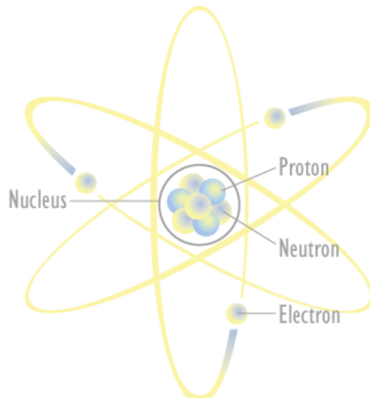
ASSESSMENT OF SHAPE MEMORY ALLOYS – FROM ATOMS TO ACTUATORS – VIA *IN SITU* NEUTRON DIFFRACTION



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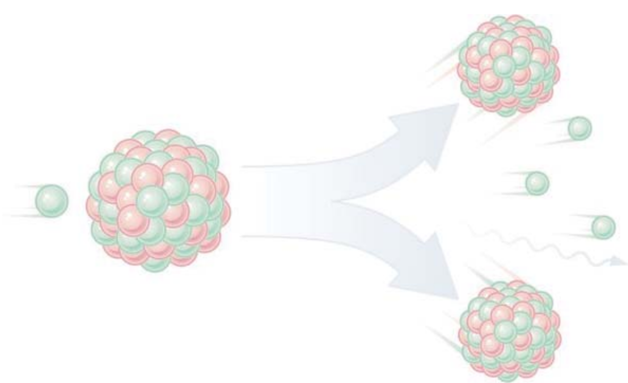

The ASME 2014 Conference on Smart Materials, Adaptive Structures and Intelligent Systems, September 8-10, 2014 – Newport, Rhode Island

It Takes a  …

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Los Alamos Neutron Science Center

Los Alamos National Laboratory

K. An and H.D. Skorpenske

Spallation Neutron Source

Oak Ridge National Laboratory

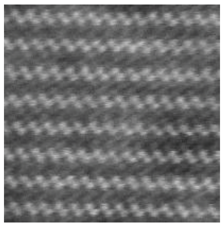
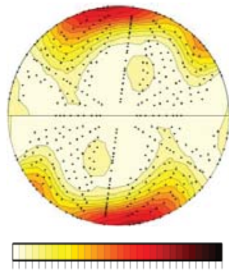
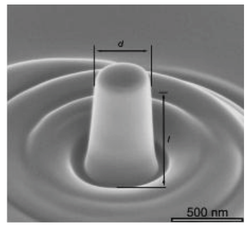
Acknowledgment

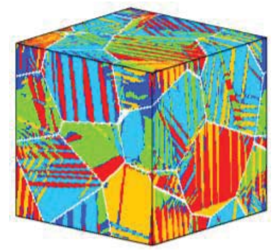
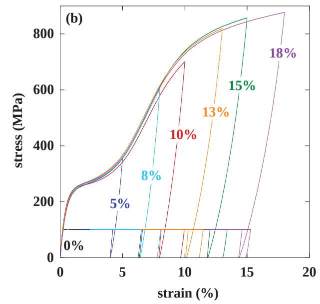
- NASA Fundamental Aeronautics Program, Fixed-Wing and Aeronautical Sciences Projects
- Basic Energy Sciences (DOE)

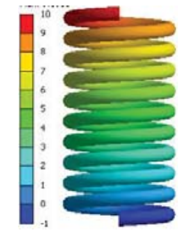
Motivation and Objectives

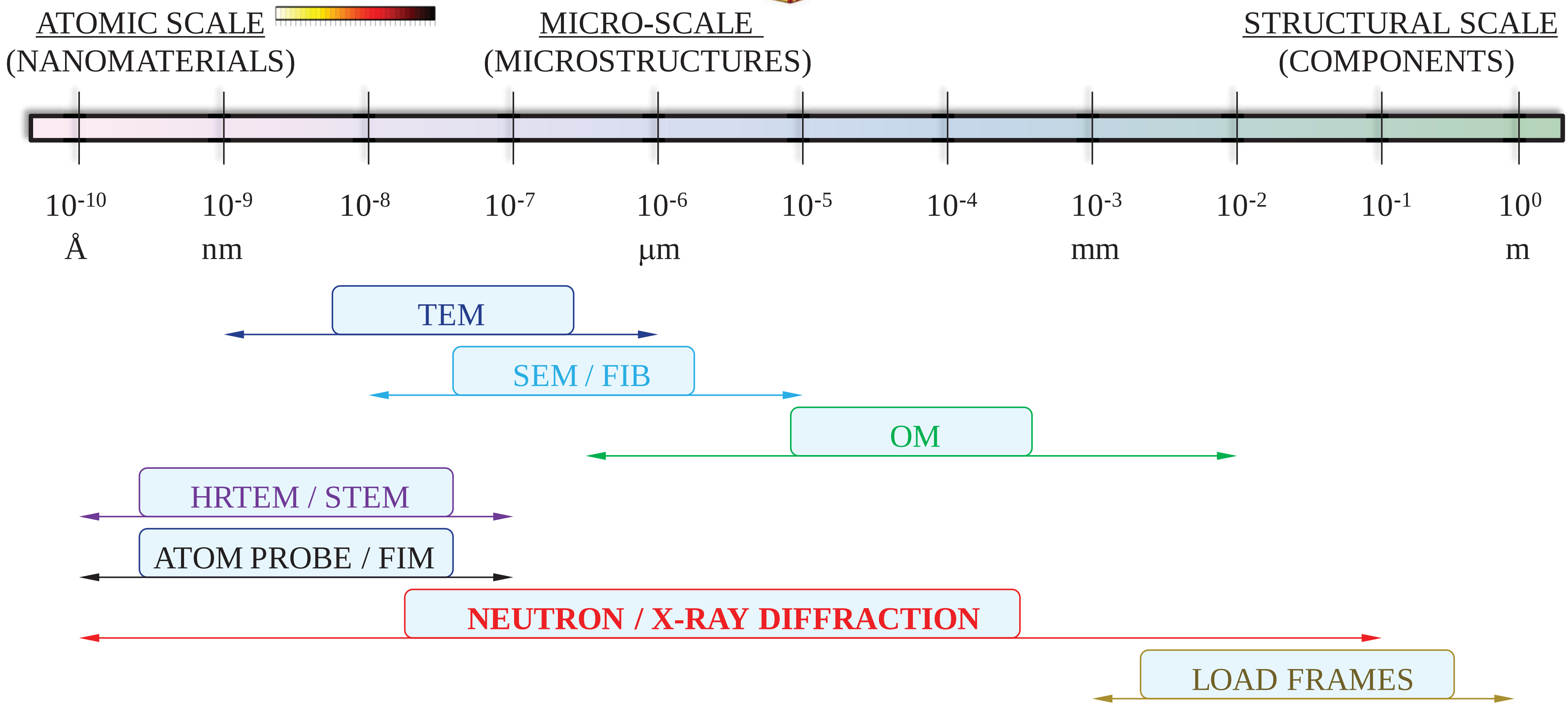
- We examine microstructures of:
  - Conventional structural materials by quenching in the high temperature structure and examining at room temperature.
  - This cannot be done for SMA's because of the diffusionless phase transformation (austenite/martensite) cannot be suppressed by quenching

Length Scale in Engineering Materials
Where Does Neutron Diffraction Fit?

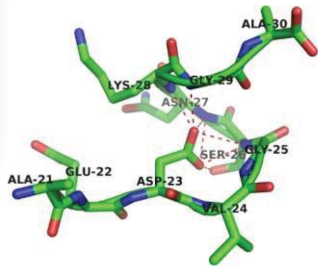


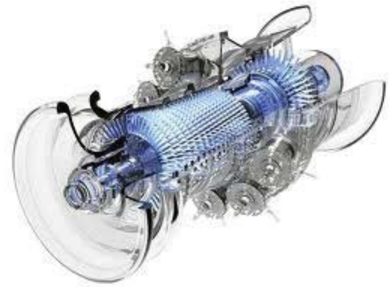
Applications of Neutron Diffraction

Chemistry

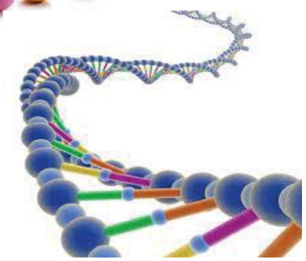
Physics



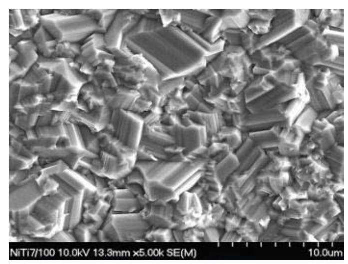
Engineering



Life sciences



Biosciences



Materials science

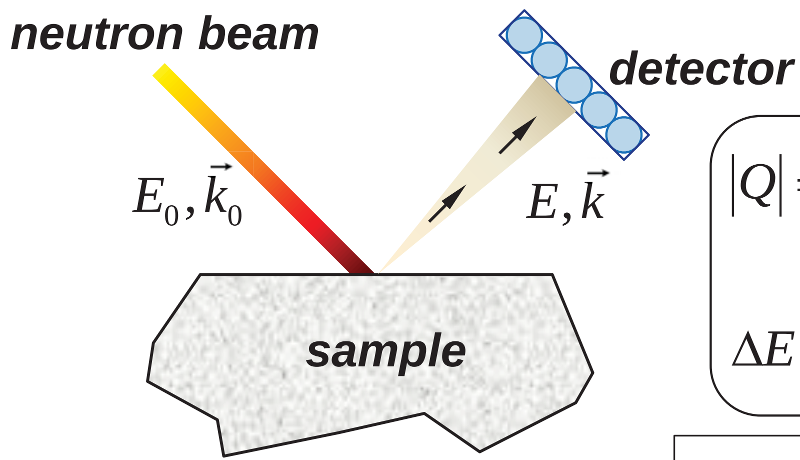
Geological sciences

Archeology

Courtesy: Mario Bieringer

Neutrons at the Experimental Area

- **Now we have neutrons, what next?**



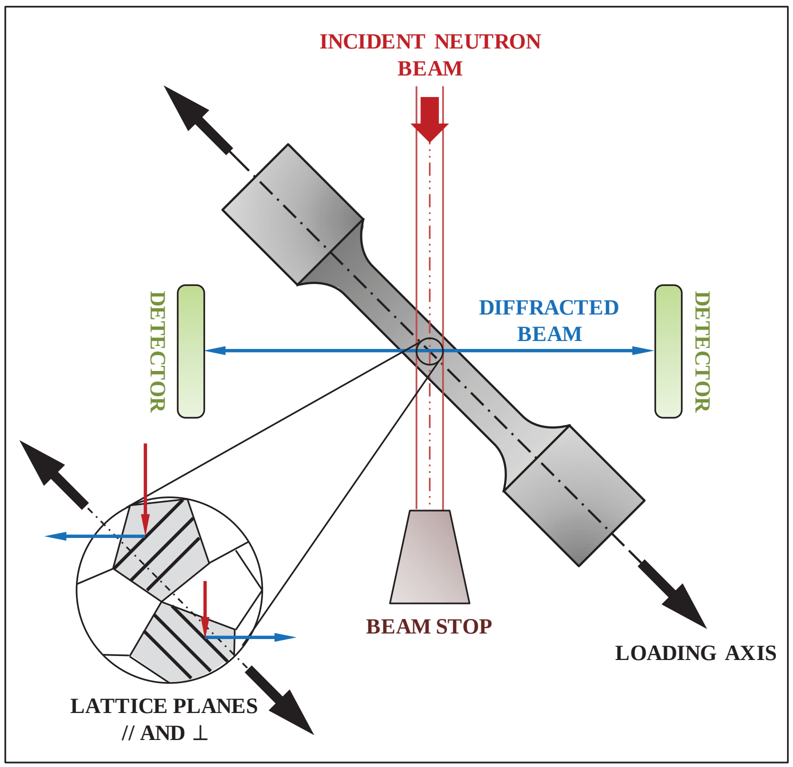
$$|Q| = |\vec{k}_0 - \vec{k}| = \frac{4\pi \sin\theta}{\lambda}$$

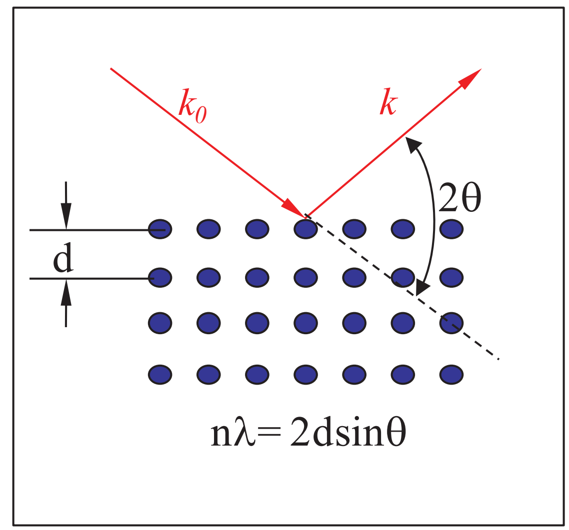
$$\Delta E = E_0 - E = \hbar\omega = \hbar^2 \frac{\left(k_0^2 - k^2\right)}{2m}$$

Nomenclature

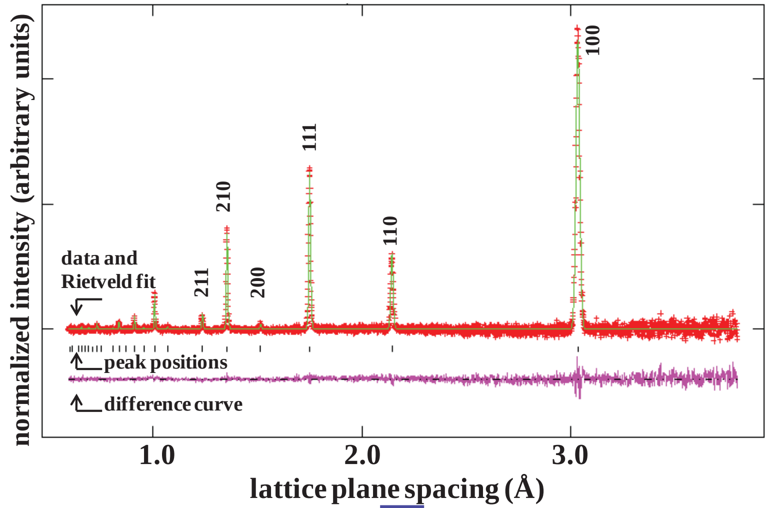
k: wavevector
E: energy
Q: scattering vector
ħ: reduced Planck constant
m: mass (1.67×10^{-24}g)
λ: wavelength
2θ: scattering angle

- Neutron beam with a known wavevector (k_0) and energy (E_0)
- Detect number of scattered neutrons with a wavevector (k) as a function of the scattering function $S(Q,\omega)$

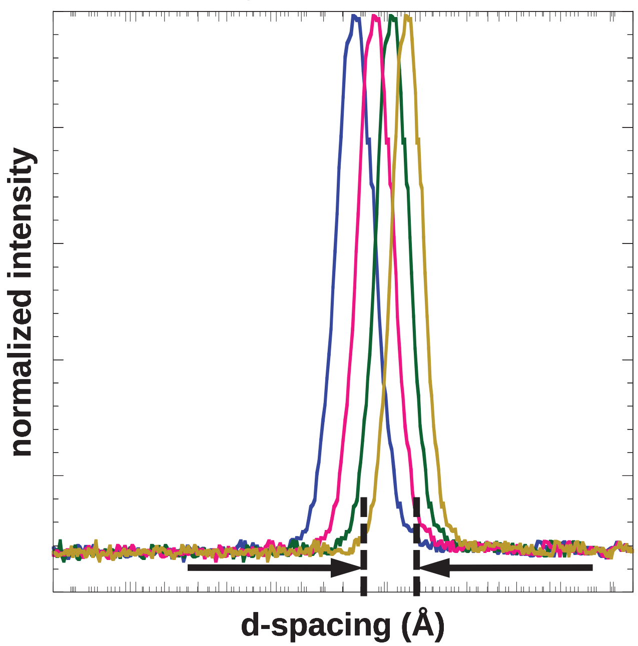




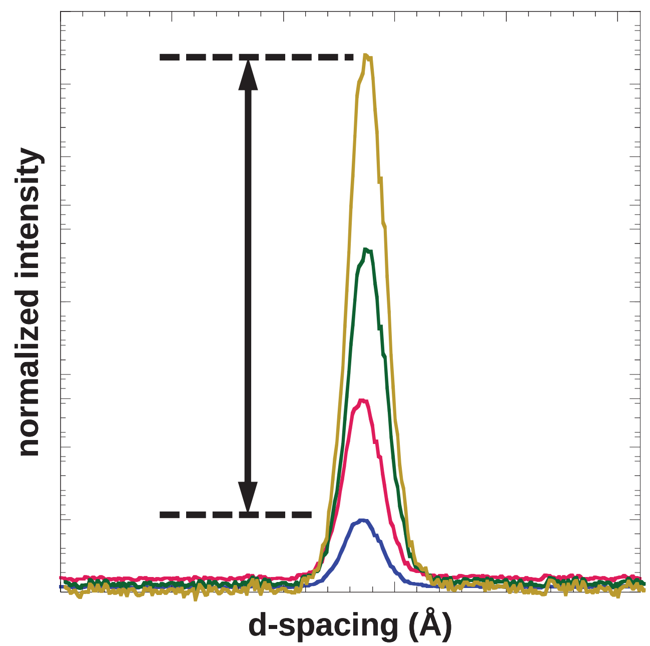
Neutron Diffraction Data



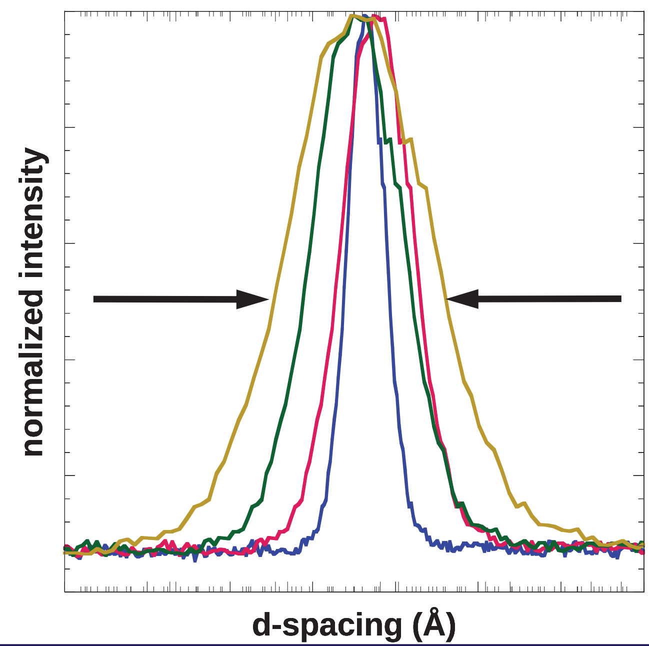
- Peak position
  - •Elastic lattice strain
  - •Intergranular strains



