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STATIC LONGITUDINAL STABILITY AND CONTROL CHARACTERISTICS
OF AN UNSWEPT WING AND UNSWEPT HORIZONTAL-TAIL
CONFIGURATION AT MACH NUMBERS FROM 0.70 TO 2.22

By Victor L. Peterson and Gene P. Menees

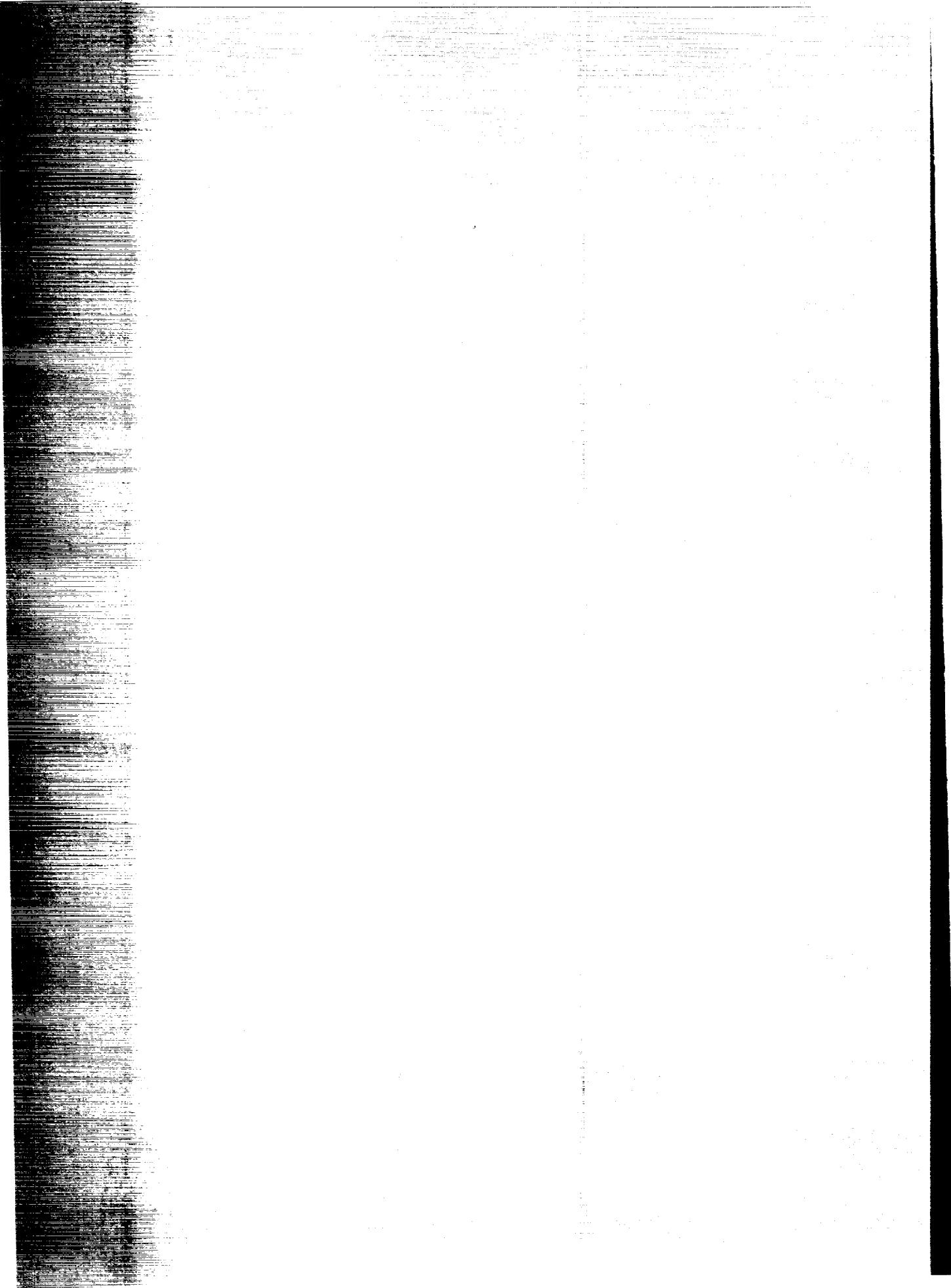
Ames Research Center
Moffett Field, Calif.

NATIONAL AERONAUTICS AND
SPACE ADMINISTRATION

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STATIC LONGITUDINAL STABILITY AND CONTROL CHARACTERISTICS
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By Victor L. Peterson and Gene P. Menees

SUMMARY

Results of an investigation of the static longitudinal stability and control characteristics of an aspect-ratio-3.1, unswept wing configuration equipped with an aspect-ratio-4, unswept horizontal tail are presented without analysis for the Mach number range from 0.70 to 2.22. The hinge line of the all-movable horizontal tail was in the extended wing chord plane, 1.66 wing mean aerodynamic chords behind the reference center of moments. The ratio of the area of the exposed horizontal-tail panels to the total area of the wing was 13.3 percent and the ratio of the total areas was 19.9 percent. Data are presented at angles of attack ranging from -6° to $+18^\circ$ for the horizontal tail set at angles ranging from $+5^\circ$ to -20° and for the tail removed.

INTRODUCTION

A general research program directed at the investigation of longitudinal control devices capable of achieving low trim drag and adequate maneuverability at supersonic speeds is in progress at the Ames Research Center. As a part of this program, a number of reports have been published showing the longitudinal and lateral-directional characteristics of configurations utilizing canard controls (see refs. 1 through 9). The results for two other trimming devices, a full-span trailing-edge flap and a configuration incorporating camber in the forward part of the body, were also reported in reference 9.

This report is one of the series pertaining to the program and presents without analysis the longitudinal stability and control

characteristics of one additional configuration and its component parts. The complete configuration consisted of an aspect-ratio-3.1, unswept wing, an all-movable, unswept horizontal tail of aspect ratio 4, and a low-aspect-ratio vertical tail mounted on a Sears-Haack body of 12.5 fineness ratio. The basic configuration, consisting of the unswept wing, the low-aspect-ratio vertical tail, and the Sears-Haack body, was identical to that tested with the unswept canard of references 5 and 6.

NOTATION

\bar{c}	mean aerodynamic chord of wing, ft
C_D	drag coefficient, $\frac{\text{drag}}{qS}$
C_{D_0}	drag coefficient at zero lift
C_L	lift coefficient, $\frac{\text{lift}}{qS}$
C_{L_α}	lift-curve slope taken through 0° angle of attack, per deg
C_m	pitching-moment coefficient, referred to the projection of the 0.15 \bar{c} point onto the body center line, $\frac{\text{pitching moment}}{qS\bar{c}}$
$(\frac{L}{D})_{\max}$	maximum lift-drag ratio
M	free-stream Mach number
q	free-stream dynamic pressure, lb/ s^2 ft
S	wing area formed by extending the leading and trailing edges to the vertical plane of symmetry, sq ft
α	angle of attack of wing root chord, deg
δ	angle of deflection of the horizontal tail with respect to the extended wing chord plane, positive when trailing edge is down, deg

Configurations are denoted by the following letters used in combination:

B body
 H horizontal tail
 V vertical tail
 W wing

APPARATUS

Test Facility

The experimental data were obtained in the Ames 6- by 6-foot supersonic wind tunnel which is a closed-circuit variable-pressure type with a Mach number range continuous from 0.70 to 2.22. The tunnel floor and ceiling have perforations to permit transonic testing. A somewhat more detailed description is given in reference 1.

The model was sting mounted and the forces and moments were measured with an internal, strain-gage-type, six-component balance.

