

# (12) United States Patent

## Welser et al.

### (54) HIGH EFFICIENCY QUANTUM WELL WAVEGUIDE SOLAR CELLS AND METHODS FOR CONSTRUCTING THE SAME

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#### Related U.S. Application Data

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#### (56) References Cited

#### U.S. PATENT DOCUMENTS



### OTHER PUBLICATIONS

Xi et al., Optical thin-film materials with low refractive index for broadband elimination of Fresnel reflection, Nature Photonics 1, 176-179 (2007). doi:10.1038/nphoton.2007.26.\*

## (lo) Patent No.: US 8,921,687 B1  $(45)$  Date of Patent: Dec. 30, 2014

Matheu, et al., "Metal and Dielectric Nanoparticle Scattering for Improved Optical Absorption in Photovoltaic Devices", "Applied Physics Letters", Sep. 18, 2008, pp. 113108-1-113108-3, vol. 93, No. 113108, Publisher: American Institute of Physics, Published in: US. Xi, et al., "Optical Thin-Film Materials With Low Refractive Index for Broadband Elimination of Fresnel Reflection", "Letters", Mar. 2007, pp. 176-179, vol. 1, Publisher: Nature Publishing Group.

\* cited by examiner

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### (57) ABSTRACT

Photon absorption, and thus current generation, is hindered in conventional thin-film solar cell designs, including quantum well structures, by the limited path length of incident light passing vertically through the device. Optical scattering into lateral waveguide structures provides a physical mechanism to increase photocurrent generation through in-plane light trapping. However, the insertion of wells of high refractive index material with lower energy gap into the device structure often results in lower voltage operation, and hence lower photovoltaic power conversion efficiency. The voltage output of an InGaAs quantum well waveguide photovoltaic device can be increased by employing a III-V material structure with an extended wide band gap emitter heterojunction. Analysis of the light IV characteristics reveals that non-radiative recombination components of the underlying dark diode current have been reduced, exposing the limiting radiative recombination component and providing a pathway for realizing solar-electric conversion efficiency of 30% or more in single junction cells.

#### 8 Claims, 5 Drawing Sheets









Fiq, 2





**Fig. 3B** 









SOLAR CELLS AND METHODS FOR CONSTRUCTING  $10$ THE SAME, the entire disclosure of which is herein incor- ture to achieve high open circuit voltages. porated by reference.

# STATEMENT REGARDING FEDERALLY<br>SPONSORED RESEARCH OR DEVELOPMENT

under Grant Number NNX11CE59P, awarded by the gap material within the depletion region adjacent to the emit-<br>National Aeronautics and Space Administration (NASA) and ter and incorporating step-graded quantum wells. This st National Aeronautics and Space Administration (NASA) and ter and incorporating step-graded quantum wells. This struc-<br>Grant Number ERDA1-0000021389 awarded by the New <sup>20</sup> ture enhances the open circuit voltage of quantum Grant Number ERDA1-0000021389 awarded by the New <sup>20</sup> ture enhances the open circuit voltage of quantum well<br>York State Energy Research and Development Authority waveguide solar cell structures. Advanced quantum well solar York State Energy Research and Development Authority waveguide solar cell structures. Advanced quantum well solar<br>(NYSERDA). The government may have certain rights in this cell structures both minimize the underlying diode (NYSERDA). The government may have certain rights in this invention. The interest of the optical path length to deliver solar rents and increase the optical path length to deliver solar

### FIELD OF THE INVENTION 25 range of spectral conditions.

state semiconductor devices, commonly known as solar cells, convert sunlight into electrical power by generating both a 35 BRIEF DESCRIPTION OF THE DRAWINGS current and a voltage upon illumination. The current source in a solar cell is the charge carriers that are created by the The invention description below refers to the accompanyabsorption of photons. These photogenerated carriers are ing drawings, of which: typically separated and collected by the use of PN or PIN FIG. 1 is a schematic cross-sectional side view of a thin junctions in semiconductor materials. The operational volt- 40 film solar cell device according to an illustrative embodiment age of the device is limited by the dark current characteristics incorporating a lower band gap, waveguiding absorption of the underlying PN or PIN junction, among other limiting layer and optical coatings to increase the optical path length characteristics. Thus improving the power output perfor- of incident light through the active region of the device; mance of any solid state solar cell generally entails simulta-<br>
FIG. 2 is a graphical diagram of the approximate refractive neously maximizing absorption and carrier collection while 45 index as a function of position profile for three different minimizing dark diode current. InGaAs quantum well waveguide solar cell structures, in

