

# Thermal Modeling Method Improvements for SAGE III on ISS

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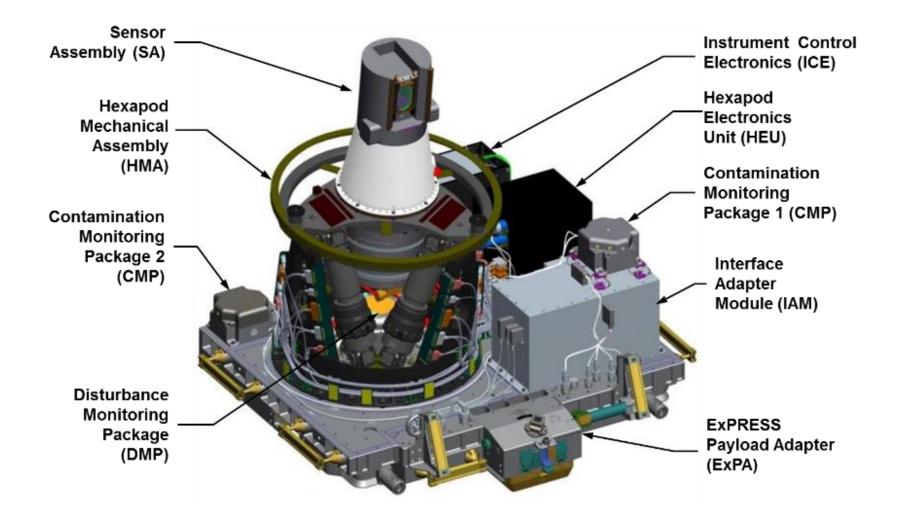


- Background
  - SAGE III on ISS
  - Model Development
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  - Inclusion of TVAC chambers and GSE
  - Use of assemblies for Dragon model updates
  - Creation of time-varying orbital parameters
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  - Incorporation of a convection submodel
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# SAGE III on ISS Background

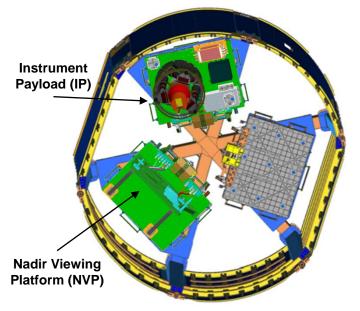
- SAGE III is an ISS-mounted science payload, to be launched on Falcon vehicle/Dragon capsule in 2016
- Three year minimum lifetime on ISS
- Monitors aerosols and other gases in stratosphere
- Thermal analyses are being completed for launch vehicle and all ISS scenarios
- Instrument Payload (IP) mounted on Nadir Viewing Platform (NVP)
- Several subsystems built in 1990's and placed in storage
  - Text legacy thermal models

#### **Instrument Payload**

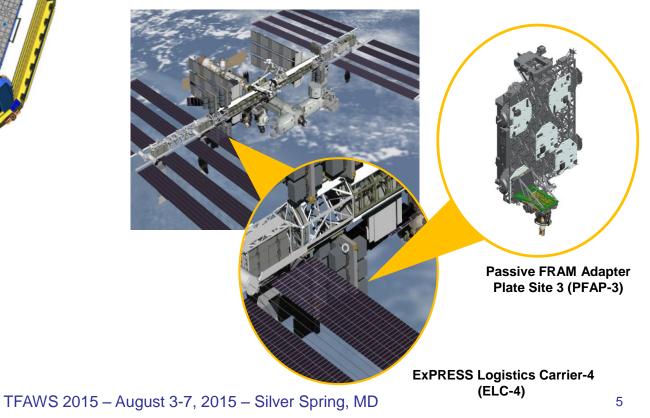


#### **Dragon and ISS Configuration**

**Dragon Unpressurized Cargo Module** 



S3 Truss Payload Attachment System-4 Site (PAS-4)



# **Model Development Background**

- Developed in Thermal Desktop® beginning in 2011
- Includes ISS and Dragon capsule
- Shared between several NASA engineers, contractors, and Italian payload partners
- Versioned: Current version 55f
  - Number represents major model change (number of nodes, sav file no longer valid), letter represents minor tweak
- Initial development of efficient modeling methods was presented at TFAWS 2013