Model

The model consisted of an aspect-ratio-3.1 unswept wing, an aspect-ratio- $\frac{1}{4}$, all-movable, horizontal tail, and a low-aspect-ratio vertical tail mounted on a fineness-ratio-12.5 Sears-Haack body. A dimensional sketch of the model is shown in figure 1. The wing and vertical tail had NACA 2S-(50)(015)-(50)(015) and NACA 0003-63 sections streamwise, respectively. The horizontal tail had NACA 2S-(30)(015)-(30)(015) sections streamwise and was hinged about the line passing through the 0.30 chord points. The hinge line, which was in the extended wing chord plane, was 1.66 wing mean aerodynamic chord lengths behind the reference center of moments ($0.15\bar{c}$). The ratio of the area of the exposed tail panels to the total area of the wing was 13.3 percent and the ratio of the total areas was 19.9 percent.

All of the component parts of the model were of solid steel construction to minimize aeroelastic effects. The surfaces were polished smooth and were further treated to prevent corrosion.

TEST AND PROCEDURES

Range of Test Variables

Mach numbers of 0.70, 0.90, 1.00, 1.10, 1.30, 1.70, and 2.22 and angles of attack ranging from -6° to $+18^\circ$ were covered in the investigation. Data were obtained for horizontal-tail deflections ranging from $+5^\circ$ to -20° and for the configuration with the horizontal tail removed.

The test Reynolds number based on the wing mean aerodynamic chord was 1.89 million. Wires were placed on the model at the locations shown in figure 1 to induce transition.

Reduction of Data

The data presented herein have been reduced to standard coefficient form. The moment center for the data presented herein was chosen so that the minimum static margin in the range of trim-lift coefficients between 0 and 0.5 throughout the Mach number range investigated was $0.03\bar{c}$; the resulting moment center was at the 0.15 point of the wing mean aerodynamic chord. The results have been adjusted for base drag and stream inclination.

The base pressure was measured and the data were adjusted to correspond to a base pressure equal to the free-stream static pressure.

The data were adjusted for a stream inclination of less than $\pm 0.30^\circ$ which existed throughout the Mach number range of the tests.

RESULTS

The data are presented without analysis in order to expedite publication. All of the experimental data are tabulated in table I. Selected portions of the data are presented in figures 2 and 3. Figure 2 presents the lift, drag, and pitching-moment characteristics with the horizontal tail deflected at various angles and with the tail off for five test Mach numbers. Summarized in figure 3 are the maximum lift-drag ratios, lift-curve slopes, minimum drag coefficients, and aerodynamic center locations as a function of Mach number for the horizontal tail on at zero deflection and for the tail removed. It should be noted that data were not available to cross-plot the parameters shown in figure 3 between the Mach numbers 0.90 and 1.00 and the Mach numbers 1.00 and 1.10. Previous data on this type of wing have shown that results at intermediate Mach numbers are necessary in order to make accurate cross plots. Additional transonic data for a model of the same geometry as that used in the present investigation are available in reference 10.

Ames Research Center
National Aeronautics and Space Administration
Moffett Field, Calif., Mar. 12, 1959

REFERENCES

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10. Stivers, Louis S., Jr., and Lippman, Garth W.: Effects of Fixing Boundary-Layer Transition for an Unswept-Wing Model and an Evaluation of Porous Tunnel-Wall Interference for Mach Numbers From 0.60 to 1.40. NACA TN 4228, 1958.

TABLE I.- LONGITUDINAL AERODYNAMIC CHARACTERISTICS
(a) BVW

M	α , deg	C_L	C_D	C_m	M	α , deg	C_L	C_D	C_m
0.70	-06.2	-0.464	.0561	.0311	1.30	-06.0	-0.424	.0654	.1118
-04.1	-0.308	.0305	.0139			-04.0	-0.290	.0410	.0750
-02.0	-0.156	.0173	.0097			-01.9	-0.145	.0254	.0357
-01.6	-0.127	.0160	.0092			-01.5	-0.115	.0234	.0275
-00.1	-0.011	.0132	.0013			-00.0	0.002	.0202	-.0013
00.4	0.023	.0132	.0040			00.5	0.035	.0206	-.0078
01.9	0.126	.0159	.0003			02.0	0.142	.0253	-.0350
03.9	0.281	.0273	-.0071			04.1	0.288	.0407	-.0724
05.9	0.440	.0506	-.0232			06.0	0.417	.0631	-.1084
07.9	0.586	.0857	-.0596			08.1	0.561	.0988	-.1470
09.9	0.705	.1313	-.1084			10.0	0.686	.1400	-.1810
						11.9	0.795	.1871	-.2102
0.90	-05.9	-0.578	.0720	.0963		14.0	0.917	.2447	-.2448
-03.9	-0.381	.0364	.0431			16.1	1.022	.3085	-.2714
-01.9	-0.169	.0181	.0118			18.0	1.153	.3856	-.3073
-01.5	-0.135	.0166	.0120						
00.1	-0.002	.0135	.0059		1.70	-06.1	-0.309	.0511	.0940
00.6	0.046	.0142	.0030			-04.2	-0.212	.0331	.0653
02.1	0.175	.0180	-.0006			-02.1	-0.116	.0219	.0362
04.1	0.395	.0388	-.0399			-01.6	-0.086	.0199	.0265
06.0	0.583	.0710	-.0835			-00.2	-0.005	.0171	.0023
08.1	0.740	.1173	-.1255			00.4	0.018	.0171	-.0031
10.0	0.884	.1693	-.1636			01.8	0.092	.0199	-.0253
12.1	1.034	.2339	-.2133			03.9	0.195	.0301	-.0557
						05.9	0.292	.0462	-.0846
1.00	-05.8	-0.528	.0790	.1116		07.9	0.394	.0709	-.1154
-03.7	-0.352	.0459	.0643			09.9	0.496	.1027	-.1463
-01.7	-0.157	.0297	.0217			11.8	0.588	.1396	-.1740
-01.2	-0.120	.0259	.0182			13.9	0.680	.1841	-.2037
00.2	0.020	.0260	-.0018			15.9	0.769	.2354	-.2310
00.8	0.072	.0243	-.0095			17.9	0.852	.2912	-.2552
02.2	0.212	.0324	-.0316						
04.2	0.404	.0546	-.0782		2.22	-05.6	-0.215	.0356	.0685
06.3	0.583	.0901	-.1273			-03.5	-0.139	.0225	.0439
08.2	0.742	.1350	-.1747			-01.6	-0.062	.0151	.0203
10.2	0.886	.1854	-.2176			-01.2	-0.044	.0139	.0145
12.3	1.028	.2494	-.2616			00.4	0.014	.0130	-.0020
14.3	1.147	.3175	-.2982			00.8	0.027	.0134	-.0054
16.3	1.253	.3919	-.3321			02.4	0.086	.0167	-.0238
18.3	1.343	.4682	-.3621			04.3	0.159	.0253	-.0464
						06.4	0.235	.0392	-.0702
						08.4	0.310	.0585	-.0946
1.10	-05.8	-0.501	.0775	.1079		10.3	0.385	.0830	-.1181
-03.8	-0.340	.0490	.0647			12.4	0.463	.1144	-.1428
-01.7	-0.165	.0302	.0235			14.4	0.543	.1523	-.1680
-01.3	-0.128	.0286	.0197			16.4	0.622	.1968	-.1933
00.2	0.006	.0222	-.0067			18.4	0.694	.2449	-.2172
00.8	0.052	.0218	-.0126						
02.2	0.196	.0322	-.0325						
04.2	0.361	.0518	-.0725						
06.2	0.522	.0822	-.1157						
08.2	0.673	.1253	-.1582						
10.2	0.812	.1742	-.1996						
14.2	1.058	.2971	-.2762						
16.2	1.155	.3639	-.3073						
18.2	1.248	.4366	-.3382						

