



Development of Stable Two-Way Shape Memory Behavior in a Polycrystalline NiTi Shape Memory Alloy



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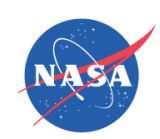
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Acknowledgment

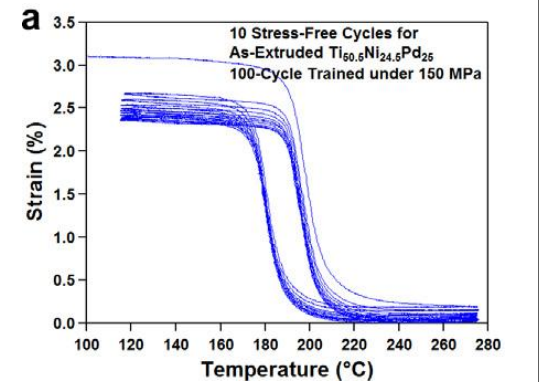
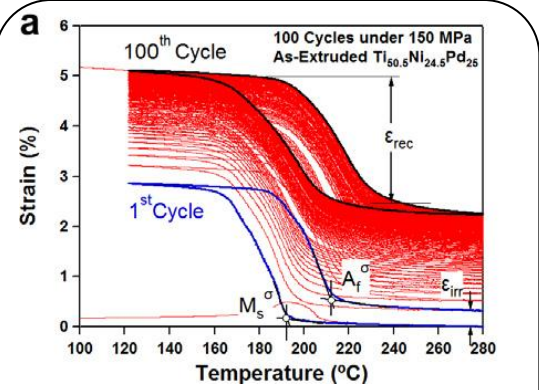
- **NASA Fundamental Aeronautics Program, Supersonics and Fixed-Wing Programs**
- **Basic Energy Sciences (DOE)**
- **CASMART**



Two-Way Shape Memory Effect (TWSME)

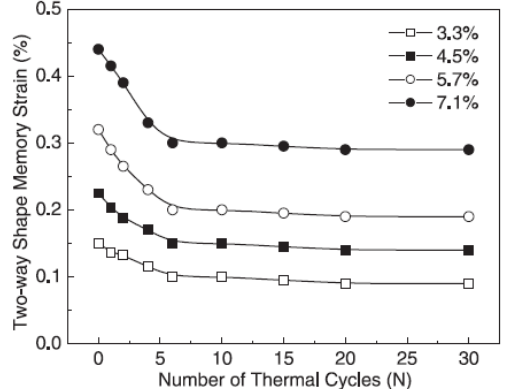
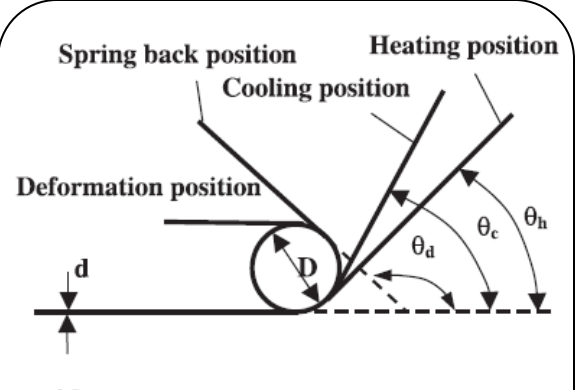
- Two-Way Shape Memory effect (TWSME) is not an inherent behavior of SMAs
- Can be obtained after specific thermomechanical training procedures (many different training methods have been developed)

Thermomechanical cycling



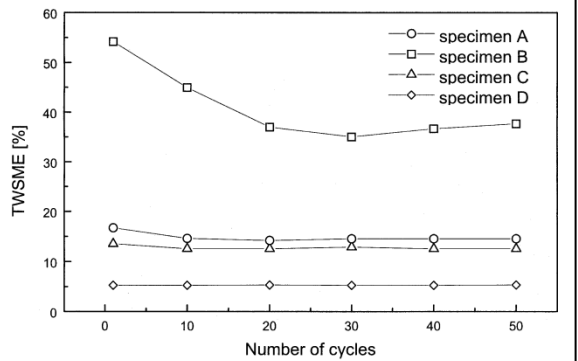
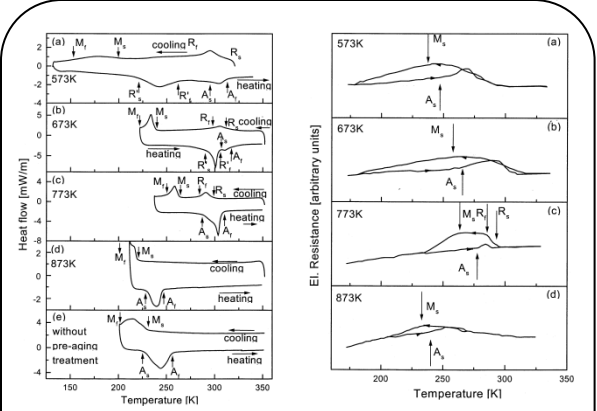
[1] K. C. Atli et al. / Scripta Materialia 65 (2011) 903–906

Martensite deformation



[2] X.L. Meng et al. / Materials Letters 57 (2003) 4206–4211

Precipitation/aging



[3] C.-Y. Chang et al. / Metall. Mater. Trans. A 32 (2001) 1629



Motivation and Objectives

Motivation:

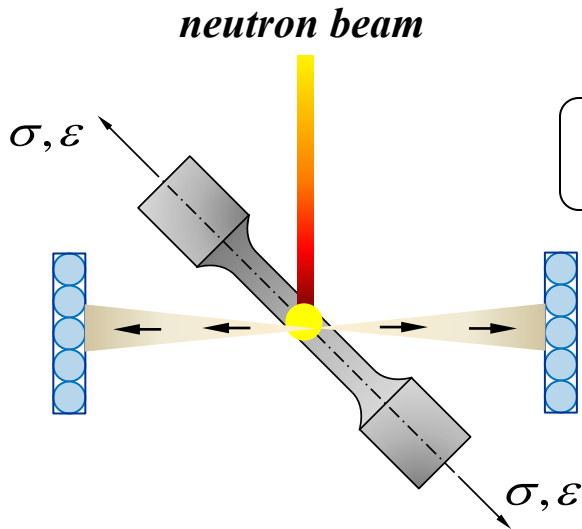
- Training by martensite deformation is relatively easy and quick [4] Y. Liu et al./Acta Mater. 47, (1998)
- Requires little more than a onetime deformation of the material
- Multiple thermomechanical cycles are **NOT REQUIRED**

Objectives:

- Investigate the role of deformation on the stability and efficacy of the TWSME
- Examine the micromechanical and microstructural changes associated with the training procedure (neutron diffraction)
- Optimize training for a specific TWSME actuator application
- Use the same training method to obtain different properties
- Can we apply this to the load-biased actuators??

Neutron Diffraction at LANL

(i) Experiment



(ii) Model

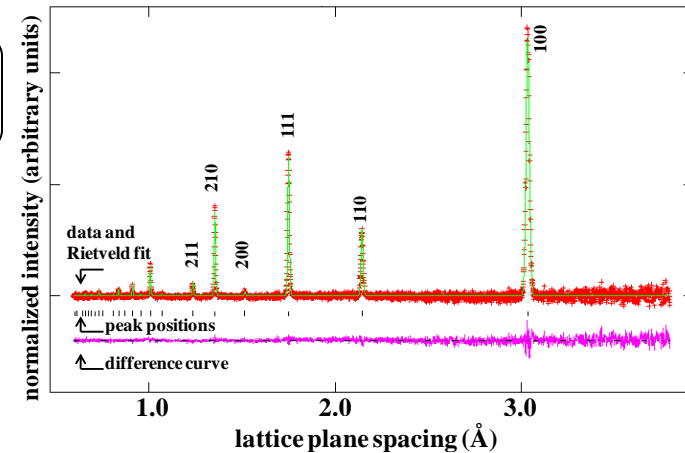
Rietveld refinement

multi parameter curve fitting

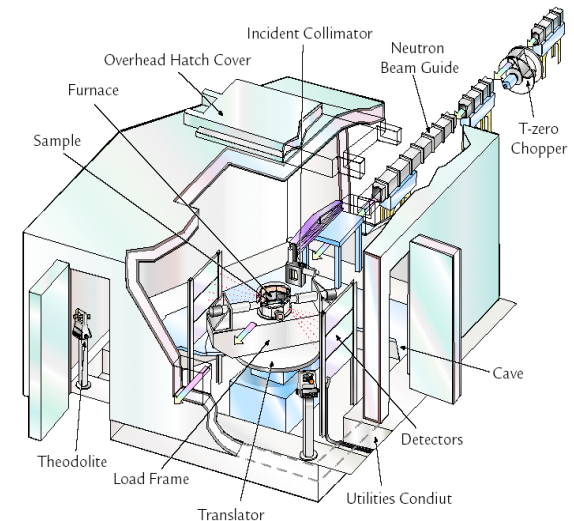
$$Y_{ci} = Y_{bi} + s \sum_k L_k |F_k|^2 \phi(2\theta_i - 2\theta_k) P_k A$$

