Flight Envelope Information-Augmented Display for Enhanced Pilot Situation Awareness

Kasey A. Ackerman^{*}, Benjamin D. Seefeldt[†], Enric Xargay[‡], Donald A. Talleur[§], Ronald S. Carbonari[¶], Alex Kirlik^{||}, Naira Hovakimyan^{**}

University of Illinois at Urbana-Champaign, Urbana, IL 61801

Anna C. Trujillo^{††}, Christine M. Belcastro^{‡†}, Irene M. Gregory^{§§} NASA Langley Research Center, Hampton, VA 23681

This paper presents an interface system display which is conceived to improve pilot situation awareness with respect to a flight envelope protection system developed for a mid-sized transport aircraft. The new display is designed to complement existing cockpit displays, and to augment them with information that relates to both aircraft state and the control automation itself. In particular, the proposed display provides cues about the state of automation directly in terms of pilot control actions, in addition to flight parameters. The paper also describes a forthcoming evaluation test plan that is intended to validate the developed interface by assessing the relevance of the displayed information, as well as the adequacy of the display layout.

I. Introduction

Automated systems are common in the cockpits of transport class aircraft, and the level of complexity of cockpit automation has steadily increased. There are now many more levels of technology between the pilot and the aircraft control surfaces than were present only a few decades ago. Automated systems have the benefits of improving aircraft handling qualities and reducing pilot workload under normal operating conditions, among other benefits. At the same time, cockpit automation has increased the likelihood of human error, and human factors problems arising from prolific use of automated systems are highly active areas of research. One of the main problems that occurs when tasks are automated is that the true state of the aircraft may be disguised or altogether obscured in the event of a failure or in a vehicle upset condition. Moreover, today's automation is predominantly designed for nominal conditions and often disengages when conditions become off-nominal – which can add further confusion to the crew at the worst possible time and/or result in transient disturbances that further exacerbate the adverse condition. Approaches to reducing the opacity of the automation with respect to the flight crew include pilot training, system design tools, and feedback displays [1].

In this paper, we adopt the latter approach; we design a display that incorporates tools and devices that are already familiar to the pilot to provide information about the vehicle dynamical state, and augment it with additional information about the state of onboard automation. In particular, we present here the design of a novel pilot interface designed around a dynamic Flight Envelope Protection (FEP) system augmented with logic for loss-of-control (LoC) prediction and prevention implemented on NASA's Transport Class

[†]Doctoral Student, Dept. of Computer Science; seefldt2@illinois.edu.

^{*}Doctoral Student, Dept. of Mechanical Science and Engineering; kaacker2@illinois.edu. Student Member AIAA.

[‡]Postdoctoral Research Associate, Dept. of Mechanical Science and Engineering; xargay@illinois.edu. Member AIAA.

 $[\]$ Associate Aviation Education Specialist, Institute of Aviation; dtalleur@illinois.edu.

 $[\]P Research \ Programmer, Beckman Institute; rcarbona@illinois.edu.$

^{||}Professor, Dept. of Computer Science; kirlik@illinois.edu.

^{**}Professor, Dept. of Mechanical Science and Engineering; nhovakim@illinois.edu. Associate Fellow AIAA.

^{††}Senior Research Engineer, Crew Systems and Aviation Operations Branch; a.c.trujillo@nasa.gov. Member AIAA.

^{‡‡}Senior Research Engineer, Dynamic Systems and Control Branch; christine.m.belcastro@nasa.gov. Associate Fellow AIAA.

^{§§}Intelligent Flight Systems Technical Lead, Research Directorate; irene.m.gregory@nasa.gov. Senior Member AIAA.

Model (TCM) [2,3]. Incorporation of envelope protection into the flight control system, while desirable to prevent the aircraft from entering unsafe conditions, necessitates improved pilot feedback methods. In the event that the FEP system intervenes, the pilot is forced to infer its action through the aircraft performance indicators or through some other alert. The objective of the display design is therefore to reduce the opacity of the automated FEP system by presenting dynamic flight envelope limit information in reference to both the aircraft performance indicators and the pilot control input space, as well as displaying the state and output of the protection system.

The remainder of this paper is organized as follows: Section II presents the motivation for the design and integration of the display, and Section III provides background information related to the flight control system and FEP system. Sections IV and V discuss the design and operation of the proposed cockpit display, and Section VI provides discussion of a forthcoming piloted simulation test plan for display evaluation. Section VII offers some concluding remarks.

II. Motivation

Two factors have promoted a significant increase over recent decades in the level of research devoted to achieving safe and effective human-automation interaction. As described in [4], the 1980s saw the implementation of significantly higher levels of automation functionality in aviation, such as flight management computers, known colloquially as a transition to the "glass cockpit." This transition resulted in the identification of numerous problems in coupling flight crews with automated systems [5], and it took about two decades of research, redesign, and new training methods before pilot confidence in automation and pilot proficiency in using automation effectively became widespread.

Yet, problems associated with achieving a safe and efficient integration of pilots and flight control automation continue to exist, most typically as a result of the inability of flight crews to understand the true state of the aircraft and the state of the onboard automated systems. These problems have resulted in a number of high-profile commercial aviation accidents. For example, the crash of Air France flight 447 was the result of the failure of the automation to clearly disclose sensor inconsistencies as detected by the automation until the disconnection of the autopilot [6]. In another incident, American Eagle flight 4184 crashed near Roselawn, IN after automation returned control to pilots with no indication of current envelope limitations for safe control input or recovery under icing conditions [7]. Additionally, automation actions not desired nor understood by the pilots resulted in the crash of Scandinavian Airlines flight 751 [8]. Much more recently, misunderstanding of the autothrottle operation during approach led to the collision of Asiana Airlines flight 214 with the runway seawall in San Francisco [9]. In each of these incidents, the state of the automated systems was opaque to the flight crew, and in some cases the actions of the automation obscured the state of the aircraft as well. As the level of automation in the cockpit increases, it becomes ever more important to improve the pilot interface to provide the flight crew with an intuitive and veridical representation of not only the state of the aircraft, but also the state of the onboard automated systems.