TABLE I.- LONGITUDINAL AERODYNAMIC CHARACTERISTICS - Continued
(b) BWH; $\delta = 0^\circ$

M	α , deg	C_L	C_D	C_m	M	α , deg	C_L	C_D	C_m
0.70	-06.1	-0.480	.0593	.0582	1.30	-06.0	-0.468	.0728	.1856
	-04.1	-0.319	.0335	.0312		-04.0	-0.314	.0449	.1217
	-02.1	-0.160	.0195	.0168		-02.0	-0.171	.0292	.0668
	-00.6	-0.048	.0154	.0070		-00.5	-0.040	.0230	.0179
	-00.1	-0.017	.0151	.0083		00.0	-0.000	.0226	.0038
	00.4	0.015	.0151	.0070		00.5	0.038	.0231	-0.0092
	01.9	0.129	.0178	-.0049		02.0	0.149	.0281	-0.0502
	03.9	0.295	.0303	-.0204		04.0	0.309	.0446	-0.1113
	05.9	0.456	.0540	-.0458		05.9	0.460	.0707	-0.1734
	07.8	0.621	.0923	-.0975		08.0	0.615	.1091	-0.2379
	09.9	0.744	.1390	-.1632		09.8	0.753	.1519	-0.2971
						12.0	0.896	.2127	-0.3604
						14.0	1.036	.2766	-0.4574
						15.9	1.153	.3468	-0.5030
						17.9	1.275	.4266	-0.5172
					1.70	-06.1	-0.353	.0582	.1689
						-04.0	-0.241	.0371	.1163
						-02.2	-0.129	.0245	.0640
						-00.7	-0.040	.0196	.0230
						-00.1	-0.006	.0191	.0068
						00.2	0.015	.0190	-0.0026
						01.8	0.105	.0223	-0.0455
						03.9	0.222	.0334	-0.0995
						05.7	0.337	.0521	-0.1531
						07.8	0.451	.0807	-0.2071
						09.8	0.561	.1155	-0.2598
						11.8	0.679	.1596	-0.3166
						13.8	0.775	.2084	-0.3648
						15.8	0.872	.2647	-0.4129
						17.8	0.971	.3291	-0.4600
1.00	-05.7	-0.547	.0820	.1385	2.22	-05.7	-0.247	.0408	.1192
	-03.6	-0.346	.0499	.0702		-03.7	-0.166	.0267	.0806
	-01.7	-0.163	.0321	.0253		-01.6	-0.075	.0175	.0377
	-00.2	-0.024	.0259	.0056		-00.2	-0.010	.0148	.0078
	00.3	0.026	.0277	-.0013		00.4	0.009	.0149	-0.0008
	00.8	0.062	.0264	-.0031		00.9	0.034	.0151	-0.0127
	02.2	0.210	.0352	-.0272		02.3	0.094	.0185	-0.0407
	04.2	0.404	.0550	-.0751		04.3	0.182	.0285	-0.0825
	06.3	0.610	.0950	-.1698		06.3	0.267	.0442	-0.1228
	08.2	0.795	.1441	-.2519		08.3	0.356	.0669	-0.1658
	10.2	0.960	.2026	-.3298		10.3	0.438	.0945	-0.2064
	12.2	1.111	.2707	-.4057		12.3	0.530	.1313	-0.2516
	14.2	1.250	.3460	-.4788		14.3	0.617	.1713	-0.2944
	16.2	1.379	.4291	-.5540		16.3	0.708	.2225	-0.3400
	18.2	1.509	.5237	-.6402		18.5	0.797	.2816	-0.3847
1.10	-05.7	-0.517	.0829	.1382					
	-03.8	-0.345	.0526	.0764					
	-01.7	-0.168	.0341	.0264					
	-00.2	-0.018	.0273	-.0008					
	00.3	0.028	.0273	-.0060					
	00.7	0.064	.0289	-.0135					
	02.1	0.198	.0354	-.0398					
	04.2	0.383	.0563	-.1005					
	06.1	0.553	.0891	-.1653					
	08.2	0.724	.1357	-.2363					
	10.2	0.879	.1899	-.3079					
	12.2	1.027	.2546	-.3786					
	14.1	1.161	.3246	-.4503					
	16.2	1.283	.4035	-.5233					
	18.2	1.398	.4902	-.5979					

TABLE I.- LONGITUDINAL AERODYNAMIC CHARACTERISTICS - Continued
(c) BVWH; $\delta = -5^\circ$

M	α , deg	C_L	C_D	C_m	M	α , deg	C_L	C_D	C_m
0.70	-06.2	-0.549	.0707	.1504	1.30	-06.0	-0.513	.0822	.2658
	-04.1	-0.382	.0408	.1207		-04.0	-0.366	.0535	.2061
	-02.1	-0.216	.0239	.1060		-02.0	-0.200	.0328	.1391
	-00.6	-0.100	.0184	.0915		-00.5	-0.086	.0264	.0959
	-00.1	-0.067	.0174	.0906		-00.0	-0.046	.0252	.0811
	00.4	-0.028	.0174	.0859		00.5	-0.010	.0257	.0686
	01.9	0.080	.0186	.0748		02.0	0.106	.0287	.0276
	03.8	0.237	.0281	.0608		04.0	0.258	.0422	-.0289
	05.9	0.402	.0503	.0352		06.0	0.410	.0662	-.0891
	07.9	0.564	.0865	-.0159		08.0	0.564	.1019	-.1533
	09.9	0.691	.1317	-.0827		10.0	0.700	.1440	-.2105
						14.0	0.980	.2588	-.3661
						18.0	1.218	.4064	-.4057
0.90	-06.0	-0.650	.0858	.2083	1.70	-06.0	-0.389	.0674	.2280
	-03.8	-0.443	.0451	.1514		-04.0	-0.270	.0434	.1713
	-01.9	-0.246	.0263	.1278		-02.0	-0.147	.0278	.1124
	-00.4	-0.105	.0200	.1169		-00.6	-0.062	.0223	.0719
	00.0	-0.062	.0189	.1128		-00.1	-0.035	.0214	.0591
	00.5	-0.028	.0192	.1111		00.4	-0.006	.0212	.0456
	02.1	0.108	.0210	.1015		01.8	0.077	.0228	.0072
	04.0	0.316	.0362	.0735		03.8	0.187	.0314	-.0435
	05.9	0.528	.0713	.0148		05.8	0.304	.0490	-.0969
	08.0	0.683	.1134	-.0309		07.8	0.422	.0757	-.1533
	10.1	0.865	.1712	-.1115		09.8	0.529	.1080	-.2030
						13.8	0.740	.1963	-.3048
						17.9	0.938	.3131	-.4021
1.00	-05.8	-0.612	.0956	.2542	2.22	-05.7	-0.267	.0459	.1575
	-03.6	-0.414	.0564	.1788		-03.7	-0.177	.0293	.1140
	-01.7	-0.226	.0368	.1329		-01.6	-0.090	.0195	.0721
	-00.2	-0.088	.0312	.1152		-00.1	-0.029	.0165	.0438
	00.3	-0.040	.0303	.1071		00.3	-0.009	.0159	.0342
	00.8	0.014	.0347	.0910		00.8	0.012	.0162	.0243
	02.2	0.143	.0356	.0815		02.3	0.075	.0187	-.0050
	04.3	0.355	.0571	.0146		04.3	0.161	.0270	-.0447
	06.3	0.549	.0901	-.0632		06.2	0.243	.0408	-.0833
	08.2	0.724	.1350	-.1386		08.3	0.331	.0620	-.1263
	10.3	0.892	.1913	-.2137		10.4	0.415	.0888	-.1666
	14.2	1.177	.3251	-.3508		14.3	0.590	.1615	-.2498
	18.2	1.424	.4908	-.5136		18.4	0.766	.2642	-.3355
1.10	-05.9	-0.582	.0950	.2465					
	-03.7	-0.397	.0584	.1762					
	-01.7	-0.224	.0382	.1238					
	-00.3	-0.084	.0310	.0978					
	00.2	-0.038	.0306	.0908					
	00.7	0.009	.0310	.0823					
	02.2	0.148	.0360	.0571					
	04.2	0.327	.0551	-.0033					
	06.2	0.504	.0868	-.0687					
	08.2	0.662	.1279	-.1321					
	10.1	0.805	.1765	-.1937					
	14.2	1.097	.3067	-.3353					
	18.2	1.334	.4640	-.4893					

