

# Phased Array Measurements Made on the GE Counter-Rotating Open Rotor Model, F31/A31 Blades

Gary Podboy NASA GRC

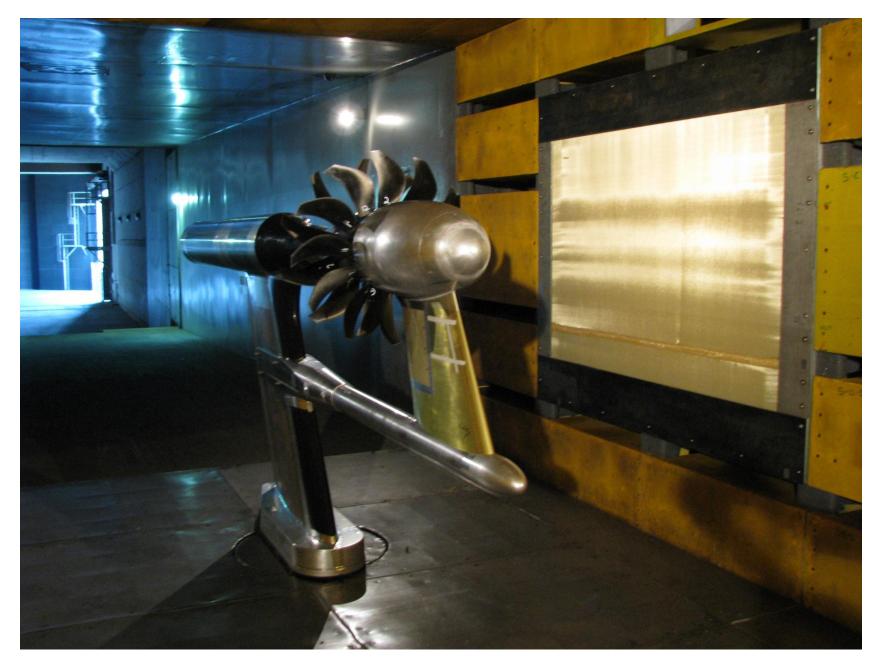
Csaba Horvath ASRC Aerospace

Acoustics Technical Working Group

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Support Provided by the Environmentally Responsible Aviation Program

#### GE Counter Rotating Open Rotor Model Installed in the NASA Glenn 9 x 15 Ft Wind Tunnel



Purpose

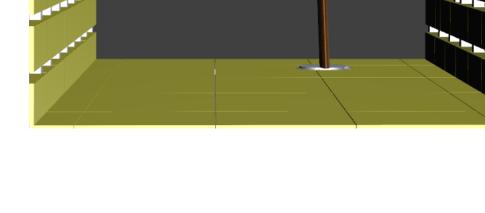
#### Locate the noise sources on the model

Location of Array48 

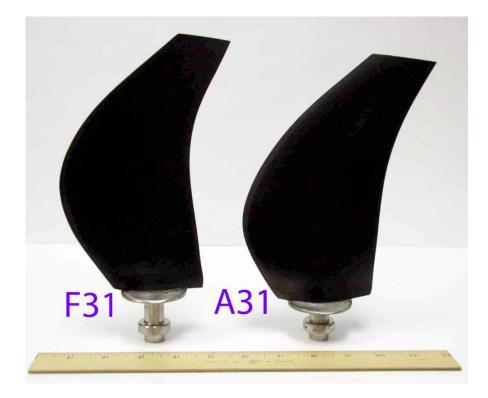
3D Schematic of 9 x 15 Ft Wind Tunnel

Photo showing Array48 in south wall of Wind Tunnel





#### F31/A31 Blades



12 Front Rotor Blades

10 Aft Rotor Blades

Front Rotor Speed = Aft Rotor Speed

#### **Test Conditions**

#### Corrected Rotor Speeds, RPM

	Approach Blade Angle (33.5°/35.7°)	Take-off Blade Angle (40.1°/40.8°)
Mach 0.2 0° AOA	<mark>5598,</mark> 6325, 6773, 7245, 7487	4628, 5277, 5561, 6080, 6316, <mark>6450</mark>
Mach 0.2 -3° AOA	5598, 6325, 6773	4628, 5561, 6316
Mach 0.2 -8° AOA	5598, 6325, 6773	4628, 5561, 6316
Mach 0.22 0° AOA	5903, 6617, 7054	4880, 5790, <mark>6530</mark>

No Pylon



Front Rotor Speed = Aft Rotor Speed Green designates Approach design speed Red designates Take-off design speed

#### **Test Conditions**

#### Corrected Rotor Speeds, RPM

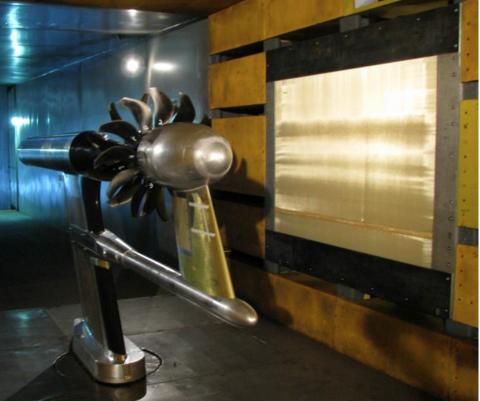
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Pylon

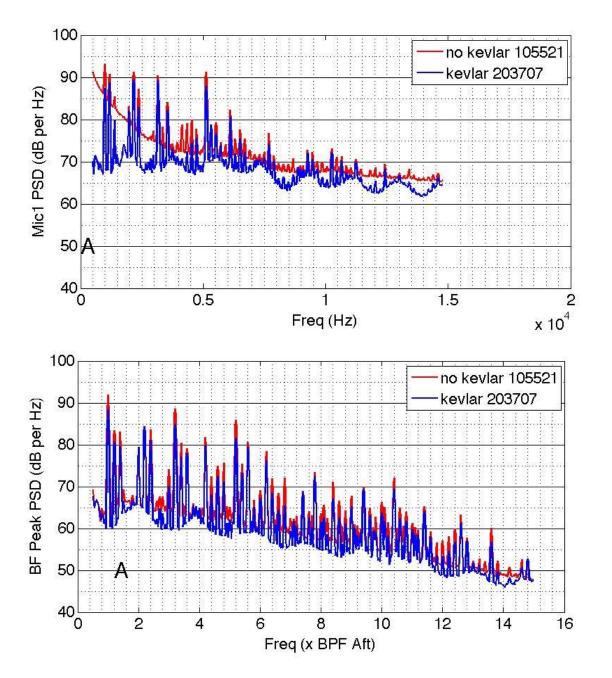
Front Rotor Speed = Aft Rotor Speed Green designates Approach design speed Red designates Take-off design speed First Use of Kevlar Window