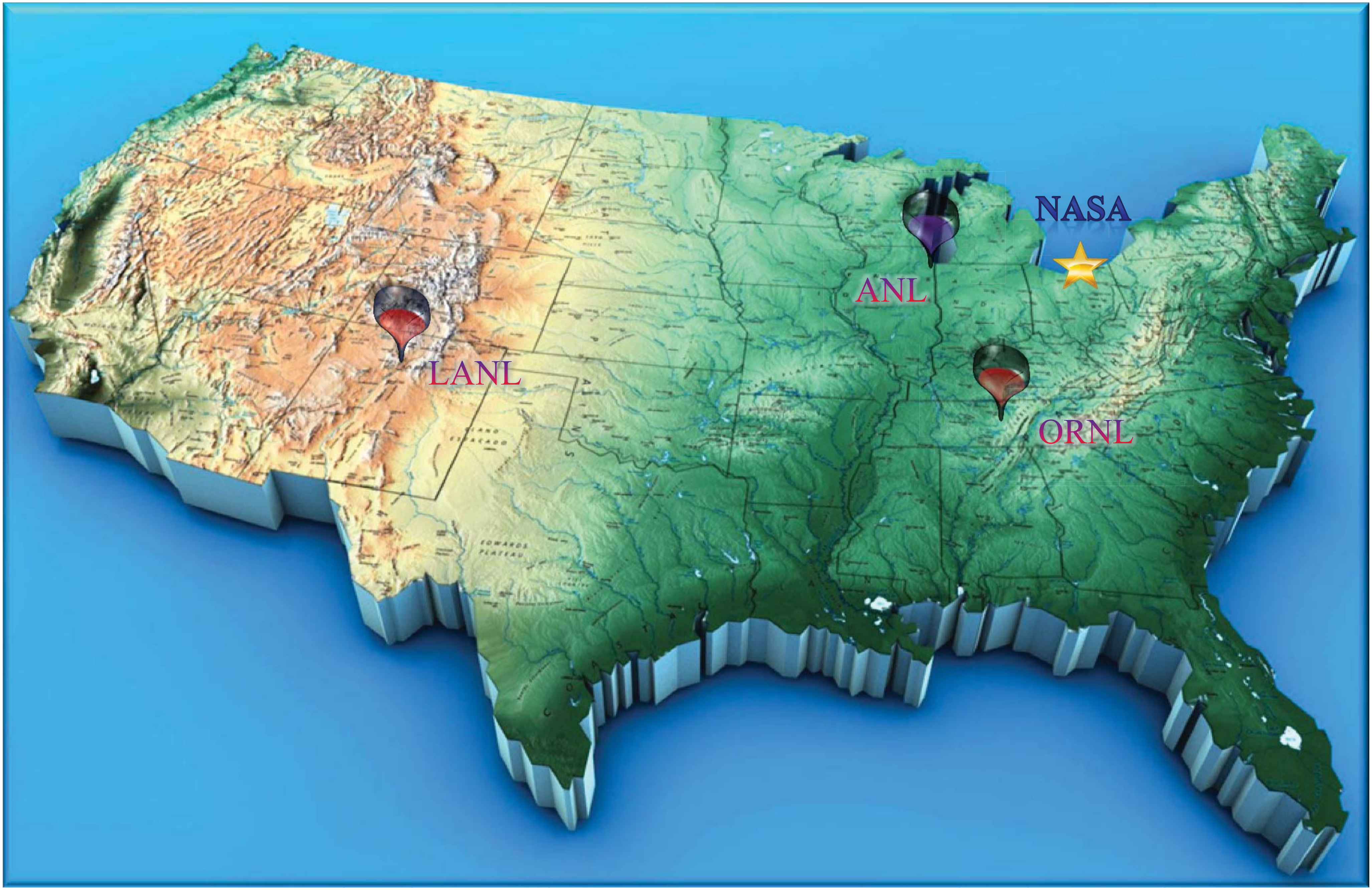
- Peak intensity
  - •Texture changes
  - •Phase fraction



- Peak width
  - •Qualitative information

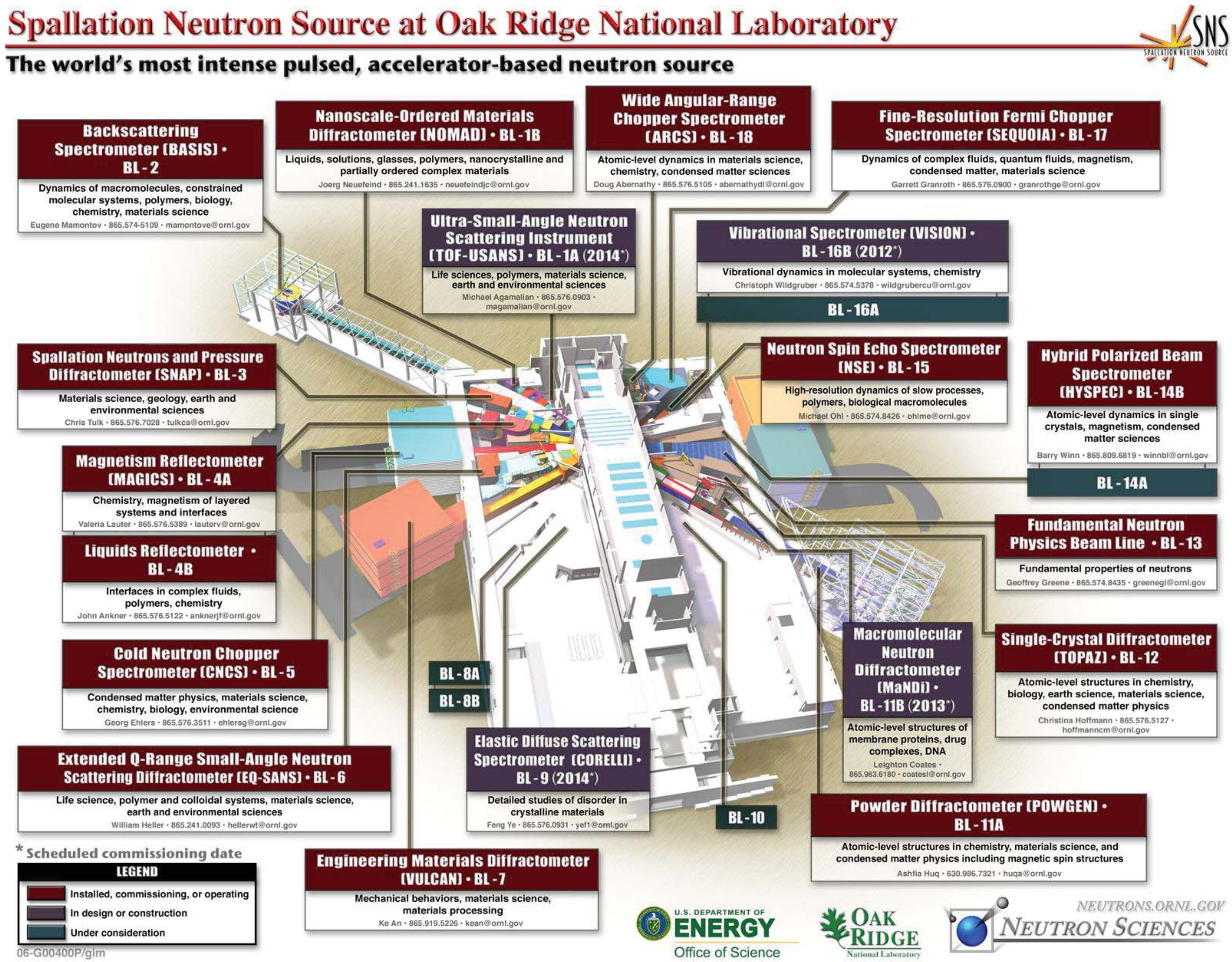


Neutron/Synchrotron Sources in the USA

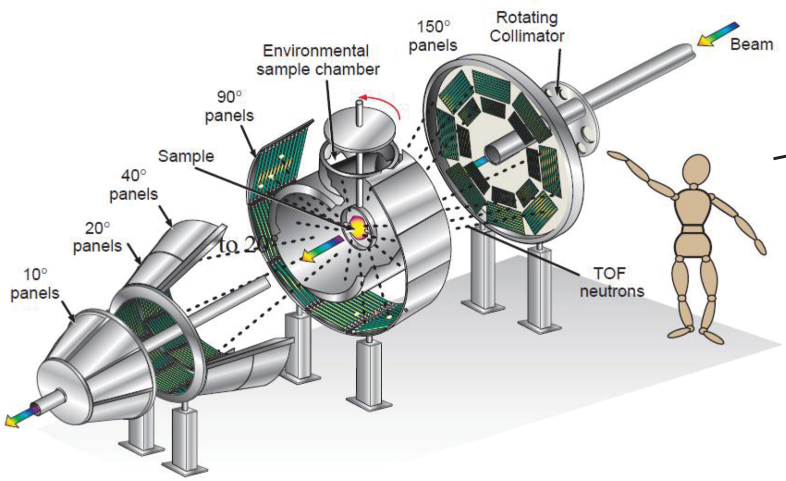


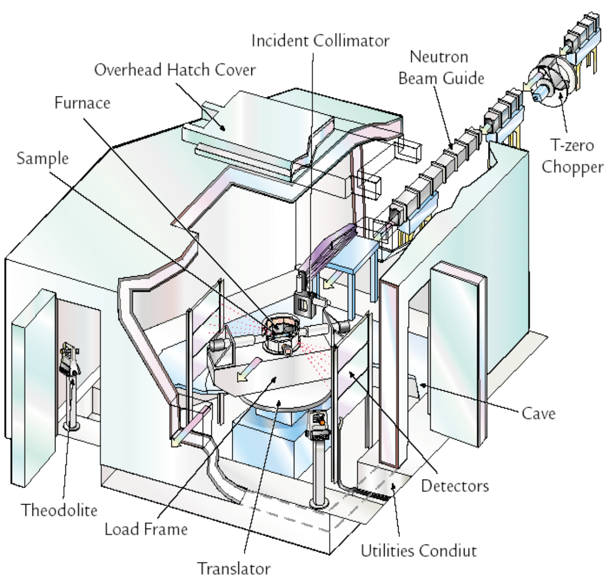
Neutron and Synchrotron Sources Around the World

