

2014 IEEE International Symposium on Electromagnetic Compatibility
August 3-8, Raleigh NC

Simple Statistical Model to Quantify Maximum Expected EMC in Spacecraft and Avionics Boxes

Workshop Session FR-AM-2
"EMC for Space Applications"

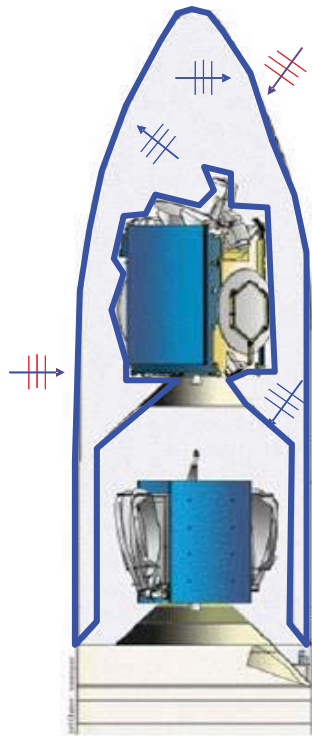
Dawn Trout Launch Services Program, NASA Kennedy Space Center
Paul Bremner Robust Physics



Robust Physics

NASA Requirement

Need to know RF environment in large fairings



- **Challenges:**

1. Interior and exterior sources

- ***C- S- and X-band transmitters***
- ***Lightning strike***
- ***External RF, interference***

2. Electrically large

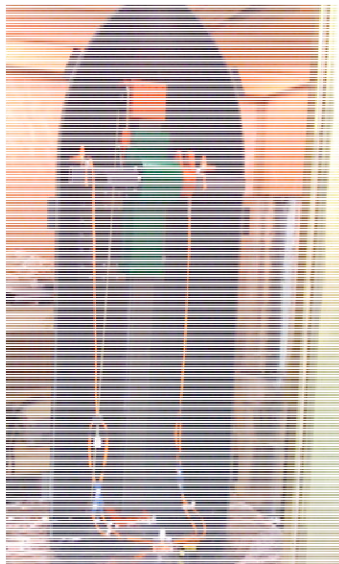
- ***Sensitive to details***

3. Details only known approximately

- ***Fairing lining dimensions***
- ***Payload dimensions***
- ***Payload surface impedances***



Model scale fairing EM field tests at KSC



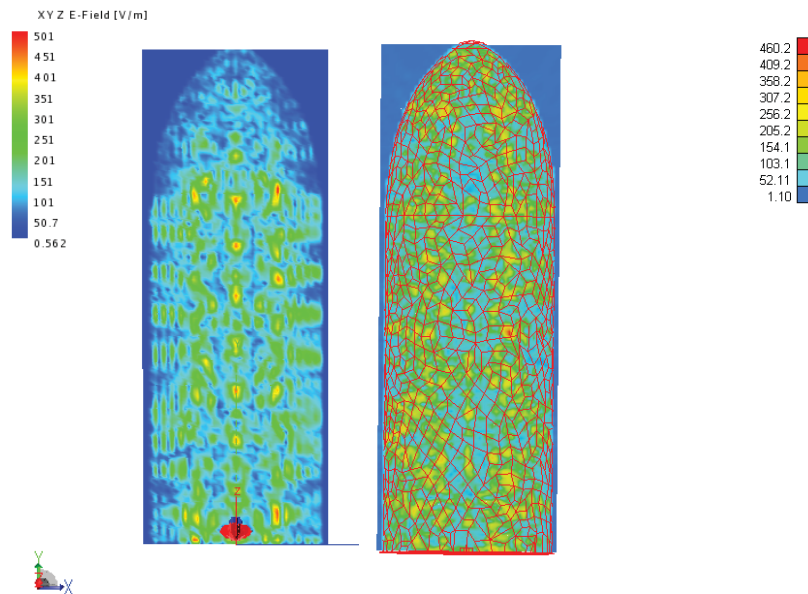
inner probe placement

Composite fairing half test set-up with fiberglass mount - outer probe positions

- **Fiber optic sensors to on a fiberglass mount used in 56 location within the fairing to measure the distribution.**
- **Spatial and frequency variation used.**