Recently, advanced control automation has been broadly implemented for commercial and research applications, prompting novel concepts for more flexibly and robustly designing human-automation interaction, most notably, techniques for adaptive automation, adaptable automation, adjustable autonomy, and mixed-initiative control schemes [10–12]. For example, the adaptive automation approach attempts to make automation more intelligent so it provides humans increased support when it is most needed, as in conditions of high workload. Alternatively, the adaptable automation approach gives humans discretionary control over the level of automation active at any time. Adjustable autonomy and mixed initiative schemes are even more sophisticated, seeking to emulate a flexible, shared or distributed control allocation scheme between humans and automation akin to how teams of people self-organize and reconfigure their responsibilities in the face of changing circumstances and task demands.

At this point no single magic bullet yet exists for designing the safest and most effective humanautomation interaction protocol in the general case. Universal agreement, however, does exist on at least a few tenets for supporting robust and effective human-automation interaction. First, and motivated in part by aforementioned examples of incidents and accidents due to automation failure, agreement exists that the ultimate authority for mode of control (human vs. automation) will rest with the human operator [13]. Due to the inability of engineers to anticipate all possible situations, events, failures, etc., it is only realistic to put ultimate control authority in the hands of the human, who may at least have the opportunity to improvise [14] a control solution for unanticipated situations, or situations thought to be virtually impossible (e.g., in aviation, a double bird-strike failing two engines simultaneously, as with US Airways flight 1549, or an engine failure knocking out all three of an aircraft's hydraulic systems, as in United Airlines flight 232).

A second uncontroversial tenet is that automation that draws the operator out of control loops does so at the cost of the human's situation awareness [15, 16], resulting in a problem known as "out-of-the-loop" syndrome. As described in [17], the problem is not so much "over-automation" but instead the fact that all too often automation is designed without providing the operator with sufficient feedback on its current and future behavior. As such, there is tremendous motivation for novel cockpit interface design solutions that will allow the pilot, while remaining in the control loop, to be maximally informed about the underlying, often opaque, state of control automation. Specifically, the adoption of interface designs that provide adequate feedback to maximize pilot situation awareness with respect to aircraft automation has the opportunity to improve aviation safety by directly addressing human-automation interaction issues. In the rest of this paper we present an attempt to apply the aforementioned design tenets to an augmented aircraft model with an automated FEP system.

III. Background

III.A. iReCoVeR Control Architecture

The Integrated Reconfigurable Controller for Vehicle Resilience (iReCoVeR) is part of an ongoing research collaboration between researchers at the University of Illinois at Urbana-Champaign (UIUC) and the University of Connecticut (UConn), in an effort to develop technologies to prevent accidents and incidents resulting from LoC events in transport class aircraft. The iReCoVeR architecture is based on the AIRSAFE concept [18–20], and integrates technologies for fault-tolerant flight control [21, 22], fault detection and isolation [23], safe flight envelope estimation and protection [2], and LoC prediction and prevention [3]. Under this concept, the core subsystems of the iReCoVeR architecture work together to arrest the development of an LoC sequence by breaking the chain of events at its different stages. In addition, to ensure a robust interaction between pilots and the iReCoVeR automation, the framework also envisions the design and integration of enhanced cockpit interfaces. These interfaces should be conceived to make the behavior of the iReCoVeR automation transparent to the flight crew by providing timely and effective situation awareness, not solely about the aircraft, but also about the current and future operation of the developed automation. The iReCoVeR architecture along with the situational awareness interfaces are shown schematically in Figure 1.



Figure 1: The iReCoVeR flight control architecture for loss-of-control prevention.

III.B. Flight Envelope Protection System

In [2], the authors present the design and implementation of a dynamic FEP system, which is one of the core subsystems of the iReCoVeR architecture. The FEP system ensures that the aircraft remains within a predefined (dynamic) portion of the flight envelope that is determined to be safe. The protection scheme is based on a command-limiting architecture that is designed to protect excursions in angle of attack, angle of sideslip, pitch angle, bank angle, vertical load factor, airspeed (or dynamic pressure), and total specific energy. The protection scheme related to flight parameters of the *longitudinal dynamics* of the aircraft has a hierarchical structure based on the criticality of each flight parameter, and relies on dynamic inversion control laws to anticipate limit exceedances and, when required, generate command signals that prevent the protected flight parameters from exceeding their corresponding limits. The *lateral-directional* protection scheme instead has a parallel architecture that relies on simple control laws designed to prevent excursions in bank angle and angle of sideslip. Moreover, a pitch-to-bank cross-feed prevents overspeed limit exceedances in tight turns. The system also includes a *total energy* protection scheme that adjusts engine power setting and speedbrake deflection to prevent the aircraft from flying into inadmissible energy states. Figure 2 shows a functional block diagram of the dynamic flight envelope protection system proposed in [2].



Figure 2: Functional block diagram of the command-limiting flight envelope protection scheme.

The protection system is augmented with an LoC-prediction logic that actively controls the limits of the protected envelopes; see [3]. These dynamic limits, which characterize the safe flight envelope at a given time, are constrained to vary between appropriately defined *absolute limits* (which are to be understood as "never-exceed limits") and more restrictive *LoC limits*, depending on aircraft configuration and flight condition^a. Figure 3 shows the set of limits used in [3] for the FEP system developed for NASA's TCM. The limits appear grouped in three two-dimensional envelopes relating to aircraft aerodynamics, flight dynamics,

^aThe design of the LoC-prediction logic described in [3] is based on the quantitative definition of loss of control proposed in [24].



Figure 3: Absolute and loss-of-control limits used in [3] for the flight envelope protection system developed for NASA's TCM. (*Solid blue:* loss-of-control limits; *solid red:* absolute limits.)

and structural integrity. We note that throughout this paper we will refer to the dynamic limits used by the protection scheme as *hard limits*, while the more restrictive LoC limits will be referred to as *soft limits*.

Because the FEP system can override the commands generated by the pilot, it is critical to augment this automation with cockpit interfaces that provide appropriate feedback to the flight crew, so as to mitigate potential negative interactions between the pilot, the protection system, and the aircraft. In the next section, we propose a novel interface display that is intended to make the behavior of this protection system maximally transparent to the pilot. The design of the new display builds upon a standard general-aviation primary flight display, which is then augmented with both quantitative and qualitative information provided by the FEP system. The newly added information relates to both aircraft state and pilot control inputs, and thus the proposed display provides cues about the state of automation directly in terms of pilot control actions, in addition to flight parameters. Moreover, as will become clear later in the paper, the automation-interface system can be operated such that the protection system does not override pilot commands, but it is only used to provide "suggested" commands to the flight crew through the developed interface.