Quantum well solar cells seek to harness a wide spectrum accordance with the illustrative embodiment; of photons at high voltages in a single junction device by FIG. 3A is a graphical diagram of the photoluminescence embedding narrow energy-gap wells within a wide energy- spectra from an InGaAs quantum well solar cell structure gap matrix. By avoiding the limitations of current matching 5o having GaAs as a base structure, according to the illustrative inherent in multi junction devices, quantum well waveguide embodiment; solar cells have the potential to deliver ultra-high efficiency FIG. 3B is a graphical diagram of the photoluminescence over a wide range of operating conditions. Quantum well spectra from an InGaAs quantum well solar cell structure solar cells have been demonstrated in a variety of different having AlGaAs as a base structure, according to the illustramaterial systems, and the basic concept has been extended to 55 tive embodiment; include quantum dots. Clear improvements in lower energy FIG. 3C is a graphical diagram of the light voltage and spectral response have been experimentally confirmed in both current ("IV") characteristics from an InGaAs quantum well quantum well and quantum dot solar cells. However, photon solar cell structure having GaAs as a base structure, according absorption, and thus current generation, is hindered in con-<br>to the illustrative embodiment; absorption, and thus current generation, is hindered in con-<br>ventional quantum structured solar cells by the limited path 60 FIG. 3D is a graphical diagram of the light IV characterisventional quantum structured solar cells by the limited path 60 FIG. 3D is a graphical diagram of the light IV characteris-<br>length of incident light passing vertically through the device. tics from an InGaAs quantum well s length of incident light passing vertically through the device. Moreover, the insertion of narrow energy-gap material into GaAs as a base structure, according to the illustrative embodithe device structure often results in lower voltage operation, ment; and hence lower photovoltaic power conversion efficiency. FIG. 4 is a graphical diagram of the short circuit current

Optical scattering into laterally propagating waveguide 65 density as a function of open circuit voltage derived from increase photocurrent generation in quantum well solar cells structures, according to the illustrative embodiment;

**HIGH EFFICIENCY QUANTUM WELL** via in-plane light trapping. The refractive index contrast in a **WAVEGUIDE SOLAR CELLS AND METHODS** typical quantum well solar cell provides lateral optical con-**FOR CONSTRUCTING THE SAME** finement and naturally forms a slab waveguide structure. Coupling of normally incident light into lateral optical propa-RELATED APPLICATIONS  $\frac{5}{2}$  gation paths has been reported to lead to increases in the short circuit current of InP/InGaAs quantum well waveguide solar This application claims the benefit of U.S. Provisional cells coated with nanoparticles. However, maintaining high Application Ser. No. 61/525,707, filed Aug. 19, 2011, entitled open circuit voltage remains a universal challenge for all<br>HIGH EFFICIENCY QUANTUM WELL WAVEGUIDE quantum well and quantum dot solar cell devices. It is there-HIGH EFFICIENCY QUANTUM WELL WAVEGUIDE quantum well and quantum dot solar cell devices. It is there-<br>SOLAR CELLS AND METHODS FOR CONSTRUCTING <sup>10</sup> fore desirable to provide a device with a novel material struc-

### SUMMARY OF THE INVENTION

15 This invention overcomes the disadvantages of the prior art by providing a solar cell design and process for constructing This invention was made with U.S. government support a solar cell that employs an extended region of wide energy<br>der Grant Number NNX11CE59P, awarded by the gap material within the depletion region adjacent to the emitelectric conversion efficiencies exceeding 30% over a wide

In an illustrative embodiment, a conventional homojunc-This invention relates to semiconductor-based photovol- tion structure incorporates an InGaAs well embedded within taic energy converters, also known as "solar cells," and to the a GaAs matrix. To reduce the diode dark current, wider design and fabrication of the same. energy-gap InGaP and AlGaAs material is employed in the emitter and inserted into the depletion region adjacent to the BACKGROUND OF THE INVENTION emitter, forming an extended wide band gap emitter heterojunction structure. Illustratively, the refractive index contrast With appropriate electrical loading, photovoltaic solid is further enhanced by employing an AlGaAs base layer.

illuminated IV measurements on two different quantum well

density as a function of quantum well energy for an InGaAs In an illustrative embodiment one or more of the layers in the

a function of base layer energy gap for both coated and provide a mechanism by which incident light can be scattered<br>uncoated devices, according to the illustrative embodiment: horizontally into the plane of the underlying uncoated devices, according to the illustrative embodiment; and In the illustrative embodiment shown in FIG. 1, the PIN

conventional GaAs solar cell performance to an InGaAs 10 quantum well structure, according to the illustrative embodi-<br>lower energy gap material 134 within the depletion region of ment. **the PIN diode structure 130.** Lower energy gap material also

volume of low band gap material, and thus requires advanced SiGe, SiC, etc.), group III-V materials (GaAs, A1GaAs, light trapping structures to reach its potential performance InGaP, InGaAs, InP, AlInAs, GaAsSb, InAsSb, AlAsSb, levels. Light management is achieved by assuring that inci- GaN, InGaN, A1GaN, etc.), group II-VI materials (CdS, dent photons are not lost due to reflections but are instead 20 CdTe, etc.), and group I-III-VI<sub>2</sub> materials (CIGS, etc.). In directed into the semiconductor absorbing layers. The scat- another illustrative embodiment, the PIN diode device structering of incident light to ensure each photon has a non-<br>normal trajectory is a strategy for increasing the optical path illustrative embodiment, the refractive index and thickness of normal trajectory is a strategy for increasing the optical path length of photons within the absorption layer. In addition, the the semiconductor materials used in the top window/contact application of a back reflector to bounce any unabsorbed 25 layers  $132$  is tailored to function as part of a step graded photons back up into the active layers of the device is a refractive index antireflection structure. Electrical contact is beneficial aspect of any effective photovoltaic light trapping made to the top window/contact layers 132 via metal contacts scheme. However, the most effective light trapping schemes 125. will also direct light horizontally into the plane of the absorb-<br>In the illustrative embodiment shown in FIG. 1, the back of ing layer. Waveguide structures in which thin layers of high 30 the semiconductor PIN diode 130 is coated with a conductive, refractive index material are surrounded by low refractive transparent optical coating 140. In an illustrative embodi-