3D EM Wavefield modelers



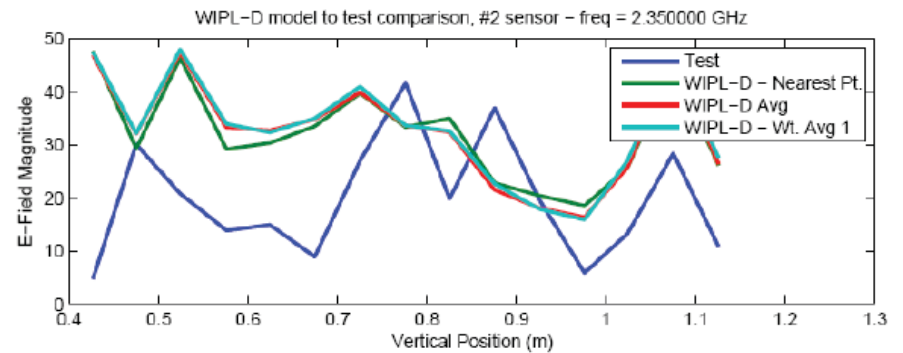
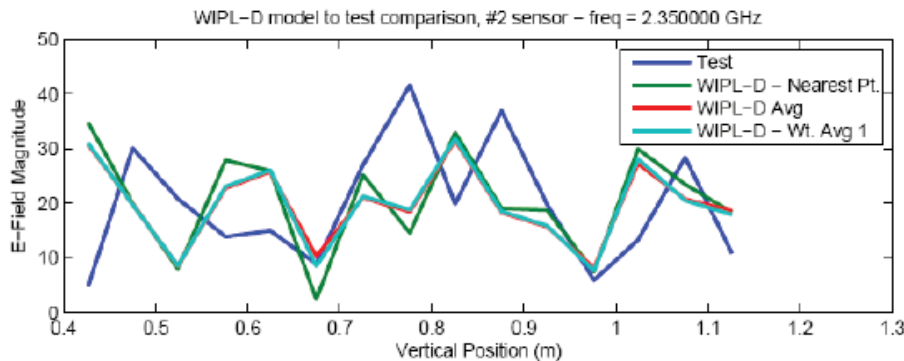
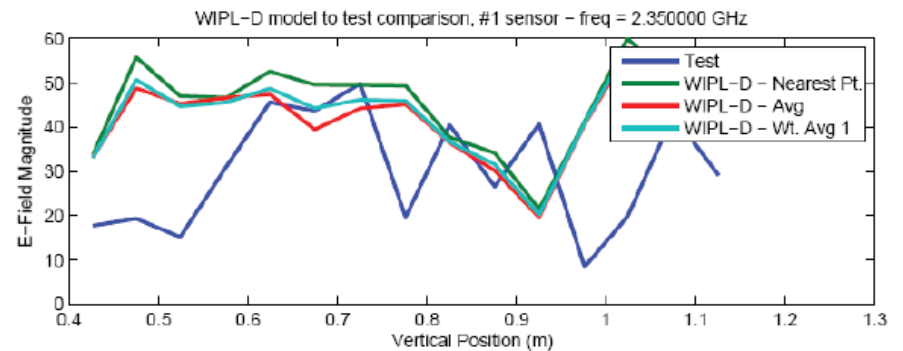
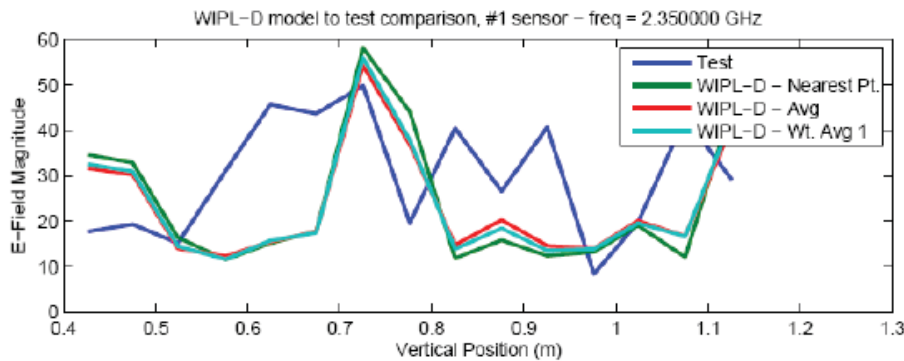
Field distribution of lossless fairing model at 5.65 GHz of small composite model MLFMM (FEKO) and MoM (WIPL-D)



