



# LAVA APPLICATIONS TO OPEN ROTORS\*

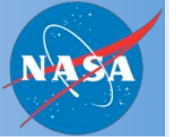
*\*Partially funded by ARMD – AATT Project*

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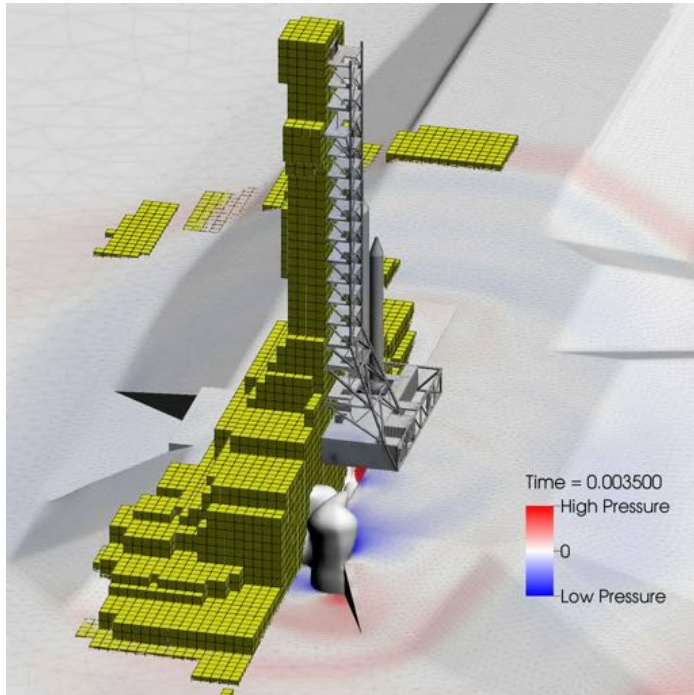
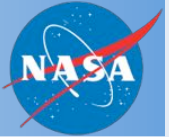
Fall 2015 Acoustics Technical Working Group Meeting  
October 20-21, Cleveland OH

# OUTLINE



- *LAVA (Launch Ascent Vehicle Aerodynamics)*
  - *Introduction*
  - *Acoustics Related Applications*
- *LAVA Applications to Open Rotor*
  - *Structured Overset Grids*
  - *Cartesian Grid with Immersed Boundary*
    - *High Speed Case*
    - *High Speed Case with Plate*
    - *Low Speed Case*

# LAUNCH ASCENT VEHICLE AERODYNAMICS (LAVA)



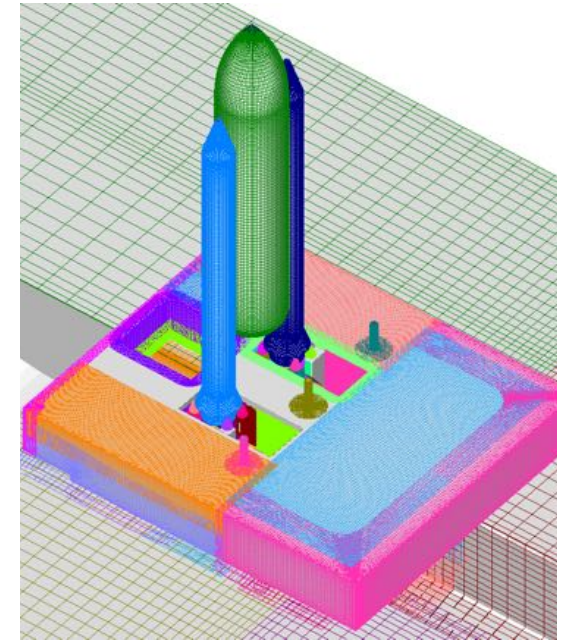
## ***Cartesian AMR***

- Essentially no manual grid generation
- Highly efficient Adaptive Mesh Refinement (AMR)
- Low computational cost
- Reliable higher order methods are available
- Non-body fitted -> Resolution of boundary layers problematic/ inefficient



## ***Unstructured Arbitrary Polyhedral***

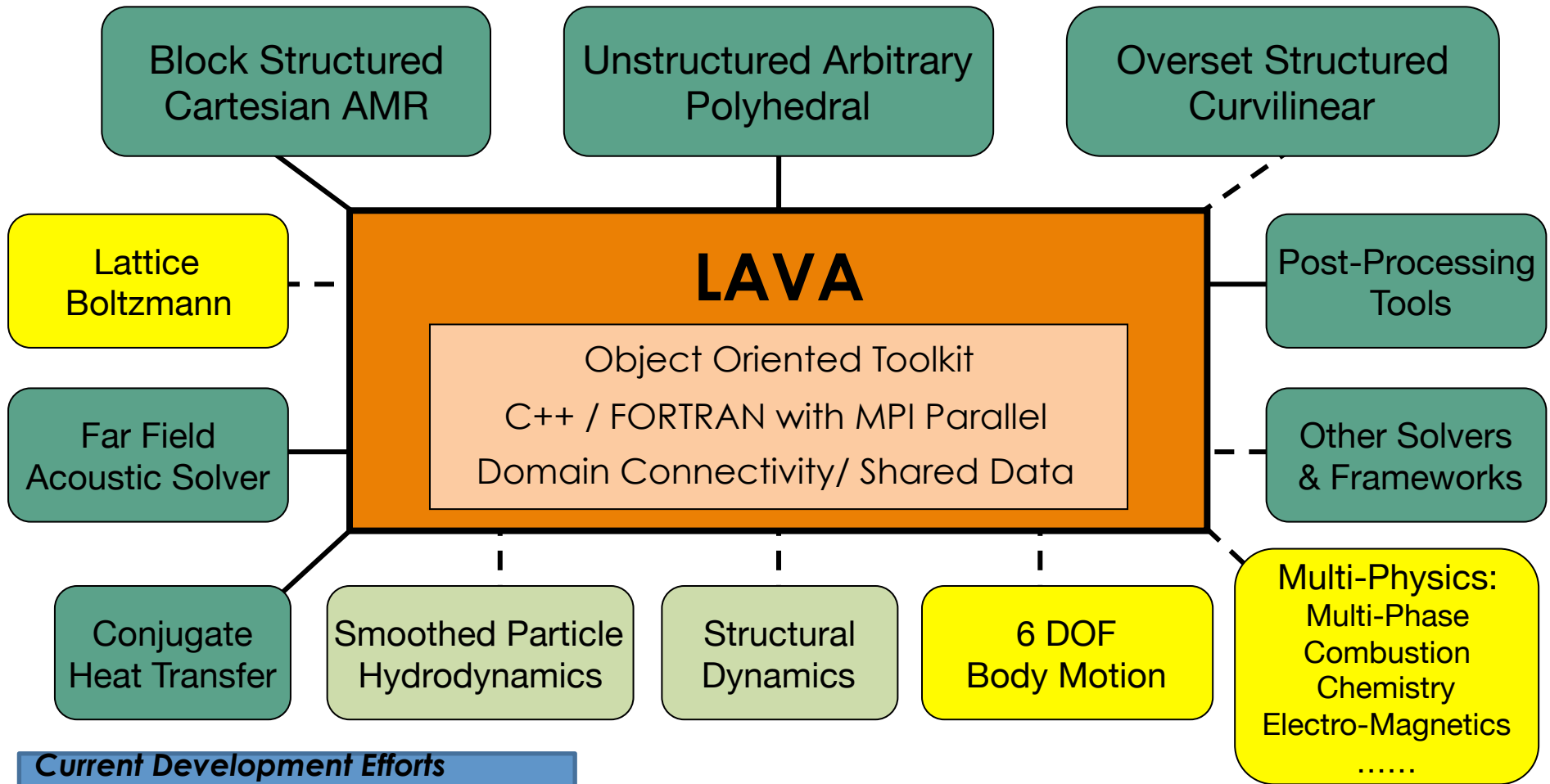
- Grid generation is mostly automated
- Body fitted grids
- Grid quality can be questionable
- High computational cost
- Higher order methods are yet to fully mature



## ***Overset Structured Curvilinear***

- High quality, body fitted grids
- Low computational cost
- Reliable higher order methods are available
- Grid generation is largely manual and time consuming

# MULTI-DISCIPLINARY ANALYSIS FRAMEWORK



## Current Development Efforts

- Higher Order Methods
- Grid Generation
- Wall Function
- LES/DES/ILES Turbulence
- HEC (GPU and future platforms)

— Connected

- - - Not Yet Connected

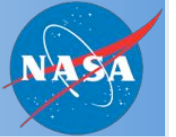
Existing

Developing

Future

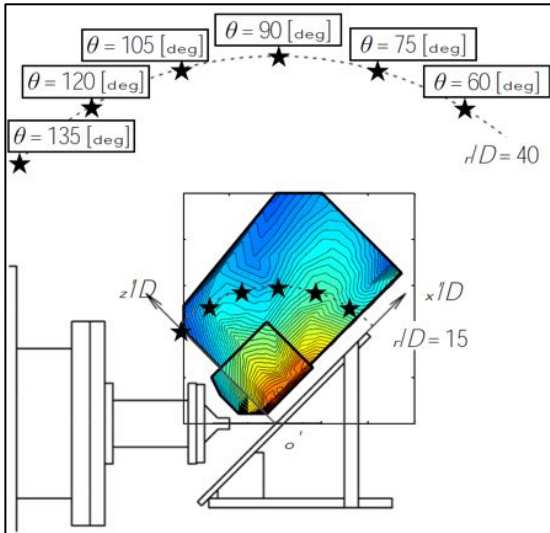
Framework

# OUTLINE

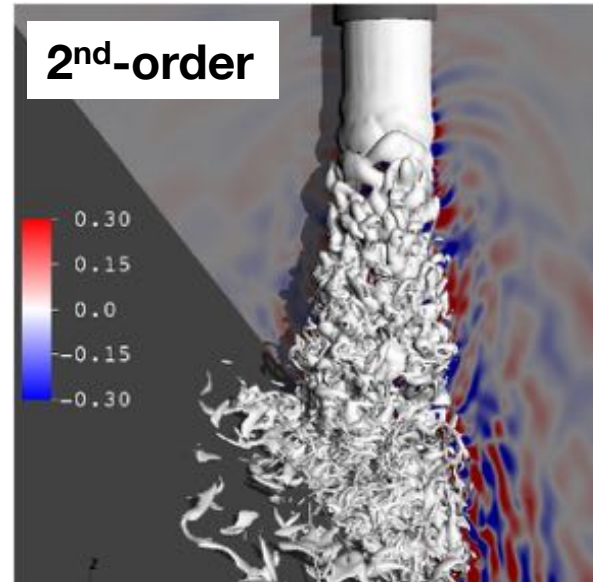


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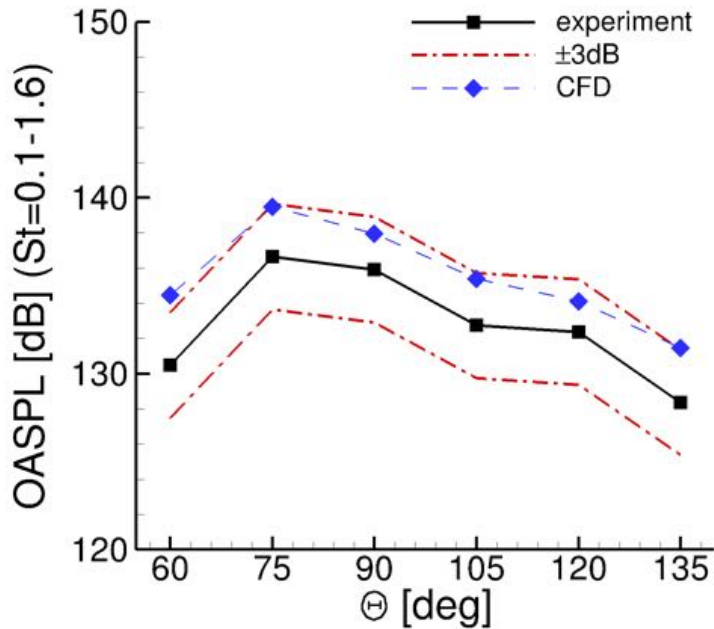
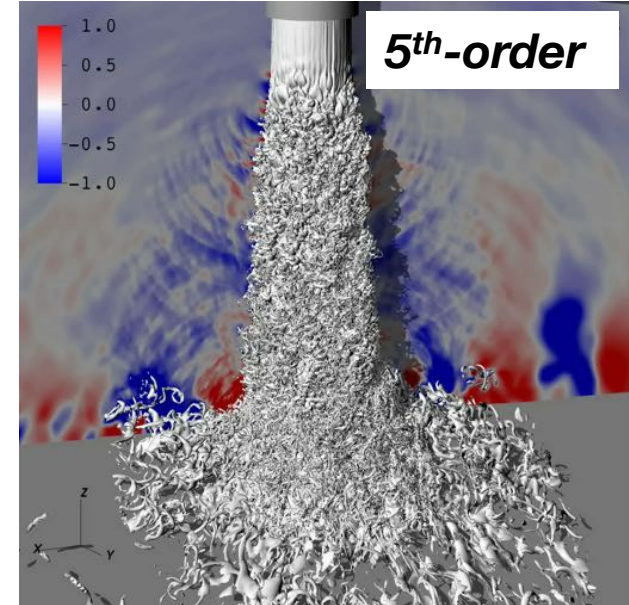
# JAXA COLLABORATION - JET ACOUSTICS



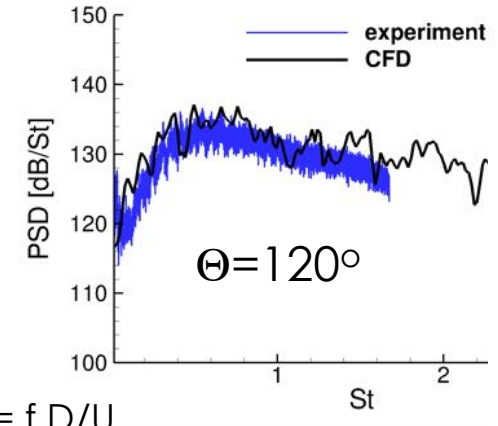
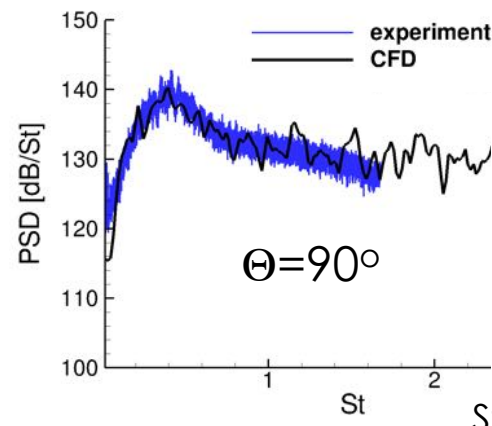
University of Tokyo Experiment  
Nakanishi et. Al. AJCPP2012-129



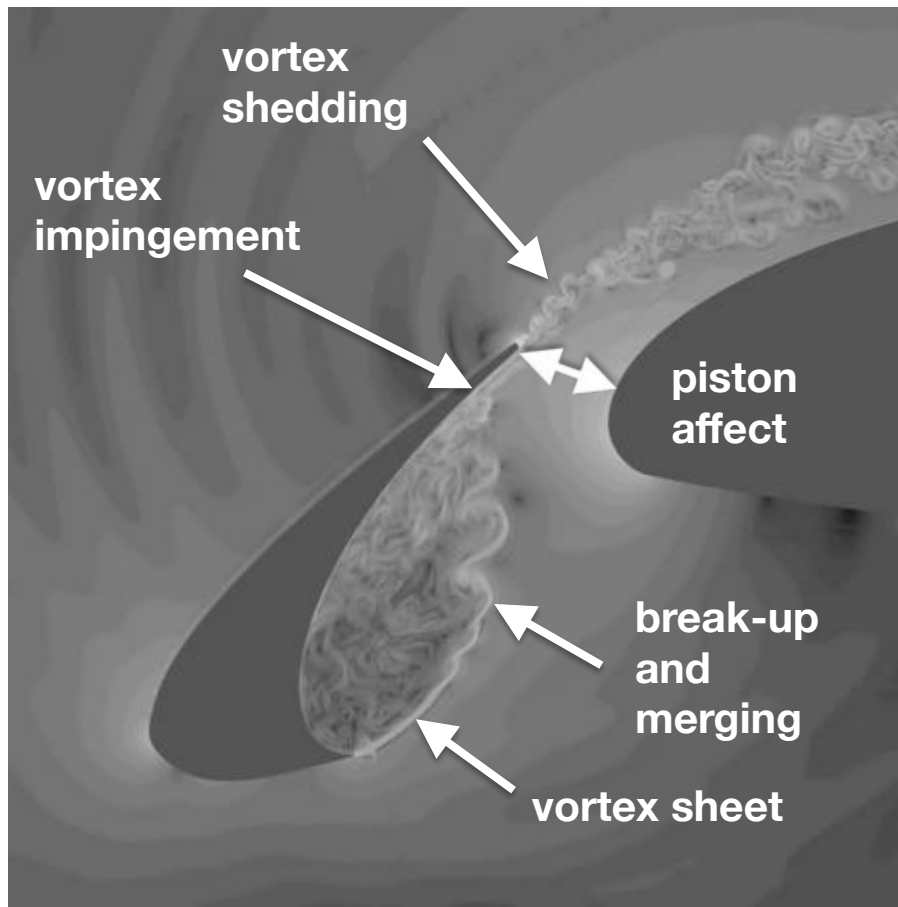
$M=1.8$



- OASPL predictions within 3 dB are obtained
- Good comparison in PSD observed



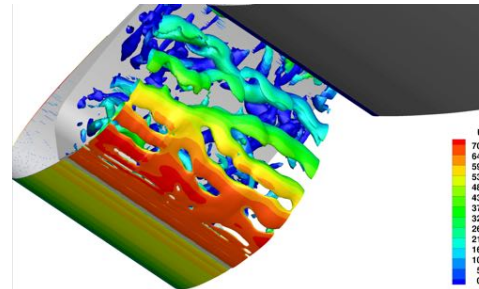
- BANC III Workshop problem has been revisited
- QFF tunnel study has been performed for conventional slat and various Krueger slat geometries



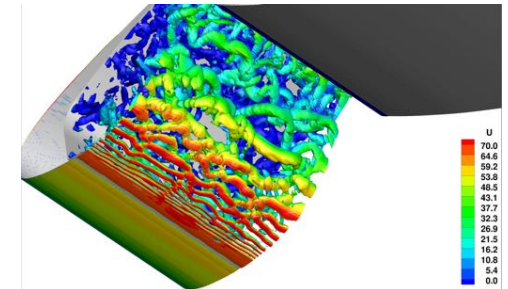
# TTT – ENHANCEMENT IN LAVA FOR SLAT NOISE



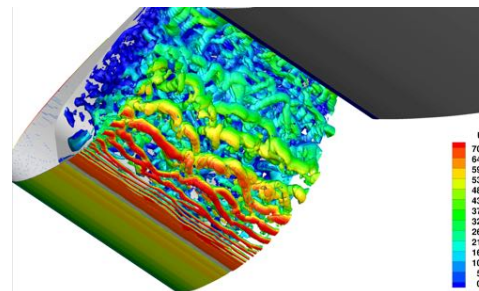
- Major algorithmic improvements have been implemented in the LAVA solver framework to help support the ERA noise reduction goals:
  - Improved DDES model with enhanced LES length scale and zonal DES approach
  - Increase from 5<sup>th</sup> order to 7<sup>th</sup> order accurate convective flux discretization in the span-wise direction
  - Blending of the upwind and central variable interpolation procedures for increased spectral resolution



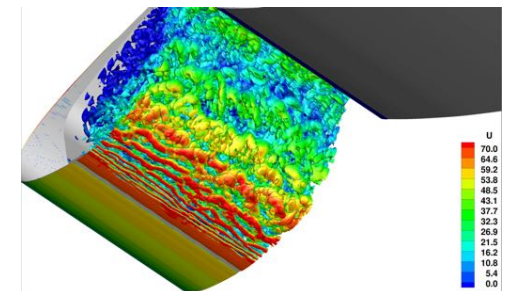
Original Algorithm



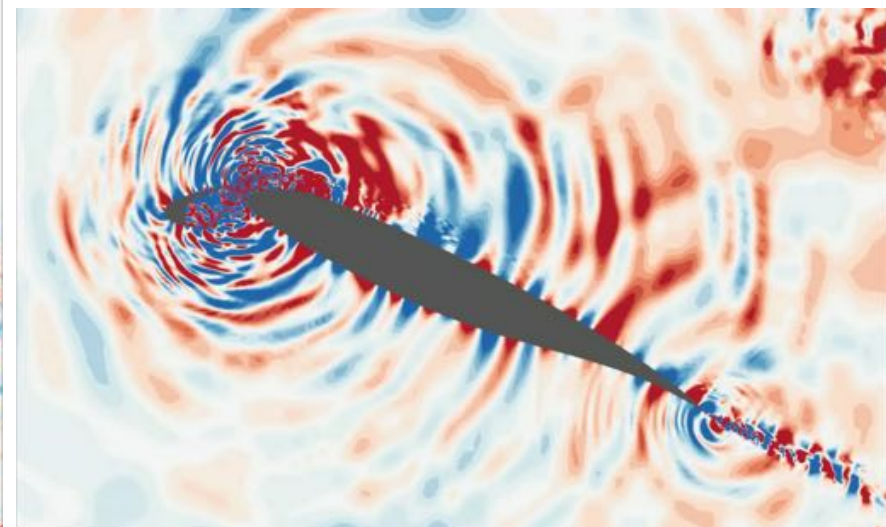
Improved DDES model



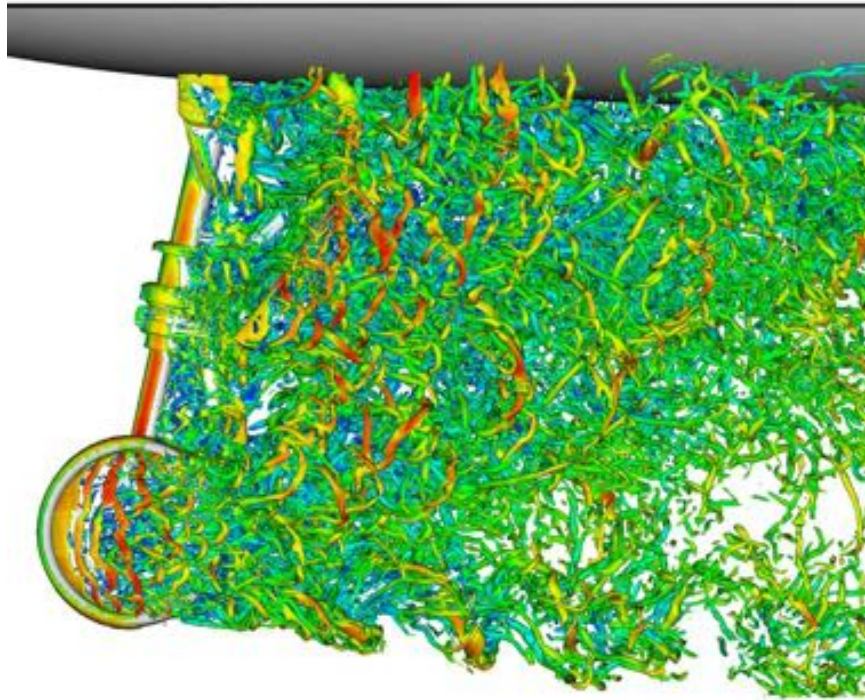
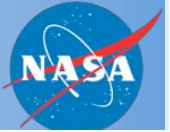
7<sup>th</sup> order accurate in span



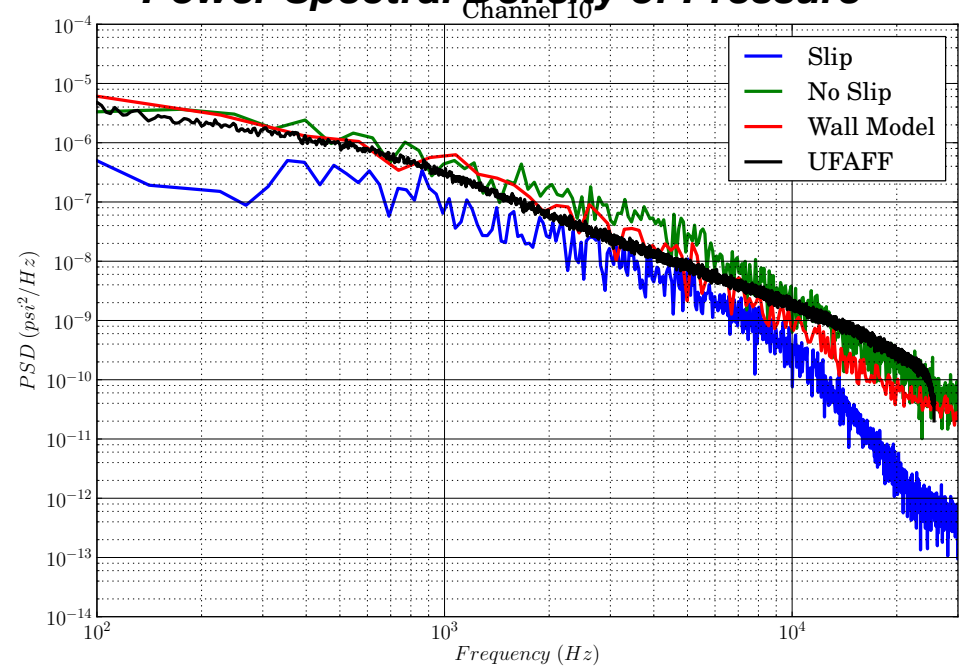
Blended Upwind/Central



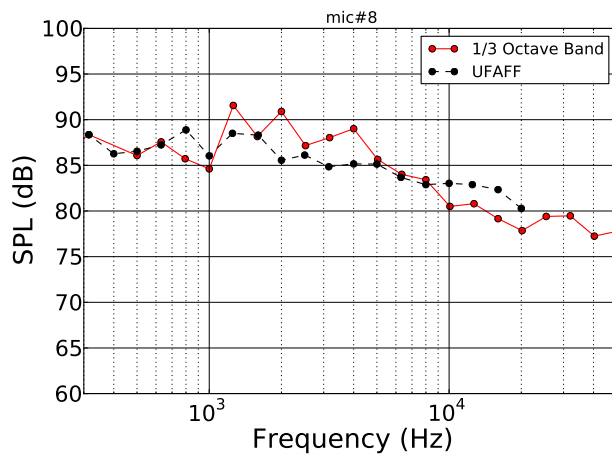




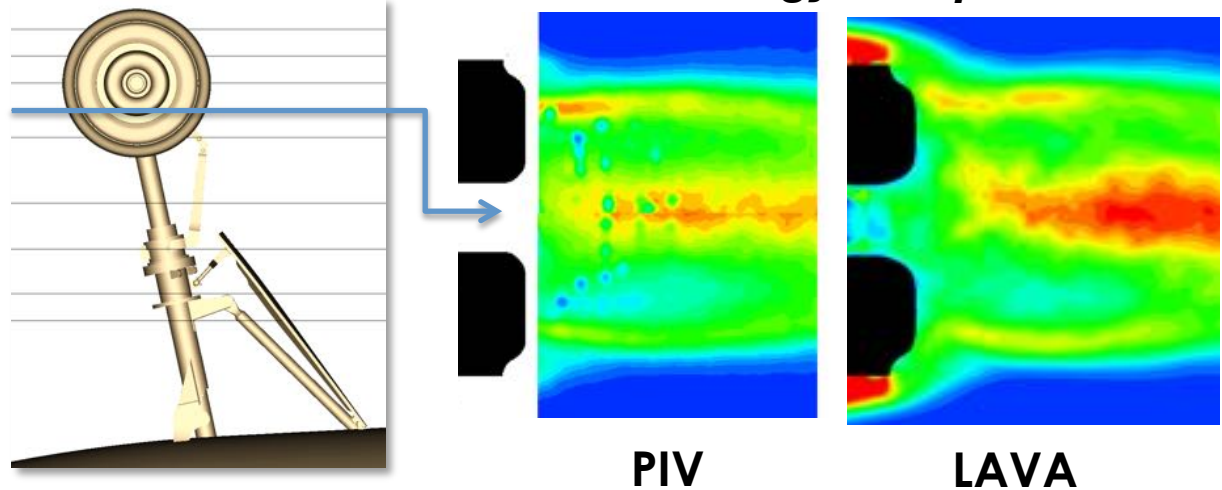
### Power Spectral Density of Pressure



### Far Field Acoustic SPL



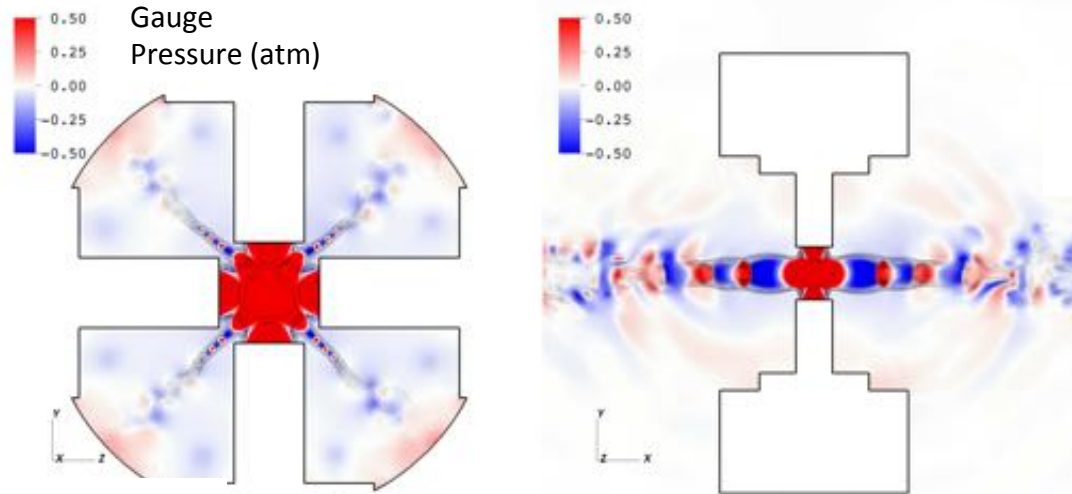
### PIV Mean Turbulent Kinetic Energy Comparison



