# Cost-Performance-Parametrics for Transporting Small Packages to the Mars Vicinity 

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## Why Small Packages to Mars?

- A permanent presence on Mars will be a logistical challenge

Arriving mass on continual basis is needed during build-up and assembly phase to augment the delivery of large/mid-size elements

- In addition to seven (7) heavy lift missions, many smaller deliveries required:
- $15-20 \mathrm{t}=7$ flights
- 10-15 t=14 flights
- $5-10 \mathrm{t}=7$ flights
- $<5$ t = 87 flights
- Outfitting and resupply needs as build-up occurs
- Low cost, low mass services: resupply, imaging, comm/navigation
- Arriving mass on continual basis is needed during sustainment
- Much smaller mass throughput required during sustainment than build-up
- Critical spares, commodities, components, and equipment-often driven by unplanned events and unknowns
- Frequency often critical need-will a 2-year dwell between critical supplies be acceptable?
- Standardized packaging/containerization
- Starts with the small standard shipping packages and aggregates to the larger shipping containers


## Example Mars Surface Facility Masses (Metric Tons)

[from Koelle, H. H., Lunar Base Quarterly, vol. 11, No. 2, April 2003, Berlin, DE]


## Example Earth-Mars Direct Transit Modes

(Earth/Lunar distant aggregation methods also under review, not covered in this initial investigation)


1. Direct Transfer (All-up Single launch)

2. LEO Parking/Departure


Typical plot of total $\Delta \mathrm{V}(\mathrm{km} / \mathrm{s})$ for impulse case Mars transits from LD-HEO to 10-sol Mars orbit (2034-2035)


## Plots of total $\Delta \mathrm{V}(\mathrm{km} / \mathrm{s})$ for impulse case Mars transits from LD-HEO to 10 -sol Mars orbit (2017-2035)

Total Delta $V(\mathrm{~km} / \mathrm{s})$


## Transit System Assumptions (Initial Investigation)

| TRANSIT SPACECRAFT |  |
| :--- | :---: |
|  | CHEMICAL |
| Fuel | Malue |
| Onits |  |
| Oxidizer | NTO |
| $\mathrm{I}_{\text {sp }}$ | 315 s |
| Mass ratio | 0.1085 |
| Propellant mass fraction | 0.8915 |
| Engine mass fraction | 0.0060 |
| Fuel tank mass fraction | 0.0221 |
| Oxidizer tank mass fraction | 0.0222 |
| Structural mass fraction | 0.0045 |
| Dry mass fraction | 0.0548 |
| Payload mass fraction | 0.0537 |
|  |  |


| DRY MASS TABLE (EP) |  |
| :--- | :---: |
|  | value units |
| Propellant Tank characterisitics |  |
| Density | $3080 \mathrm{~kg} / \mathrm{m3}$ |
| Safety factor | 4 |
| Material specific density () | $4 \mathrm{~kg} / \mathrm{m3} / \mathrm{Mpa}$ |
| MEOP pressure | 23.44 Mpa |
| Propellant fraction \% | $27.5 \%$ |
|  |  |
| Structural coefficient, $\varepsilon s$ | 0.04 |


| DRY MASS TABLE |  |
| :---: | :---: |
|  | value units |
| Fuel Tank characterisitics |  |
| Density | $875 \mathrm{~kg} / \mathrm{m} 3$ |
| Safety factor | 4 |
| Material specific density () | $4 \mathrm{~kg} / \mathrm{m} 3 / \mathrm{Mpa}$ |
| MEOP pressure | 1.8 Mpa |
| Propellant fraction \% | 37.74 pct (\%) |
| Oxidizer Tank characterisitics |  |
| Density | $1443 \mathrm{~kg} / \mathrm{m} 3$ |
| Safety factor | 4 |
| Material specific density | $4 \mathrm{~kg} / \mathrm{m} 3 / \mathrm{Mpa}$ |
| MEOP pressure | 1.8 Mpa |
| Propellant fraction \% | 62.26 pct (\%) |
| Structural coefficient, $\varepsilon$ s | 0.04 |
| TRANSIT SPACECRAFT - ELECTRIC |  |
|  | value units |
| Propellant | Xe |
| $\mathrm{I}_{\text {sp }}$ | 3,000 s |
| Propellant mass fraction | 0.2749 |
| Propulsion Power/Mass | 2.7000 W/kg |
| Thruster efficiency | 0.6000 |
| PPU and Power Efficiency | 0.9500 |
| Propulsion alpha | $0.0300 \mathrm{~kg} / \mathrm{W}$ |
| Solar power alpha | $0.0100 \mathrm{~kg} / \mathrm{W}$ |
| Duty cycle (correction) | 0.9000 |
| Structural mass fraction | 0.0344 |
| Dry mass fraction | 0.2890 |

- Spacecraft sizing approach used simple characteristics/mass fraction
- LEO to LD-HEO scale factor of $30 \%$ found across launch vehicle classes
- Key Isp parameters were 315 s (chemical); 3,000 s (electric)


## Example plot of chemical system departure and arrival masses across two synodic cycles (nano-micro launch class delivery case)



## Constant thrust orbital transfer for electric propulsion case in optimal (left) and minimal payload (right) transfers


--x- - Vehicle + $\mathrm{p} / \mathrm{I}$ mass in HEO
-ロ—Accumulated payload mass to Mars orbit


## Affordability and flight rate capability parametric plots under investigation

Earth-to-orbit (ETO) Launch Price-per-kg
(Zapata, E., CRASTE 2014)



## Early results for high-frequency, variable capacity Mars transits from LD-HEO



## Variety of size classes to construct and sustain large space facilities

In-Space Facility Assembly Campaign
(ISS, 1998-2011)


## Conclusions

- Prospects promising for smaller class systems using higher frequency full synodic cycle deliveries
- Could augment assembly \& logistics; will explore future packaging and shipping options
- Transit time and trajectory optimization needed
- Methods of varying cadence/distribution of departures and arrivals should be investigated
- Size class roles/options need further investigation to maximize logistical deliveries by shipment size
- Need more data on support system functions and their logistics masses/rates required
- Investigation of different concepts for lunar and Mars vicinity waypoint operations-e.g., aggregated shipments
- Further investigation of affordability analysis warranted (i.e., from Earth-Surface to Mars surface)
- Commercial/economic potential-service sector implications of packaged cargo delivery rather than monolithic designs (i.e., cost of service to one player is the revenue to another)
- Package deliveries to Mars-small and large—may be enabling to support ambitious plans

