#### 42<sup>nd</sup> Aerospace Mechanisms Symposium

Presenter
Jared Dervan
Date
May 15, 2014

# Development Testing and Subsequent Failure of a Spring Strut Mechanism

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# Agenda

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- Background & Approach
- Hardware Description
- Development Testing
- Root Cause Investigation
- Failure Scenario Summary and Supporting Rationale
- Follow-on Development Testing
- Lessons Learned
- Conclusion

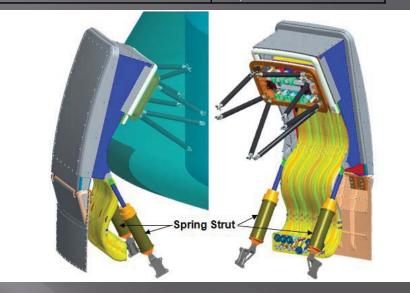
# **Background & Approach**

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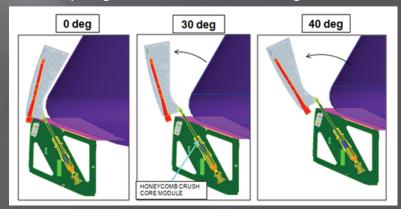
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#### Background

- Commodities transferred between CM-SM via external umbilical
- Dual spring-loaded struts drive umbilical away during separation
- No vibration testing on strut development units scoped in Orion Multi Purpose Crew Vehicle (MPCV) program plan



Spring Strut in Stowed Configuration



**Umbilical Separation** 

# **Background & Approach**

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Background (contd.)

 Problems discovered on other Orion spring assemblies during vibration testing (e.g. Spacecraft Adapter Fairing Jettison Spring (SAFJS) Assembly)



SAFJS Assembly



SAFJS Assembly Wear Post Vibration Testing

# **Background & Approach**

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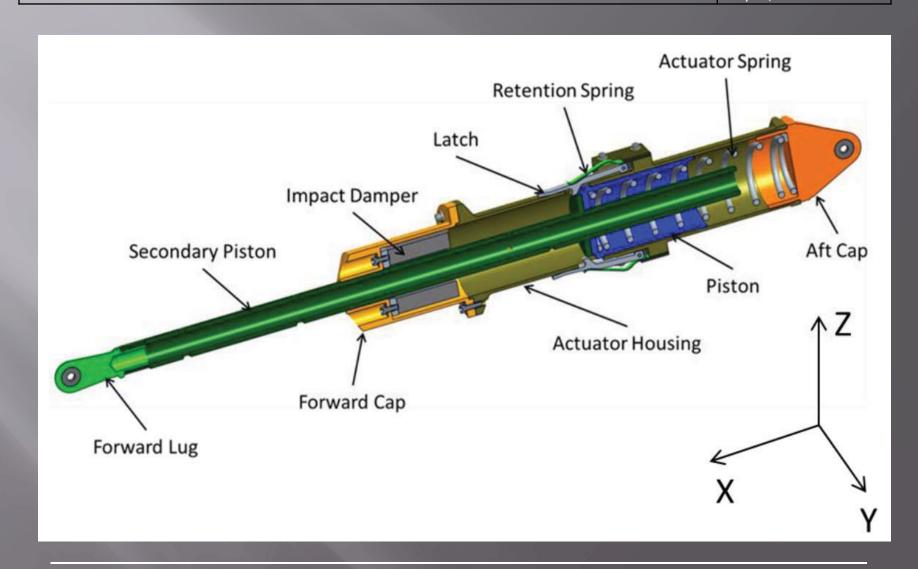
#### Approach

- Joint NASA Engineering and Safety Center (NESC) and Lockheed Martin (LM) team
  - Assessment No. 11-00747
- Perform development testing on a single Exploration Flight Test 1 (EFT-1) spring strut development unit
- Testing included functional and random vibration testing
- Preliminary results inform qualification unit development and follow-on testing