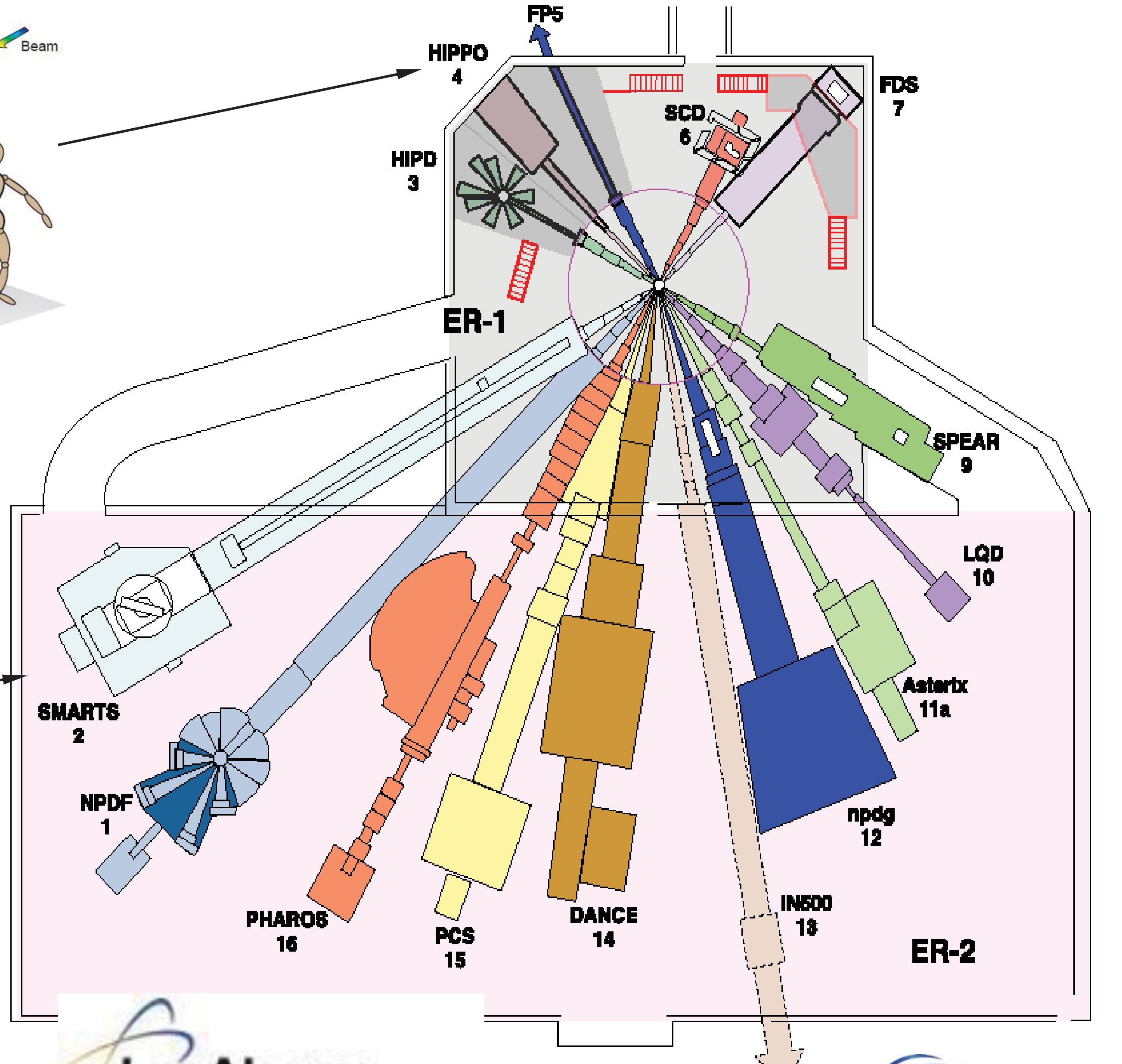
Oak Ridge National Laboratories-SNS



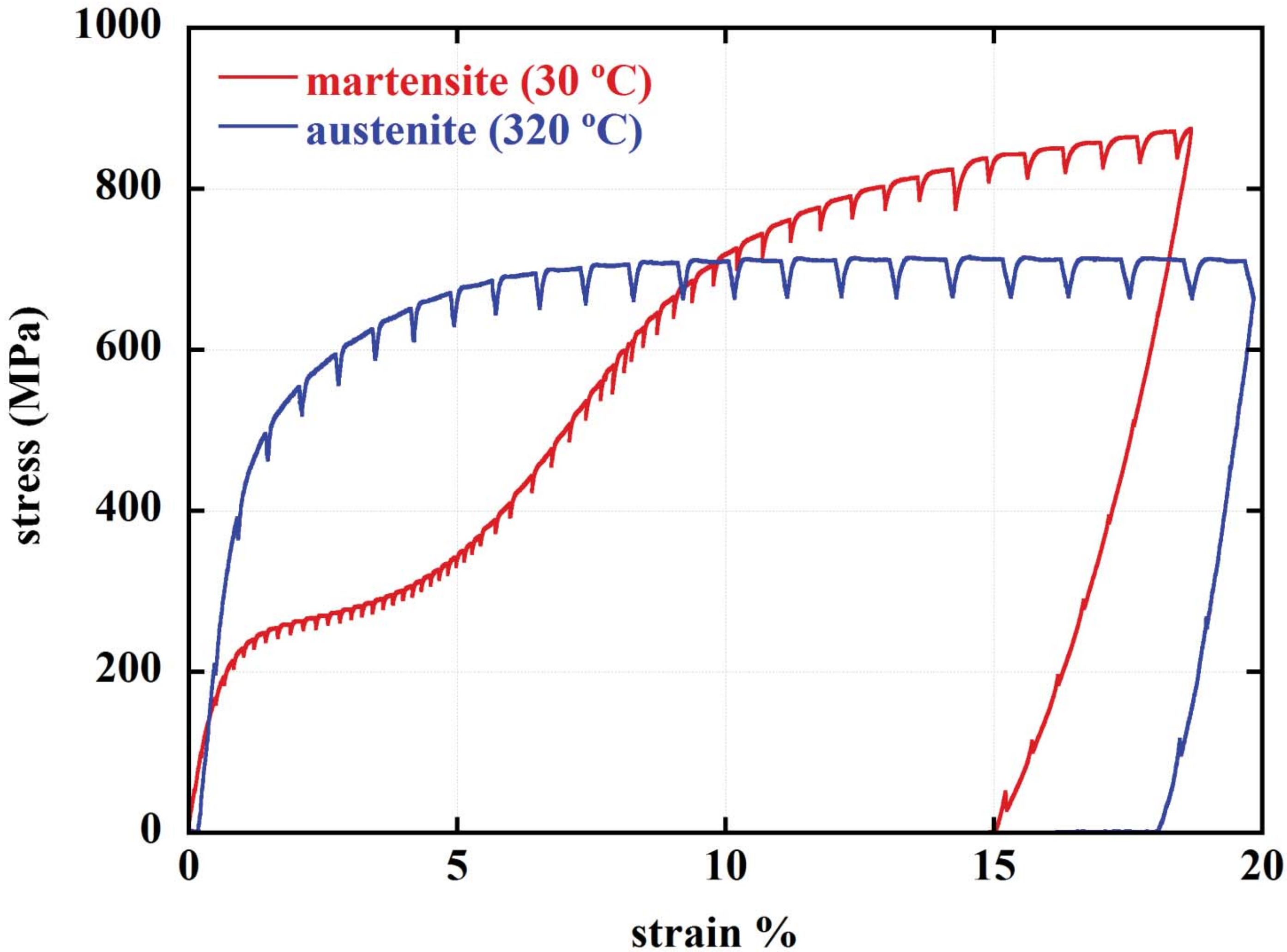
Los Alamos National Laboratory-LANSCE





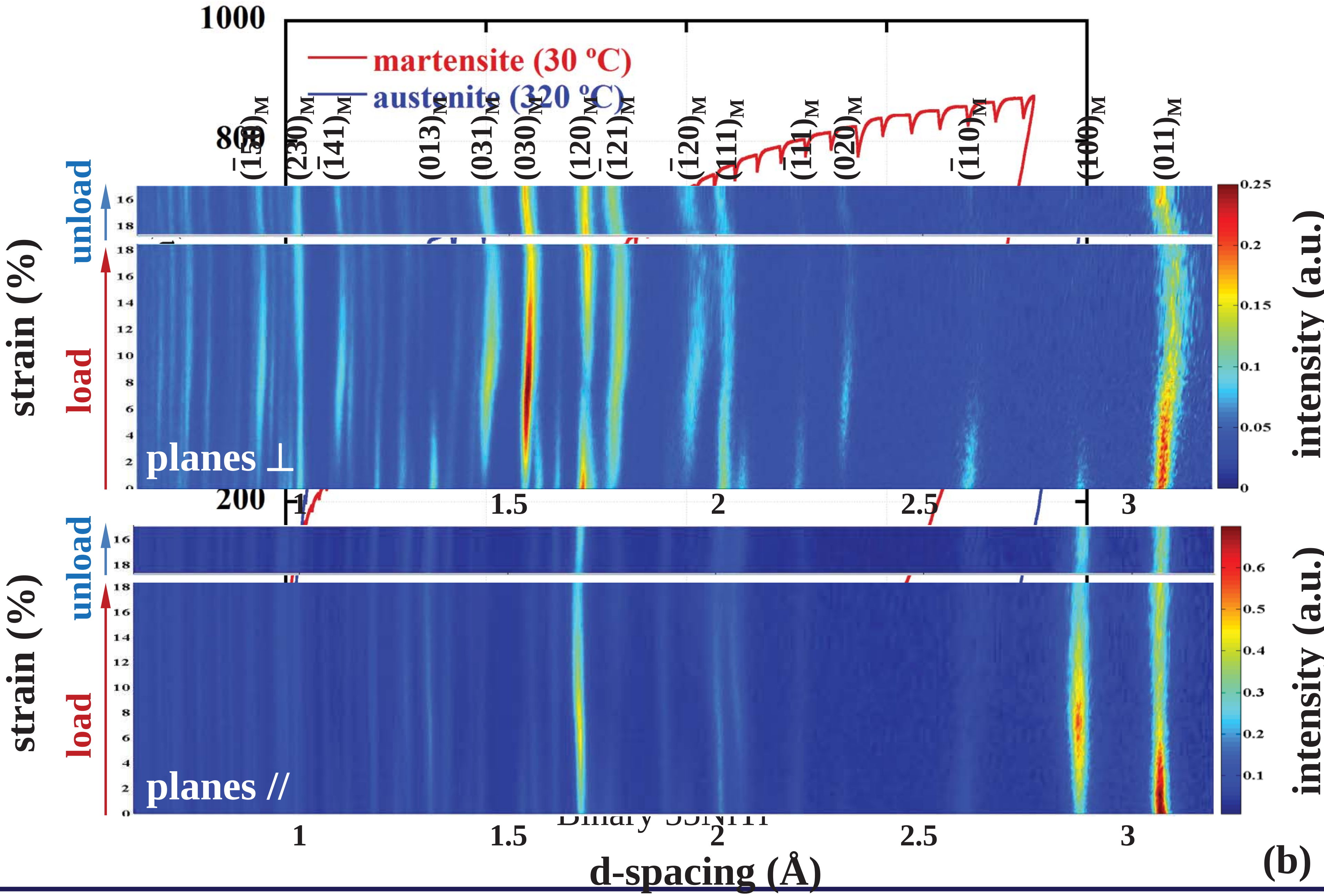


Isothermal Deformation - Loading Actuators



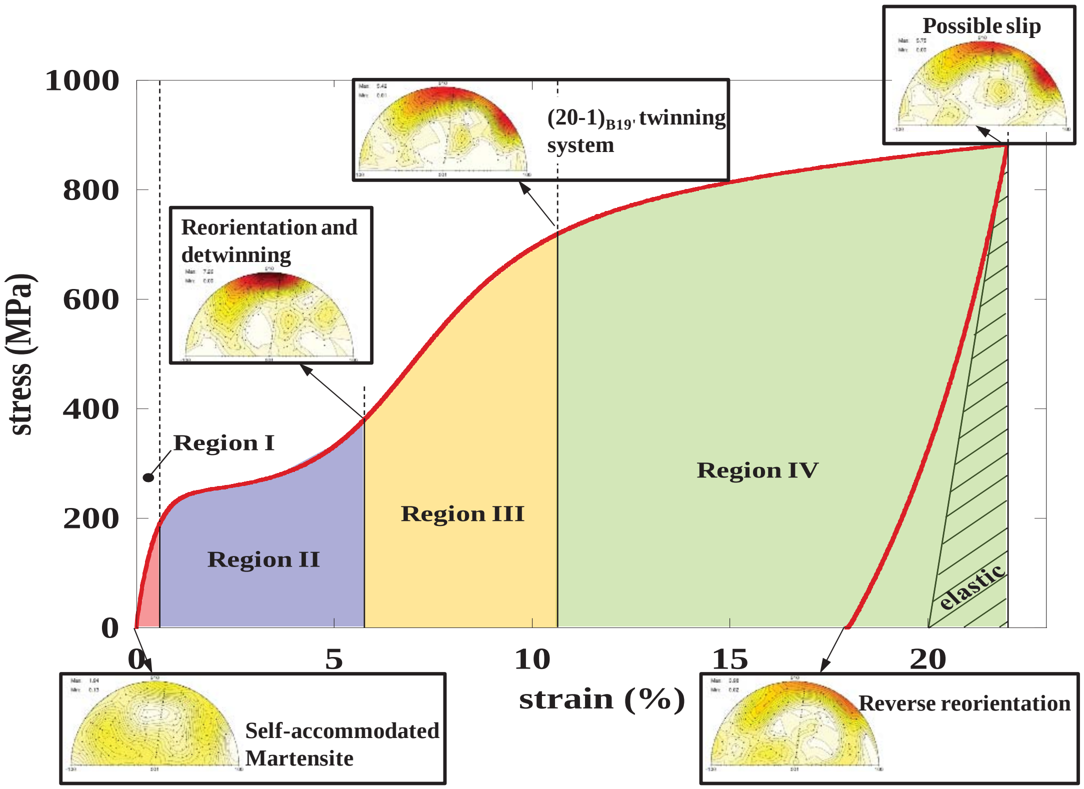
Binary 55NiTi

Isothermal Deformation - Loading Actuators

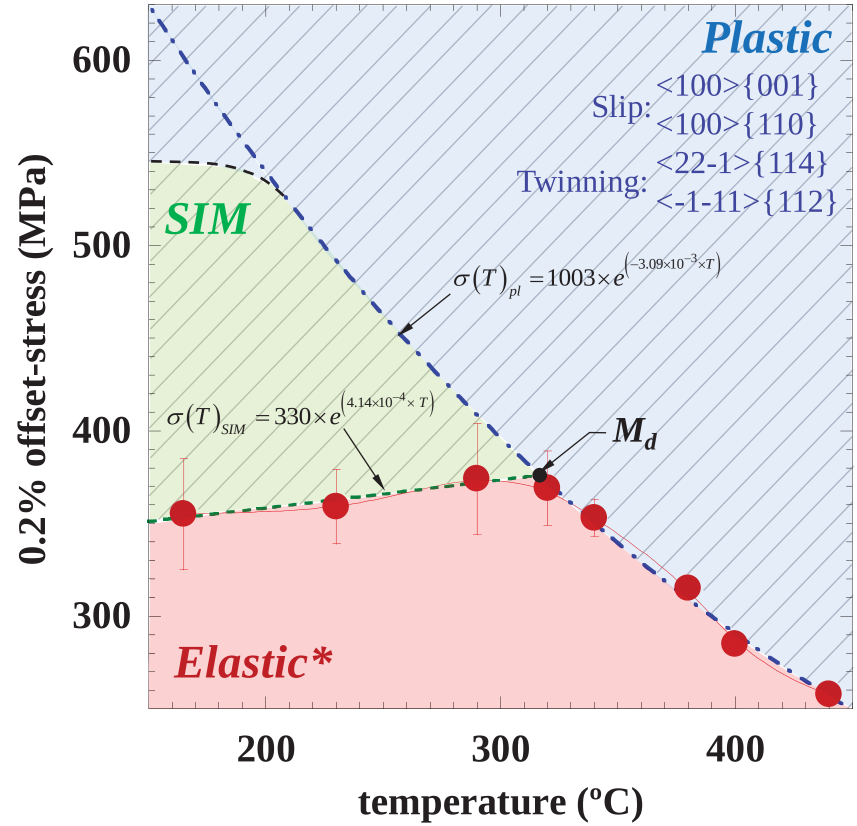


Isothermal Deformation - Loading Actuators

Martensite

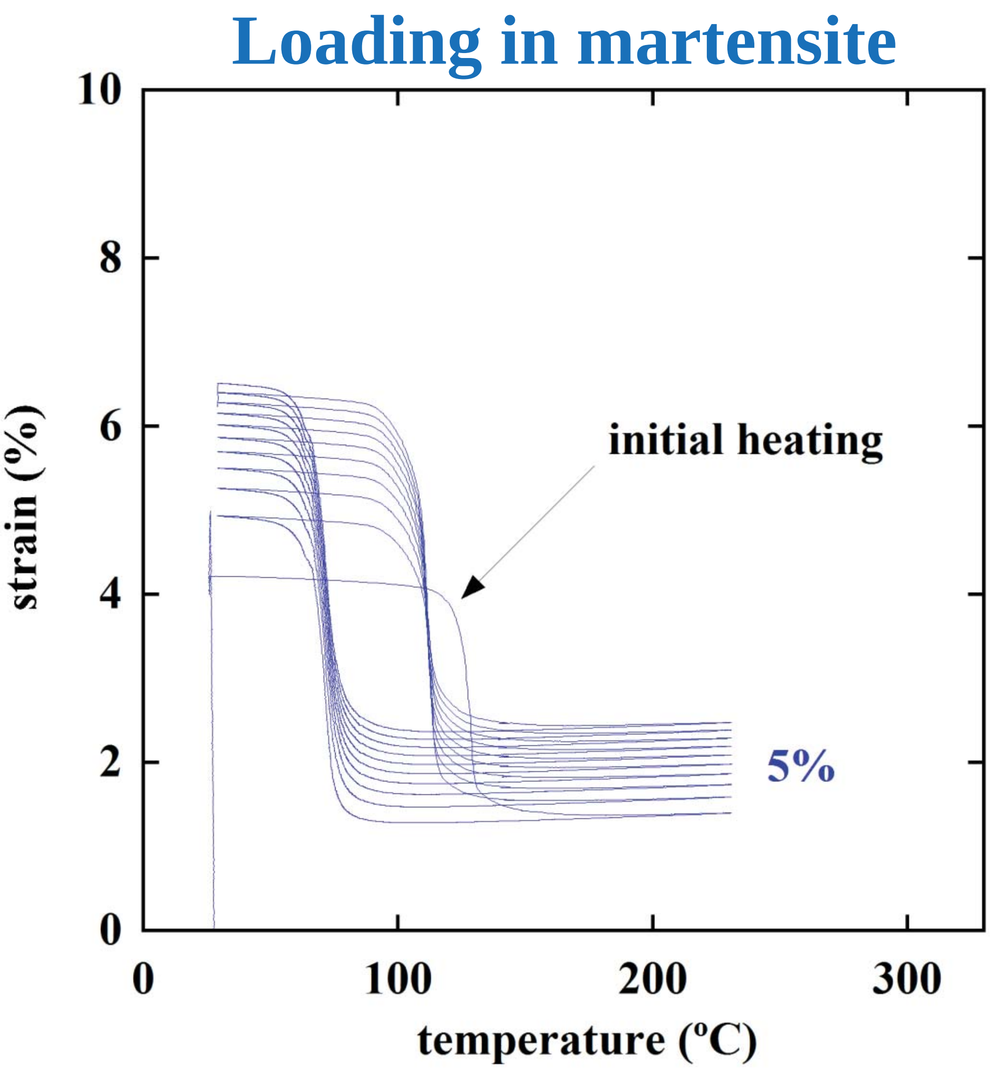


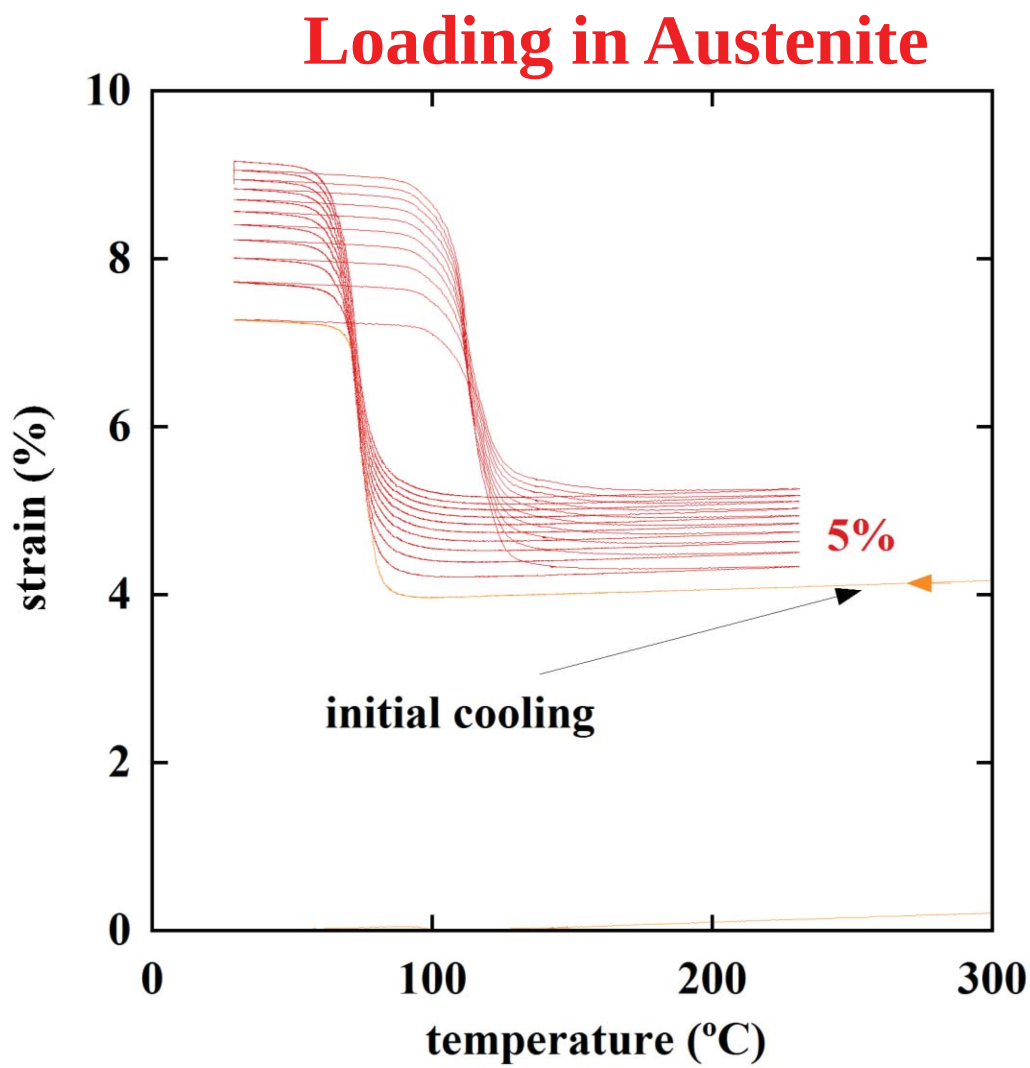
Austenite



- Deformation mechanisms revealed- complexity and multiplicity of mechanisms can't be resolved another way
- e.g., reorientation planes/limits, stress- induced-martensite region, martensite desist...

Isothermal Deformation – Where to Load Actuators? Does it Matter?





- No major differences in transformation strains
- Large strain evolution (ratcheting) difference

O. Benafan et al., *International Journal of Plasticity*, 2014, 56, p. 99–118.

SMA Properties – Can they be Optimized for Actuators?