# ERA - HYBRID WING BODY ENGINE NOISE EMULATOR



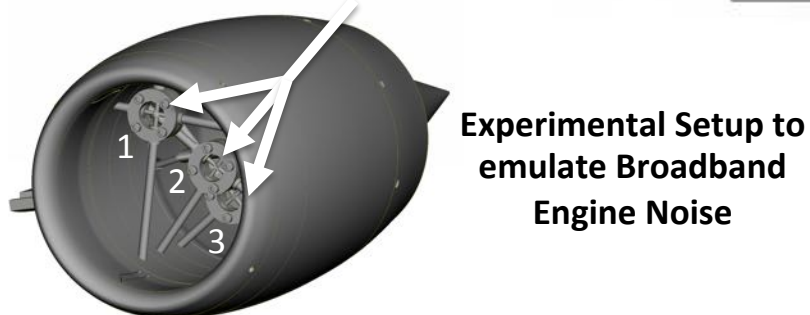
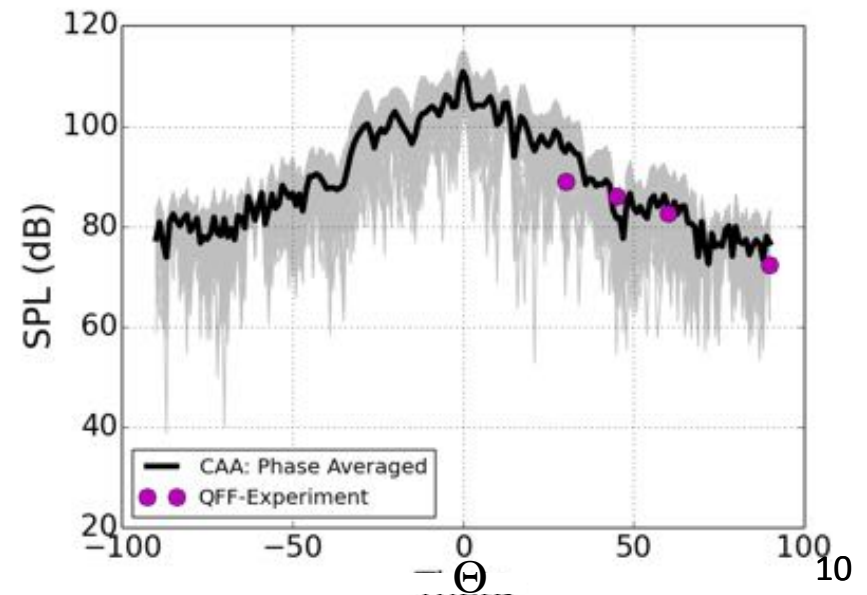
High fidelity CFD simulation of Four-Jet-Impingement device that is used as broadband noise source



Engine placement study is performed using linear acoustic scattering code

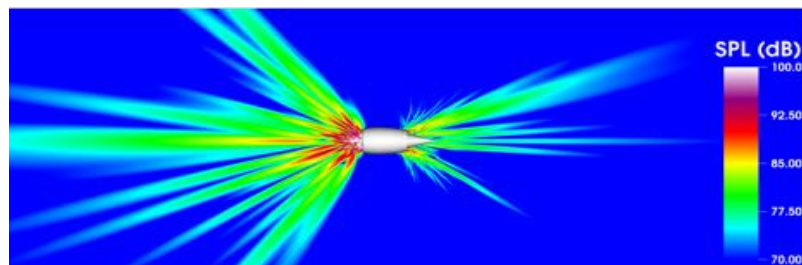


Comparison of BENS simulation with experimental results by Hutcheson et al. (2014)

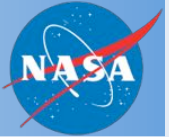


Experimental Setup to emulate Broadband Engine Noise

Sound Pressure Level Obtained with Linear Acoustic Scattering Code using Reduced Order Model



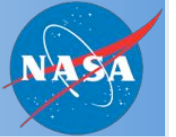
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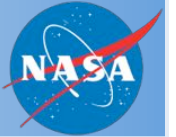


- CROR Overset Simulation (High Speed)
  - Computational Approach
  - Overset Grid System
  - Acoustic Propagation Surfaces
  - Flow Visualization
  - Results and Comparison to WT Data
- Single Blade Time-step Resolution Study
  - Geometry and Overset Grid System
  - Solver Parameters
  - Results and Conclusions
- Fine Mesh Overset Grid System (High Speed and Low Speed)
  - Comparison between new and old grid systems



## *Conditions:*

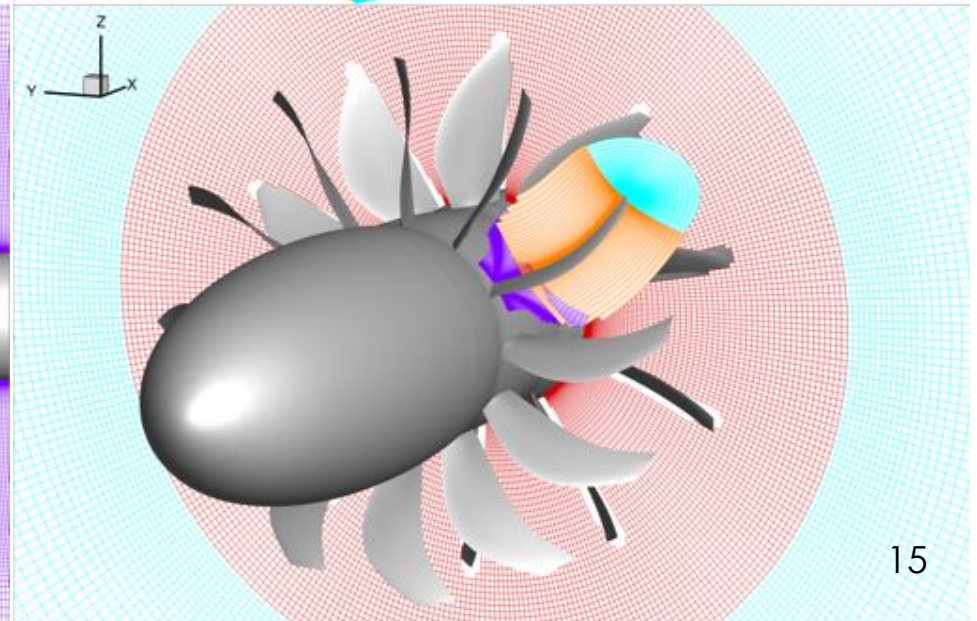
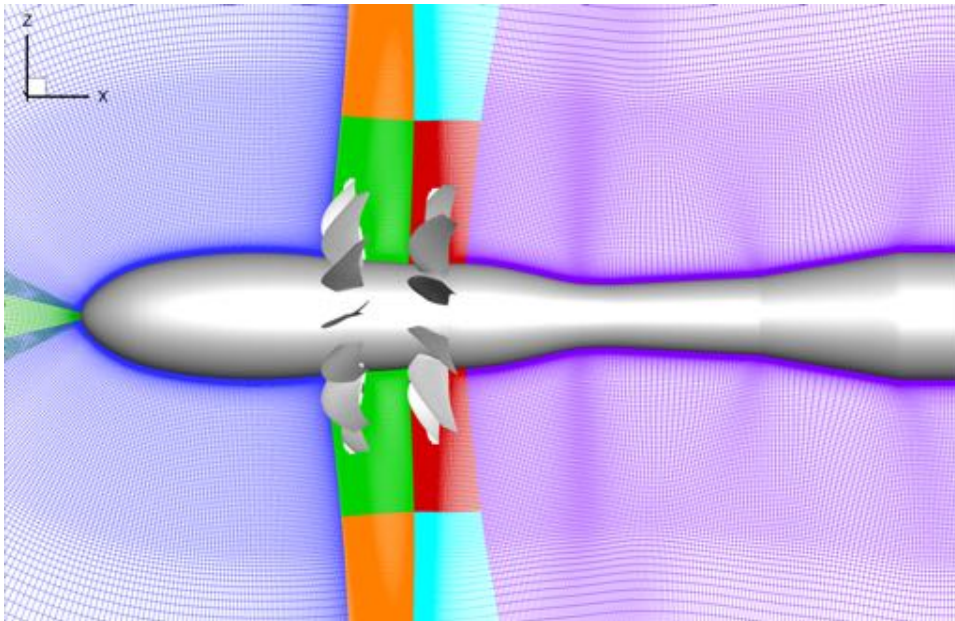
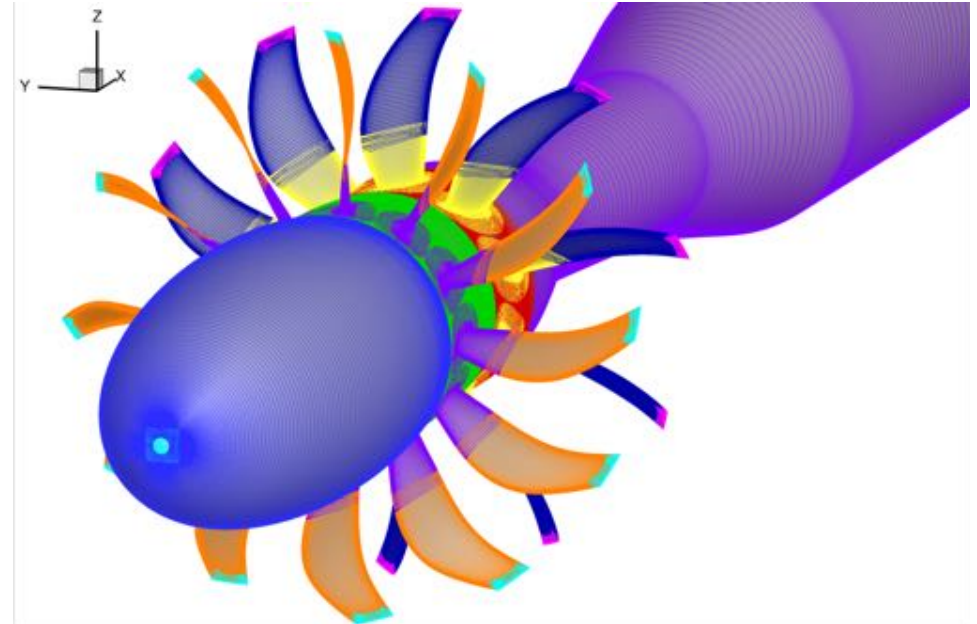
- Mach = 0.78
- Rotation speed = 6848 [RPM]
- Pressure = 101325.353 [Pa]
- Velocity = (265.4709, 0.0, 0.0) [m/s]
- Temperature = 288.15 [K]
- Condition for blades: fwd @ 64.4, aft @ 61.8 degrees
- Sound field measured at 0.43, 0.51, 0.69, 0.87, 1.16 [m]
- Initial runs have no plate or wind-tunnel geometry included  
(plate is included in a subsequent analysis)



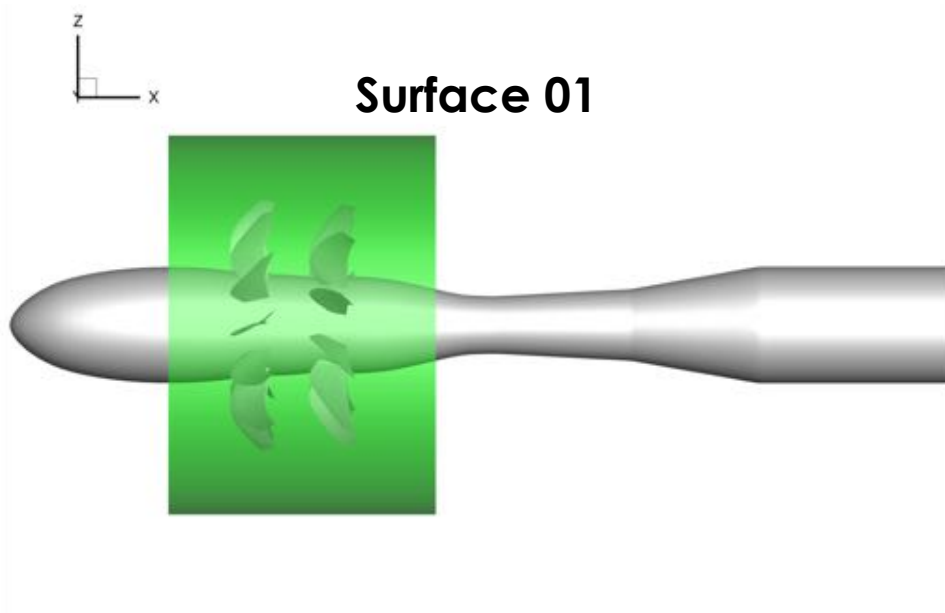
- 3-D Structured Overset Curvilinear Navier-Stokes Solver
- Hybrid RANS/LES using Spalart-Allmaras
- Modified Roe convective flux – 5<sup>th</sup> order WENO reconstruction
- 2<sup>nd</sup> order central differencing for viscous fluxes
- 2<sup>nd</sup> order backward differencing in time ( $dt = 1.2e-05$  s –  $\frac{1}{2}$  deg.)
- Implicit dual-time stepping ( $CFL_{loc} = 10$ ,  $CFL_{Tloc} = 10$ )
  - 20 sub-iterations (approx. 2-3 orders of residual reduction)
  - Alternating Line Jacobi Relaxation (2 sweeps)
- A total of 11 rotor revolutions were simulated from an impulsive start using free-stream conditions (1 rev.  $\approx$  20hrs. on 980 cores)
- Impermeable Ffowcs Williams-Hawkings formulation for far-field propagation from solid surfaces
- SPL Spectral data obtained by averaging 5 segments, each segment contains 4 rotor revolutions with a single rotor revolution overlap

# CROR OVERSET GRID SYSTEM

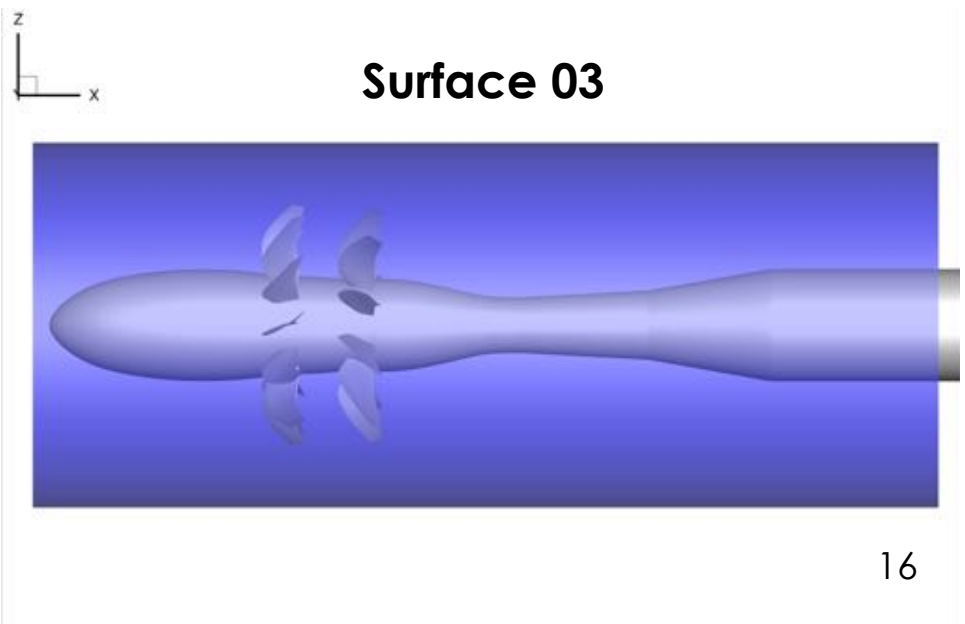
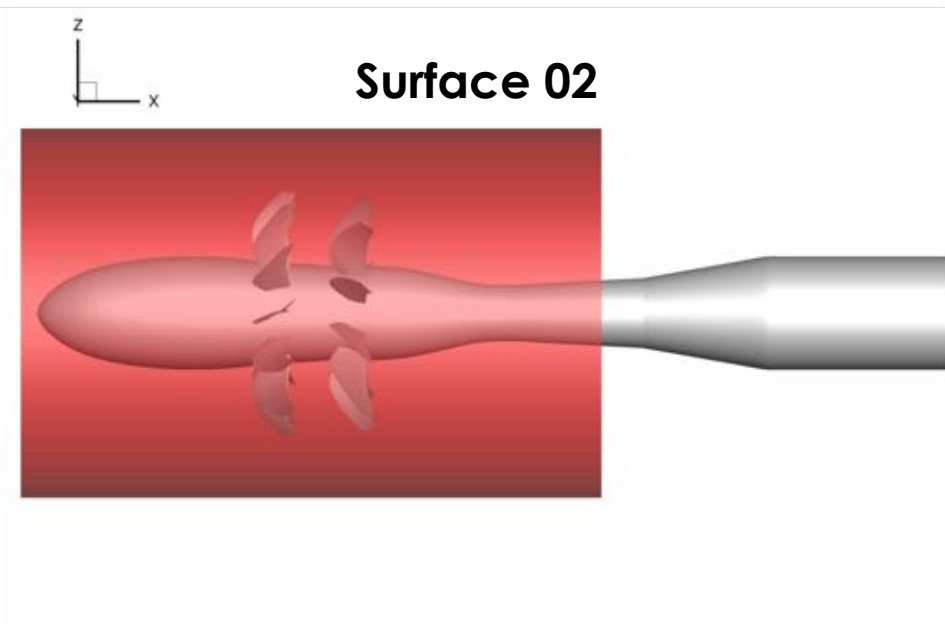
- 123 zones and 164.6 M grid points
- Triple fringe with 0 orphans
- Grid script required < 2 days to make
- Blade deflection angle parameterized
- Grid generation + connectivity 7-10 min.
- Computed  $y^+$  4-5 at blade tip
- $\Delta\theta = 6\text{mm}$   $\Delta r = 7\text{mm}$  near blade tip



# ACOUSTIC PROPAGATION SURFACE

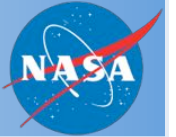


- 3 closed surface triangulations were generated to store unsteady CFD data for acoustic propagation
- An edge length 8.65 mm is used
- Triangulation is labeled with component IDs allowing various combinations of surfaces to be included in propagation

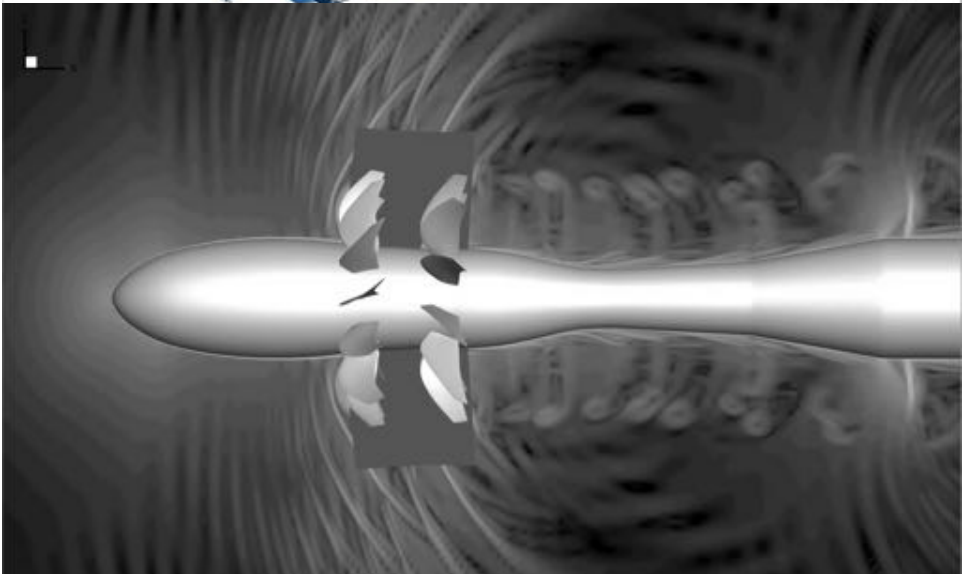
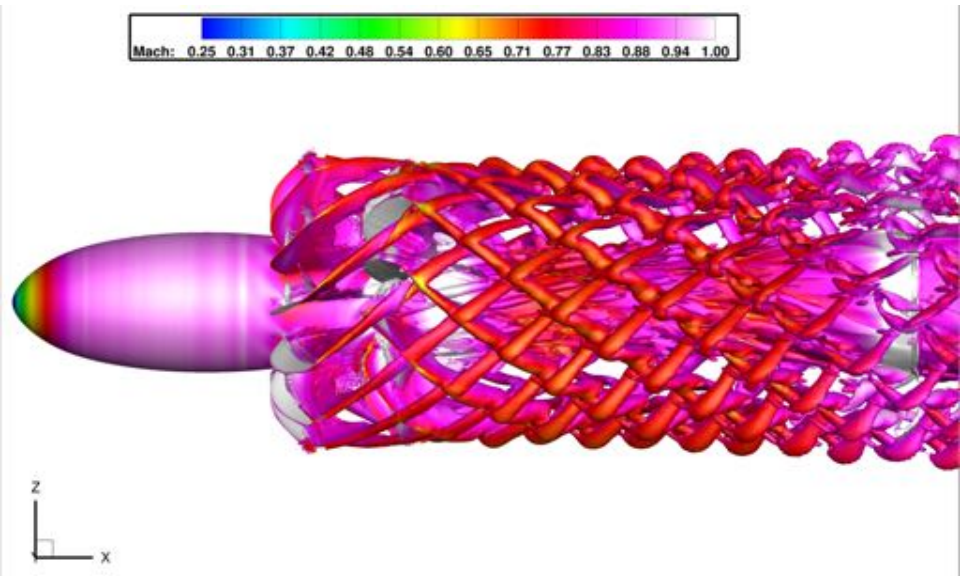
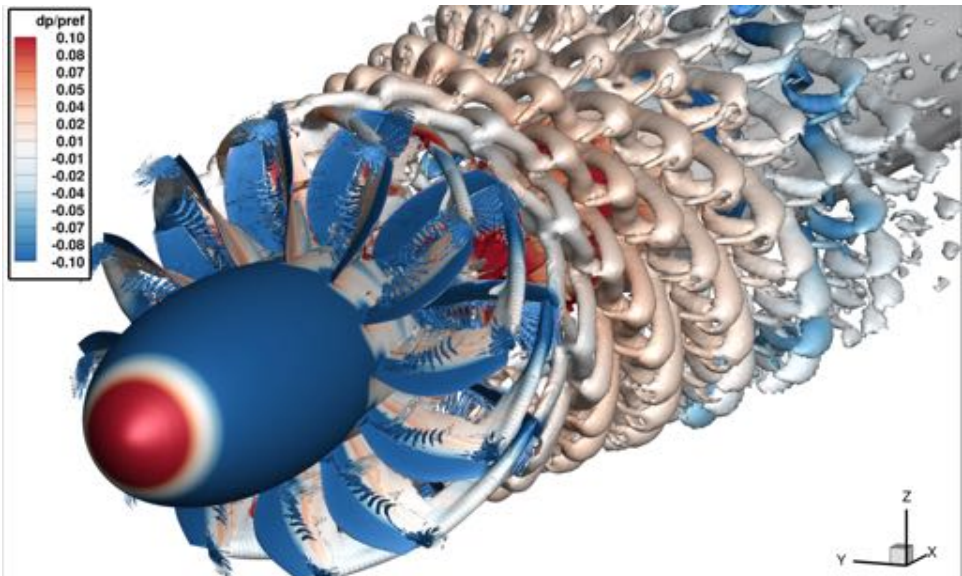




# OVERSET GRIDS – FLOW VISUALIZATION



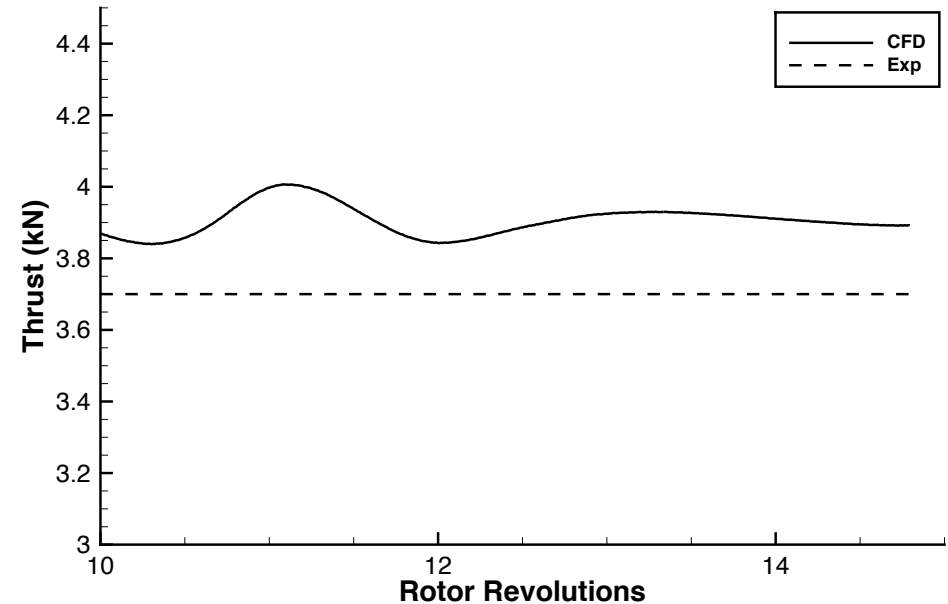
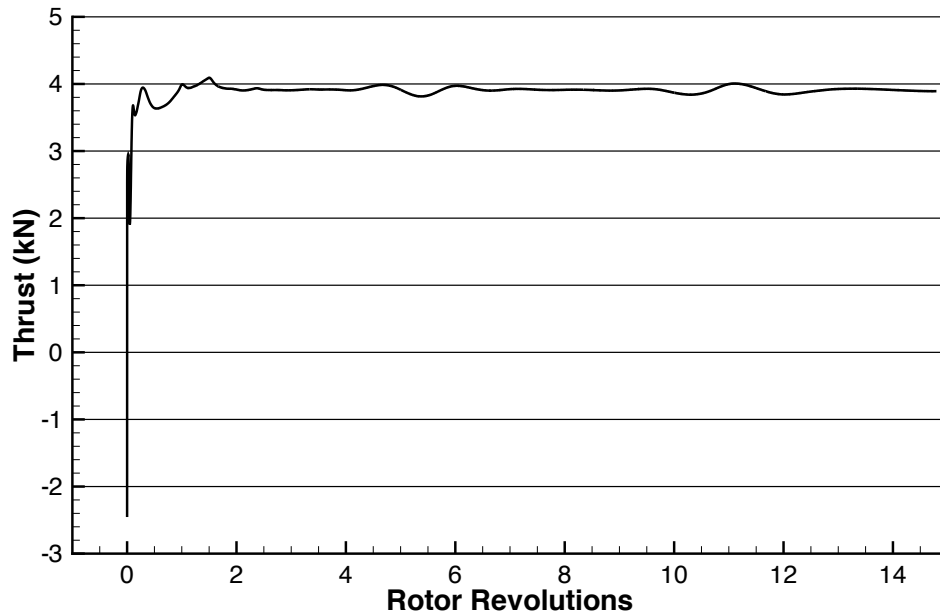
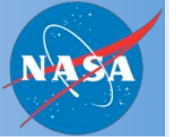
## Iso-contour of vorticity magnitude colored by pressure