IV. Display Design

The instrument panel used for this project is designed to represent the critical flight parameter ranges for a medium sized transport category aircraft, based on NASA's TCM dynamical model. The layout of the instrument panel display elements closely follows the primary flight display (PFD) used to fly the NASA AirSTAR vehicle [25]. Although the AirSTAR PFD was presented as a modified heads-up display, the adaptation presented in this paper necessitates a heads-down configuration that precludes any outthe-window information from being presented. Furthermore, this modified arrangement is in line with the blended primary flight display discussed in [26], and is a format that has been adopted in Boeing transport category aircraft.

The PFD, shown in Figure 4, consists of the flight instrumentation superimposed on a black background. Display elements are in lighter contrasting colors that can be easily differentiated and comply with FAA and industry recommendations for electronic display color coding [27]. Display instrumentation can be differentiated via (i) a break in background coloring, (ii) display element coloring and/or shape, and (iii) placement relative to the central flight instrument. The addition of three new displays to the instrument panel facilitate the transfer of new flight parameter information to the pilot. However, the placement of two of the new displays directly next to the attitude indicator, while designed to support pilot awareness of energy information, is in conflict with the regulatory requirement of FAA 25.1321(b) for electronic display of flight instrumentation. However, since these displays are being investigated for their utility in maintaining energy state awareness, it is necessary to place them in locations that are most congruent with the pilot's expectations.



Figure 4: Primary flight display with FEP limit augmentation.

IV.A. Primary Flight Display

IV.A.1. Airspeed Tape

The airspeed indication is located to the left side of the instrument panel to form the T-line concept (also referred to as the Basic-T); the "T" being formed by the command indicators of the airspeed, altitude and neutral pitch bar aligned horizontally to each other [26, 27]. The indicator is of the vertical tape style with white numerals superimposed on a dark grey background. Major airspeed values indicated by tick marks at every 20 knots calibrated airspeed (KCAS), and unlabeled tick marks at every 10 KCAS. Current airspeed is indicated in a white bordered box marker and is centered vertically in the tape scale.

Additional symbology has been added to the airspeed indicator to provide the pilot with FEP-derived airspeed limit information. A pair of yellow bars are added to the airspeed tape to provide the pilot with an indication of the FEP upper airspeed limit. The soft limit is coded by a yellow bar that crosses the normal airspeed tick marks and extends to a large yellow tick mark that indicates the (dynamic) hard limit, nominally 350 KCAS. The lower limit for airspeed is indicated by a red and white tape superimposed on the airspeed tape, to maintain consistency with current practice for indication of critically low airspeed.

IV.A.2. Angle of Attack Scale

Inset between the airspeed tape and the attitude indicator, the angle of attack (AoA or α) indicator is a new display feature and represents the range of AoA values possible for this transport category model. Its location next to the airspeed tape facilitates a quick comparison during critical flight phases such as slow speed operations. As opposed to a current indication box marker, the AoA tape display utilizes a running bar scale with a chevron-shaped marker to indicate the current AoA value. Slightly less salient size and color differentiates this tape scale from the nearby airspeed tape. Major AoA increments are indicated by labeled tick marks at every 10 degrees with unlabeled tick marks every 5 degrees in-between. The full range is always displayed on the tape and is representative of simulation data [2].

FEP-derived limit symbols have also been added to the AoA scale. Upper and lower hard and soft limits are displayed to indicate the boundaries of the safe range of AoA. Soft limits are indicated by a yellow bar crossing the normal AoA tick marks and hard limits are indicated by yellow bars parallel to the normal tick marks. The range of safe AoA values between the positive and negative hard limits depends on the location of the aircraft with respect to the three envelopes in Figure 3, as described in Section III.B. Additional description of how the FEP limits are modified can be found in [3].

IV.A.3. Attitude Indicator

Sizing of the attitude indicator display was modeled directly from a Rockwell Collins EFIS-700 electronic flight system attitude-direction-indicator unit. Display elements presented in the attitude indicator include a conventional pitch (θ) ladder with major labeled increments at every 10 degrees and minor increments every 2.5 degrees. Red chevrons are visible in the ladder at ± 50 degrees and serve to advise the pilot as to the direction of neutral pitch during extreme attitude maneuvering. At the top of the attitude display is an angle of bank (ϕ) arc with major tick marks at 30 and 60 degrees and minor tick marks at every 10 degrees. By design, the angle of bank indicator does not serve as a sky pointer, but retains its aspect to the pitch indicator ladder during banked flight. In keeping with the standard coloring, the background area above zero degrees pitch is blue and below zero degrees is brown [27]. Current pitch is indicated by a black pitch dot with miniature wings.

Four sets of soft and hard limit bars are added to the attitude indicator representing the FEP limits. For pitch limits, a vertical yellow bar crossing the pitch ladder indicates the soft limit and a horizontal bar parallel to the pitch ladder tick marks indicates the hard limit for both positive and negative pitch values. Bank angle soft limits are indicated by a yellow arc that crosses the angle of bank tick marks, while hard limits are indicated by a yellow bar parallel to the tick marks. Both pitch and bank angle limits are a function of aircraft location with respect to the three envelopes of Figure 3, as described in Section III.B and in further detail in [3].

IV.A.4. Altimeter Tape

The altimeter indicator is of standard tape design and is located to the right of the attitude indicator. Major tick marks are labeled every 200 ft with minor unlabeled tick marks at 100 ft. Coloring is the same as for the airspeed indicator. Current altitude is indicated in a command marker box similar in appearance to that used for airspeed.

IV.A.5. Vertical Speed Indicator

The vertical speed indicator is of standard design and located to the right of the altimeter indicator tape. Coloring is the same as for the airspeed indicator. The display has major tick marks appropriate to the range of the aircraft's performance. Major tick marks are labeled at 1000, 2000, and 6000 feet-per-minute and minor tick marks at 500 ft/min between zero and 2000, and 2000 ft/min between 2000 and 6000. Current vertical speed is indicated by a white running bar that extends from zero. The zero point is level with neutral pitch, as well as the command box indicators for the airspeed and altimeter tapes.