- Y_{bi} : background intensity
- s : scale factor
- L_k : Lorentz factor a
- F_k : structure factor
- f : reflection profile function
- $2\theta_i$: observed Bragg peak position
- $2\theta_k$: corrected calculated Bragg peak position
- P_k : preferred orientation function
- A : absorption factor

(iii) Result



- Bulk penetration ~1cm
- Ability to follow micromechanical and microstructural changes
- Phase specific, quantitative information during heating/cooling and loading
- **Material: 55NiTi (wt%), d = 5.08 mm**



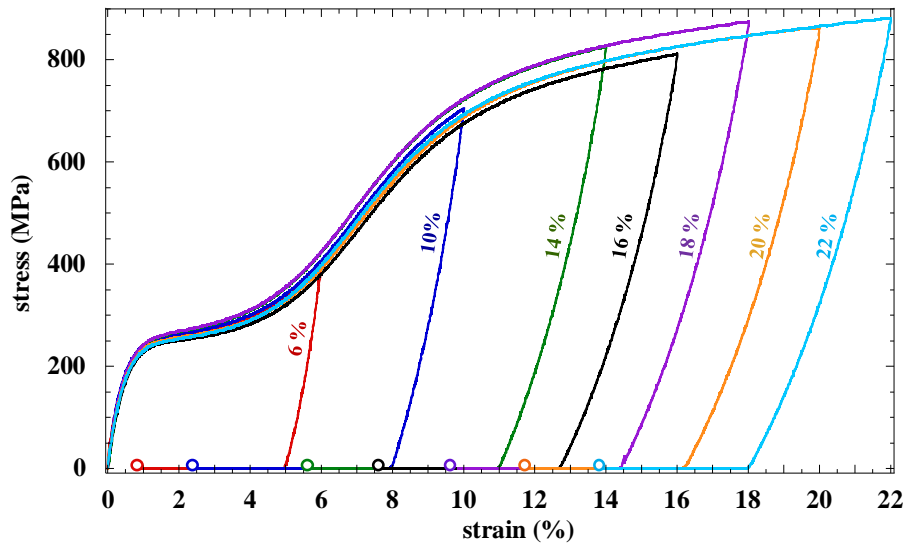
Spectrometer for Materials Research at Temperature and Stress (SMARTS)



Training Procedures

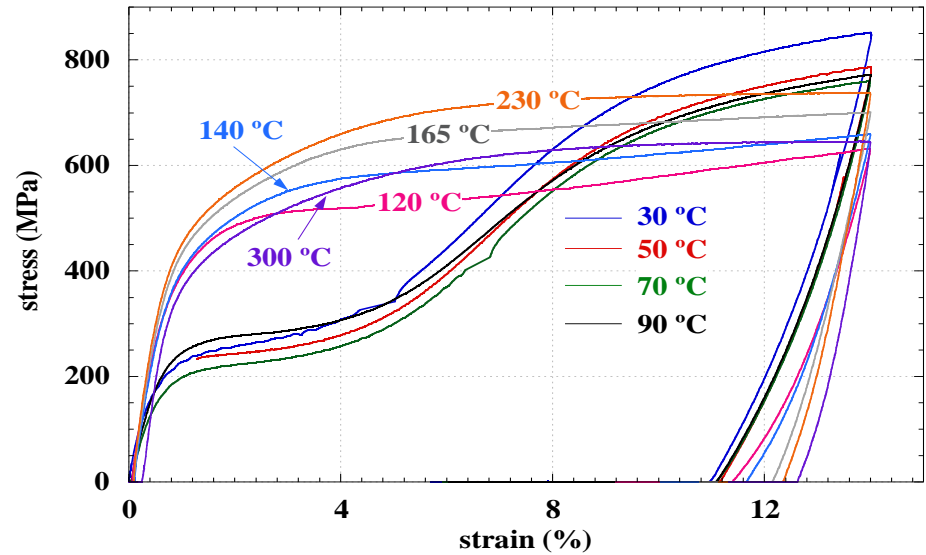
Training I

Constant temperature
Variable strain

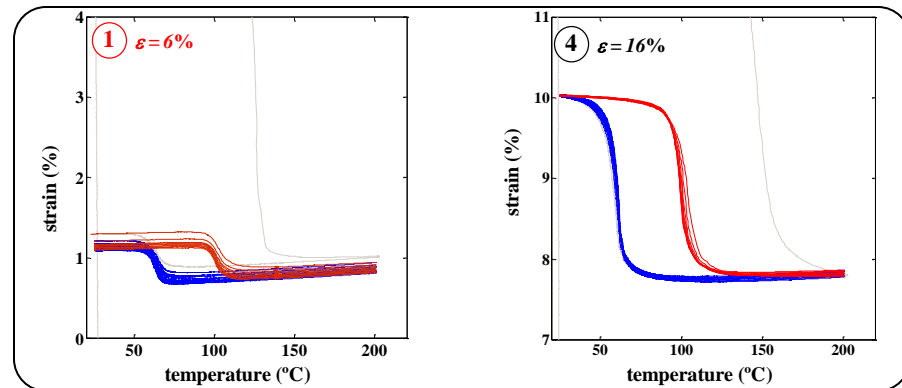


Training II

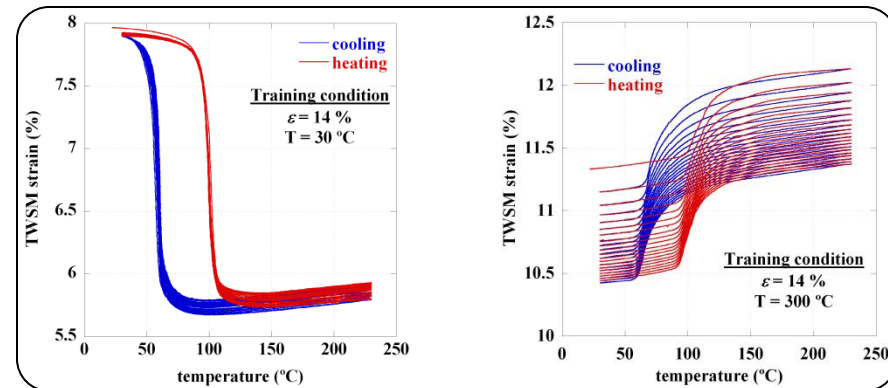
Constant strain
Variable temperature



No-load thermal cycling (TWSME)



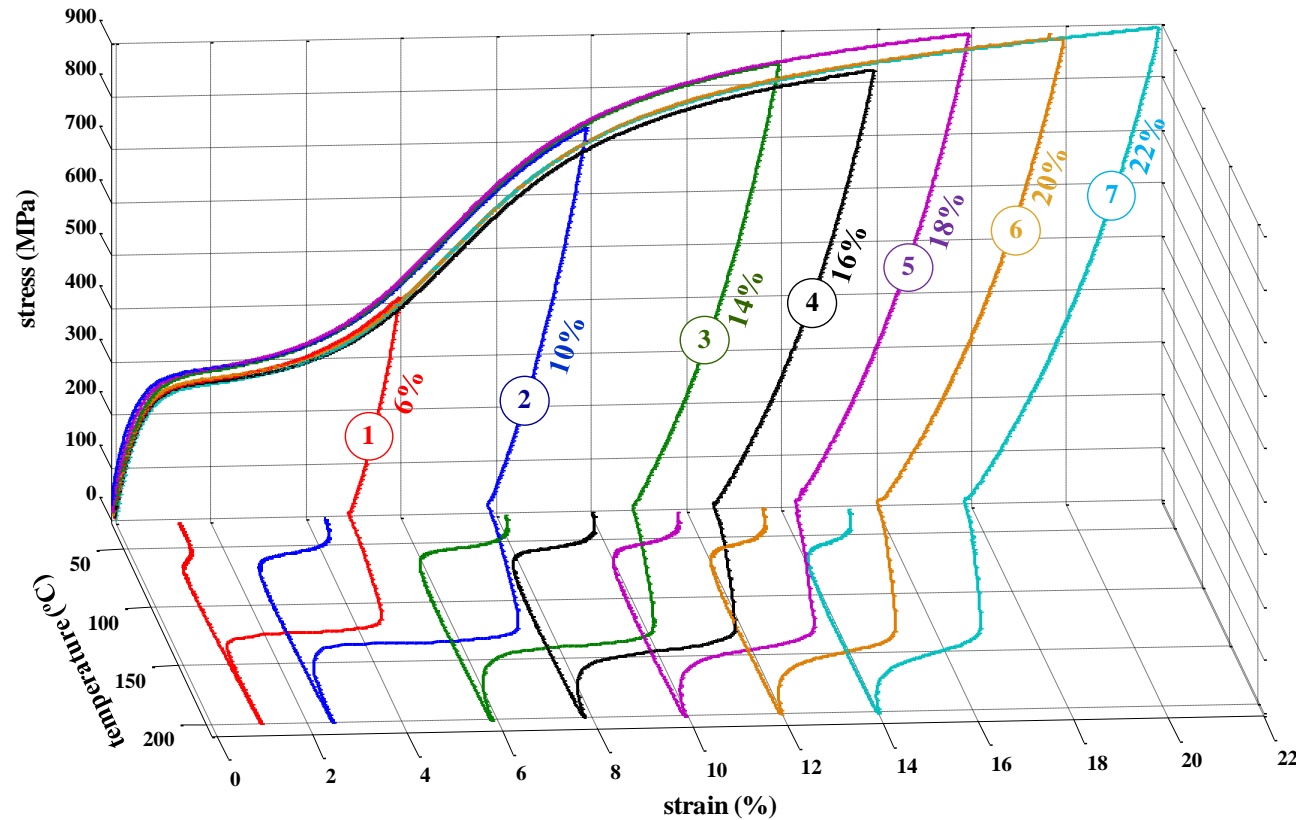
No-load thermal cycling (TWSME)