## Magnitude of Density Gradient

Acoustic waves generated by the fwd and aft blades propagated in both the upstream and downstream directions and interact with the fish tail shock on the strut of the hub

# OVERSET – TIME HISTORY OF THRUST



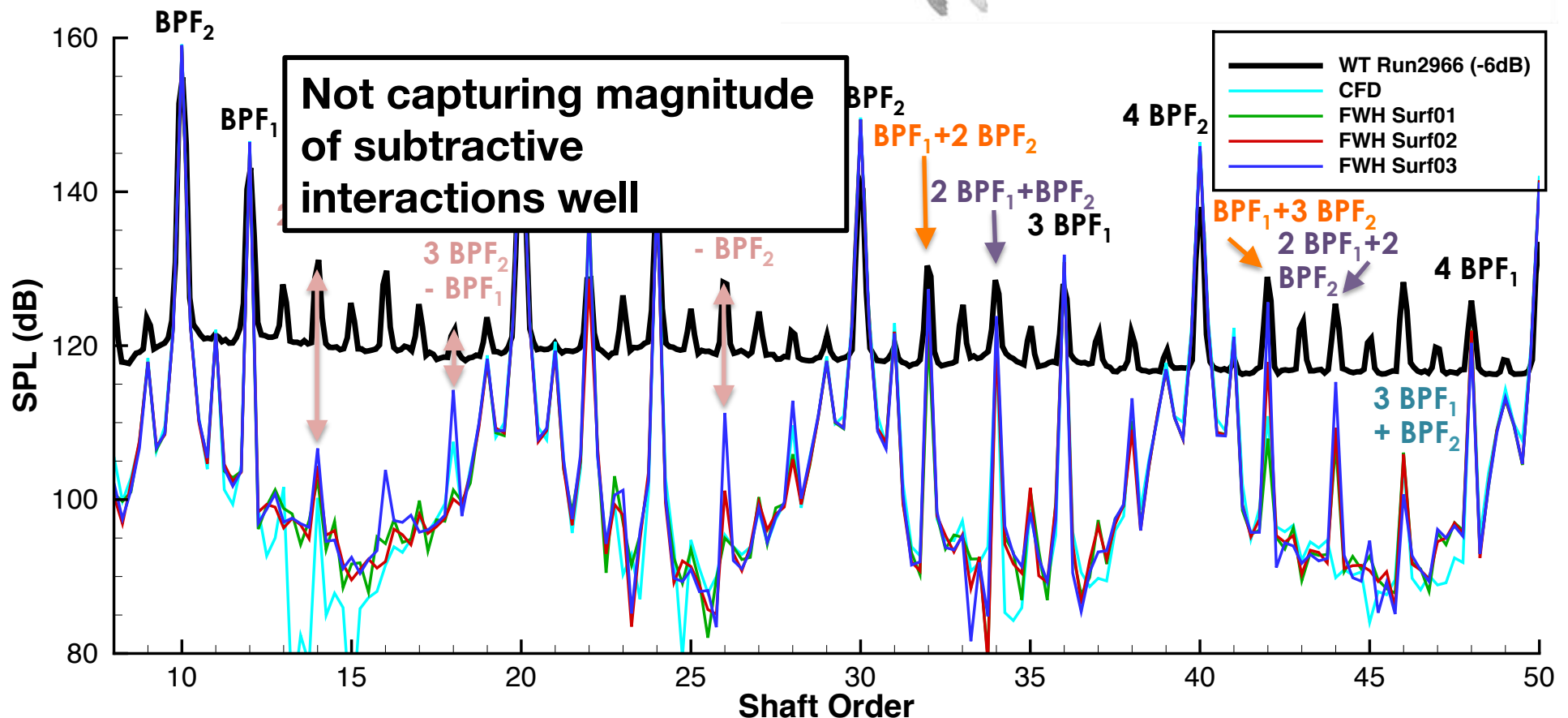
- Time-averaged thrust appears slightly larger than the WT data
- Computed  $y^+$  near the blade tips are between 4 and 5 causing an under-prediction of the viscous contribution leading to larger thrust
- Small oscillations appearing every 4.5 to 5 rotor revolutions is caused by inflow boundary condition reflection effects (these effects have been reduced using highly stretched far-field grid and non-reflecting BCs)

# OVERSET – SPL SPECTRAL COMPARISON



- Capturing  $n\text{BPF}_1$  and  $n\text{BPF}_2$  ( $n \leq 4$  and higher)
- Capturing  $\text{BPF}_1 + \text{BPF}_2$ ,  $\text{BPF}_1 + 2 \text{BPF}_2$ ,  $2 \text{BPF}_1 + \text{BPF}_2$ , and  $\text{BPF}_1 + 3 \text{BPF}_2$
- Loss of magnitude at  $3 \text{BPF}_1 + \text{BPF}_2$

Kulite 9 H = 0.51m

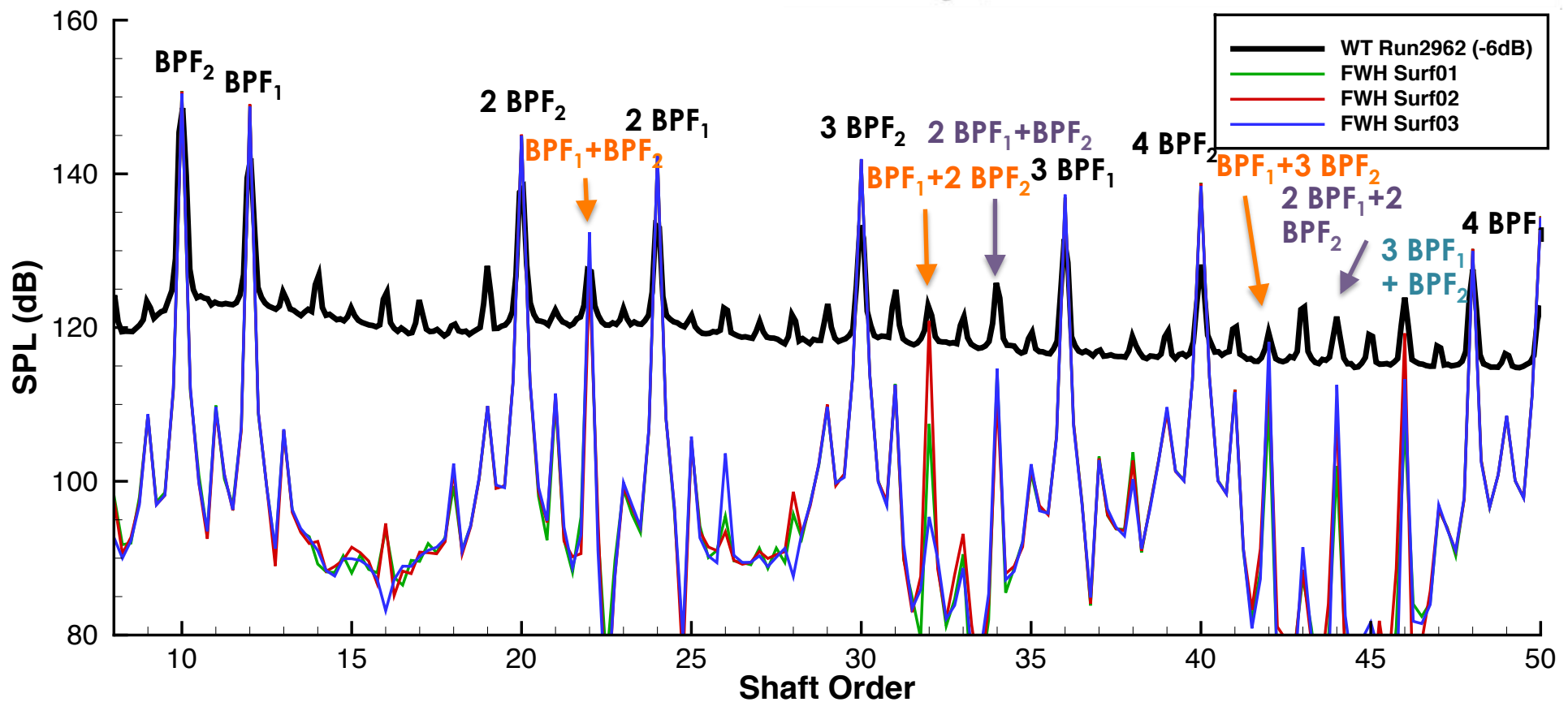


# OVERSET – SPL SPECTRAL COMPARISON

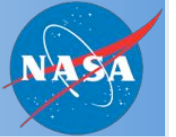


- Acoustic surface 2 appears to provide the best comparison at interaction frequencies
- $2BPF_1+2BPF_2$  and greater interaction amplitudes not well captured

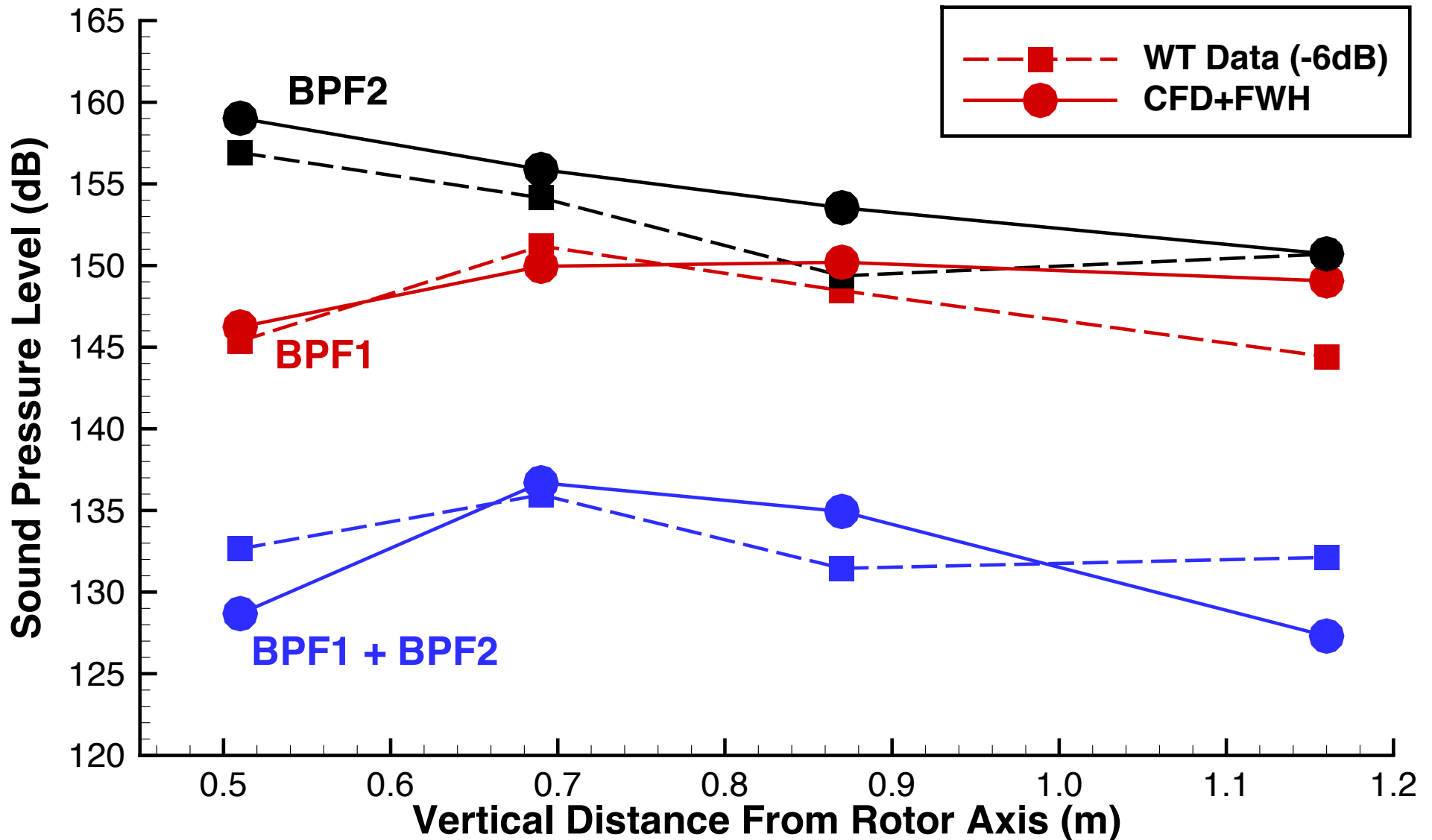
Kulite 9 H = 1.16m



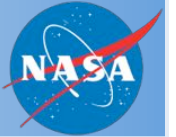
# OVERSET – SPL TONE COMPARISON



## Kulite 9

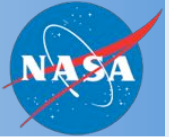


# OVERSET - TIME-STEP RESOLUTION STUDY

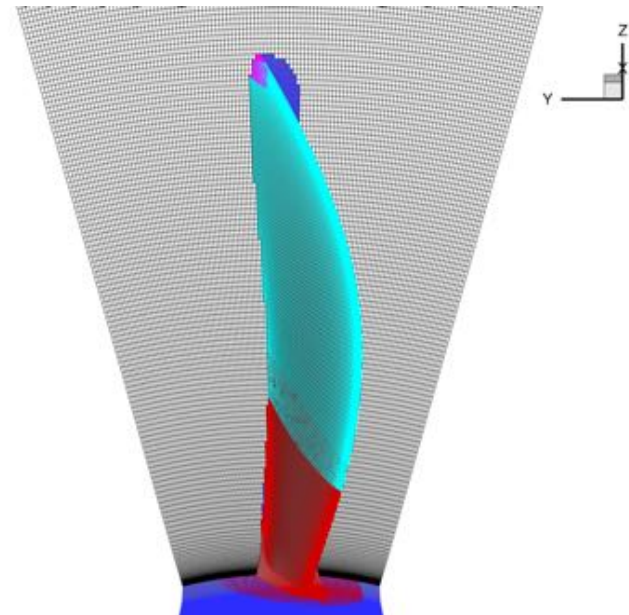
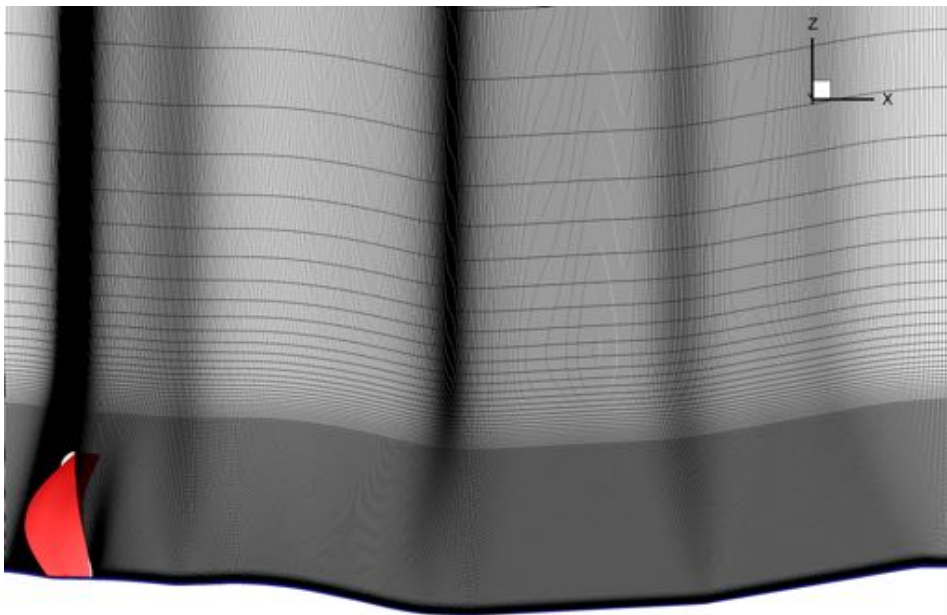
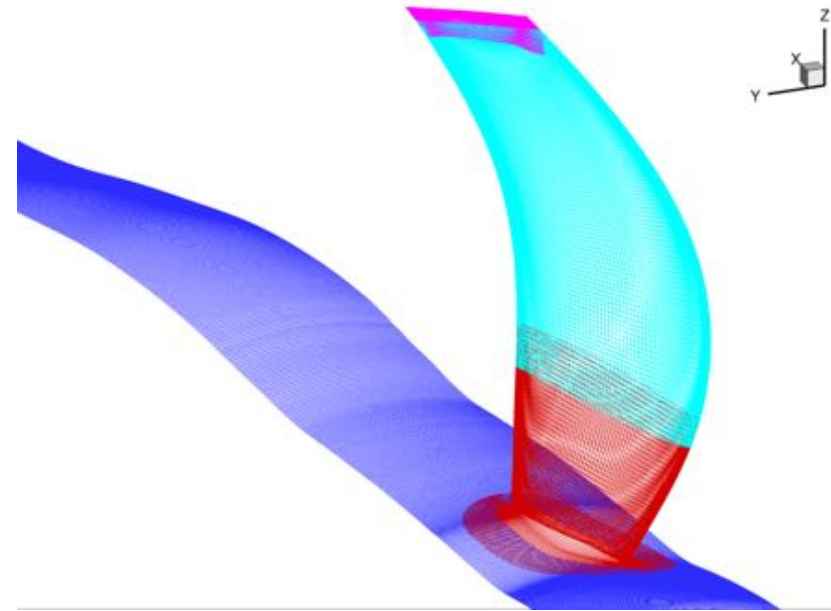


- Curvilinear solver utilized implicit 2<sup>nd</sup> order backward differencing in time allowing large time-steps to be utilized while maintaining stable solutions with viscous meshes
- When utilizing high-resolution spatial discretizations, temporal error discretization may dominate if too large a time-step is used
- A time-step resolution study for a single forward rotor (modeling 1/12<sup>th</sup> of the geometry) was performed to determine an accurate time-step for the finest mesh open rotor calculation
- Outline of the study:
  - Geometry and overset grid description
  - Numerical discretization and solver parameters
  - Simulation results
  - Conclusions
- Recent enhancements implemented in the Curvilinear LAVA code to be used in future Open Rotor simulations

# GEOMETRY AND OVERSET GRID



- Single forward blade mounted on hub with cylindrical extension (1/12<sup>th</sup> model)
- 11 zones, 52.1 M points
- Triple fringe (no orphans)
- Entire grid rotates (no relative motion)



# DISCRETIZATION AND SOLVER PARAMETERS



- LAVA structured overset grid curvilinear Navier-Stokes solver
- Hybrid RANS/LES using Spalart-Allmaras
  - Unsteady Reynolds Averaged Navier-Stokes (URANS)
  - Manual specification of RANS/LES interface based on URANS
  - Delayed Detached Eddy Simulation (DDES)
- Modified Roe convective flux – 5<sup>th</sup> order reconstruction
- 2<sup>nd</sup> order central differencing for viscous flux
- 2<sup>nd</sup> order backward differencing in time
  - $dt = 1.217e-05$  seconds (1/2 deg.)
  - $dt = 6.085e-06$  seconds (1/4 deg.)
  - $dt = 3.042e-06$  seconds (1/8 deg.)
  - $dt = 1.521e-06$  seconds (1/16 deg.)
  - $dt = 7.606e-07$  seconds (1/32 deg.)
- Strict 2-orders of magnitude residual reduction each physical time-step (requires different number of sub-iterations for each dt)
- 3.5 - 5 rotor revolutions completed for each case

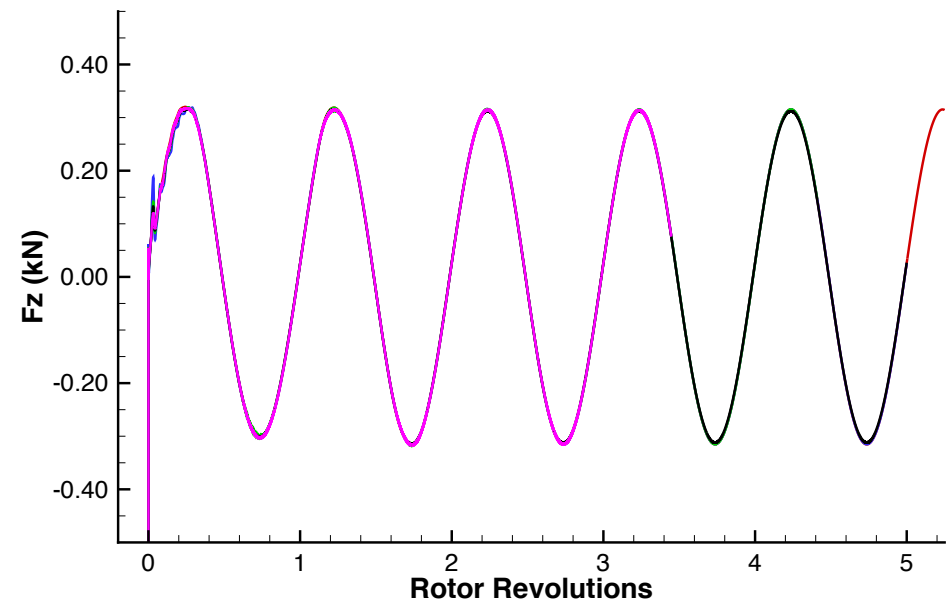
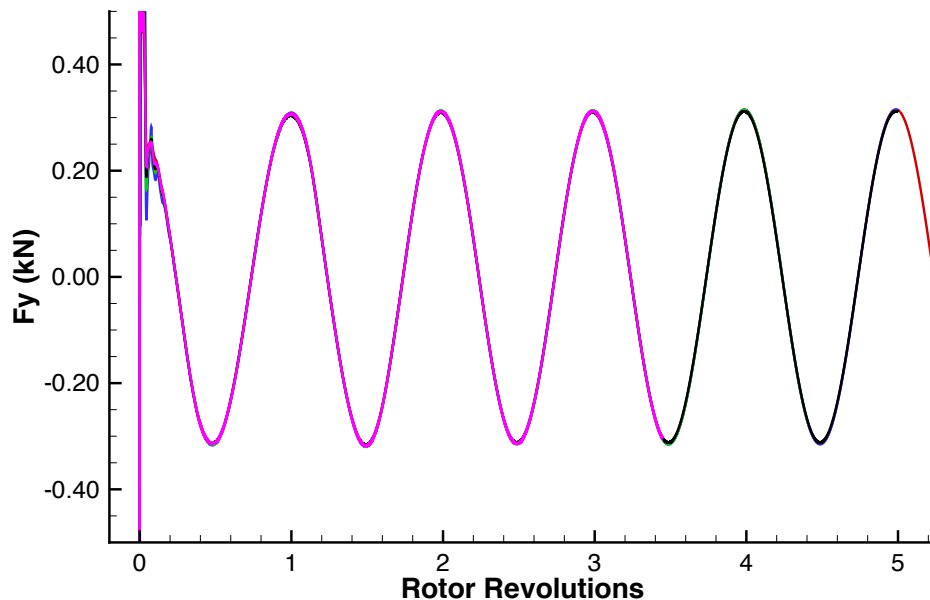
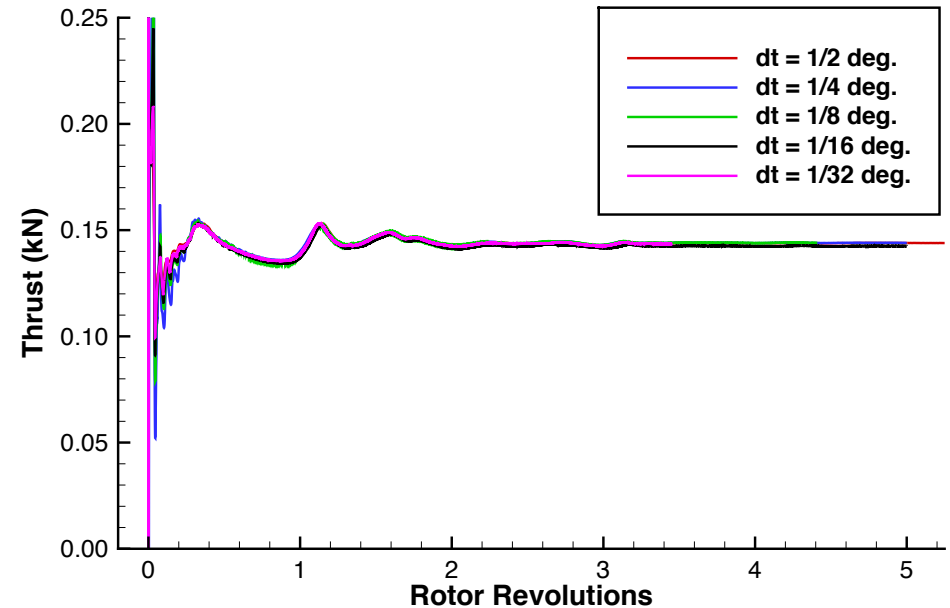


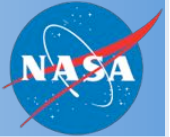
# TIME-STEP RESOLUTION RESULTS



## Single Forward Blade Loads

- Thrust appears to converge within 3.5 to 4 rotor revs
- Almost no difference is observed in the predicted loads with respect time-step changes