1. Material and Geometry‡

- Binary 55NiTi → ϕ = 5.08mm (0.2in)
- Stress free transformation temperatures
  - $A_s = 92\ °C$
  - $A_f = 105\ °C$
  - $M_s = 71\ °C$
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- Effective coefficient of thermal expansion
  - $\alpha_A^* = 13.0 \times 10^{-6}\ /\ °C$
  - $\alpha_M^* = 6.4 \times 10^{-6}\ /\ °C$
- Effective elastic moduli
  - $E_A^* = 74\ GPa$
  - $E_M^* = 50\ GPa$
- Effective Poisson's ratios
  - $\nu_A^* = 0.33$
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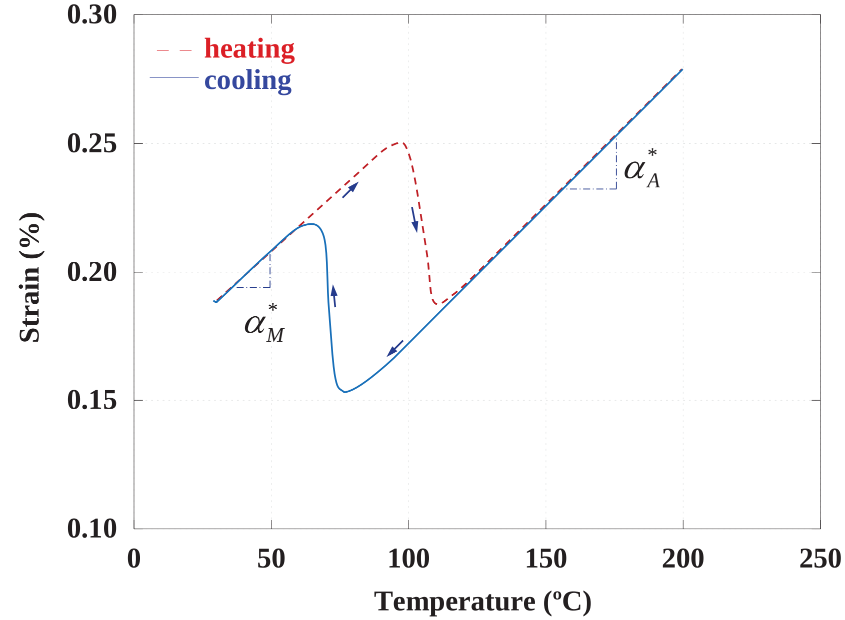
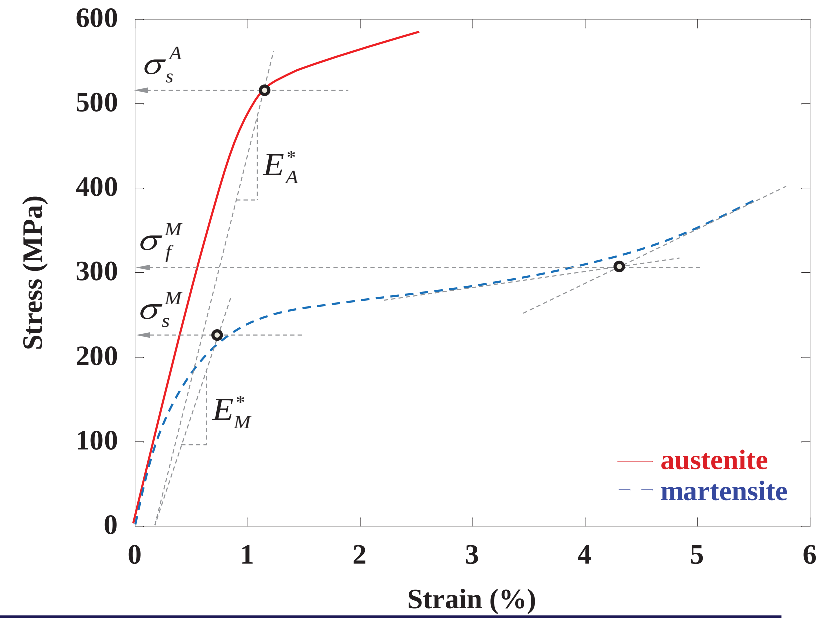
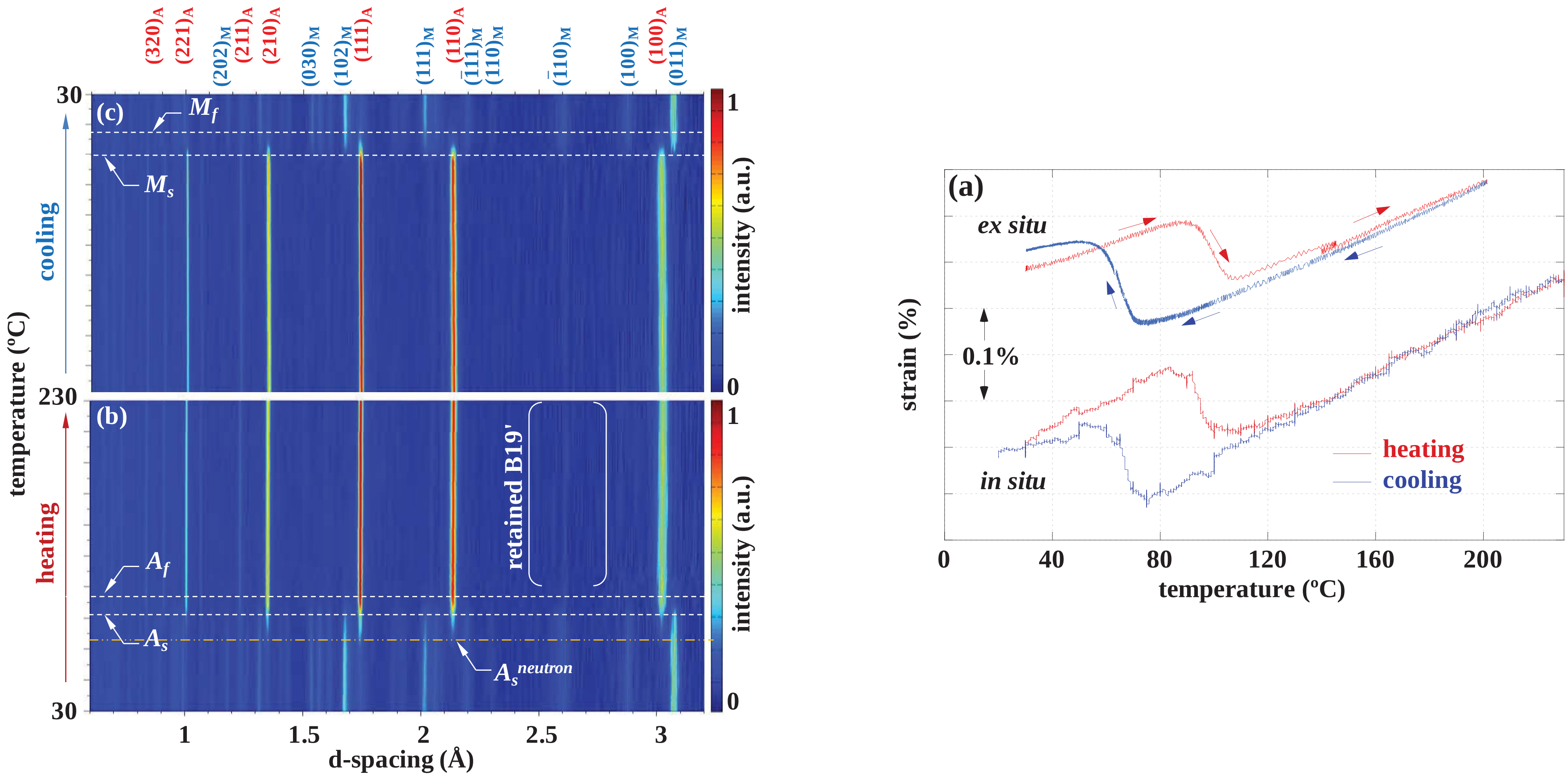


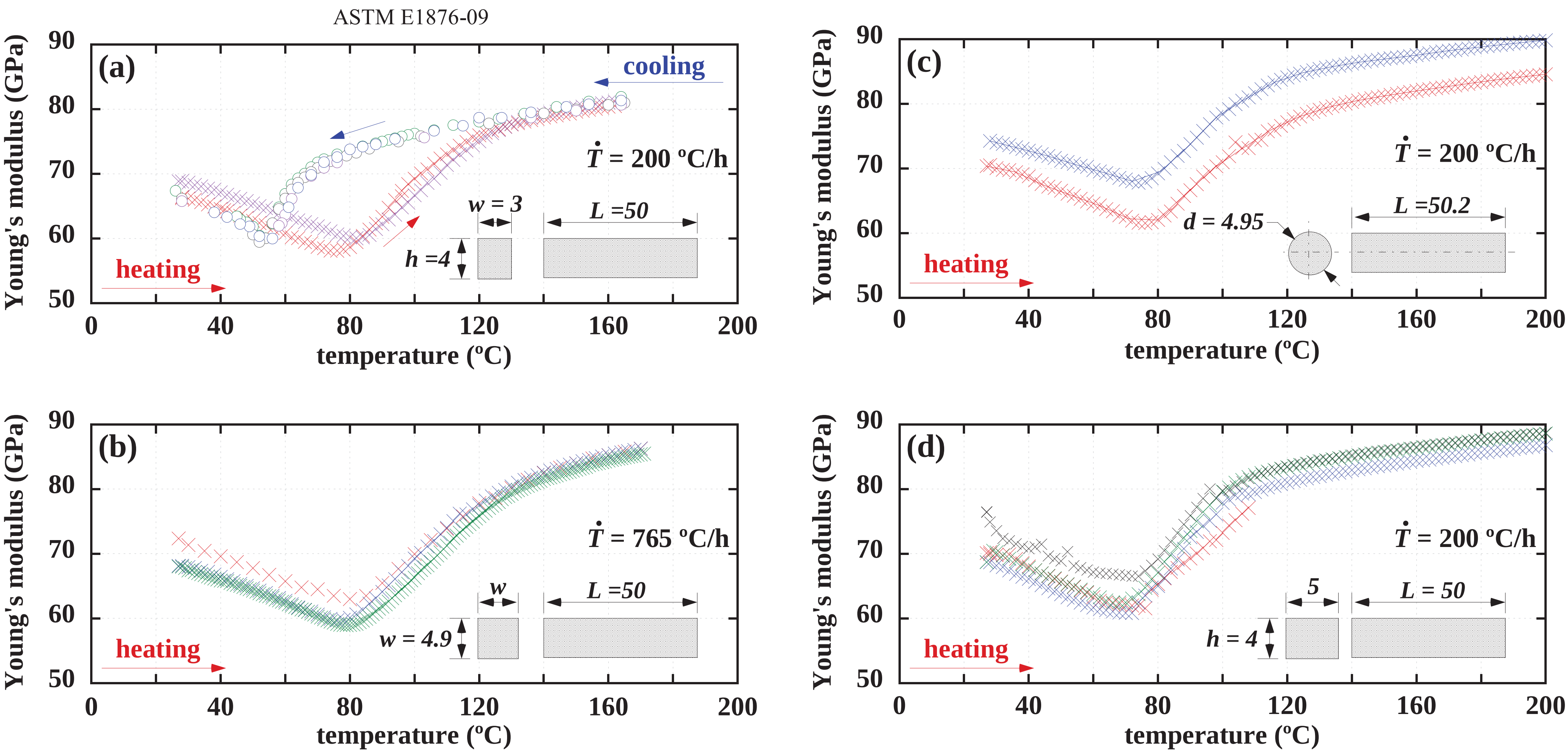


Transformation Temperatures: DSC vs. Strain-Temperature vs. Neutrons



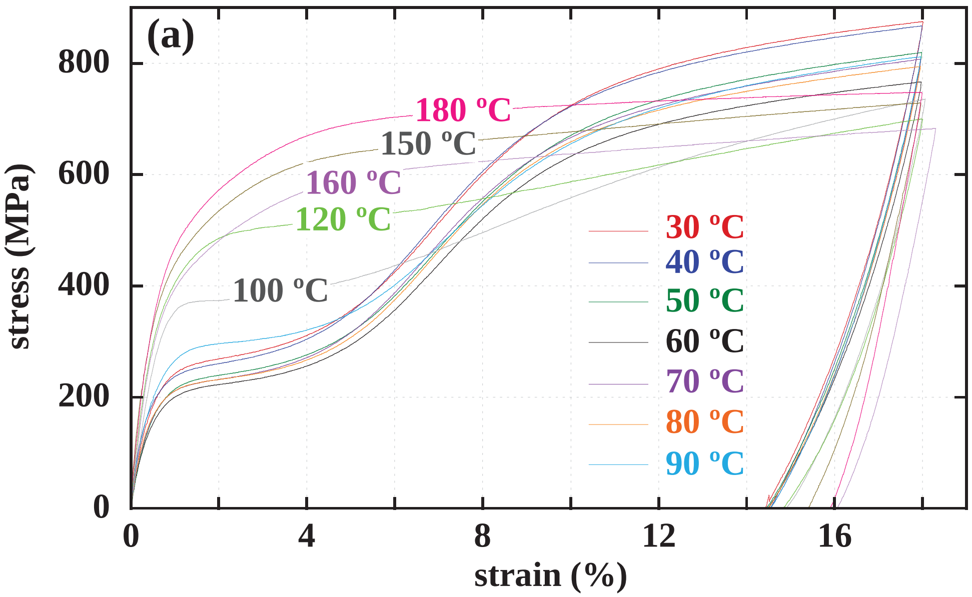
- Transformation temperatures during the reverse transformation measured from strain-temperature and DSC data were found to differ from the actual onset of transformation as revealed from neutron spectra.
- The austenite phase starting to form at ~75 °C,

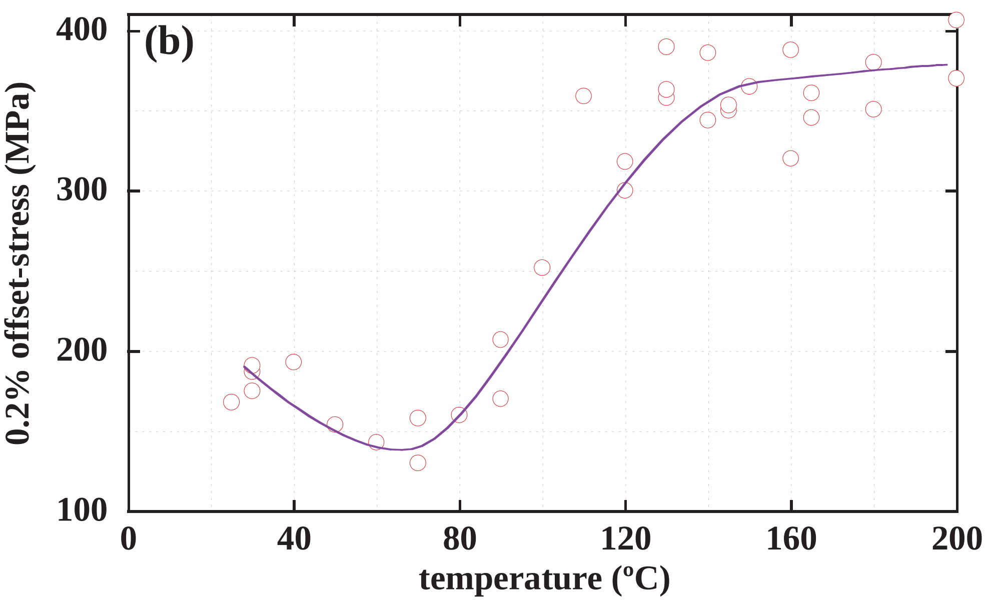
Dynamic Young's Modulus for $Ni_{49.9}Ti_{50.1}$



- Dynamic Young's modulus data obtained from the impulse excitation of vibration tests.
- The average dynamic modulus of martensite at room temperature was about 70 GPa, but decreased with increasing temperature with an average minimum value of 60 GPa at ~80 °C.

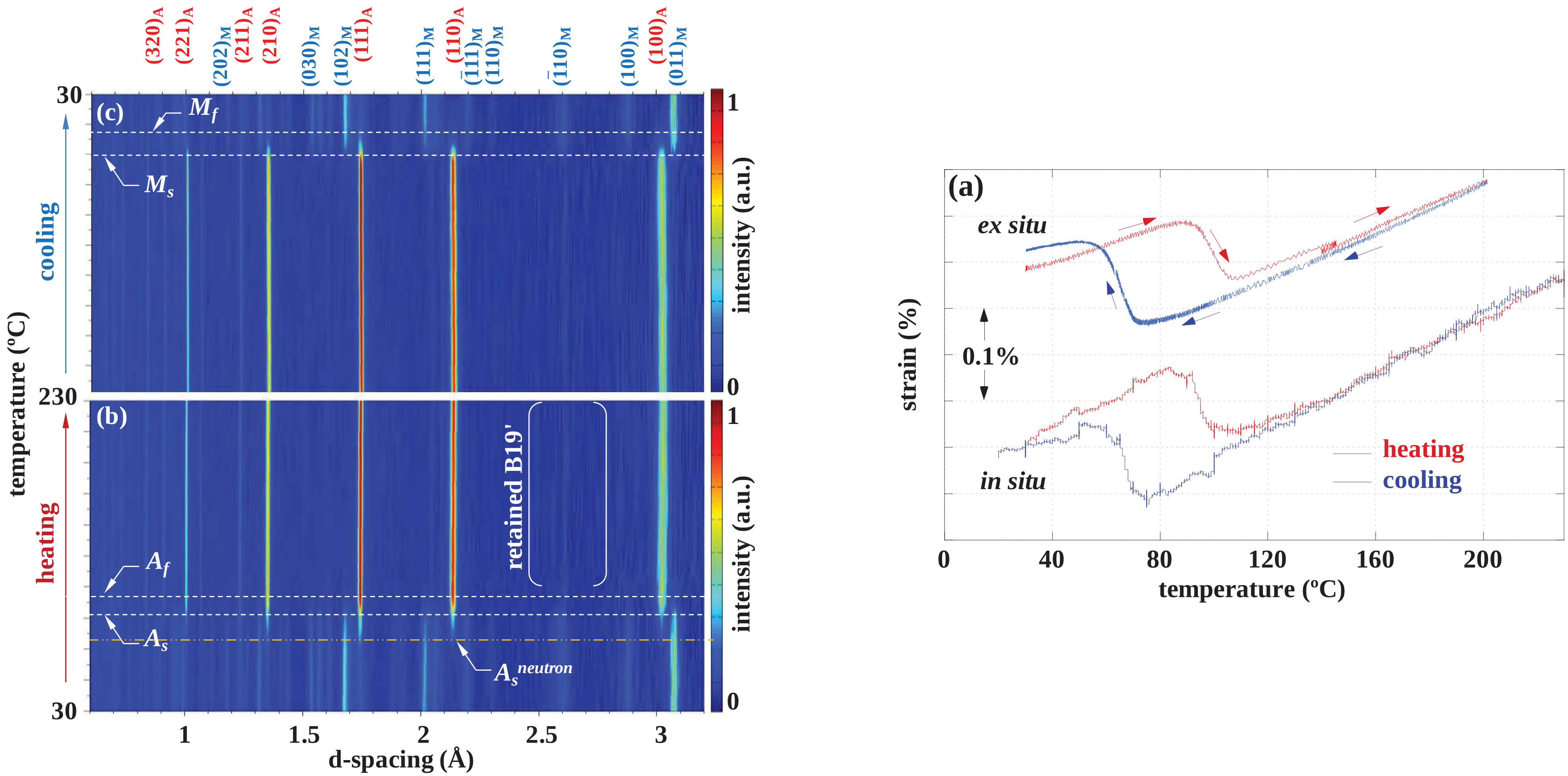
0.2% Offset "Yield" Stress Behavior of $Ni_{49.9}Ti_{50.1}$





- The onset of inelastic deformation (generally referred to as 'yield') in the martensite phase is dominated by reorientation and detwinning mechanisms.
- Decrease with increasing temperature, reaching an averaged minimum value of 140 MPa between 65 and 80 ºC.
- The onset stress then sharply increased in the two-phase region and reached near saturation (with a still slightly positive slope) at 350 MPa near 130 ºC.
- Inelastic deformation over this temperature range (~90 – 130 ºC), which includes the B19'→ B2 phase transition, is attributed to the nearly concurrent operation of stress-induced martensite and plastic deformation.