structure is depicted in FIG. 1. This thin film waveguide solar 35 ing metallic layer **150.** In another illustrative embodiment, the cell incorporates lower band gap, higher index of refraction bottom optical coating 140 consists of multiple layers differmaterials in the active region of the device, along with tai- ing in refractive index to form a distributed Bragg reflector. In lored, nanostructured optical coatings. The optical path yet another illustrative embodiment one or more of the layers length of light incident upon this novel device is dramatically in the bottom optical coating 140 also incorporate nanoparenhanced via coupling into laterally propagating waveguide 40 ticles or nanorods. In yet another illustrative embodiment, the modes. This combination of active device structure and pas- back-scattering structure, consisting of the back optical coatsive coatings redirects normally incident light into laterally ing 140 and back metal contact **150,** employ plasmonic strucpropagating waveguides modes, and represents a dramatic tures. Plasmonic structures closely coupled to absorbing change in thin film solar cell design. Semiconductors can be used to increase the photocurrent in a

taic device **100** is depicted according to an illustrative length of the plasmon resonance is adjustable to match the embodiment. In operation, incident light 101 first encounters absorption band of the nearby semiconductor layers, particua top covering surface 110, which can be a top cover glass, larly the lower band gap, higher index material 134. For a transparent epoxy or other light transmitting covering sur- more detailed description of methods for the construction of face. A front anti-reflective coating 105 is applied to the top 50 the back reflector structure **140, 150,** refer to commonly covering surface according to an illustrative embodiment. assigned provisional patent application Ser. No. 13/528,581, The top covering surface 110 is located above a PIN diode filed Jun. 20, 2012, entitled DIFFUSE OMNI-DIRECsemiconductor material device structure 130. The PIN diode TIONAL BACK REFLECTORS AND METHODS OF structure is coated with a transparent optical coating 120 that MANUFACTURING THE SAME, by Welser, et al., the minimizes reflection losses and scattering incident light into 55 teachings of which are incorporated by reference as useful the underlying PIN diode 130. For a more detailed description background information. the underlying PIN diode 130. For a more detailed description of methods for the construction of the top antireflective coat- In the illustrative embodiment shown in FIG. 1, optical ing 120, refer to commonly assigned provisional patent appli- scattering by the nanoparticles or nanorods above the semication Ser. No. 13/528,792, filed Jun. 20, 2012, entitled LAT- conductor device structure can lead to coupling of photons ERALLY SCATTERING ANTIREFLECTIVE COATINGS 60 incident normal to the device surface into lateral optical<br>AND METHODS OF MANUFACTURING THE SAME, by propagation paths, i.e., paths parallel to the device surface. Welser, et al., the teachings of which are incorporated by These parallel optical modes 170 result from the introduction

tratively adapted to generate a graded index of refraction 65 length of photons through thin film solar cell device strucantireflection coating, consisting of one or more layers with tures. Unabsorbed, lower energy photons that are not coupled

 $3 \hspace{2.5cm} 4$ 

FIG. 5 is a graphical diagram of the saturation current material 110 and the PIN diode semiconductor material 130. quantum well solar cell with an extended heterojunction, top optical coating 120 also incorporate nanoparticles or according to the illustrative embodiment; nanorods which differ in refractive index from that of their FIG.  $\vec{\bf{6}}$  is a graphical diagram of the short circuit current as  $\vec{5}$  surrounding material. Nanostructured optical coatings 120 function of base layer energy gap for both coated and provide a mechanism by which in

FIG. 7 is a graphical diagram of IV curves comparing diode device structure consists of top window/contact layers nower tional GaAs solar cell performance to an InGaAs 10 132, back surface field/contact layers 136, and inc tends to have a higher index of refraction, thereby resulting in DETAILED DESCRIPTION the formation of a waveguide structure. The PIN diode device 15 structure can consist of any common semiconductor materi-A typical thin film solar cell structure contains a limited als, including but not limited to group IV materials (Si, Ge,

index material provide a physical mechanism by which to ment, the refractive index of the bottom optical coating 140 achieve this type of in-plane light trapping.<br>has a value of approximately 1.5 or lower, thereby creating hieve this type of in-plane light trapping. has a value of approximately 1.5 or lower, thereby creating an A schematic diagram of an exemplary waveguide solar cell Omni-directional reflector when combined with the underly-Omni-directional reflector when combined with the underly-With reference to FIG. 1, a thin film waveguide photovol-45 variety of thin film solar cells. In particular, the peak wave-

propagation paths, i.e., paths parallel to the device surface. reference as useful background information. of a lateral wave vector component into the forward scattered The refractive index of the top optical coating 120 is illus- wave **160,** and can dramatically enhance the optical path refractive index intermediate between the covering surface into the waveguide modes 170 pass through the PIN diode

140. Back-scattered light 180 is directed into the active, absorbing layers of the device by the presence of the back- the scattered wave, and can dramatically enhance the optical scattering structure, which consists of the back optical coat- path length of photons through thin film solar cell device ing 140 and back metal contact 150. 5 structures.

