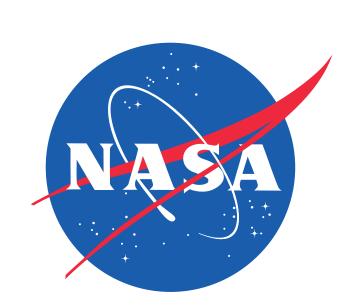
# PERFORMANCE ANALYSIS OF A HARDWARE IMPLEMENTED COMPLEX SIGNAL KURTOSIS RADIO-FREQUENCY INTERFERENCE DETECTOR

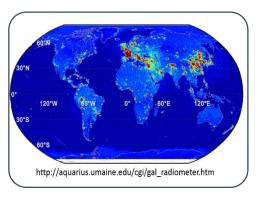


Adam J. Schoenwald<sup>1</sup>, <u>Adam.Schoenwald@nasa.gov</u> Damon C. Bradley<sup>1</sup>, Priscilla N. Mohammed<sup>1, 2</sup>, Jeffrey R. Piepmeier<sup>1</sup>, Mark Wong<sup>1</sup>

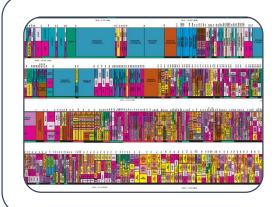


(1) NASA Goddard Space Flight Center, Greenbelt, MD (2) Goddard Earth Sciences Technology and Research, Morgan State University

#### Motivation



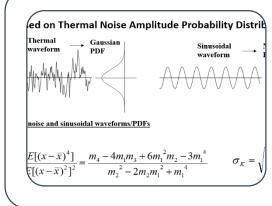
RFI compromises quality of science products.



Spectrum is becoming crowded and shared.



Hardware capabilities allow for digital radiometry.



Need more sensitive detectors for wide-band interference.

# Complex Signal Kurtosis

Given a complex baseband signal z(n) = I(n) +jQ(n), moments  $\alpha_{\ell,m}$  of z(n) are defined as

$$lpha_{\ell,m}=\mathbb{E}ig[(z-\mathbb{E}[z])^\ell(z-\mathbb{E}[z])^{*m}ig]$$
 ,  $\ell$  ,  $m\in\mathbb{R}\geq 0$ 

With  $\sigma^2 = \alpha_{1.1}$  , Standardized moments  $\varrho_{\ell,m}$  can then be found as

$$\varrho_{\ell,m} = \frac{\alpha_{\ell,m}}{\sigma^{\ell+m}}$$

Leading to the CSK (Complex Signal Kurtosis) rfi test statistic used [1,2].

$$C_K = \frac{\varrho_{2;2} - 2 - \left| \varrho_{2;0} \right|^2}{1 + \frac{1}{2} \left| \varrho_{2;0} \right|^2}$$

## Real Signal Kurtosis

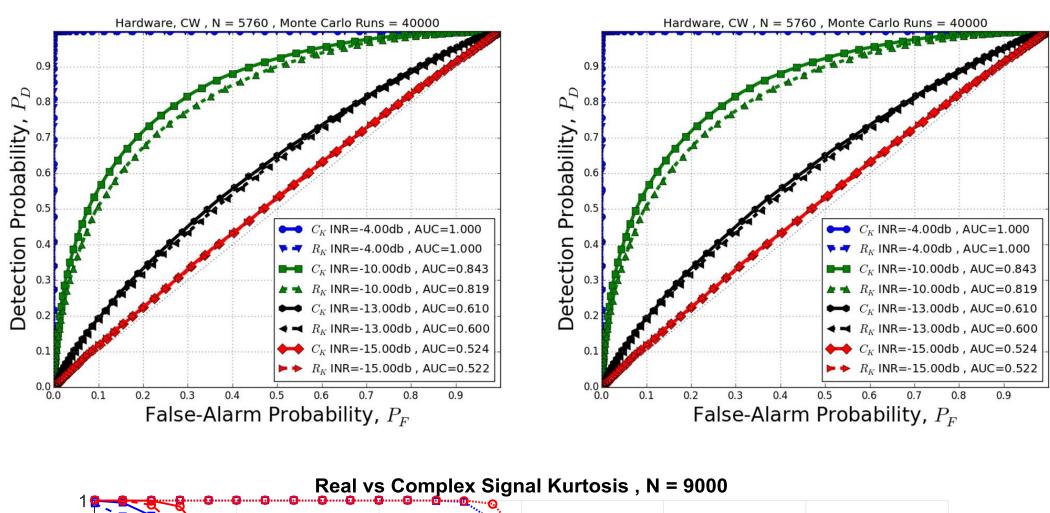
Given a complex baseband signal z(n) = I(n) + I(n)the fourth standardized moment is computed independently for both the real and vectors, I and Q as was used in imaginary SMAP[3].

