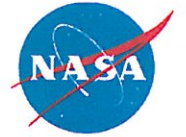


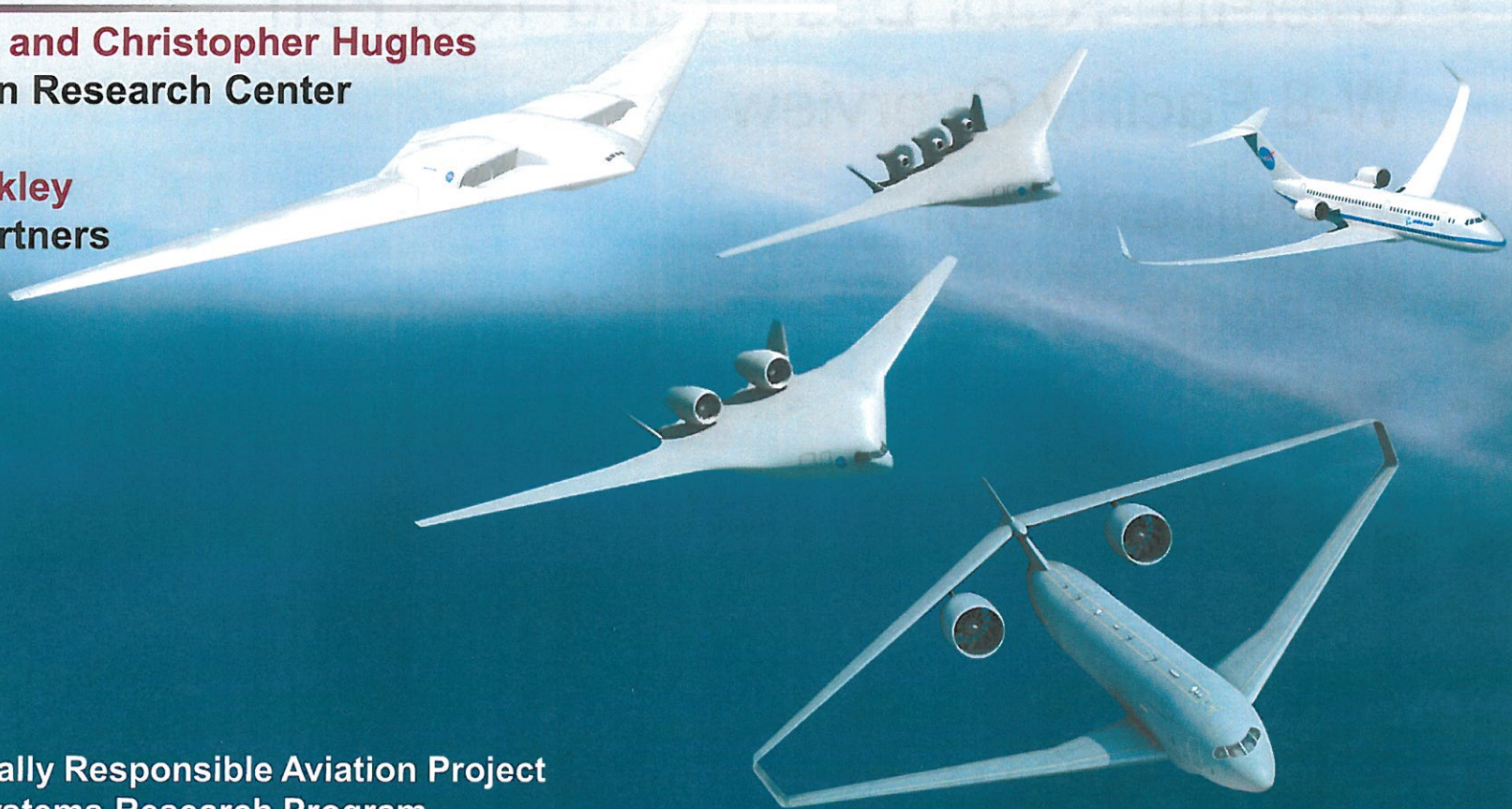
National Aeronautics and Space Administration



# The Aerodynamic Performance of an Over-the-Rotor Liner with Circumferential Grooves on a High Bypass Ratio Turbofan Rotor

**Rick Bozak and Christopher Hughes**  
NASA Glenn Research Center

**James Buckley**  
Vantage Partners



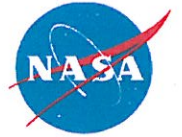
Environmentally Responsible Aviation Project  
Integrated Systems Research Program

ASME Turbo Expo June 2-7, 2013

[www.nasa.gov](http://www.nasa.gov)

# Outline

---



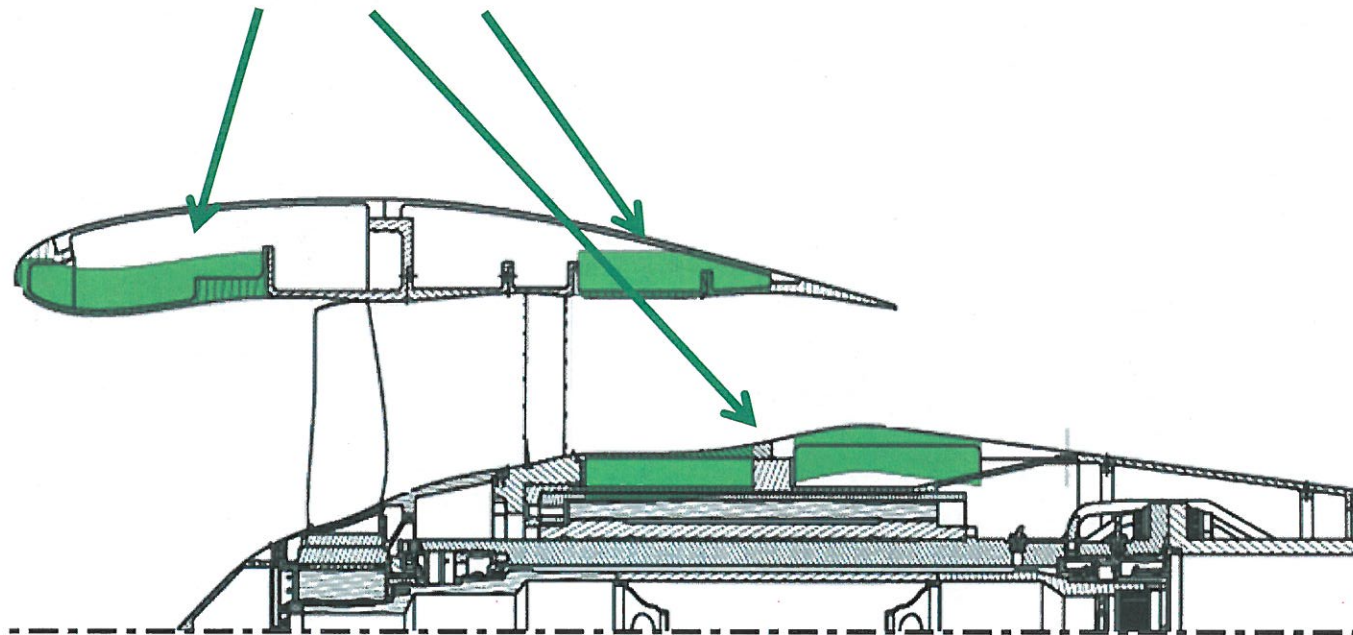
- Over-the-Rotor Treatment Development at NASA
- Over-the-Rotor Design and Test Fan
- W-8 Facility Overview
- Instrumentation
- Measurement Uncertainties
- Test Results
- 9x15 Wind Tunnel Test