#### Kevlar Window





#### First Use of Kevlar Window



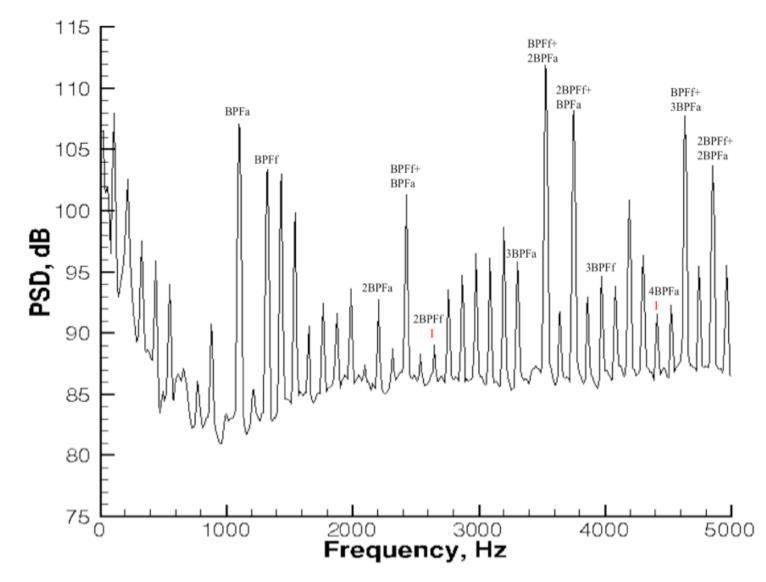
No Kevlar Window



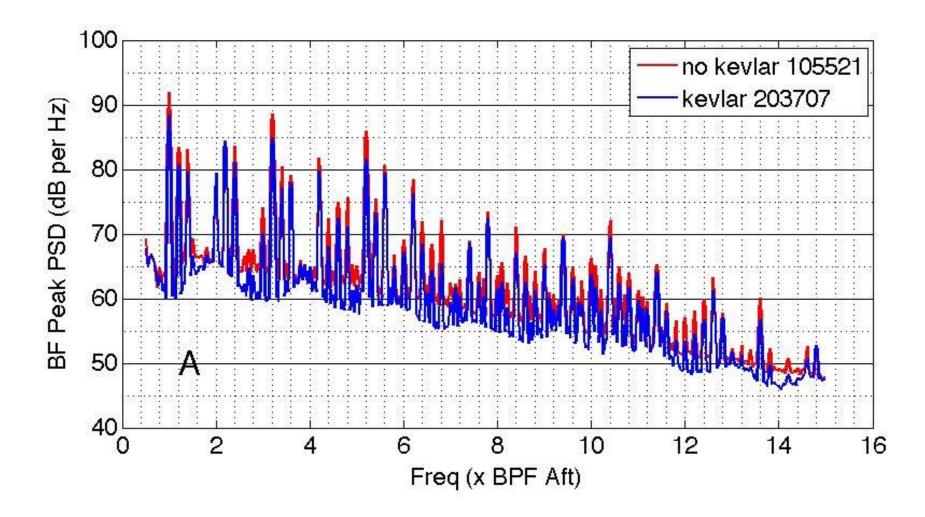
Kevlar Window



# Want to determine source location of each tone and the broadband noise between the tones



Data processed between 0.5 BPFA and 15 BPFA

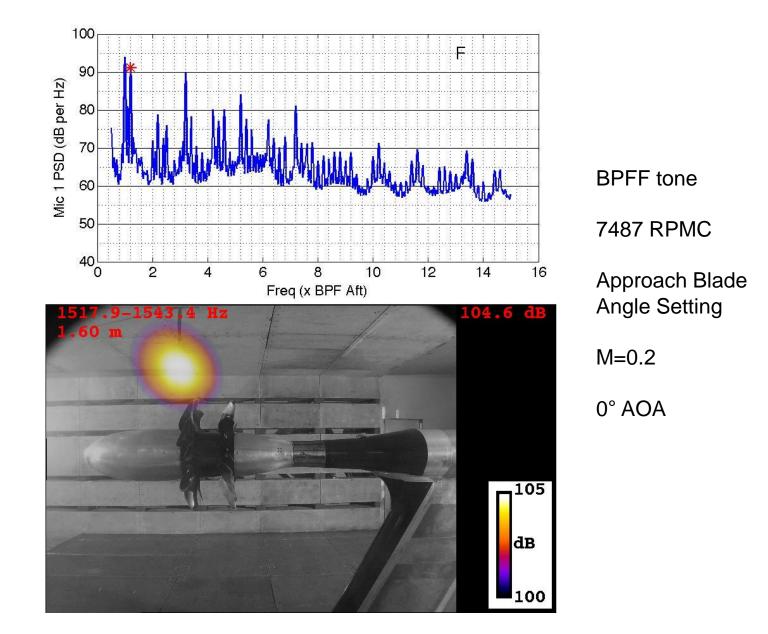


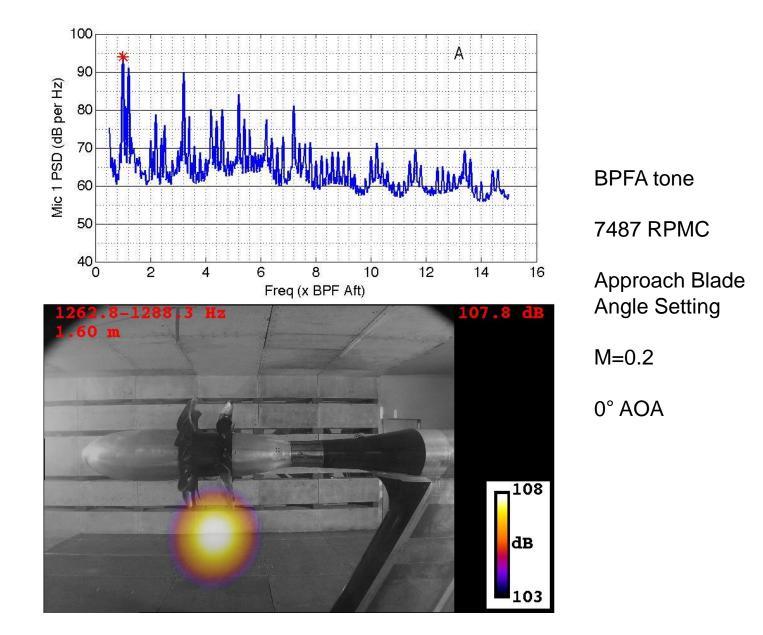
Data processed between 0.5 BPFA and 15 BPFA

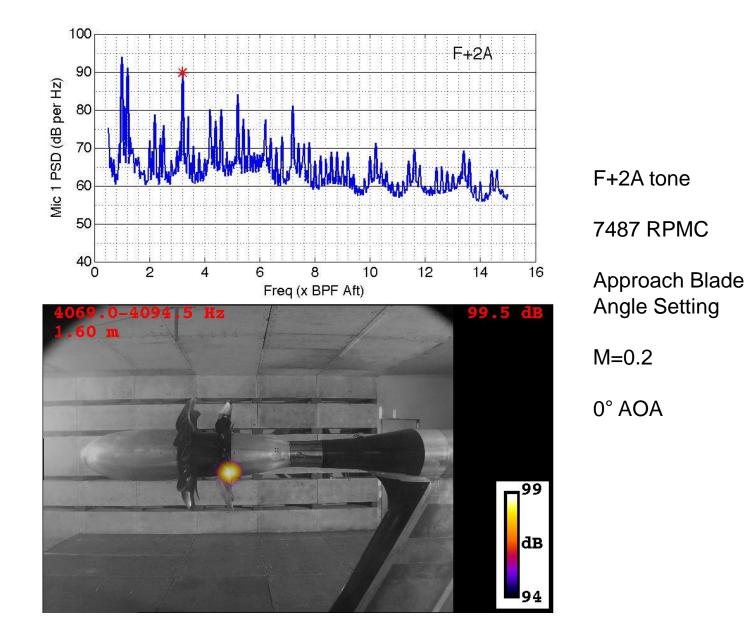
using bin widths that varied with RPM (5 frequency bins between consecutive shaft orders)