TABLE I.- LONGITUDINAL AERODYNAMIC CHARACTERISTICS - Continued
 (d) BWB; $\delta = -10^\circ$

M	α , deg	C _L	C _D	C _m	M	α , deg	C _L	C _D	C _m
0.70	-06.0	-0.593	.0851	.2333	1.30	-05.9	-0.553	.0970	.3376
	-04.1	-0.436	.0552	.2008		-03.9	-0.400	.0645	.2747
	-02.0	-0.259	.0352	.1797		-01.9	-0.238	.0430	.2083
	-00.5	-0.151	.0281	.1712		-00.4	-0.122	.0348	.1651
	-00.0	-0.112	.0268	.1673		-00.0	-0.088	.0338	.1539
	00.4	-0.080	.0259	.1647		00.4	-0.051	.0333	.1418
	01.9	0.027	.0261	.1550		01.9	0.059	.0353	.1046
	03.8	0.177	.0331	.1436		03.9	0.213	.0472	.0488
	05.9	0.343	.0529	.1176		05.9	0.359	.0681	-0.0074
	07.9	0.514	.0872	.0628		07.9	0.515	.1008	-0.0726
	09.8	0.635	.1274	-0.046		09.9	0.661	.1432	-0.1324
						13.9	0.927	.2472	-0.2763
						17.9	1.163	.3878	-0.3402
0.90	-05.8	-0.701	.1002	.2986	1.70	-06.0	-0.406	.0774	.2757
	-03.7	-0.479	.0584	.2351		-04.1	-0.295	.0538	.2234
	-01.9	-0.294	.0393	.2045		-02.1	-0.182	.0368	.1672
	-00.4	-0.156	.0318	.1950		-00.5	-0.093	.0292	.1240
	00.0	-0.108	.0308	.1920		-00.1	-0.067	.0283	.1116
	00.6	-0.067	.0296	.1884		00.3	-0.041	.0275	.0993
	02.0	0.052	.0309	.1840		01.8	0.043	.0275	.0603
	04.1	0.274	.0465	.1569		03.8	0.167	.0352	.0025
	06.0	0.460	.0765	.1119		05.7	0.277	.0500	-0.0486
	07.9	0.610	.1148	.0732		07.9	0.392	.0746	-0.1011
	10.1	0.765	.1647	.0178		09.8	0.497	.1046	-0.1500
	14.0	1.103	.3028	-0.1353		13.7	0.706	.1872	-0.2494
						17.8	0.905	.2998	-0.3472
1.00	-05.7	-0.664	.1110	.3505	2.22	-05.5	-0.279	.0534	.1931
	-03.6	-0.486	.0741	.2826		-03.6	-0.196	.0369	.1513
	-01.6	-0.274	.0509	.2298		-01.5	-0.109	.0253	.1086
	-00.1	-0.138	.0429	.2121		-00.1	-0.048	.0214	.0796
	00.2	-0.093	.0432	.2035		00.3	-0.026	.0206	.0682
	00.7	-0.053	.0429	.1964		00.8	-0.007	.0203	.0585
	02.2	0.084	.0462	.1752		02.4	0.057	.0220	.0283
	04.2	0.289	.0645	.1199		04.3	0.141	.0288	-0.0107
	06.2	0.482	.0949	.0402		06.3	0.222	.0415	-0.0488
	08.2	0.661	.1369	-0.0344		08.2	0.306	.0601	-0.0878
	10.2	0.823	.1873	-0.1063		10.3	0.394	.0859	-0.1296
						14.3	0.569	.1558	-0.2130
						18.4	0.737	.2532	-0.2939
1.10	-05.7	-0.628	.1092	.3345					
	-03.5	-0.447	.0713	.2654					
	-01.7	-0.270	.0491	.2135					
	-00.3	-0.135	.0411	.1878					
	00.1	-0.093	.0405	.1794					
	00.7	-0.034	.0405	.1692					
	02.2	0.096	.0439	.1450					
	04.2	0.273	.0609	.0884					
	06.1	0.443	.0884	.0269					
	08.2	0.606	.1280	-0.0389					
	10.2	0.764	.1786	-0.1037					
	14.0	1.029	.2934	-0.2352					
	16.5	1.265	.4055	-0.3311					

TABLE I.- LONGITUDINAL AERODYNAMIC CHARACTERISTICS - Continued
(e) BWH; $\delta = -15^\circ$

M	α , deg	C_L	C_D	C_m	M	$\frac{C}{d \cdot g}$	C_L	C_D	C_m
0.70	-05.9	-0.606	.1012	.2631	1.30	-05.9	-0.579	.1169	.3979
	-04.1	-0.455	.0714	.2332		-04.0	-0.438	.0847	.3391
	-01.9	-0.274	.0496	.2118		-02.1	-0.287	.0617	.2764
	-00.6	-0.176	.0432	.2064		-00.4	-0.160	.0513	.2321
	-00.1	-0.143	.0415	.2048		-00.1	-0.127	.0498	.2220
	00.4	-0.105	.0405	.2004		00.5	-0.092	.0488	.2114
	01.8	-0.001	.0399	.1928		02.0	0.020	.0493	.1749
	03.9	0.158	.0463	.1858		04.0	0.171	.0594	.1216
	05.9	0.309	.0638	.1714		05.9	0.316	.0780	.0670
	07.8	0.460	.0943	.1309		08.1	0.476	.1099	.0014
	09.4	0.563	.1252	.0834		10.0	0.619	.1489	-.0576
						13.8	0.877	.2433	-.1864
						15.9	0.998	.3097	-.2245
0.90	-05.9	-0.734	.1211	.3481	1.70	-06.1	-0.435	.0963	.3256
	-03.8	-0.537	.0796	.2920		-04.1	-0.324	.0697	.2726
	-02.0	-0.313	.0541	.2410		-02.2	-0.211	.0511	.2147
	-00.4	-0.177	.0466	.2305		-00.6	-0.122	.0420	.1733
	00.0	-0.134	.0438	.2241		-00.2	-0.096	.0405	.1622
	00.6	-0.094	.0454	.2312		00.4	-0.063	.0390	.1472
	01.9	0.018	.0466	.2412		01.9	0.017	.0384	.1111
	04.1	0.243	.0571	.2021		03.7	0.120	.0433	.0653
	06.0	0.437	.0895	.1617		05.8	0.250	.0573	.0049
	08.0	0.576	.1286	.1370		07.9	0.360	.0789	-.0473
	10.0	0.705	.1711	.1039		09.8	0.471	.1083	-.0989
	11.4	0.823	.2122	.0525		13.8	0.684	.1877	-.2001
						17.9	0.893	.3007	-.3025
1.00	-05.7	-0.717	.1380	.4341	2.22	-05.7	-0.307	.0707	.2383
	-03.7	-0.520	.0944	.3605		-03.6	-0.218	.0499	.1915
	-01.7	-0.335	.0719	.3143		-01.8	-0.138	.0375	.1502
	-00.2	-0.191	.0628	.2927		-00.1	-0.070	.0313	.1164
	00.2	-0.146	.0635	.2852		00.3	-0.048	.0304	.1068
	00.7	-0.103	.0618	.2759		00.8	-0.029	.0294	.0973
	02.3	0.046	.0634	.2501		02.4	0.035	.0297	.0662
	04.4	0.254	.0825	.1992		04.3	0.122	.0353	.0240
	10.3	0.776	.1975	-.0114		06.3	0.203	.0462	-.0147
	14.1	1.054	.3162	-.1405		08.3	0.291	.0638	-.0572
						10.4	0.380	.0887	-.0983
						14.3	0.554	.1552	-.1802
						18.3	0.723	.2480	-.2576
1.10	-05.8	-0.679	.1357	.4168					
	-03.7	-0.505	.0960	.3496					
	-01.7	-0.324	.0707	.2964					
	-00.3	-0.181	.0604	.2713					
	00.2	-0.133	.0595	.2629					
	00.7	-0.092	.0588	.2541					
	02.2	0.042	.0612	.2291					
	04.2	0.223	.0740	.1743					
	06.2	0.403	.1031	.1084					
	08.2	0.560	.1388	.0476					
	10.3	0.711	.1865	-.0126					
	14.1	0.986	.2998	-.1457					