# Over-the-Rotor Acoustic Treatments

---

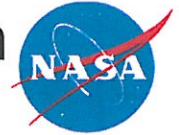


## Traditional Liner Locations

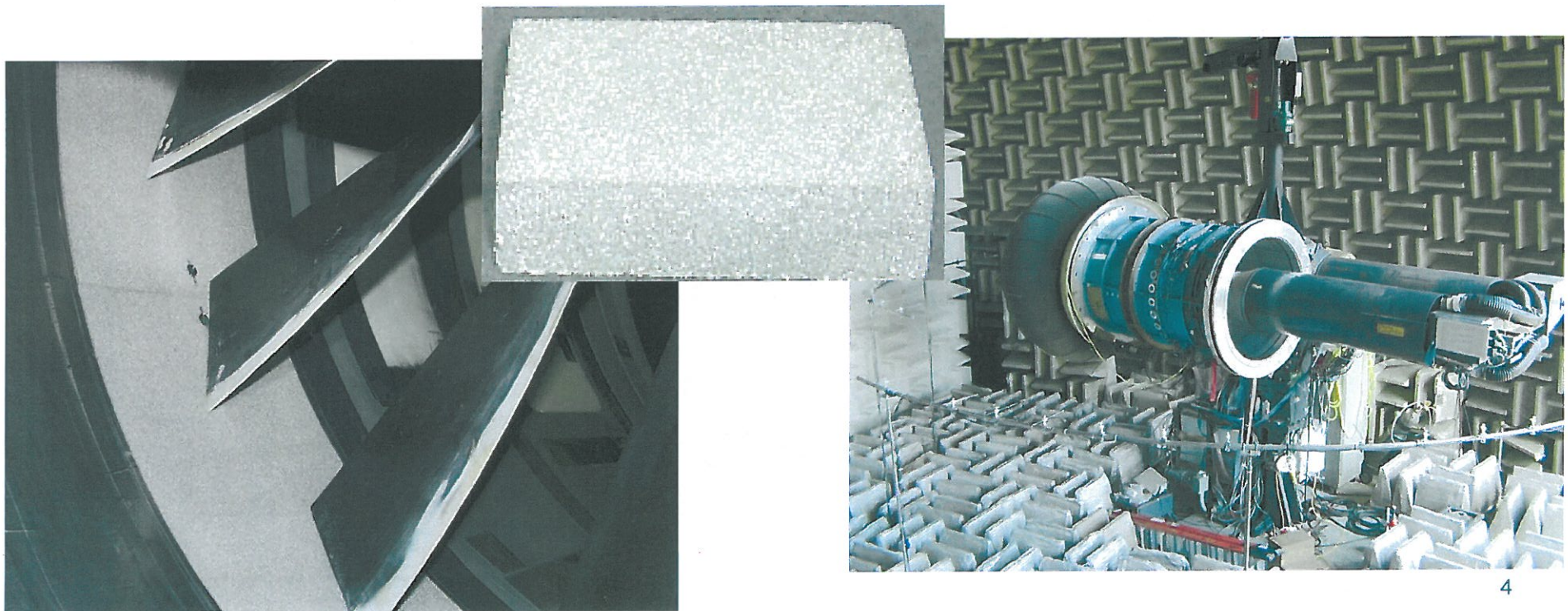


# Foam Metal Over-the-Rotor Liner on a Low Speed Fan

Sutliff and Jones, AIAA 2008-2897



- A foam metal liner was installed directly over-the-rotor as well as about a chord forward and aft of the rotor.
- Up to 4dB of broadband attenuation was achieved.
- The liner altered the tip flow and increased the size and strength of the rotor tip vortex.
- Fan performance cannot be evaluated on this low speed fan.

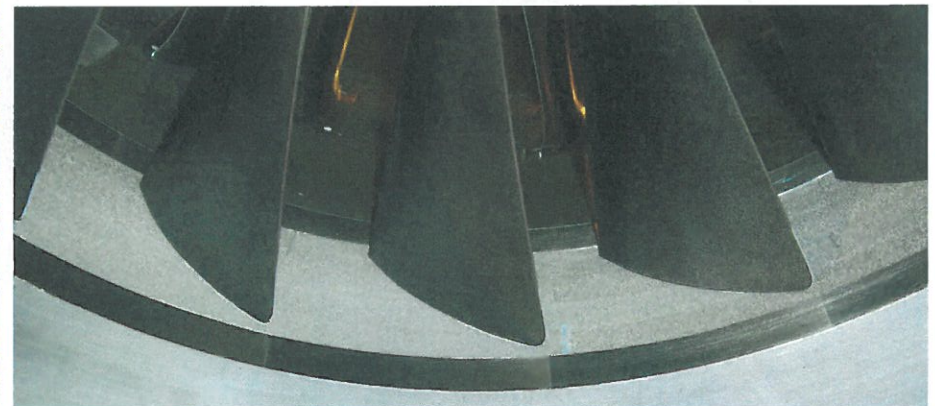
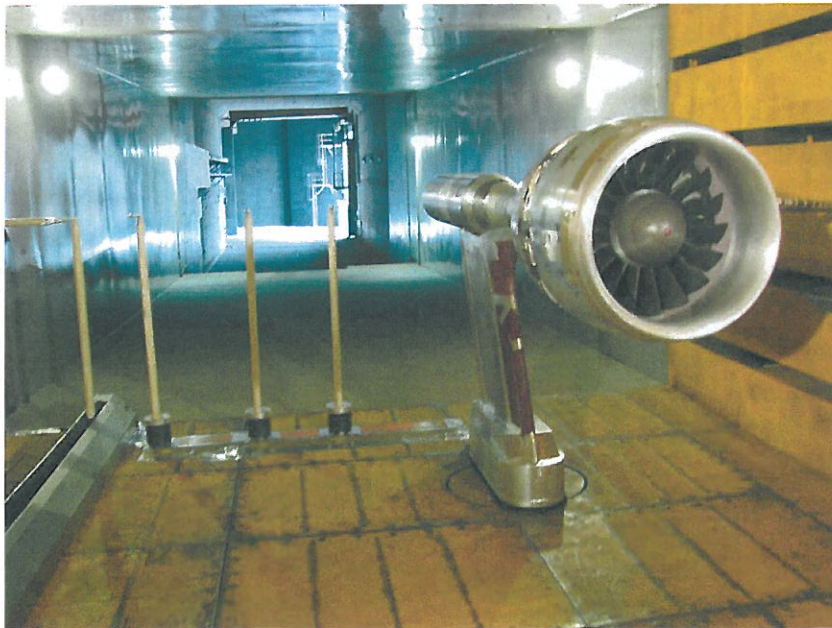
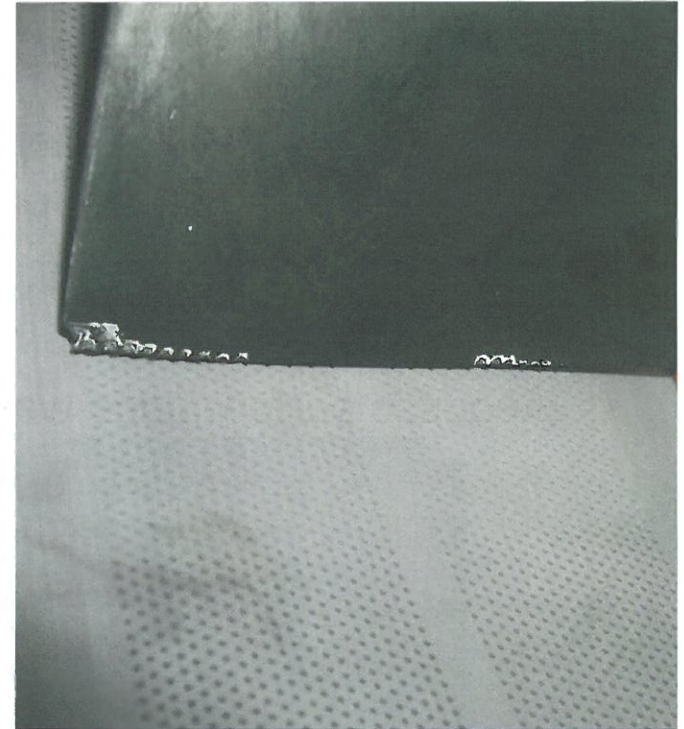


# The Advanced Ducted Propulsor Test in the 9x15 Wind Tunnel

Elliott, Woodward, and Podboy, AIAA 2009-3140  
Hughes and Gazzaniga, AIAA 2009-3139

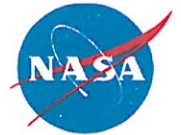


- A foam metal liner was installed directly over-the-rotor and behind a perforated sheet.
- The broadband noise reduction resulted in a 1 dB reduction in overall acoustic power level.
- The treatment caused a 3.75% to 8.75% loss in efficiency compared to a hardwall baseline case.
- The composite fan blades were damaged by pressure fluctuations through the perforated plated.