### **CM-SM Umbilical Spring Strut Detail**

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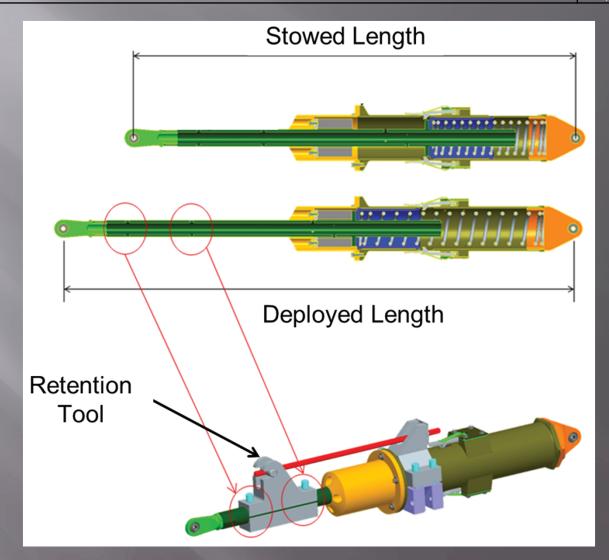
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# **Retention Tool**

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# **Random Vibration Testing**

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- Two shaker tables utilized (uncorrelated)
- Other configurations traded (single shaker (correlated); grounding one end)





Z-Axis Successful

X-Axis Successful

Y-Axis

# **Test Failure Observations**

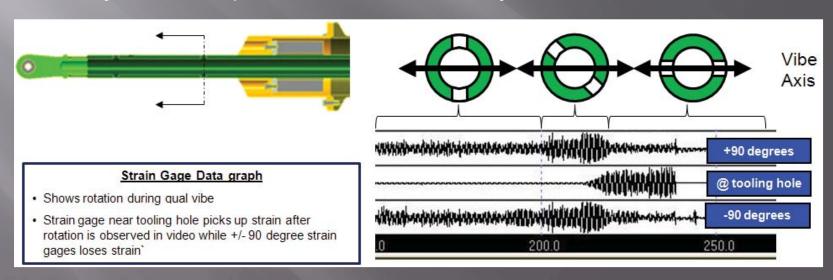
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#### **Test Failure Observations**

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- Rotation of strut forward and aft subassemblies
  - Actuator Housing rotates clockwise
  - Failure of forward subassembly lockwire
  - Counterclockwise rotation of secondary piston ~90 degrees
- Noticeable decrease in noise ~30 seconds after qualification levels applied
- Less dynamic response in strut assembly



# **Post-Test Inspection**

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- Failure of forward lockwire and loosening of Forward Lug
- Structural failure of Secondary Piston through tooling hole
- Indications of fatigue on opposite tooling hole
- Crack identified as fatigue failure at tooling hole



Forward Lug Lockwire Failure



Y-axis Post-RV



Secondary Piston Failure

# **Post-Test Inspection**

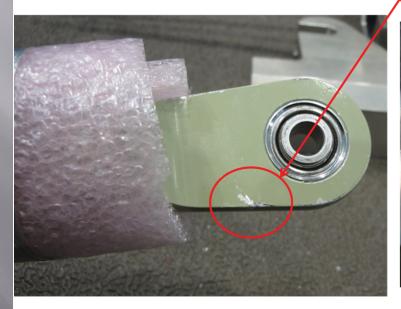
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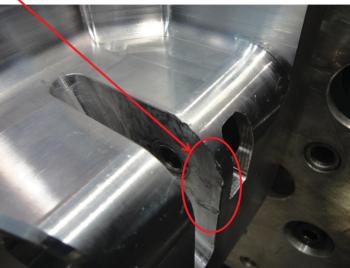
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#### External Wear

- Indications of contact at the end fittings and interfacing clevis
- Contact (rotational offset) observed during testing

