1.077	1.372	0.442	1.899	0.142	1.770	0.214	1.710	0.444
10.549 1.639 1.550 1.556 0.481 1.454 0.443 2.105 0.776 1.781 0.390 1.809 0.130 1.700 0.163 1.699 0.406	10.504	1.520	1.604	1.526	0.522	1.503	0.325	2.033	0.925	1.694	0.532	1.838	0.130	1.722	0.194	1.702	0.429
	10.549	1.639	1.550	1.556	0.481	1.454	0.443	2.105	0.776	1.781	0.390	1.809	0.130	1.700	0.163	1.699	0.406

•

6. APPENDIX—Continued

	(	Orthopy	roxene													
wavelength (in.um)	Sla	b k	Pow	der k	Kaoli n	nite k	Serpe	ntine k	Pyroph n	iyilite k	Montme	brillonite k	Sapo n	nite k	Palag n	onite k
10.593	1.679	1.457	1.562	0.441	1.494	0.585	2.118	0.628	1.767	0.278	1.780	0.133	1.679	0.150	1.695	0.396
10.638	1.637	1.407	1.556	0.418	1.617	0.638	2.093	0.506	1.729	0.215	1.752	0.139	1.660	0.139	1.692	0.388
10.684	1.577	1.461	1.558	0.415	1.676	0.586	2.050	0.412	1.659	0.160	1.726	0.132	1.625	0.129	1.689	0.375
10.730	1.823	1.752	1.624	0.369	1.615	0.662	1.956	0.289	1.632	0.148	1.698	0.204	1.609	0.113	1.689	0.369
10.823	2.153	1.663	1.630	0.306	1.701	0.761	1.912	0.248	1.609	0.140	1.713	0.234	1.594	0.107	1.690	0.362
10.870	2.305	1.340	1.605	0.252	1.803	0.794	1.872	0.217	1.590	0.136	1.748	0.242	1.579	0.101	1.692	0.354
10.917	2.202	0.926	1.500	0.218	2.217	0.830	1.802	0.171	1.558	0.130	1.782	0.183	1.553	0.091	1.697	0.335
11.013	1.782	0.951	1.469	0.204	2.289	0.483	1.771	0.155	1.545	0.129	1.769	0.155	1.540	0.087	1.698	0.324
11.062	1.665	1.101	1.408	0.273	2.218	0.305	1.743	0.141	1.533	0.128	1.749	0.136	1.528	0.084	1.698	0.311
11.111	1.711	1.234	1.462	0.240	2.131	0.210	1.694	0.129	1.522	0.128	1.707	0.128	1.506	0.078	1.693	0.286
11.211	1.629	1.268	1.391	0.303	1.994	0.124	1.672	0.111	1.501	0.128	1.692	0.135	1.495	0.075	1.689	0.274
11.261	1.563	1.506	1.406	0.368	1.942	0.103	1.651	0.104	1.491	0.128	1.688	0.145	1.485	0.073	1.683	0.262
11.312	1.720	1.811	1.461	0.415	1.898	0.089	1.632	0.098	1.402	0.129	1.704	0.130	1.410	0.069	1.668	0.232
11.416	2.380	1.853	1.598	0.406	1.827	0.071	1.596	0.088	1.462	0.131	1.705	0.123	1.457	0.068	1.660	0.233
11.468	2.559	1.824	1.644	0.360	1.796	0.065	1.580	0.084	1.451	0.133	1.697	0.106	1.448	0.067	1.652	0.226
11.521	2.955	1.701	1.666	0.315	1.769	0.060	1.564	0.080	1.439	0.135	1.682	0.093	1.439	0.065	1.634	0.219
11.574	3.058	1.260	1.698	0.213	1.720	0.053	1.535	0.075	1.411	0.158	1.648	0.086	1.423	0.064	1.625	0.208
11.682	3.348	0.784	1.681	0.160	1.698	0.051	1.522	0.073	1.408	0.189	1.637	0.093	1.415	0.064	1.616	0.204
11.737	3.097	0.429	1.653	0.123	1.677	0.050	1.508	0.071	1.442	0.202	1.642	0.099	1.407	0.063	1.607	0.200