## **Inclusion of TVAC Chambers and GSE**

- SAGE III thermal vacuum (TVAC) testing has occurred in two chambers at NASA LaRC
  - 6'x6' chamber has 3 independently-controlled temperature zones (GN<sub>2</sub>-controlled shroud and two LN<sub>2</sub>/heater controlled platens)
  - 8'x15' chamber has an LN2-controlled shroud and quartz lamps separated into 6 zones
- Representations of each chamber have been included in the system-level model (same model with ISS)
  - 6'x6' model includes two platens and a node to represent the shroud temperature
  - 8'x15' model includes an accurate representation of the full chamber geometry
- SAGE III Ground Support Equipment (GSE), primarily heater plates, has also been included in each chamber model

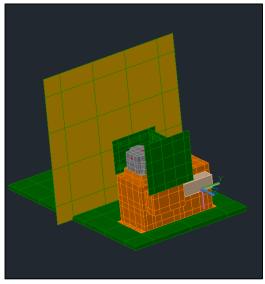


### Method

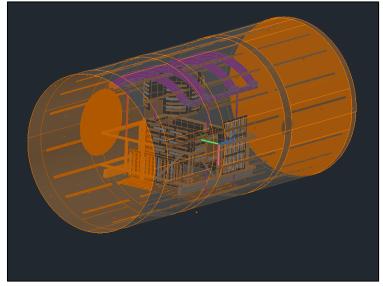
- Chambers are turned on/off using flags
- 8'x15' chamber position is adjusted to match the positioning in the chamber only for cases where that chamber is on
  - Symbols were created for X/Y/Z translation and rotation, controlled via logic (i.e., (Flag\_IP\_Tvac == 1)? 90:0)
- Symbols are used to set zone temperatures
- In addition to chamber controls, SAGE III utilizes heater plates to achieve subsystem temperature targets
  - Heater plate GSE is included in the chamber models and turned on/off using the same flags

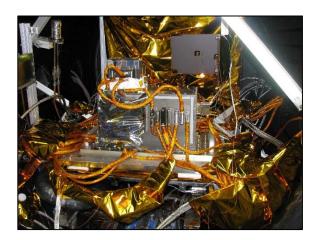
#### **Photos and Model Images**

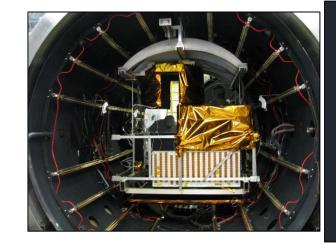
#### 6' x 6' Chamber

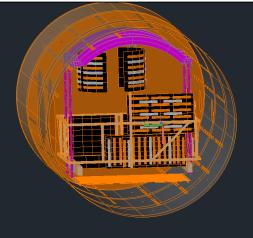


#### 8'x15' Chamber









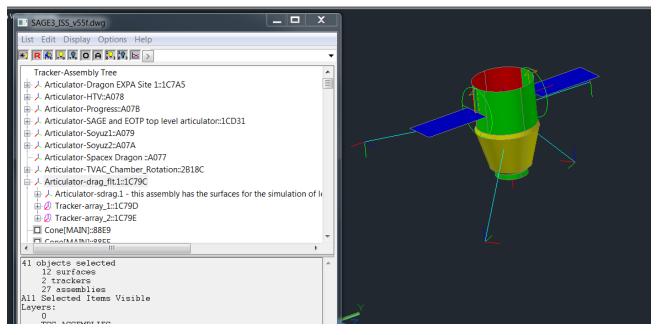
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### **Benefits**

- Accurate pre-test predictions are useful for verifying that targets can be achieved and estimating test time
- Having the chamber models in place prior to testing expedites correlation of the model to TVAC test data
- Including the chambers in the system-level model, rather than creating TVAC-specific versions, prevents the TVAC model from falling behind when the system-level model is updated
- Chamber models can be shared with future payloads