Rotational model of a typical large fairing with size of lab model fields shown for comparison



Models have not correlated well with test



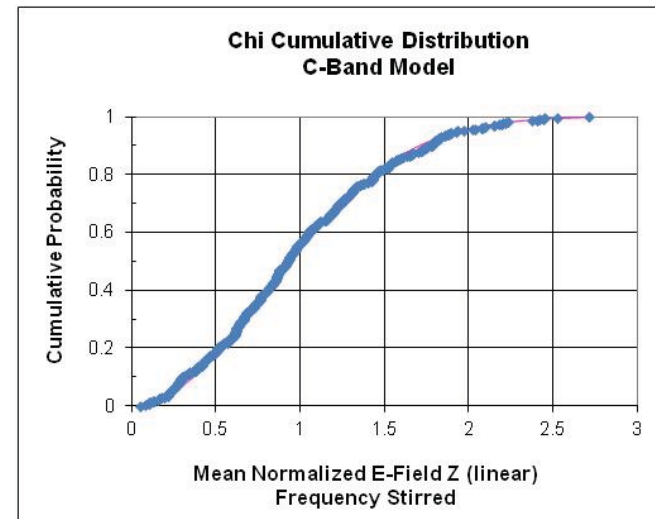
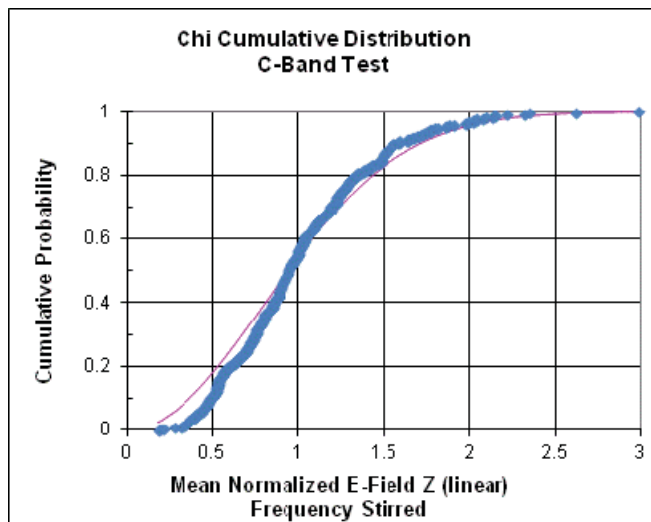
Magnitude of 3 axis E-field comparison for composite three layer model

With fiberglass mount

Without fiberglass mount



However, both model AND test show EM field collapses to 2 parameter PDF



C-Band composite fairing position and frequency stirring test and model data following Chi distribution.



Power balance (PWB) method

Recently extended to predict Variance & Max Expected E-field

An electronic enclosure of volume V has EM modal density

$$n = \frac{8\pi V f^2}{c^3}$$

The asymptotic statistical mean EM field energy in the enclosure is governed by the excitation source power and enclosure Q factor

$$E[U] = \frac{\text{Source power}}{\omega \eta}$$

Hill (2009) has shown that: $Q = 1/\eta$ $Q = \frac{3V}{2\mu_r \delta S}$, $\delta = \sqrt{\frac{1}{\pi f \mu_w \sigma_w}}$

where S is the surface area of the cavity walls μ_r , μ_w , and σ_w are respectively the relative permeability, the permeability, and the conductivity of the cavity walls.

Langley [2004] has shown the asymptotic relative variance of the cavity energy is:

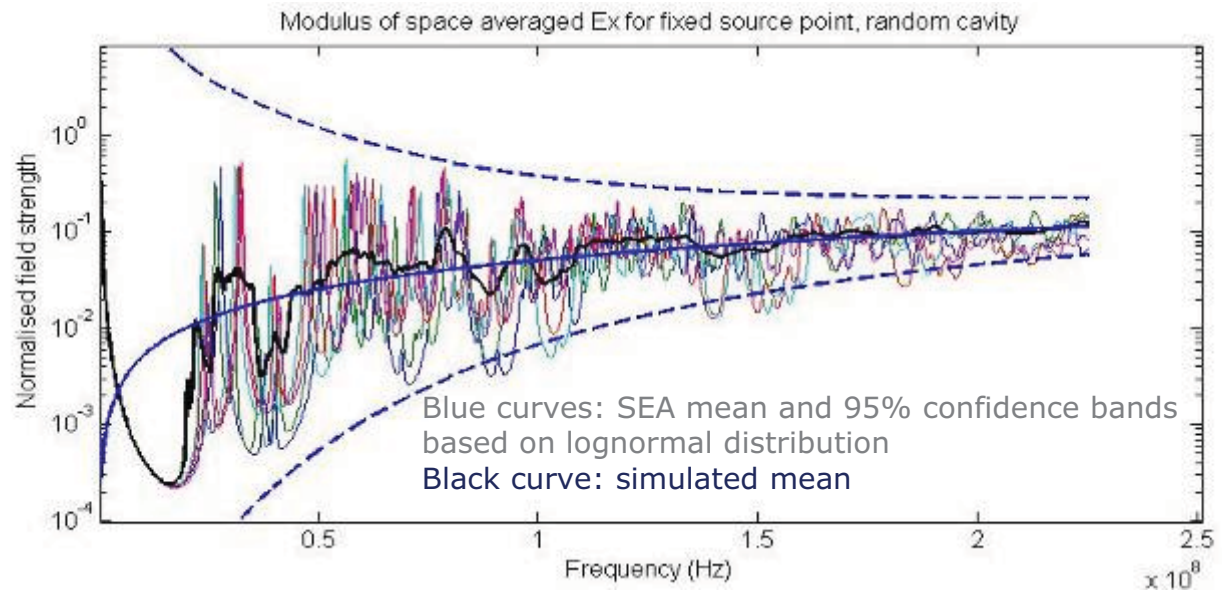
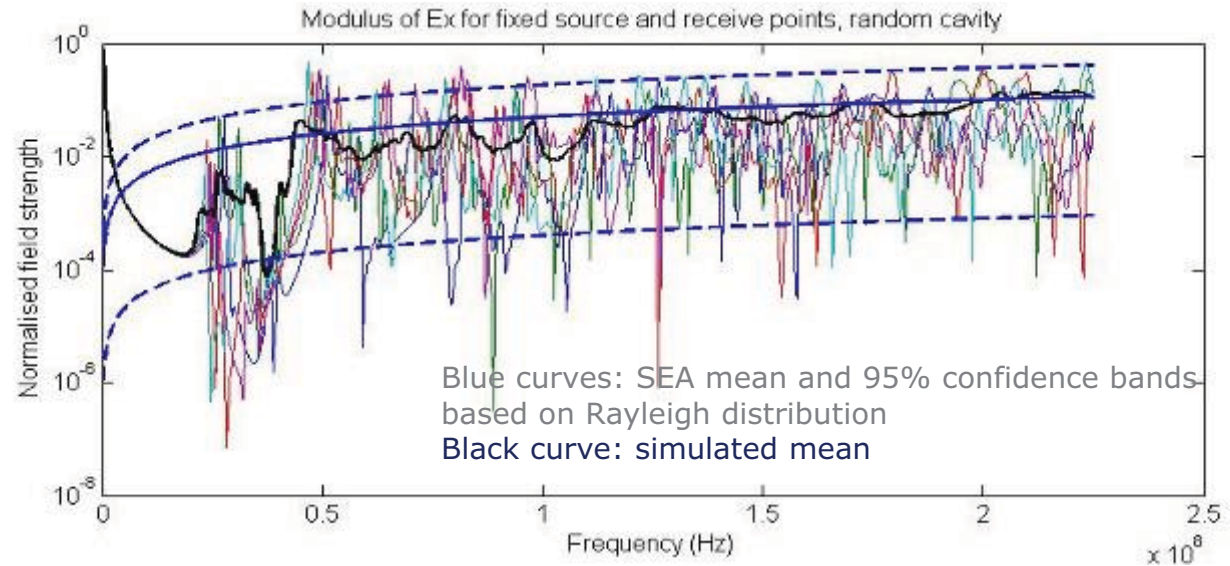
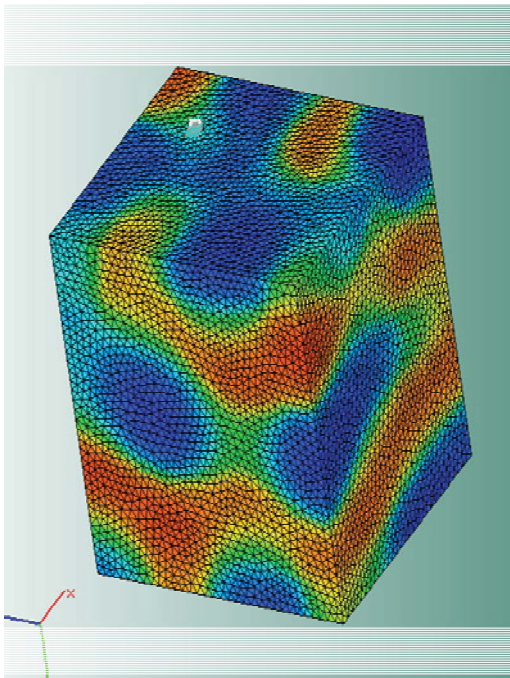
$$\text{RelVar}[U] = \frac{1}{\pi m} \left\{ \alpha - 1 + \frac{1}{2\pi m} [1 - e^{-2\pi m}] + E_1(\pi m) \left[\cosh(\pi m) - \frac{1}{\pi m} \sinh(\pi m) \right] \right\}$$