Contact Locations between Forward Lug and tool clevis





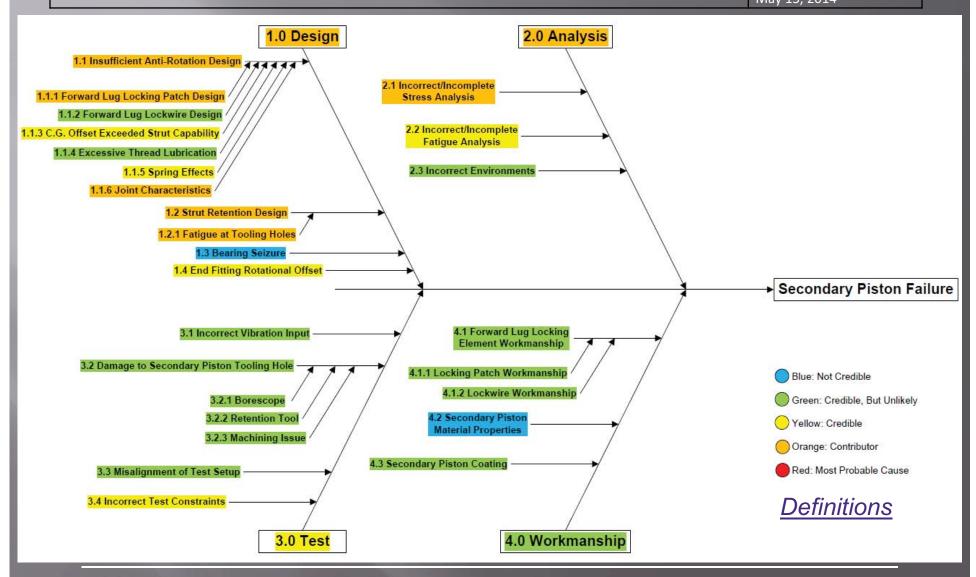
Forward Lug Wear (Post-RV)

Umbilical Side Tool Wear (Post-RV)

## **Fishbone**

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# **Failure Scenario Summary**

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- 1. Rotational misalignment cause contact at end fittings
- 2. Inertial forces due to strut C.G. offset result in off-axis contact force
- 3. Induced force results in loosening torque
- 4. Torque exceeds resistive capability of joint
- 5. Lockwire breaks; rotation until C.G. offset aligns with applied force vector
- 6. Secondary piston tooling holes placed in maximum bending
- 7. Fatigue failure at secondary piston tooling hole



Rotational Misalignment (Aft Cap)

#### **Contributors:**

- 1.1.1 Forward Lug locking patch design
- 1.1.6 Joint characteristics
- 1.2.1 Fatigue at tooling holes
- 2.1 Incorrect/incomplete stress analysis

#### Credible:

- 1.1.3 C.G. offset exceeded strut capability
- 1.1.5 Spring effects
- 1.4 End fitting rotational offset
- 2.2 Incorrect/Incomplete fatigue analysis
- 3.4 Incorrect test constraints

# LM-led Development Testing

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- Due to resource constraints, LM implemented corrective actions addressing proximate cause
- NESC continued root cause investigation
- LM 2<sup>nd</sup> Development Test
  - Corrective Actions: larger locking patches; larger diameter lockwire and quantity; increase in joint preload
  - Select parts reused from previous test
  - Fatigue failure due to life exceedance on Forward Lug
- LM 3<sup>rd</sup> Development Test
  - Corrective Actions: integral forward end fitting; aft assembly locking patch removed and joint adhesively bonded
  - Select parts reused from previous test with supporting fatigue life analysis
  - Y-axis qualification test completed successfully





2<sup>nd</sup> Development Test: Forward Lug Fatigue Failure

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- Care must be taken in adapting heritage designs to new applications.
  - Actuator design adapted from another mission
  - Obsolete features were retained (forward interface)
- Threaded aluminum parts should only be used in lightly loaded applications.
  - Lower permissible preloads and severe cyclic loads promote self loosening
  - Galling potential drives uncertainty in locking torque

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Avoid designs that have the potential to utilize fastener thread locking features to react applied or induced torque in the higher level assembly.