# Use of Assemblies for Dragon Model Updates

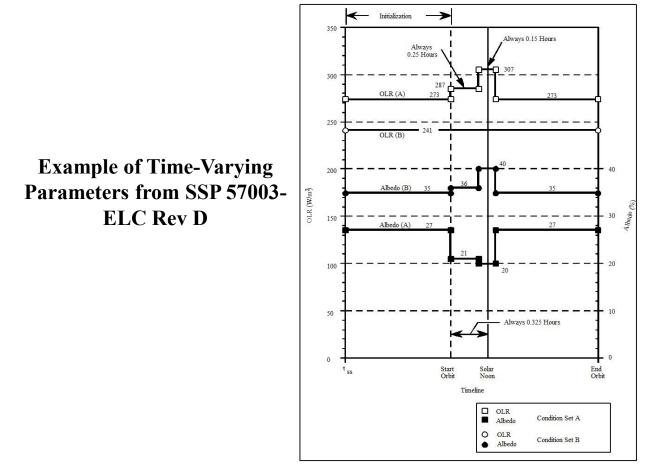
- Orbits in the Dragon model v3r1 are substantially different from those defined in v2r1
- Assemblies were used to change the orientation of the Dragon, IP, and NVP submodels
  - Prevents having to re-orient the SAGE III model in a fixed way
  - Allows for easy incorporation of future Dragon orbits



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# **Creation of Time-Varying Orbital Parameters**

- Per ISS requirements, SAGE III implemented time-varying orbital parameters (albedo and Earth IR)
  - First time this has been done in a payload developer's thermal model



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### Method

- Arrays were created to represent the timeline and changing values for both parameters in each of the ISS-defined cases
  - ISS defines "A" and "B" cases for hot and cold, also broken down into "nominal" and "extreme" cases
- The interp function was used to create symbols for each parameter (albedo and Earth IR) for each of the ISS-defined cases
  - Ex: interp(albedo\_times\_hot,albedo\_values\_hot\_extreme\_B,hrTime)
  - A total of 8 timelines was created for each parameter
- Code has been made available to all NASA Centers on the Agencywide share drive

Name	Result	Expression	Comment
albedo_times_cold	array	0.001.25.251.4.401hrPeriod	times in hours for albedo values, desi
albedo_times_hot	array	0.001.25.251.4.401hrPeriod	times in hours for albedo values, desi
albedo_time_varying_cold_A	0.27	interp(albedo_times_cold,albedo_values_cold_A.hrTime)	albedo in design cold A as function of
albedo_time_varying_cold_B	0.22	interp(albedo_times_cold,albedo_values_cold_B,hrTime)	albedo in design cold Bas function of t
albedo_time_varying_cold_extreme_A	0.27	interp(albedo_times_cold,albedo_values_cold_extreme_A.hrTime)	albedo in extreme cold A as function o
lbedo_time_varying_cold_extreme_B	0.2	interp(albedo_times_cold,albedo_values_cold_extreme_B,hrTime)	albedo in extreme cold Bas function of
albedo_time_varying_hot_A	0.27	interp(albedo_times_hot,albedo_values_hot_A,hrTime)	albedo in design hot A as function of ti
lbedo_time_varying_hot_B	0.35	interp(albedo_times_hot,albedo_values_hot_B,hrTime)	albedo in design hot B as function of ti
lbedo_time_varying_hot_extreme_A	0.3	interp(albedo_times_hot,albedo_values_hot_extreme_A,hrTime)	albedo in extreme hot A as function of
lbedo_time_varying_hot_extreme_B	0.4	interp(albedo_times_hot,albedo_values_hot_extreme_B,hrTime)	albedo in extreme hot B as function of
lbedo_values_cold_A	array	.270.0.27.27.27.27	albedo values, design cold A case, fr
lbedo_values_cold_B	array	.220.022.22.22.22	albedo values, design cold B case, fro
lbedo_values_cold_extreme_A	array	.270.0.27.27.27.27	albedo values, extreme cold A case, f
lbedo_values_cold_extreme_B	array	.200.020.20.20.20	albedo values, extreme cold B case, t
lbedo_values_hot_A	array	.27.21.21.20.20.27.27	albedo values, design hot A case, fro
lbedo_values_hot_B	array	.35.36.36.40.40.35.35	albedo values, design hot B case, from
lbedo_values_hot_extreme_A	array	.30.25.25.25.25.30.30	albedo values, extreme hot A case, fro
lbedo_values_hot_extreme_B	array	.40.45.45.53.53.40.40	albedo values, extreme hot B case, fro
DLR_time_varying_cold_A	217	interp(albedo_times_cold,OLR_values_cold_A.hrTime)	OLR in design cold A as function of tim
)LR_time_varying_cold_B	241	interp(albedo_times_cold,OLR_values_cold_B,hrTime)	OLR in design cold B as function of tim
LR_time_varying_cold_extreme_A	206	interp(albedo_times_cold,OLR_values_cold_extreme_A.hrTime)	OLR in extreme cold A as function of tir
LR_time_varying_cold_extreme_B	241	interp(albedo_times_cold,OLR_values_cold_extreme_B,hrTime)	OLR in extreme cold B as function of til
LR_time_varying_hot_A	273	interp(albedo_times_hotOLR_values_hot_A.hrTime)	OLR in design hot A as function of time
I D time van ind het R	9.41	intern(albada, times, bot OLP, values, bot R hrTime)	OLD in docion hat B as function of time