IV.A.6. Load Factor Scale

Between the attitude indicator and the altimeter tape is a new display to indicate load factor in the z-axis. Similar to the AoA scale, the load factor (n_z) display utilizes a running bar scale with a chevron-shaped marker to indicate the current n_z value. Slightly less salient size and color differentiates this scale from the nearby altitude tape. The scale ranges from -1g to 4g with major load factor increments indicated by labeled tick marks at every 1g and unlabeled tick marks every 0.5g. The full range is always displayed on the tape and is representative of simulation data [2].

As with other protected flight parameters, upper and lower FEP limits are superimposed onto the load factor scale to provide the pilot with an indication of the aircraft's proximity to the envelope limits. Soft limits are indicated by a yellow bar crossing the normal load factor tick marks and the hard limits are indicated by a yellow bar parallel to the normal tick marks. The range of safe load factor values between the positive and negative hard limits depends on the location of the aircraft with respect to the envelopes of Figure 3, as described in Section III.B and [3].

IV.A.7. Angle of Sideslip Scale

The sideslip scale is a new display feature and represents the range of expected possible sideslip angles (β) that can occur during flight for this aircraft model. The scale is located directly below the attitude indicator and uses the same layout and coloring as the angle of attack and load factor scales. The scale is zero-centered and ranges from -15 to 15 degrees with tick marks and labels every 5 degrees. Here positive values indicate

right sideslip. The inclusion of this new display renders the standard split trapezoid sideslip indicator at the top of the attitude indicator redundant; therefore the split trapezoidal indicator is not displayed.

The FEP limits for this display element are indicated by yellow bars as a function of aircraft location with respect to the envelopes of Figure 3. Similar to the other limit indicators, soft limits are indicated by a yellow bar crossing the normal sideslip tick marks and hard limits are indicated by yellow bars parallel to the normal tick marks.

IV.A.8. Heading Indicator

The heading indicator arc is located below the sideslip scale and completes the T-line arrangement of critical flight instrumentation. Presented as a partial arc, 110 degrees of heading (ψ) are visible with a current heading command marker box at the top of the scale. A lubber line extends below the scale as in conventional horizontal situation indicators. Coloring of the scale is the same as the airspeed indicator. Tick marks indicate every 5 degrees of heading, with major tick marks every 10 degrees and labels every 30 degrees.

IV.B. Envelope Protection Display

The FEP system described in [2] and [3] limits pilot control inputs to prevent violations of critical flight parameter limits. Pilot control inputs and safe flight envelope limits are monitored by the FEP system, which modifies the control inputs as necessary to keep the aircraft within this set of safe operational envelopes.

To the right of the PFD, the Envelope Protection Display (EPD) – shown in Figure 5 – is a new display that indicates the pilot control inputs and the modifications to these inputs by the FEP system. The display represents an indication of the available control authority^b, accounting for both pilot intent (yoke, wheel, pedal, and throttle control inputs) and aircraft safety (safe envelope violations). The display in a way also represents a mapping of the FEP limits into the aircraft control input space, indicating the pilot commands required to maintain safe operation of the aircraft. All of the elements of the EPD, which are described in detail in the remainder of this section, are driven by the FEP system logic. In this sense, the development of this display does not require the implementation of any significant additional logic in the control architecture presented in [2, 3].



Figure 5: Envelope Protection Display.

^bHere, we refer to *control authority* as the margin between the current pilot command input and the FEP input space limits, not necessarily the available control surface deflection with respect to actuator limits.

IV.B.1. Pilot Input Display

The Pilot Input Display (PID) consists of a square pitch/roll command box positioned directly to the right of the PFD, approximately the same size as the attitude indicator, and a horizontal yaw command bar below the box. Horizontal and vertical axes bisect the box, with the intersection of the axes level with the neutral pitch indicator. The vertical axis is an indication of pitch-axis control input, and follows a "nose-pointing" convention for positive and negative pitch commands. Thus a more positive control input (higher vertical position within the box) will pitch the aircraft nose up. The horizontal axis indicates roll-axis control inputs. Both axes are normalized from -1 to 1 such that the edges of the box represent the maximum possible values for the inputs. Axis tick marks are set to 0.2, representing 10% of the total input range. The yaw bar is positioned directly below the box and indicates yaw channel input commands. The upper and lower limits of the yaw bar are normalized in the same manner as the pitch and roll axes, with tick marks every 0.2. The edges of the pitch/roll box and the yaw bar are white to ensure visibility against a black background.

Within the pitch/roll box is a light gray box with dynamic borders defined by yellow bars. The interior of the light gray box defines the set of "safe" control inputs^c. Restriction of control inputs to within the light gray box will ensure that the aircraft never exceeds the hard FEP limits and does not enter into a potentially unsafe state as defined by the envelopes of Figure 3. The area of safe control inputs is dynamic and changes as a function of aircraft state and pilot inputs. In certain conditions, the safe area may shrink down to a point; in this case the point represents the only safe input (or the safest input). Any unsafe portion of the pitch/roll box (defined as being outside the yellow-bordered safe area) is shaded in dark gray. The safe area of the yaw bar is defined by a light gray interval with yellow edge markers, with unsafe areas shaded dark gray. Functionality of the yaw bar is the same as that of the pitch/roll box.

The PID also shows control inputs, which are indicated by round markers on the pitch/roll box and vertical bars on the yaw bar. A blue marker indicates the control input set by the pilot. In addition, a green marker indicates the actual control input that is being sent to the aircraft as computed by the FEP, i.e., the most preferable control input, taking into account both pilot intent and aircraft safety. Whenever the pilot sets a safe control input, the command of the FEP is identical to the pilot command, and the input is shown as a blue marker with a green halo.