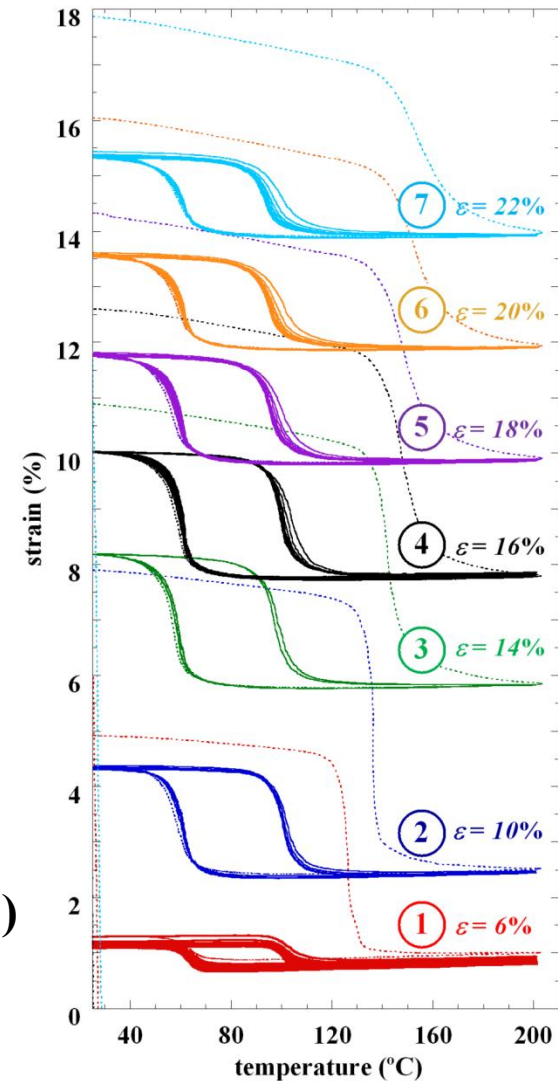


Training I: Constant Temperature/Variable Strain

Isothermal deformation



TWSME

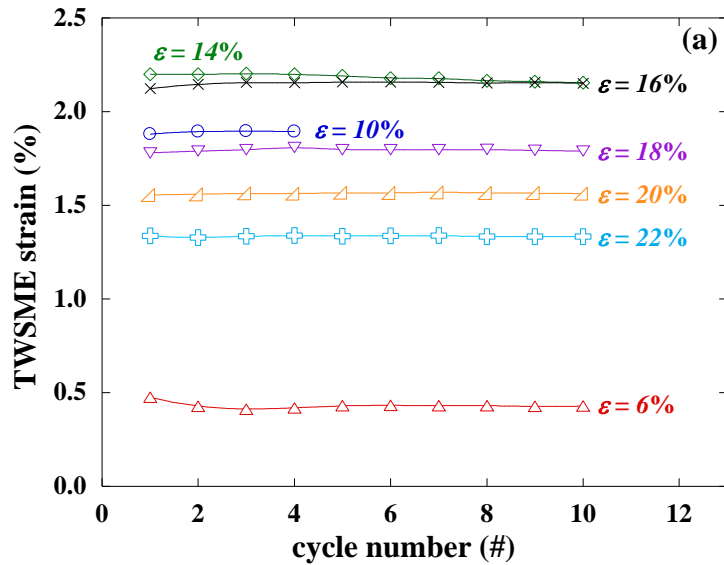


- Room temperature deformation in strain control ($1 \times 10^{-4} \text{ sec}^{-1}$)
- No-load thermal cycling ($30 \leftrightarrow 200 \text{ }^\circ\text{C}$)

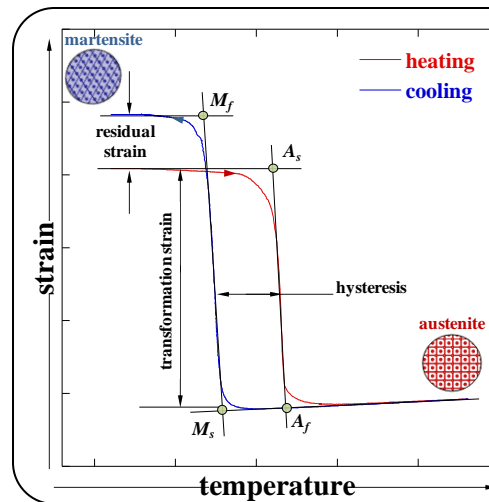
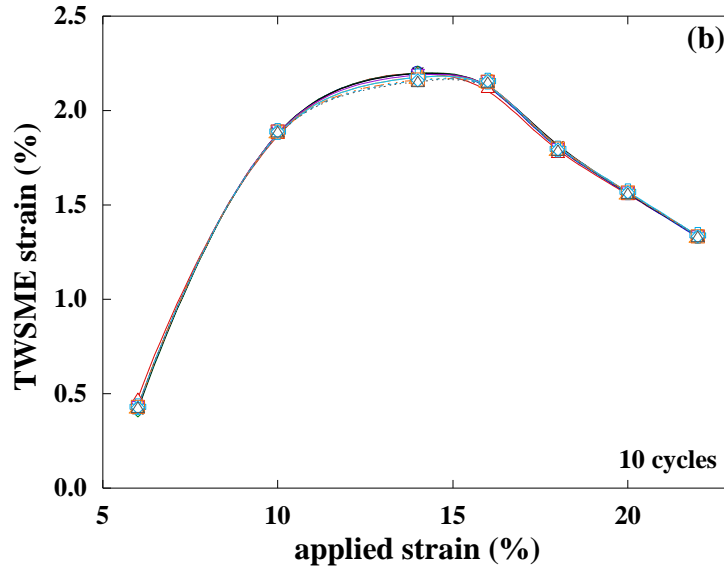
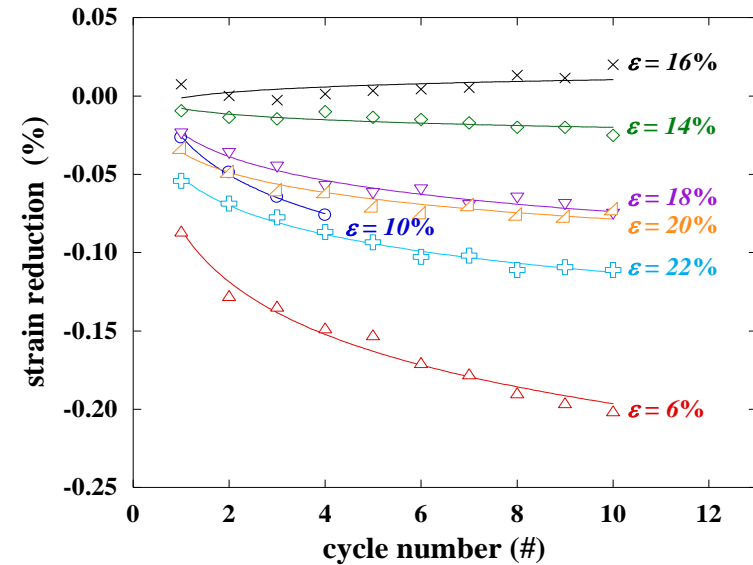