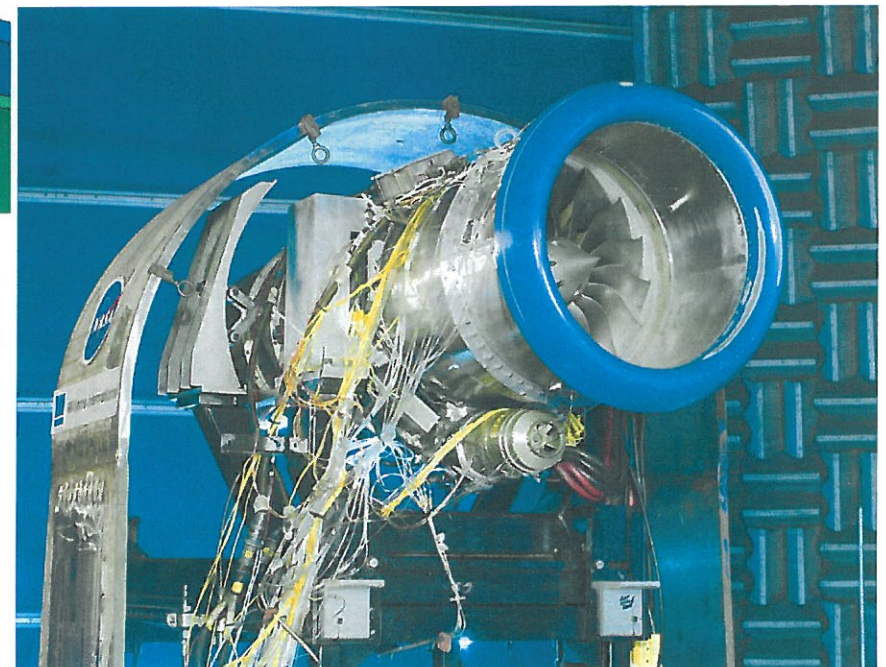
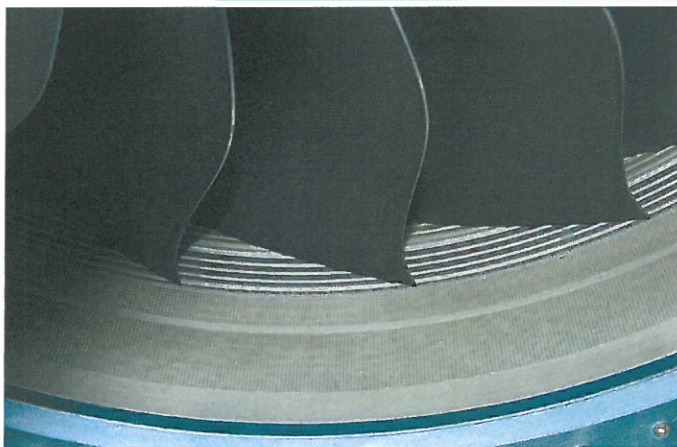
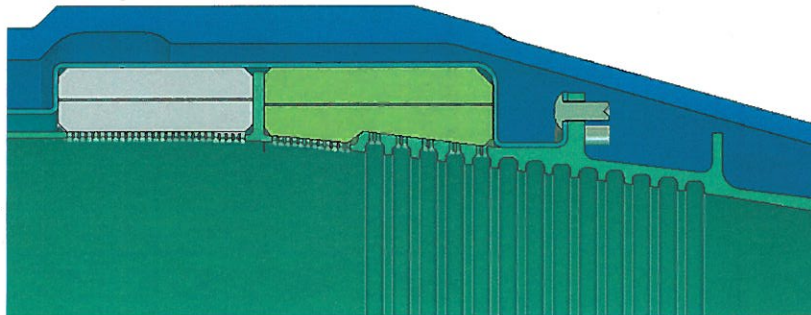


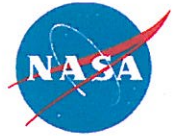
# Williams International FJ44-3A Static Engine Test

Sutliff, Elliott, Jones and Hartley, AIAA 2009-3141



- Foam metal liner was installed behind a perforated plate in the inlet
- The over-the-rotor section covered the forward 1/3 of the blade chord and was installed behind circumferential grooves.
- 5dB inlet acoustic power level attenuation (2.5dB overall)
- Up to a 2% loss in performance
- Acoustic performance was reduced at sonic tip speeds

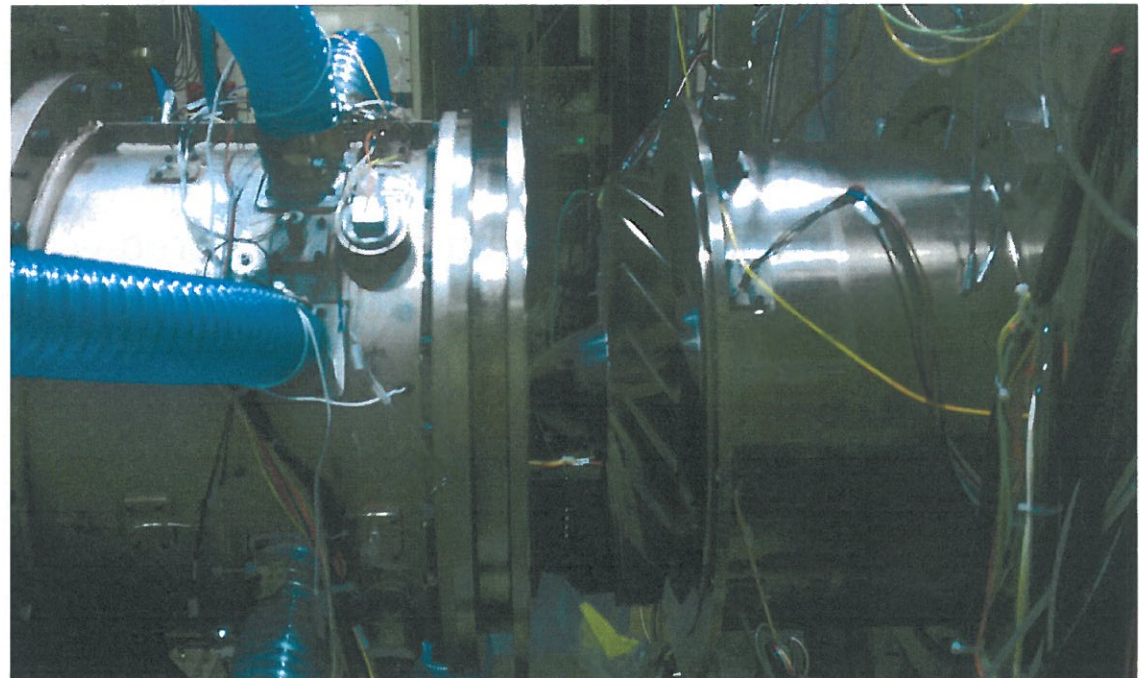




# Source Diagnostic Test Hardware

- The Source Diagnostic Test hardware was tested in a rotor alone configuration in the 9x15 wind tunnel and the W-8 Single Stage Axial Compressor Facility in the early 2000's
- R4 Fan: 22 blades
- 12,657 RPMc design speed and pressure ratio of 1.5
- Testing at part speed was used to simulate a lower pressure ratio fan at subsonic tip Mach numbers.

