Progress on Green's Function Calculations for Non-Axisymmetric Jets

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Presentation Outline

- I. Motivation
- II. Acoustic Analogy Approach
 - i. Problem for Green's function
- III. Previous Work
- IV. Status of Green's function solver
- V. Ongoing and Future Work

Jet Noise Prediction Needs

Next generation aircraft will involve complex exhaust system geometries

Non-circular exits



Multiple Streams



Nearby Solid Surfaces



In order to make noise predictions for Next GEN exhaust systems, need physics-based prediction methods that can handle:

- •Non-axisymmetric mean flows
- Interactions with solid surfaces

Acoustic Analogy Approach

 Current work based on Goldstein (2003) formulation.

Formula for the Acoustic Spectrum

$$I_{\omega}(\mathbf{x}) = 2\pi \int_{V} \int_{-\infty}^{\infty} \int_{V} \Gamma_{\lambda j}(\mathbf{x} | \mathbf{y}; \omega) \Gamma_{\kappa l}^{*}(\mathbf{x} | \mathbf{y} + \boldsymbol{\eta}; \omega) e^{-i\omega\tau} \mathcal{R}_{\lambda j \kappa l}(\mathbf{y}, \boldsymbol{\eta}, \tau) d\boldsymbol{\eta} d\tau d\mathbf{y}$$

Propagator Function (Green's Function) $\Rightarrow \Gamma_{\lambda i}$ -- Computed

$$\Gamma_{\lambda j}(\mathbf{x} | \mathbf{y}; \mathbf{\omega}) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{i\omega(t-\tau)} \left[\frac{\partial g_{\lambda 4}^{a}(\mathbf{y}, \tau | \mathbf{x}, t)}{\partial y_{j}} - (\gamma - 1) \frac{\partial \tilde{v}_{\lambda}}{\partial y_{j}} g_{44}^{a}(\mathbf{y}, \tau | \mathbf{x}, t) \right] d(t-\tau)$$

Source Terms $\Rightarrow \mathcal{R}_{\lambda j \kappa l} = \mathcal{E}_{\lambda j, \sigma m} R_{\sigma m \gamma n} \mathcal{E}_{\kappa l, \gamma n}$; $\mathcal{E}_{\lambda j, \sigma m} \equiv \delta_{\lambda \sigma} \delta_{jm} - \frac{\gamma - 1}{2} \delta_{\lambda j} \delta_{\sigma m}$ $R_{\sigma m \gamma n}$ Reynolds Stress Auto-Covariance Tensor -- Modeled

Computation of the Green's function is generally the most time-consuming part of the prediction.

Acoustic Analogy Approach Computation of Green's function

- Reduced-order models.
 - Relatively quick turn-around time for design and concept evaluation.
- Locally parallel mean flow, observer in the far field.

Problem for adjoint scalar Green's function

$$\frac{\partial}{\partial y_{j}} \frac{\widetilde{c^{2}}(\mathbf{y}_{\perp})}{\left[1 - M(\mathbf{y}_{\perp})\cos\theta\right]^{2}} \frac{\partial g(\mathbf{y}_{\perp};\boldsymbol{\varphi},\boldsymbol{\theta}:\boldsymbol{\omega})}{\partial y_{j}} + \omega^{2} \left\{1 - \frac{\left(\widetilde{c^{2}}(\mathbf{y}_{\perp})/c_{\omega}^{2}\right)\cos^{2}\theta}{\left[1 - M(\mathbf{y}_{\perp})\cos\theta\right]^{2}}\right\} g(\mathbf{y}_{\perp};\boldsymbol{\varphi},\boldsymbol{\theta}:\boldsymbol{\omega}) = 0 \quad j=2,3$$

$$g(\mathbf{y}_{\perp};\boldsymbol{\varphi},\boldsymbol{\theta}:\boldsymbol{\omega}) \rightarrow \frac{\left(\boldsymbol{\omega}/c_{\infty}\right)^{2} e^{-i\boldsymbol{\omega}/c_{\infty}\sin\boldsymbol{\theta}\mathbf{y}_{\perp}\cos\left(\boldsymbol{\varphi}-\boldsymbol{\varphi}_{0}\right)} e^{i\pi/4}}{2\left(2\pi\right)^{2}\sqrt{2\pi\sin\boldsymbol{\theta}\boldsymbol{\omega}/c_{\infty}}} + \text{outgoing waves}$$