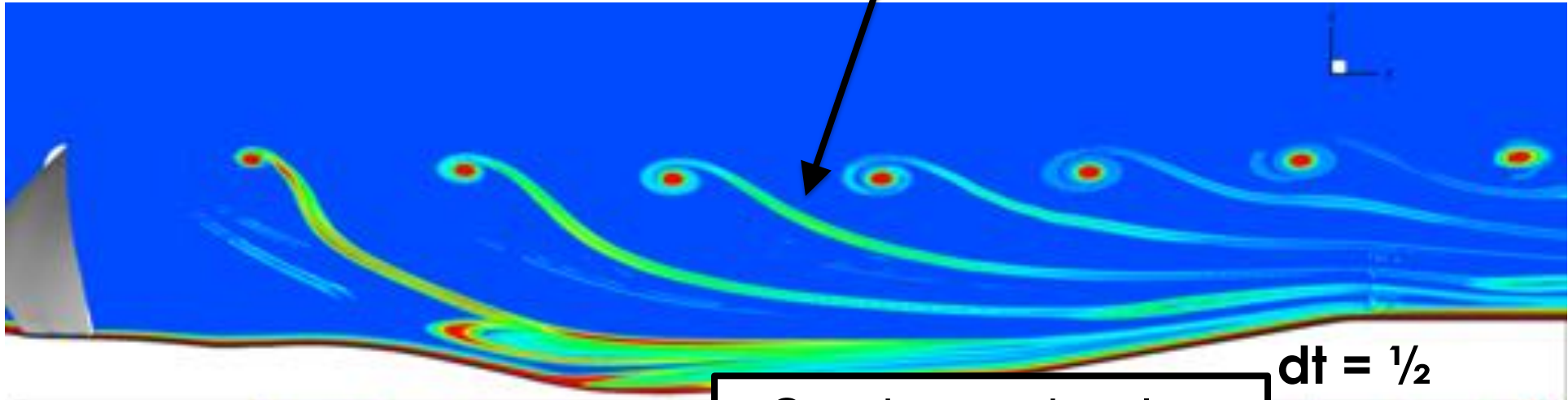




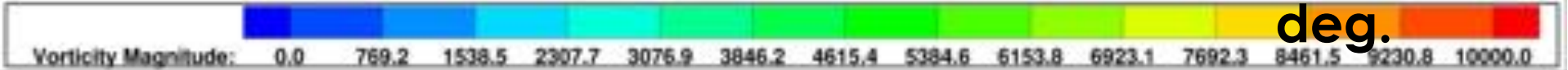
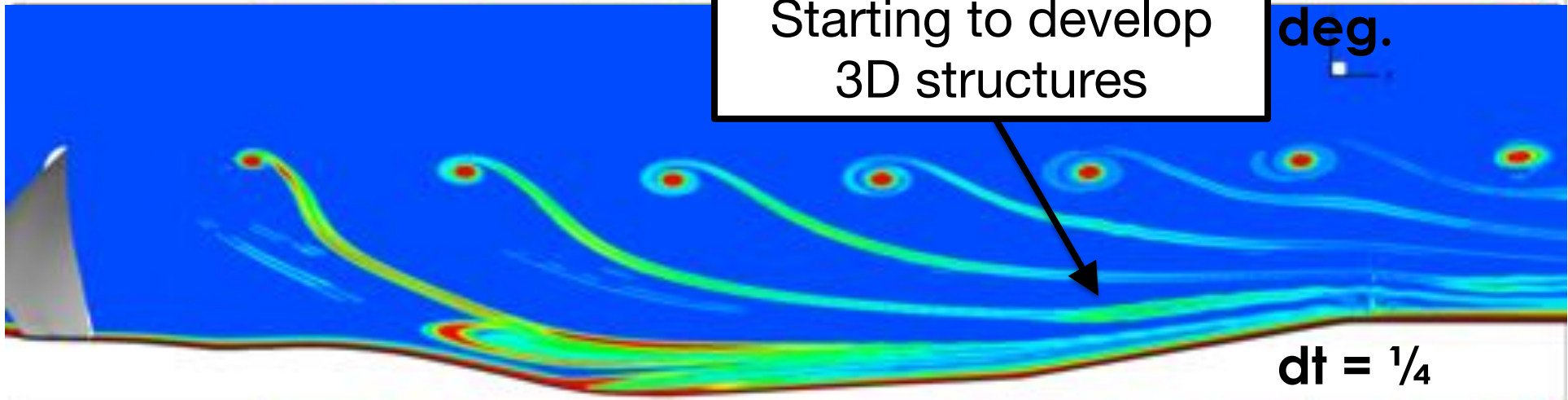
# TIME-STEP RESOLUTION RESULTS

## *Wake Resolution Time-Step Sensitivity*

Very Smooth Structures



Starting to develop 3D structures

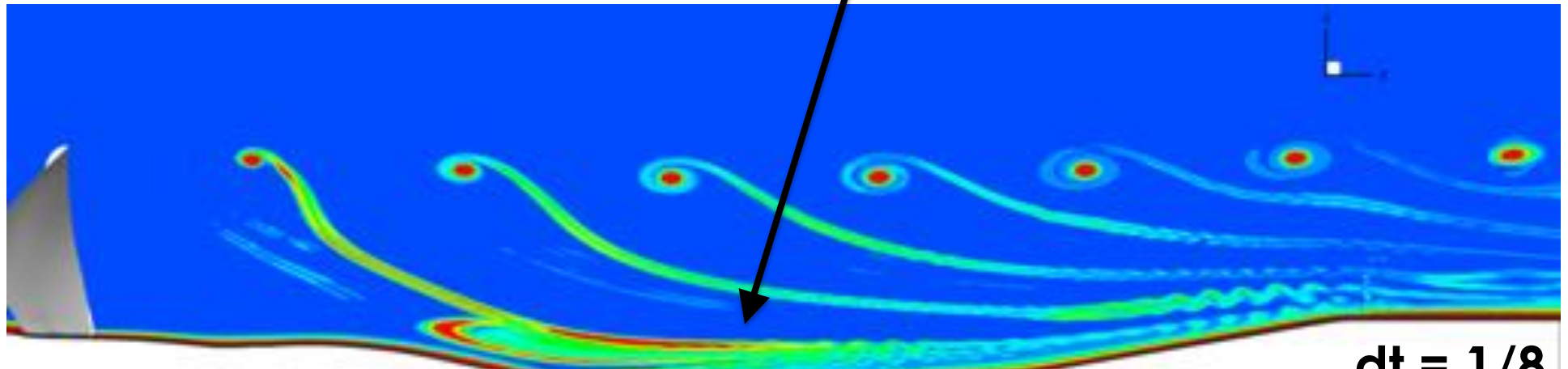




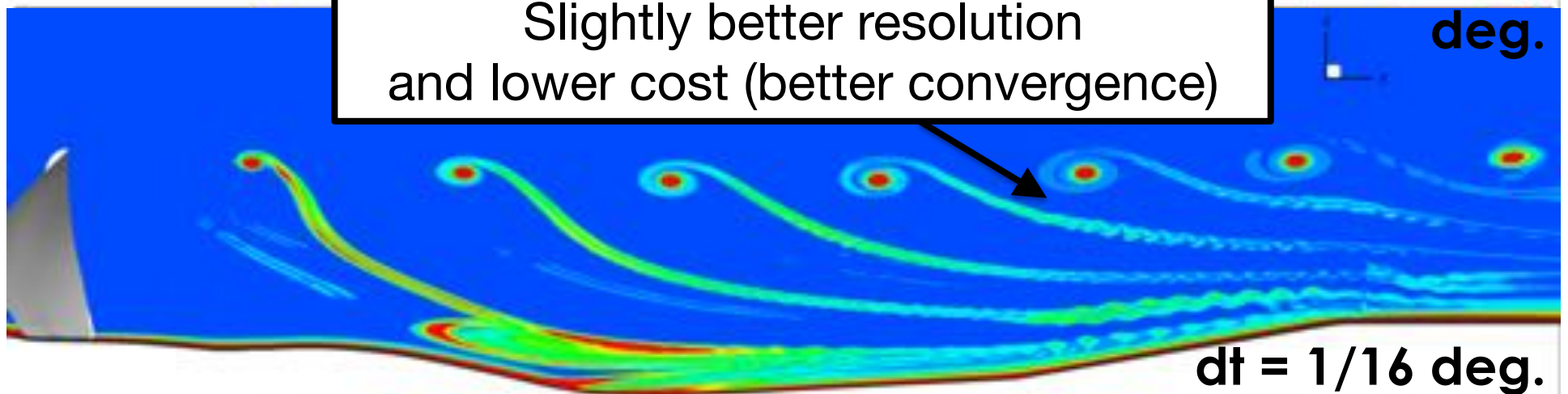
# TIME-STEP RESOLUTION RESULTS

## *Wake Resolution Time-Step Sensitivity*

Earlier Development



Slightly better resolution and lower cost (better convergence)

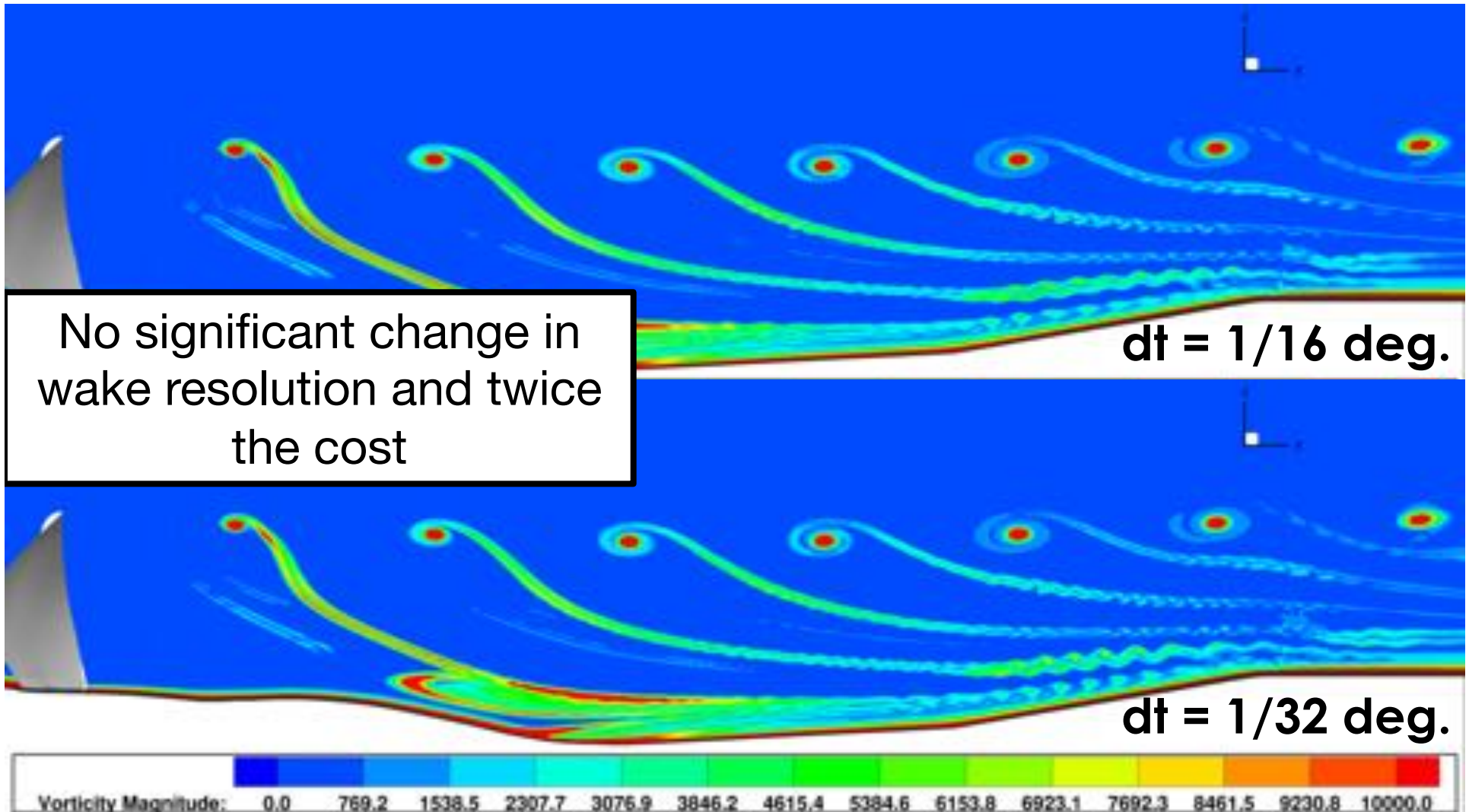


Vorticity Magnitude: 0.0 769.2 1538.5 2307.7 3076.9 3846.2 4615.4 5384.6 6153.8 6923.1 7692.3 8461.5 9230.8 10000.0

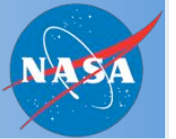
# TIME-STEP RESOLUTION RESULTS



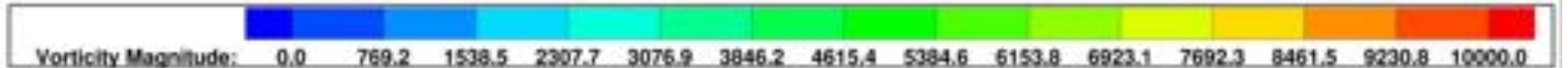
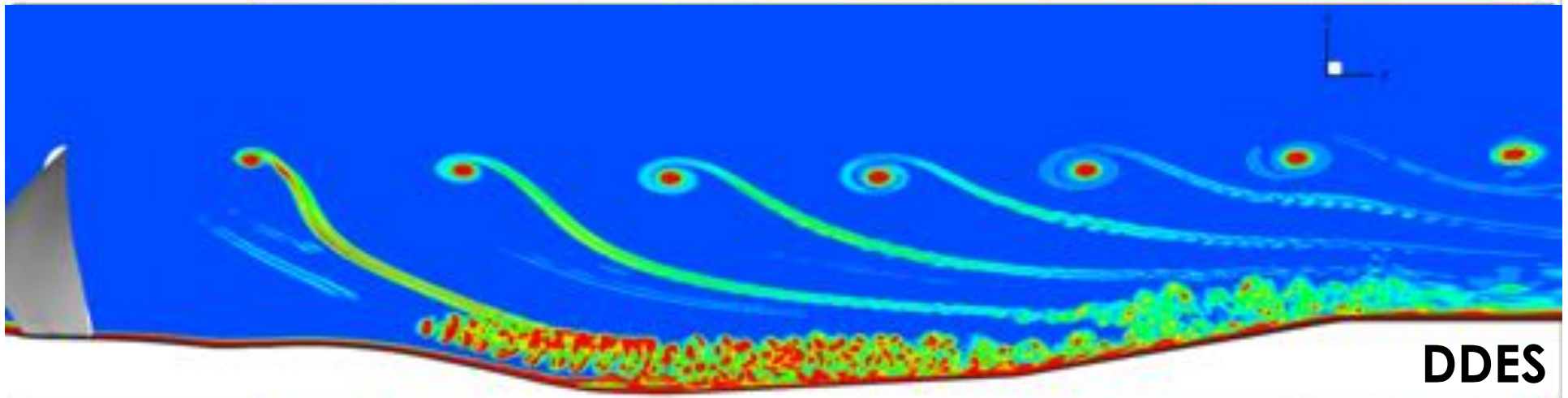
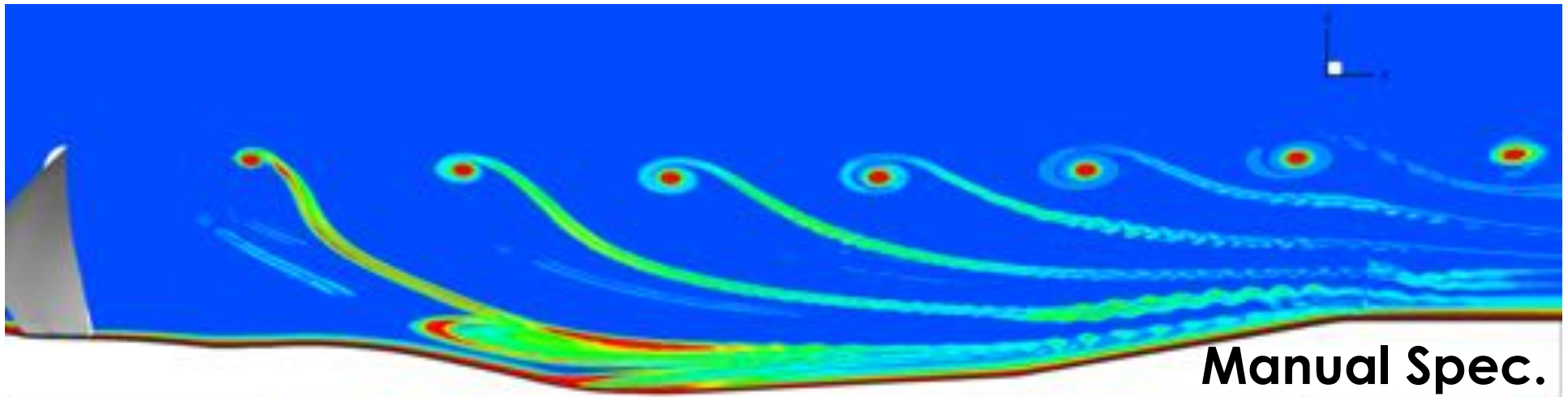
## *Wake Resolution Time-Step Sensitivity*



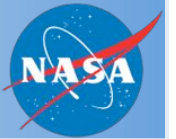
# TIME-STEP RESOLUTION RESULTS



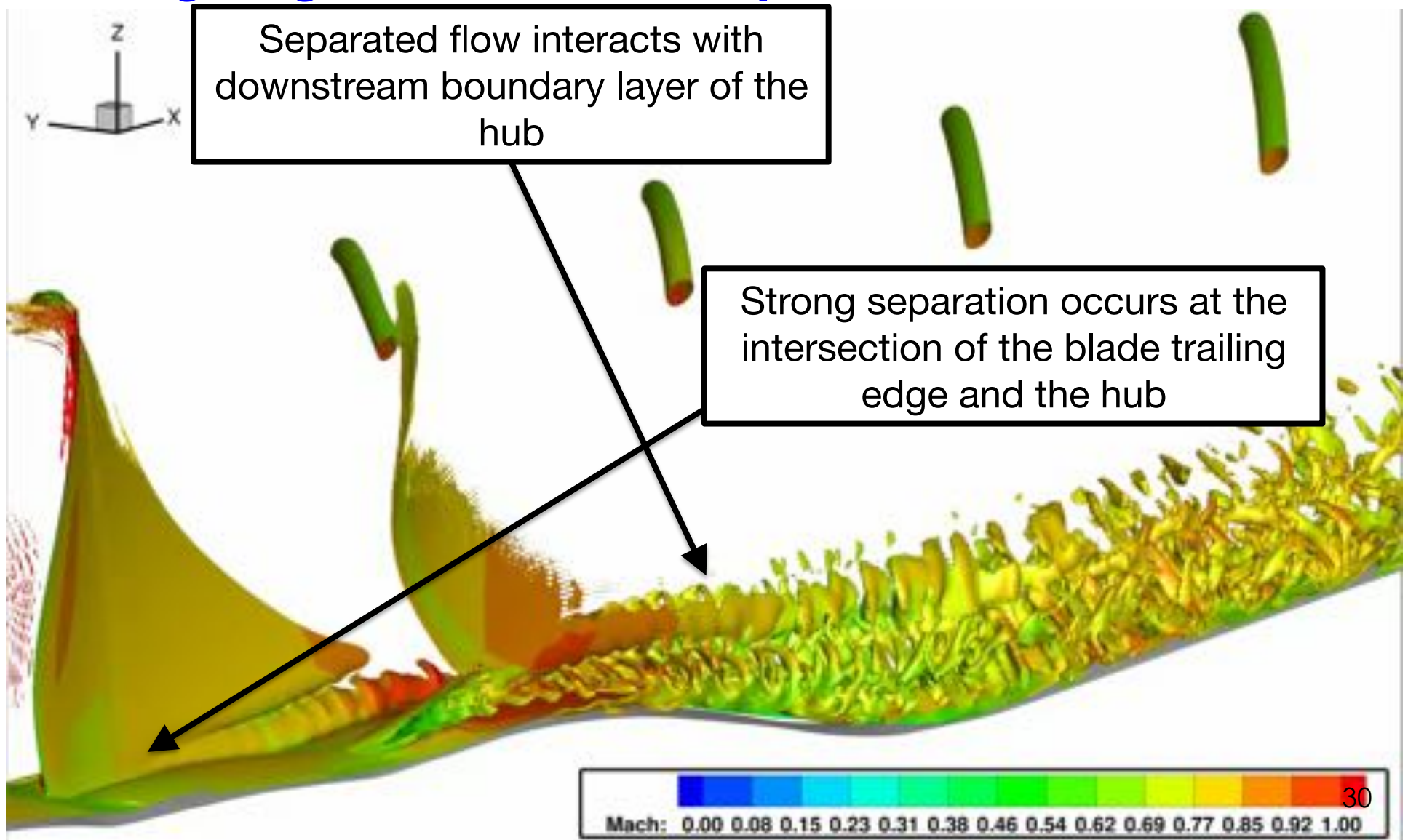
## *Wake Resolution Turbulence Model Sensitivity* ( $dt = 1/16$ deg.)



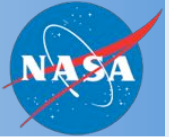
# TIME-STEP RESOLUTION RESULTS



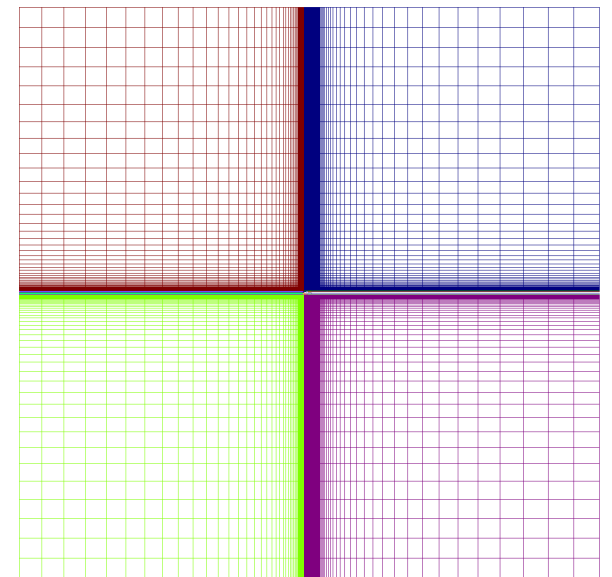
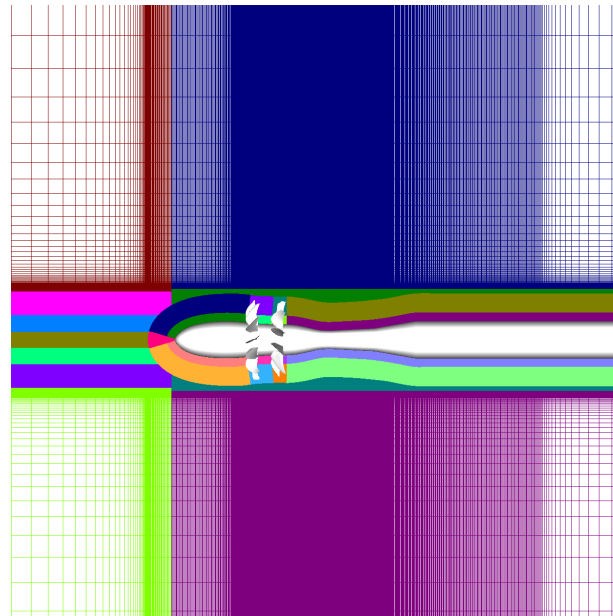
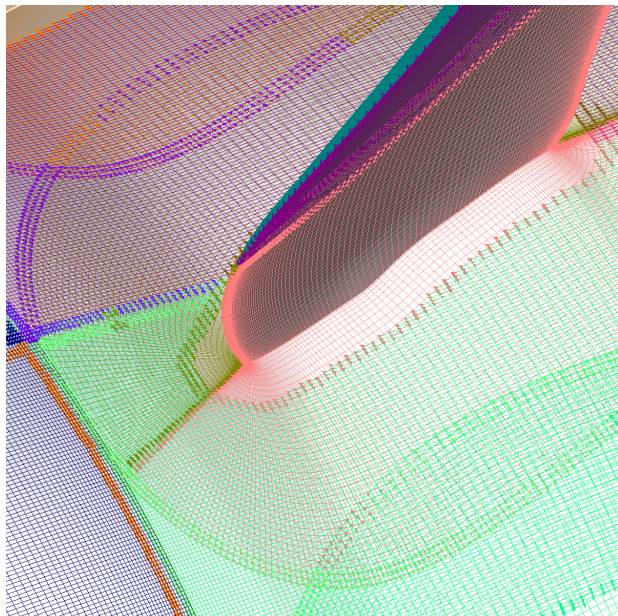
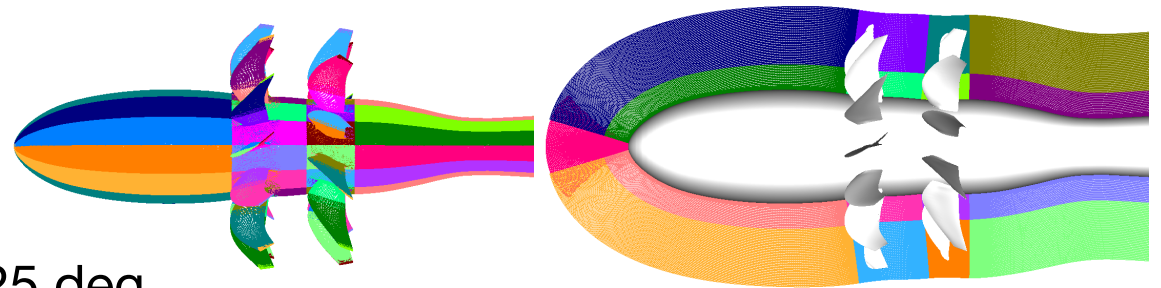
## *Trailing Edge/Hub Corner Separation*



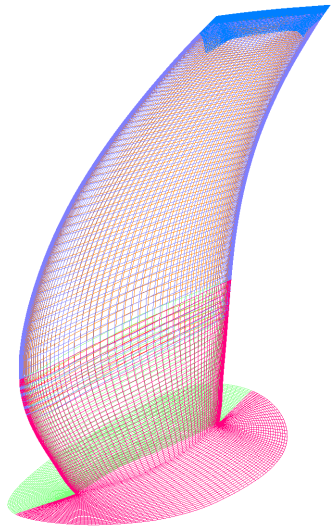
# FINE MESH OVERSET GRID SYSTEM



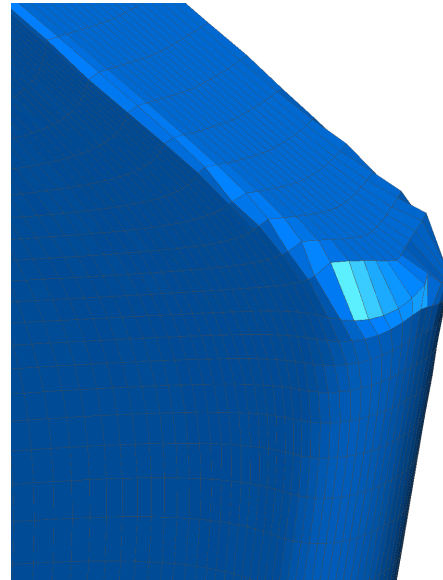
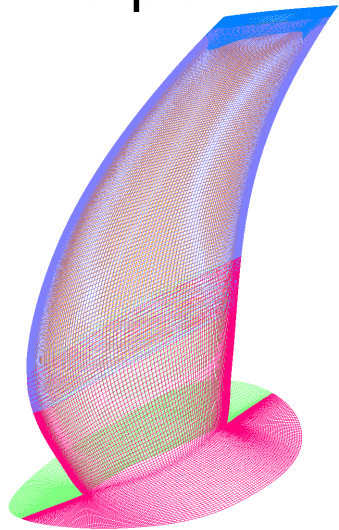
- 268 zones, 836.7 M points
- Triple fringe layer
- No orphans
- Finer wall spacing for  $y^+ < 1$
- Extended farfield
- Improved blade grids
- Circumferential spacing  $< 0.25$  deg.