% Design Speed	RPM <sub>c</sub>	Nominal Mass Flow, lb <sub>m</sub> /sec
50.0%	6329	46.8
61.7%	7809	57.7
65.0%	8227	60.9
70.0%	8860	65.8
77.5%	9809	73.2
87.5%	11075	83.6

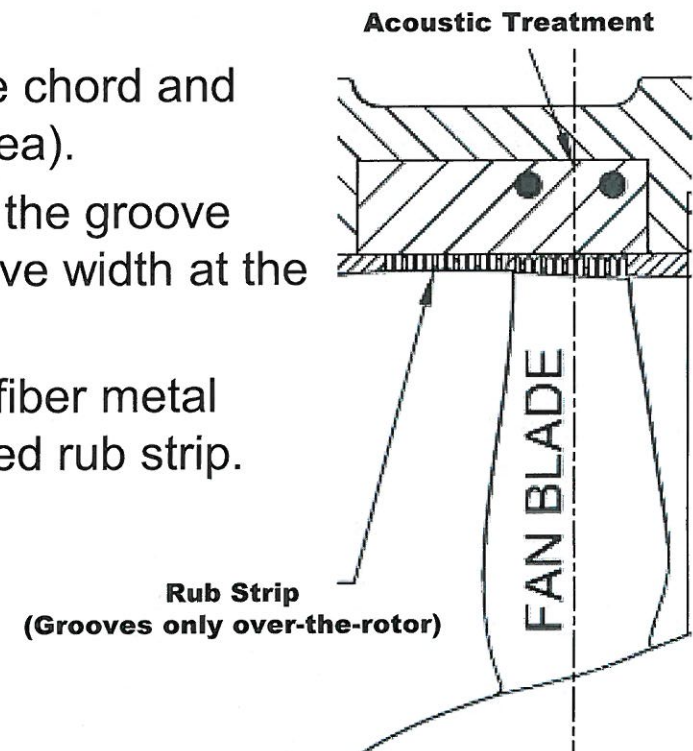




# Over-the-Rotor Liner Design

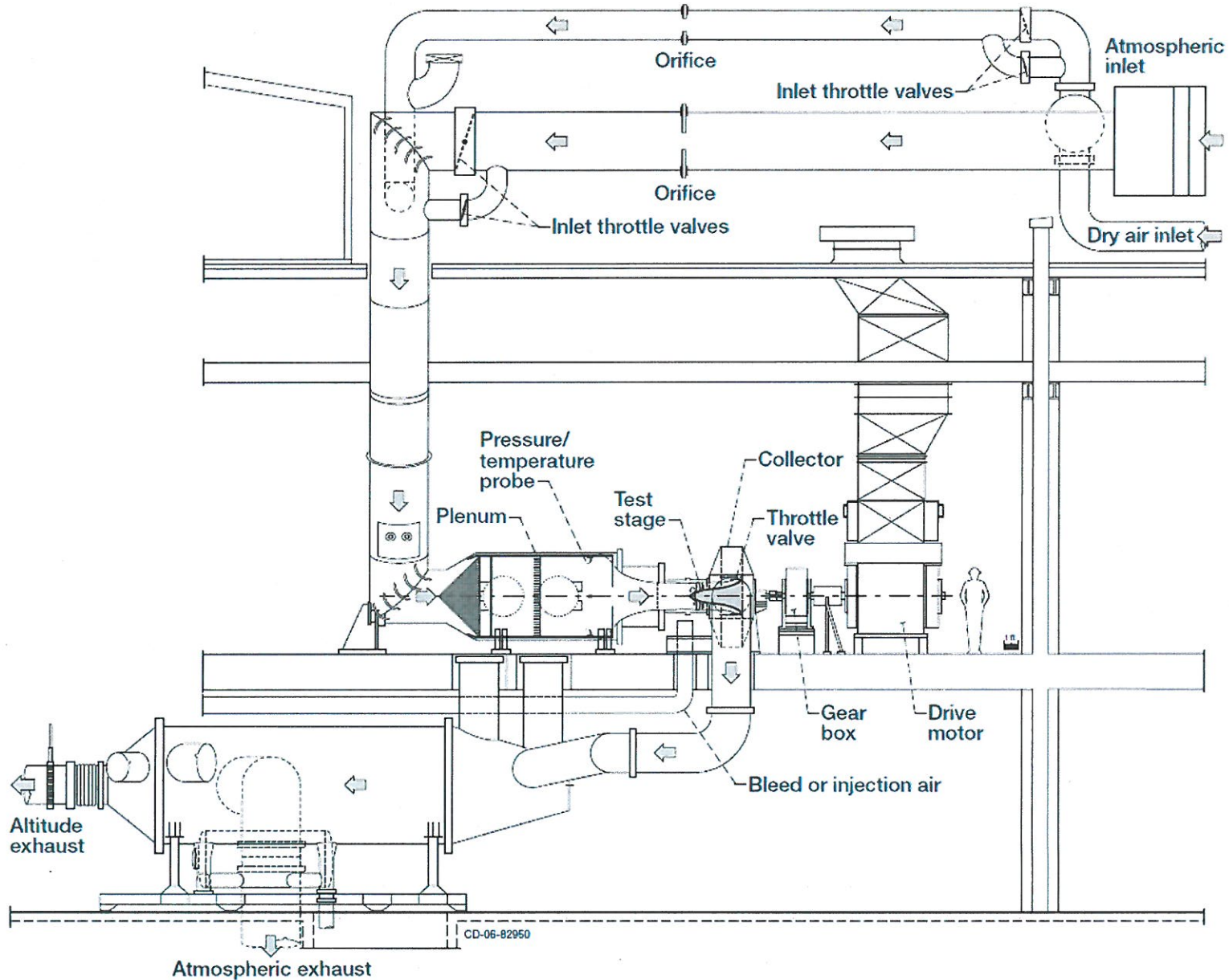
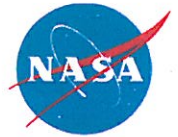
- Acoustic design by Mike Jones (NASA Langley Research Center)
- Aerodynamic design by Dan Tweedt (AP Solutions)
- Hardware design by Jim Buckley (Vantage Partners)

- The circumferential grooves cover the entire blade chord and have about 67% open area (groove width/ total area).
- The depth of the grooves vary from about 2 times the groove width at the rotor leading edge to 3 times the groove width at the rotor trailing edge.
- Slots in the bottom of the grooves covered with a fiber metal screen allow acoustic waves to through the grooved rub strip.