TABLE I.- LONGITUDINAL AERODYNAMIC CHARACTERISTICS - Continued
(f) BVWH; $\delta = -20^\circ$

M	α , deg	C_L	C_D	C_m	M	α , deg	C_L	C_D	C_m
0.70	-06.1	-0.620	.1148	.2630	1.30	-06.0	-0.609	.1417	.4478
	-04.0	-0.447	.0784	.2292		-04.0	-0.461	.1046	.3845
	-02.0	-0.287	.0603	.2106		-01.9	-0.304	.0802	.3212
	-00.6	-0.170	.0518	.2005		-00.5	-0.193	.0709	.2862
	-00.1	-0.128	.0504	.1952		00.0	-0.151	.0691	.2736
	00.3	-0.099	.0491	.1918		00.5	-0.121	.0680	.2640
	01.8	0.010	.0487	.1826		02.0	-0.012	.0677	.2286
	03.9	0.168	.0559	.1731		04.0	0.141	.0762	.1771
	05.8	0.321	.0740	.1568		06.0	0.289	.0940	.1191
	07.8	0.474	.1082	.1315		07.9	0.442	.1224	.0600
	09.8	0.567	.1442	.0944		09.9	0.580	.1592	.0067
						13.9	0.833	.2517	-.1073
0.90	-05.9	-0.750	.1391	.3780	1.70	-06.2	-0.464	.1179	.3715
	-03.8	-0.539	.0938	.3066		-04.1	-0.347	.0872	.3135
	-01.9	-0.326	.0706	.2706		-02.2	-0.234	.0663	.2560
	-00.4	-0.180	.0589	.2455		-00.7	-0.149	.0575	.2190
	00.1	-0.146	.0602	.2538		-00.0	-0.118	.0553	.2049
	00.5	-0.103	.0565	.2383		00.3	-0.097	.0541	.1958
	02.0	0.026	.0578	.2355		01.8	-0.014	.0522	.1605
	04.0	0.240	.0702	.2032		03.9	0.100	.0566	.1106
	05.9	0.518	.1196	.1773		05.7	0.211	.0678	.0605
	08.0	0.586	.1366	.1128		07.8	0.327	.0880	.0077
	10.0	0.732	.1839	.0667		09.9	0.440	.1160	-.0457
1.00	-05.8	-0.739	.1579	.4677	2.22	13.8	0.654	.1926	-.1508
	-03.8	-0.561	.1185	.4073		17.7	0.860	.2957	-.2521
	-01.8	-0.362	.0926	.3603					
	-00.3	-0.214	.0841	.3365		-05.6	-0.333	.0876	.2814
	00.3	-0.166	.0819	.3284		-03.6	-0.241	.0647	.2312
	00.7	-0.128	.0812	.3208		-00.2	-0.096	.0447	.1598
	02.2	0.013	.0815	.2960		00.4	-0.073	.0432	.1483
	04.2	0.216	.1007	.2459		00.8	-0.056	.0421	.1401
	06.1	0.393	.1270	.1895		02.3	0.007	.0410	.1095
	08.2	0.572	.1652	.1183		04.3	0.094	.0446	.0662
	10.2	0.727	.2120	.0546		06.3	0.181	.0541	.0236
	14.2	1.014	.3301	-.0694		08.3	0.269	.0704	-.0204
						10.3	0.355	.0922	-.0618
						14.3	0.531	.1558	-.1450
						18.3	0.707	.2483	-.2289

TABLE I.- LONGITUDINAL AERODYNAMIC CHARACTERISTICS - Concluded
(g) BVWH; $\delta = +5^\circ$

M	α , deg	C_L	C_D	C_m	M	α , deg	C_L	C_D	C_m
0.70	-06.1	-0.430	.0555	-.0208	1.30	-06.0	-0.423	.0685	.1023
	-04.1	-0.267	.0313	-.0488		-03.9	-0.269	.0433	.0399
	-02.1	-0.117	.0201	-.0619		-02.0	-0.120	.0296	-.0166
	-00.6	-0.004	.0175	-.0726		-00.5	-0.009	.0255	-.0564
	-00.1	0.030	.0173	-.0755		00.0	0.036	.0258	-.0725
	00.4	0.074	.0192	-.0803		00.4	0.069	.0263	-.0837
	01.8	0.181	.0226	-.0904		01.9	0.191	.0332	-.1297
	03.9	0.348	.0371	-.1086		04.0	0.355	.0527	-.1939
	05.8	0.509	.0626	-.1344		05.9	0.502	.0809	-.2533
	07.9	0.678	.1057	-.1865		07.9	0.654	.1207	-.3144
	10.0	0.795	.1551	-.2525		09.9	0.800	.1699	-.3753
						13.9	1.074	.2965	-.5311
						18.0	1.316	.4529	-.6096
0.90	-05.9	-0.518	.0730	-.0118	1.70	-06.2	-0.328	.0551	.1177
	-03.9	-0.306	.0366	-.0699		-04.1	-0.213	.0353	.0628
	-01.9	-0.113	.0229	-.0963		-02.1	-0.104	.0249	.0125
	-00.4	0.017	.0191	-.1009		-00.6	-0.019	.0216	-.0268
	00.0	0.060	.0201	-.1069		-00.2	0.009	.0213	-.0397
	00.5	0.094	.0201	-.1076		00.3	0.039	.0216	-.0542
	02.0	0.241	.0269	-.1179		01.8	0.130	.0263	-.0969
	04.0	0.459	.0479	-.1482		03.8	0.251	.0398	-.1543
	06.0	0.661	.0871	-.2061		05.7	0.362	.0598	-.2074
	08.0	0.833	.1363	-.2592		07.8	0.477	.0902	-.2629
	09.9	0.995	.1952	-.3274		09.8	0.591	.1289	-.3175
						13.3	0.804	.2248	-.4185
						17.3	0.995	.3479	-.5077
1.00	-05.7	-0.488	.0787	.0346	2.22	-05.7	-0.229	.0387	.0833
	-03.8	-0.298	.0513	-.0288		-03.5	-0.137	.0247	.0405
	-01.7	-0.111	.0352	-.0763		-01.5	-0.062	.0171	.0048
	-00.2	0.028	.0302	-.0959		-00.1	0.011	.0167	-.0292
	00.3	0.072	.0312	-.1027		00.4	0.030	.0169	-.0379
	00.7	0.115	.0328	-.1092		00.7	0.049	.0175	-.0472
	02.2	0.266	.0401	-.1323		02.3	0.115	.0220	-.0785
	04.2	0.476	.0669	-.2035		04.3	0.201	.0335	-.1191
	06.1	0.669	.1078	-.2836		06.2	0.290	.0508	-.1619
	08.1	0.856	.1610	-.3689		08.3	0.373	.0743	-.2038
	10.2	1.021	.2222	-.4457		10.3	0.460	.1044	-.2469
	14.2	1.312	.3740	-.5870		14.2	0.636	.1841	-.3356
	18.2	1.548	.5534	-.7310		18.3	0.812	.2938	-.4232
1.10	-05.8	-0.466	.0809	.0407					
	-03.7	-0.284	.0512	-.0231					
	-01.8	-0.114	.0358	-.0719					
	-00.3	0.019	.0321	-.0958					
	00.3	0.069	.0323	-.1047					
	00.6	0.104	.0325	-.1086					
	02.1	0.252	.0409	-.1397					
	04.1	0.436	.0650	-.2022					
	06.1	0.612	.1018	-.2710					
	08.2	0.790	.1520	-.3458					
	10.1	0.934	.2073	-.4107					
	14.1	1.213	.3480	-.5467					
	18.1	1.434	.5154	-.6813					