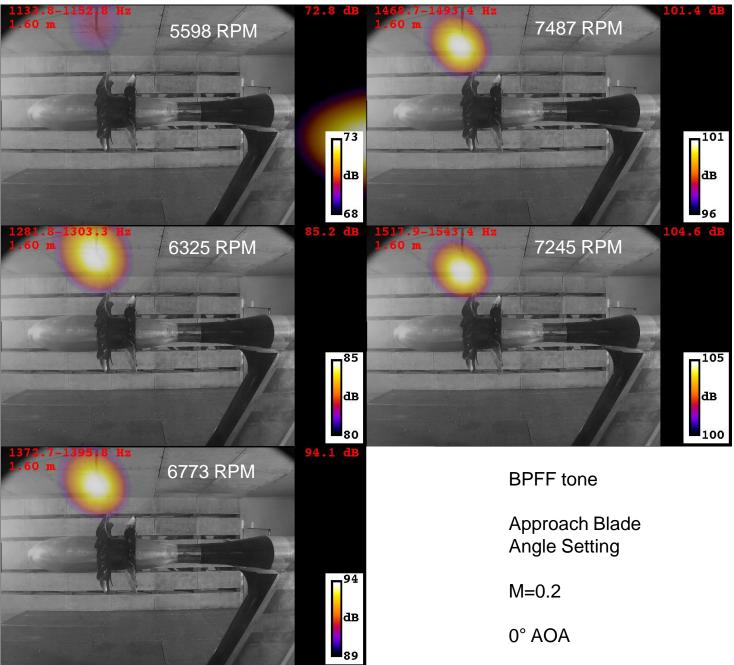
725 beamforming images per set

shaft order processing makes it easier to find images corresponding to certain tones

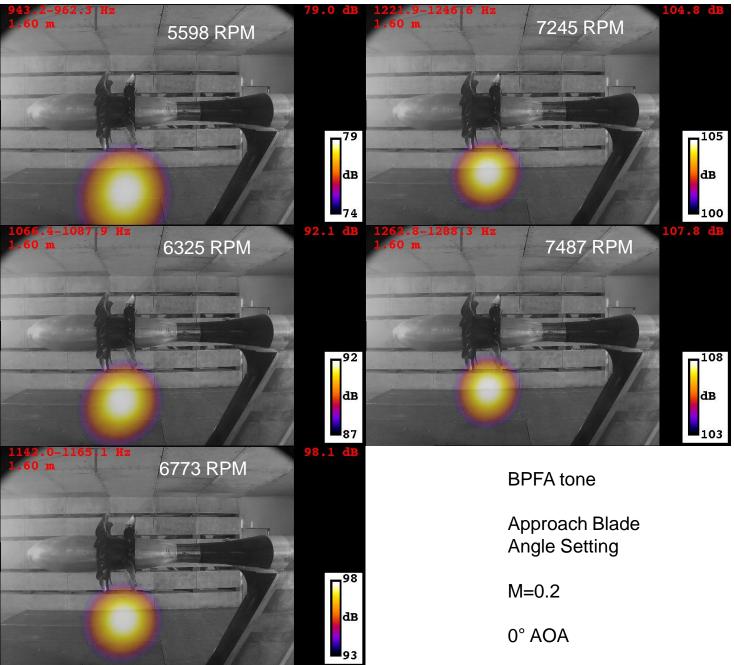






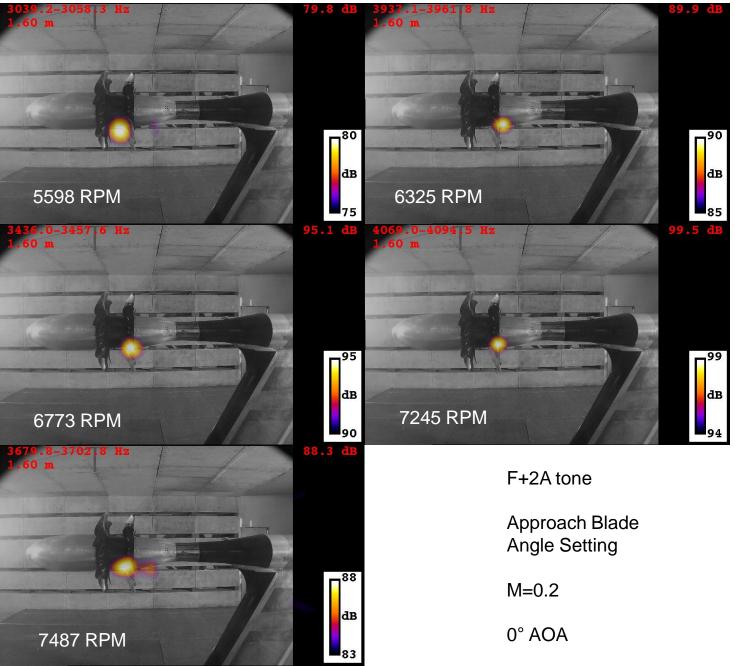


National Aeronautics and Space Administration



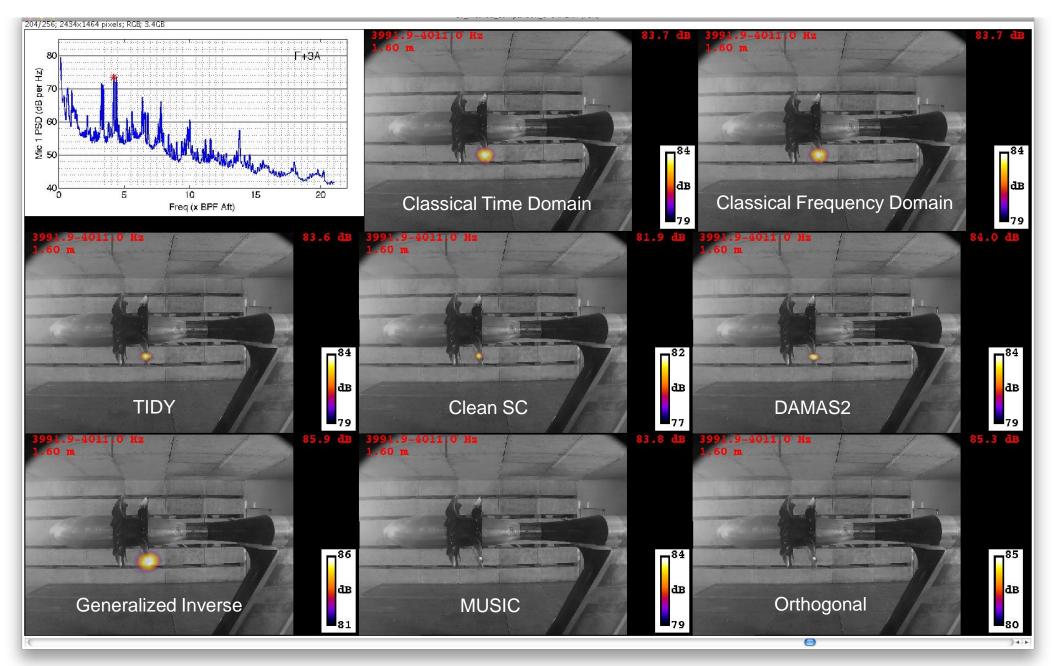
National Aeronautics and Space Administration

Are the source locations accurate?