Transformation Temperatures: DSC vs. Strain-Temperature vs. Neutrons



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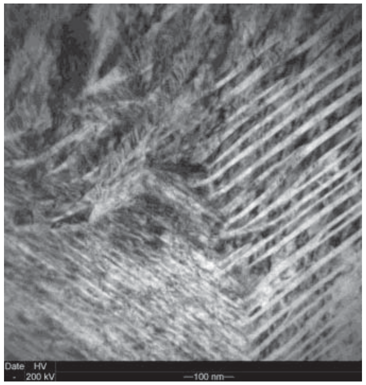
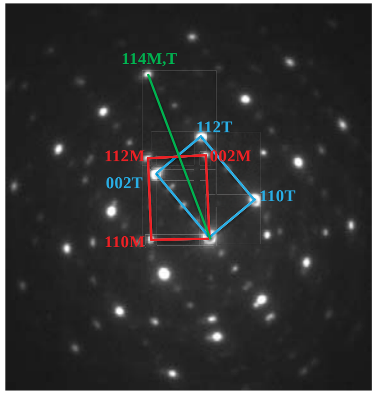
Thermomechanical Cycling of Actuators

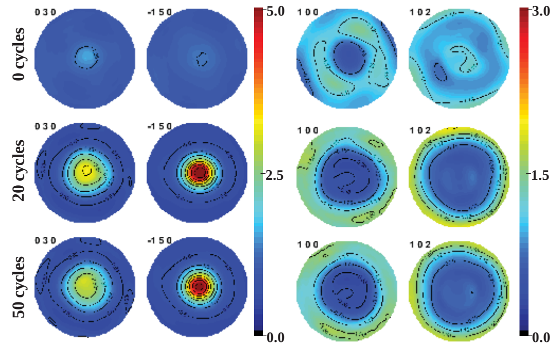
55NiTi

Electron diffraction

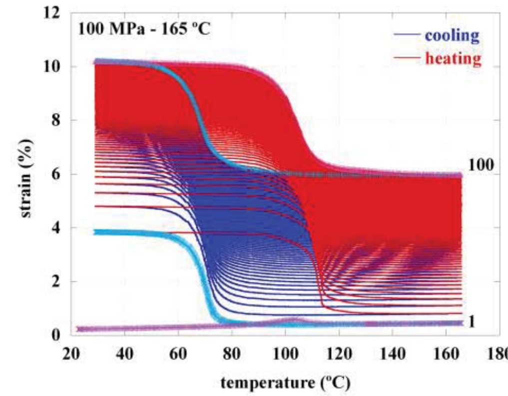




In situ diffraction



Outcome



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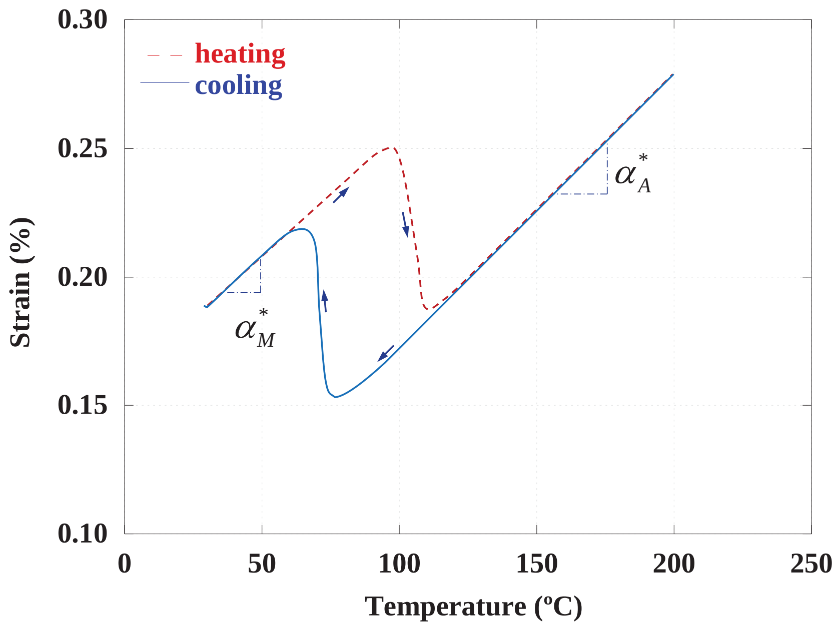
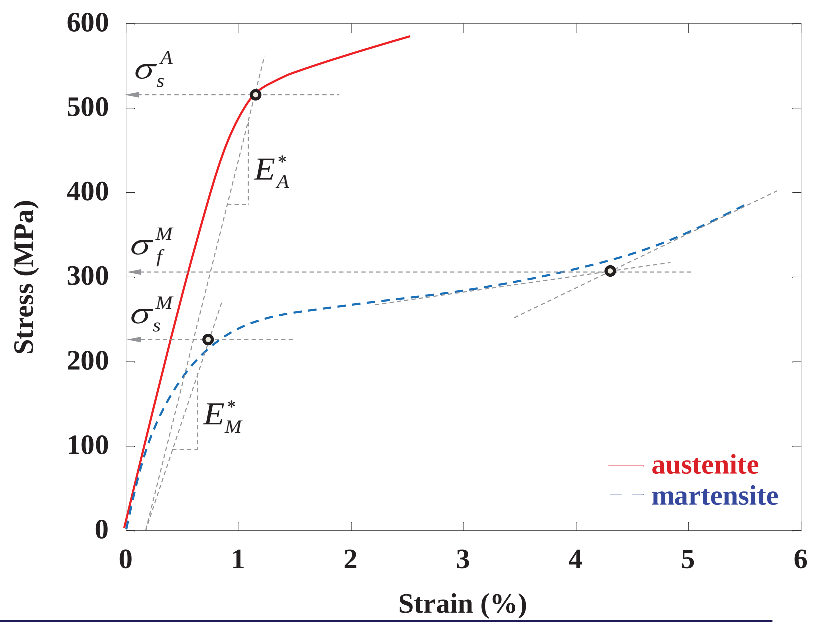
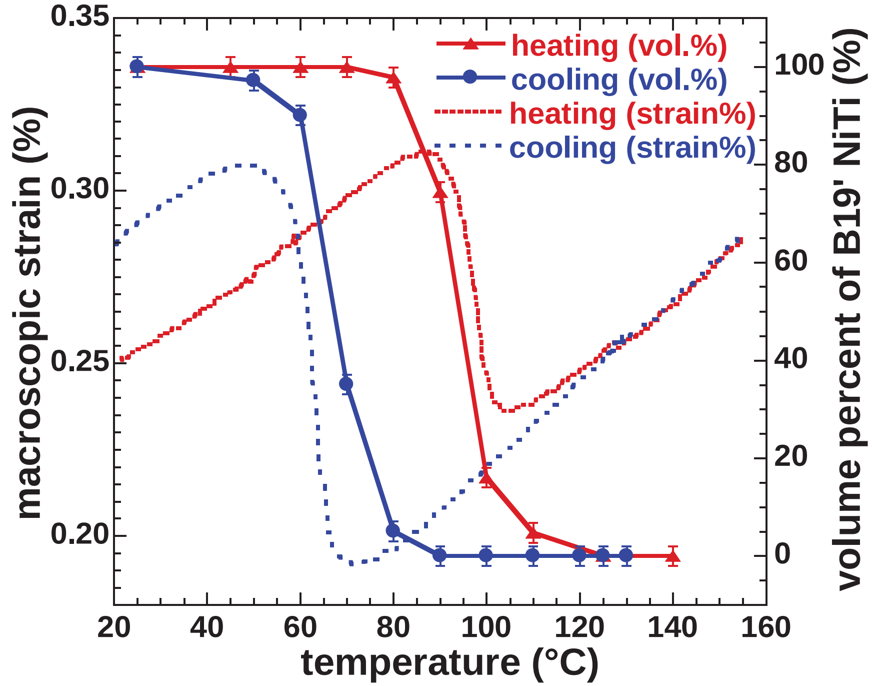
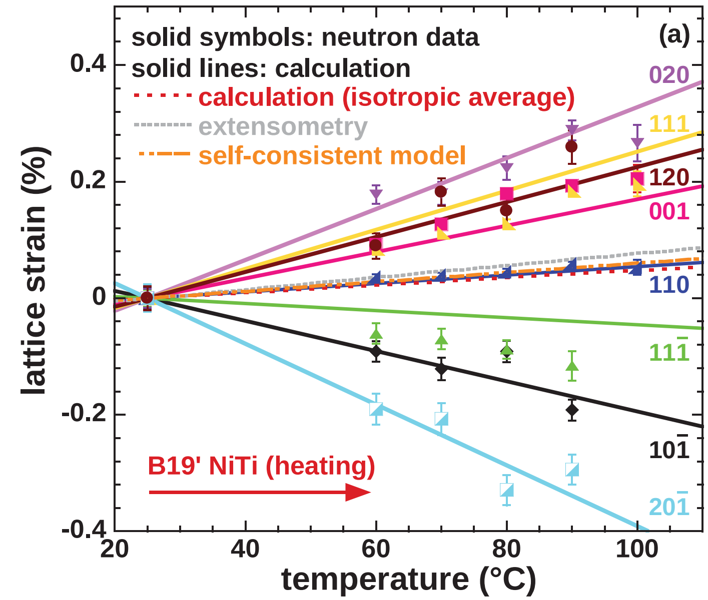




Coefficient of Thermal Expansion: Large Anisotropy

- Atomic scale measurements of thermal strains





			Heating (10^{-6}/°C)	Cooling (10^{-6}/°C)
B19' NiTi	Thermal expansion tensor components	α_{11}	-47.2	-30.8
		α_{22}	43.8	32.1
		α_{33}	22.7	27.3
		α_{31}	29.0	32.4
	CTE*		6.4	9.5
	CTE†		8.1	10.9
	CTE (extensometry)		10.3	9.0
B2 NiTi	CTE*		13.0	13.1
	CTE (extensometry)		12.4	12.3

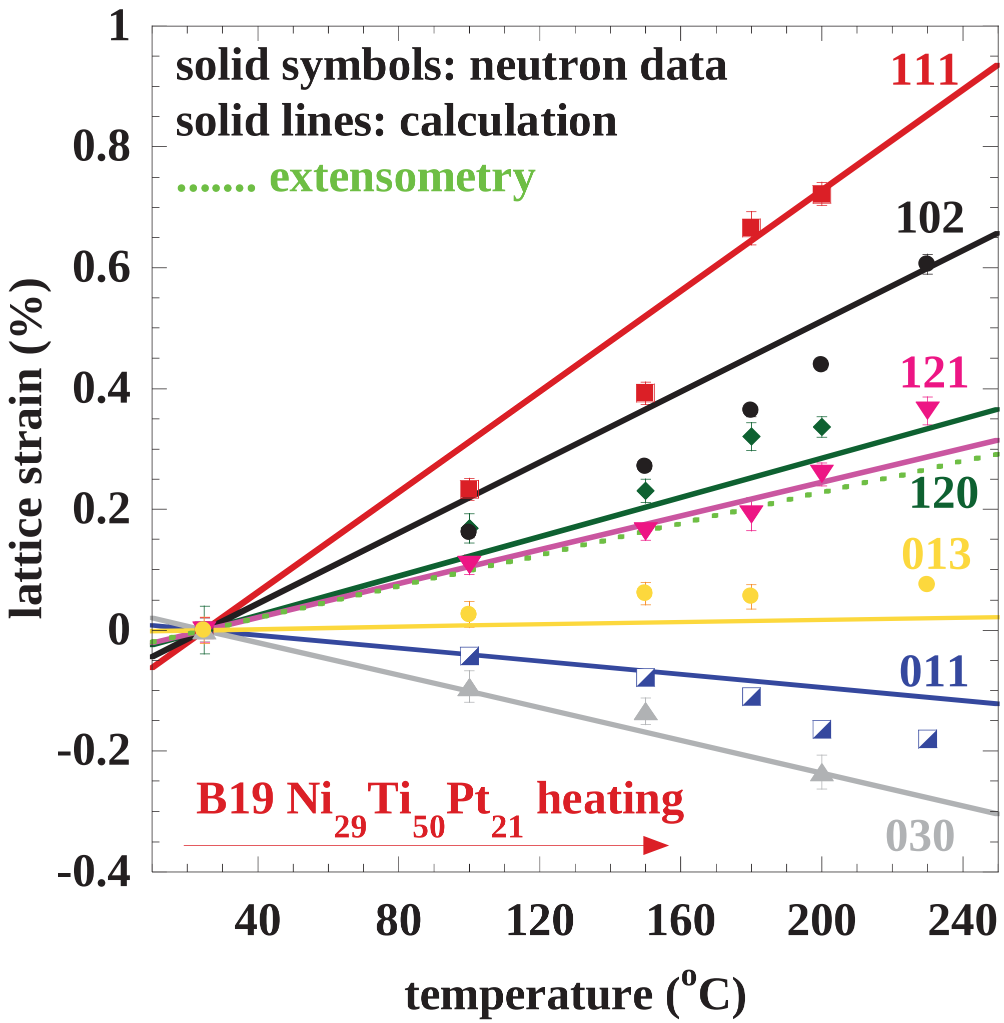
*isotropic average †self-consistent model

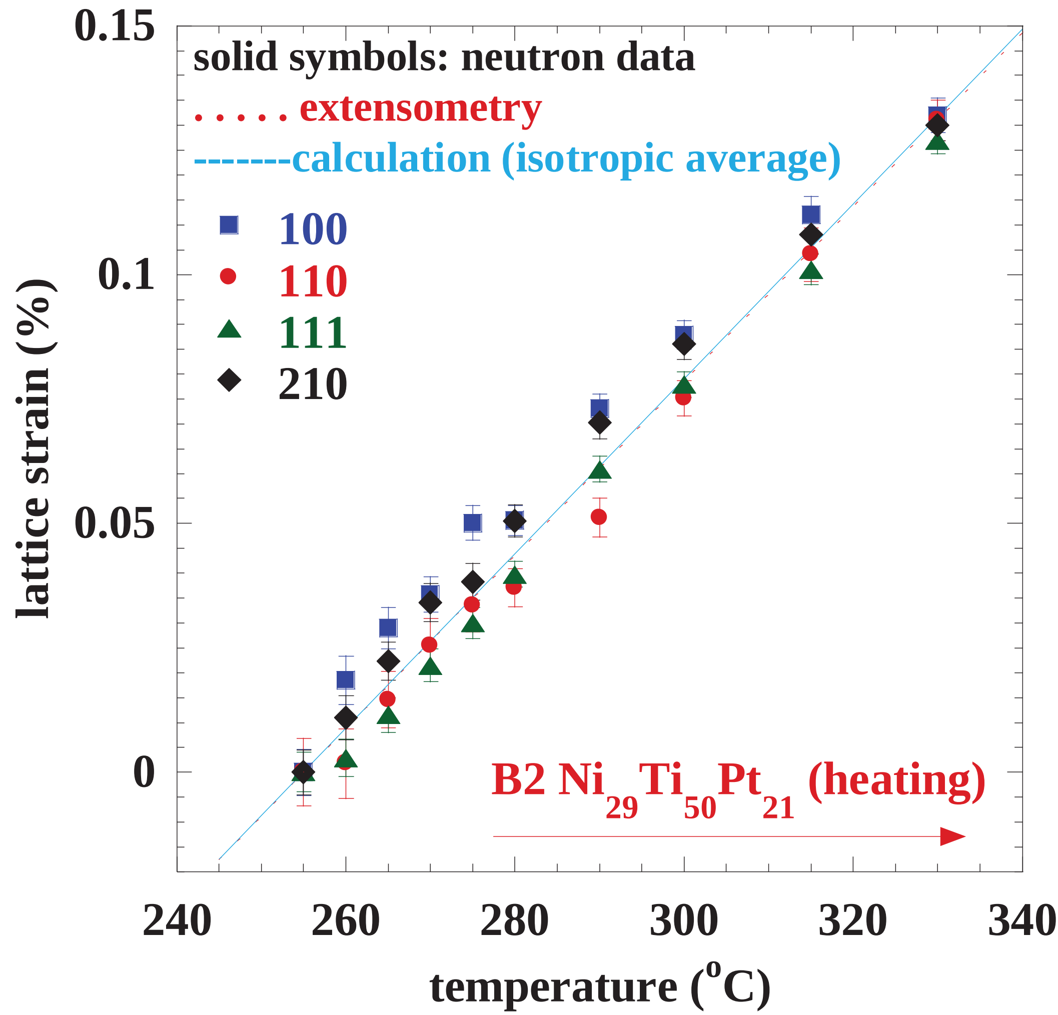
- **Outcome**
  - First report on NiTi CTE tensor (monoclinic martensite) including negative expansion in certain crystal orientations
  - Parametric input for most SMA models