Training I: Constant Temperature/Variable Strain

TWSME magnitude



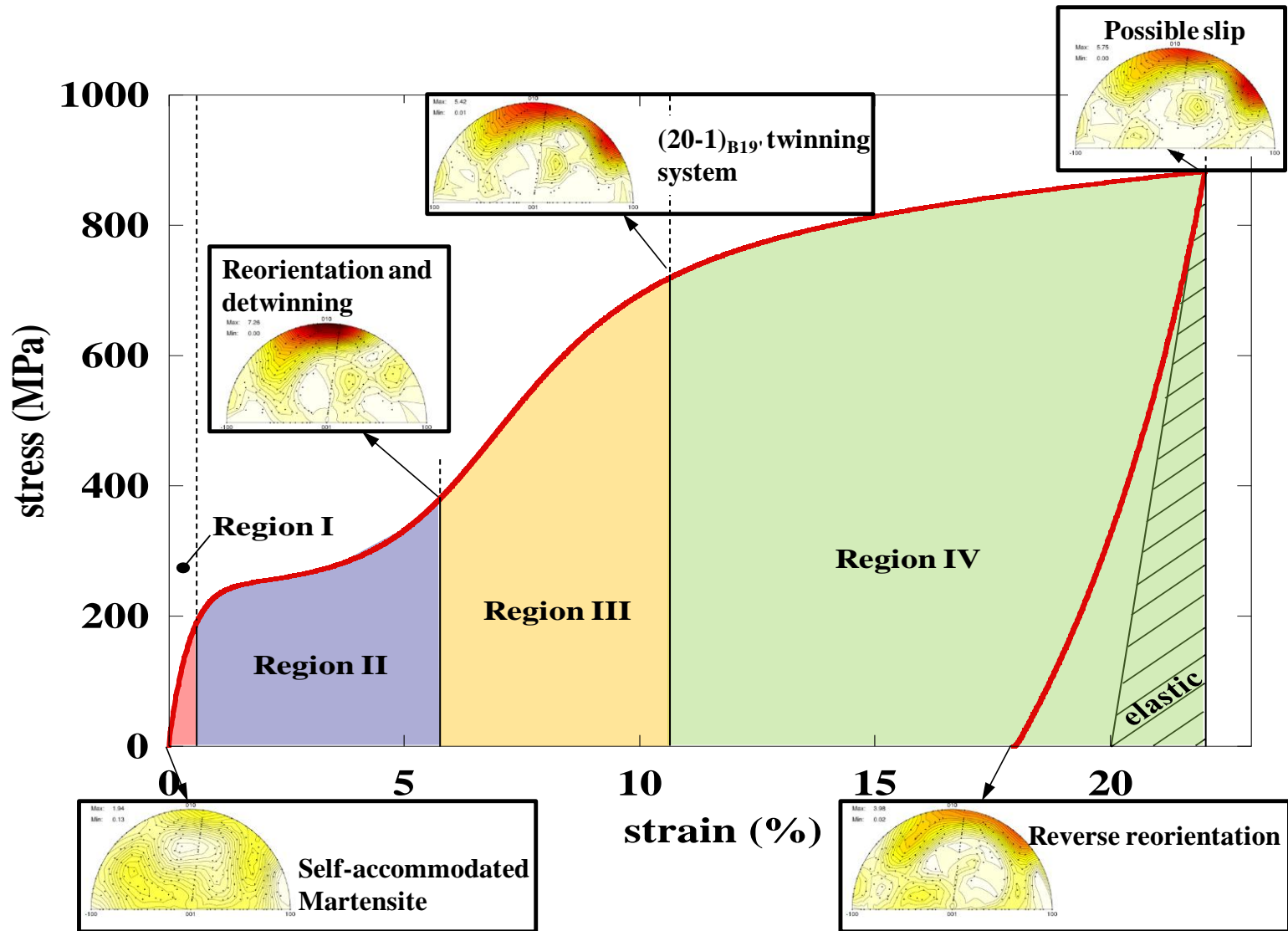
TWSME stability



- Straining to 14 - 16% was found to be optimum for this material
- Stable TWSME strain of 2.2% was obtained with near-zero strain reduction
- Why 14-16%?



Deformation Mechanisms in Martensitic NiTi

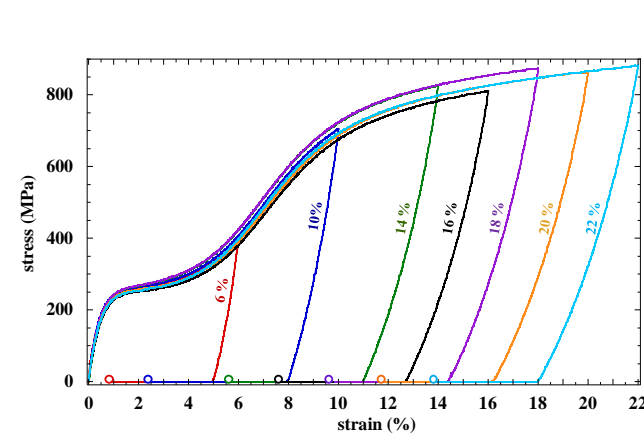
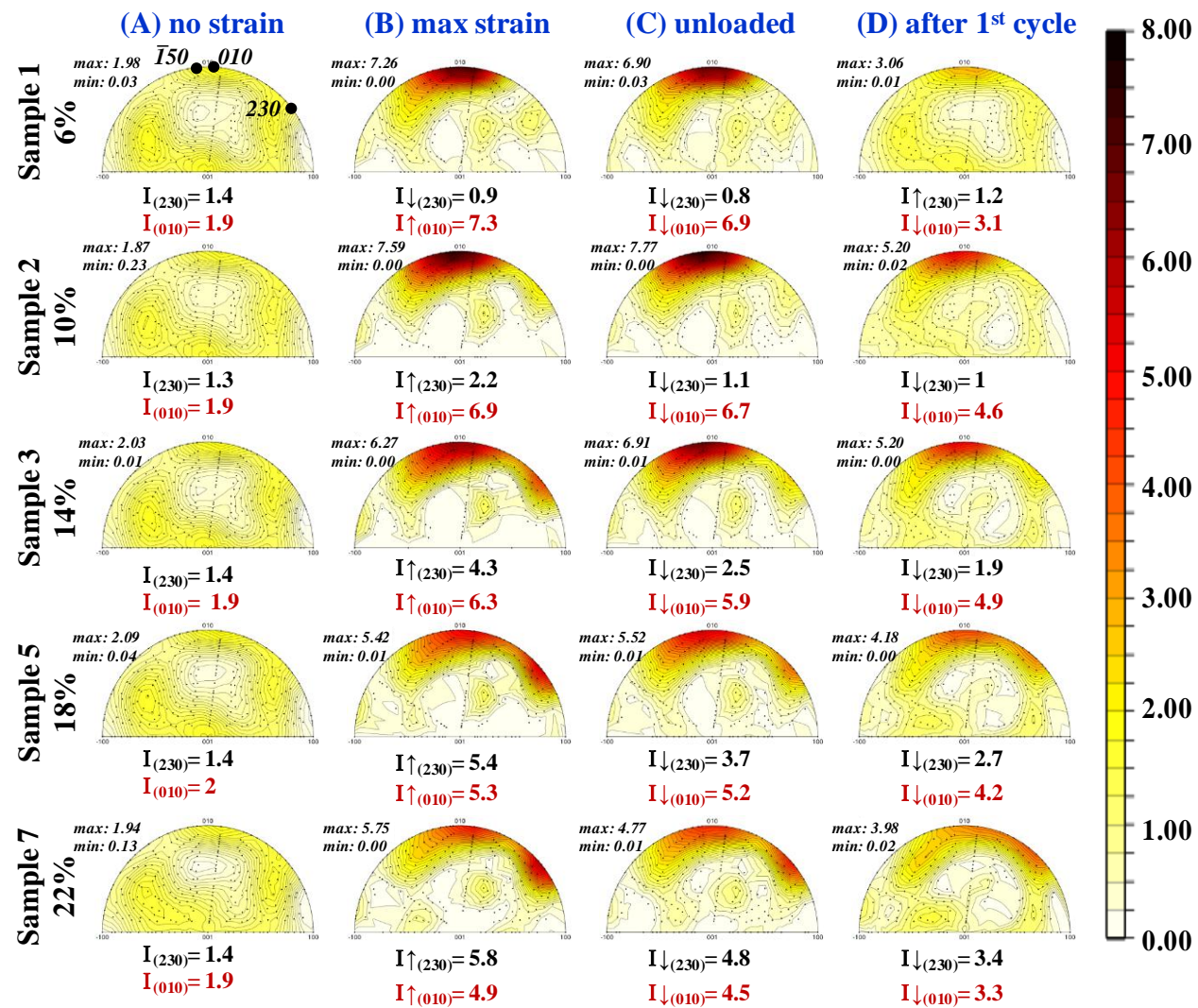