National Aeronautics and Space Administration

Phased Array Measurements Made on the GE Counter-Rotating Open Rotor Model, F31/A31 Blades 17



#### **Test Conditions**

#### Corrected Rotor Speeds, RPM

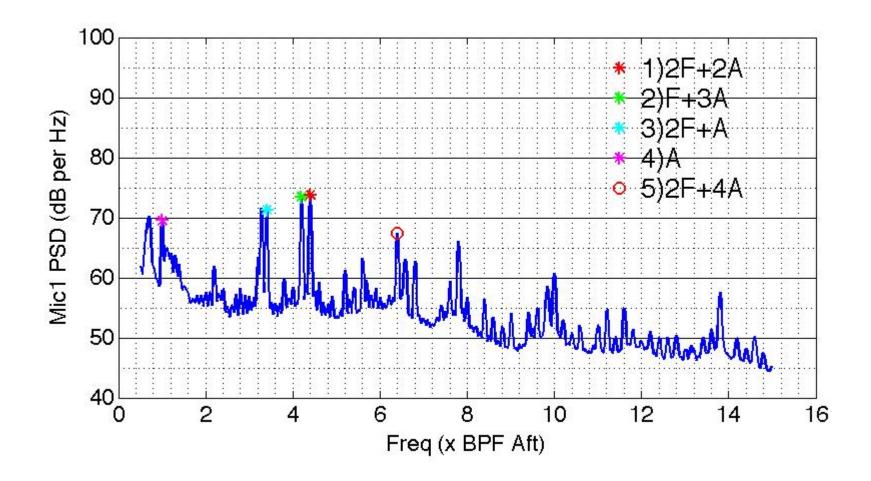
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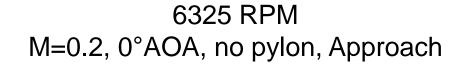
No Pylon

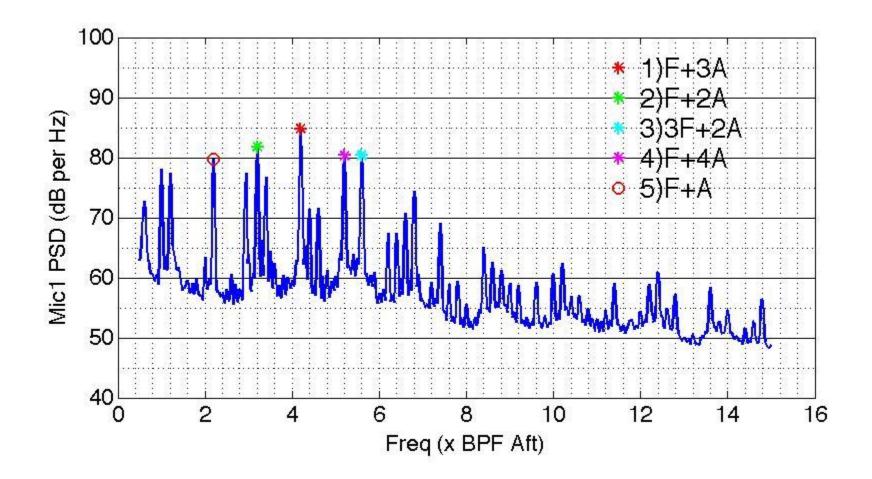


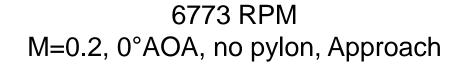
Front Rotor Speed = Aft Rotor Speed Green designates Approach design speed Red designates Take-off design speed

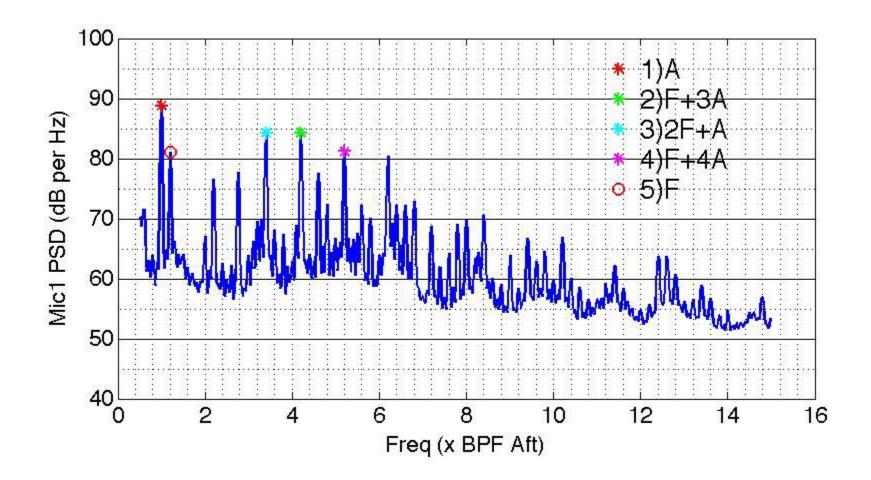
#### 5598 RPM M=0.2, 0°AOA, no pylon, Approach