[1] S. Qiu et al., Appl. Phys. Lett. 95, 141906 (2009)

Coefficient of Thermal Expansion: Large Anisotropy

- Similar observation in HTSMAs (e.g., NiTiPt – B19)





O. Benafan et al., unpublished work

www.nasa.gov

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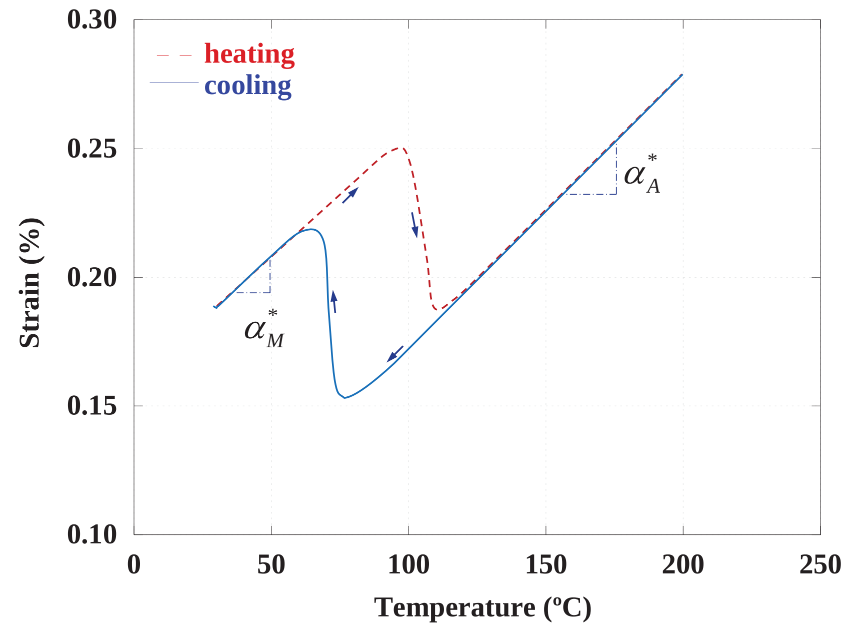
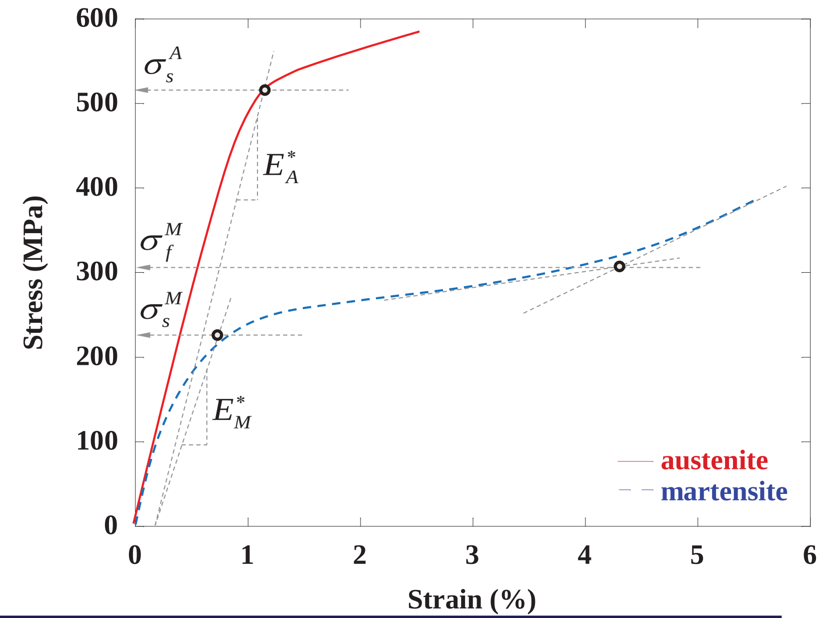
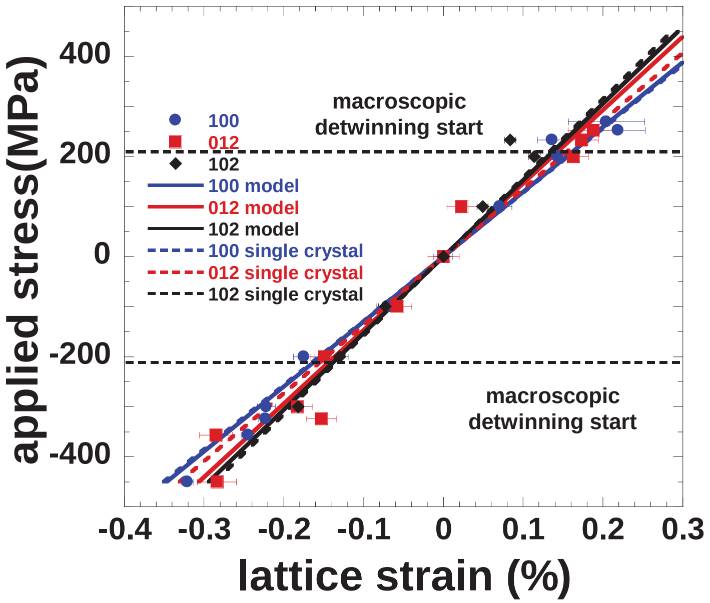
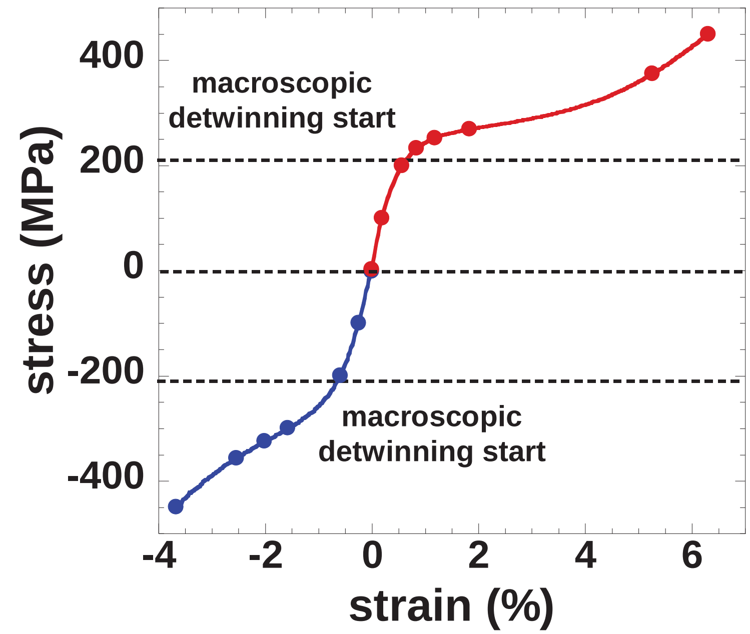




Elastic Moduli: Hard and Soft Orientations

- Strain anisotropy and texture measurements





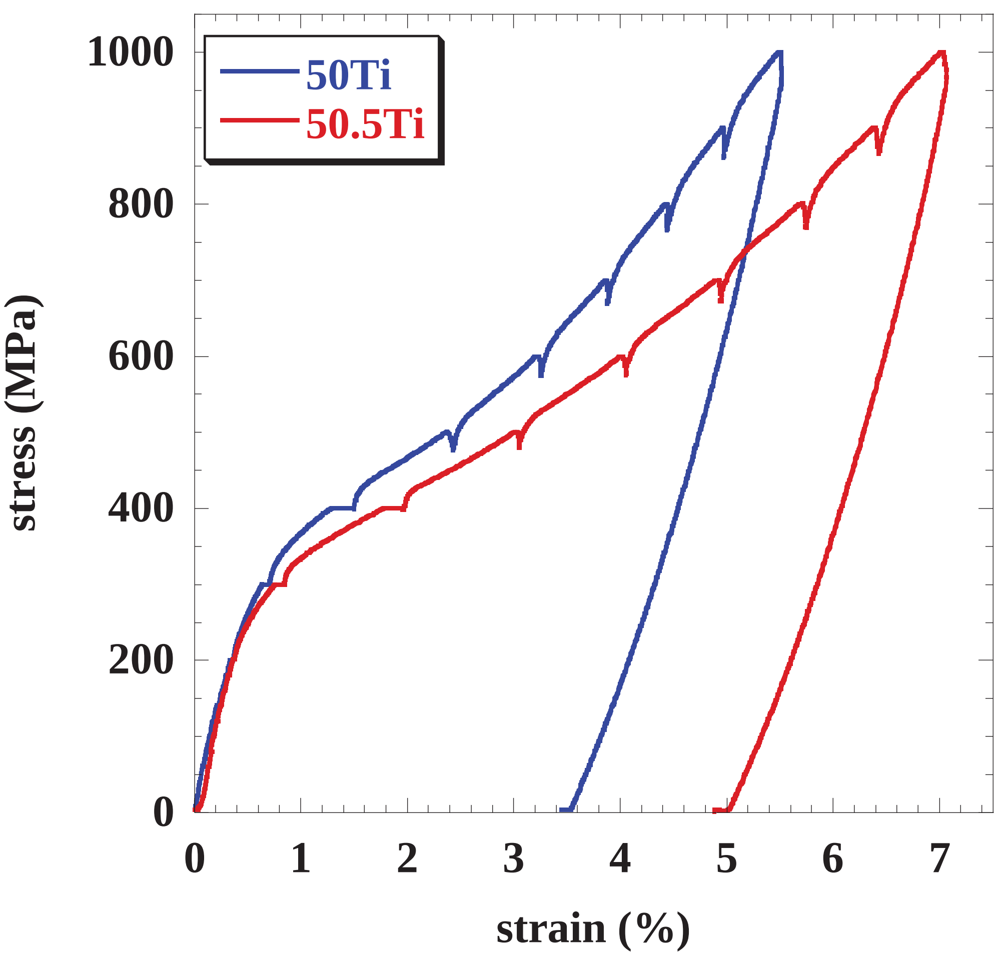
- **Outcome**
  - First validation of *ab initio* calculation
  - Entire compliance matrix, not just a Young's modulus
  - Revealed mechanisms responsible for deflated modulus values obtained from conventional macroscopic tests

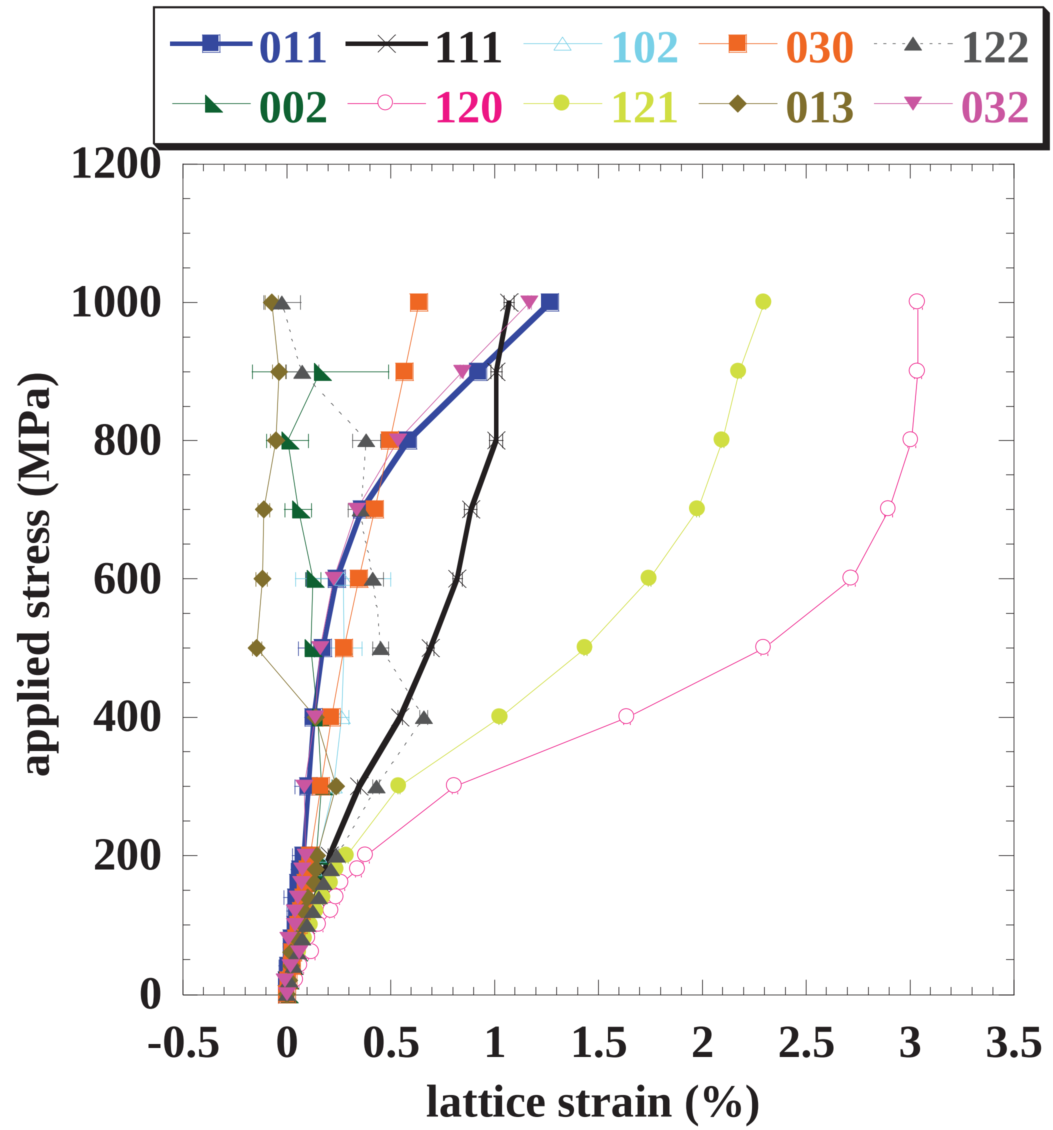
hkl	Single crystal $E_{hkl}^{crystal}$	Model E_{hkl}^{model}	Neutron diffraction $E_{hkl}^{neutron}$		
			$E_{hkl}^{neutron}$	# of points	R
100	128.2	129.8	132.2	6	0.997
012	136.0	146.7	145.4	6	0.978
102	157.3	152.8	167.1	6	0.999
-120	33.8	106.0	101.4	6	0.997
121	84.2	116.3	104.6	6	0.996
-112	177.6	147.6	165.1	6	0.999
-122	120.2	143.7	110.5	5	0.991
-111	85.9	130.2	104.7	5	0.999
011	175.9	155.7	117.1	6	0.995
-121	53.4	122.0	93.3	5	1.000
-110	41.0	105.1	78.2	6	0.997