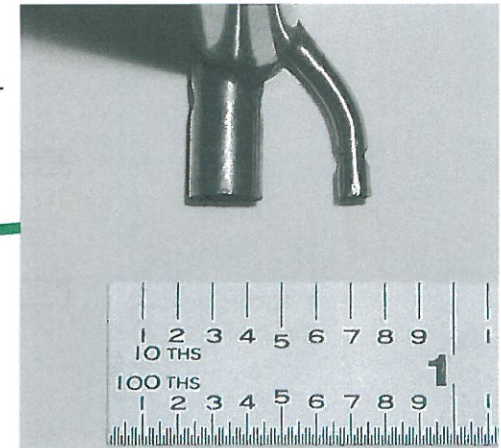
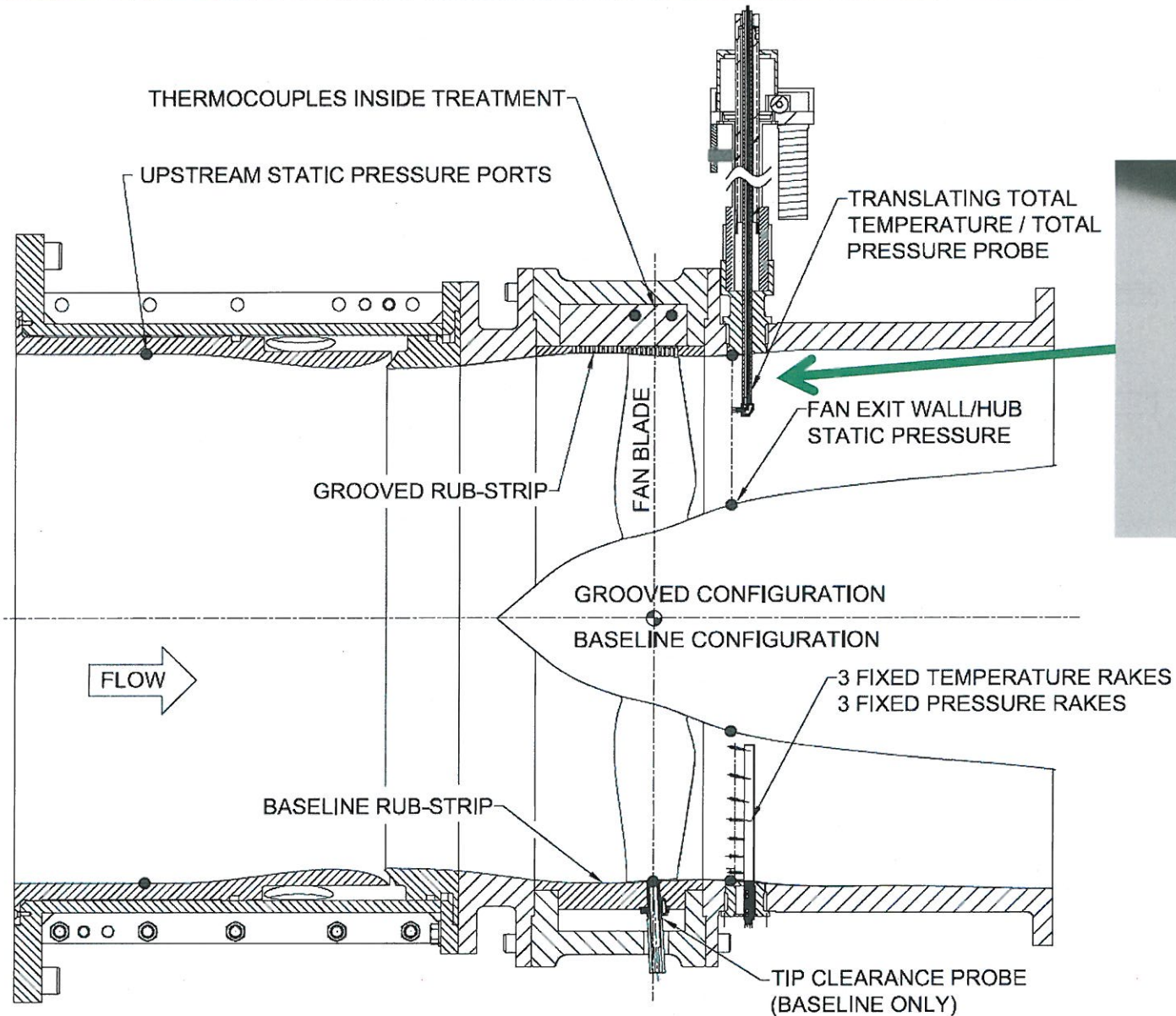
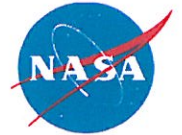




# W-8: Single-Stage Axial Compressor Facility

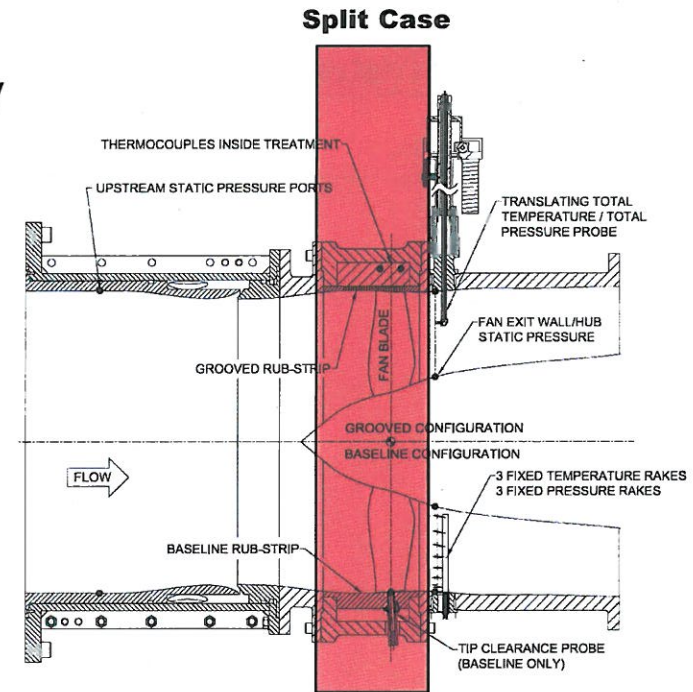


# Test Hardware and Instrumentation

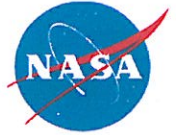


# Measurement Uncertainties

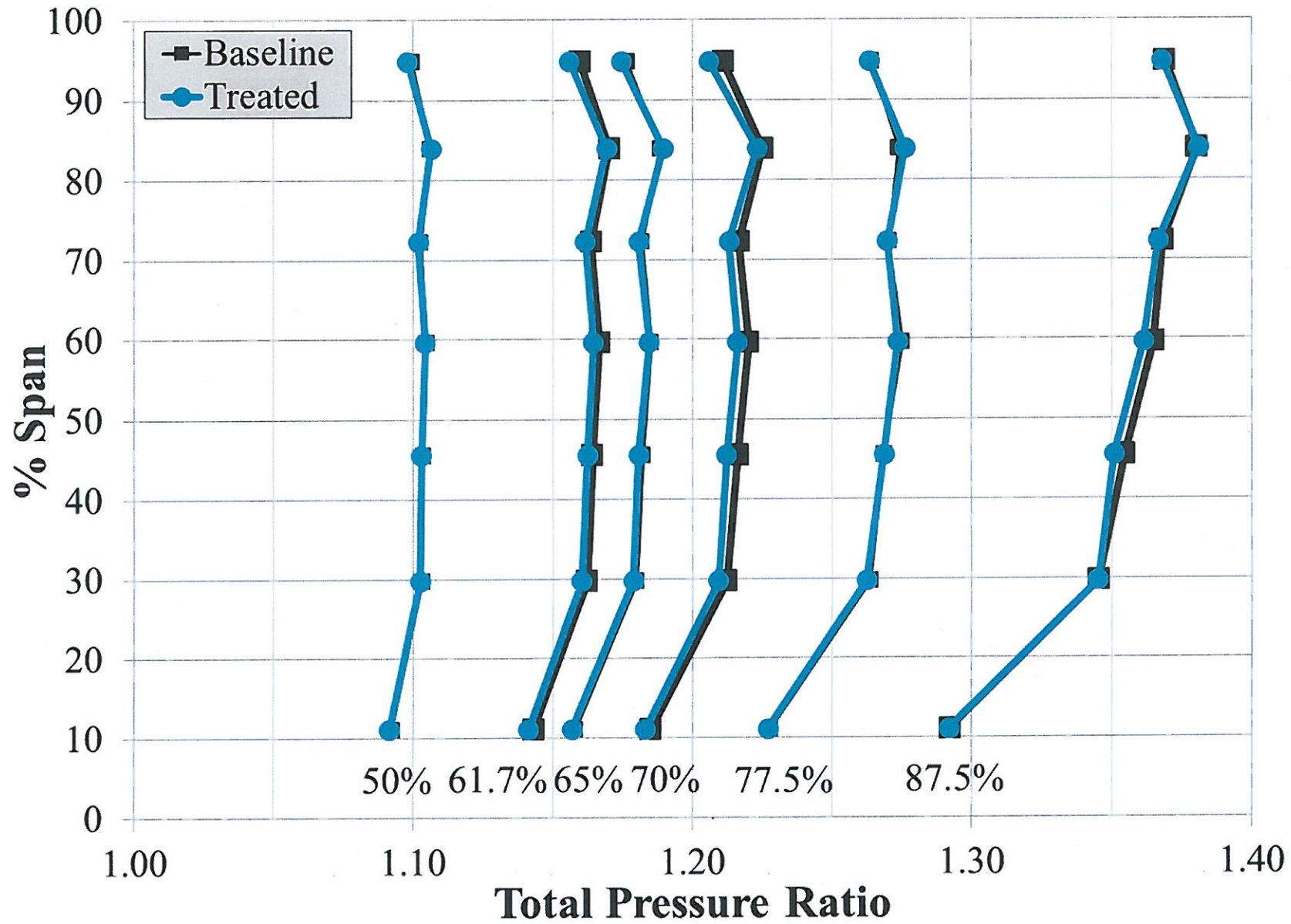
- When the desired result is a  $\Delta$  between two configurations, bias errors can be minimized by reducing the differences between the two configurations.
- Precision errors, some bias errors, and nonlinear errors cannot be reduced.
- The remaining errors could only be estimated from the experimental results.