According to various embodiments, the front optical coat-<br>  $\frac{1}{20}$  Oblique-angle deposition is a method of growing arrays of<br>  $\frac{1}{20}$  is configured and arranged with transparent antire-<br>
nanorods in a wide variety of flection coating structures to reduce the reflection of incident diffusion and self-shadowing effects during the deposition photons at the material interface between the light transmit- process. Because the resulting thin films are porous, obliqueting covering surface 110 and semiconductor device structure 10 angle deposition is utilized as an effective technique for tai-**130.** The back optical coating 140 is configured and arranged loring the refractive index of a variety of thin film materials to maximize the reflection of unabsorbed photons back into (see for example, by way of useful background, J.-Q. Xi, M. the semiconductor device structure. In the various embodi- F. Schubert, J. K. Kim, E. F. Schubert, M. Chen, S.-Y. Lin, W. ments, the front coating 120 and the back coating 140 are Liu, and J. A. Smart, *Optical Thin-Film Materials with Low*  implemented in accordance with industry standard processes 15 *Refractive Index for Broad-Band Elimination of Fresnel* and materials known to those skilled in the art. These mate-<br> *Reflection*, Nat. Photon., vol. 1, pp. 1 rials include, but are not limited to, titanium dioxide, silicon illustrative embodiment, the bottom optical coating 140 comdioxide, indium tin oxide, zinc oxide, and other transparent prises of a layer nanostructured, porous indium tin oxide layer conductive oxides (TCOs). The antireflection coating can be with a refractive index of 1.5 or lower deposited by oblique synthesized using a variety of techniques, including sputter- 20 angle deposition. In another illustrative embodiment, the top ing, evaporation, and oblique-angle deposition. Transparent optical coating 120 comprises multiple layers, with at least antireflection coating structures can comprise a single layer one layer of dense indium tin oxide and at least one layer of or multiple layers of materials having an index of refraction porous indium tin oxide or porous titanium dioxide deposited intermediate between the semiconductor structure 140 and by oblique-angle deposition. the media in which the incident photons are delivered, which 25 In another illustrative embodiment, the top optical coating by way of example is illustrated as a cover glass or encapsu- 120 and the bottom optical coating 140 comprise dielectric lant 110 in FIG. 1. Back reflector structures can comprise and/or metallic nanoparticles embedded within a dense optieither a single metallic layer, or a plurality of layers consisting cal film material. Examples include SiO<sub>2</sub> nanoparticles of a metallic layer in combination with one or more layers of embedded within a dense layer of indium tin oxide,  $SiO<sub>2</sub>$ transparent optical material having an index of refraction  $30$  nanoparticles embedded within a dense layer of TiO<sub>2</sub>, TiO<sub>2</sub> lower than the semiconductor material. In particular, Omni- nanoparticles embedded within a transparent encapsulant, directional reflectors (ODRs), which combine a metal layer  $\overline{10}_2$  nanoparticles embedded within a dense layer of SiO<sub>2</sub>, with a low-refractive index layer, provide ultra-high reflec- and metallic nanoparticles embedde tivity over a wide range of wavelengths and incident angles. ITO. Note that deposition of the nanoparticles can occur

index of the various layers is as follows: the front antireflec- ments. tive coating 105 has a refractive index of n~1 to 1.5, the cover The operating voltage of a semiconductor PIN diode solar glass or encapsulant 110 of n~1.5, the forward scattering cell 130 is generally dictated by the underlying dark diode antireflection coating  $120$  of n $\sim$ 1.5 to 3, the top window current of the device. The dark diode current of semiconduccontact layer 132 of  $n-3$ , the PIN diode with lower band gap, 40 tor devices is composed of several different components, all higher index material 134 of n-3.8, the back surface field of which are dependent upon the energy gap of the material contact layer **136** of n-3, and the back scattering optical used in the active junction of the device. Typically, each cell coating of  $n-1.1$ . The refractive index of the various layers is in a solar cell consists of one type of material, and the energy variable within ordinary skill to achieve the desired function- gap of that material influences both the current and voltage

with a continuous thin film material, the forward- and back-<br>lower operating voltage. Therefore, it is desirable to provide scattered light is well known to depend upon the optical a device structure **130** that can harness the current generating properties of the thin film and surrounding environments capabilities of narrow energy gap material while also mainwhich dictate the reflection, refraction, and absorption char- 50 taining a high operating voltage. acteristics of the light. Employing an array of nanoparticles or Reference is now made to FIG. 2, showing a graphical nanorods can provide unique and desirable physical phenom- diagram **200** of the approximate refractive index as a function ena, particularly when the particle size is very small com- of position profile for three different InGaAs quantum well pared to the incident wavelength. In this case, the scattering waveguide solar cell structures, according to the illustrative and absorption characteristics of the forward wave front 55 embodiment. An extended region of wide energy gap material depend upon the size, shape, density, and permittivity of the is employed within the depletion region a depend upon the size, shape, density, and permittivity of the nanoparticles. See for example, by way of useful background ter and incorporates step-graded quantum wells. For a information, P. Matheu, S. H. Lim, D. Derkacs, C. detailed description of structures of quantum wells, refer to McPheeters, and E. T. Yu, *Metal and dielectric nanoparticle* commonly assigned U.S. patent application Ser. No. 12/985, *scattering for improved optical absorption in photovoltaic* 60 748, filed Jan. 6, 2011, entitled QUA *devices, Appl. Phys. Lett. 93, 113108-1-3 (2008). Nanopar*ticle coatings can provide additional light-trapping benefits STRUCTING THE SAME, by Welser et al., the teachings of when the adjoining semiconductor device structure contains which are incorporated by reference as useful background distinct index of refraction steps. In this case, optical scatter- information. In a conventional homojunction structure, an ing by nanoparticles atop a semiconductor device structure 65 InGaAs well is embedded within a GaAs matrix, resulting in can lead to coupling of photons incident normal to the device a refractive index profile such as that can lead to coupling of photons incident normal to the device surface into lateral optical propagation paths, i.e., paths par-<br>dashed line 210 in FIG. 2. To reduce the diode dark current