IV.B.2. EPR Scale with FEP Display

The engine pressure ration (EPR) scale provides the pilot with an indication of power produced by each engine, and is controlled via the throttle lever for both engines. For each engine, a white chevron-shaped command marker indicates the commanded EPR level corresponding to the current setting of the throttle lever. Two blue bars extending upwards from the bottom of the tape indicate the actual EPR of the engines. A digital readout of EPR is shown just below the tape for each respective engine. The color convention for the EPR scale is slightly different than that for the PID. The engine dynamics are slow compared to the aircraft pitch, roll, and yaw dynamics, where the aircraft response is roughly equivalent to the commanded input. It is therefore necessary to indicate the actual state of the engines as well as the command, with the engine state shown as the blue marker.

Since the FEP system is designed to protect vehicle energy through use of throttle/EPR, additional features are added to the EPR scale. The EPR FEP display is similar in operation to the PID. A safe area is indicated by a light gray area on the EPR scale, with yellow horizontal bars indicating the upper and lower limits of the safe zone. Unsafe areas are shaded dark gray. A horizontal green bar indicates the actual EPR command that is being sent to the aircraft as computed by the FEP system. If the pilot sets a safe throttle command, the pilot and FEP commands are coincident.

IV.B.3. Flap Scale

The flap scale is located to the right of the EPR scale and indicates current flap setting in degrees. Flap settings of 0, 1, 5, 15, 20, 25, and 30 degrees are shown. The commanded flap setting is indicated by a white chevron-shaped command marker, and the actual flap deflection is shown as a blue bar extending downward from the top of the tape.

^cThe authors in [28, 29] use a similar representation to communicate estimates of "safe" control input bounds which, if violated, would potentially result in flight envelope limit exceedances. In those works, the bounds are computed via model predictive control techniques and are presented as minimum constant control inputs that would lead to envelope violations at the end of a pre-specified prediction horizon. In a separate work, the authors of [30] use optimal control techniques to provide visual and haptic input-space pilot cues for vehicle upset recovery.

IV.B.4. Speedbrake Scale with FEP Display

The speedbrake scale provides the pilot with an indication of the (symmetric) spoiler deflection used as speedbrake, and is controlled via the speedbrake lever. A white chevron shaped command marker indicates the commanded speedbrake deflection. A blue bar extending downwards from the top of the tape indicates the actual speedbrake deflection.

The FEP system is designed to protect (maximal) vehicle energy through use of the speedbrake. As with the EPR display, a green marker indicates the actual speedbrake command that is being sent to the aircraft as computed by the FEP system.

IV.B.5. FEP State Annunciator

An FEP state annunciator has been added above the PID to indicate the current functional mode (or submode) of the FEP. When the FEP system is "On" but not actively modifying the pilot command, the system is "Armed" and the annunciator shows the label "FEP Armed" in black on a yellow background. If the FEP overrides at least one of the control inputs set by the pilot, the annunciator turns green and the label changes to "FEP Active", also in black. The color green has been chosen to be consistent with the green markers on the control-input displays that represent the most preferable control input.

V. Display Operation

V.A. Normal Operational Mode

The FEP display has been created to facilitate pilot situation awareness with respect to the automated FEP system. Piloted simulations have revealed that pilots may react adversely to this type of command-modifying automation if they are not aware that (i) their command is being modified by the automation, and (ii) why the automation is modifying their command. For example, in a simulated severe wind shear event using only conventional flight instruments, the FEP system commanded a nose-down pitch to prevent an imminent stall. The pilot, unaware that the FEP had intervened, felt he had "lost control" of the aircraft, when in fact the FEP had potentially prevented an LoC event from occurring. The proposed display is an attempt to provide this information to the pilot in an intuitive, veridical, and unintrusive manner. It is not claimed that the proposed display format is optimal in any sense; however, the *information* that the display provides is the critical aspect of its design. The display provides necessary information to the pilot about the state of the automation that previously has not been readily available. As will be demonstrated shortly, the FEP information feedback is provided to the the pilot both in the *output space* (vehicle performance as indicated by the PFD) and in the *input space* (vehicle control inputs as indicated by the EPD) in a non-redundant manner.

During normal operation with the FEP system "On" and the pilot command within the safe region of the input space, the FEP system is referred to as "Armed." The protection system is actively monitoring the aircraft state and will intervene by limiting the pilot commands in the event that the pilot inputs an unsafe command, or if the vehicle impinges on an unsafe portion of the flight envelope. The FEP system is said to be "Active" when it is actively limiting pilot commands.

As an illustration, consider the following scenario. Initially, the aircraft is in level flight at roughly 200 KCAS. The aircraft is given a pitch-up command and held at higher than normal pitch attitude with the throttles near idle, as shown in Figure 6a. As the vehicle loses airspeed, the angle of attack increases toward the hard upper limit. With the aircraft still being commanded to pitch up, the FEP detects that the vehicle is nearing an unsafe portion of the flight envelope and reduces the safe input space area to pitch the aircraft nose down and prevent stall, as shown in Figure 6b. Here, the blue dot indicates pilot intent, while the actual command sent to the vehicle by the FEP, depicted by the green dot, remains within the safe portion of the input space. Together with the appearance change of the FEP annunciator, this indicates both that the pilot command is in conflict with the FEP and how the pilot's command is being modified. Additionally, the performance indicators around the PFD on the left of 6b show that airspeed and AoA are at the FEP limits, and there is a color change of the AoA limit to red to highlight the limiting variable(s).

While the scenario presented above is simplistic, it is illustrative of the motivating concept. The EPD, along with the modified PFD, is a means to communicate to the pilot the state of the aircraft and the state of the automated FEP system. The PFD provides performance indicators which allow determination of

the state of the aircraft in both absolute sense and in relation to the safe flight envelope limits. The EPD indicates pilot control inputs and the modifications to these inputs as implemented by the protection system, and presents an indication of the available control authority with respect to the FEP limits. In some sense, the display is also a means by which to map the FEP limits into the aircraft control input space, indicating the commands required to maintain safe operation of the aircraft with respect to the flight envelopes of Figure 3. The combination of the FEP display and PFD therefore is an attempt to allow the pilot to quickly determine the state of the aircraft and the automation, as well as the *intent* of the automation. In essence, to communicate not only *what* the automation is doing, but also *why* the automation is taking a particular action.