Training I: Constant Temperature/Variable Strain

Microstructure

Macroscopic response

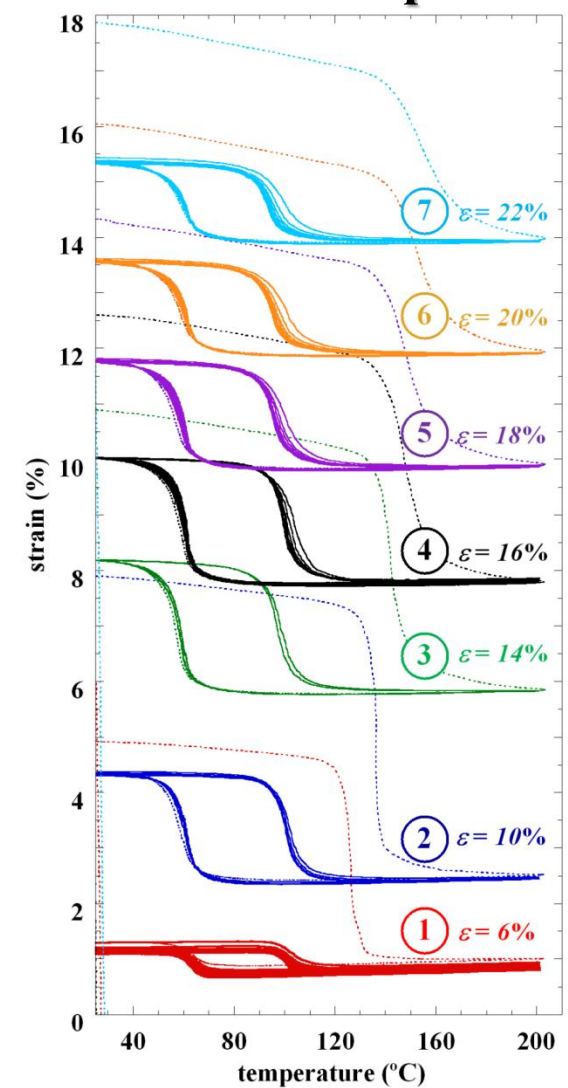
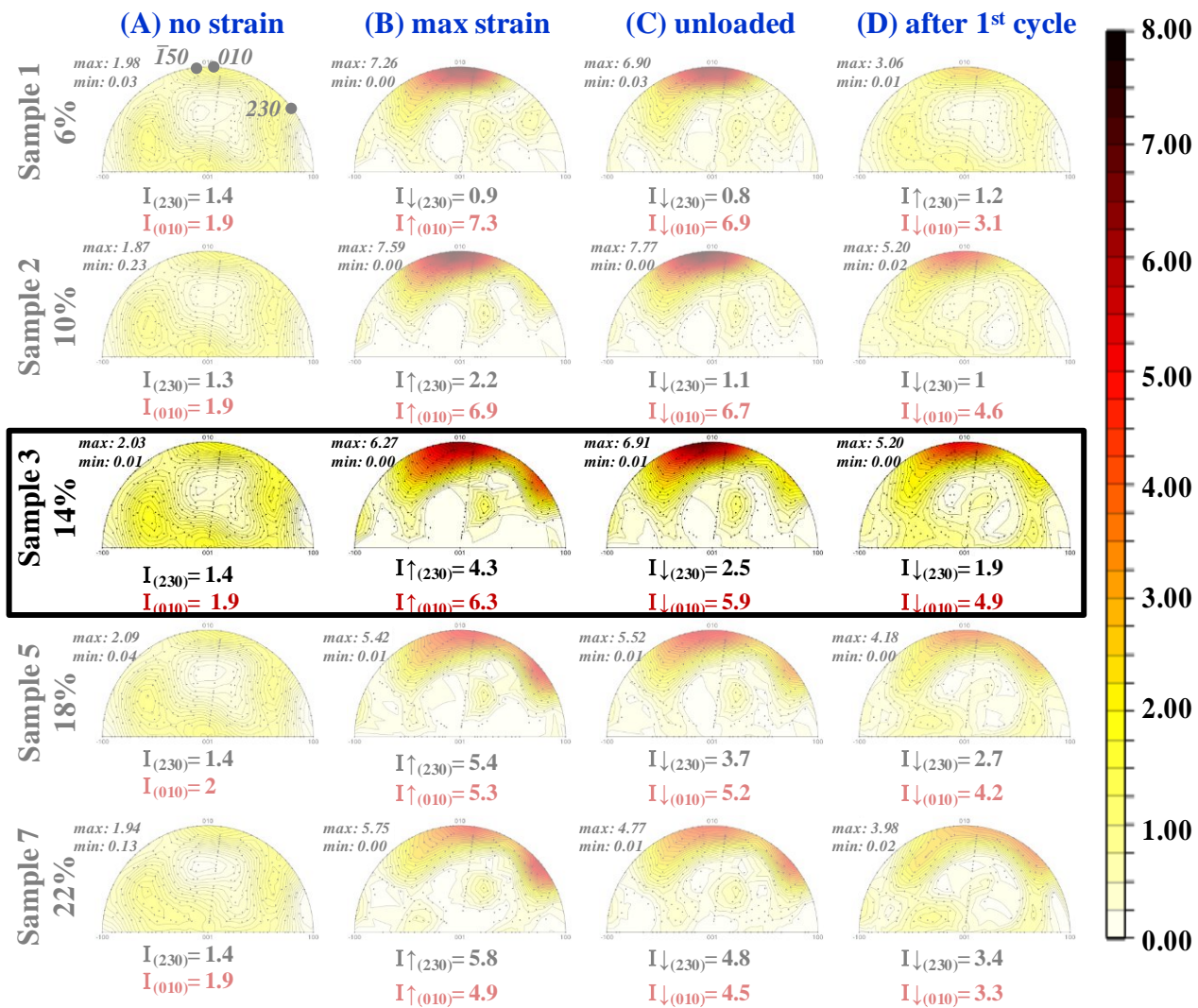