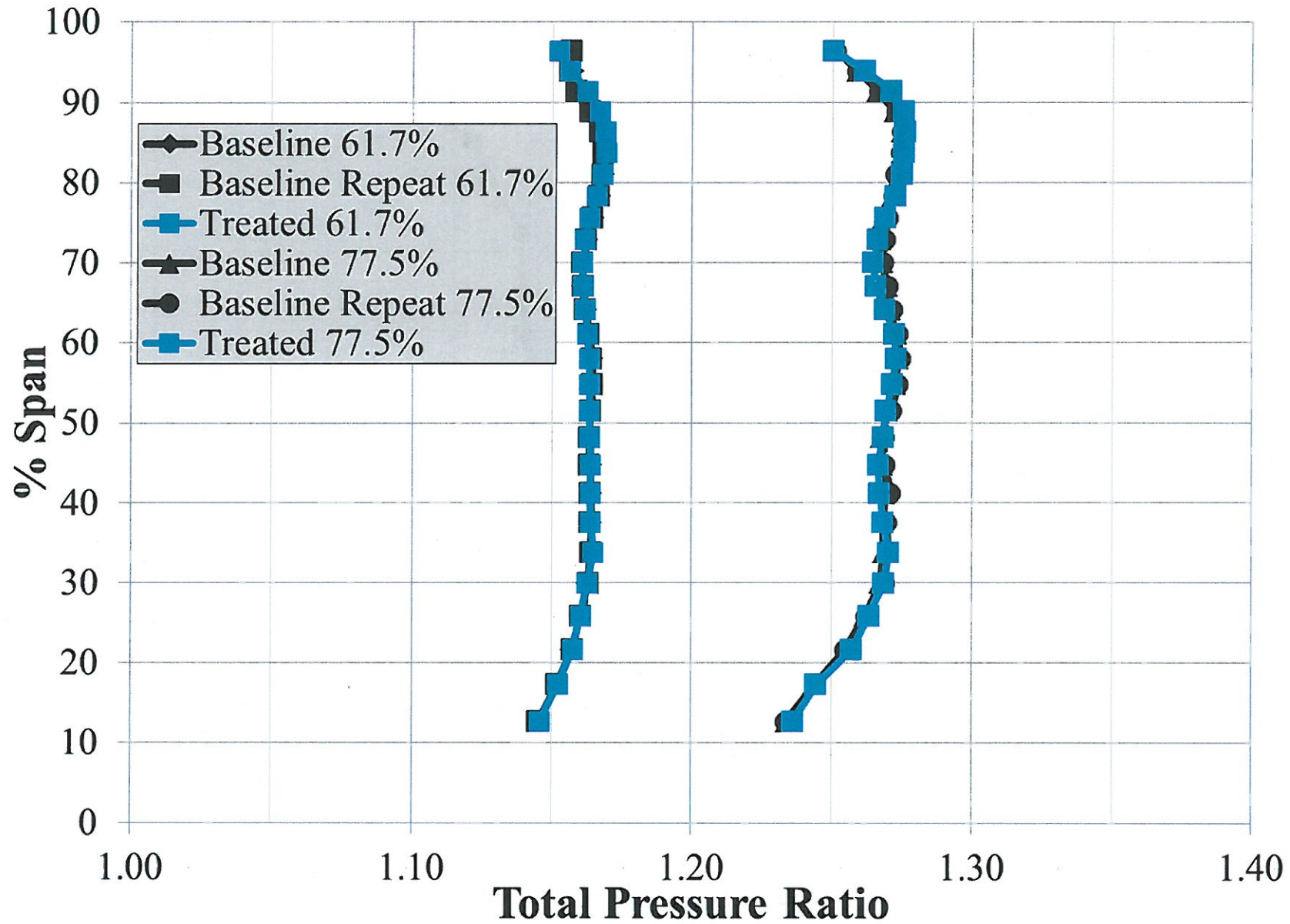
% Design Speed	RPM <sub>c</sub>	Fan Total Pressure Ratio (PR) Relative Errors		Fan Total Temperature Ratio (TR) Relative Errors		Fan Adiabatic Efficiency (FAE) Relative Errors	
		Absolute Uncertainty, %	Repeatability, %	Absolute Uncertainty, %	Repeatability, %	Absolute Uncertainty, %	Repeatability, %
61.7%	7809	±0.52	±0.04	±16.0	±0.03	±13.9	±0.77
77.5%	9809	±0.31	±0.06	±10.7	±0.04	±8.9	±0.65
87.5%	11075	±0.23	±0.11	±8.4	±0.07	±7.2	±0.60