- Thread locking features resist self loosening
- Applied loads significant relative to capability

Ensure sufficient preloads are obtained to reduce the potential for joint loosening.

- Preload much lower than best practice (25% vs. ~70% of tensile yield strength)
- Preload primary means to prevent self loosening

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Conduct machining operations prior to surface treatments to reduce the potential for crack initiation.

- Machining after anodic coating application promotes crack initiation
- Reduction in fatigue life and bending endurance limits
- Utilize dedicated tooling for locking patch process development.
  - Reduces unnecessary cycling of threads (aluminum particularly sensitive)

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- Utilize visual movement indicators for threaded joints.
  - Torque stripping flags relative motion at joints
- Conduct testing to determine the required limits on running torque for joint designs not conforming to available standards and specifications.
  - Running torque and preload recommendations dependent on joint material and geometry
  - Steel fastener recommendations not applicable
  - Compliance in joint due to hollow geometry

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Perform a bounding fatigue analysis in all possible orientations on mechanism components that are subject to rotation.

- Off-nominal contact conditions
- Joint susceptible to rotation
- Tooling hole fatigue analyzed without worst-case considerations

Review requirements, references, and methodologies used in the analyses for design applicability.

- Bending not considered in joint separation
- Standards applicable to bolted joints and fasteners

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Assess the contribution of assumed secondary effects to analysis results, and perform an analysis and correlation study that reflects the major contributors.

- C.G offset found to induce substantial loads relative to joint capability
- Sliding fits, spring buckling, and assembly tolerances driver for C.G.
   offset
- Off-axis contact condition at clevises induced loosening torque

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# Summary

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- NESC/LM spring strut development testing resulted in failure, highlighting design deficiencies
- Root cause investigation conducted and failure scenario identified
  - Evidence to support failure scenario not definitive
  - Demonstration of successful development test by LM reduces risk
  - Strengthening rationale would require more resources with limited benefit to current Orion flight opportunity
- Lessons Learned identified and communicated

# **Special Thanks**

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- NASA Engineering and Safety Center (NESC)
- Lockheed Martin Space Systems Company

# Assessment Team Members and Support

Arthur Brown (NASA MSFC)
Damon Delap (NASA GRC)
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Steven Gentz (NESC/MSFC)
Ryan Gordon (LMSSC)

Tom Irvine (Dynamic Concepts, Inc.)
Brent Knight (NASA MSFC)
Ryan Pfeiffer (LMSSC)
Ivatury Raju (NESC/LaRC)
Kyong Song (NASA LaRC)
Philip White (NASA MSFC)
Christina Williams (NESC/LaRC)

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# BACKUP

#### **Fishbone Element Classification**

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#### Definitions

- Most Probable Cause: single event or element that resulted in failure; supported by conclusive evidence with allowance for minimal reinterpretation
- Contributor: event or element that, when combined with other elements, resulted in the failure; evidence, quantitative or qualitative, must be conclusive with allowance for minimum reinterpretation
- Credible: event or element that may have contributed to the failure; conclusive evidence is not available or multiple interpretations exist such that event or element cannot be considered to satisfy the definition of 'Contributor'
- Credible, But Unlikely: event or element that has a potential to contribute to the failure; available evidence, while not conclusive, suggests event or element's potential for contribution is unlikely
- Not Credible: event or element, supported by conclusive evidence, that did not contribute to failure

## **Findings Technical Limitations**

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- Unable to prove exceedance of torque resistive capability with linear FEM (only spreadsheet calculations)
- No photographic evidence available showing misalignment of Forward Lug prior to Y-axis test
- Forward Lug wear to indicate loosening less evident
- Insufficient information on as-built assembly process
- Unverified lockwire torque capability
- C.G. offset of assembly unavailable
- Unverified spring static torque contribution