 $5\qquad \qquad 6$ 

130 device before striking a back scattering optical coating allel to the device surface. These parallel optical modes result 140. Back-scattered light 180 is directed into the active, from the introduction of a lateral wa

nanorods in a wide variety of materials, enabled by surface Reflection, Nat. Photon., vol. 1, pp. 176-179, 2007). In one

and metallic nanoparticles embedded within a dense layer of According to an illustrative embodiment, the refractive 35 according to conventional techniques in illustrative embodi-

alities as described herein. 45 output of the device. Lower energy gap material can enhance When light is incident upon a semiconductor device coated the current generating capability, but typically results in a

748, filed Jan. 6, 2011, entitled QUANTUM WELL WAVEGUIDE SOLAR CELLS AND METHODS OF CON-

below that obtained in conventional structures, wider energygap InGaP and A1GaAs material is employed in the emitter and inserted into the depletion region adjacent to the emitter, forming an extended wide band gap emitter heterojunction structure. Other materials can be employed as conventionally 5 available and employed by those having ordinary skill to achieve the desired functionalities. The circle-dashed line 220 in FIG. 2 illustrates this second type of quantum well structure. To further enhance the refractive index contrast around the InGaAs well, a third structure employs anAlGaAs io base layer, as shown by the solid black line 230 in FIG. 2.

The InGaAs quantum well solar cell structures described herein are illustratively synthesized via metal-organic chemical vapor deposition (MOCVD) by Kopin Corporation. Any appropriate chemical vapor deposition technique can be <sup>15</sup> employed, as readily apparent to those having ordinary skill. Single InGaAs quantum wells with a target thickness of approximately 33 nm are located within the built-in field of the junction depletion region. A step-graded InGaAs compositional profile is employed to form a series of smaller energy 20 steps (~35 meV) that photogenerated carriers can overcome to escape from the potential well. The effective energy gap of the InGaAs well is a function of both the well compositional profile and thickness, and can be quantified by photoluminescence (PL) emissions. The illustrative structures are charac- 25 terized by PL measurements generated with excitation from both 532 nm and 785 nm laser sources.

Small, simple mesa test devices are fabricated with standard wet etch chemistry and photolithography to define devices with junction area as small as approximately 75 µmx75 µm. A variety of tests can be performed on these devices, including measuring dark current versus voltage, capacitance versus voltage, and illuminated current versus voltage measurements. For light I-V measurements, the photocurrent is generated by illumination with an un-calibrated 35 halogen lamp through a probe station microscope that can be varied in intensity. A test structure consisting of a device with a junction area of approximately 200 µmx340 µm and an open aperture of approximately 120  $\mu$ m × 260  $\mu$ m is used to measure the illuminated current versus voltage characteristics of all 40 three structures. In addition, the extended heterojunction structure with a GaAs base has been re-grown and fabricated into a larger, nearly 500 µmx500 µm device. Specifically, the larger device has a junction area of approximately 0.2236  $mm<sup>2</sup>$ , and an aperture area that is nearly 98.4% of the junction 45 area. While the results obtained from the smaller devices are consistent with the larger devices, the larger relative aperture size of the 500  $\mu$ m $\times$ 500  $\mu$ m device enables the illuminated I-V performance to be characterized at slightly higher current consistent with the larger devices, the larger relative aperture<br>size of the 500  $\mu$ m $\times$ 500  $\mu$ m device enables the illuminated I-V<br>performance to be characterized at slightly higher current<br>densities. 50 s

The photoluminescence spectra and light IV characteristics from the two InGaAs quantum well solar cell structures employing an extended wide energy-gap emitter are shown in FIGS. 3A-3D. More specifically, FIG. 3A is a graphical diagram of the photoluminescence spectra from an InGaAs 55 quantum well solar cell structure having GaAs as a base structure. FIG. 3B is a graphical diagram of the photoluminescence spectra from an InGaAs quantum well solar cell structure having A1GaAs as a base structure. FIG. 3C is a graphical diagram of the IV characteristics from an InGaAs 60 quantum well solar cell structure having GaAs as a base structure. FIG. 3D is a graphical diagram of the IV characteristics from an InGaAs quantum well solar cell structure having GaAs as a base structure.

As shown in FIGS. 3A and 3B, in both structures, the PL 65 emission from the step-graded InGaAs well peaks (316, 326) near 1.30 eV, while the extended A1GaAs emitter material

luminescence peaks (317, 327) around 1.72 eV. The base layer emissions differ, as expected, with a peak 318 near 1.42 eV for the GaAs base structure line 315 and a peak 328 of approximately 1.52 eV for the A1GaAs base structure line 325.