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# **Setting Model Parameters with Case Definition**

- Model includes a small set of registers that fully control case definition
  - Parameters such as initial temperature, heater voltage, power dissipation
  - Type of case such as payload location, flight scenario (science event type), TVAC case (balance or functional), special scenarios (plume heating, parked ISS trackers, etc.)
- Flags are used in case sets, logic blocks, and enable blocks to set up the desired scenarios
  - Case\_def (values 0, 1, 2, and 3) is used to represent cold, nominal and hot cases; controls boundary conditions and component power dissipations
  - Flag\_NVP\_MOV and Flag\_SAGE\_MOV are used to define the position of the payload (Dragon, EOTP, ELC)
  - Flag\_voltage sets voltage to minimum or nominal
  - Flag\_IP\_TVAC and Flag\_TVAC\_6x6 are used to specify TVAC cases
  - Flag\_survival and Flag\_transfer are used to define scenarios with survival heater power only or no power during transfer from one location to another
  - Flag\_plume\_heat and Flag\_park\_port\_SARG define special scenarios
- Allows many different scenarios to be run by simply defining a few flags in the case set TFAWS 2015 – August 3-7, 2015 – Silver Spring, MD

#### **Examples of Case Definition**

#### Flight Hot Op Case on ELC

Advance	ed Props Sy	mbols (	Comments	
Ov	verride List			
Sy	mbol O	verride	Glob	bal
FI FI N	ase_def  ag_NVP_MOV  ag_SAGE_MO umOrbits umOrbits			
>			-	

#### Flight Cold Survival Case on EOTP

Advar	nced Props	Symbols	Com	iments	
	Override List				
1	Symbol	Overrid	е	Global	
	Case_def case_SITE Flag_NVP_M Flag_SAGE_		0 1 2 2	1 0 0 0	
>	flag_survival NumOrbits switch_EOTP	_DOE	1 15 1	0 20 0	

#### **IP TVAC Case**

lva	nced Props Symbols (	Comments		
	Override List			
	Symbol Override	Global		
	flag_IP_TVAC	1	0	
	flag_main_output_file_set	0	1	
	Flag_NVP_MOV	1	0	
	flag_QFLOW	0	1	
	flag_Tshrouds_uniform	1	0	
	Gflux_coupled	1000	250	
	t_end	40	48	
	T_shroud_rings	-180	-140	
	T_TVAC_CMP1_plate	92	20	
	T_TVAC_CMP1Z2_plate	92	20	
	T_TVAC_CMP2_plate	111	20	
	T_TVAC_ExPA_plate	82	20	
	T_TVAC_HEU_plate	57	20	
	T_TVAC_IAM_plate	-150	20	
	T_TVAC_ICE_plate	32	20	
	T TVAC SA plate	40	20	

