

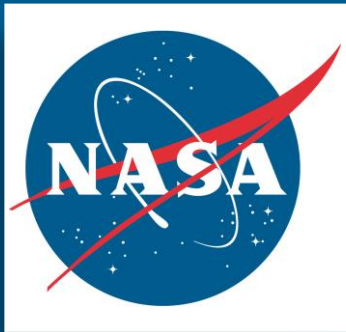
# THE EFFECT OF MICROSTRUCTURAL HETEROGENEITY ON DUCTILE FAILURE

**GEOFFREY BOMARITO\***, **JAMES WARNER\***, **DEREK WARNER+**

\* NASA LANGLEY RESEARCH CENTER

+ CORNELL UNIVERSITY

13TH US NATIONAL CONGRESS ON COMPUTATIONAL MECHANICS



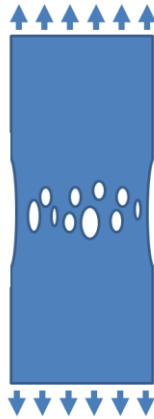
# DUCTILE FAILURE



Nucleation



Growth



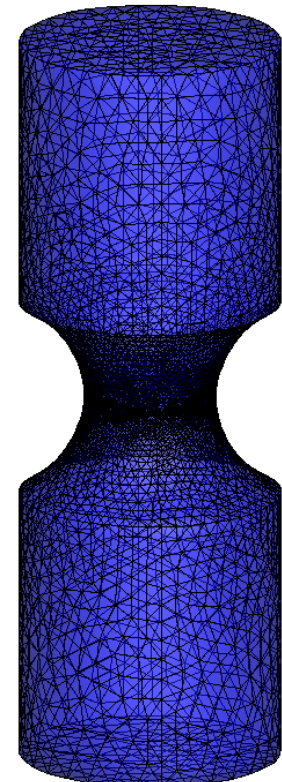
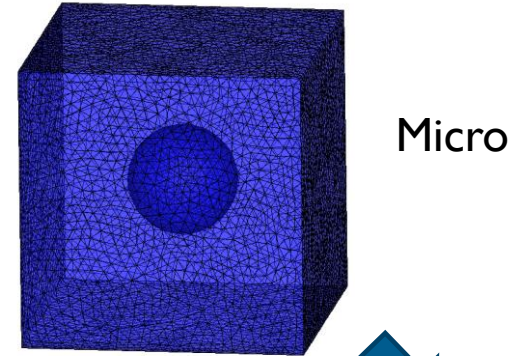
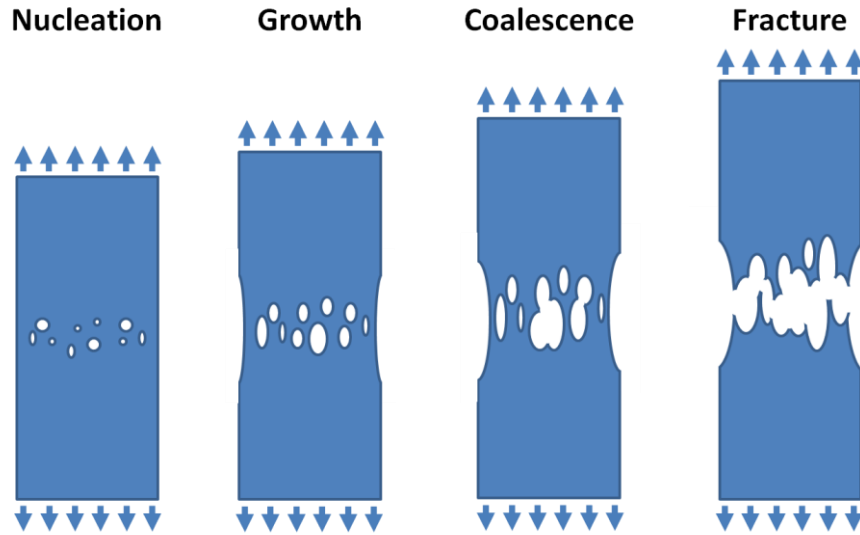
Coalescence