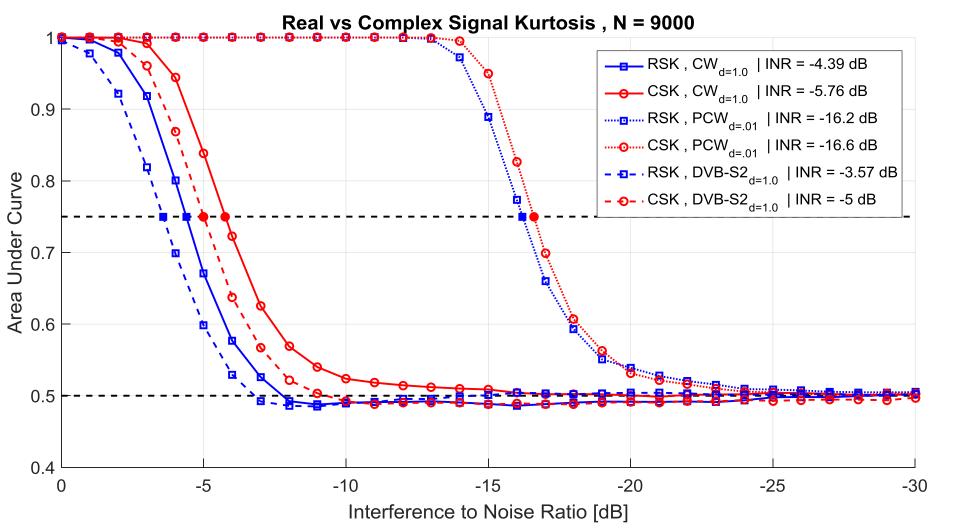
$$RSK_{I} = \frac{\mathbb{E}[(I - \mathbb{E}[I])^{4}]}{(\mathbb{E}[(I - \mathbb{E}[I])])^{2}} - 3, RSK_{Q} = \frac{\mathbb{E}[(Q - \mathbb{E}[Q])^{4}]}{(\mathbb{E}[(Q - \mathbb{E}[Q])])^{2}} - 3$$