where m is the EM modal overlap factor: $m = f \eta n = f n / Q$,

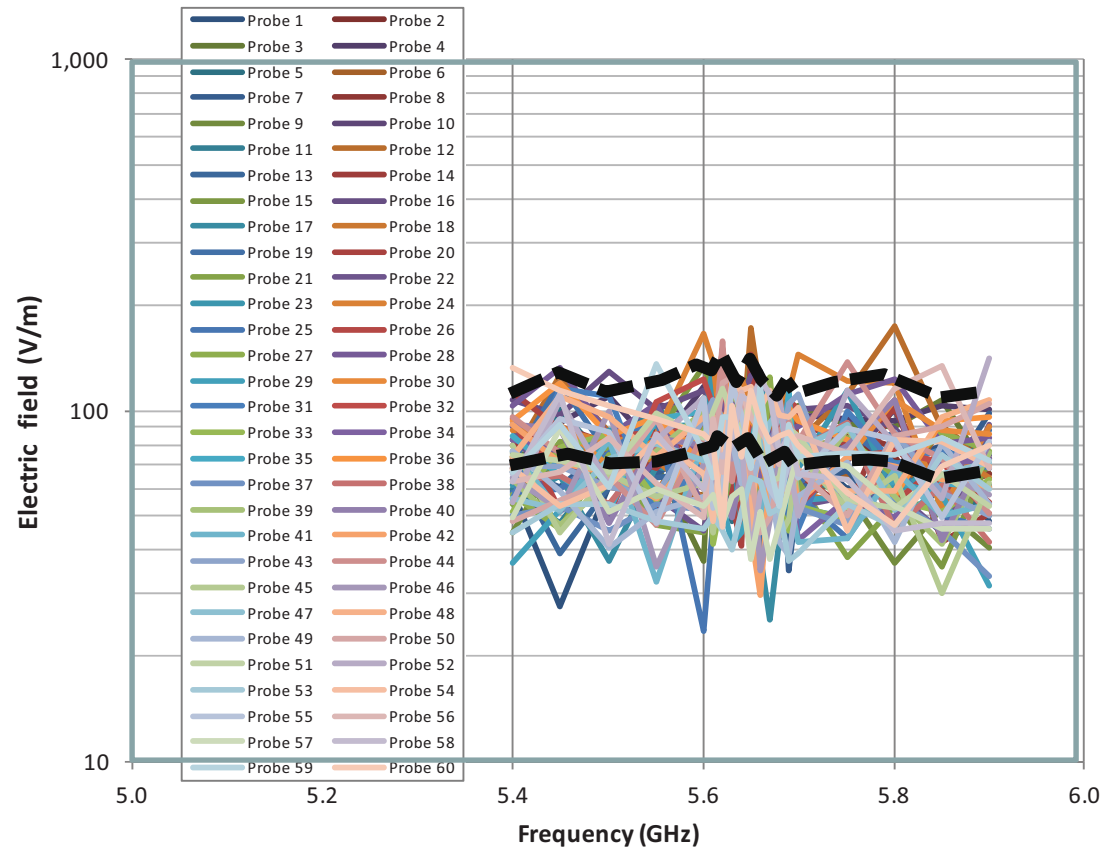
The relative variance of a field component at a point is: $1 + 2 \text{RelVar}[U]$