11.792	2.882	0.297	1.620	0.100	1.637	0.048	1.495	0.069	1.422	0.172	1.639	0.070	1.392	0.063	1.589	0.195
11.905	2.603	0.190	1.579	0.073	1.619	0.047	1.471	0.066	1.397	0.209	1.624	0.060	1.385	0.064	1.581	0.193
11.962	2.503	0.163	1.559	0.065	1.600	0.047	1.459	0.066	1.459	0.276	1.610	0.054	1.378	0.064	1.572	0.192
12.019	2.419	0.143	1.542	0.058	1.582	0.048	1.447	0.063	1.500	0.153	1.590	0.050	1.363	0.065	1.555	0.191
12.136	2.282	0.1120	1.511	0.050	1.545	0.051	1.425	0.064	1.472	0.141	1.570	0.049	1.357	0.066	1.547	0.190
12.195	2.225	0.108	1.498	0.047	1.526	0.054	1.414	0.064	1.452	0.147	1.558	0.050	1.350	0.067	1.539	0.191
12.255	2.172	0.101	1.485	0.045	1.506	0.058	1.403	0.064	1.451	0.165	1.546	0.051	1.343	0.068	1.531	0.191
12.315	2.124	0.095	1.475	0.043	1.465	0.005	1.381	0.064	1.475	0.132	1.521	0.059	1.330	0.071	1.515	0.192
12.438	2.036	0.087	1.451	0.040	1.446	0.095	1.370	0.065	1.461	0.117	1.510	0.067	1.324	0.073	1.507	0.196
12.500	1.995	0.084	1.440	0.039	1.435	0.124	1.359	0.066	1.448	0.109	1.503	0.078	1.317	0.074	1.500	0.198
12.563 12.626	1.956	0.082	1.430	0.039	1.447	0.150	1.348	0.068	1.430	0.103	1.505	0.092	1.305	0.078	1.492	0.201
12.690	1.882	0.081	1.410	0.039	1.497	0.134	1.327	0.069	1.415	0.100	1.527	0.089	1.299	0.081	1.478	0.207
12.755	1.847	0.081	1.400	0.039	1.487	0.107	1.315	0.070	1.406	0.098	1.526	0.075	1.293	0.083	1.471	0.211
12.821	1.811	0.082	1.391	0.040	1.407	0.091	1.304	0.072	1.397	0.096	1.516	0.064	1.287	0.088	1.404	0.215
12.953	1.740	0.086	1.371	0.043	1.419	0.083	1.281	0.076	1.380	0.093	1.495	0.052	1.276	0.091	1.451	0.224
13.021	1.703	0.090	1.362	0.045	1.396	0.087	1.270	0.079	1.371	0.092	1.484	0.050	1.270	0.094	1.444	0.229
13.089	1.666	0.096	1.352	0.047	1.373	0.098	1.208	0.081	1.302	0.091	1.474	0.048	1.265	0.091	1.439	0.234
13.228	1.585	0.116	1.334	0.055	1.347	0.140	1.233	0.088	1.345	0.089	1.453	0.047	1.254	0.102	1.427	0.246
13.298	1.542	0.132	1.325	0.061	1.359	0.159	1.220	0.092	1.336	0.089	1.443	0.047	1.249	0.105	1.422	0.252
13.369	1.496	0.156	1.317	0.067	1.377	0.154	1.200	0.096	1.327	0.088	1.433	0.048	1.244	0.108	1.410	0.259
13.514	1.403	0.244	1.306	0.083	1.361	0.116	1.179	0.106	1.308	0.087	1.412	0.050	1.233	0.114	1.407	0.273
13.587	1.374	0.322	1.304	0.091	1.339	0.106	1.164	0.111	1.298	0.087	1.402	0.051	1.227	0.117	1.403	0.280
13.661	1.387	0.419	1.305	0.096	1.314	0.102	1.149	0.118	1.287	0.087	1.392	0.053	1.221	0.120	1.399	0.287
13.812	1.567	0.494	1.304	0.090	1.264	0.103	1.117	0.123	1.266	0.087	1.370	0.057	1.207	0.126	1.392	0.303
13.889	1.620	0.417	1.297	0.090	1.239	0.113	1.100	0.142	1.254	0.087	1.359	0.060	1.200	0.129	1.389	0.310