Training I: Constant Temperature/Variable Strain

Microstructure

TWSME Response

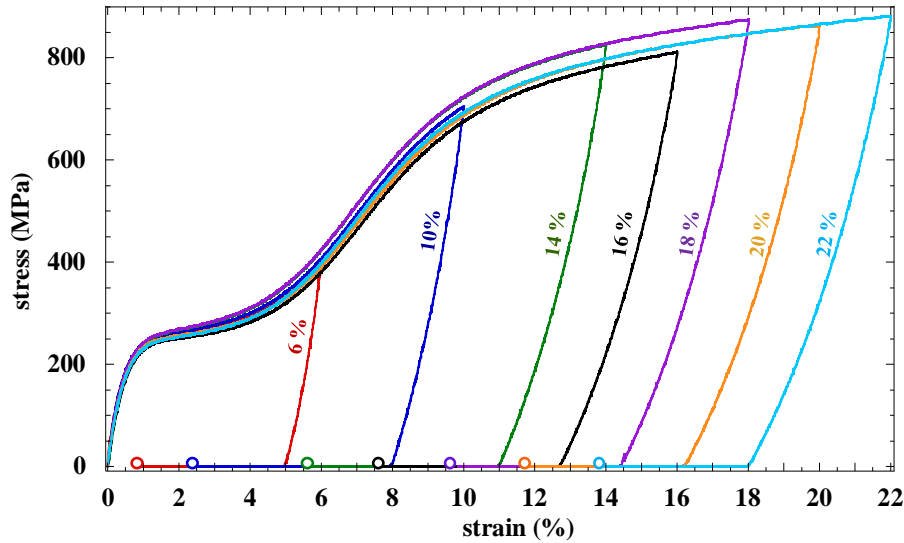




Training Procedures

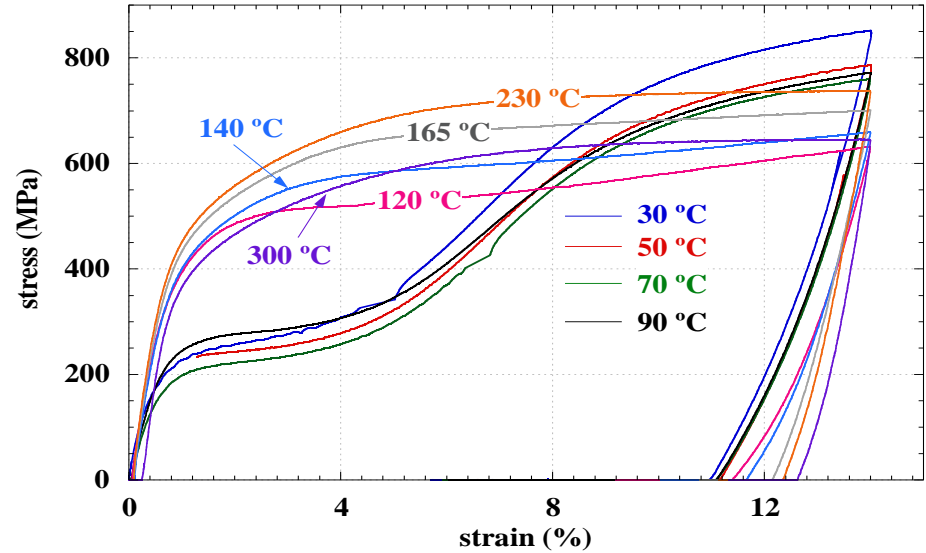
Training I

Constant temperature
Variable strain

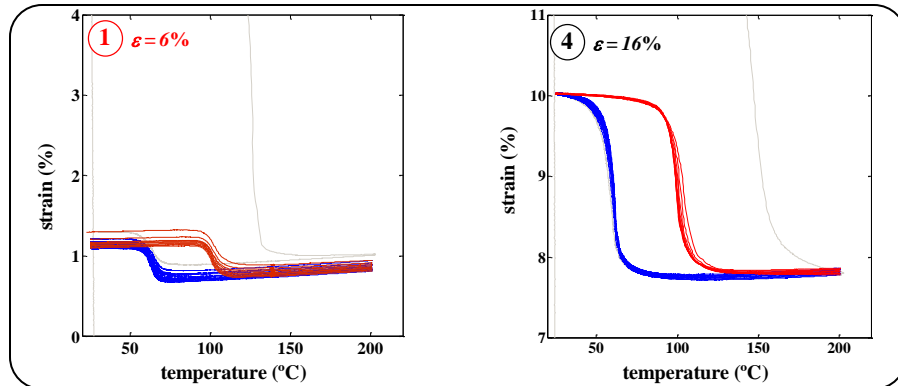


Training II

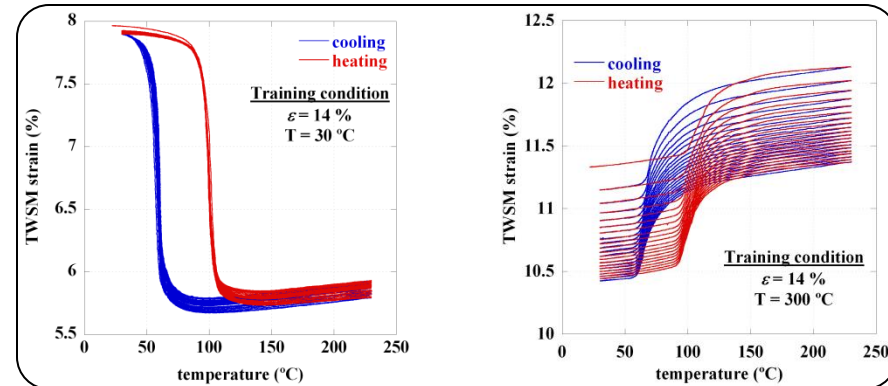
Constant strain
Variable temperature

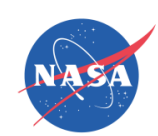


No-load thermal cycling (TWSME)



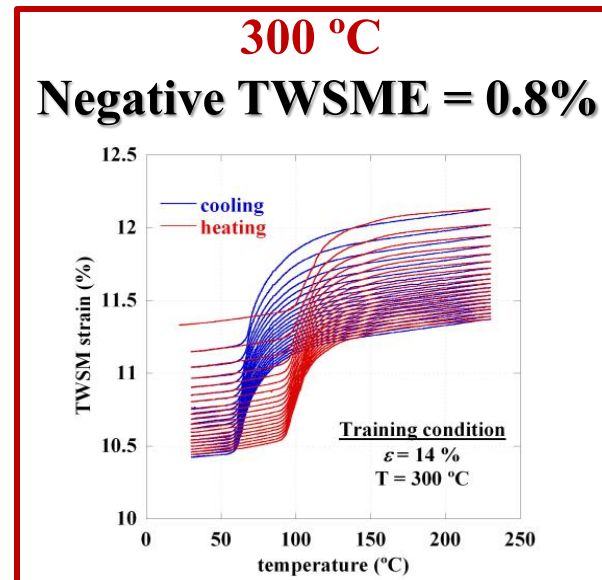
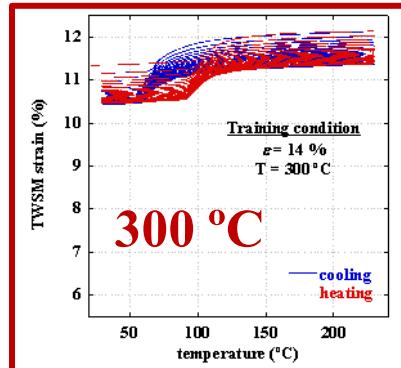
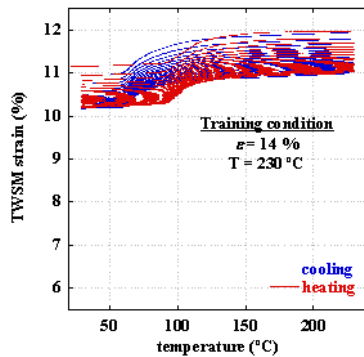
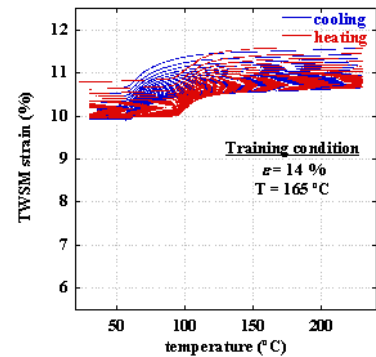
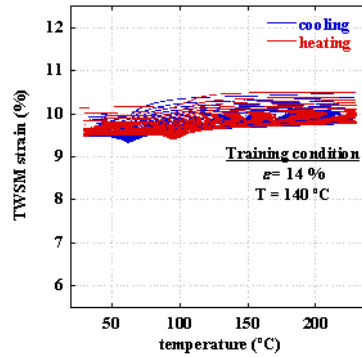
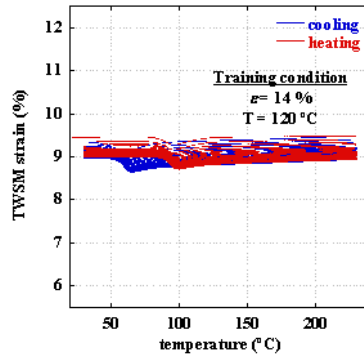
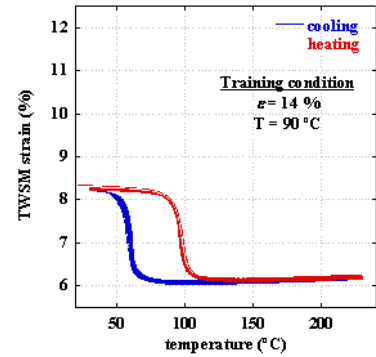
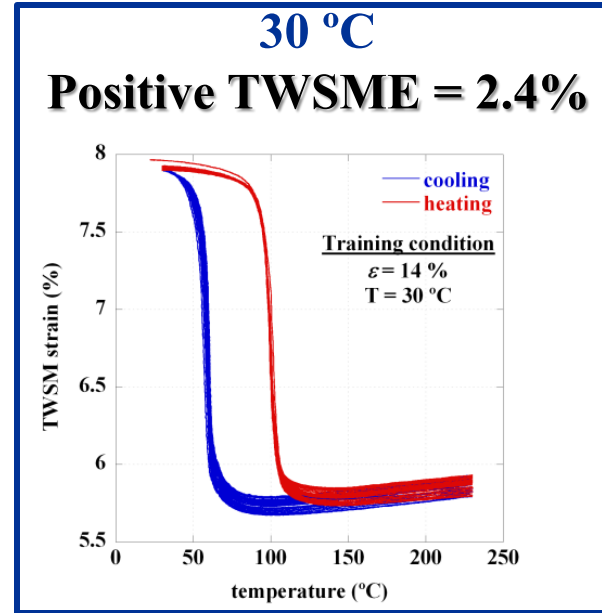
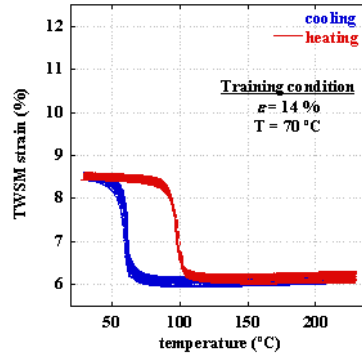
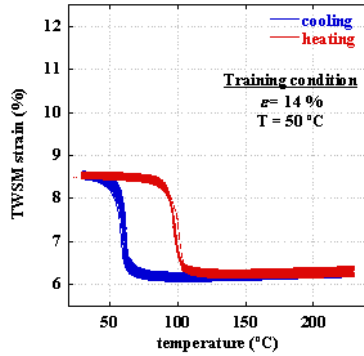
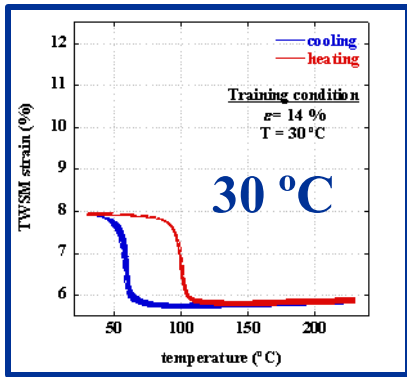
No-load thermal cycling (TWSME)