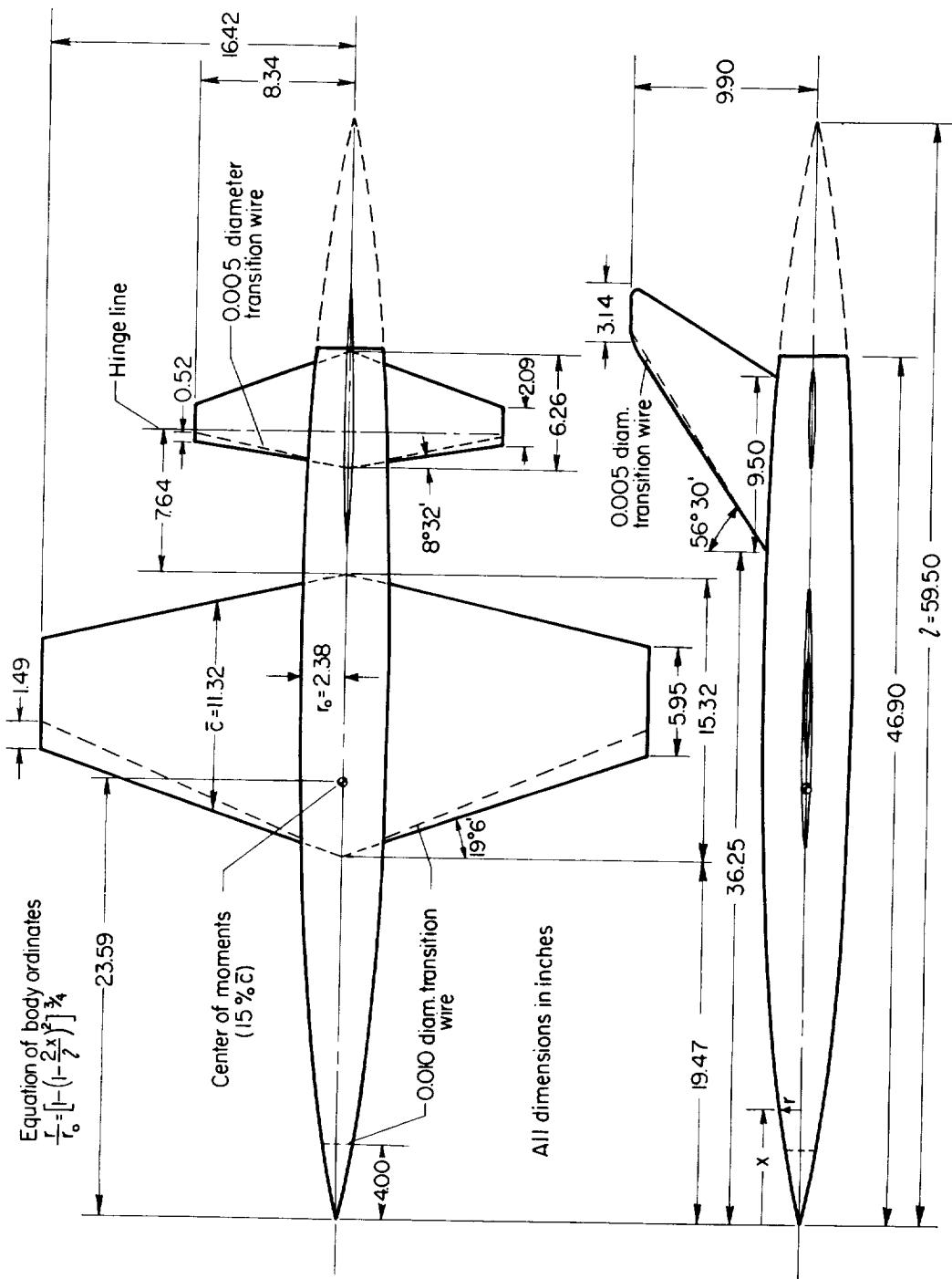
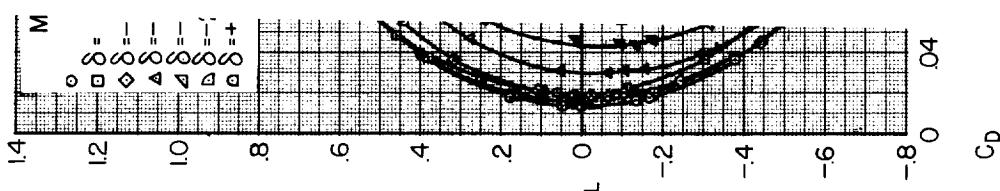


Figure 1.- Dimensional sketch of complete model.