#### Logic Based on Case Definition Flags

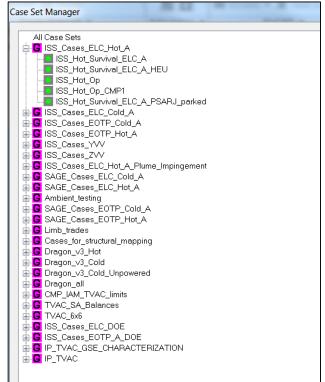
Submodel: (GLOBAL)  Code placed in: Operations Block Post Build (TDPOSTBL)  Declarations (COMMON blocks, INTEGER, REAL):	Enabled	
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<pre>IF (Case_def.qt.0) THEN T_TEC_cold_side = 15. ENDIF C Cold case block IF (Case_def.EQ.0) THEN fas_power = 0.9 Q_flex_cable_housing = 0.0 T_TEC_cold_side = 10. C Electronics box powers in cold case C CMP1 powers in cold op case C CMP1 powers in cold op case C fas_Q_CMP1 added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) fas_Q_CMP1 = 0.525 Q_CMP1_DCDC_UI_UZ = 0.75 Q_CMP1_DCDC_UI_UZ = 0.75 Q_CMP1_DCDC_UI_UZ = 0.75 Q_CMP1_DCDC_UI_UZ = 0.54 Q_CMP1_FPGA = 0.615 Q_CMP1_FPGA = 0.615 Q_CMP1_AINLG = 1.4875 Q_CMP1_AINLG = 1.4875 Q_CMP1_POWER = 0.33 C C C C C C C C Powers in cold op case C C C C C C C Powers in cold op case C C C C C C Powers in cold op case C C C C C C C Powers in cold op case C C C C C C Powers in cold op case C C C C C C C Powers in cold op case C C C C C C C Powers in cold op case C C C C C C C Powers in cold op case C C C C C C C Powers in cold op case C C C C C C Powers in cold op case C C C C C C Abaged to DCCC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C fac_Q_CMP2 = 0.571 Q_CMP2_DCDC_UI_U2 = 0.566 Q_CMP2_DCDC_UI_U2 = 0.564 Q_CMP2_DCDC_UI_U2 = 0.544 Q_CMP2_DCDC_UI = 0.544 Q_CMP2_DCDC_UI_U2 = 0.544 Q_CMP2_DC</pre>		
<pre>IF (Case_def.qt.0) THEN     T_TEC_cold_side = 15.     ENDIF C C Cold case block     IF (Case_def.EQ.0) THEN     fas_power = 0.9         Q_flex_cable_housing = 0.0         T_TEC_cold_side = 10. C C C Electronics box powers in cold case C C C CMP1 powers in cold op case C C C CMP1 power = 0.54         Q_CMP1_FOAF = 0.615         Q_CMP1_MANG = 1.4875         Q_CMP1_MANG = 0.33 C C C C C C C C C C C C C C C C C C C</pre>	o boundary oung	ALAVALLE CONTELECA LIGA C CE L (NAM) 2/20/22/ Baon Co C AN TE / 20 CO 22
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<pre>fac_power = 0.9 Q_flex cable_housing = 0.0 T_TEC_cold_side = 10. C Electronics box powers in cold case C C CMP1 powers in cold op case C CMP1 powers in cold op case C G_Q_CMP1 dded so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) fac_Q_CMP1 = 0.525 Q_CMP1_DCDC_U1 = 0.75 Q_CMP1_DCDC_U2 = 0.75 Q_CMP1_DCDC_U2 = 0.75 Q_CMP1_DCDC_U3 = 0.54 Q_CMP1_FFGA = 0.615 Q_CMP1_TQCM = 0.0 Q_CMP1_TQCM = 0.0 Q_CMP1_TQCM = 0.4875 Q_CMP1_MAIN = 0.9645 Q_CMP1_POWER = 0.33 C C CMP2 powers in cold op case C Cheaped to DCC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C fac_Q_CMP2_DCL_U2 = 0.56 Q_CMP2_DCDC_U1 = 0.56 Q_CMP2_DCDC_U3 = 0.54</pre>		
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<pre>C C CMP1 powers in cold op case C CMP1 powers in cold op case C CMP1 added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14)</pre>		
<pre>C CMP1 powers in cold op case C fac_Q_CMP1 a 0.525 Q_CMP1 = 0.525 Q_CMP1_DCDC_UI_UZ = 0.75 Q_CMP1_DCDC_US = 0.75 Q_CMP1_DCDC_US = 0.75 Q_CMP1_DCLR_UZA = 0.54 Q_CMP1_FKGA = 0.615 Q_CMP1_MP1_FFGA = 0.615 Q_CMP1_MAIN = 0.9645 Q_CMP1_FMAIN = 0.9645 Q_CMP1_FOWER = 0.33 C CMP2 powers in cold op case C CMP2 powers in cold op case C CMP2 powers in cold op case C CMP2 dded so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) fac_Q_CMP2_DCDC_UI_UZ = 0.56 Q_CMP2_DCDC_UI = 0.54</pre>	C Electronics	s box powers in cold case
<pre>C fac_Q_CMP1 added so that total CMP power will be 3.25%, measured idle value (KKL, 3/6/14)     fac_Q_CMP1_DCDC_UI_U2 = 0.75     Q_CMP1_DCDC_UI = 0.75     Q_CMP1_DCDC_UI = 0.75     Q_CMP1_DCDC_UI = 0.75     Q_CMP1_DCDC_UI = 0.54     Q_CMP1_EFGA = 0.615     Q_CMP1_TQM = 0.0     Q_CMP1_TQM = 0.0     Q_CMP1_MAIN = 0.9645     Q_CMP1_MAIN = 0.9645     Q_CMP1_POWER = 0.33 C C CMP2 powers in cold op case C Chapage to DCC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C fac_Q_CMP2_DCDC_UI_U2 = 0.56     Q_CMP2_DCDC_UI = 0.54     Q_CMP2_DCDC_UI = 0.54 </pre>	С	