The test statistic, RSK (Real Signal Kurtosis), is then defined as

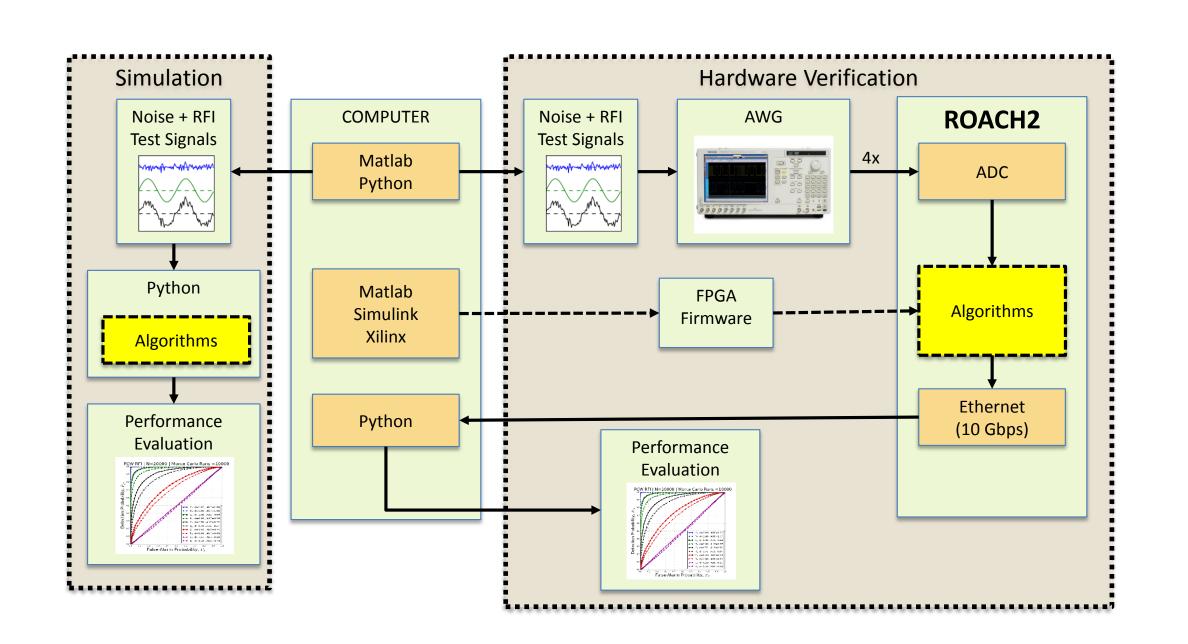
$$RSK = \frac{|RSK_I| + |RSK_Q|}{2}$$

#### Hardware Results





# Methodology



### Moment Calculation

Using the nomenclature for raw moments of the rth power,  $mI^r = \mathbb{E}[I^p]$  ,  $mQ^r = \mathbb{E}[Q^p]$  , full band moments produced to compute kurtosis include.

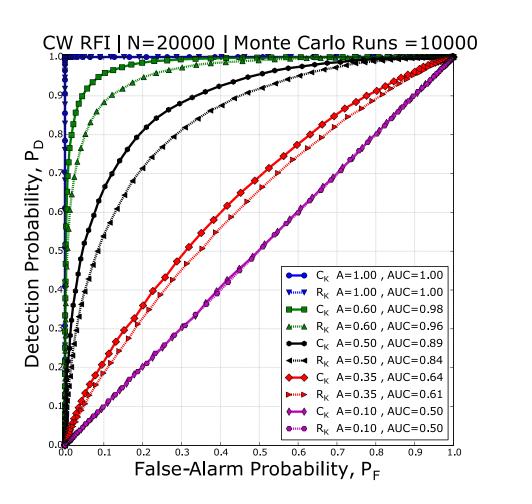
$$\{mI^r, mQ^r\}, r \in \{1,2,3,4\}$$

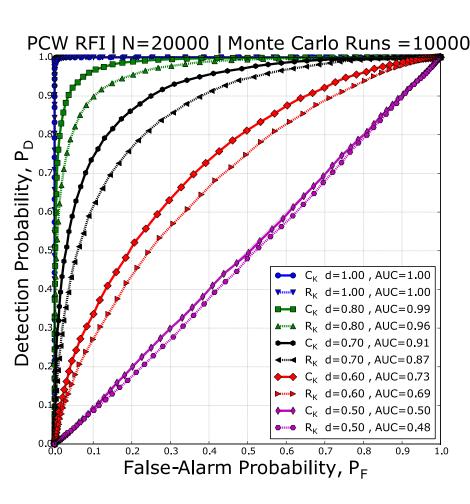
Additionally the following cross complex moments are generated.