Overall, the illuminated current-voltage characteristics 330, 340 shown in FIGS. 3C and 3D of the two emitter heterojunction structures are quite similar. Small area test devices on both structures exhibit fill factors near 83%, short circuit current density  $(J_{sc})$  on the order of 25 mA/cm<sup>2</sup> at maximum halogen lamp intensity, and open circuit voltage  $(V_{oc})$  approaching 1.05 V. These open circuit voltage values are higher than the  $V_{oc}$ -0.97 V obtained on the control structure without the extended heterojunction, and comparable to the  $V_{oc}$  of state-of-the-art bulk GaAs single junction cells, despite the addition of a narrower energy gap InGaAs well.

To further quantify the voltage characteristics of the InGaAs quantum well waveguide solar cells, the short circuit current at varying white light intensities have been analyzed as a function of open circuit voltage. The  $J_{sc}$ -V<sub>oc</sub> curve that results from characterizing and plotting the short circuit current as a function of open circuit voltage provides an effective measurement of the underlying dark diode current, unencumbered by the effects of series resistance. FIG. 4 illustrates a graphical diagram 400 that compares the diode current 410 of a conventional structure to the diode current 420 of the InGaAs quantum well structure with a GaAs base layer and an extended heterojunction fabricated into a  $0.2236$  mm<sup>2</sup> device. A dramatic reduction in the n=2 space charge recombination is observed (412), allowing the n=1 saturation current density  $(J_{01})$  to be extracted from a two-diode fit (422) of the short circuit current versus open circuit voltage data. The diode fit assumes the underlying dark current can be described as the sum of two diodes at room temperature  $(25^{\circ} C)$ , one with an ideality factor of one  $(n=1)$  as line 410 and the other with an ideality factor of two  $(n=2)$  as line 420. Diode fits indicate that the n=1 saturation current density of the diode current can be reasonably fit as  $J_{01} = 4.5 \times 10^{-17}$  mA/cm<sup>2</sup> for both InGaAs quantum well solar cells employing an extended heterojunction.

While Shockley injection typically limits the n=1 component of bulk III-V diodes, radiative recombination within the InGaAs quantum well could also play a role. Indeed, the observed lack of sensitivity of the voltage characteristics to the addition of aluminum to the base layer may suggest that radiative limits have been reached at 1-sun bias levels in quantum well solar cells employing an extended heterojunction structure. The concept of detailed balance is a well established means of computing the expected radiative current that should limit the performance of photonic devices. As noted by Henry (see, for example, C. H. Henry, "Limiting Efficiencies of Ideal Single and Multiple Energy-gap Terrestrial Solar Cells," J. Appl. Phys., vol. 51, pp. 4494-4500, August 1980), the n=1 saturation current density  $(J_{o1})$  in the radiative limit should equal the thermal radiation current  $(J_{th})$ , such that:

$$
J_{th} = \left(\frac{q(n_{cell}^2 + 1)kTE_g^2}{4\pi^2\hbar^5c^2}\right) \exp\left(\frac{-E_g}{kT}\right) \tag{1}
$$

where  $E_g$  corresponds to the peak energy of the photons emitted at temperature T. An absorbing bottom substrate is assumed in Equation (1), with photons escaping via the top surface into a media with a refractive index  $(n_{top})$  of one (e.g. air). Following the teachings of Henry, it is assumed in Equation (1) that the refractive index of the cell  $(n_{cell})$  and the bottom substrate ( $n_{bottom}$ ) are both equal to that of GaAs  $(n_{GaAs}$ ~3.5). Assuming an effective energy gap of 1.3 eV for the InGaAs well, Equation (1) implies  $J_{o1} = 1 \times 10^{-15}$  mA/cm<sup>2</sup>, which is nearly an order and a half higher in magnitude than the value inferred from measurements on InGaAs quantum <sup>5</sup> wells with an extended heterojunction structure. This indicates that the InGaAs quantum well structures are actually operating in a regime of suppressed radiative recombination.

A number of different physical mechanisms can lead to a suppression in radiative current relative to that predicted by 10 Equation (1), including the finite volume of the InGaAs well, photon recycling, and perturbations in the diode quasi-Fermi level. Photon recycling is an intriguing phenomenon that can be leveraged to further reduce the dark current and hence increase the operation voltage of InGaAs quantum well solar <sup>15</sup> cells operating in the radiative limit. Radiative emissions can be suppressed in structures which support the re-absorption of emittedphotons by reflecting emitted photons back into the absorber region of the device. In the devices described herein, such photon recycling is expected to be negligible due to 20 basic geometrical considerations associated with fabricating test structures with limited lateral dimensions on a relatively thick substrate  $(-625 \,\mu m)$ . However, photon recycling effects can be greatly enhanced by removing the GaAs substrate and fabricating devices with a thin-film architecture. Back reflec- 25 tions and photon recycling are further enhanced by the use of an omni-directional back reflector incorporating a low index film between the substrate and the back metal (such as coating **140** of FIG. 1). FIG. 5 illustrates a graphical diagram **500** of the potential reduction in dark current that is realized by <sup>30</sup> fabricating InGaAs quantum well solar cells with an extended heterojunction in a thin-film format which promotes efficient light trapping. The dashed line 510 represents the results of a traditional detailed balance calculations (for example as articulated by Henry hereinabove) assuming optically thick <sup>35</sup> cells and an absorbing substrate. The solid lines 520, 530 and 540 represent a modified model that employs extended wide band gap emitters and projecting the impact of photon recycling.