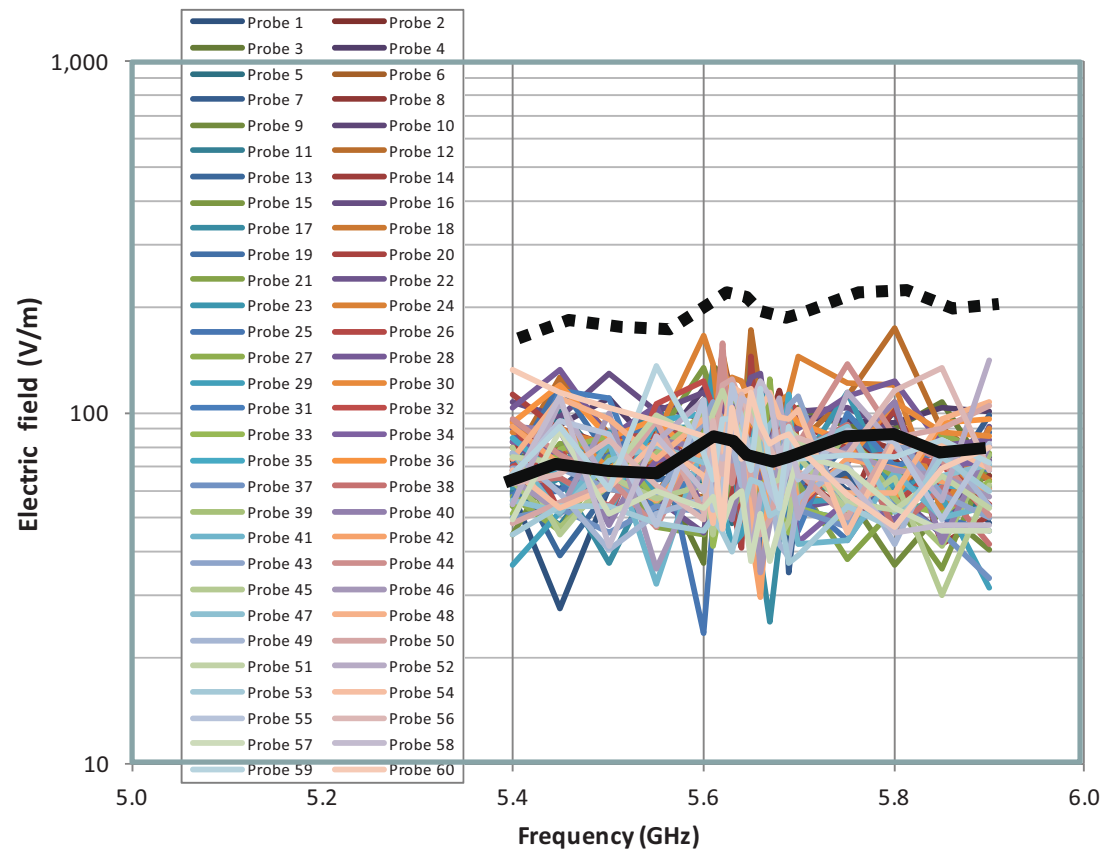
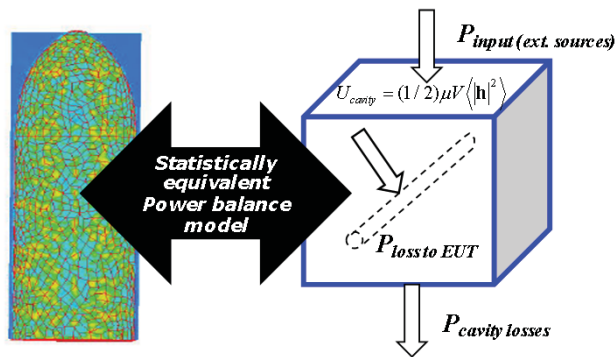
New Variance & Max Expected checked on modes of rectangular cavity



EM field Mean & Max Expected Measured



EM field Mean & Max Expected Predicted with simple PWB statistical model



Conclusions

- **Statistical PWB models look promising**
 - Ideal for complex payloads in fairings when EM design parameters are only ever known approximately
 - Statistical model predicts:
 - **Mean**
 - **Standard deviation**
 - **Max expected (eg 97.5% quartile)**
 - No time wasted meshing details
 - PWB model solves in seconds on laptop computer
 - Can also predict induced current & voltages in wiring harnesses