# Activities to Address Technical Limitations

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- Incorporate non-linear effects (e.g., contact conditions) and C.G. offset into FEM to measure induced torque at joint interfaces
- C.G. measurement of assembly and additional piece parts (Secondary Piston, Spring)
- Lockwire torque test
- Use empirical methods to sanity check environments
- Static compression spring torsion induced torque test

# Performance Testing

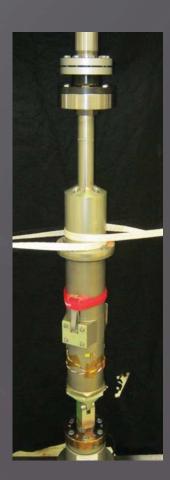
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- Ensures adequate force margin exists after being subjected to qualification levels
- Pre-random vibration
  - Both ends of strut attached to Instron through clevis
  - 'Slow' performance test measuring force vs. displacement; data compared to analytical prediction
  - Wear-in testing performed at deployment velocity; 15 cycles
- Post-random vibration
  - Secondary piston truncated aft of 1<sup>st</sup> development test failure location
  - Cupping interface to Instron at secondary piston
  - Performance test conducted at two speeds (slow and deployment)
  - Pre- and post-vibration data compared





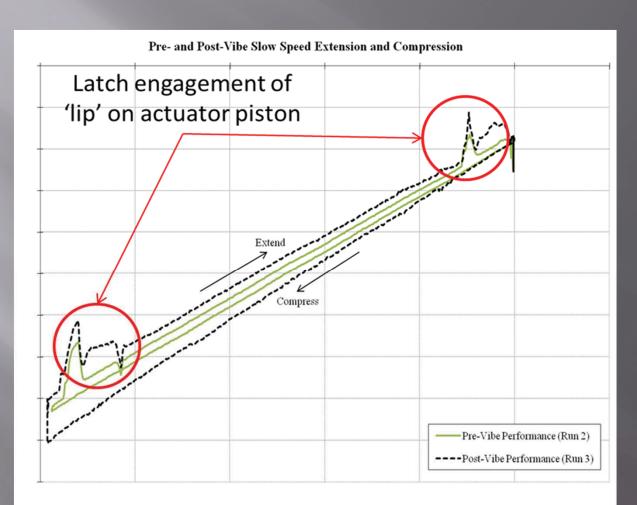


Post-RV

# **Performance Testing**

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Nominal engagement of anti-back travel latches

Results yielded acceptable force margin

### **Assessment Timeline**

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- NESC funded the fabrication at MSFC of flight-like spring strut parts using Lockheed Martin (LM) drawings
- LM assembled the spring strut and configured to flight length with help of LM Retention Tool
- Pre- and post-random vibration performance testing performed at LM Materials Technology Laboratory (MTL) (Pre-RV: 07/25/2012; Post-RV: 08/24/2012)
- Random vibration testing performed at LM Acoustics Vibration Laboratory (AVL) (08/15-16/2012, 08/20-21/2012)
  - Fatigue failure of Secondary Piston at Y-axis qualification levels
- Root cause investigation initiated (08/21/2012)
- LM assumed ownership of development test program implementing corrective actions
  - 2<sup>nd</sup> Development Test (fatigue failure, unrelated to first test) (11/28/12)
  - 3<sup>rd</sup> Development Test (success) (02/14/13)
- NESC root cause investigation completed (~02/26/13)
- Final report completed (11/07/13)

# **Post-Test Inspection**

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#### Internal Wear & Particulate Formation

- Borescope inspection between random vibration test axes (insertion through tooling hole)
- Larger particulate accumulated at Aft Cap; powder observed throughout
  - Observed existing tooling holes, latch holes, and Forward Cap-to-Secondary Piston interface during testing
  - Powder most noticeable internal to Secondary Piston