Enhanced light trapping, in addition to providing an <sup>40</sup> avenue to further suppress radiative recombination, is leveraged to dramatically increase the short circuit current of thin film solar cells. Photon absorption, and thus current generation, is typically hindered in conventional thin film solar cell designs, including quantum well structures, by the limited 45 path length of incident light passing vertically through the device structure. FIG. 6 illustrates a graphical diagram **600** of the projected short circuit current of InGaAs waveguide solar cells employing a single 33 nm well with an absorption edge at 950 nm  $(-1.3 \text{ eV})$  embedded within a 0.5  $\mu$ m higher energy 50 gap base layer. The calculations summarized in FIG. 6 employ realistic estimates of the absorption coefficient and assume the solar spectrum can be approximated by that of a 5800K blackbody. Under these conditions, the short circuit current of uncoated cells typically decreases slightly with <sup>55</sup> increasing base layer energy gap, as shown by line 610. Applying a standard two-layer antireflection (AR) coating to the front surface and employing a simple reflector at the back surface to double the optical path length is shown at line 620 to nearly double the short circuit current. Short circuit cur- <sup>60</sup> rents approaching  $40 \text{ mA/cm}^2$  are projected for devices with 1.3 eV wells that employ more advanced light trapping structures to leverage the waveguide properties of the quantum well structure and further increase the optical path length. Even higher short circuit currents are shown as line **630** from <sup>65</sup> light trapping structures employing lower energy gap wells. We note that AMO (and AM1.5) efficiencies in excess of 30%

can be achieved in devices that can combine  $J_{o1}$  values on the order of  $1 \times 10^{-18}$  mA/cm<sup>2</sup> with J<sub>sc</sub> values above 40 mA/cm<sup>2</sup> (or  $32 \text{ mA/cm}^2$ ).

Conventional state-of-the-art GaAs solar cells output nearly 34 mA/cm<sup>2</sup> of current at a  $V_{oc}$  just over 1.04 volts under AMO illumination, yielding a solar-electric conversion efficiency approaching 22%. Increasing the efficiency to 30% in space environments requires novel device designs that can boost both the current and voltage output. The InGaAs quantum well structures with an extended wide band gap emitter described herein have the ability to increase both the operating voltage and current of GaAs-based solar cells. By suppressing both non-radiative and radiative recombination, the underlying dark current is dramatically reduced and the operating voltage of the device is increased. The addition of lower energy gap InGaAs also raises the current generating capability of GaAs-based solar cells. However, to achieve enhanced current output, advanced light trapping techniques are desirably incorporated into the overall device design.

Photon absorption, and thus current generation, is hindered in quantum well structures by the limited path length of incident light passing vertically through the device structure. Optical scattering into lateral waveguide structures provides a physical mechanism to dramatically increase photocurrent generation through in-plane light trapping. Moreover, lateral waveguide modes can be enhanced by the higher refractive index of the InGaAs well.

The application of light trapping structures both above and below the active region can increase the optical path length of lower energy photons through the quantum wells. Light trapping can also reduce radiative recombination, and thus further increase the operating voltage of InGaAs quantum wells with extended wide band gap emitters, via the well-established phenomena of photon recycling. Nanostructured optical coatings offer unique methods for engineering the optical properties of thin film coatings.

Nanostructured indium tin oxide (ITO) with low refractive index (n) can be employed in omni-directional reflector (ODR) structures consisting of a low-n dielectric/metal film bilayer. ODRs combine the omni-directionality of metal films with the high peak reflectivity of a distributed Bragg reflector (DBR), and can function as a high-performance back reflector in an InGaAs quantum well waveguide solar cell. Mie scattering from the nano structured ITO layer can also enhance the coupling of long wavelength photons into the lateral waveguide modes of the quantum well absorber layer.

FIG. 7 shows a graphical diagram **700** of the projected performance of a 30% efficient device employing both an InGaAs quantum well/extended wide band gap emitter and advanced light trapping structures. Conventional state-ofthe-art GaAs solar cells collect approximately 85% of the current available in an AMO space spectrum above approximately 1.42 eV, the band gap of the GaAs absorber layer. Significant increases in the current output 710 of conventional designs are unlikely, as much of the current loss is due to reflection and absorption of high energy photons in the overlaying cover glass, AR coatings, and top surface of the semiconductor window layer. InGaAs quantum well structures, however, provide a pathway to generate higher currents via the collection of lower energy photons. The projected 44  $mA/cm<sup>2</sup>$  current density of the InGaAs quantum well device shown as line 720 in FIG. 7 assumes a 95% collection efficiency for the otherwise uncollected photons between approximately 1.26 eV and 2.1 eV in the AMO spectrum. Collection efficiencies of 95% or higher are readily available in bulk III-V semiconductor devices, but will require increasing the optical path length through a 300 A quantum well via light trapping by a factor of 50-100x.

The projected open circuit voltage of the InGaAs quantum well device shown in FIG. 7 assumes the dark current is limited by radiative recombination, and that the radiative recombination suppression factor (RSF) is 200. Photon recycling due to the reflection and re-absorption of emitted photons is expected to further decrease the radiative current density by over IOx, and thus should ultimately lead to RSF values well in excess of 200 in devices with light trapping.