Training II: Constant Strain/Variable Temperature

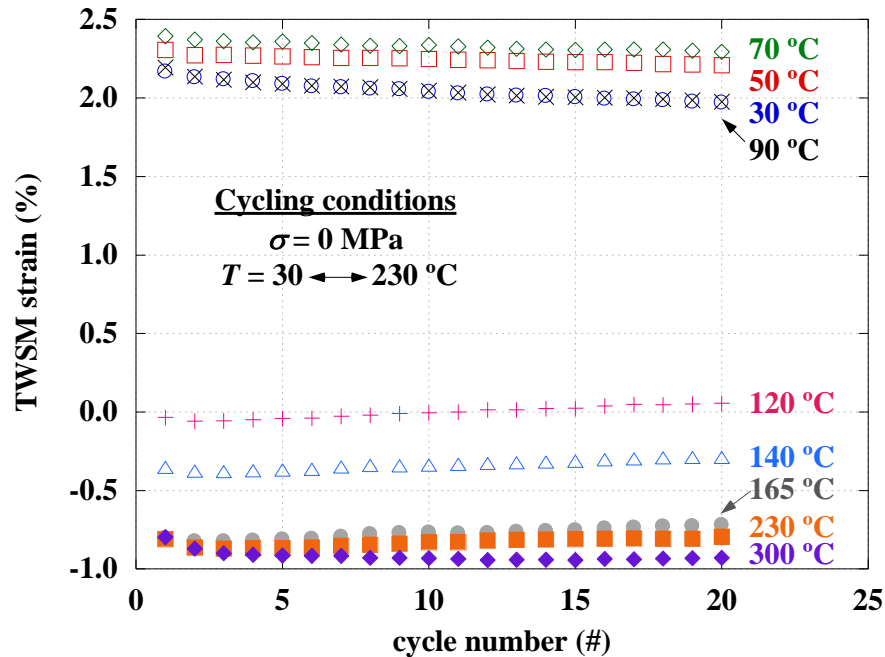
TWSME Response



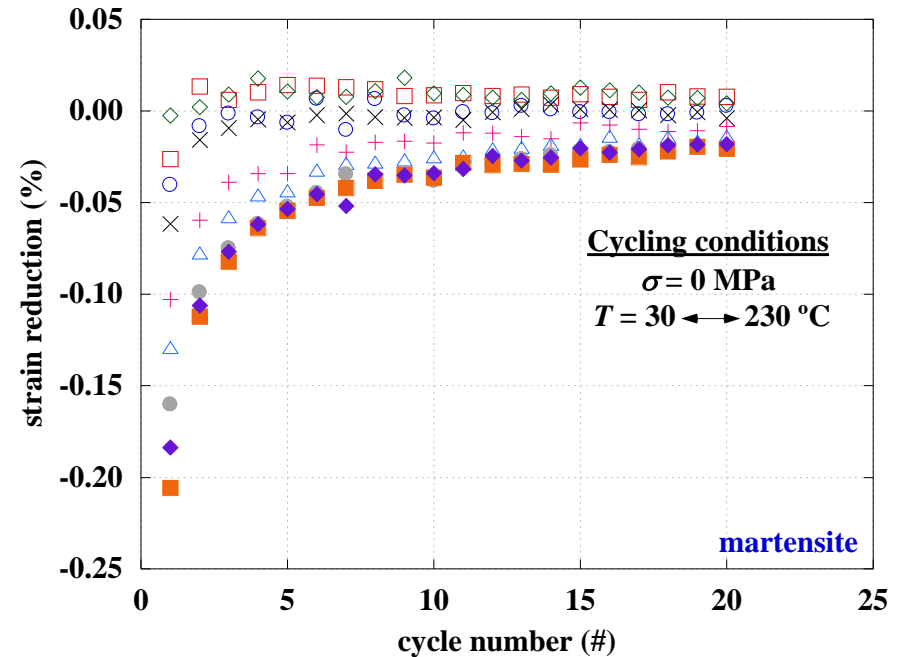


Training II: Constant Strain/Variable Temperature

TWSME magnitude



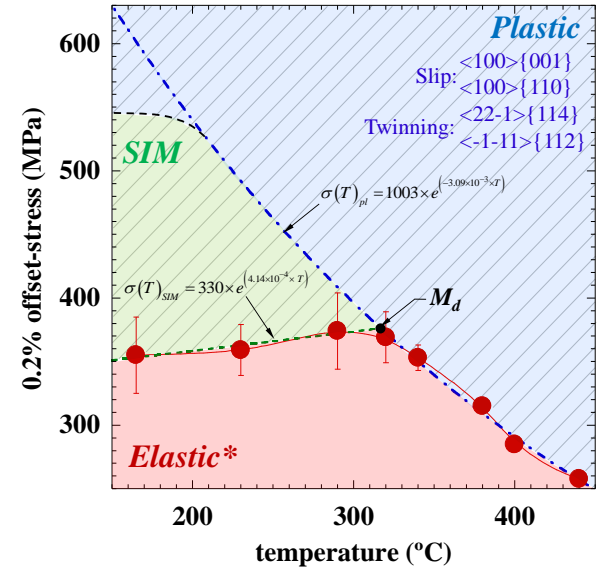
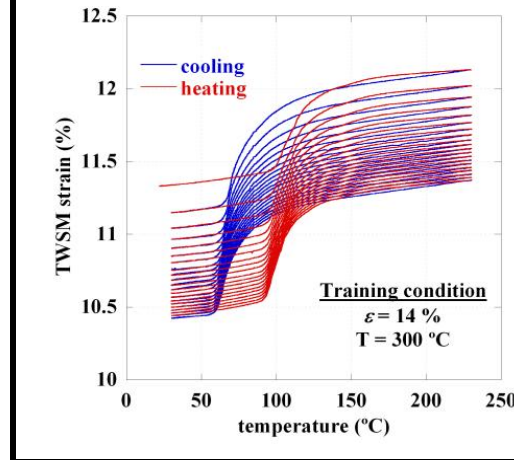
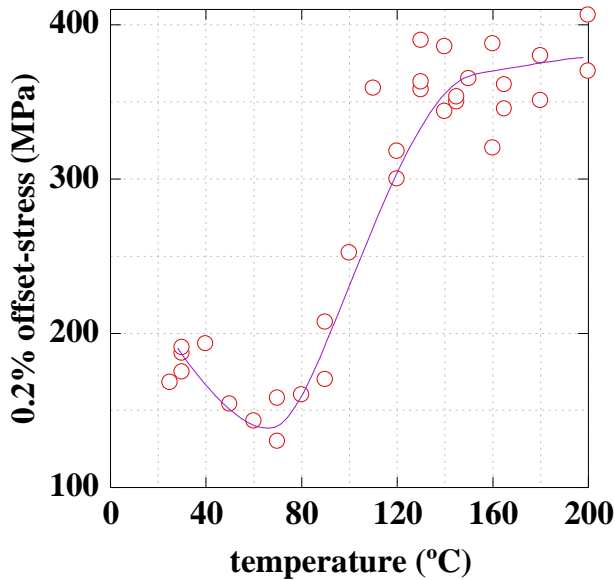
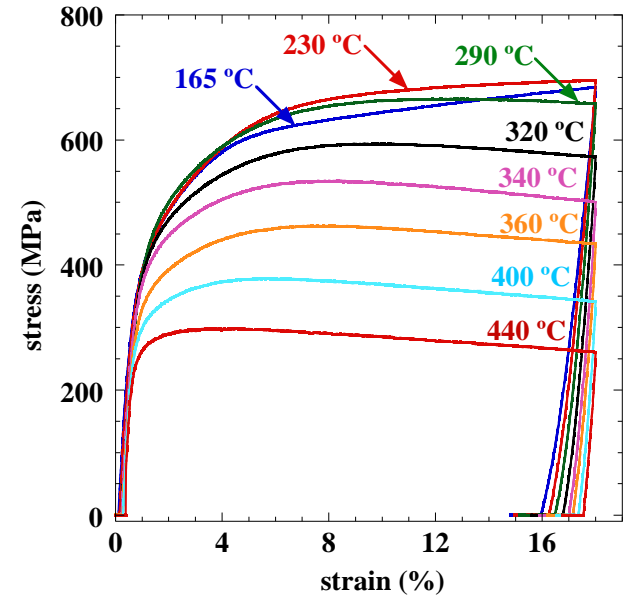
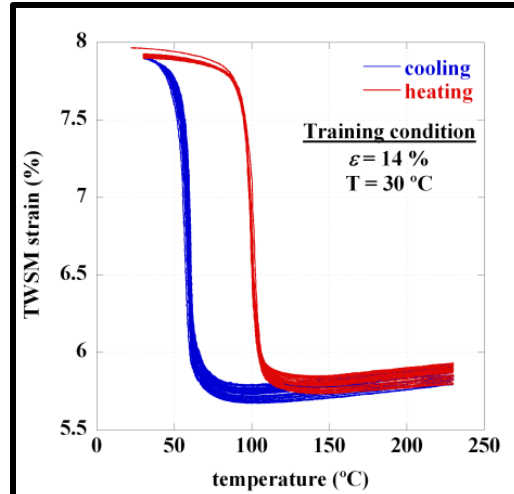
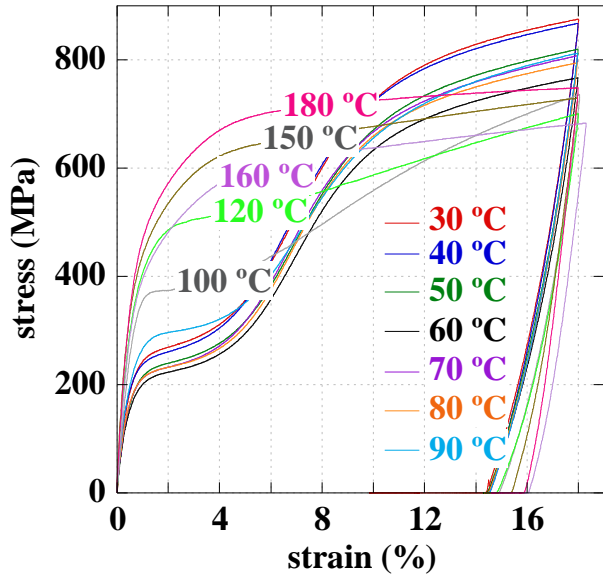
TWSME stability