13.966	1.606	0.344	1.286	0.088	1.213	0.122	1.082	0.152	1.243	0.088	1.347	0.064	1.191	0.132	1.386	0.318
14.124	1.555	0.302	1.255	0.089	1.161	0.151	1.045	0.104	1.217	0.089	1.323	0.075	1.172	0.142	1.382	0.334
14.205	1.413	0.337	1.236	0.108	1.136	0.171	1.025	0.192	1.204	0.091	1.313	0.083	1.160	0.148	1.379	0.343
14.286	1.375	0.432	1.219	0.133	1.113	0.195	1.005	0.209	1.190	0.092	1.308	0.092	1.147	0.156	1.377	0.351
14.368	1.438	0.553	1.210	0.174	1.093	0.225	0.964	0.229	1.115	0.094	1.304	0.093	1.118	0.180	1.373	0.367
14.535	1.679	0.425	1.309	0.207	1.076	0.293	0.942	0.277	1.143	0.098	1.281	0.092	1.101	0.199	1.372	0.375
14.620	1.643	0.308	1.330	0.163	1.081	0.323	0.922	0.307	1.125	0.101	1.266	0.095	1.085	0.225	1.370	0.384
14.706 14.793	1.571	0.244	1.317	0.127	1.092	0.343	0.902	0.340	1.107	0.105	1.231	0.100	1.066	0.200	1.368 1.367	0.393
14.881	1.421	0.212	1.266	0.101	1.105	0.347	0.870	0.422	1.066	0.114	1.219	0.113	1.077	0.363	1.365	0.411
14.970	1.351	0.228	1.239	0.102	1.094	0.341	0.860	0.470	1.043	0.120	1.203	0.122	1.116	0.422	1.363	0.420
15.060	1.293	0.268	1.212	0.112	1.070	0.340	0.855	0.522	1.019	0.127	1.186	0.131	1.187	0.462	1.361	0.431
15.132	1.294	0.329	1.174	0.169	1.003	0.375	0.866	0.635	0.963	0.146	1.151	0.155	1.345	0.416	1.357	0.452
15.337	1.326	0.344	1.190	0.208	0.979	0.417	0.884	0.695	0.932	0.159	1.133	0.169	1.380	0.351	1.355	0.464
15.432	1.304	0.289	1.231	0.212	0.980	0.459	0.912	0.753	0.898	0.175	1.115	0.186	1.384	0.291	1.353	0.477
15.528	1.244	0.252	1.245	0.179	0.995	0.472	0.990	0.810	0.801	0.190	1.079	0.204	1.348	0.244	1.351	0.490
15.723	1.091	0.240	1.199	0.139	0.938	0.460	1.055	0.906	0.784	0.260	1.062	0.248	1.323	0.187	1.351	0.520

		Orthopy	roxene													
wavelength	Sla	ьb	Pow	der	Kaol	inite	Serpe	ntine	Pyrop	hyllite	Montm	orillonite	Sapo	nite	Palag	onite
(in µm)	מ	k	n	k	n	k	n	k	<u>n</u>	k	n	k	n	k	n	k
15.823	1.009	0.256	1.167	0.137	0.882	0.486	1.122	0.941	0.750	0.306	1.046	0.274	1.297	0.170	1.352	0.536
15.924	0.924	0.286	1.134	0.144	0.828	0.535	1.196	0.963	0.726	0.357	1.031	0.303	1.272	0.159	1.353	0.553
16.026	0.836	0.332	1.101	0.157	0.784	0.603	1.273	0.970	0.713	0.402	1.019	0.334	1.248	0.152	1.355	0.571
16.129	0.748	0.398	1.068	0.177	0.755	0.682	1.350	0.960	0.696	0.436	1.009	0.367	1.224	0.148	1.359	0.589
16.234	0.669	0.487	1.035	0.205	0.742	0.768	1.421	0.933	0.602	0.472	1.003	0.401	1.201	0.147	1.303	0.609
16.340	0.611	0.596	1.003	0.241	0.745	0.855	1.482	0.893	0.017	0.827	0.999	0.430	1.117	0.141	1.370	0.049
16.447	0.580	0.715	0.975	0.288	0.700	0.939	1.920	0.043	0.510	0.000	1 001	0.970	1.194	0.149	1.310	0.049