Accordingly, the unique material structure described herein minimizes the dark current of InGaAs quantum wells, and when coupled with advanced light trapping structures, provides a pathway to increase the efficiency of single junction GaAs-based solar cells to over 30%. Record high open circuit voltages have been demonstrated in InGaAs quantum well waveguide solar cell structures. Higher open circuit voltages result from the use of a novel structure incorporating a wide band gap barrier layer within a heterojunction depletion region to suppress non-radiative recombination. A dramatic reduction in the n=2 space charge recombination is observed, allowing the n=1 saturation current density to be extracted from a simple two-diode fit of the short circuit current versus open circuit voltage data. Analysis suggests that these highvoltage InGaAs quantum well devices are operating in a regime of suppressed radiative recombination. The applica- 25 tion of advanced light trapping structures provides a means to both further suppress the radiative dark current and enhance the optical path length within the absorbing layers. The resulting increases to the operating voltage and short circuit current are projected to result in solar-electric conversion efficiencies 30 exceeding 30%. 10

The illustrative embodiments of a quantum well waveguide solar cell described herein with reference to FIGS. **2-6**  employs a single narrow energy gap InGaAs well. However, the teachings herein are applicable to structures employing more than one quantum well. Such multiple quantum well structures are well-known to those ordinarily skilled in the art of III-V materials and devices. An extension of the structure depicted in FIG. 2 divides the single InGaAs quantum well shown into two or more InGaAs wells, separated from each another by wider energy gap barrier material. The wider energy gap material can include GaAs or A1GaAs (as shown in FIG. 2), or can include wide band-gap, strain-balancing material such as GaP, InGaP, or GaAsP.

Furthermore, the illustrative embodiments of a waveguide solar cell described herein with reference to FIGS. **2-6**  employs III-V material. However, the teachings herein are applicable to similar structures employing other material types. For example both the narrow band gap well and the wider band gap extended emitter, base, widow and back surface field layers could be composed of chalcogenide materials such as copper indium gallium (di)selenide (CIGS). According to an illustrative embodiment, CIS or CIGS with high indium compositions is employed for the narrow band gap well, while CGS or CIGS with high gallium compositions are used elsewhere in the structure. CdS and other wide band gap materials can also be employed in the extended emitter <sup>55</sup> and back surface field regions. Finally, the thickness of the narrow band gap well is not necessarily constrained in chalcogenide materials, and it does not need to exhibit quantum well effects. For example a well or wells of CIS or CIGS with high indium compositions can be thicker than 50 nm, but are 60 desirably still be placed within the depletion region and away from the zone of enhanced space charge recombination.

The foregoing has been a detailed description of illustrative embodiments of the invention. Various modifications and additions can be made without departing from the spirit and scope of this invention. Each of the various embodiments

described above may be combined with other described embodiments in order to provide multiple features. Furthermore, while the foregoing describes a number of separate embodiments of the apparatus and method of the present invention, what has been described herein is merely illustrative of the application of the principles of the present invention. For example, the illustrative embodiments can include additional layers to perform further functions or enhance existing, described functions. Likewise, while not shown, the electrical connectivity of the cell structure with other cells in an array and/or an external conduit is expressly contemplated and highly variable within ordinary skill. More generally, while some ranges of layer thickness and illustrative materials are described herein. It is expressly contemplated that additional layers, layers having differing thicknesses and/or material choices can be provided to achieve the functional advantages described herein. In addition, directional and locational terms such as "top", "bottom", "center", "front", "back", "above", and "below" should be taken as relative conventions only, and not as absolute. Furthermore, it is expressly contemplated that various semiconductor and thin films fabrication techniques can be employed to form the structures described herein. Accordingly, this description is meant to be taken only by way of example, and not to otherwise limit the scope of this invention.

What is claimed is:

- 1. A photovoltaic device comprising:
- a base layer,
- a step-graded quantum well comprising InGaAs, the stepgraded quantum well embedded within the base layer, the step-graded quantum well forming a series of approximately 35 meV energy steps between each step; and
- an extended emitter region disposed directly adjacent to the base layer, thereby falling within a junction depletion 35 region, the extended emitter including a lightly or undoped first material having a higher energy gap than the base layer;
	- an emitter disposed adjacent to the extended emitter region, the emitter including a second material having a higher energy gap and opposite doping polarity than the base layer.

2. The photovoltaic device of claim 1 wherein the base layer comprises A1GaAs.

3. The photovoltaic device of claim 1 wherein the base layer comprises GaAs.

4. The photovoltaic device of claim 1 wherein the semiconductor depletion region comprises a PIN diode including at least one of: a group IV, group III-V, group II-VI and group I-III-VI<sub>2</sub> semiconductor materials.

5. The photovoltaic device of claim 4 wherein a back surface of the PIN diode is coated with a conductive, transparent optical coating having a refractive index in the range of 1.05 and 1.5.

6. The photovoltaic device of claim 1 wherein the quantum well comprises material that has a lower energy gap relative to the base layer material.

7. The photovoltaic device of claim 1, wherein a photoluminescence spectrum output of the solar cell structure when exposed to an un-calibrated halogen lamp comprises a first peak at approximately 1.30 eV corresponding to the stepgraded quantum well and a second peak at approximately 1.72 eV corresponding to the extended emitter region.

8. The photovoltaic device of claim 1, wherein a saturation current density of the photovoltaic device is less than  $10^{-17}$  $mA/cm<sup>2</sup>$ , indicating that the step-graded quantum well is operating in a regime of suppressed radiative current.