It is important to note that the FEP information displayed in the PFD and in the EPD is *not* redundant, as information is not duplicated between the two displays. The PFD contains information about the vehicle state, in the output space of the system, and informs the pilot of vehicle aircraft response and location in relation to protected flight parameters. However, in the case of the FEP system, the automation state is not directly observable to a pilot through the augmented PFD; it is not clear whether the FEP system is modifying the pilot commands from the vehicle performance indicators and parameter limits alone. For example, an aggressive command near the boundaries of the safe flight envelope may be limited by the FEP before the vehicle actually approaches the boundary. Alternatively, the aircraft could be right on the edge of the safe flight envelope, which would manifest on the PFD as one or more parameters at the hard limit(s), but a pilot command that holds this aircraft state constant would not necessarily be modified. Under certain conditions, the pilot may be able to discern whether or not the system is actively modifying the commanded input, but this relies heavily on the pilot's mental model of the system and increases pilot workload, hence additional information is needed. Moreover, information from the EPD is not duplicated on the PFD. The control input limits of the EPD contain no specific information about the state of the aircraft, only the restriction on the control inputs imposed by the set of flight envelope limits.

To illustrate this point, consider the situation presented in Figure 6c. The aircraft is banked at 30° , and the pilot commands an aggressive pitch-up and roll maneuver, represented by the blue dot in the upper left corner of the EPD. The FEP anticipates that following this command will cause imminent violation of the safe envelope limits, and limits the commands to maximum safe value. Notice here that the aircraft is not in violation of any of the hard or soft limits shown on the PFD in Figure 6c, and there is no indication on the PFD as to why the vehicle performance is different from what the pilot commanded. Only by presenting the information from the input space is it clear why the vehicle response is different from the commanded response.

Finally, we note that it is in no way the intent of the authors to suggest that the format of the display presented here is the best format for implementation in the cockpit. The location and sizing of the EPD, and the limit displays on the PFD are designed to evaluate their efficacy during simulation-based testing. The design of the display elements themselves are a first attempt at providing FEP information to the pilot in a simple, intuitive, and veridical manner, and it is highly likely that these elements would undergo many design and testing iterations prior to any real-world implementation. However, the key point of emphasis is not the physical representation of the information, but rather the information itself. Providing the pilot with enough information to be able to observe the aircraft and automation state in both the input and output space makes the system more observable to the pilot, places less reliance on the pilot's mental model of the automation, and reduces likelihood of adverse human-automation interaction. Determination of the "best" information and method of presentation is a difficult open problem; the display presented here is one attempt at improving human-automation interaction in the cockpit of an augmented aircraft.

V.B. An Alternative Mode: FEP Information without Intervention

The logic which drives the FEP calculation of envelope limits and safe control inputs can also be leveraged to assist pilots without actually limiting pilot commands. In this alternative mode, the FEP logic is running but the system will not alter the pilot commands in any way; the pilot has complete authority over the aircraft at all times. The envelope limits are still displayed on the PFD and operate exactly the same as previously described. Additionally, the EPD is shown with the dynamic safe control input box, which also operates as previously described. The safe input command as calculated by the FEP, accounting for pilot intent and aircraft safety, is displayed as a green dot, but the pilot command, represented by the blue marker, is always sent to the aircraft. If the pilot command is outside of safe control input area, a red halo appears around the blue marker to indicate that the FEP has determined the command to be unsafe, and also to



(a) FEP armed, no envelope violations and pilot input within safe command area.



(b) FEP actively modifying pilot input to prevent angle of attack limit violation.



(c) Aggressive pilot input triggering FEP command modification without PFD limit impingement, demonstrating non-redundancy of the two displays.

Figure 6: Extended flight display in normal operational mode with FEP "On."

distinguish between normal and alternative operational modes. Also, the FEP annunciator changes from gray to red as a reminder that the FEP will not intervene. If the pilot command is always within the safe control input area, then as before, the FEP suggested command and pilot command are identical and the aircraft will not exceed the protected parameter envelopes of Figure 3.

To demonstrate this alternative mode, consider the same scenario as in Figures 6a and 6b. The aircraft is held at high pitch attitude with throttles near idle, as shown in Figure 7a. As airspeed drops and the angle of attack increases, the pilot command falls outside of the safe control input area. The red halo appears around the pilot input and the green dot indicates the closest safe command as calculated by the FEP logic; see Figure 7b.

The alternative mode retains the flight envelope information generated by the FEP, but avoids some of the human-automation interaction issues that arise from limiting pilot control authority, albeit at the cost of absence of envelope protection and LoC prevention. Another benefit of the alternative mode (as opposed to lack of any display augmentation) is that the system is able to provide a suggested command to recover the aircraft from an unsafe condition. At extreme attitudes or flight conditions where envelope violations are more likely to occur, it is not always clear to the pilot the correct course of action to recover the aircraft, especially since these situations may often be accompanied by failures, alarms, or other factors which drastically increase pilot workload. The ability to provide a suggested input to recover the aircraft to within the safe portion of the flight envelope, especially in a potentially confusing, high-workload environment, may be of great benefit and could potentially support pilot training for upset recovery. Early simulation data have indicated that by tracking the suggested command (i.e., tracking the green dot on the EPD), the aircraft can be recovered to a safe state while accounting for vehicle safety (structural integrity, stall, etc.).

VI. Piloted Simulation Evaluation

Testing of the new cockpit interface will be conducted using the pilot-in-the-loop flight simulator at the Illinois Simulator Laboratory, a Beckman Institute facility at UIUC. The simulator, shown in Figure 8, is based on a Frasca 142 cockpit, with three projectors providing a roughly 180° view of the "world." The simulator uses the NASA TCM aircraft dynamics model running in Matlab/Simulink, and graphics are driven by an array of computers running X-Plane. In the cockpit, flat panel digital monitors are used for the pilot display interface, and an eye-tracking camera system is used to monitor pilot attention. The dynamics model, graphics computers, cockpit display, and camera system are interfaced through a local area network. Additional details about the simulator facility can be found in [31].