<pre>- Tac 0 CMP1 = 0.525 Q CMP1 DCDC U1 U2 = 0.75 Q CMP1 DCDC U1 = 0.75 Q CMP1 DCDC U3 = 0.75 Q CMP1 DCDC U3 = 0.75 Q CMP1 FRAF = 0.615 Q CMP1 FRAF = 0.615 Q CMP1 TQCM = 0.0 Q CMP1 TQCM = 0.0 Q CMP1 TQCM = 0.0 Q CMP1 TQCM = 0.33 C C CMP2 powers in cold op case C CMP2 powers in cold op case C CMP2 powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C fac 0 CMP2 added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) T fac 0 CMP2 DCDC U1 U2 = 0.56 Q CMP2 DCDC U1 U2 = 0.54 Q CMP2 DCDC U3 = 0.54</pre>		
<pre>Q_CMPI_DCDC_UI_UZ = 0.75 Q_CMPI_DCDC_UI = 0.75 Q_CMPI_DCLR_UZA = 0.54 Q_CMPI_DCLR_UZA = 0.54 Q_CMPI_MINT = 0.0 Q_CMPI_MAIN = 0.0 Q_CMPI_ANLG = 1.4875 Q_CMPI_FOWER = 0.33 C C CMP2 powers in cold op case C Changed to DCC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C fac_Q_CMP2_Dowers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C fac_Q_CMP2_DOWER = 0.51 Q_CMP2_DCDC_UI_UZ = 0.56 Q_CMP2_DCDC_UI = 0.54</pre>		
<pre>Q_CMP1_DCDC_UB=0.75 Q_CMP1_DCLR_U2A = 0.54 Q_CMP1_FEPGA = 0.615 Q_CMP1_FEPGA = 0.615 Q_CMP1_ANIG = 1.4875 Q_CMP1_ANIG = 1.4875 Q_CMP1_ANIG = 1.4875 Q_CMP1_MAIN = 0.9645 Q_CMP1_POWER = 0.33 C C CMP2 powers in cold op case C Changed to DCDC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1) C fac_Q_CMP2_DCDC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1) C fac_Q_CMP2_DCDC u1_U2 = 0.56 Q_CMP2_DCDC_UB = 0.643 Q_CMP2_DCLR_U2A = 0.54</pre>		
<pre>Q_CMP1_DCLR_UZA = 0.54 Q_CMP1_FFGA = 0.615 Q_CMP1_MFGA = 0.615 Q_CMP1_MFT = 0.0 Q_CMP1_NLG = 1.4875 Q_CMP1_FAULE = 1.4875 Q_CMP1_FOWER = 0.33 C C CMP2 powers in cold op case C Changed to DCC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1) C fac_Q_CMP2 powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1) C fac_Q_CMP2 added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) fac_Q_CMP2 DCDC_U1_U2 = 0.56 Q_CMP2_DCDC_U2 = 0.54 Q_CMP2_DCDC_U2 = 0.54</pre>		
<pre>Q_CMP1_FPGA = 0.615 Q_CMP1_FPGA = 0.615 Q_CMP1_TQCM = 0.0 Q_CMP1_TQCM = 0.0 Q_CMP1_RANG = 1.4875 Q_CMP1_MAIN = 0.9645 Q_CMP1_POWER = 0.33 C C CMP2 powers in cold op case C Chapged to DCCD powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C fac_Q_CMP2_added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) fac_Q_CMP2 = 0.571 Q_CMP2_DCDC_UI = 0.564 Q_CMP2_DCDC_UI = 0.54</pre>		
<pre>Q_CMP1_MSFT = 0.0 Q_CMP1_TQCM = 0.0 Q_CMP1_AILG = 1.4875 Q_CMP1_MAIN = 0.9645 Q_CMP1_POWER = 0.33 C C CMP2 powers in cold op case C Changed to DCDC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1) C fac_Q_CMP2 added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14)</pre>		
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C Changed to DCDC powers to hot case values becasue cold powers listed were higher than hot case (KKL 2/1/1: C facCMP2 added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) facCMP2 = 0.571 Q_CMP2_DCDC U1_U2 = 0.56 Q_CMP2_DCDC_U3 = 0.643 Q_CMP2_DCDC_U3 = 0.54		a in cold op case
C fac_Q_CMP2 added so that total CMP power will be 3.25W, measured idle value (KKL, 3/6/14) fac_Q_CMP2 = 0.571 Q_CMP2_DCDC_U1_U2 = 0.56 Q_CMP2_DCDC_U3 = 0.643 Q_CMP2_DCLR_U2A = 0.54		
- fac_Q_CMP2 = 0.571 Q_CMP2_DCDC_U1_U2 = 0.56 Q_CMP2_DCDC_U8 = 0.643 Q_CMP2_DCLC_U8 = 0.643 Q_CMP2_DCLR_U2A = 0.54		
Q_CMP2_DCDC_U1_U2 = 0.56 Q_CMP2_DCDC_U8 = 0.643 Q_CMP2_DCLR_U2A = 0.54		
Q_CMP2_DCLR_U2A = 0.54	C fac_Q_CMP2	
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<u>x_date_reak</u> of the	C fac_Q_CMP2 fac_Q Q_CMP2 Q_CMP2	2_DCDC_U8 = 0.643