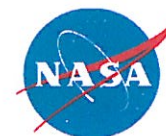


# Rake Averaged Fan Pressure Ratio

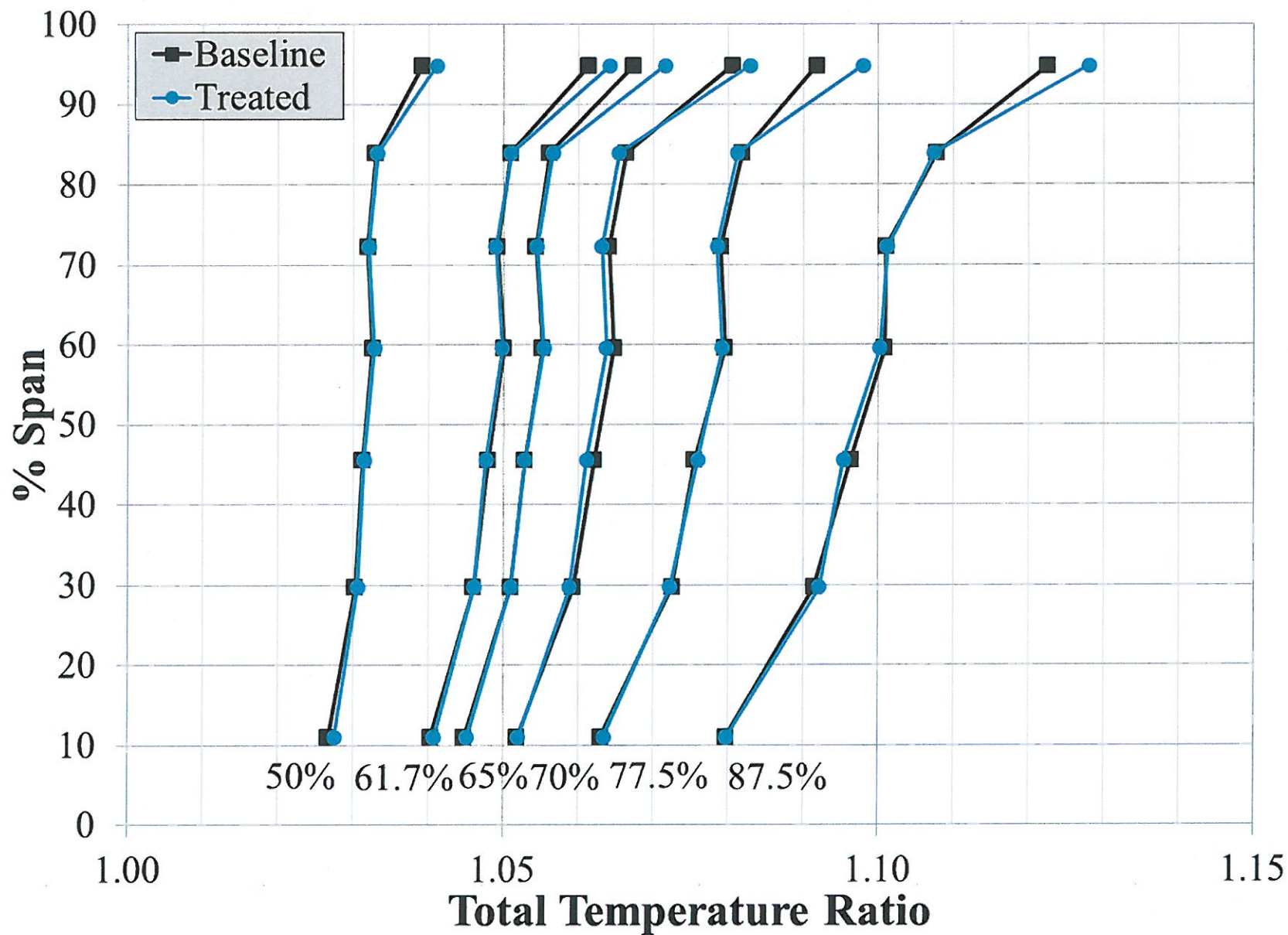


# Total Pressure Probe Survey

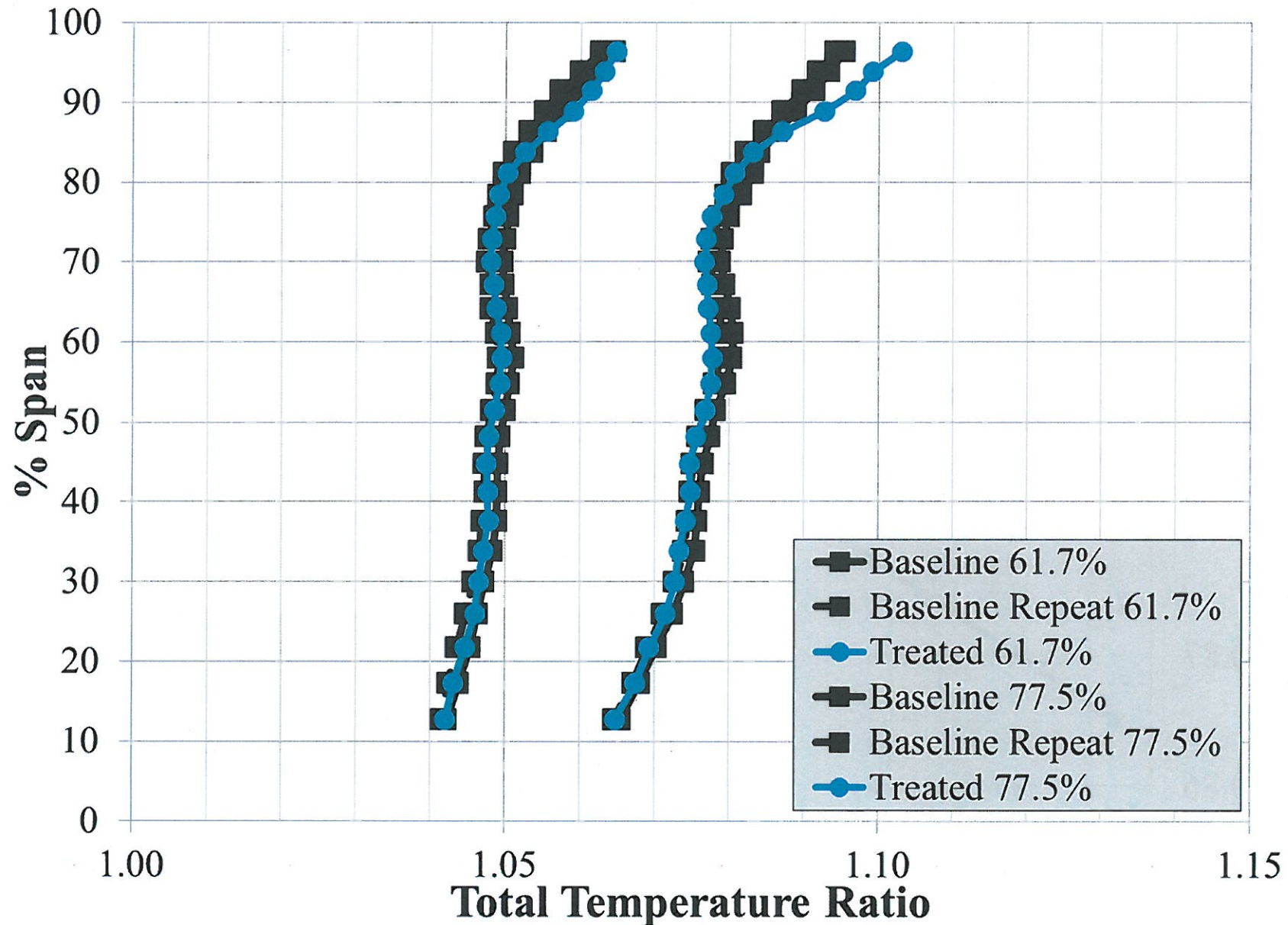
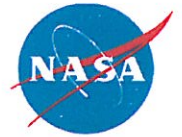