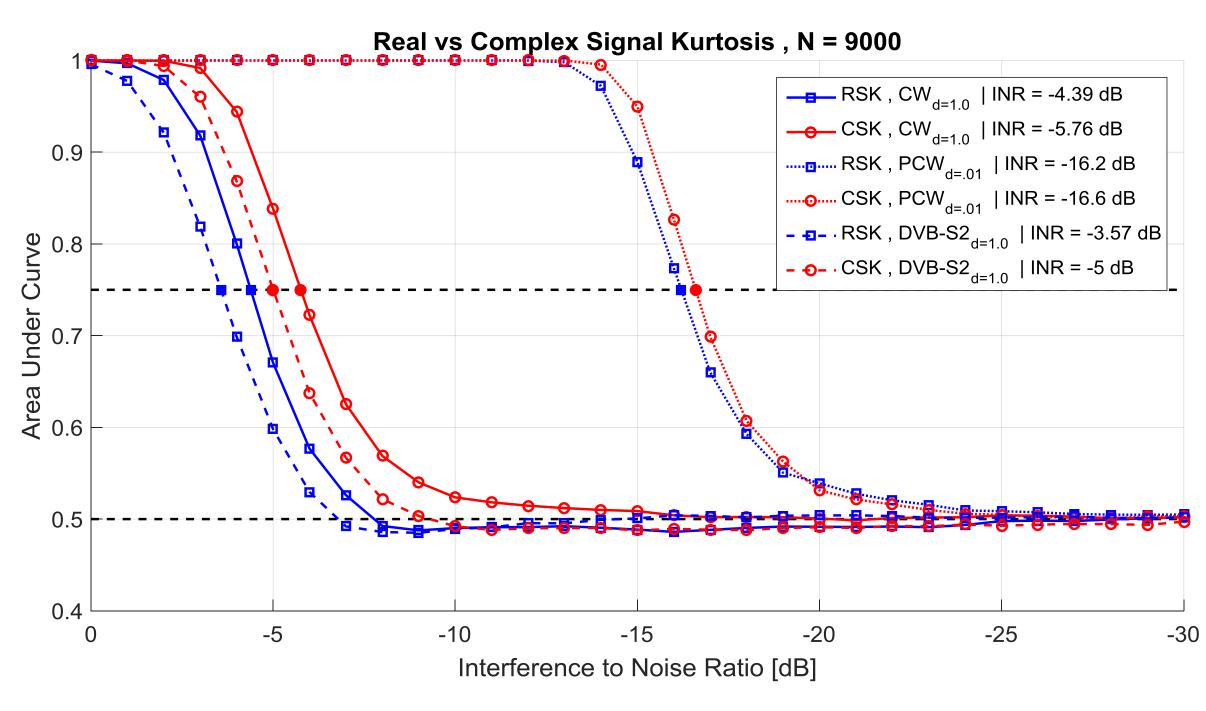
 $\{mIQ, mIQQ, mIIQ, mIIQQ\}$ 

In the case of sub-banding, all 12 moments for each polarization are produced for every sub-band.

#### Simulation Results







#### Conclusions

CSK (Complex Signal Kurtosis) provides a better detection rate than real signal kurtosis.

becomes detectable at Interference (Interference to Noise Ratio) of 2dB lower than what can be detected using RSK (Real Signal Kurtosis).

#### References

- 1. D. C. Bradley, A. J. Schoenwald, M. Wong, P. N. Mohammed and J. R. Piepmeier, "Wideband digital signal processing test-BED for radiometric RFI mitigation," Geoscience and Remote Sensing Symposium (IGARSS), 2015 IEEE International, Milan, 2015, pp. 3489-3492.
- 2. E. Ollila, J. Eriksson and V. Koivunen, "Complex Elliptically Symmetric Random Variables—Generation, Characterization, and Circularity Tests," in IEEE Transactions on Signal Processing, vol. 59, no. 1, pp. 58-69, Jan. 2011.
- 3. J. Piepmeier, J. Johnson, P. Mohammed, D. Bradley, C. Ruf, M. Aksoy, R. Garcia, D. Hudson, L. Miles, and M. Wong, "Radio-frequency interference mitigation for the soil moisture active passive microwave radiometer," IEEE Transactions on Geoscience and Remote Sensing, vol. 52, no. 1, pp. 761-775, January 2014.

#### Acknowledgments

The research team would like to thank the NASA Earth Science Technology Office NNH13ZDA001NACT program for funding this research.