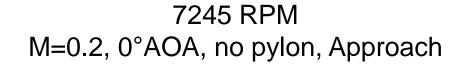


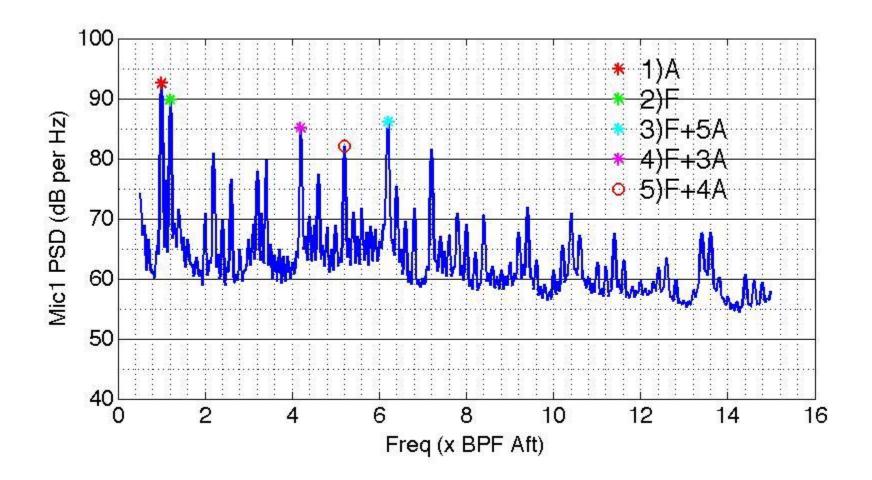


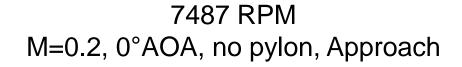


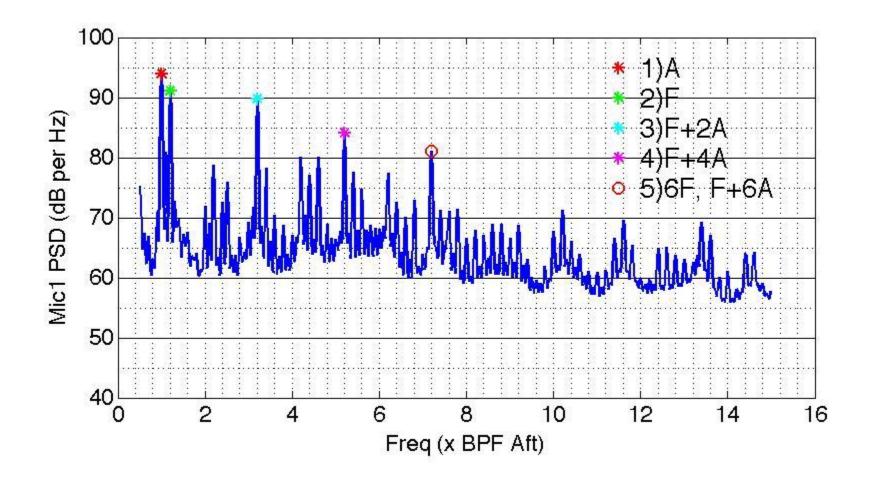


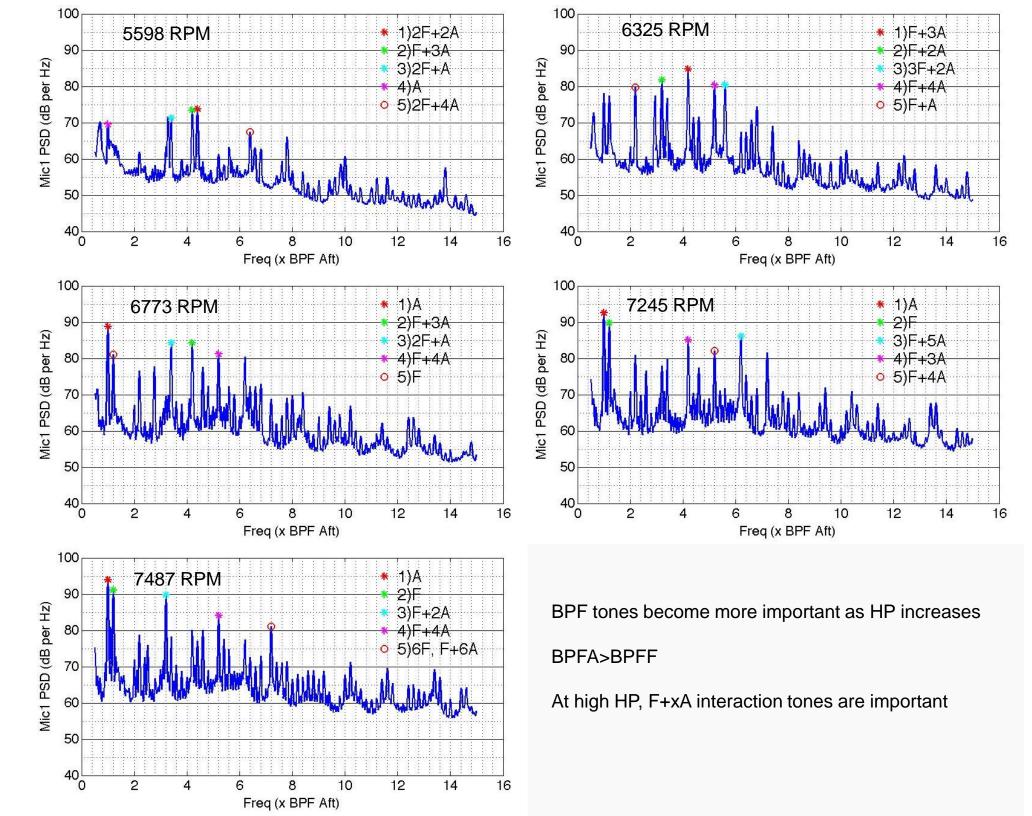




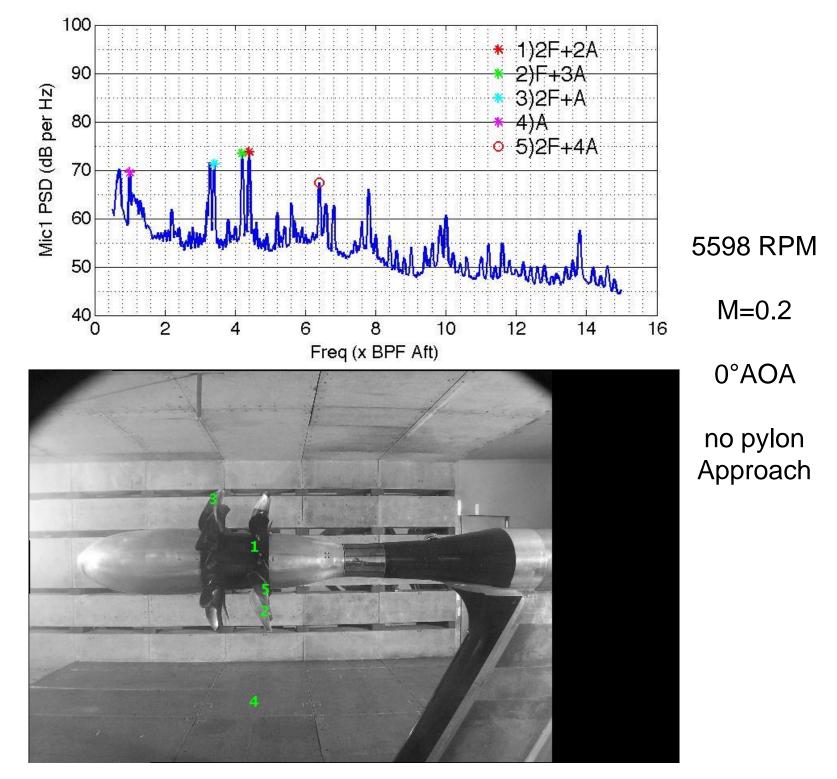


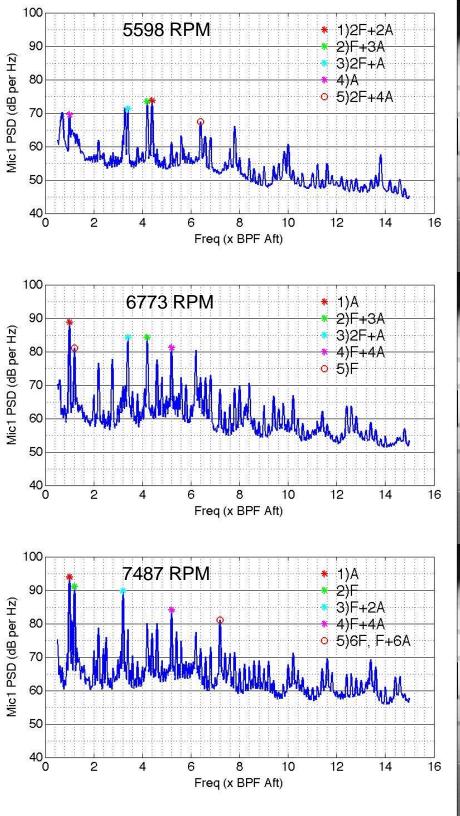


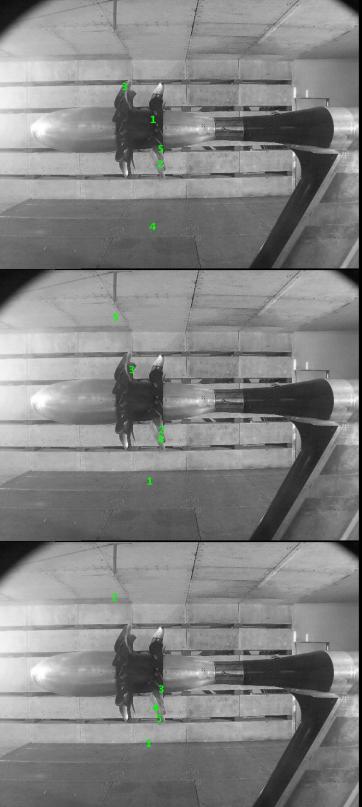




# Noise source location of dominant tones M=0.2, 0° AOA, no pylon, Approach, varying HP







-The dominant tones are, for the most part, located on the side of the rig where the blade is rotating toward the phased array.