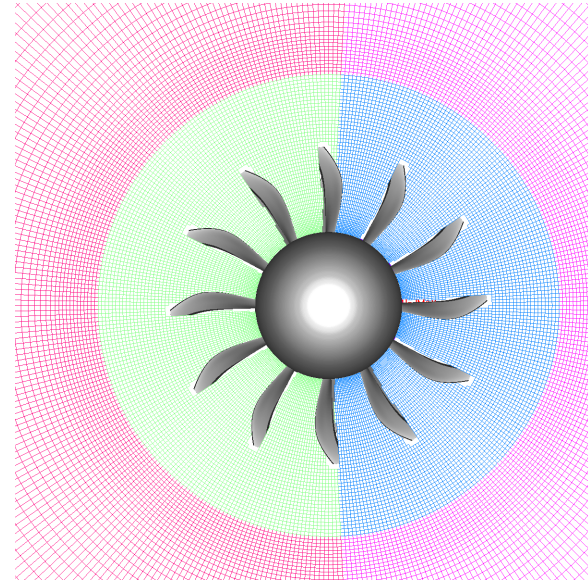
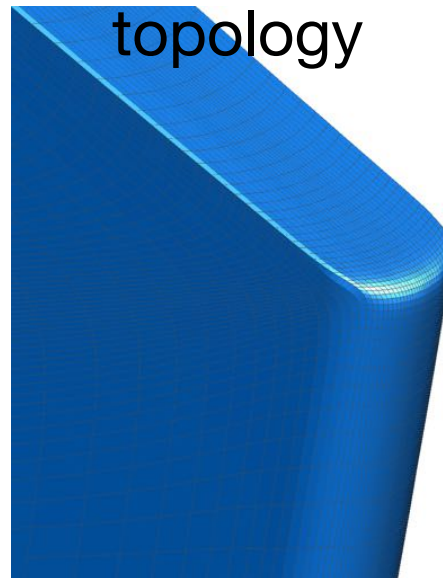
# FINE MESH OVERSET GRID SYSTEM



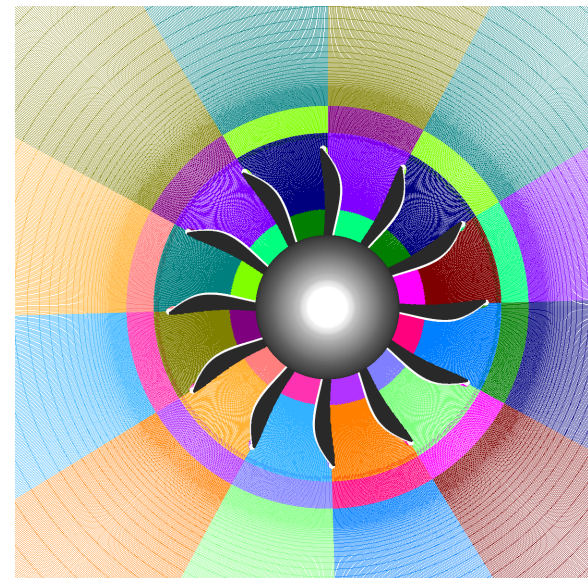
5.5 M to 10.6 M  
points per blade



Improved  
topology



Highly Refined



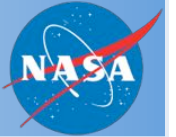
Old

New

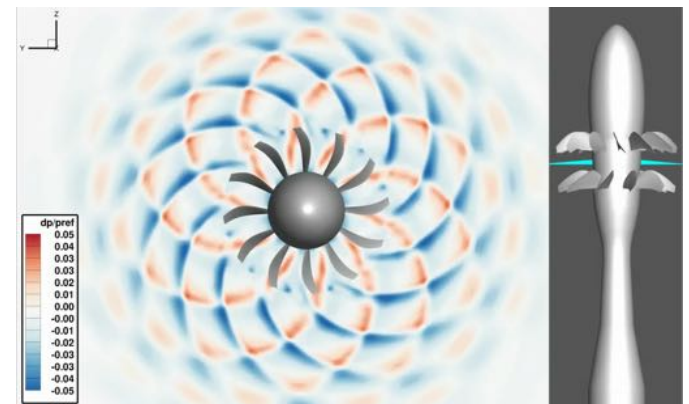


# SUMMARY AND FUTURE WORK

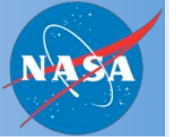
## LAVA STRUCTURED OVERSET



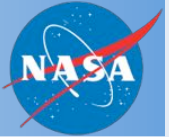
- Algorithm improvements:
  - Far-field BCs and Grid-Stretching Strategy to reduce reflections
  - High-order Blended Upwind/Central Variable Interpolation
- Lessons Learned:
  - Smaller time-step ( $1/16^{\text{th}}$  deg.) leads to more accuracy and efficiency with increased sub-iteration convergence
  - Utilization of DDES model with improved length scale increases the resolution capacity of the grid and reduces delay in the development of 3D turbulent structures
- Open rotor simulations:
  - High speed case
    - Coarse mesh (164M) complete
    - Fine mesh (837M) in progress
  - Low speed case
    - Fine mesh (837M) in progress



# OUTLINE



- *LAVA (Launch Ascent Vehicle Aerodynamics)*
  - *Introduction*
  - *Acoustics Related Applications*
- *LAVA Applications to Open Rotor*
  - *Structured Overset Grids*
  - *Cartesian Grid with Immersed Boundary*
    - *High Speed Case*
    - *High Speed Case with Plate*
    - *Low Speed Case*

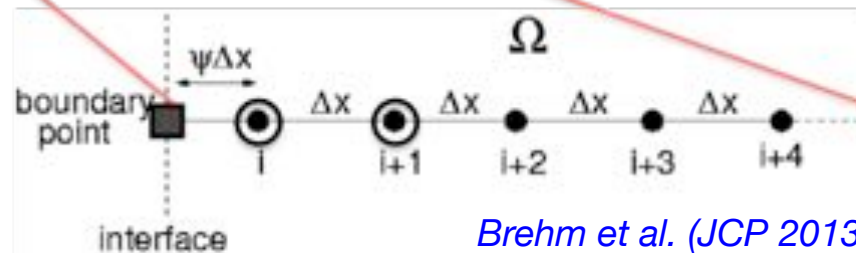
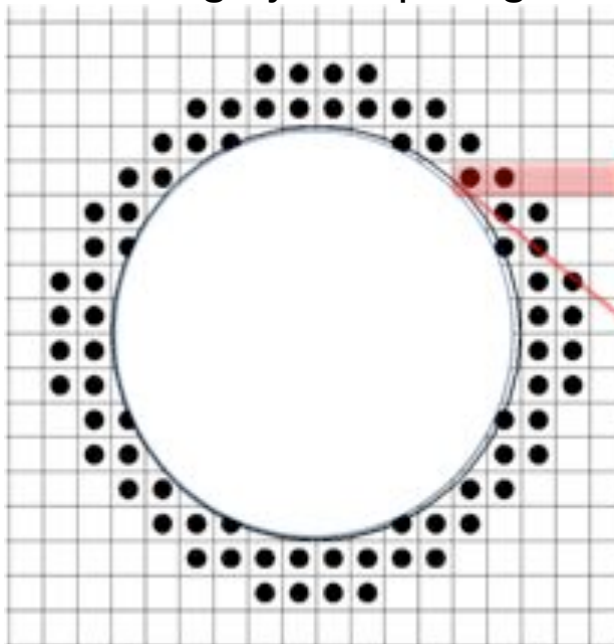
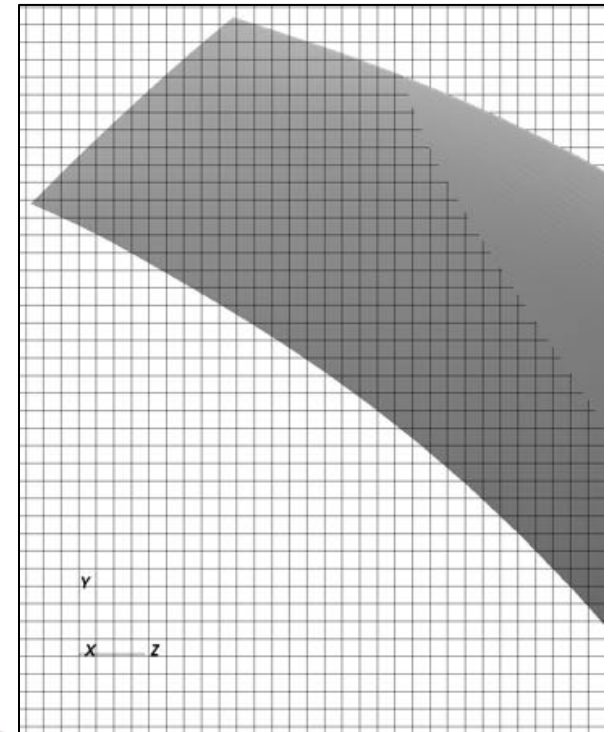


- *Computational Approach:*
- 3D Cartesian Navier-Stokes Solver
- 5<sup>th</sup> and 6<sup>th</sup> order WENO spatial discretization
- Higher-order immersed boundary method
- 4<sup>th</sup> order explicit Runge-Kutta time stepping ( $dt = 1/16$  degree)
- Rotor revolutions are simulated from an impulsive start using free-stream conditions
- Advanced post-processing used final rotor revolutions

# CARTESIAN IMMERSED-BOUNDARY



- Sharp interface immersed-boundary representation of geometry
- Boundary condition imposed at grid line intersection points
- No ghost cells needed inside body (thin body capturing capability)
- Stencil optimized for stability and higher-order accuracy
- Parallel geometry kernels are implemented:
  - Inside-outside testing by multi-resolution binning
  - Exact distance to surface triangulation (including point to plane and point to edge cases)
- Excellent for highly complex geometry, and AMR

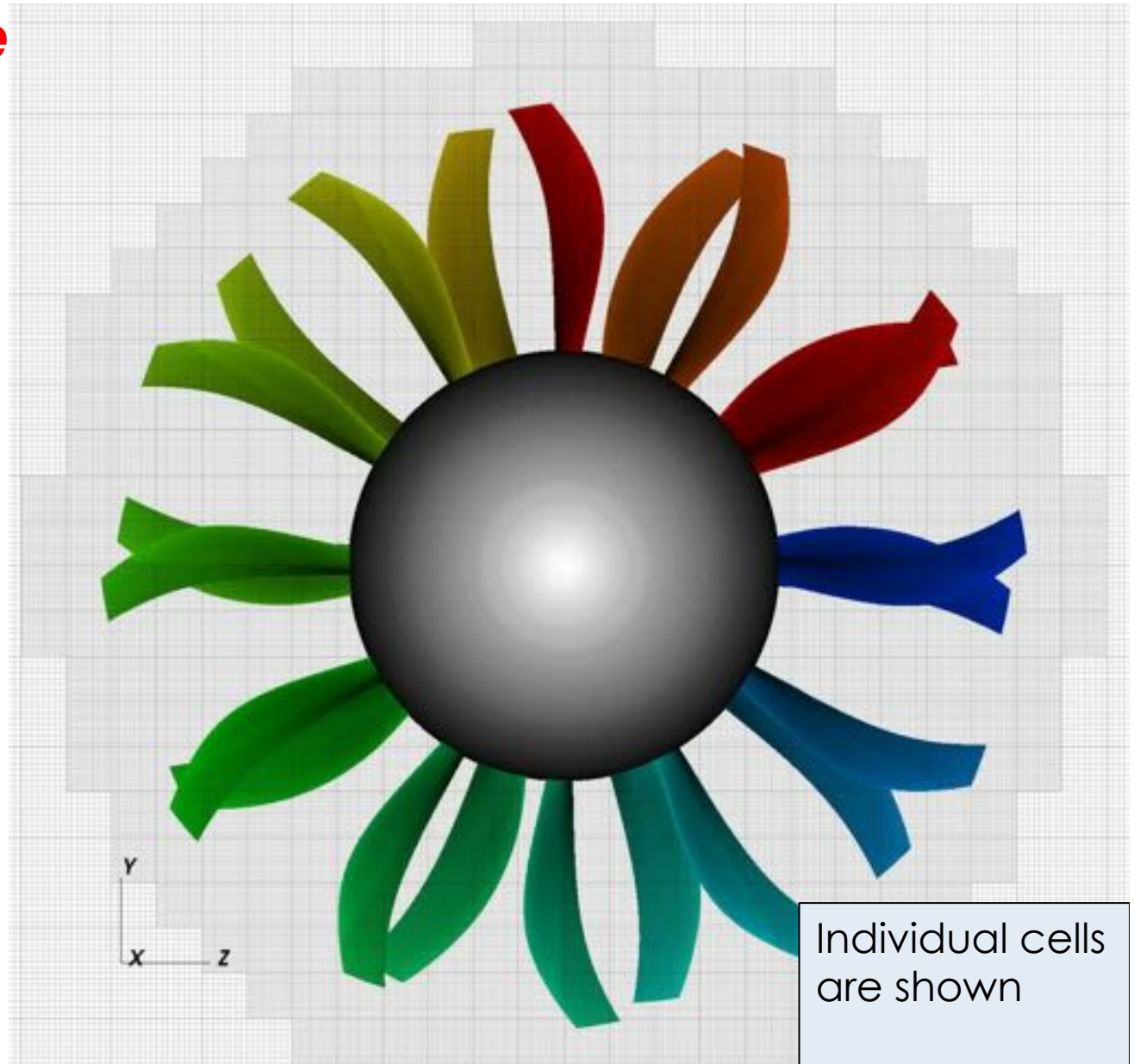


*Brehm et al. (JCP 2013,2015)*

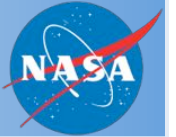
## *High Speed Case*

### *Grid System*

- 35846 zones and 146.8 M grid points
- No manual volume gridding, only surface triangulation required
- $\Delta x = 2\text{mm}$  near blades,  $\Delta x = 4\text{mm}$  in wake region

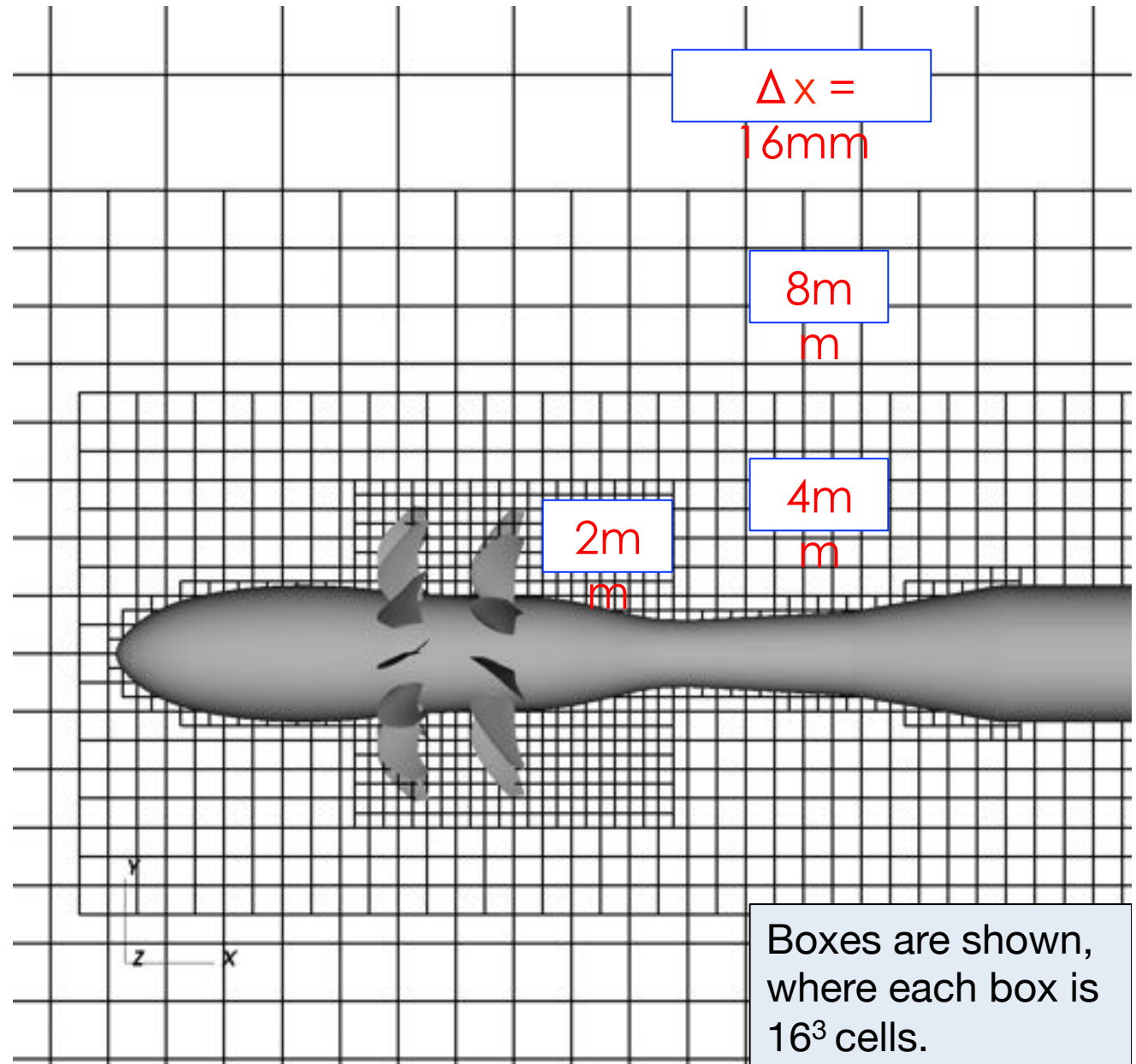


# CARTESIAN GRID WITH MOVING OR GEOMETRY

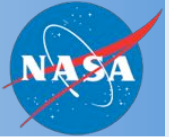


## Grid System

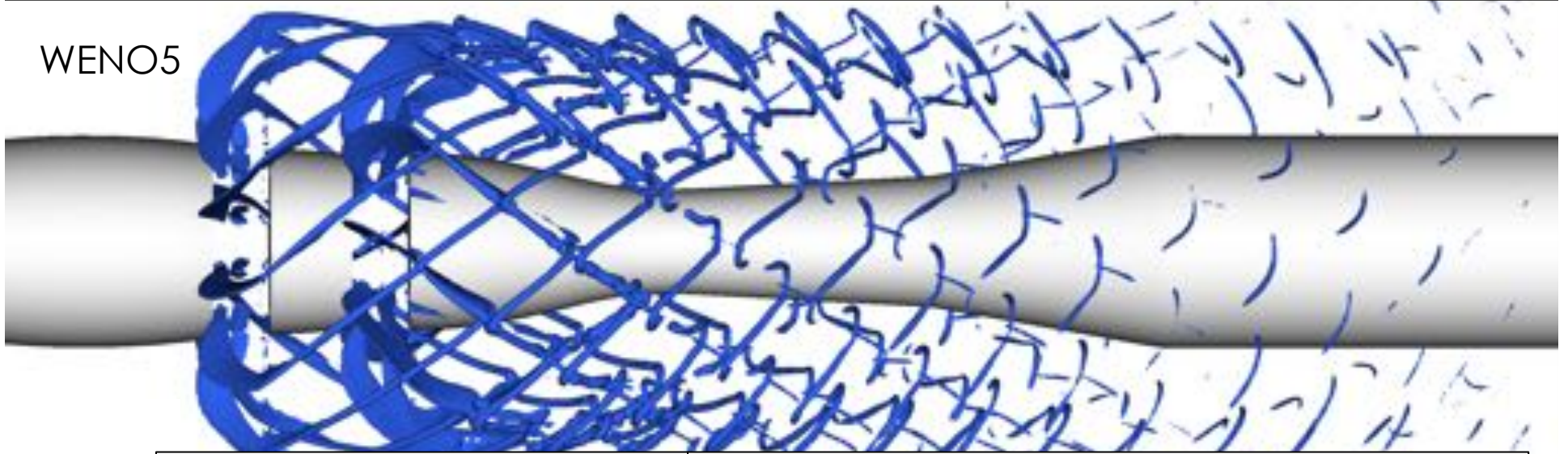
- 35846 zones and 146.8 M grid points
- No manual volume gridding, only surface triangulation required
- $\Delta x = 2\text{mm}$  near blades,  $\Delta x = 4\text{mm}$  in wake region



# LAVA CARTESIAN : WENO5 vs WENO6



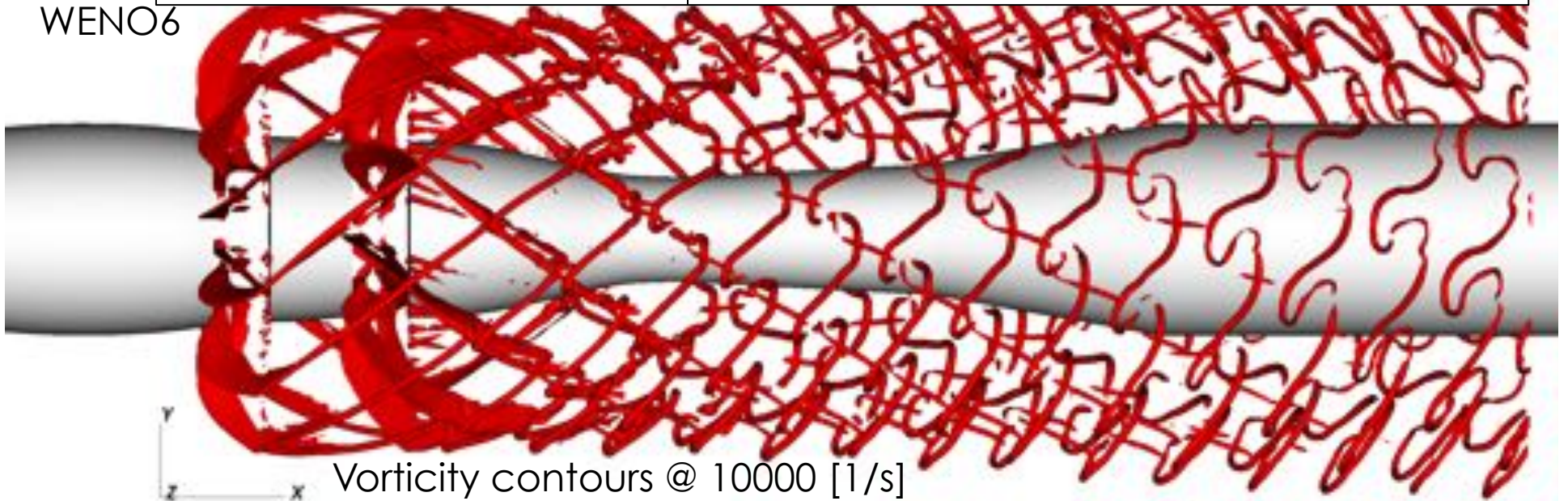
WENO5



2mm

4mm

WENO6



Vorticity contours @ 10000 [1/s]

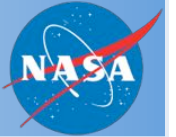
# LAVA CARTESIAN : WENO6 VORTICITY



Vorticity contours @ 10000 [1/s], colored by pressure

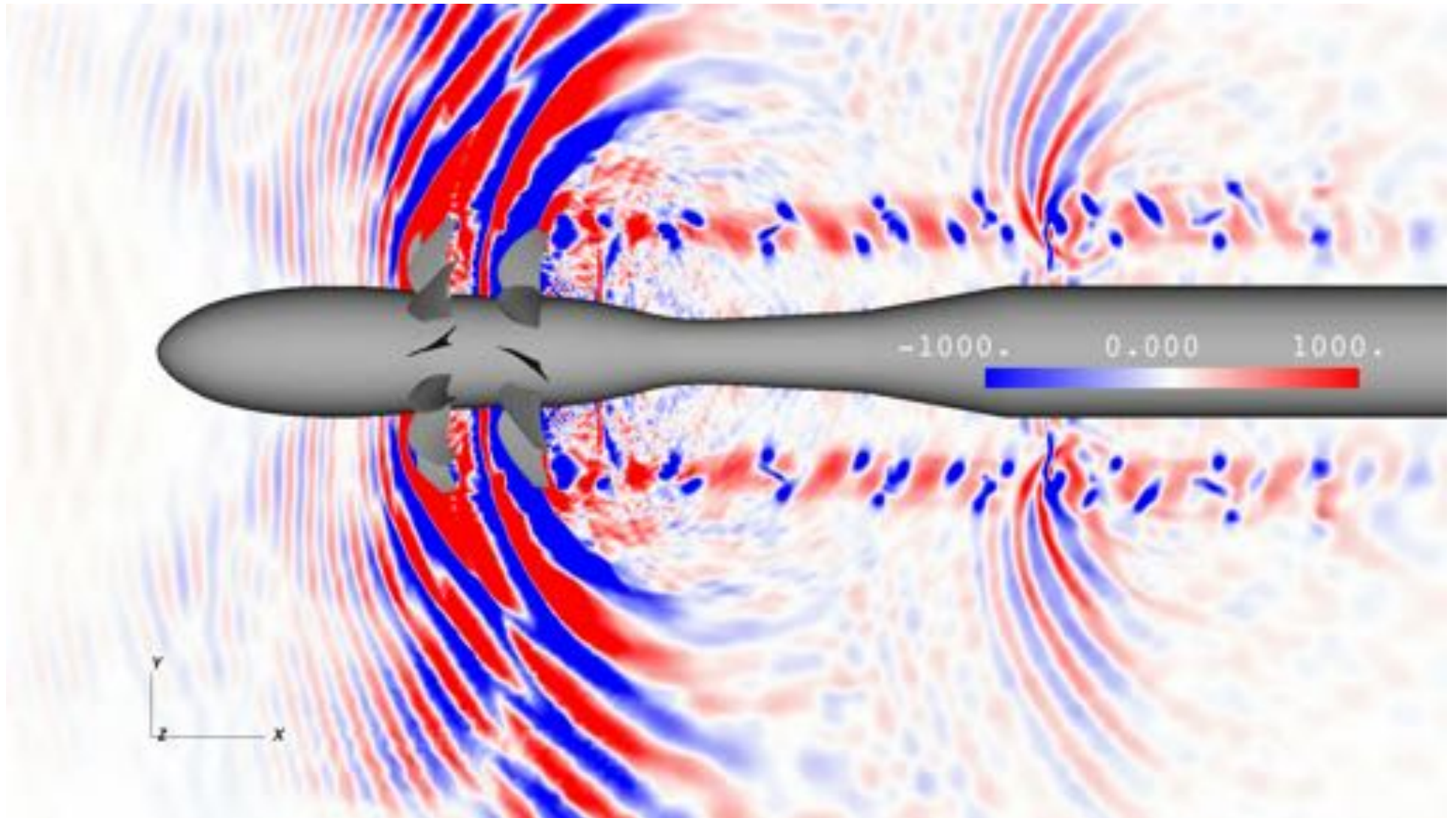
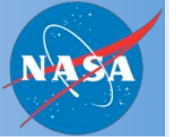


# LAVA CARTESIAN : PASSIVE PARTICLES



Passive particles seeded at trailing edges of blades: red is fwd, blue is aft seeding

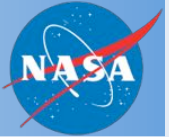
# LAVA CARTESIAN – WENO5 DISTURBANCE PRESSURE



$$P' = P - P_{ave}$$

# LAVA CARTESIAN – WENO5

## DENSITY GRADIENT

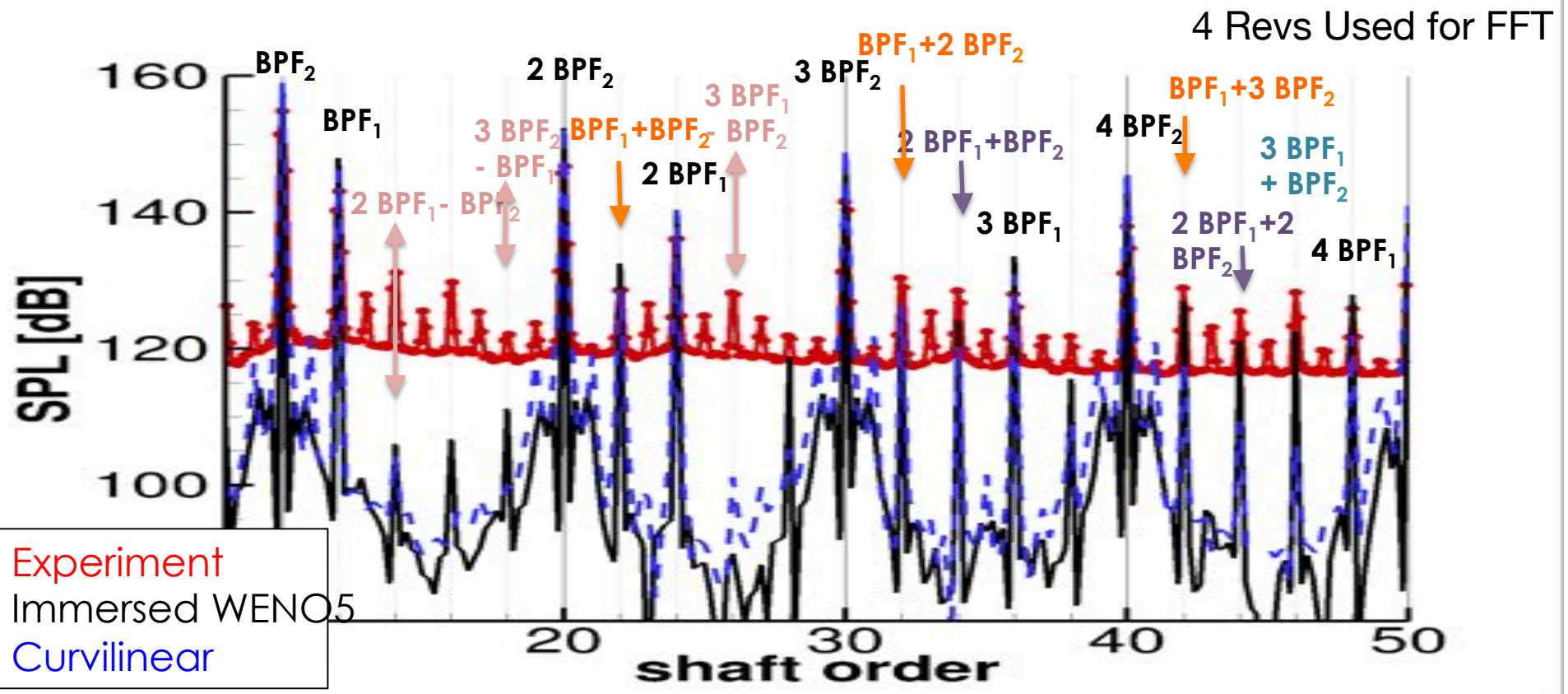
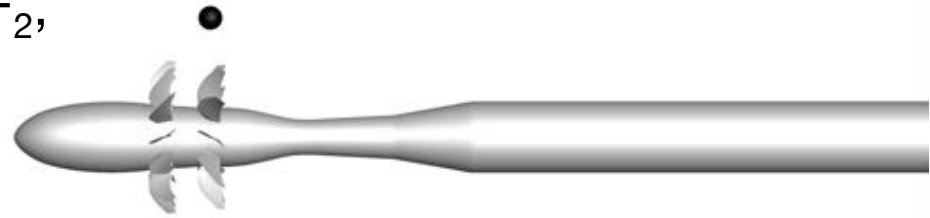