[1] S. Qiu et al., Acta Mat., 2010

Elastic Moduli: Hard and Soft Orientations

NiTiPt

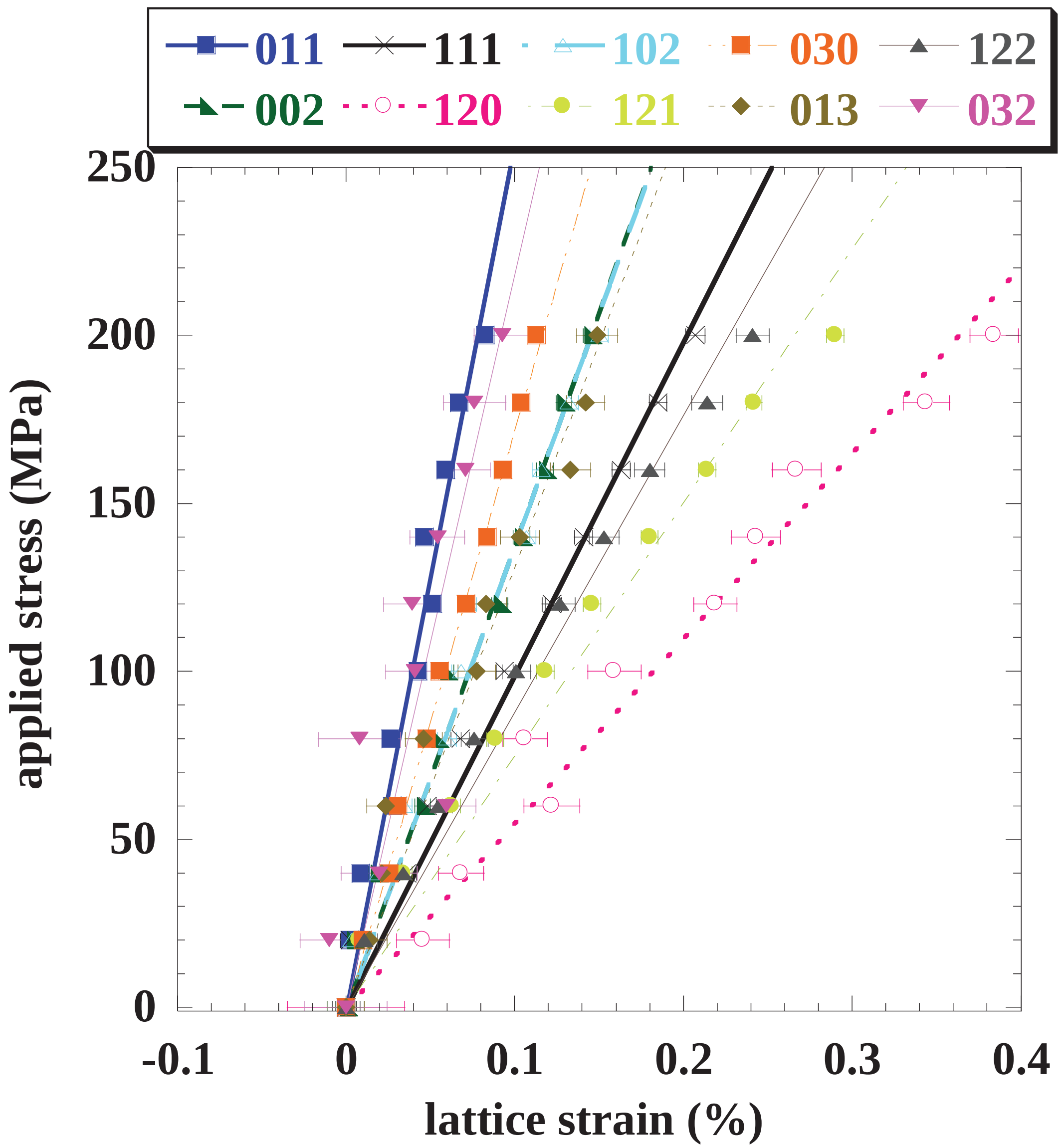




O. Benafan et al., unpublished work

Elastic Moduli: Hard and Soft Orientations

NiTiPt



E_{011}=257.8 GPa R=0.985

E_{002}=138.7 GPa R=0.994

E_{111}=99.2 GPa R=0.997

E_{120}=55.1 GPa R= 0.988

E_{102}=138.3 GPa R=0.993

E_{121}=75.3 GPa R=0.995

E_{030}=173.0 GPa R=0.998

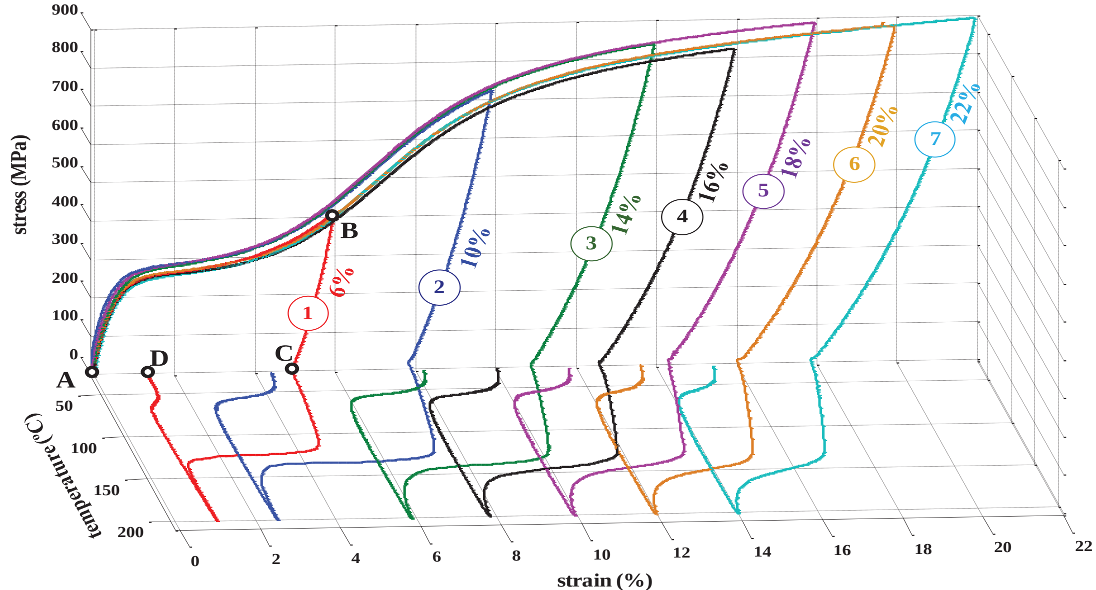
E_{013}=132.3 GPa R=0.988

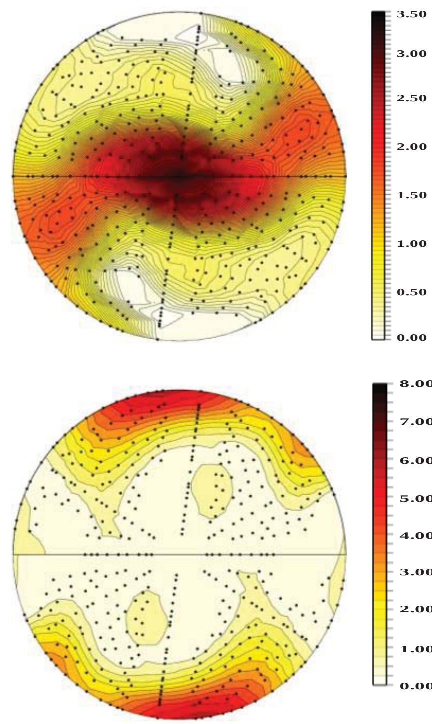
E_{122}=88.3 GPa R=0.996

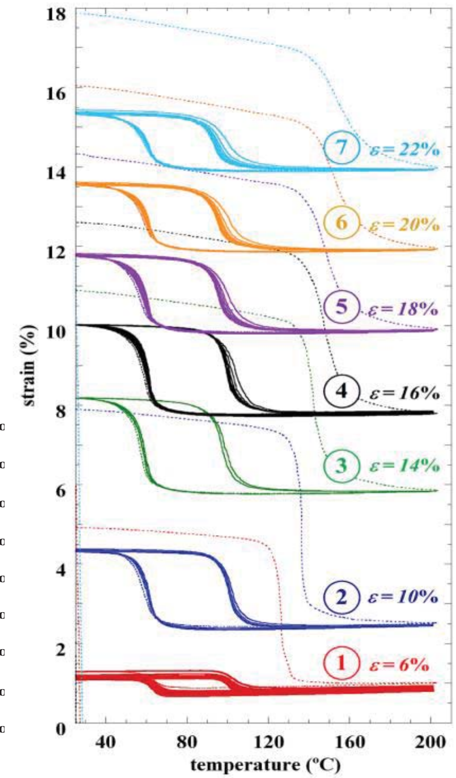
E_{032}=218.6 GPa R=0.886

Optimization of Two-Way Shape Memory Effect

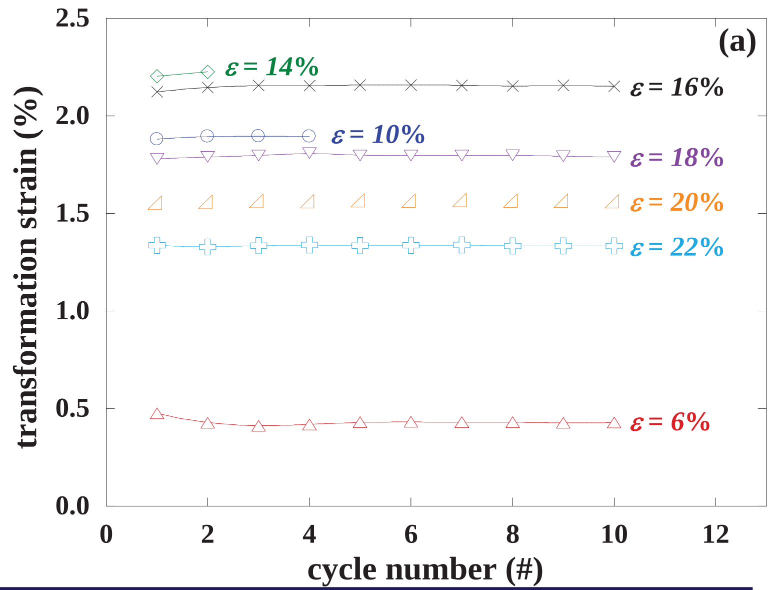
- Uniaxial deformation at room temperature followed by free recovery





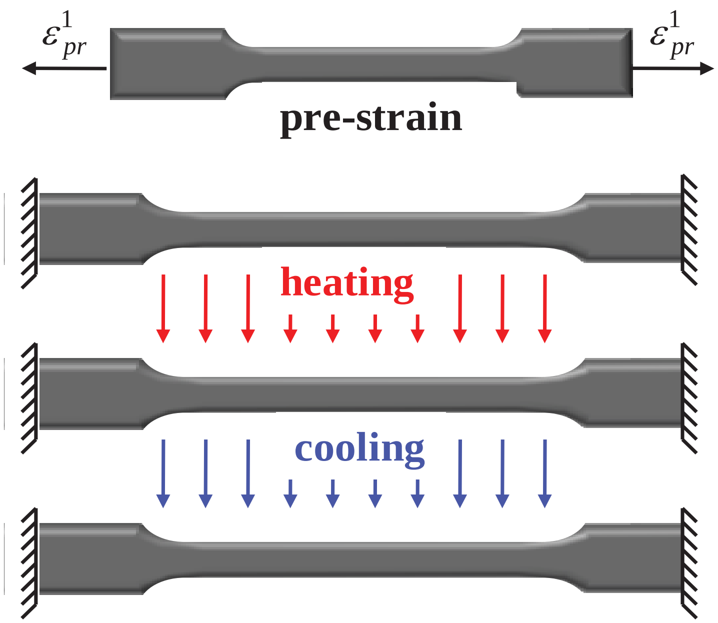


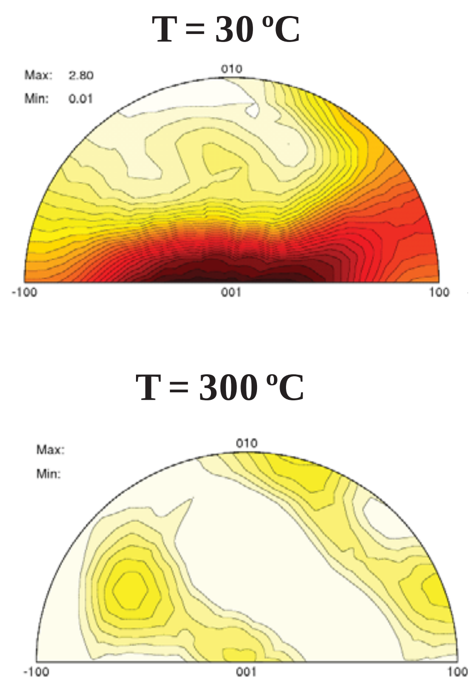
- **Outcome**
  - Established a quick and efficient method for creating a strong and stable TWSME
  - Texture maps were used to determine deformation modes – correlated with TWSME stability and magnitude (not possible another way)