# **Incorporation of Convection Submodel**

- Addition of a convection submodel that is only built for certain cases has proved useful for several situations
  - Submodel includes air nodes and convection conductors which are not built for flight cases; activated by flags
- One component underwent testing in both air and vacuum
  - Incorporating air convection allowed for correlation of all cases to occur in a single model
- Following completion of payload integration, several functional tests were completed in a clean room environment
  - Incorporating air convection allowed for early quick-look correlation work to be completed prior to TVAC testing
- Air convection model was used to show that the EMI setup with the payload bagged would not result in limit exceedences

# **Approach for Case Grouping**

- The current SAGE III system-level model contains ~250 cases
- Run directories are defined by model version, payload location, and hot/cold case (i.e. v55\_runs\ELC\_hot, v55\_runs\EOTP\_cold)
  - Keeps the cases organized in a way that's easy for multiple users to understand
- Each group of cases has a common run directory
  - Makes it easy to update the run directories when the model version is changed
  - Minimizes the necessity to re-run radk cases for new analysis runs
- TVAC cases are grouped separately from flight cases





- Methods developed have made SAGE III analysis quicker, more accurate, and more flexible
- Up-front time investment has paid off in faster analyses
- Methods shared with other programs and Centers
- Other payloads, particularly ISS and Dragon, may find these methods useful



- Thanks to all co-authors for their work in developing and perfecting these processes
  - Ruth Amundsen, Kaitlin Liles, Warren Davis, Steven Tobin, Rebecca Stavely, and Salvatore Scola, NASA Langley Research Center (LaRC)
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