To evaluate the efficacy of the extended flight display, a study is proposed consisting of multiple pilot subjects of adequate skill level to fly a series of simulation-based flight tests. Eighteen participants will be recruited from the Parkland College Institute of Aviation at UIUC. Each participant will receive a familiarity training session followed by three one-hour sessions, one of which is a control condition, and the other two are experimental conditions. The familiarity training session is intended to allow the participants to become familiar with the flight dynamics of the simulated aircraft, as well as the instrument panel and control layout, and requires participants to fly a skill pattern performing standard flight maneuvers. During familiarity training there will be no external environmental disturbances, visibility will be high, and the pilot will have a clear sightline to the outside horizon. For this session, standard glass cockpit-style instrumentation will be used (i.e., only the PFD without FEP limit augmentation, flap scale, and speedbrake scale without FEP indication will be displayed to the pilot) and the FEP system will be "Off."

After familiarity training, each participant will fly the simulation through one control condition and two experimental conditions. Condition ordering is counterbalanced among participants to reduce learning effects from one condition to another. Each session will include ten wind disturbance scenarios, each lasting approximately two minutes. To ensure the difficulty across all conditions and participants is equal, the same ten scenarios will be used for each participant. The ordering of these scenarios will be randomized for each condition, and repeated for each participant. That is, for each of the control and experimental conditions, the order of the ten disturbance scenarios will be randomized, however the ordering is invariant with respect to participants for a particular condition.

The operational mode of the display will vary for each of the control and experimental conditions. For the control condition, the display configuration is identical to that used for the familiarity training session; a standard PFD without FEP limit augmentation is used and the FEP system is "Off." The pilot will be in complete manual control of the aircraft during the disturbance scenarios. For the first of the two



(a) No limit violations, pilot command within safe command area.



(b) Upper angle of attack limit is violated and the pilot command is shown outside of the safe command area.

Figure 7: Extended flight display operating in the alternative mode with FEP "Off."

experimental conditions, the display will be operating in the alternative mode described in Section V.B. The augmented PFD and PID are displayed with the FEP logic providing suggested commands, envelope limit information, and safe control input limit information. The second experimental condition will be conducted with the display in the normal operational mode described in Section V.A, where the FEP will modify pilot inputs as the boundaries of the safe flight envelope and/or safe control input envelope are exceeded. During each experimental session, participants will be given instruction as to the effects of the FEP system and the information presented in the display for the particular operational mode they will be using. This instruction will be followed by a free-flight session to become familiar with the instrument panel configuration and automation mode. Immediately after, subjects will complete the series of ten scenarios in quick succession, pausing between each scenario to reset the simulation.

Each of the disturbance scenarios begins with the aircraft trimmed at a set altitude, airspeed, and heading, all of which the pilot is instructed to maintain throughout the duration of the scenario. Initially, the pilot will have manual control of the aircraft at the trimmed condition. After a variable length of time (15-45 seconds), the external disturbance event will begin. The disturbance events are characterized by sudden, strong gusts of wind, intended to cause vehicle upset and potential LoC without adequate pilot (or automation) compensation. The wind event will last approximate 30-60 seconds, and each scenario is designed to be similar in terms of overall difficulty.



Figure 8: Pilot-in-the-loop flight simulator at the Illinois Simulator Laboratory.

Metrics used to determine the efficacy of the experimental display include number of safe flight envelopes exceeded, duration of exceedance, and separation from desired heading, altitude, and airspeed. In addition to these metrics, the eye-tracking information will be used to determine which area of the interface panel is being attended to by participants. The data collected during flight testing will be used to examine the effect of the presence of FEP information on pilot situation awareness with respect to the aircraft and automation state, and whether this information is beneficial for recovering from (or preventing) vehicle upset conditions. It is anticipated that flight testing will reveal directions for improving the configuration of the display, as well as directions for future test development to determine the ability of the display to reduce adverse humanautomation interaction. In addition, the evaluations may suggest methods for improving pilot training for recovery from LoC events and upset conditions.

VII. Conclusion

In this paper, a novel interface for displaying flight envelope safety limits and FEP system state information has been presented. The new display is a first attempt at overcoming human-automation interaction issues arising from the addition of the FEP system to an augmented aircraft model. The display consists of a PFD augmented with flight envelope limits and key aerodynamic information, along with the EPD to convey FEP automation state information. These two primary display elements work together to provide vehicle performance and input information in a non-redundant manner. While it is not suggested that the format of the display is ideal for integration in the cockpits of modern aircraft, the display gives the pilot access to information about the aircraft and automation in both the input and output space, reducing reliance on the pilot's mental model by making the system more observable to the pilot, and therefore reducing the likelihood of adverse human-automation interaction. Piloted simulation evaluation is planned, which will evaluate the efficacy of the display and is anticipated to suggest future directions for cockpit interface design or flight training.

Acknowledgments

This research is supported by the National Aeronautics and Space Administration and by the National Science Foundation.

References

¹S. S. Vakil, J. Hansman Jr *et al.*, "Approaches to mitigating complexity-driven issues in commercial autoflight systems," *Reliability Engineering & System Safety*, vol. 75, no. 2, pp. 133–145, 2002.

²N. Tekles, E. Xargay, R. Choe, N. Hovakimyan, I. Gregory, and F. Holzapfel, "Flight envelope protection for NASA's Transport Class Model," in *AIAA Guidance, Navigation, and Control Conference*, National Harbour, MD, January 2014,

AIAA-2014-0269.

³J. Chongvisal, N. Tekles, E. Xargay, D. A. Talleur, A. Kirlik, and N. Hovakimyan, "Loss-of-control prediction and prevention for NASA's Transport Class Model," in *AIAA Guidance, Navigation, and Control Conference*, National Harbour, MD, January 2014, AIAA–2014–0784.

⁴L. Sherry, M. Feary, K. Fennell, and P. Polson, "Estimating the benefits of human factors engineering in NextGen development: Towards a formal definition of pilot proficiency," in *AIAA Aviation Technology, Integration, and Operations Conference*, Hilton Head, SC, August 2009, AIAA–2009–6974.

⁵R. Parasuraman and V. Riley, "Humans and automation: Use, misuse, disuse, abuse," *Human Factors: The Journal of the Human Factors and Ergonomics Society*, vol. 39, no. 2, pp. 230–253, 1997.

⁶ "Final report on the accident on 1st June 2009 to the Airbus A330-203 registered F-GZCP operated by Air France flight 447 Rio de Janeiro-Paris," Le Bureau d'Enquêtes et d'Analyses (BEA), July 2012.