16.556	0.575	0.829	0.950	0.345	0.780	1.010	1.559	0.781	0.550	0.704	1.001	0.505	1.130	0.155	1.307	0.070
10.007	0.590	1.010	0.901	0.408	0.010	1.000	1.576	0.731	0.588	0.010	1.004	0.564	1.081	0.156	1.333	0.031
16.002	0.641	1.012	0.902	0.470	0.851	1.149	1.570	0.613	0.643	1 003	1.009	0.594	1.055	0.175	1.428	0.732
17.007	0.645	1 1 20	1 010	0.566	0.001	1.268	1 547	0.594	0.712	1.061	1.008	0.624	1.028	0.185	1.445	0.752
17 193	0.627	1 178	1 031	0.606	0.924	1.339	1.521	0.565	0.766	1.083	1.004	0.657	1.001	0.199	1.465	0.771
17 241	0.600	1.265	1.052	0.651	0.948	1.428	1.491	0.546	0.776	1.095	0.999	0.696	0.972	0.215	1.487	0.789
17.361	0.589	1.388	1.084	0.703	0.987	1.535	1.460	0.538	0.752	1.139	0.993	0.743	0.941	0.234	1.511	0.805
17.483	0.622	1.537	1.131	0.749	1.054	1.656	1.430	0.541	0.729	1.229	0.992	0.800	0.910	0.257	1.536	0.820
17.606	0.730	1.677	1.184	0.780	1.159	1.779	1.406	0.555	0.730	1.355	0.998	0.866	0.877	0.285	1.563	0.832
17.731	0.904	1.717	1.231	0.801	1.304	1.884	1.394	0.577	0.768	1.503	1.018	0.940	0.844	0.318	1.592	0.842
17.857	0.979	1.622	1.272	0.830	1.476	1.951	1.398	0.599	0.847	1.663	1.055	1.016	0.811	0.357	1.621	0.850
17.986	0.898	1.604	1.329	0.869	1.643	1.976	1.417	0.610	0.977	1.826	1.109	1.088	0.779	0.404	1.651	0.855
18.116	0.847	1.722	1.416	0.896	1.783	1.998	1.439	0.601	1.170	1.975	1.175	1.148	0.750	0.458	1.681	0.857
18.248	0.905	1.867	1.520	0.881	1.938	2.075	1.449	0.572	1.438	2.078	1.247	1.196	0.726	0.520	1.712	0.856
18.382	1.047	1.939	1.597	0.816	2.234	2.179	1.438	0.537	1.765	2.081	1.314	1.240	0.709	0.589	1.741	0.853
18.519	1.166	1.875	1.618	0.738	2.715	2.086	1.407	0.506	2.085	1.936	1.383	1.297	0.700	0.663	1.770	0.847
18.657	1.130	1.762	1.588	0.687	3.071	1.645	1.363	0.487	2.293	1.668	1.480	1.380	0.700	0.741	1.796	0.838
18.797	0.971	1.759	1.534	0.693	3.087	1.101	1.309	0.481	2.343	1.381	1.0/4	1.404	0.710	0.022	1.021	0.821
18.939	0.817	1.898	1.502	0.773	2.936	0.834	1.250	0.489	2.271	1.1/1	1.942	1.404	0.760	0.904	1.844	0.814
19.084	0.730	2.121	1.559	0.903	2.107	0.037	1.109	0.512	2.172	1.101	2.140	1.100	0.700	1.064	1.804	0.000
19.231	0.712	2.385	1.739	0.970	2.090	0.019	1.120	0.606	2.274	0.781	2.100	0.921	0.800	1 140	1.806	0.780
19.380	0.759	2.078	1.920	0.900	2.409	0.440	1.005	0.000	1 958	0.701	1 054	0.731	0.049	1.140	1.030	0.7756
19.001	1.009	3.001	2.020	0.765	2.300	0.403	0.967	0.000	1.560	0.736	1.817	0.572	0.972	1.275	1.915	0.742
19.000	1.090	3 701	2.077	0.548	2.100	0.384	0.945	0.889	1.589	0.852	1.678	0.572	1.041	1.332	1.921	0.730
20.000	2 084	3 9/14	2.000	0.451	1 908	0.407	0.959	1.008	1.467	1.065	1.538	0.624	1.111	1.383	1.924	0.721