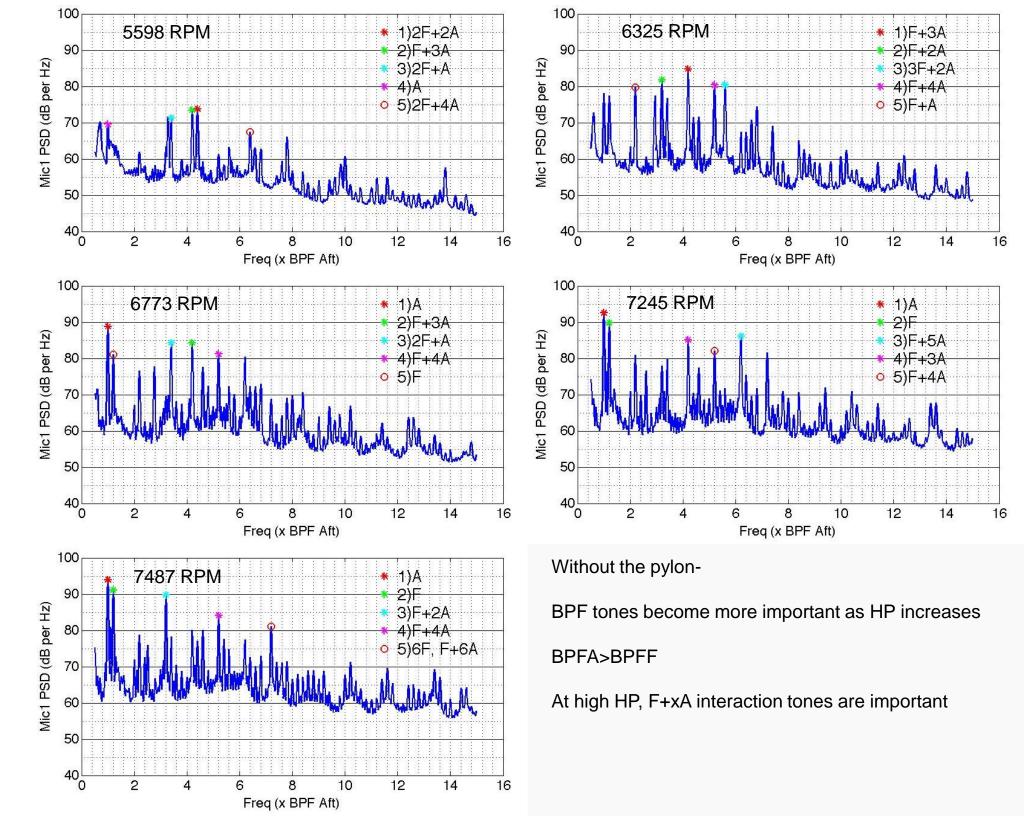
-A large percentage of the dominant tones are located on the aft rotor

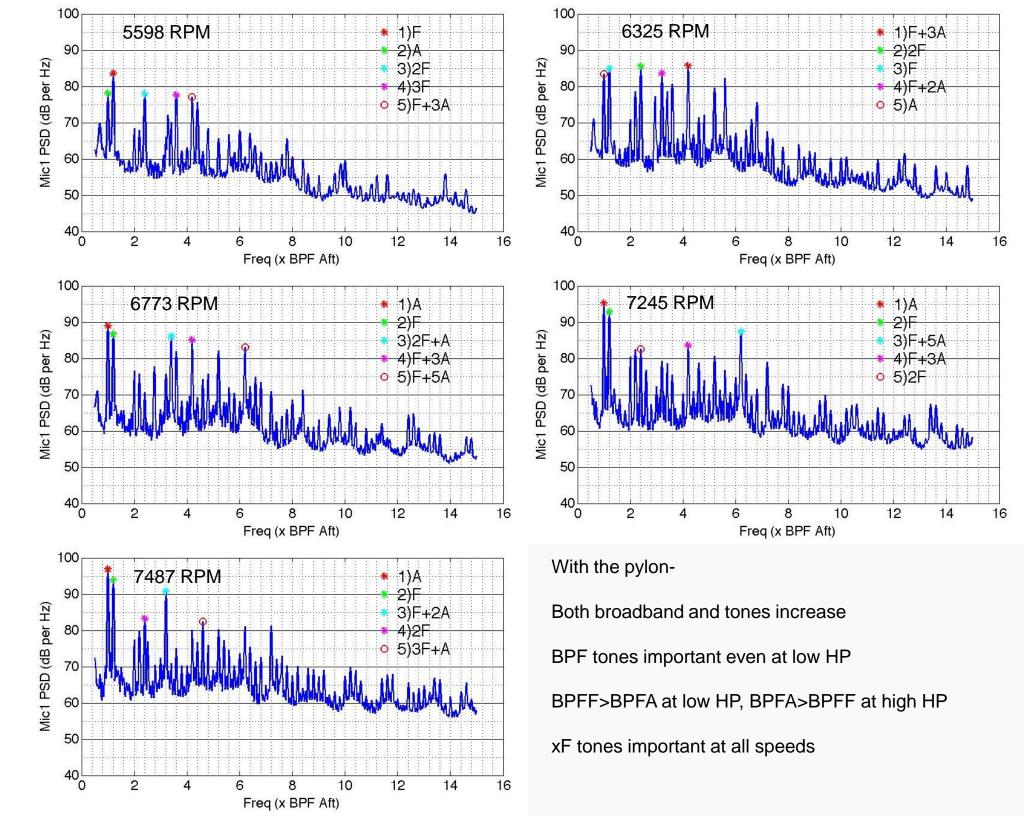
- The interaction tones seem to come from the rotor which has a higher multiple of its BPF in the interaction