- **Positive TSWME** → ~2.4%
- **No TWSME** → 0%
- **Negative TWSME** → ~-1%



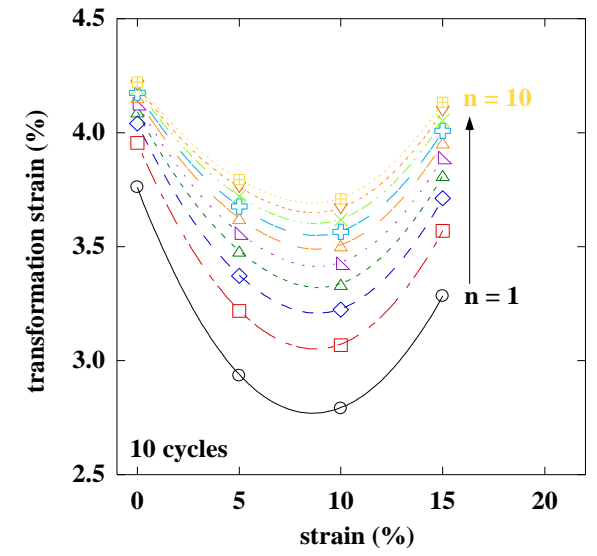
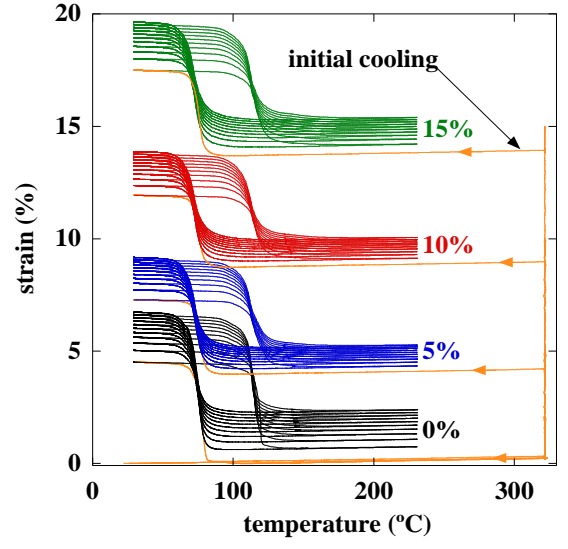
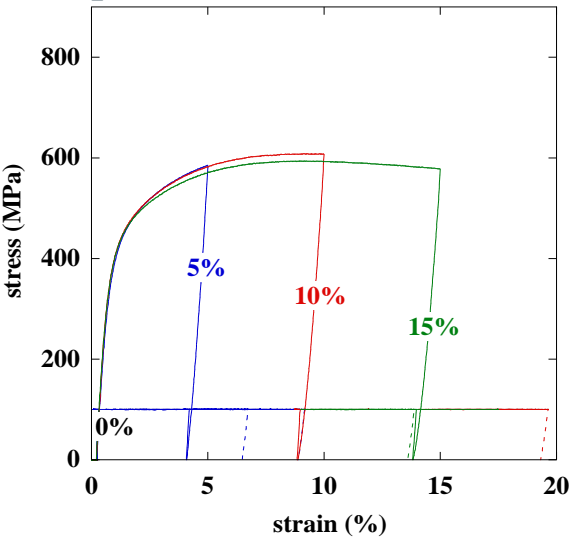
Training II: Constant Strain/Variable Temperature



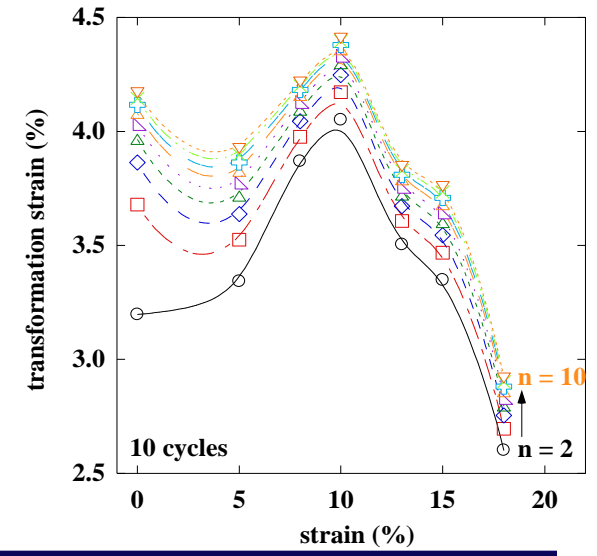
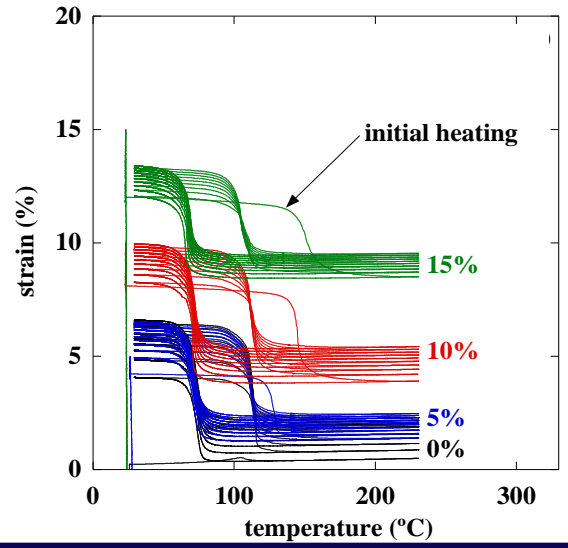
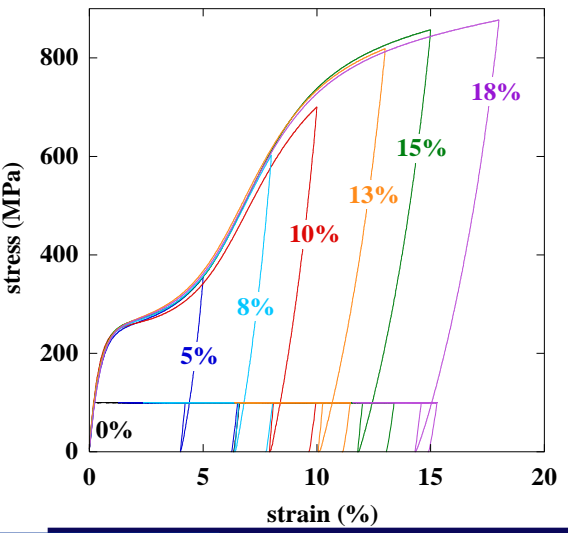


Extend from TWSME to Load-Biased On the Optimization of Actuator Properties

Samples deformed at 320 °C



Samples deformed at RT





Summary and Conclusions

- **The role of deformation and the corresponding microstructure on the TWSME training was investigated**

- **The TWSME can be optimized to fit several applications using the same training procedure**

- **In this alloy (55NiTi):**
 - **Positive TSWME → ~2.2%**
 - **No TWSME → 0%**
 - **Negative TWSME → ~-1%**

- **Can be extended to optimize SMA actuators under load**

- **Understanding the microstructure (in this work using neutron diffraction) is key in training and optimizing the structure (e.g., SMA actuators)**