⁷ "In-flight icing encounter and loss of control, Simmons Airlines, d.b.a. American Eagle flight 4184, Avions de Transport Regional (ATR), model 72-212, N401AM, Roselawn, Indiana, October 31, 1994," National Transportation Safety Board, Washington, DC, July 1996, Aircraft Accident Report NTSB/AAR-96/01.

⁸ "Air traffic accident on 27 December 1991 at Gottröra, AB county," Swedish Civil Aviation Administration, Stockholm, Sweden, October 1993, Report C 1993:57.

⁹ "Descent below visual glidepath and impact with seawall, Asiana Airlines flight 214, Boeing 777-200ER, HL7742, San Francisco, California, July 6, 2013," National Transportation Safety Board, Washington, DC, June 2014, Aircraft Accident Report NTSB/AAR-14/01.

¹⁰D. B. Kaber, "Adaptive automation," in *The Oxford Handbook of Cognitive Engineering*, ser. The Oxford Library of Psychology, J. D. Lee and A. Kirlik, Eds. New York, NY: Oxford University Press, 2014, (in press).

¹¹J.-M. Hoc, "Human-automation cooperation," in *The Oxford Handbook of Cognitive Engineering*, ser. The Oxford Library of Psychology, J. D. Lee and A. Kirlik, Eds. New York, NY: Oxford University Press, 2014, (in press).

¹²M. Sierhuis, J. M. Bradshaw, A. Acquisti, R. van Hoof, R. Jeffers, and A. Uszok, "Human-agent teamwork and adjustable autonomy in practice," in *International Symposium on Artificial Intelligence, Robotics and Automation in Space*, Nara, Japan, May 2003.

¹³C. E. Billings, "Human-centered aircraft automation philosophy," International Journal of Aviation Psychology, vol. 1, no. 4, pp. 261–270, 1991.

¹⁴A. Kirlik and S. Maruyama, "Human-technology interaction and music perception and performance: toward the robust design of sociotechnical systems," *Proceedings of the IEEE*, vol. 92, no. 4, pp. 616–631, April 2004.

¹⁵M. R. Endsley and E. O. Kiris, "The out-of-the-loop performance problem and level of control in automation," *Human Factors: The Journal of the Human Factors and Ergonomics Society*, vol. 37, no. 2, pp. 381–394, 1995.

¹⁶A. Degani and A. Kirlik, "Describing the design contributors to mode error," in Annual Symposium on Human Interaction with Complex Systems, Dayton, OH, March 1998, pp. 112–115.

¹⁷D. A. Norman, "The 'problem' with automation: inappropriate feedback and interaction, not 'over-automation'," *Philosophical Transactions of the Royal Society of London. Series B, Biological Sciences*, vol. 327, no. 1241, pp. 585–593, April 1990.

¹⁸C. M. Belcastro and C. M. Belcastro, "Future research directions for the development of integrated resilient flight systems to prevent aircraft loss-of-control accidents, part I: System technologies," NASA TM, (being finalized after review for publication).

¹⁹C. M. Belcastro and S. R. Jacobson, "Future integrated systems concept for preventing aircraft loss-of-control accidents," in *AIAA Guidance, Navigation, and Control Conference*, Toronto, Ontario, Canada, August 2010, AIAA–2010–8142.

²⁰C. M. Belcastro, "Loss of control prevention and recovery: Onboard guidance, control, and systems technologies," in *AIAA Guidance, Navigation, and Control Conference*, Minneapolis, MN, August 2012, AIAA–2012–4762.

 21 N. Hovakimyan and C. Cao, \mathcal{L}_1 Adaptive Control Theory. Philadelphia, PA: Society for Industrial and Applied Mathematics, 2010.

²²N. Hovakimyan, C. Cao, E. Kharisov, E. Xargay, and I. M. Gregory, " \mathcal{L}_1 adaptive control for safety-critical systems," *IEEE Control Systems Magazine*, vol. 31, no. 5, pp. 54–104, October 2011.

²³H. Lee, S. Snyder, and N. Hovakimyan, "An adaptive unknown input observer for fault detection and isolation of aircraft actuator faults," in *AIAA Guidance, Navigation, and Control Conference*, National Harbor, MD, January 2014, AIAA–2014–0266.

²⁴J. E. Wilborn and J. V. Foster, "Defining commercial transport loss-of-control: A quantitative approach," in *AIAA* Atmospheric Flight Mechanics Conference and Exhibit, Providence, RI, August 2004, AIAA–2004–4811.

²⁵D. E. Cox, K. Cunningham, and T. Jordan, "Subscale flight testing for aircraft loss of control: Accomplishments and future directions," in *AIAA Guidance, Navigation, and Control Conference*, Minneapolis, MN, 2012, AIAA–2012–5029.

²⁶J. M. Reising, L. C. Butterbaugh, and K. K. Liggett, "Preliminary assessment of primary flight display symbology for electro-optic head-down displays," DTIC Document, Tech. Rep., 1991, ADA253363.

²⁷ "Advisory circular (AC) 25-11B, electronic flight displays," Federal Avaiation Administration, October 2014.

²⁸J. S. Barlow, V. Stepanyan, and K. Krishnakumar, "Estimating loss-of-control: a data-based predictive control approach," in *AIAA Guidance, Navigation, and Control Conference*, Portland, OR, August 2011, AIAA–2011–6408.

²⁹K. Krishnakumar, V. Stepanyan, and J. S. Barlow, "Piloting on the edge: Approaches to real-time margin estimation and flight control," in *AIAA Guidance, Navigation, and Control Conference*, Minneapolis, MN, August 2012, AIAA–2012–4764.

³⁰N. Gandhi, N. D. Richards, and A. J. Bateman, "Simulator evaluation of an in-cockpit cueing system for upset recovery," in AIAA Guidance, Navigation, and Control Conference, National Harbor, Maryland, January 2014, AIAA–2014–0444.

³¹K. A. Ackerman, S. T. Pelech, R. S. Carbonari, A. Kirlik, N. Hovakimyan, and I. M. Gregory, "Pilot-in-the-loop flight simulator for NASA's Transport Class Model," in *AIAA Guidance, Navigation, and Control Conference*, National Harbor, MD, January 2014, AIAA–2014–0613.