as $y_{\perp} \rightarrow \infty$

Previous Work

- Noise predictions for rectangular jets¹.
 - Conformal mapping to elliptical coordinates for Green's function.
 - Hybrid (space-time/frequency wavenumber) source model².
 - Comparisons with acoustic data (Extensible Rectangular Nozzles) for cold subsonic jets over a range of aspect ratios, jet exit Mach numbers.
- Other applications for conformal mapping method³.
- Not all nozzle geometries amenable to conformal mapping method.
 - Need more general method.
- 1. Leib, S.J., 2013 Noise Predictions for Rectangular Jets Using a Conformal Mapping Method, *AIAA Journal*, Vol. 51 No. 3, pp. 721-737.
- 2. Leib, S.J. & Goldstein, M.E. 2011 A Hybrid Source Model for Predicting High-Speed Jet Noise, *AIAA Journal*, Vol. 49 No. 7, pp. 1324-1335.
- 3. Leib, S.J., Green's Functions for Prediction of Noise From Non-Axisymmetric Jets, Acoustics Technical Working Group, April 2012.

Green's Function: Reduced-Order Models Expansion in Orthogonal Functions

- Represent mean flow quantities in the governing equation for the adjoint Green's function by sum of orthogonal functions in an appropriate coordinate system.
 - For computational efficiency, a relatively small number of functions is desired.
- Expand Green's function in series of these orthogonal functions
- Solve system of coupled ordinary differential equations for Green's function modes:
 - Iterative solution (Mani).
 - Direct solution of banded system.

Green's Function: Reduced-Order Models Governing Equation

$$\frac{\partial^2 g}{\partial r^2} + \frac{1}{r} \frac{\partial g}{\partial r} + \frac{1}{r^2} \frac{\partial^2 g}{\partial \phi^2} + \mathcal{R} \frac{\partial g}{\partial r} + \mathcal{P} \frac{\partial g}{r \partial \phi} + \omega^2 \mathcal{P} g = 0$$

Mean flow dependent coefficients

$$\mathcal{R} = \left\{ \frac{2\cos\theta}{\left[1 - M\left(\mathbf{y}_{\perp}\right)\cos\theta\right]} \frac{\partial M}{\partial r} + \frac{1}{c^{2}}\left(\mathbf{y}_{\perp}\right)}{\frac{\partial c^{2}}{\partial r}} \right\} \quad \mathcal{R} = \left\{ \frac{\left[1 - M\left(\mathbf{y}_{\perp}\right)\cos\theta\right]^{2}}{c^{2}} - \frac{\cos^{2}\theta}{c^{2}}\right\} \quad \mathcal{R} = \left\{ \frac{2\cos\theta}{\left[1 - M\left(\mathbf{y}_{\perp}\right)\cos\theta\right]} \frac{\partial M}{\partial \phi} + \frac{1}{c^{2}}\left(\mathbf{y}_{\perp}\right)}{\frac{\partial c^{2}}{r} \partial \phi} \right\}$$
Fourier series expansion:
$$\mathcal{R}(r,\phi) = \sum_{l=-L}^{L} \mathcal{R}_{l}(r)e^{il\phi} \quad ; \quad \mathcal{R}(r,\phi) = \sum_{l=-L}^{L} \mathcal{R}_{l}(r)e^{il\phi} \quad ; \quad \mathcal{R}(r,\phi) = \sum_{l=-L}^{L} \mathcal{R}_{l}(r)e^{il\phi}$$

$$g(r,\phi) = \sum_{l=-L}^{N} g_{n}(r)e^{in\phi}$$

n = -N

Green's Function: Reduced-Order Models Governing Equation

System of ODEs for Fourier components of Green's function:

$$\frac{d^{2}g_{n}}{dr^{2}} + \frac{1}{r}\frac{dg_{n}}{dr} - \frac{n^{2}}{r^{2}}g_{n} + \sum_{l=-L}^{L}R_{l}\frac{\partial g_{n-l}}{\partial r} + \sum_{l=-L}^{L}F_{l}\frac{i}{r}(n-l)g_{n-l} + \omega^{2}\sum_{l=-L}^{L}H_{l}g_{n-l} = 0 \quad ; \quad -N \le n \le N$$

Boundary conditions:

(I) Far-Field:

$$\frac{dg_n}{dr} + \kappa_n g_n \to \left(\frac{d}{dr} + \kappa_n\right) \frac{\left(\omega / c_{\infty}\right)^2 e^{i\pi/4}}{4\left(2\pi\right)^2 \sqrt{2\pi \sin\theta\omega / c_{\infty}}} e^{-in(\varphi + \pi/2)} H_n^{(2)}\left(\frac{\omega}{c_{\infty}} r \sin\theta\right) \quad \text{as } r \to \infty$$