# **Comparison of Spectra**

no pylon vs. pylon

### M=0.2, 0° AOA, approach, varying HP

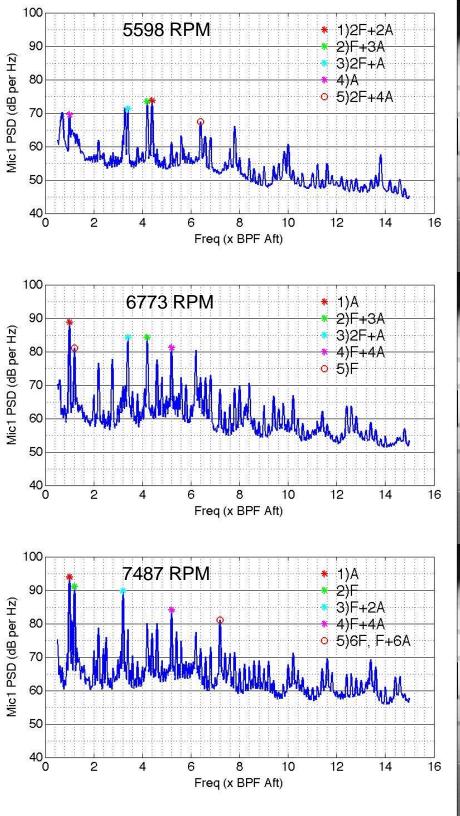


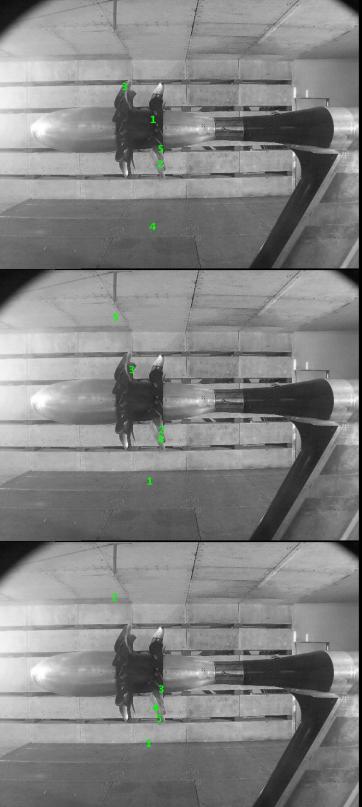


# Comparison of Dominant Tone Location

no pylon vs. pylon

M=0.2, 0°AOA, approach, varying HP

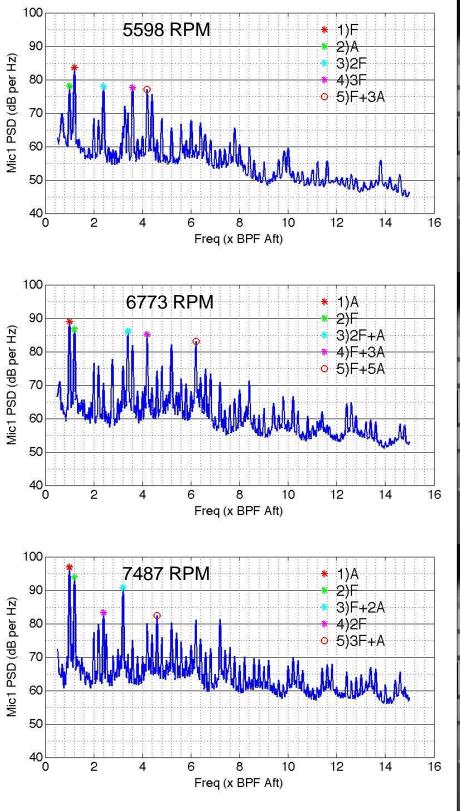


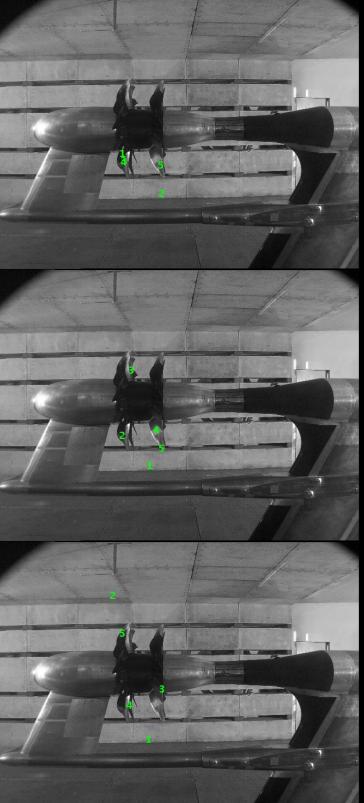


-The dominant tones are, for the most part, located on the side of the rig where the blade is rotating toward the phased array.

-A large percentage of the dominant tones are located on the aft rotor

- The interaction tones seem to come from the rotor which has a higher multiple of its BPF in the interaction





Unlike the no pylon case:

-The dominant tones are located on the lower side of the rig where the blade is passing the pylon, especially at lower HP

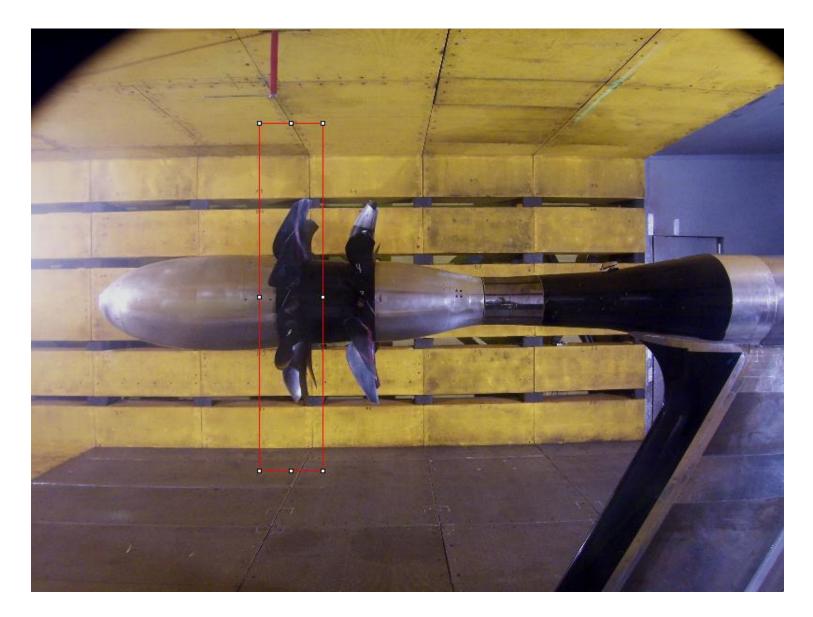
-A smaller percentage of the dominant tones are found on the aft rotor

#### Regions of Interest

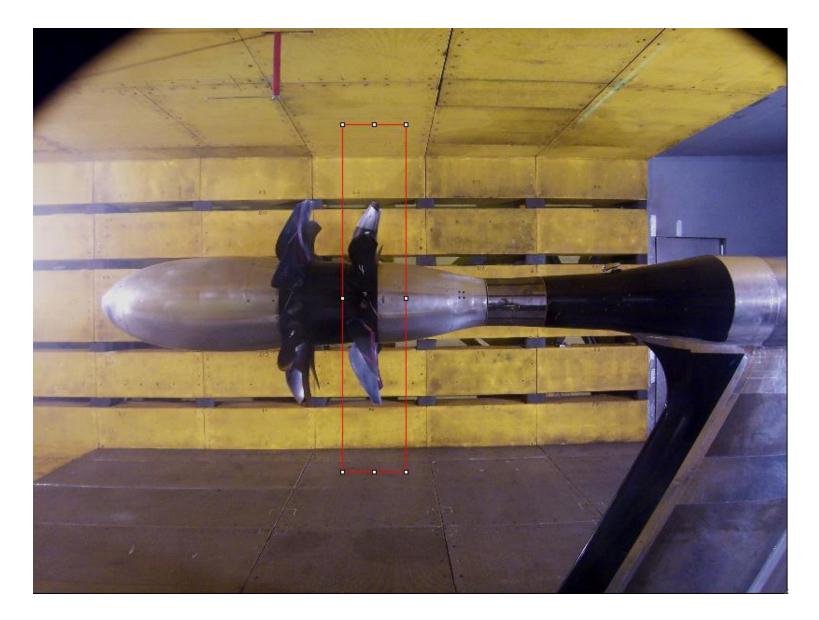
#### Can look for noise sources in entire image