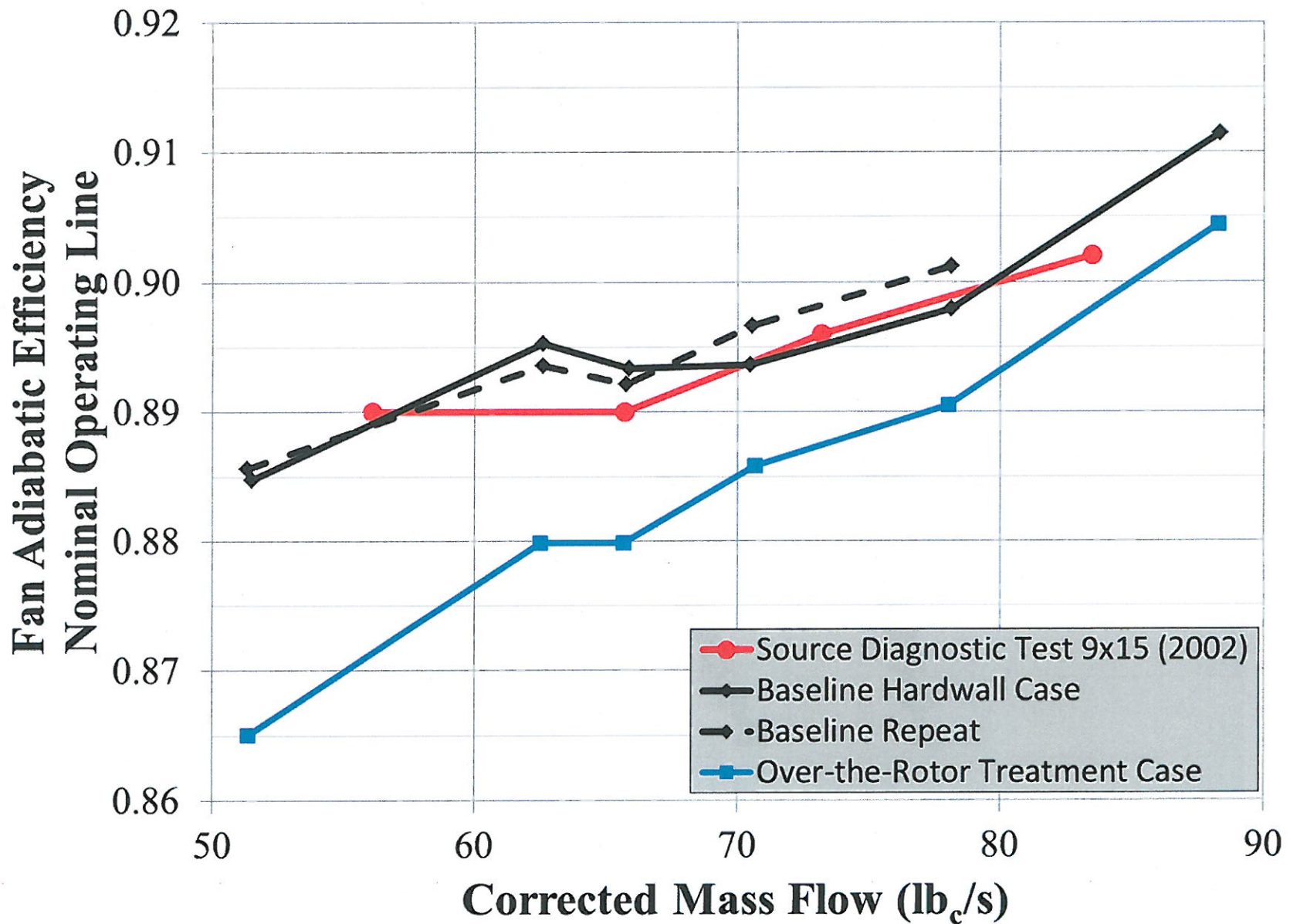
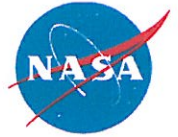
# Rake Averaged Fan Temperature Ratio



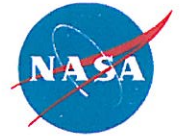
# Total Temperature Probe Survey



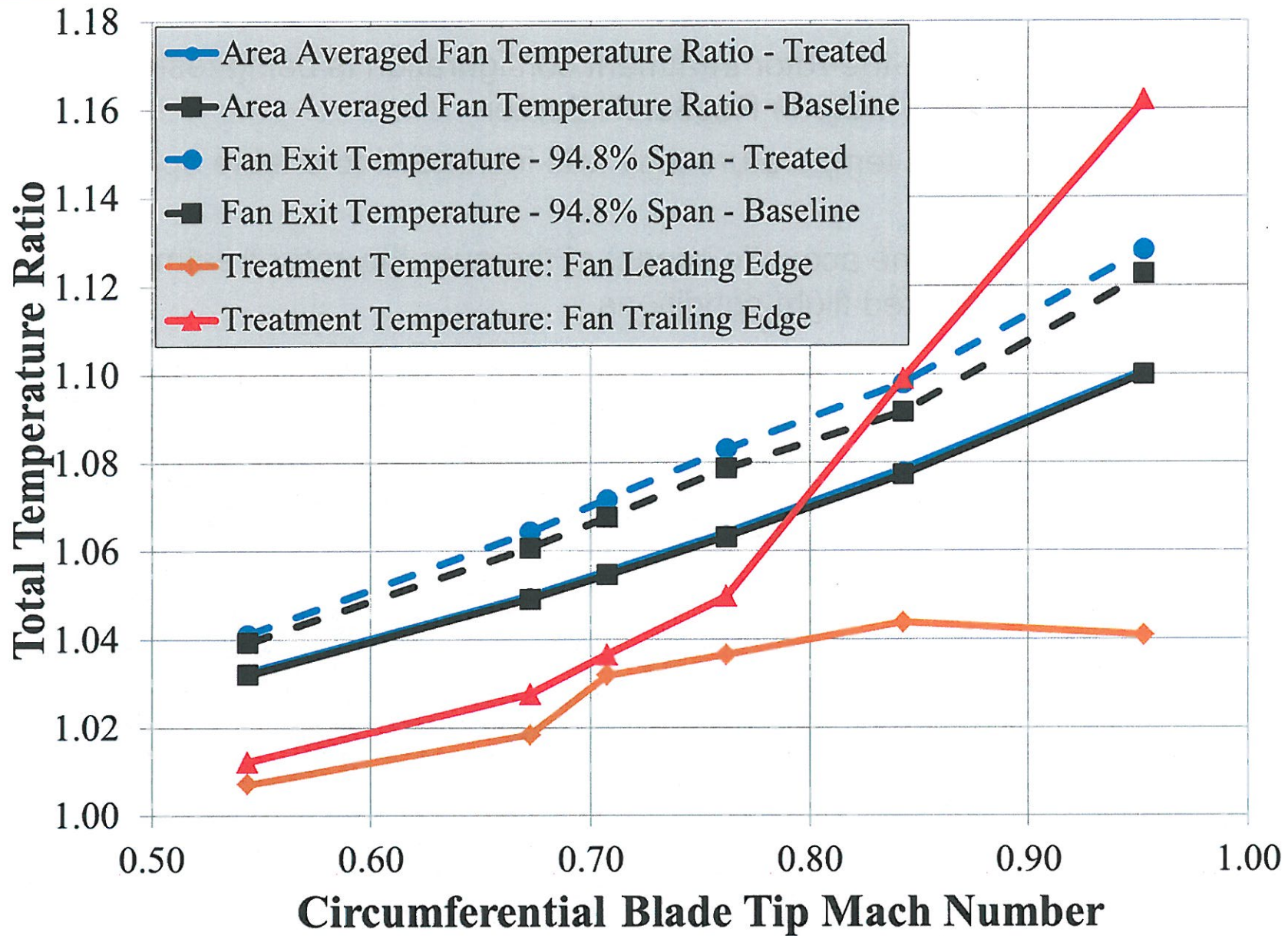
# Fan Adiabatic Efficiency (Nominal Operating Line)



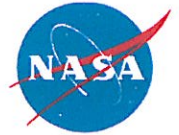




# Acoustic Treatment Temperatures



# 9x15 Wind Tunnel Test

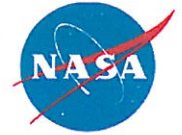


- Currently, the same over-the-rotor treatment configuration is being tested in the 9x15 wind tunnel at NASA Glenn Research Center
- The acoustic treatment's temperature limit was increased to enable operation at higher fan speeds.
- The efficiency loss and the acoustic impact of the over-the-rotor treatment will be determined at simulated flight conditions.



# Summary

---



- An over-the-rotor acoustic treatment concept was designed and tested in the W-8 Single Stage Axial Compressor Facility.
- No significant change in pressure ratio was seen, but an increase in temperature near the blade tips was seen.
- The performance loss due to the over-the-rotor treatment, in terms of fan adiabatic efficiency, varied from 0.75% to 2% over the range of conditions tested.
- When the fan tip speed approached sonic conditions, the acoustic treatment temperature increased dramatically.
- The efficiency loss and the acoustic impact of the over-the-rotor treatment will be determined at simulated flight conditions in the 9x15 wind tunnel.