(II) Centerline:

$$g_n(0;\varphi,\theta:\omega) = 0, n \neq 0$$
$$\frac{dg_0(0;\varphi,\theta:\omega)}{dr} = 0$$

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Green's Function: Reduced-Order Models Numerical Methods

- Replace radial derivatives with second-order central differences.
- Form a system of algebraic equations for the Fourier modes of the Green's function at discrete grid points is formed.

$$B_{j}g^{j-1} + A_{j}g^{j} + C_{j}g^{j+1} = 0$$
; $j = 1, J$

Solution Vector:

$$\boldsymbol{g}^{j} = \left\{ \begin{array}{cccc} g_{-N}^{j} & g_{-N+1}^{j} & \cdots & g_{0}^{j} & \cdots & g_{N-1}^{j} & g_{N}^{j} \end{array} \right\}^{T}$$

- Solve (banded system) directly using a sparse system algorithm

 Compute Fourier modes of coefficients and sum series for the Green's function using FFTW.

Validation and Test Cases

- Reproduce round jet results. ~
- Consider two non-circular test cases:



Test Case : Offset Stream Fourier Representation of Coefficients



Test Case : Fluid Shield Fourier Representation of Coefficients



Tests of Green's Function Solver

• Numerical parameters:

 $N = 16, \quad \Delta = 0.005, \quad y_T^{\text{max}} = 5.0$

- Green's function results to be presented:
 - Effect of number of mean flow modes. L = 4,6,8

- High-frequency behavior:

 $\omega^{-3/2}|g|$ independent of frequency as $\omega \to \infty$

$\theta = 30 \ ; \ \varphi = 0$ Test Case : Offset Stream Green's Function Results



$\theta = 30$; $\varphi = 0$ Green's Function Results

St =0.2,<mark>0.4</mark>,0.6 ,0.8,1.0

Long-Dash L = 4, Short-Dash L = 6, Solid L = 8



Test Case : Offset Stream Green's Function Results



$\theta = 30$; $\varphi = \frac{3\pi}{2}$ Test Case : Fluid Shield Green's Function Results

-0.007

0.006

0.004

Real (g)

-0.002

-0.004

0.002 -

0.001

0.001 (ئ السوط (ئ سات

-0.003

-0.004

-0.005

3

φ

0

Long-Dash L = 4, Short-Dash L = 6, Solid L = 8St =0.2,0.4,0.6 ,0.8,1.0 $r_0 = 0.5$ $r_0 = 0.25$ $r_0 = 1.0$ 0.006 0.01 0.004 0.005 0.002 Real (g) Real (g) 0 -0.002 -0.005 -0.004 -0.006 -0.01 φ φ φ $r_0 = 0.5$ $r_0 = 1.0$ $r_0 = 0.25$ 0.003 r 0.005 0.002 0.001 0 <u>ق</u>-0.001 (b) b=0.005 **b**i-0.002 **b**i-0.003 -0.004 -0.01 -0.005 -0.006

φ

-0.015

3

φ

Test Case : Fluid Shield Green's Function Results



Noise Shielding by Non-Axisymmetric Mean Flows St = 0.6



Noise Shielding by Non-Axisymmetric Mean Flows $\phi = \frac{\pi}{2}$



Plot $|g(r_0,\phi_0 | \omega,\phi,\theta)|$ vs. $(\phi_0 - \phi)$ for observer locations: $\left(\phi = \frac{\pi}{2}, \theta = 30\right)$ and $\left(\phi = \frac{3\pi}{2}, \theta = 30\right)$ θ = 30 $\phi = \pi/2$ $\phi = 3\pi/2$ r 0 = 0.5 St = 0.6φ**₀ -** φ $\frac{1}{6}\pi$ 0.005 0.01 0.015 |g tilde| $\frac{11}{6}\pi$ $\frac{7}{6}\pi$ π 21

Ongoing and Future Work

- Apply to non-axisymmetric mean flow obtained from RANS solution.
- Integrate with a source model for noise predictions.

- Continued development of a code for numerical solution of Green's function of acoustic analogy equations. (Collaboration with John Goodrich, GRC)
 - Validation of reduced-order models.
 - Study effects of non-parallel mean flow.
 - High-resolution calculations for cases of special interest.

<u>STATUS</u>:

- Exercising 2D LEE solver with non-uniform mean flow.
- Extend to 3D.
- Adapt for acoustic analogy equations.