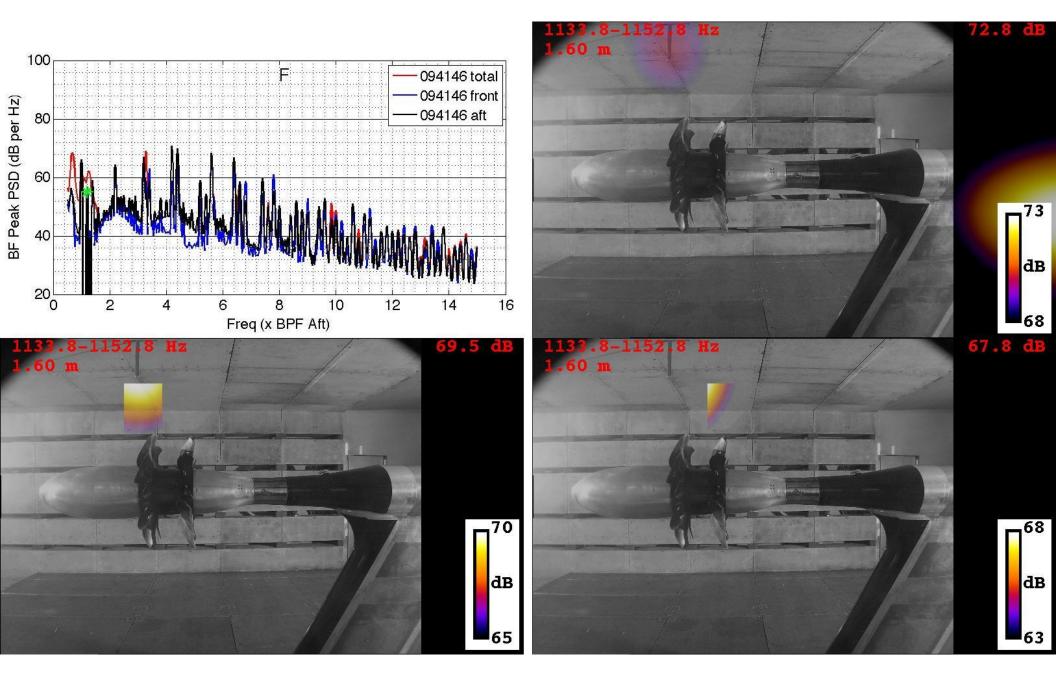
#### Regions of Interest ...or only around the front rotor



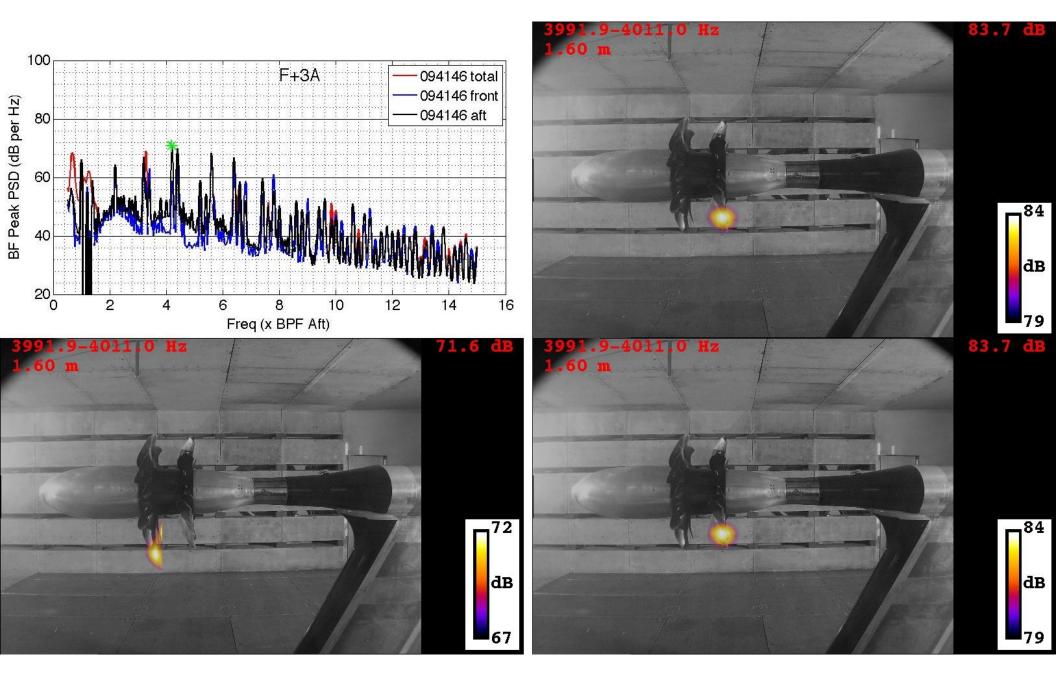
#### Regions of Interest ...or only around the aft rotor



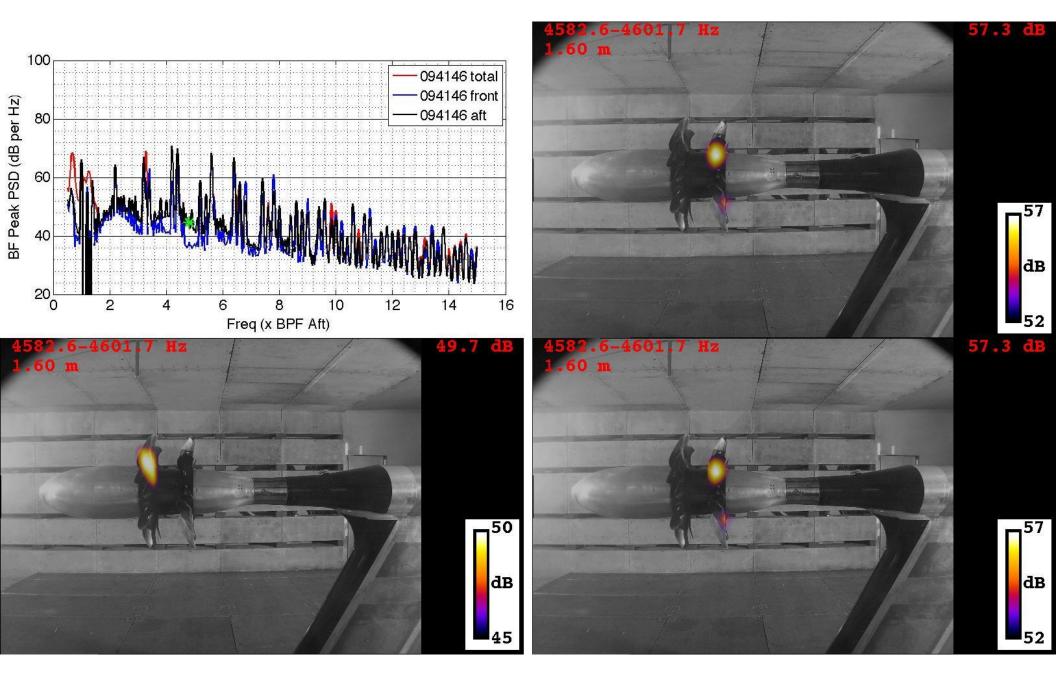
BPFF tone No pylon, Approach Blade Angle Settings , M=0.2,  $0^0$  AOA, 5598 RPM



## F+3A Interaction tone No pylon, Approach Blade Angle Settings , M=0.2, $0^0$ AOA, 5598 RPM



# Broadband noise No pylon, Approach Blade Angle Settings , M=0.2, $0^0$ AOA, 5598 RPM



#### Summary

Phased array data are presented for the GE Counter Rotating Open Rotor Model at 0° AOA, M=0.2, at the Approach condition blade angle settings.

Without a pylon:

- 1) interaction tones dominate over BPF tones at the design RPM
- 2) more broadband noise comes from the aft rotor than the front rotor at the design RPM
- 3) as RPM increases above the design speed: noise levels increase, more tones appear, and the BPF tones become more dominant. BPFA > BPFF. At high RPM, F+xA tones are important.
- 4) the tones tend to come from the side of the rotor rotating toward array (pressure side of the blades). Most tones come from the aft rotor. Dominant interaction tones tend to come from the rotor with the larger multiple in the interaction (ex: 3F+A from front, F+4A from back)

With a pylon:

- 1) at the design RPM, xF tones important
- 2) at the design RPM, BPFF>BPFA. At higher RPM, BPFA>BPFF
- 3) dominant tones located on the lower side of the rig, especially at low HP
- 4) dominant tones more evenly split between the two rotors
- 5) like the no pylon case, dominant interaction tones tend to come from the rotor with the larger multiple in the interaction