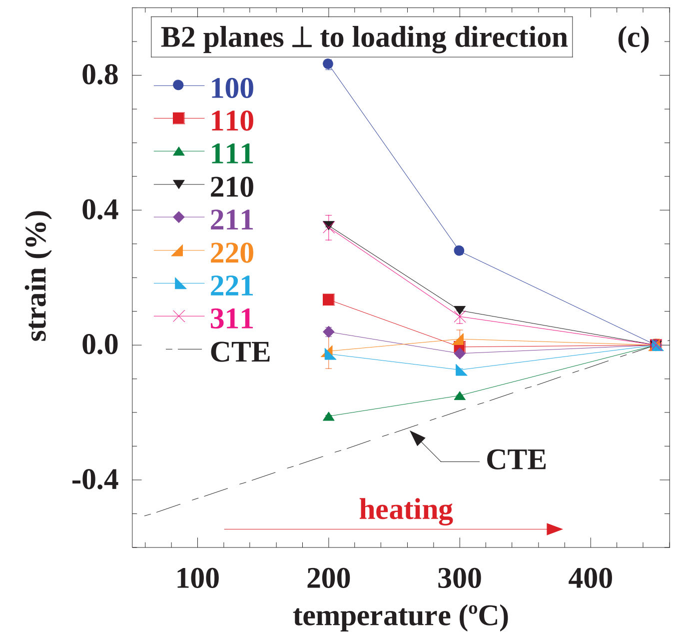


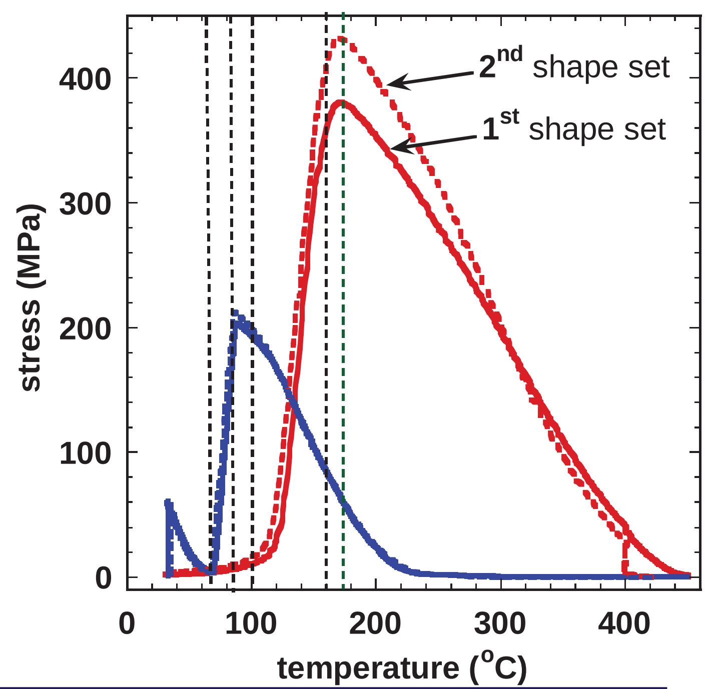
Shape Setting of SMA Actuators

- In situ neutron diffraction during shape setting of bulk polycrystalline NiTi





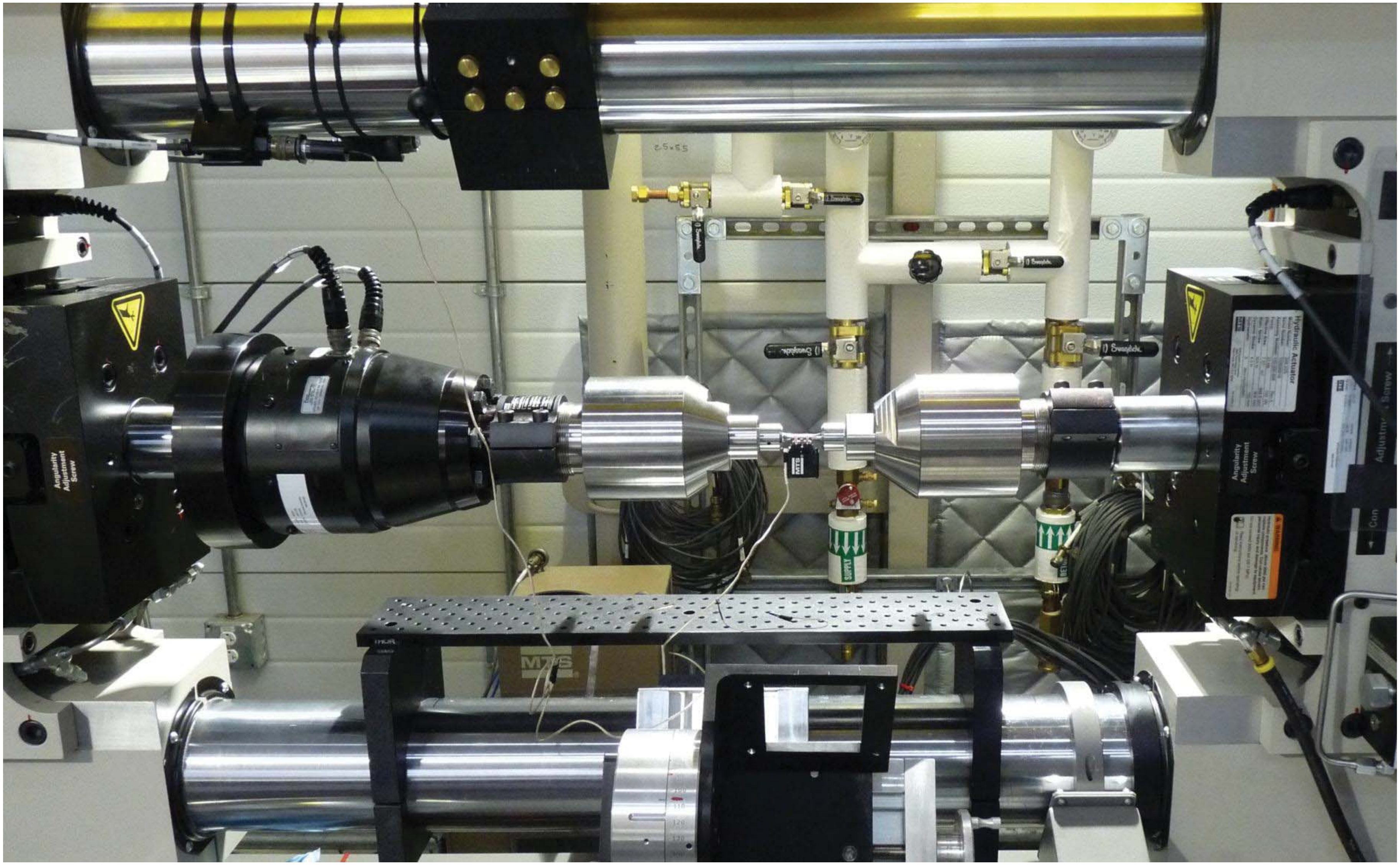




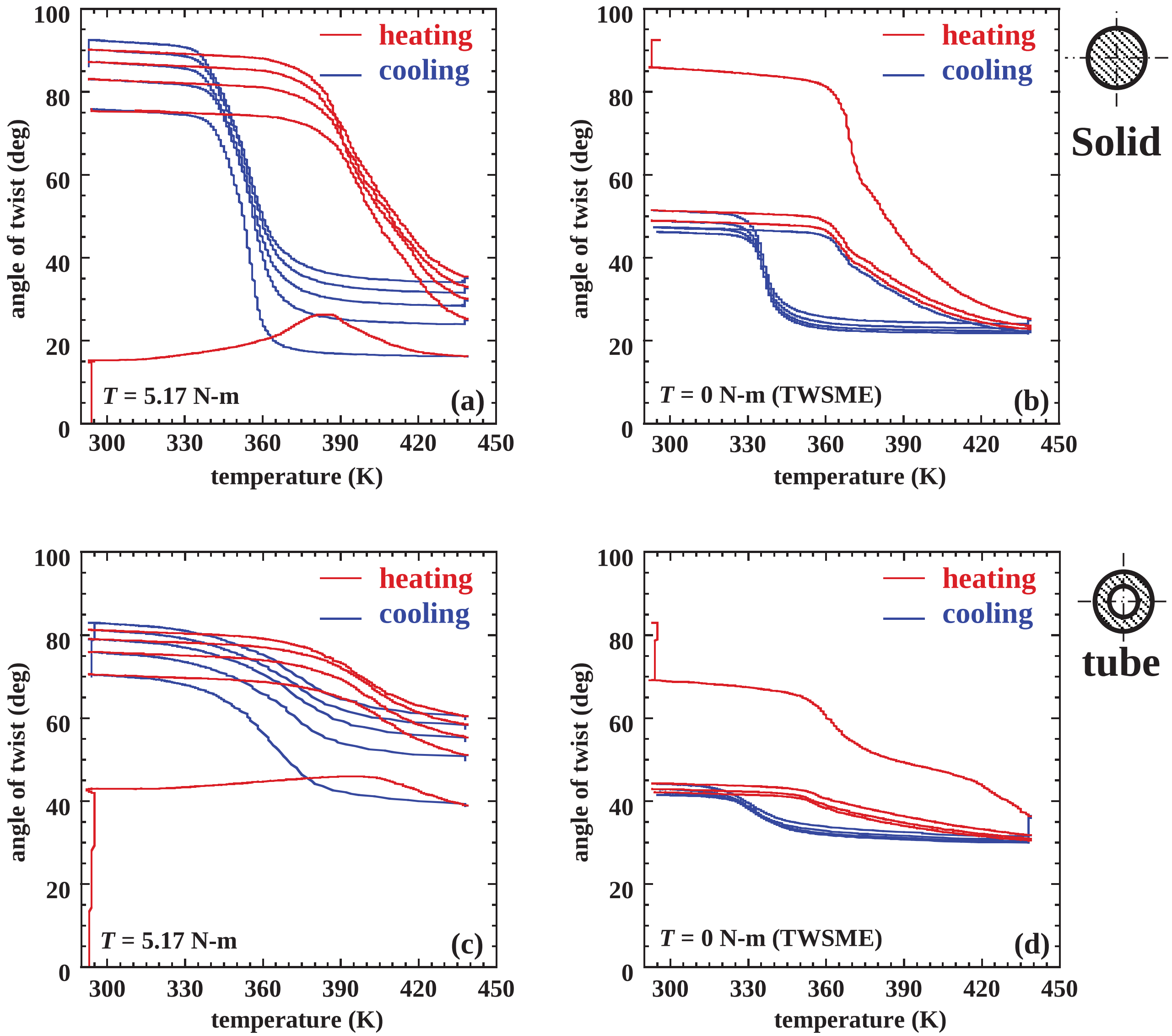
- **Outcome**
  - Guidelines for shape setting any actuator: stress and temperature limits for shape setting
  - Neutrons revealed mechanisms responsible for the stress generation and relaxation during shape setting.

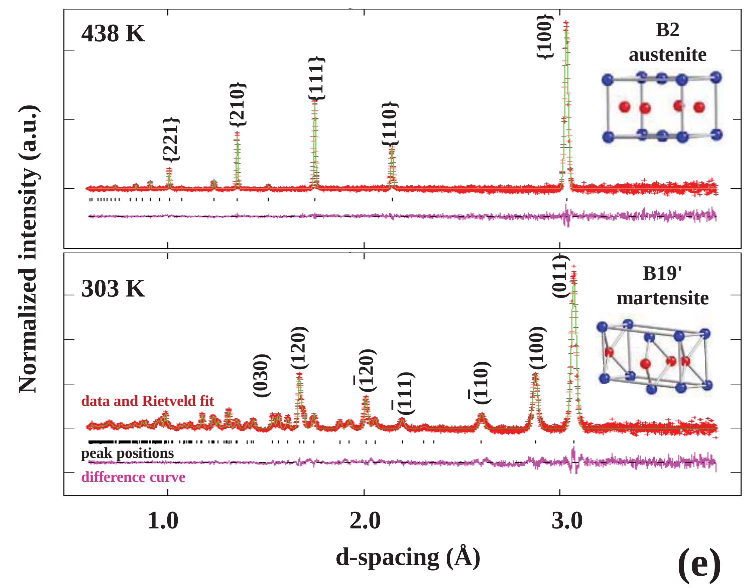
[1] O. Benafan et al. (2012)

Torsional Characteristics of 55NiTi



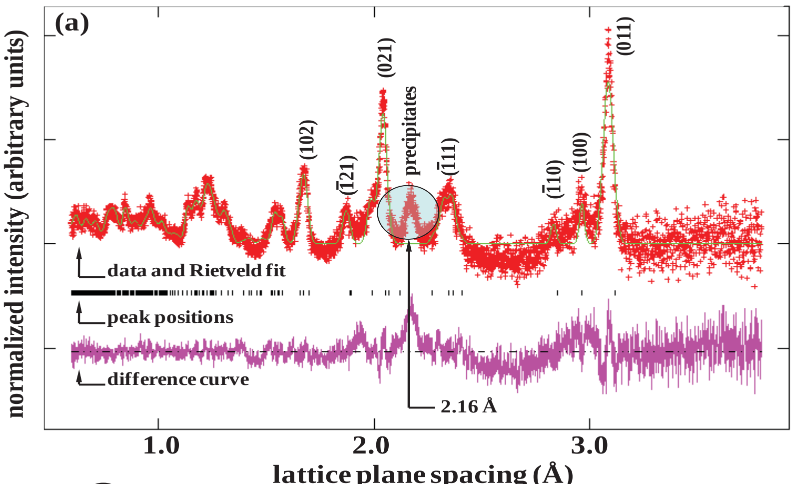
Torsional Characteristics of 55NiTi

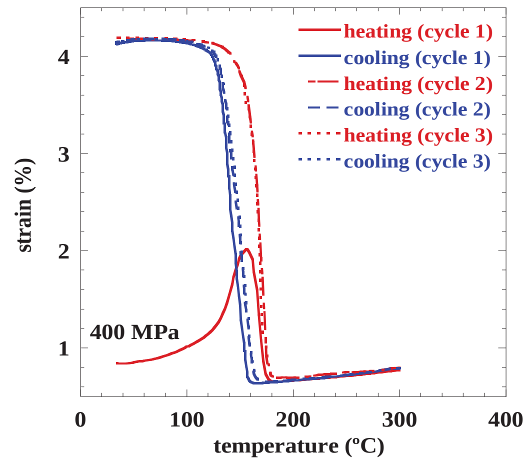


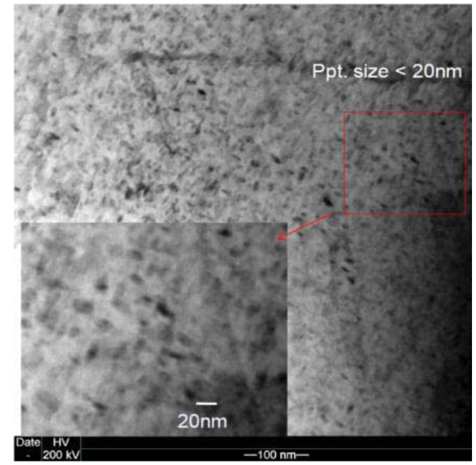


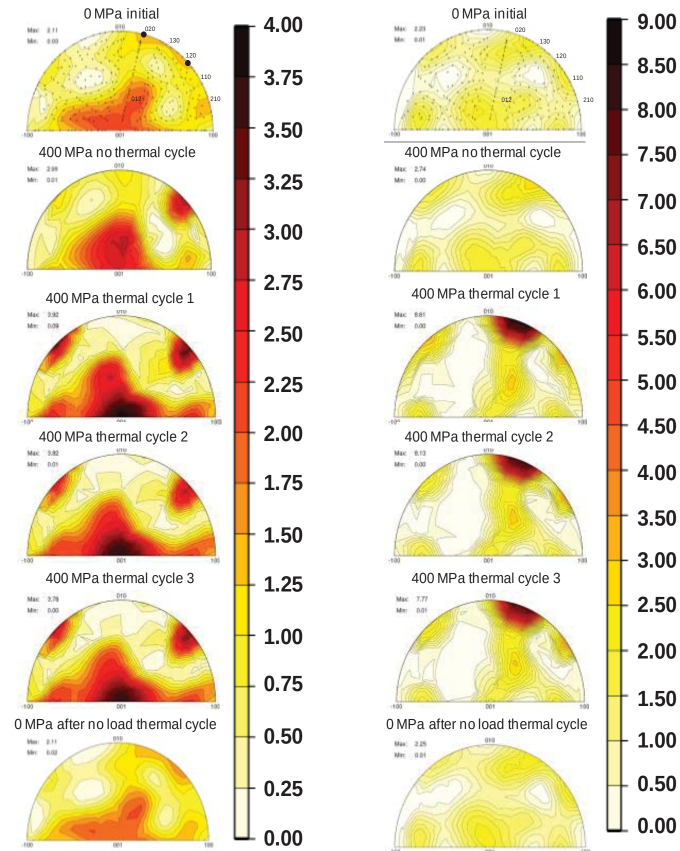
Extension of Neutrons to Novel High Temperature SMAs

- Microstructural evolution during isothermal and isobaric deformation of NiTiHf







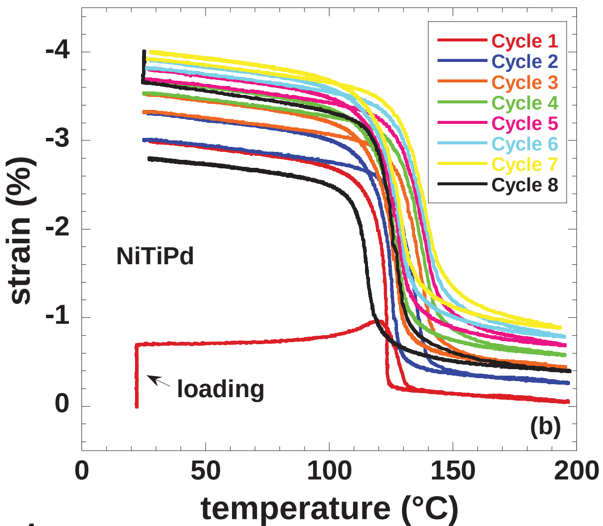


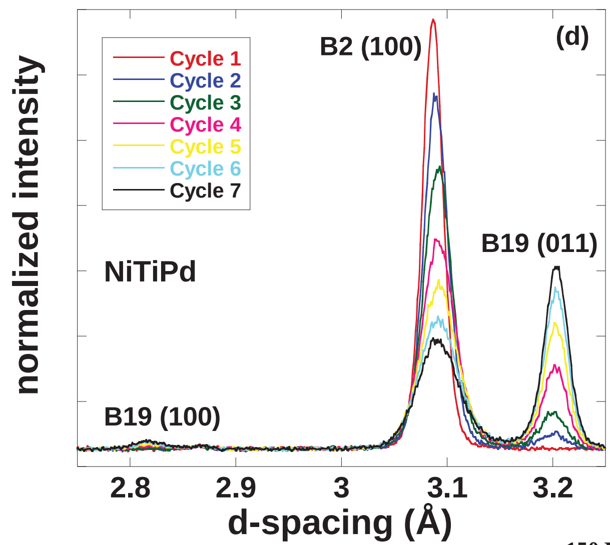
- **Outcome**
  - High work output and dimensional stability
  - Texture measurements were correlated to the lack of evolution in this alloy
  - Confirmed relationship of microstructure and load-biased tests: From Neutron spectra
  - Neutrons showed why training of Hf alloy is not necessary

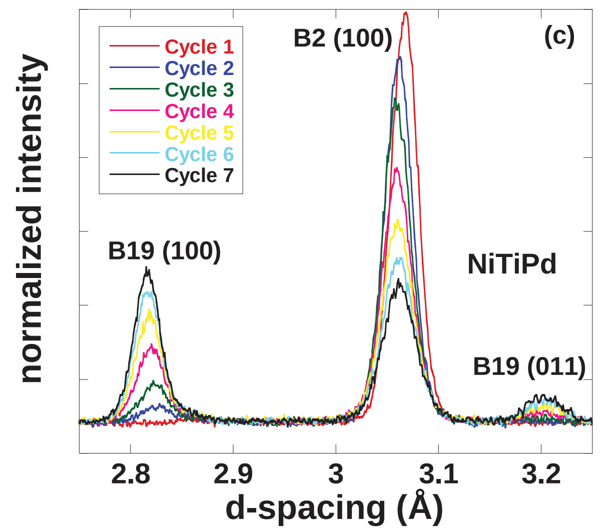
[1] O. Benafan et al. Metall. Trans. A, 43, 4539 (2012)

Extension of Neutrons to Novel High Temperature SMAs

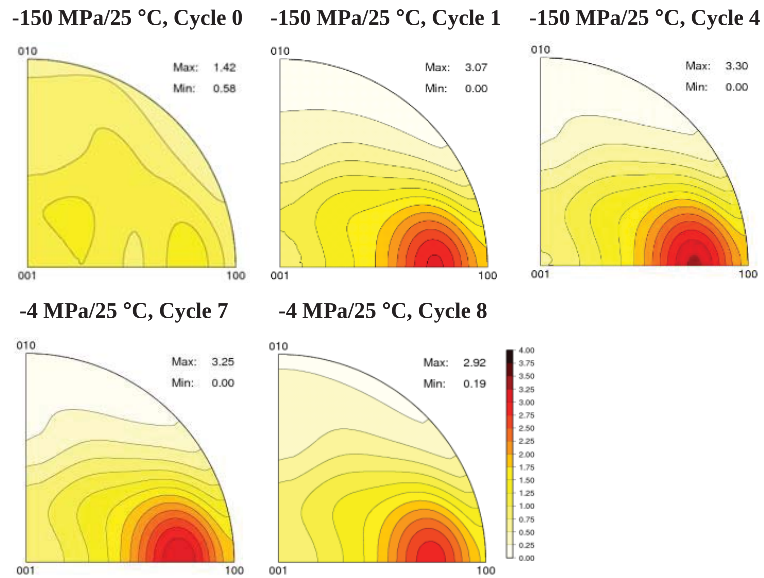
- The role of retained martensite during thermal-mechanical cycling in NiTiPd high temperature shape memory alloy was revealed



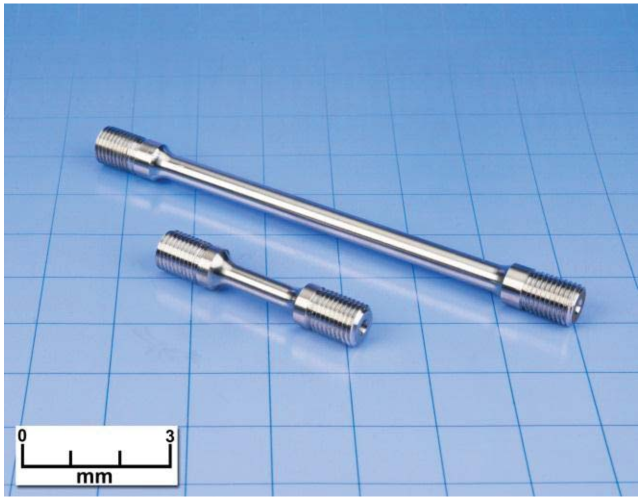


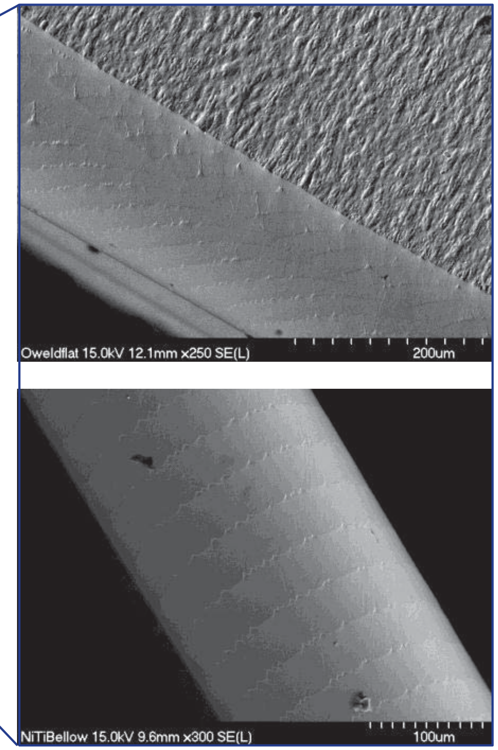


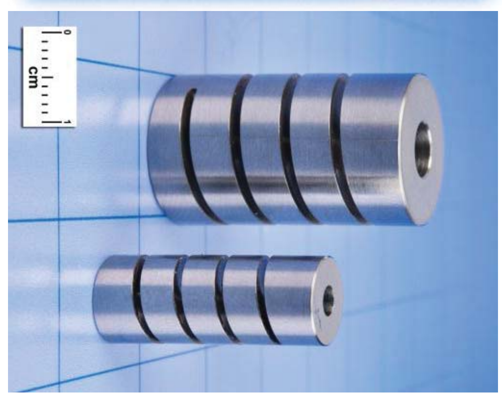
- **Outcome**
  - Direct correlations were made between macroscopic changes in actuator performance parameters, and atomic-scale evolution from neutron spectra
  - The rate of evolution of texture and volume fraction of the retained martensite plays a key role in the stability of the actuator



Neutrons can be used to study most actuator forms







CONSORTIUM FOR THE ADVANCEMENT OF SHAPE MEMORY ALLOY RESEARCH AND TECHNOLOGY

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Thank You