# SPL SPECTRAL COMPARISON

- Capturing  $n\text{BPF}_1$  and  $n\text{BPF}_2$  ( $n \leq 4$  and higher)
- Capturing  $\text{BPF}_1 + \text{BPF}_2$ ,  $\text{BPF}_1 + 2\text{BPF}_2$ ,  $2\text{BPF}_1 + \text{BPF}_2$ , and  $\text{BPF}_1 + 3\text{BPF}_2$
- Loss of magnitude at  $3\text{BPF}_1 + \text{BPF}_2$

Kulite 9 H = 0.51m

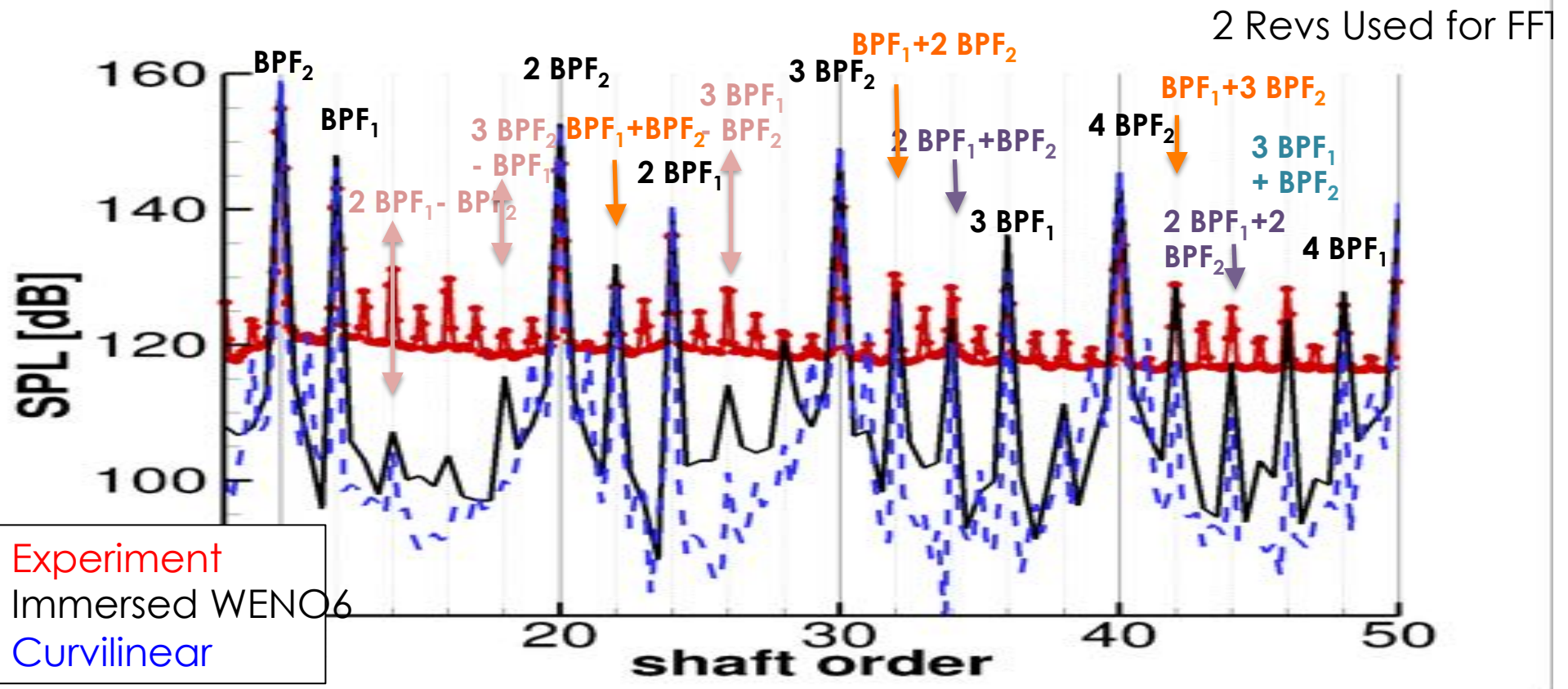


# SPL SPECTRAL COMPARISON

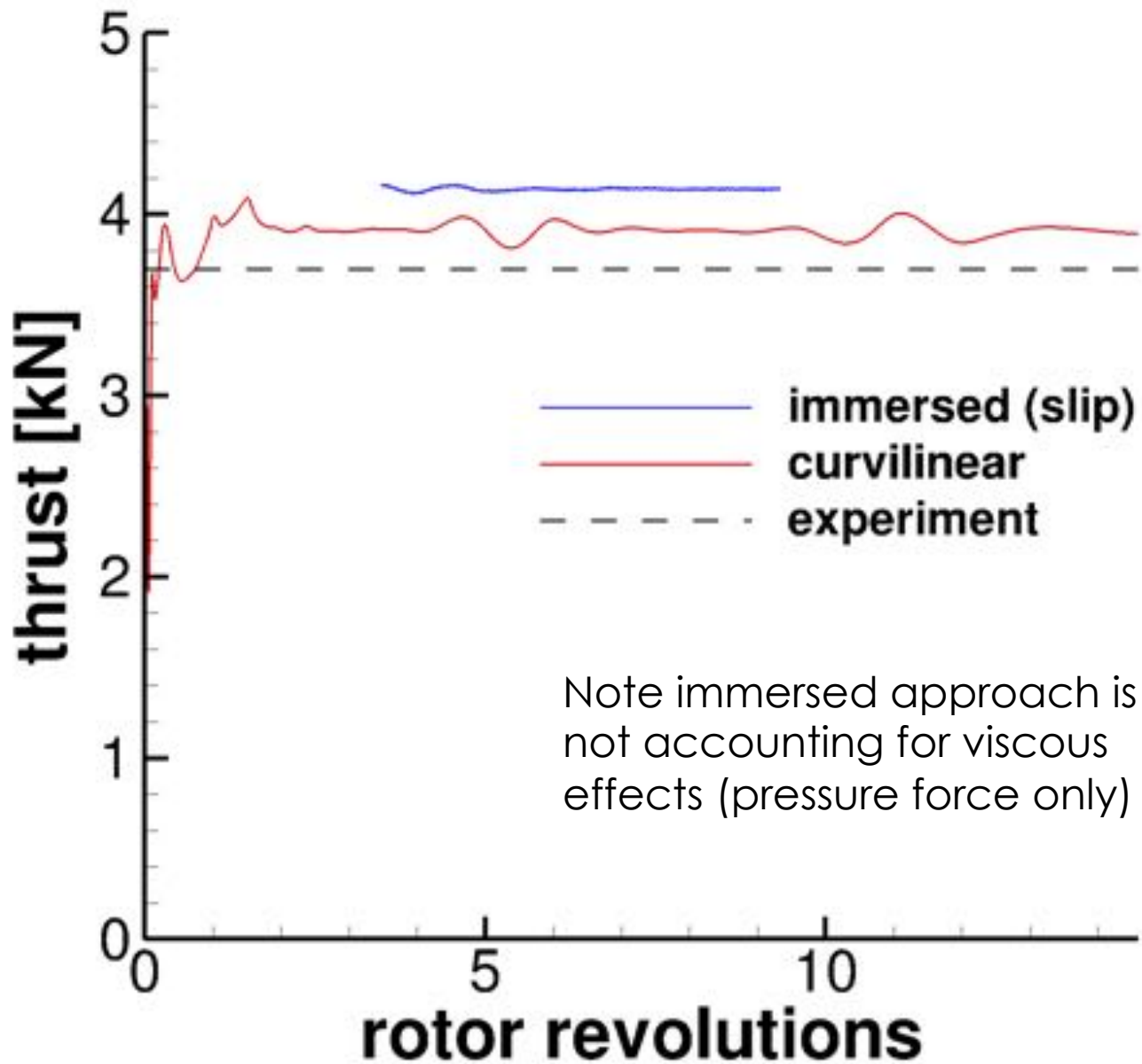


- Capturing  $n\text{BPF}_1$  and  $n\text{BPF}_2$  ( $n \leq 4$  and higher)
- Capturing  $\text{BPF}_1 + \text{BPF}_2$ ,  $\text{BPF}_1 + 2 \text{BPF}_2$ ,  $2 \text{BPF}_1 + \text{BPF}_2$ , and  $\text{BPF}_1 + 3 \text{BPF}_2$
- Loss of magnitude at  $3 \text{BPF}_1 + \text{BPF}_2$

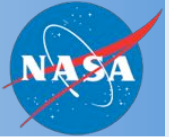
Kulite 9 H = 0.51m



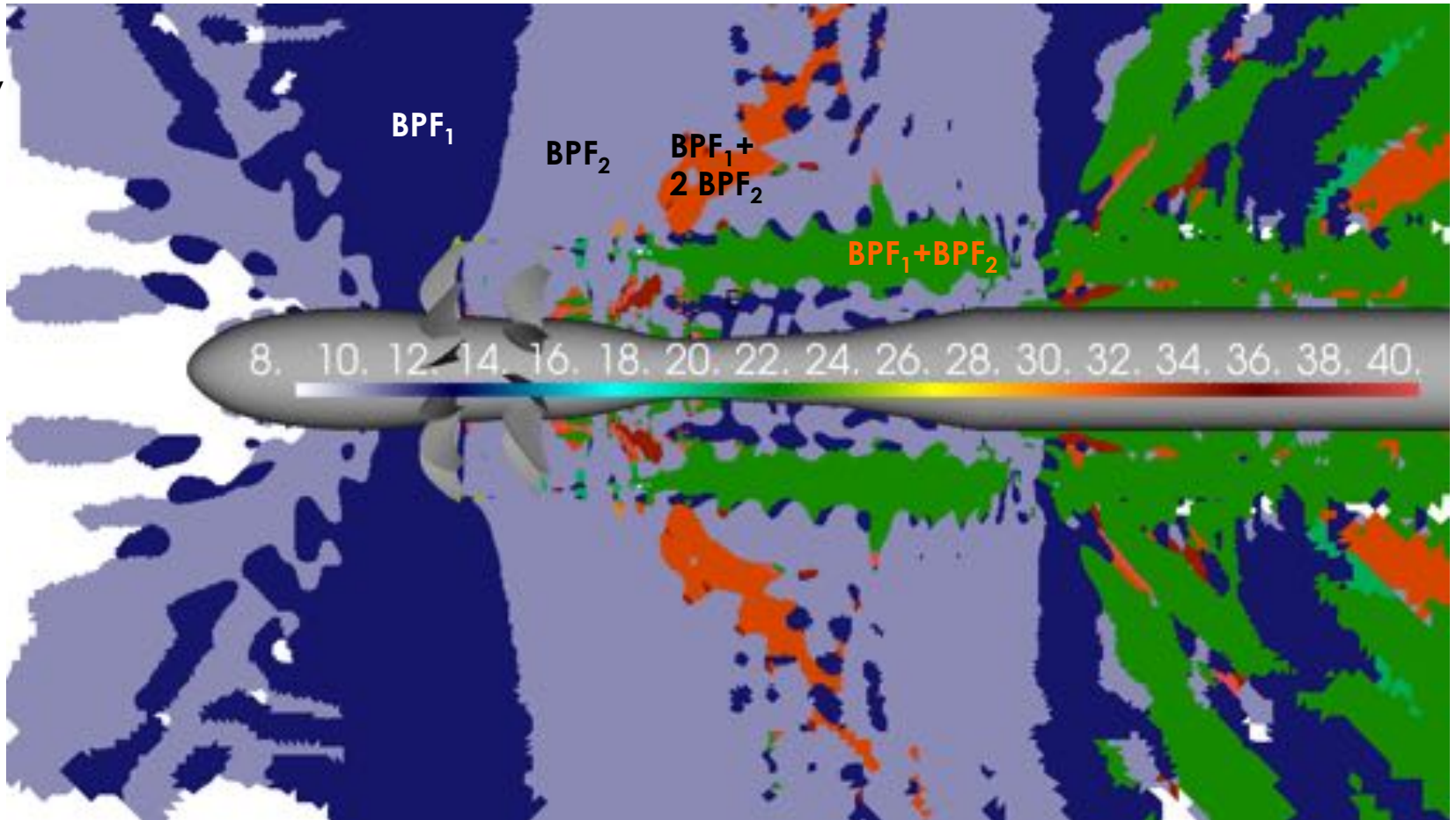
# THRUST COMPARISON



# TEMPORAL FFTs: IMMERSSED WENO5



Dominant frequency

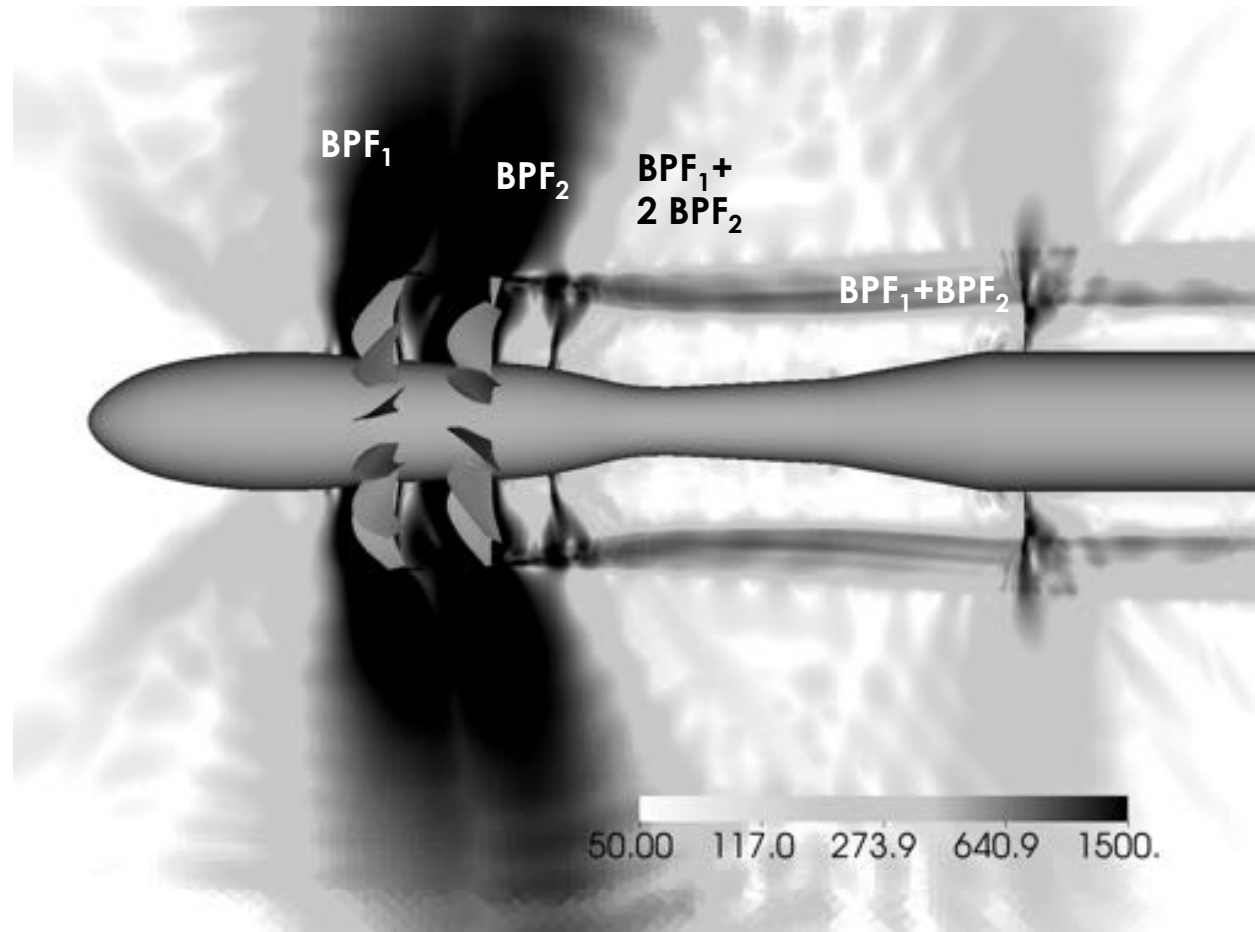


- Different noise generation mechanisms are dominating different parts of the flow field

# TEMPORAL FFTS: IMMERSSED WENO5



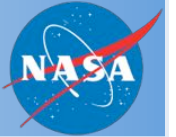
Maximum  
amplitude



- **Different noise generation mechanisms are dominating different parts of the flow field**



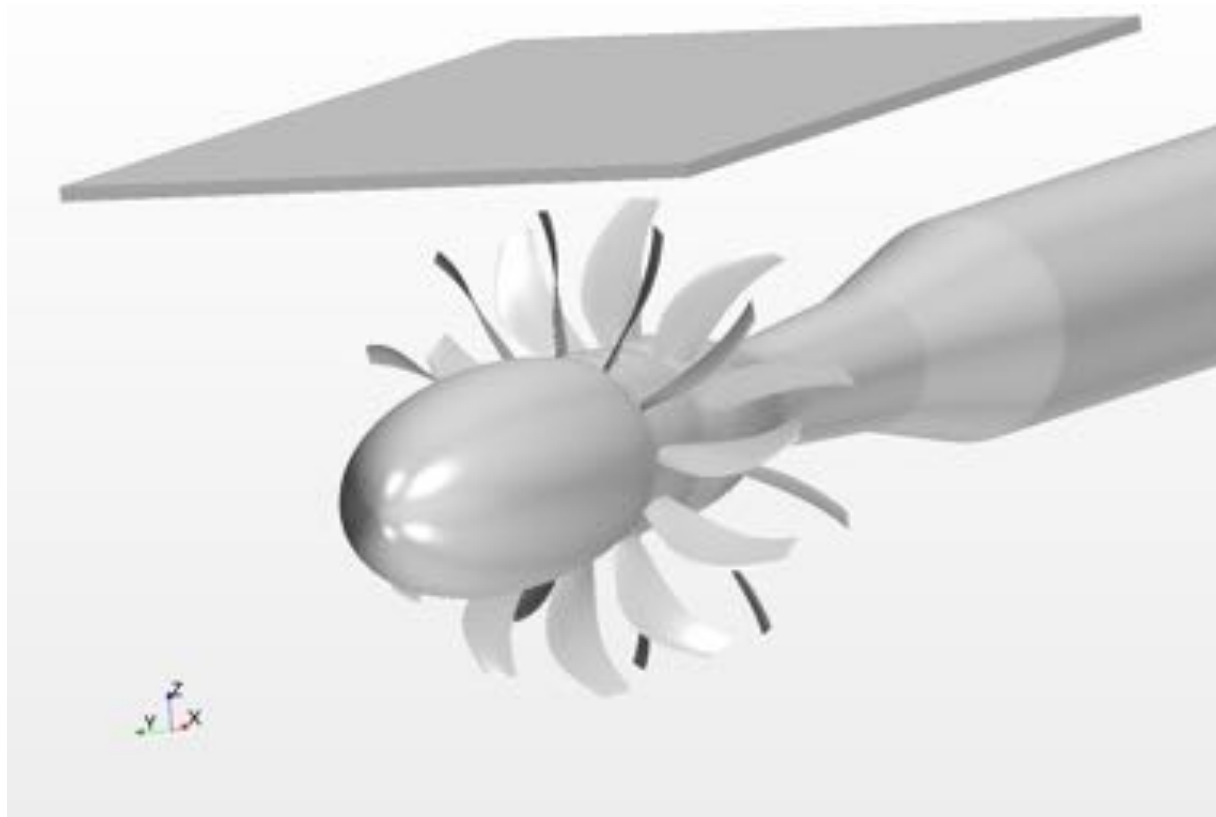
# LAVA CARTESIAN : PLATE EFFECTS



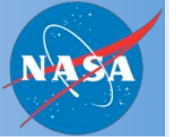
Inserted plate into existing Cartesian (WENO5) simulation.

Preliminary results:

- Additional grid points for plate
- Elevated velocity/CFL occurred at leading and trailing edge
- Plate trailing edge has unsteady wake shedding

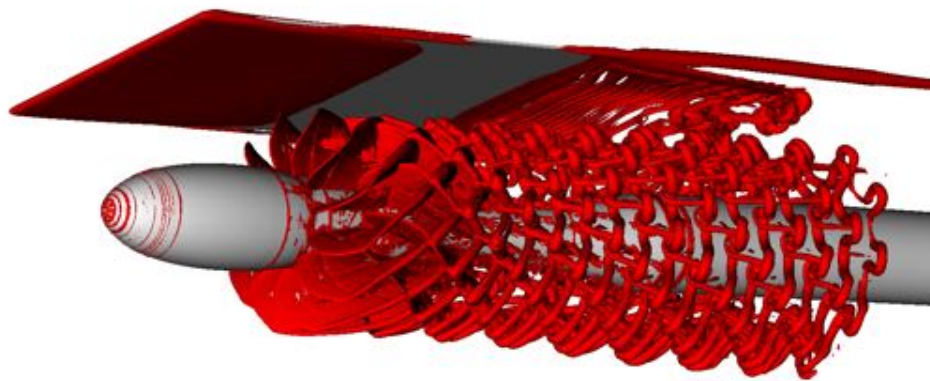


# LAVA CARTESIAN : PLATE EFFECTS

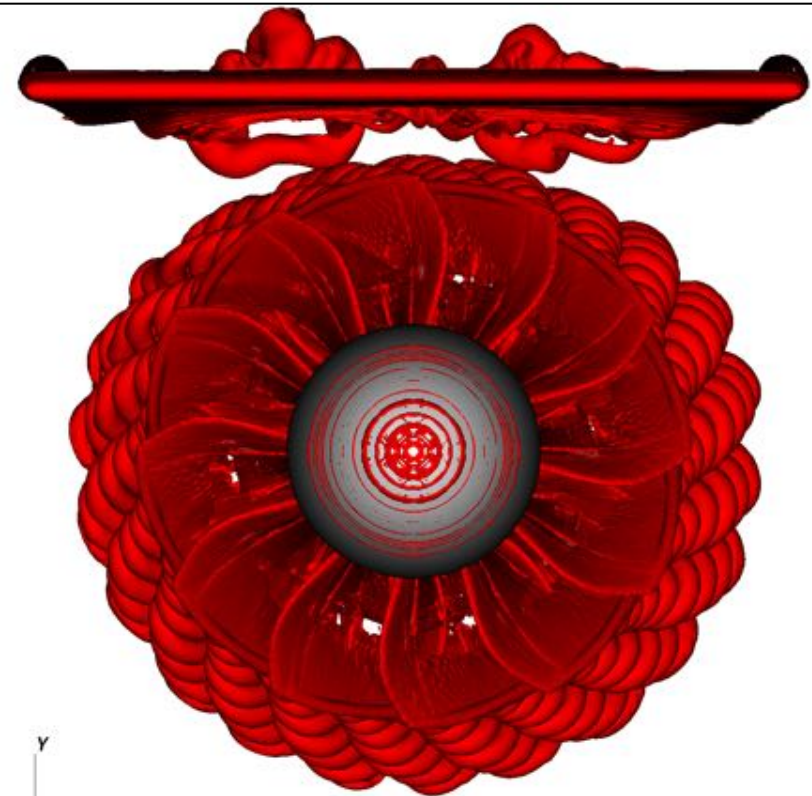


Comparisons show that the plate (@43cm) introduces flow differences:

- Asymmetry in vortex core “web” due to confinement (below right)
- Plate wake break-down (below left)



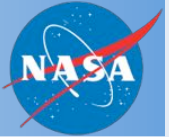
Oblique view showing plate wake



Asymmetry of vorticity “web”

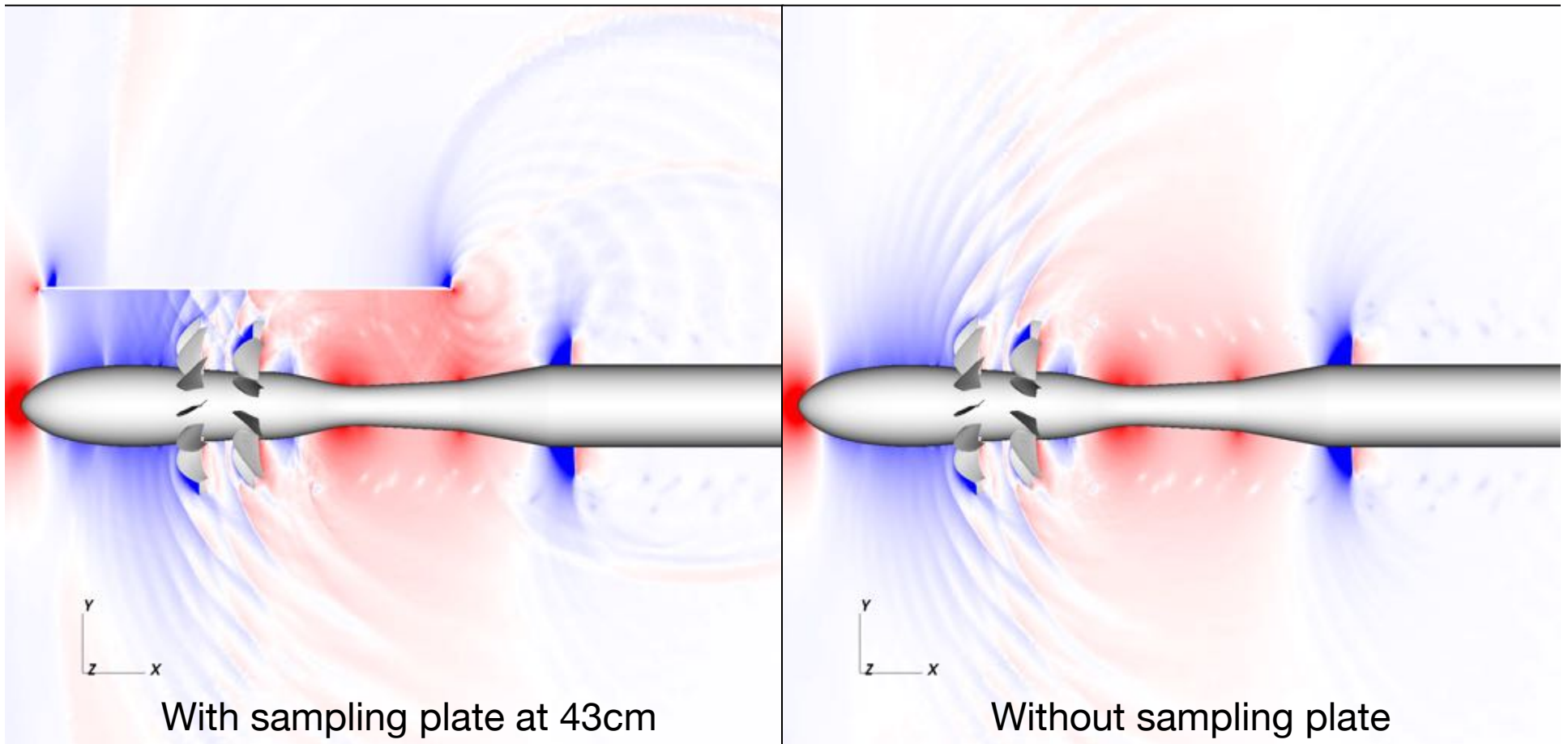
Vorticity level 2000 [1/s] contoured

# LAVA CARTESIAN : PLATE EFFECTS



Comparisons show that the plate (@43cm) introduces flow differences:

- Acoustic blocking can be seen when compared to no-plate case
- Elevated pressure levels due to confinement
- Possible higher-harmonics

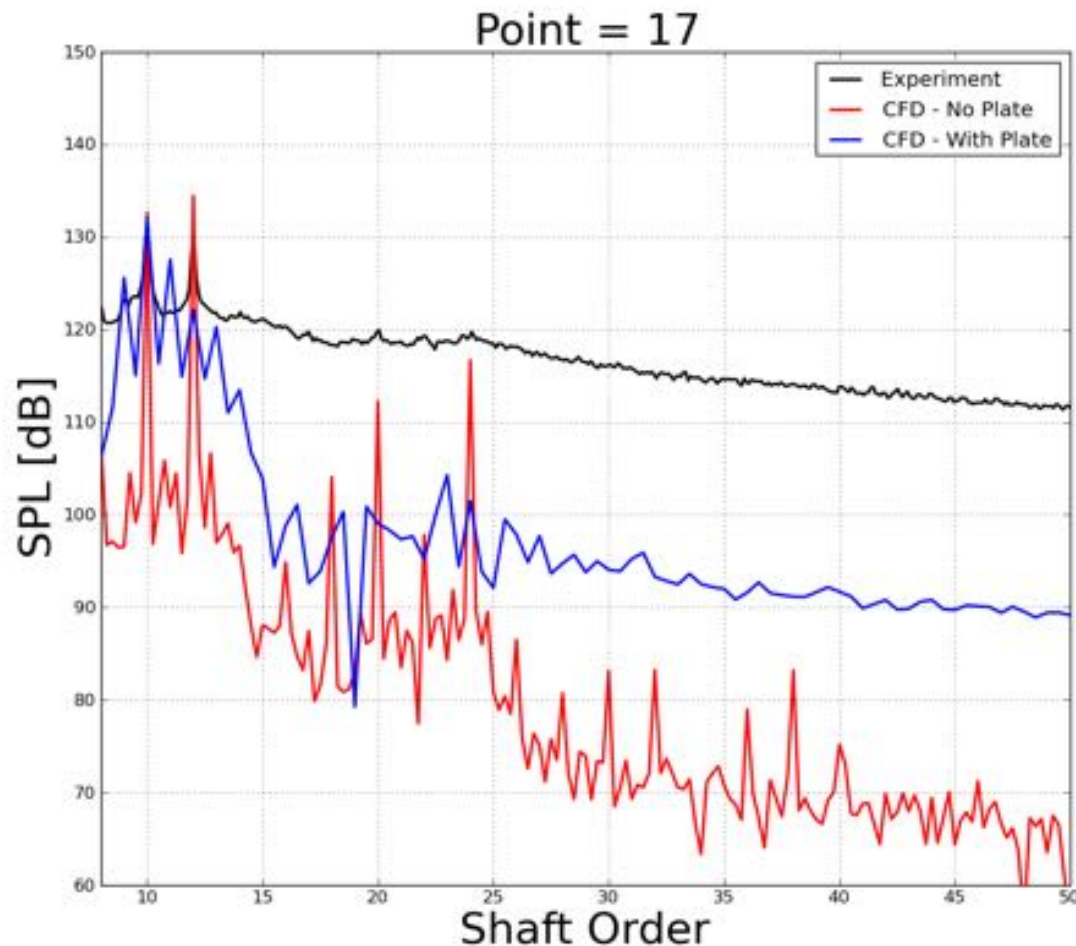


# LAVA CARTESIAN : PLATE EFFECTS



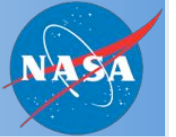
Comparisons show that the plate (@43cm) introduces flow differences:

- Elevated broadband levels
- Finer grid resolution should further improve broadband content



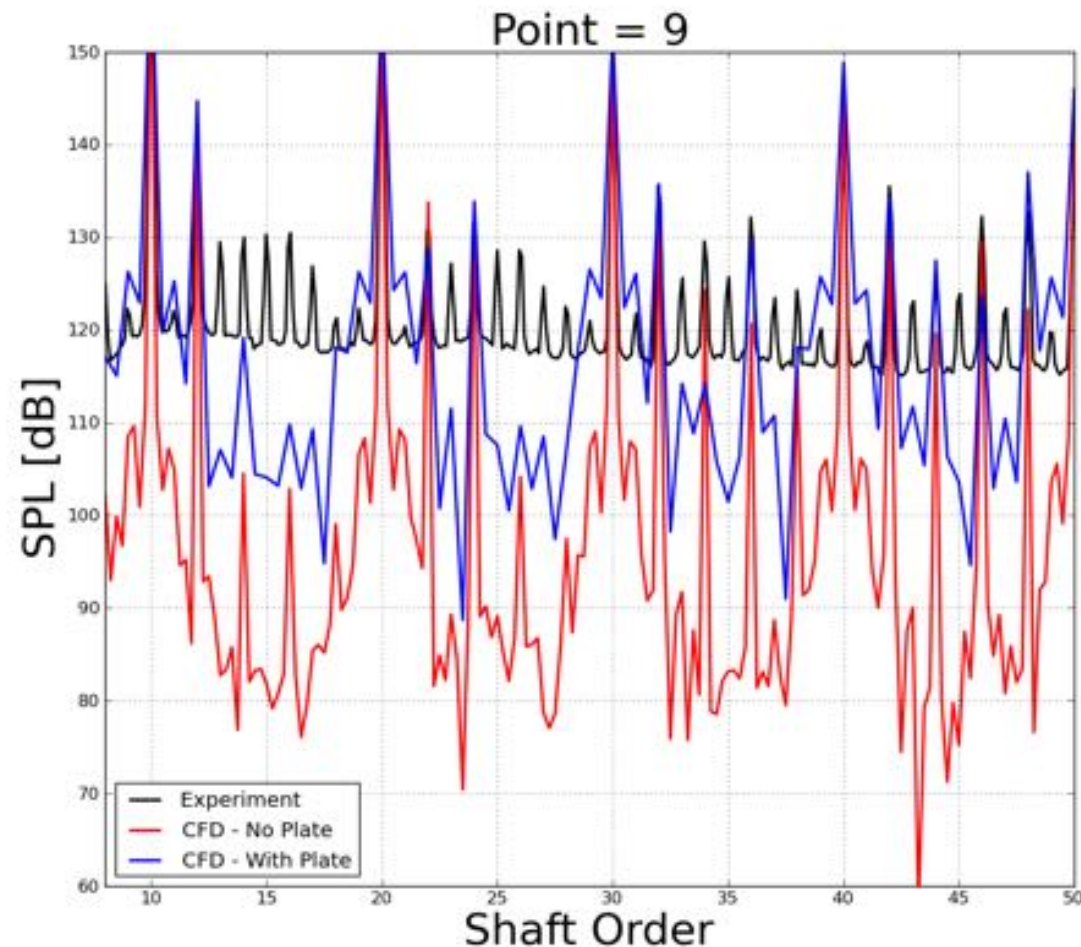
Point 17 (upstream)

# LAVA CARTESIAN : PLATE EFFECTS



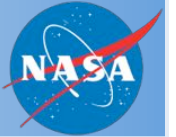
Comparisons show that the plate (@43cm) introduces flow differences:

- Elevated broadband levels
- Finer grid resolution should further improve broadband content



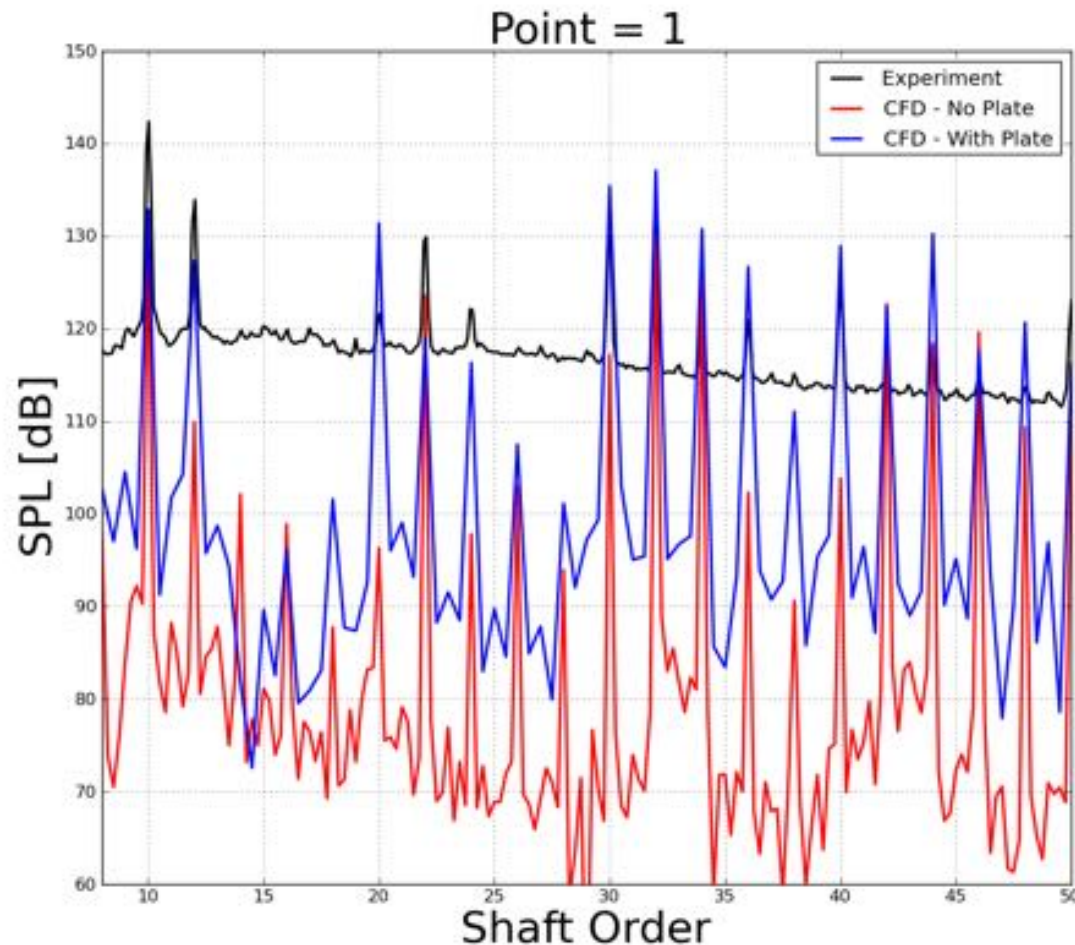
Point 9 (center)

# LAVA CARTESIAN : PLATE EFFECTS



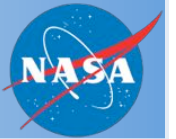
Comparisons show that the plate (@43cm) introduces flow differences:

- Elevated broadband levels
- Finer grid resolution should further improve broadband content

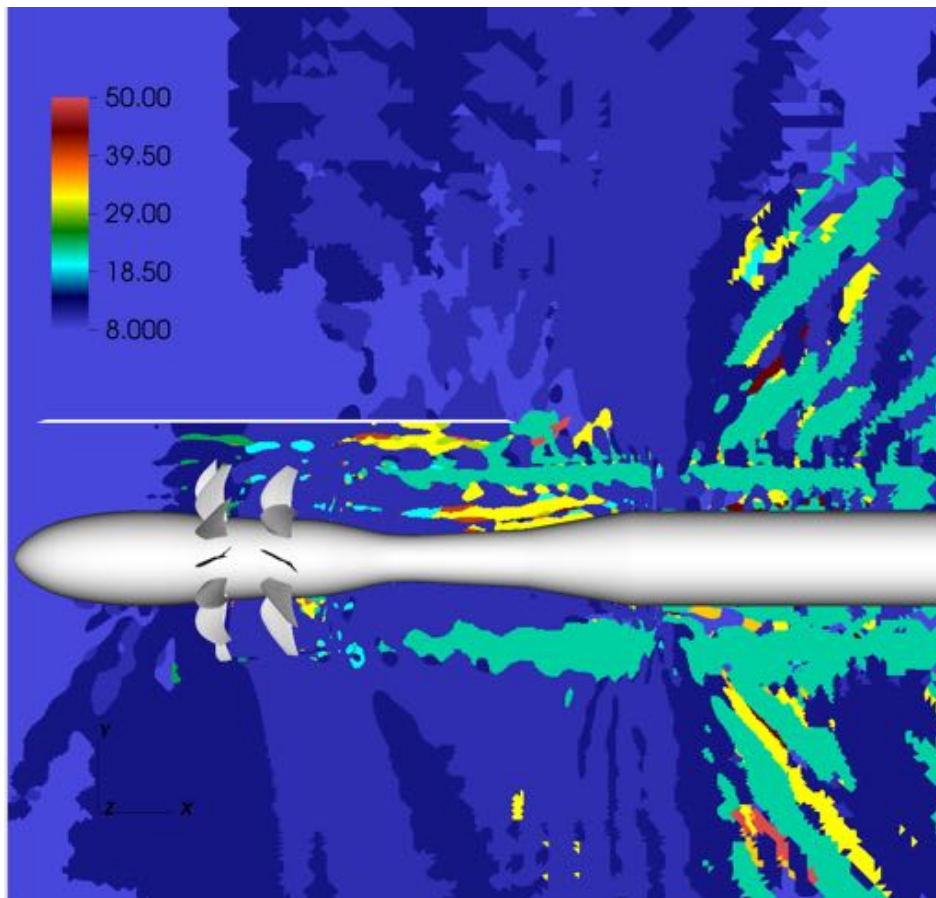


Point 1 (aft)

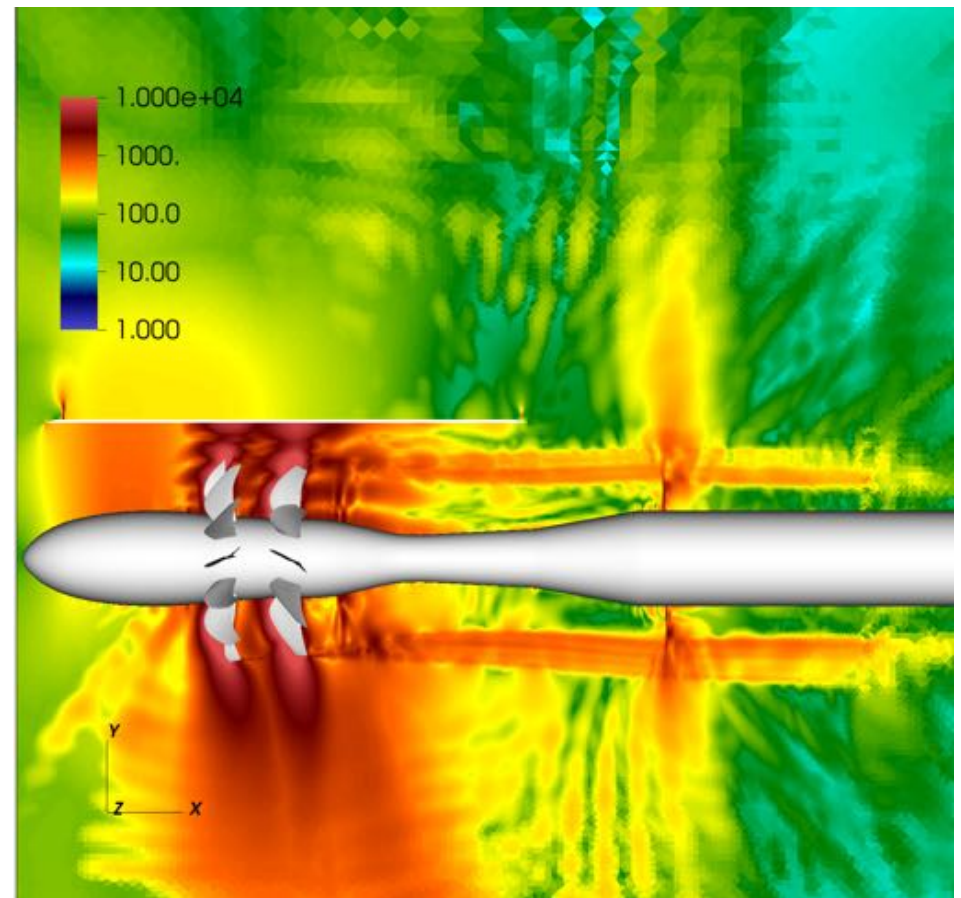
# LAVA CARTESIAN : PLATE EFFECTS



Frequency at peak amplitude [shaft orders]



Amplitude at peak frequency

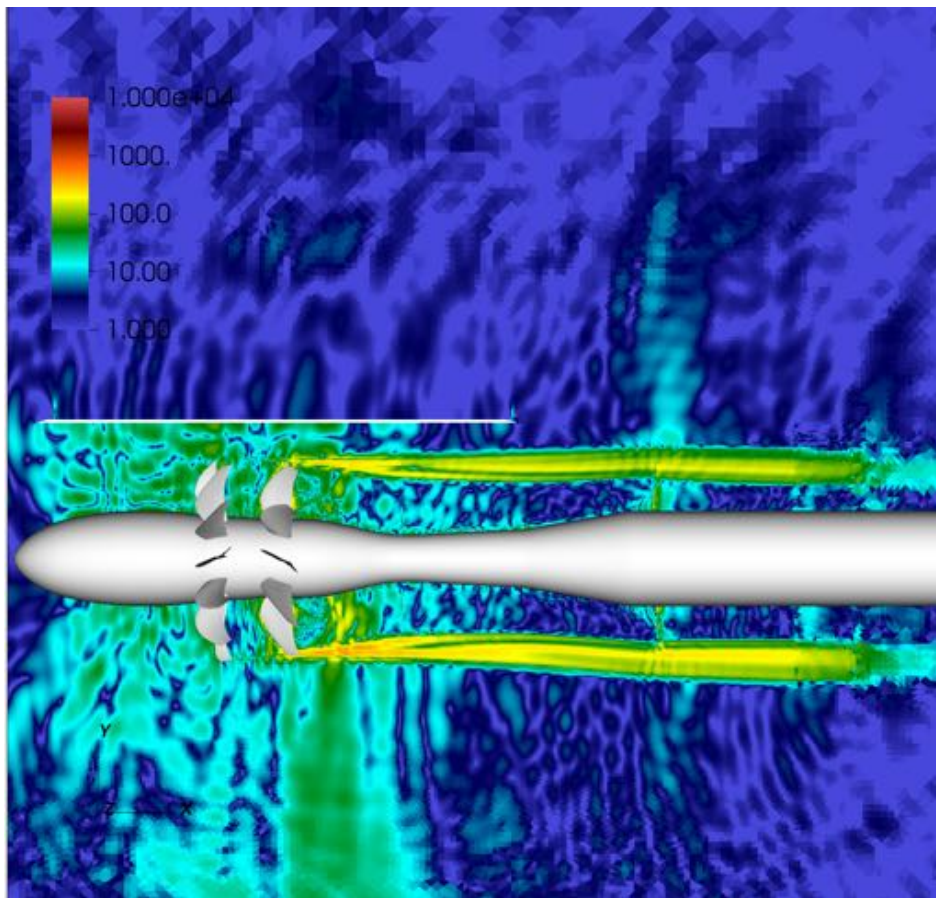


# LAVA CARTESIAN : PLATE EFFECTS

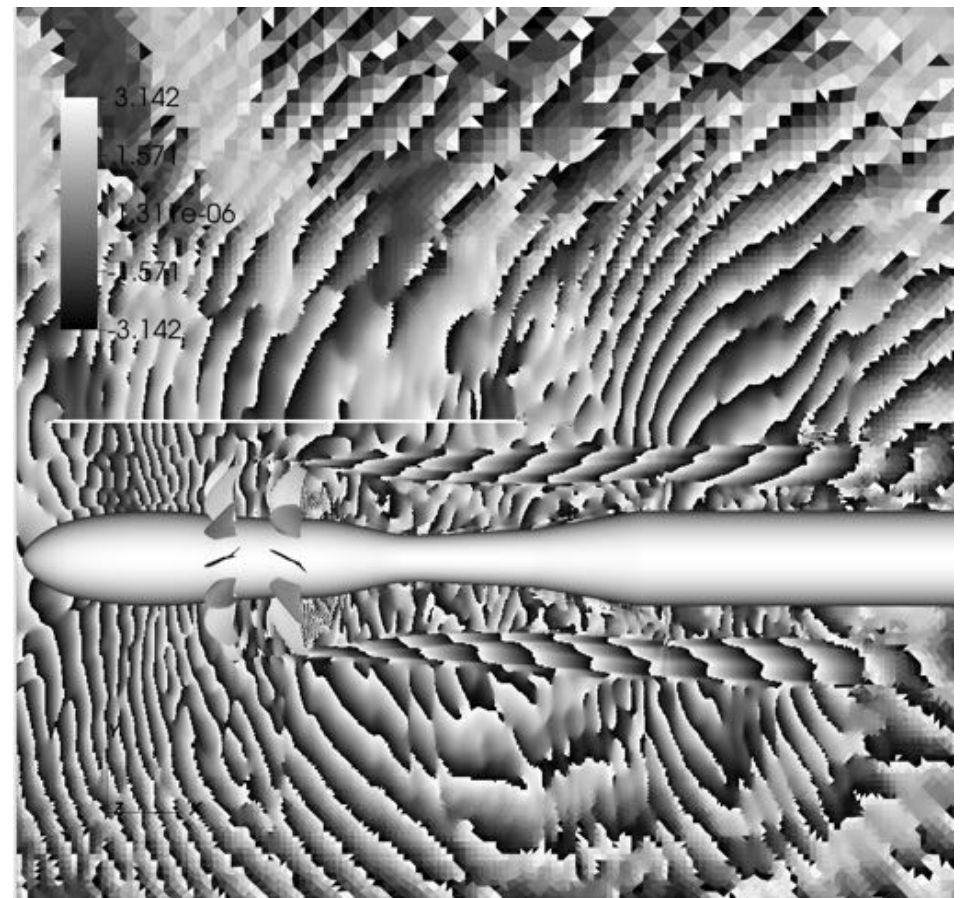


Shaft Order = 14 (2 x BPF<sub>1</sub>-BPF<sub>2</sub>)

Amplitude



Phase



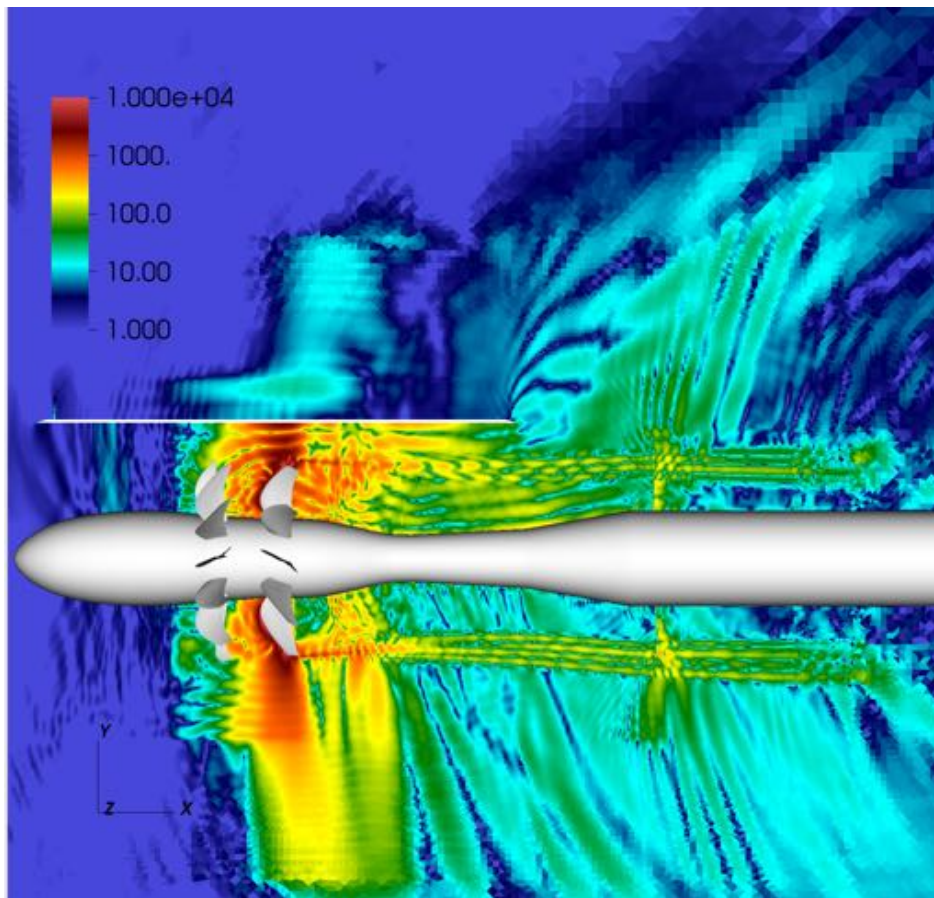


# LAVA CARTESIAN : PLATE EFFECTS

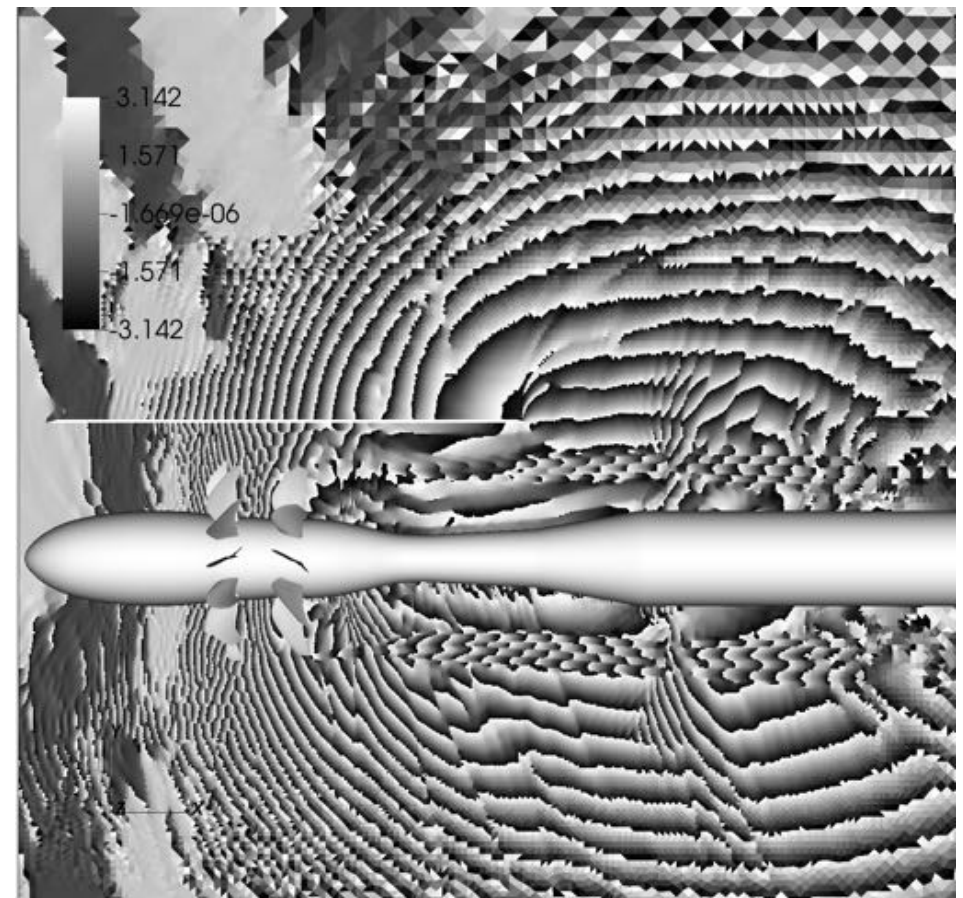


Shaft Order = 30 ( $3 \times \text{BPF}_1$ )