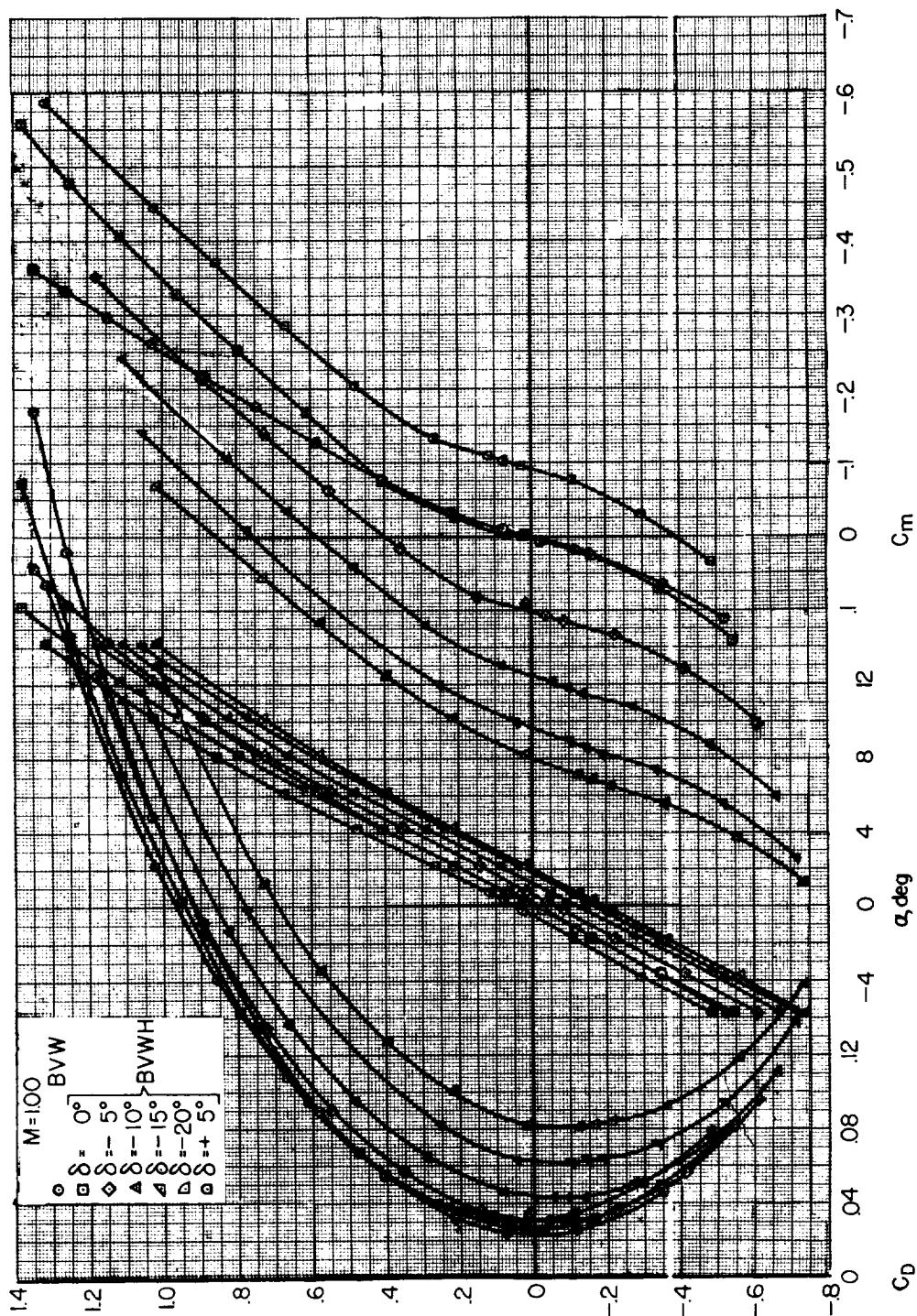
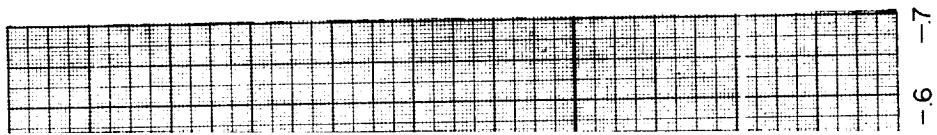


Figure 2.- Continued.

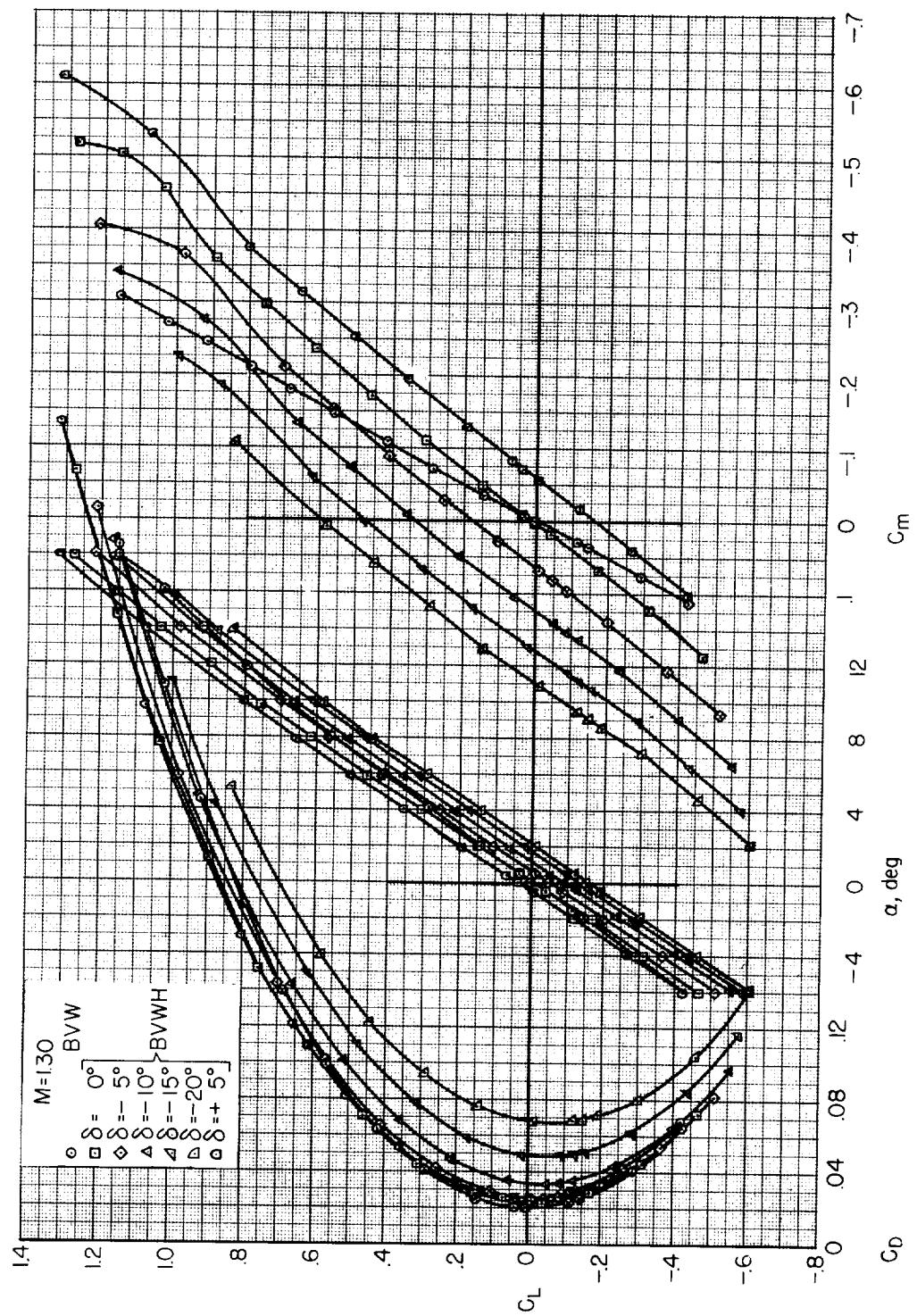
(d) $M = 1.30$

Figure 2. - Continued.