20.000	2.001	3 772	2.054	0.365	1.770	0.462	0.990	1.105	1.457	1.368	1.407	0.739	1.179	1.434	1.925	0.716
20.325	3.128	3.527	2.010	0.293	1.626	0.564	1.013	1.207	1.624	1.707	1.315	0.932	1.249	1.490	1.924	0.715
20.492	3.580	3.208	1.955	0.244	1.493	0.743	1.058	1.328	2.018	1.967	1.314	1.194	1.326	1.558	1.925	0.721
20.661	3.744	2.691	1.899	0.215	1.423	1.023	1.139	1.447	2.579	1.942	1.451	1.468	1.426	1.640	1.928	0.734
20.833	3.794	2.400	1.844	0.204	1.505	1.382	1.252	1.546	2.990	1.558	1.721	1.660	1.566	1.726	1.940	0.754
21.008	3.813	1.982	1.793	0.211	1.820	1.717	1.381	1.612	3.062	1.114	2.019	1.724	1.760	1.792	1.965	0.778
21.186	3.595	1.791	1.753	0.238	2.368	1.818	1.503	1.646	2.955	0.823	2.328	1.751	2.003	1.799	2.009	0.796
21.368	3.612	1.714	1.736	0.283	2.853	1.503	1.608	1.670	2.822	0.683	2.744	1.643	2.257	1.712	2.065	0.796
21.552	3.527	1.574	1.755	0.328	2.973	1.047	1.706	1.703	2.753	0.635	3.046	1.266	2.457	1.535	2.117	0.771
21.739	3.609	1.602	1.794	0.347	2.868	0.732	1.819	1.745	2.764	0.563	3.073	0.804	2.500	1.323	2.151	0.733
21.930	3.826	1.318	1.838	0.357	2.709	0.561	1.955	1.(19	2.(45	0.431	2.908	0.892	2.070	1.100	2.107	0.690
22.124	3.737	0.922	1.914	0.340	2.551	0.480	2.100	1.795	2.070	0.321	2.040	0.420	2.362	0.081	2.114	0.009
22.321	3.510	0.580	1.901	0.203	2.400	0.478	2.200	1.190	2.000	0.201	2.130	0.321	2.110	0.981	2.119	0.641
22.523	3.219	0.002	1.943	0.115	2.200	0.695	2.410	1.820	2.001	0.200	2.004	0.205	2.685	0.528	2.105	0.632
22.121	0.000	0.467	1.900	0.120	2.210	0.000	3 200	1.551	2.420	0.143	2.001	0.200	2.588	0.417	2 227	0.620
22.930 93 148	2.011	0.400	1.833	0.080	2.535	0.986	3,221	1.079	2.283	0.163	2.428	0.147	2.504	0.344	2.253	0.603
23 364	2.529	0.480	1.796	0.069	2.798	0.844	3.101	0.817	2.205	0.188	2.379	0.127	2.434	0.293	2.278	0.578
23.585	2.362	0.524	1.747	0.066	2.879	0.601	2.990	0.659	2.134	0.288	2.335	0.112	2.374	0.253	2.301	0.547
23.810	2.196	0.596	1.508	0.507	2.839	0.415	2.897	0.549	2.276	0.461	2.297	0.099	2.322	0.222	2.318	0.511
24.038	2.032	0.704	1.791	0.060	2.765	0.298	2.817	0.467	2.446	0.280	2.263	0.089	2.276	0.197	2.328	0.473
24.272	1.875	0.858	1.727	0.069	2.691	0.224	2.747	0.402	2.385	0.152	2.233	0.081	2.235	0.176	2.332	0.436
24.510	1.743	1.069	1.668	0.122	2.625	0.177	2.684	0.350	2.321	0.105	2.206	0.073	2.199	0.159	2.330	0.400
24.752	1.661	1.337	1.770	0.282	2.569	0.144	2.628	0.307	2.272	0.084	2.181	0.067	2.166	0.144	2.325	0.367
25.000	1.653	1.647	1.875	0.115	2.520	0.121	2.578	0.272	2.234	0.072	2.158	0.062	2.136	0.131	2.316	0.337

6. APPENDIX—Continued

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