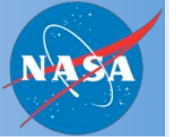
Amplitude



Phase

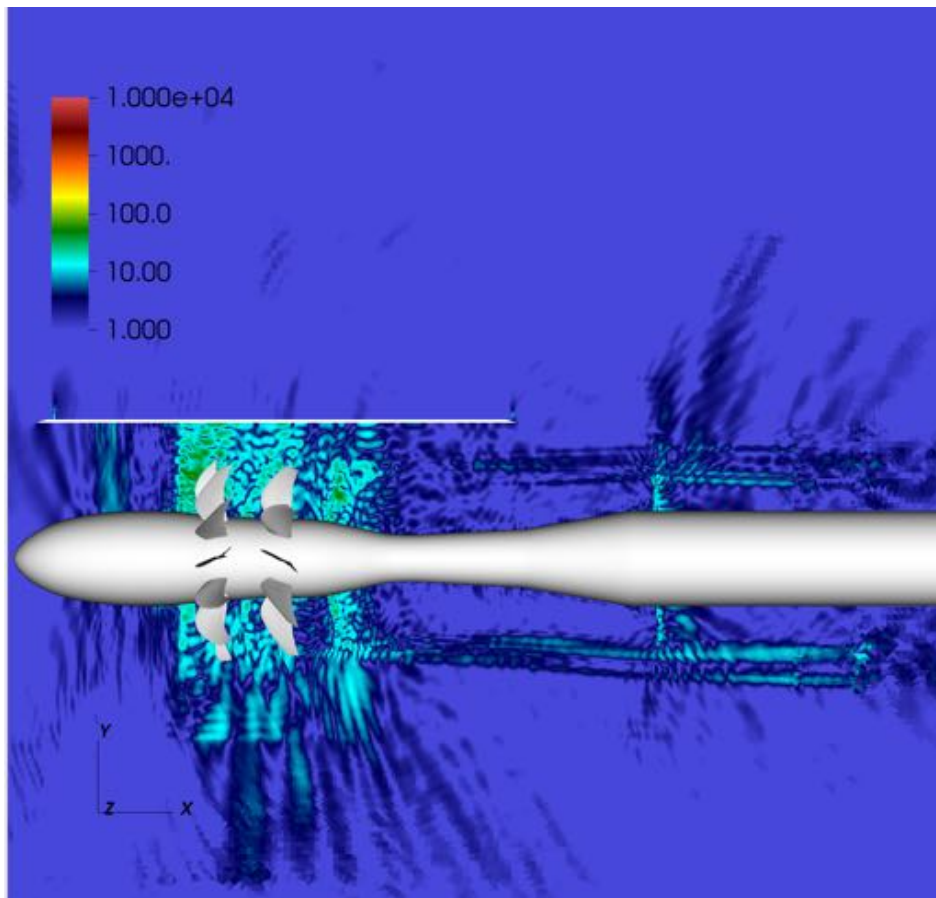


# LAVA CARTESIAN : PLATE EFFECTS

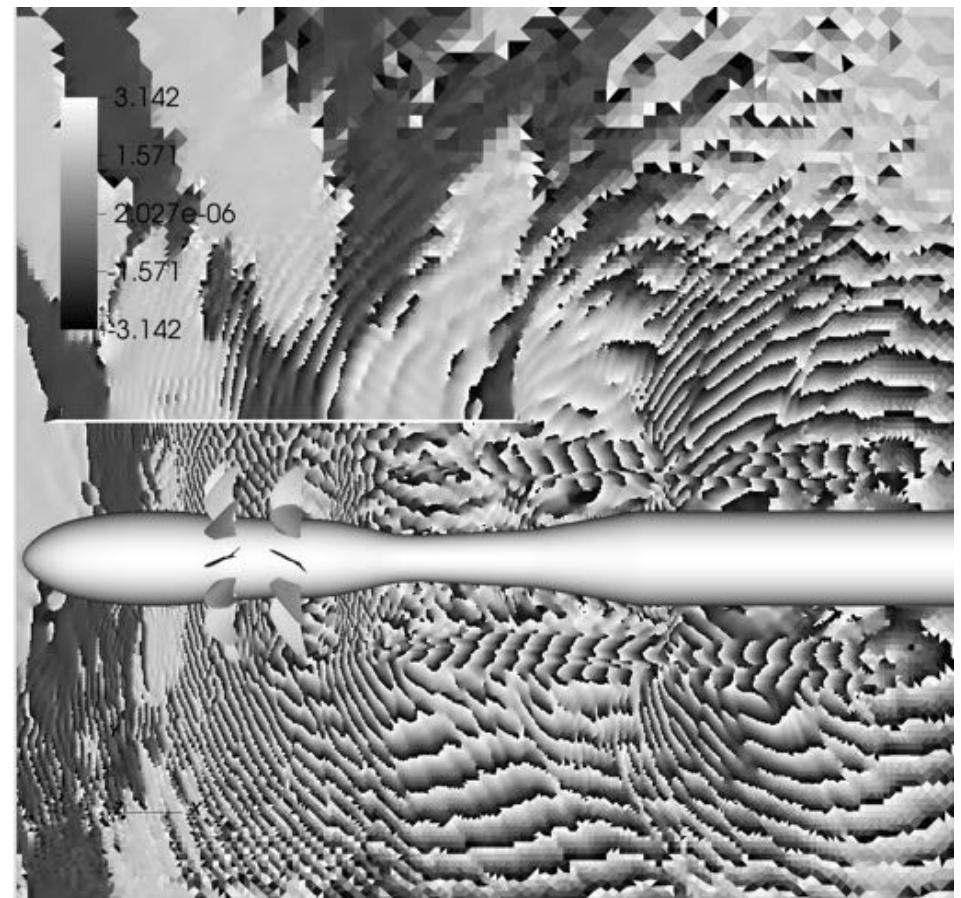


Shaft Order = 33

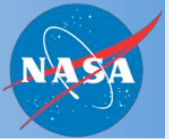
Amplitude



Phase

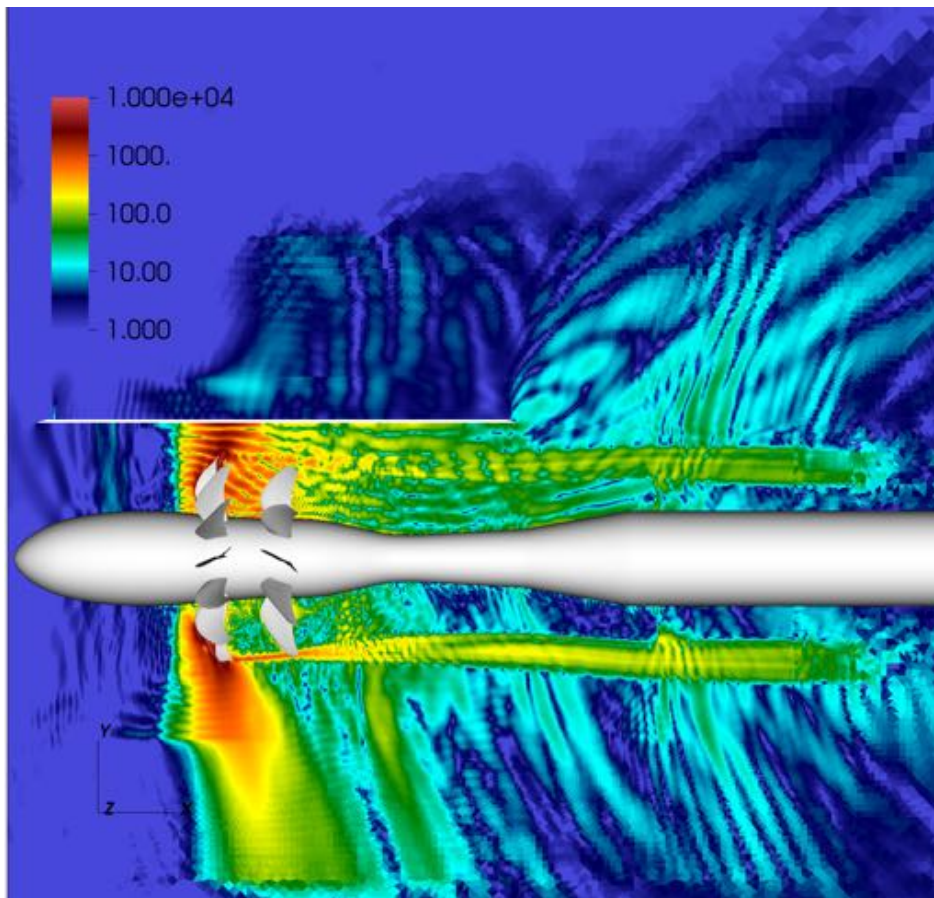


# LAVA CARTESIAN : PLATE EFFECTS

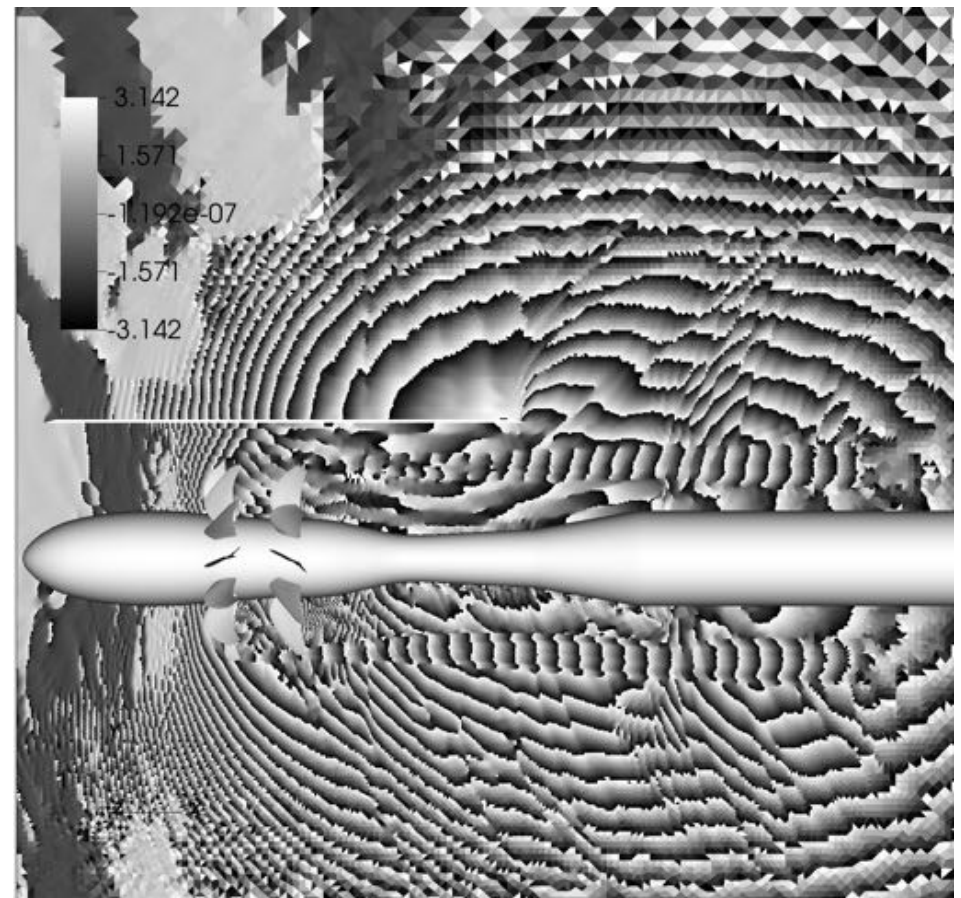


Shaft Order = 36 (3 x BPF<sub>2</sub>)

Amplitude



Phase



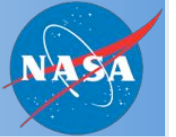
# LOW SPEED CASE SETUP



- *Conditions:*

- Mach = 0.2
- Rotation speed = 6303 [RPM]
- Pressure = 101325.353 [Pa]
- Velocity = (68.06946, 0.0, 0.0) [m/s]
- Temperature = 288.15 [K]
- Takeoff condition for blades: fwd @ 40.1, aft @ 40.8 degrees
- Sound field measured at 1.524 [m] or 60 inches (as given by E. Envia)
- No plate or wind-tunnel geometry included

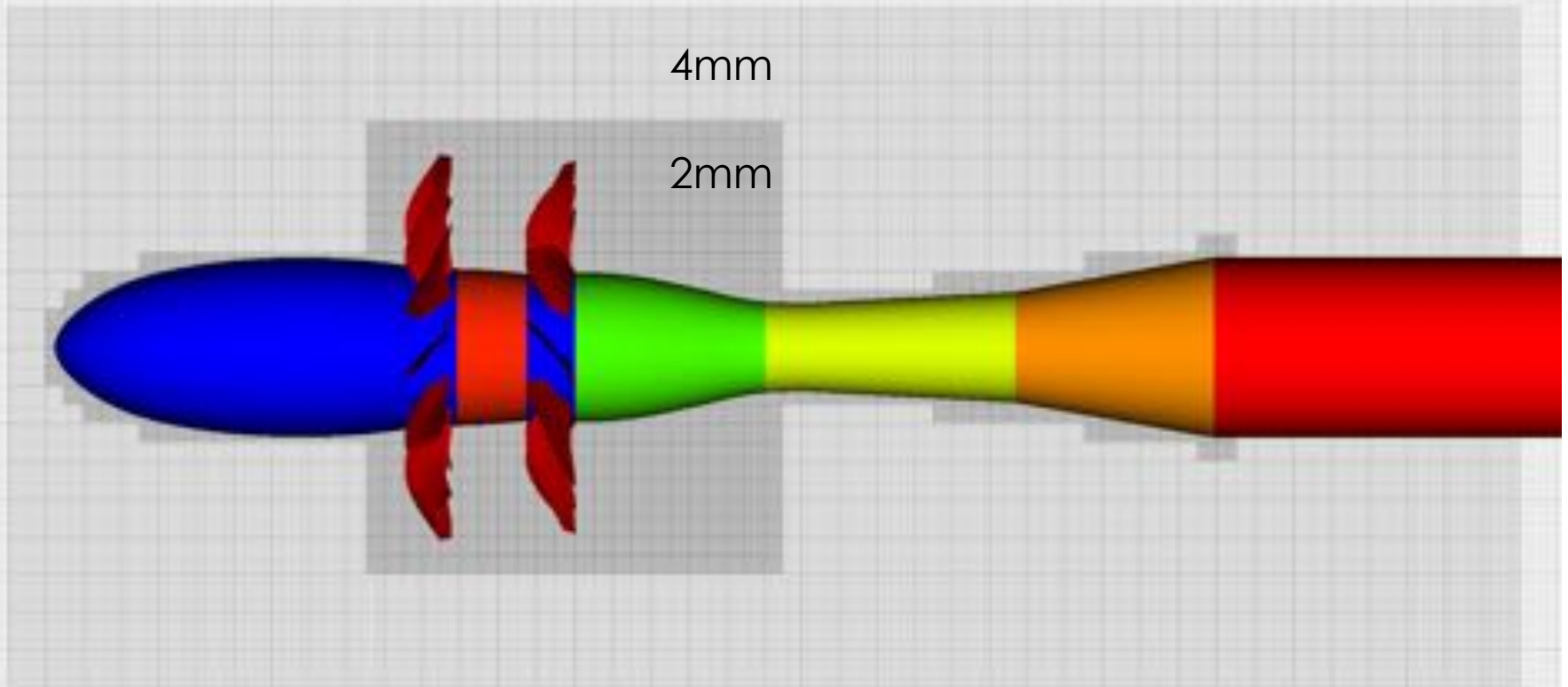
# CARTESIAN IMMERSED BOUNDARY: MESH



8mm

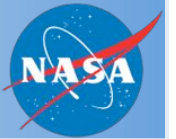
4mm

2mm

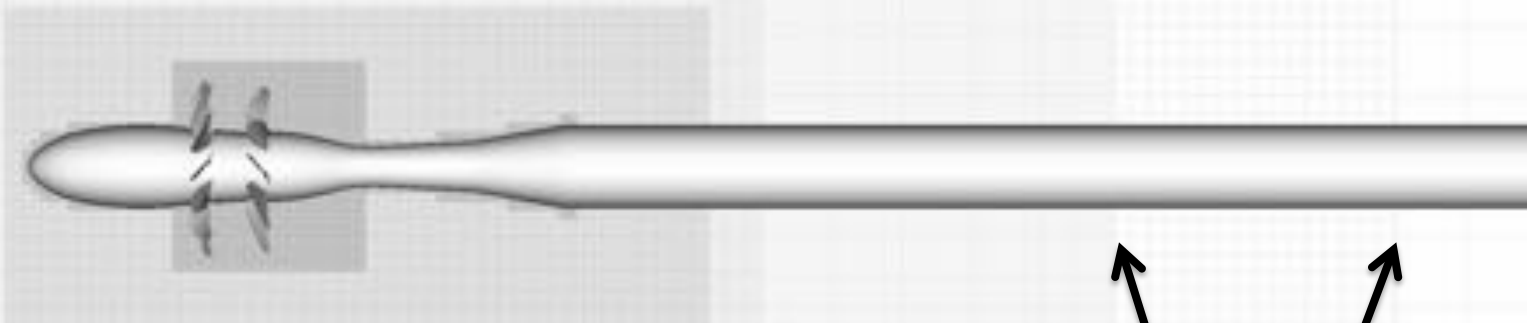


Total: 147 Million Cells

# CARTESIAN IMMERSED BOUNDARY STARTUP TRANSIENT (PRESSURE)

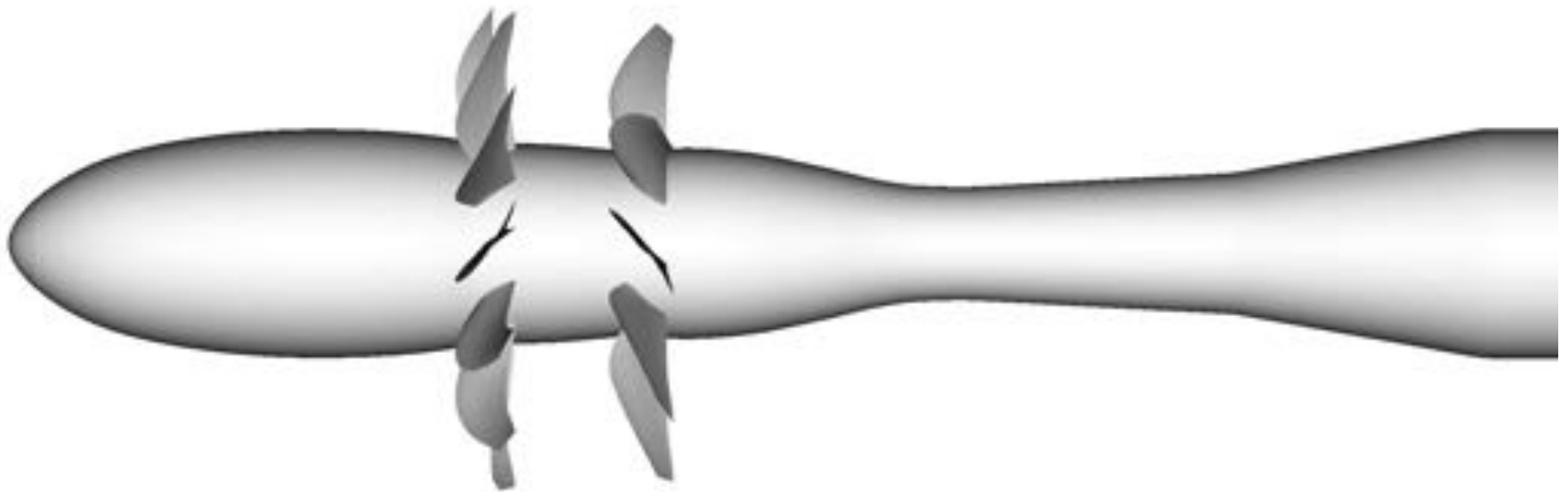
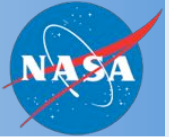


Pseudocolor  
DB: surf003.Cart.0000000.3d.vtk  
Cycle: 0 Time: 0  
Var: Pressure  
102325.353  
101825.353  
101325.353  
100825.353  
100325.353



Mesh transition

# LAVA CARTESIAN - PRESSURE MOVIE

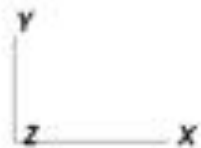
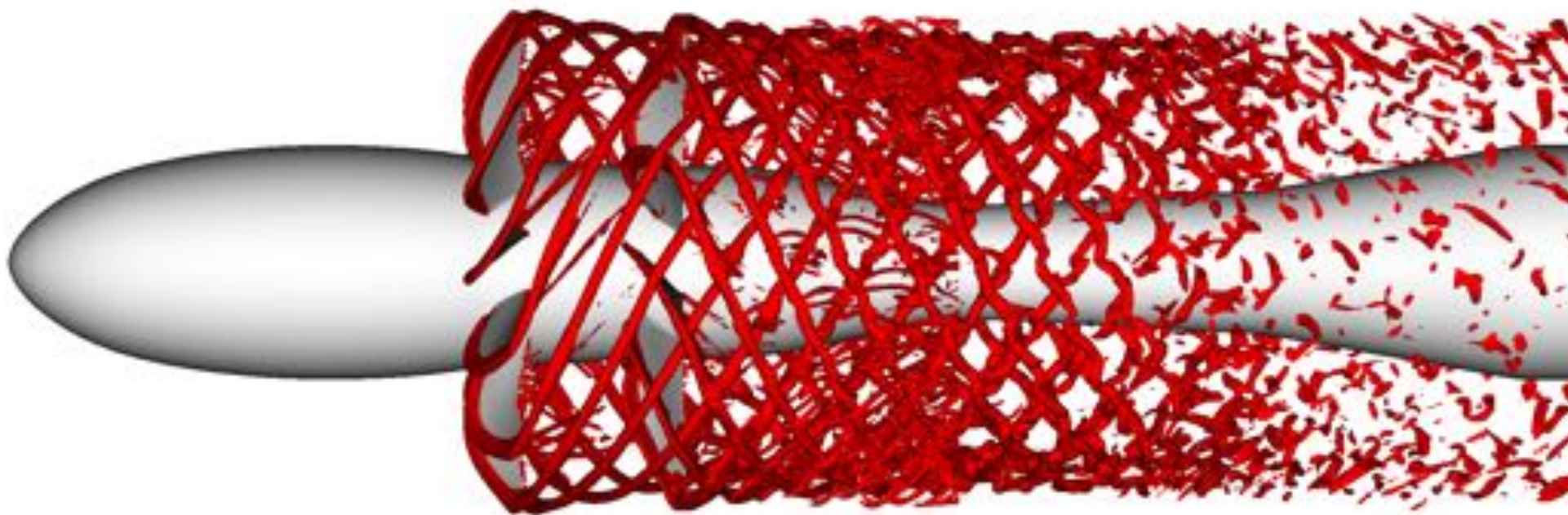
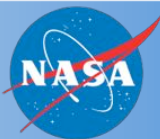


Time = 0 (s)

Time step = 0

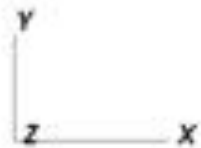
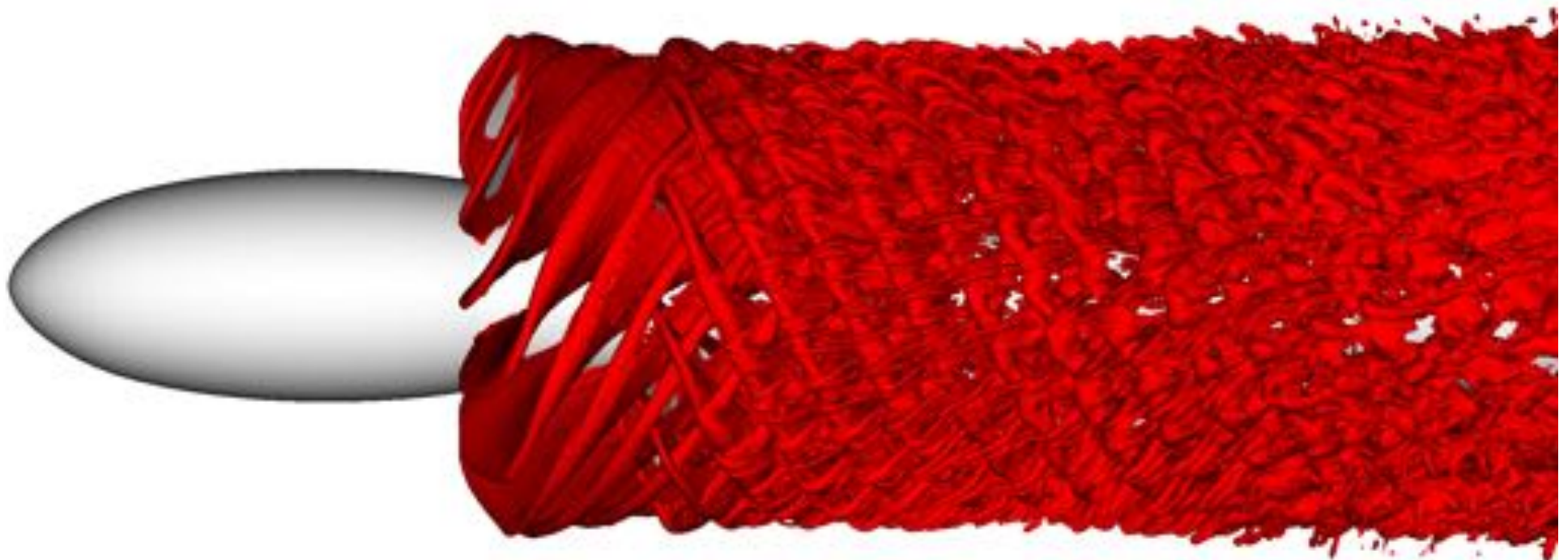
Mach = 0.20, RPM = 6303

# LAVA CARTESIAN - VORTICITY @ 5000 [1 / s]



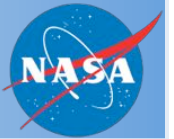


# LAVA CARTESIAN - VORTICITY @ 2000 [1 / s]

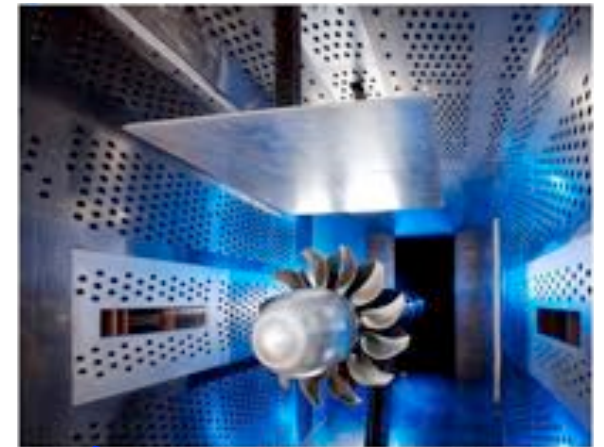


# SUMMARY AND FUTURE WORK

## LAVA CARTESIAN IMMERSED



- Algorithm improvements:
  - Thin blade handling for Immersed Boundary Method (IBM) ✓
  - High-order IBM ✓
  - Optimizations for moving bodies with IBM
    - Geometry kernels ([progressing](#))
    - Stencils ([progressing](#))
- Open rotor simulations:
  - High speed case
    - Coarse mesh (146M) ✓
      - Convective scheme sensitivity ✓
      - Plate effects ✓
      - Wind tunnel walls (8'x6') ✗
  - Low speed case
    - Coarse mesh (147M) ([running, currently at 7 revs](#))
      - Once enough revs are computed, will conduct more detailed analysis



Ref: AIAA-2014-2606