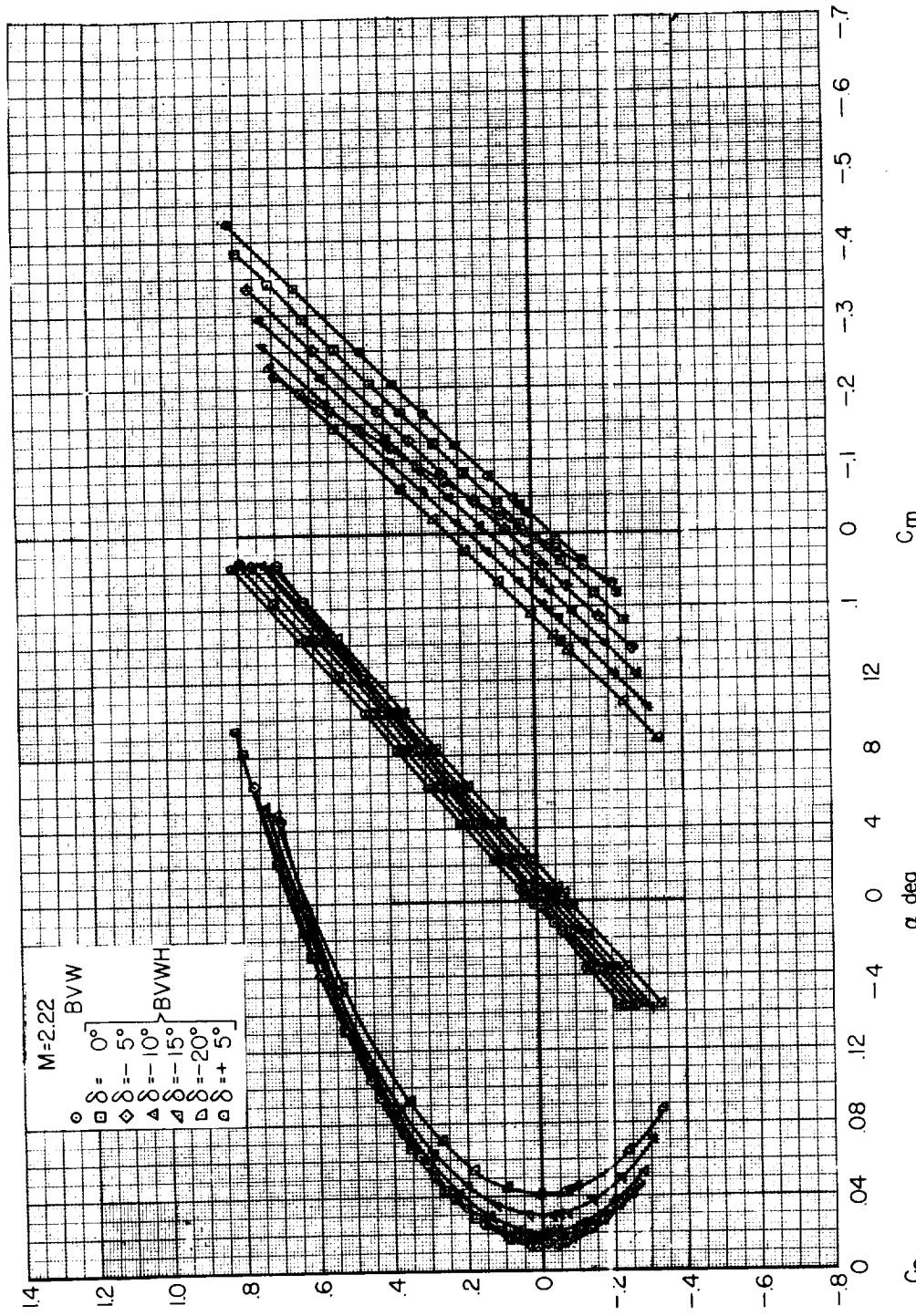


Figure 2.- Concluded.
(e) $M = 2.22$

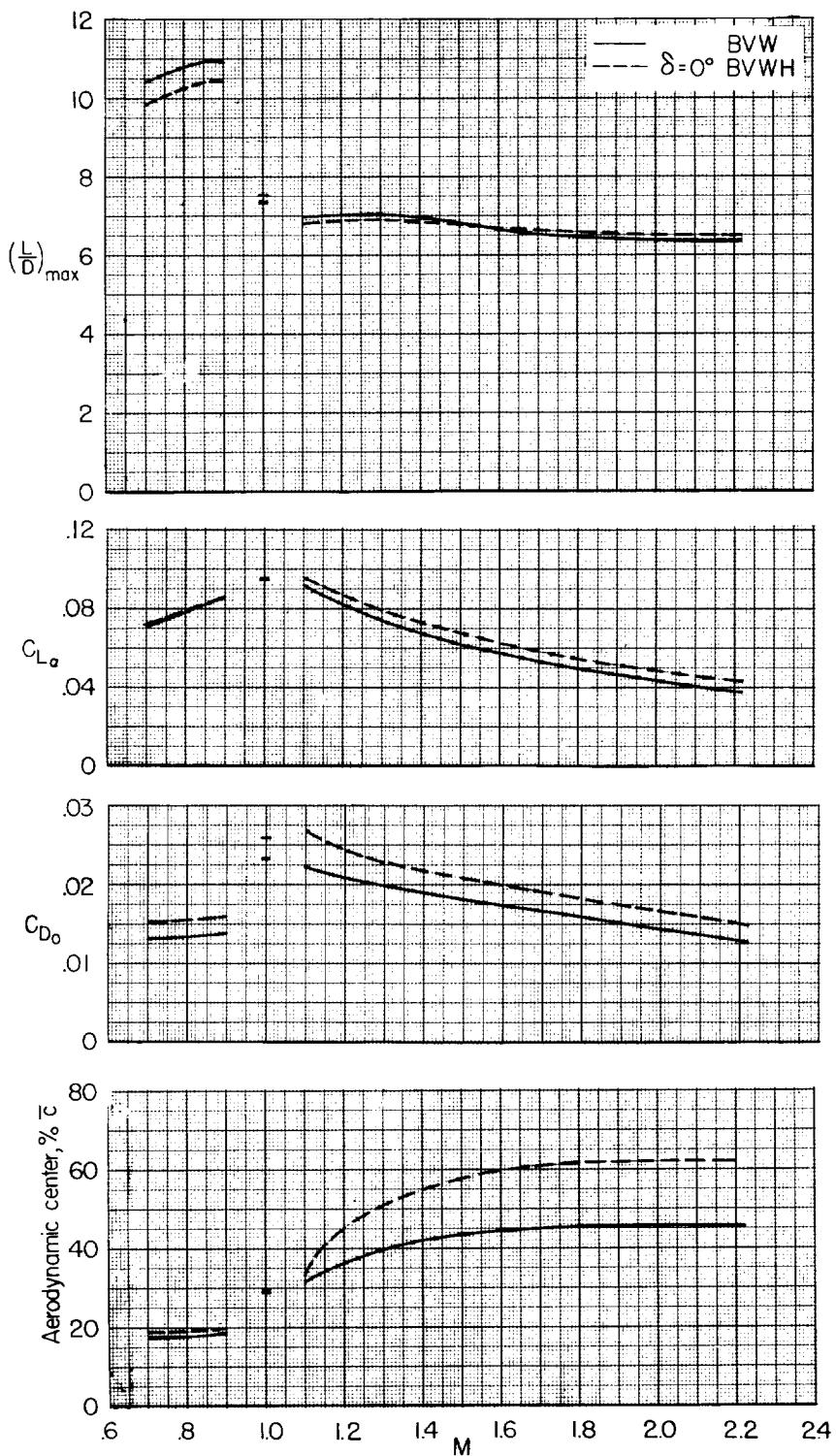


Figure 3.- Variation of maximum lift-drag ratios, lift-curve slopes, minimum drag coefficients, and aerodynamic centers with Mach number.