Fracture



# THE TWO SCALE PROBLEM

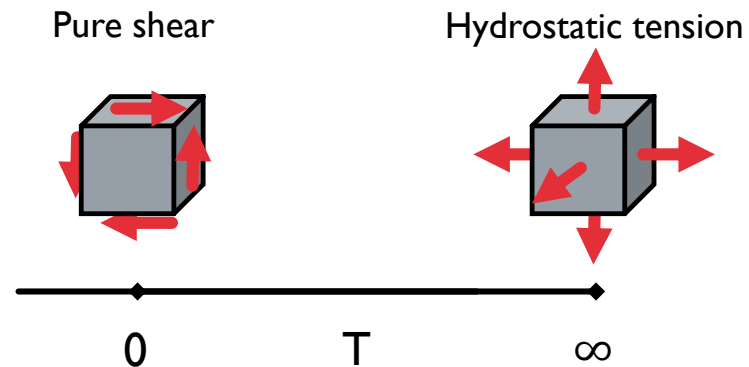


- Large-scale phenomenon controlled by micro-scale features
- We aim to capture two effects:
  - Variability in loading (micro-scale)
  - Variability in initial microstructure

- Here loading is defined by 2 parameters

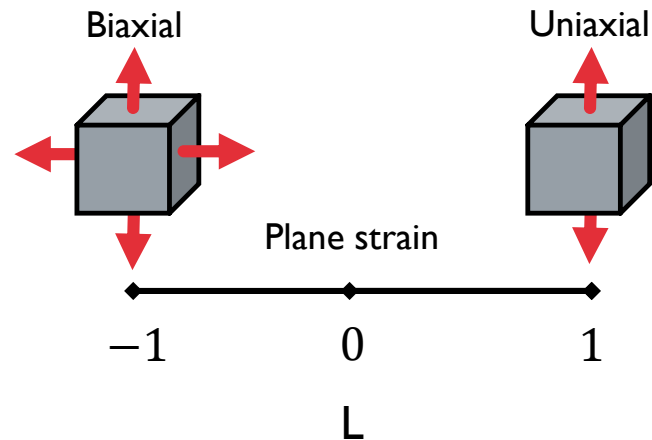
- Triaxiality

- $T = \frac{\sigma_h}{\sigma_e}$

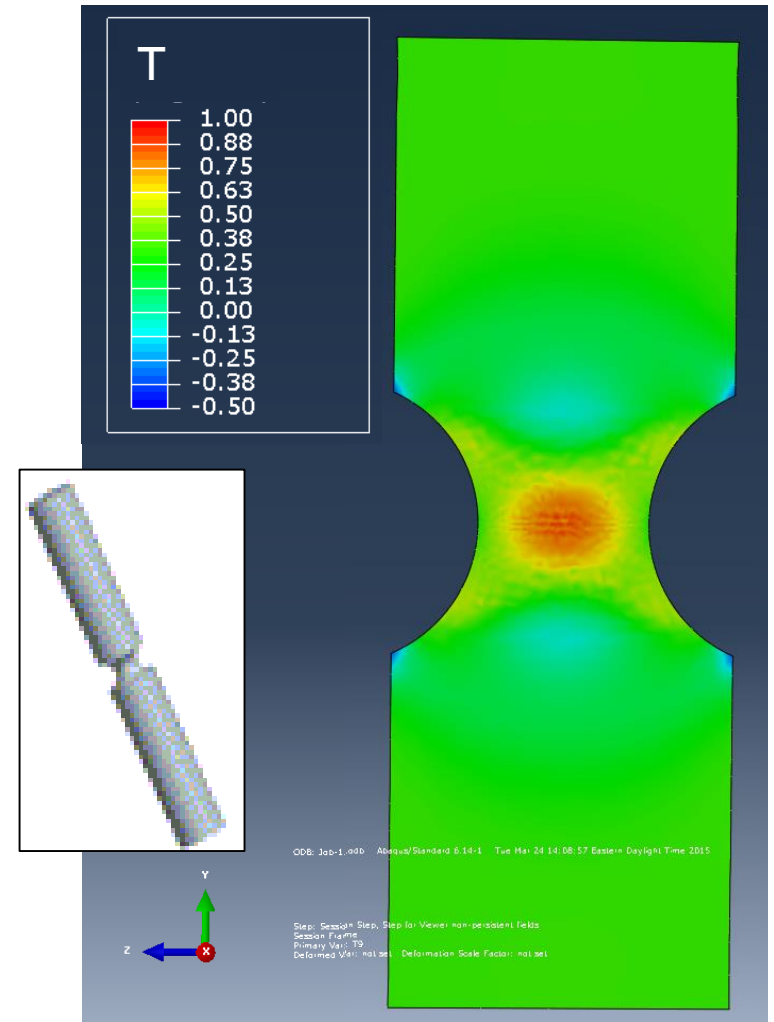
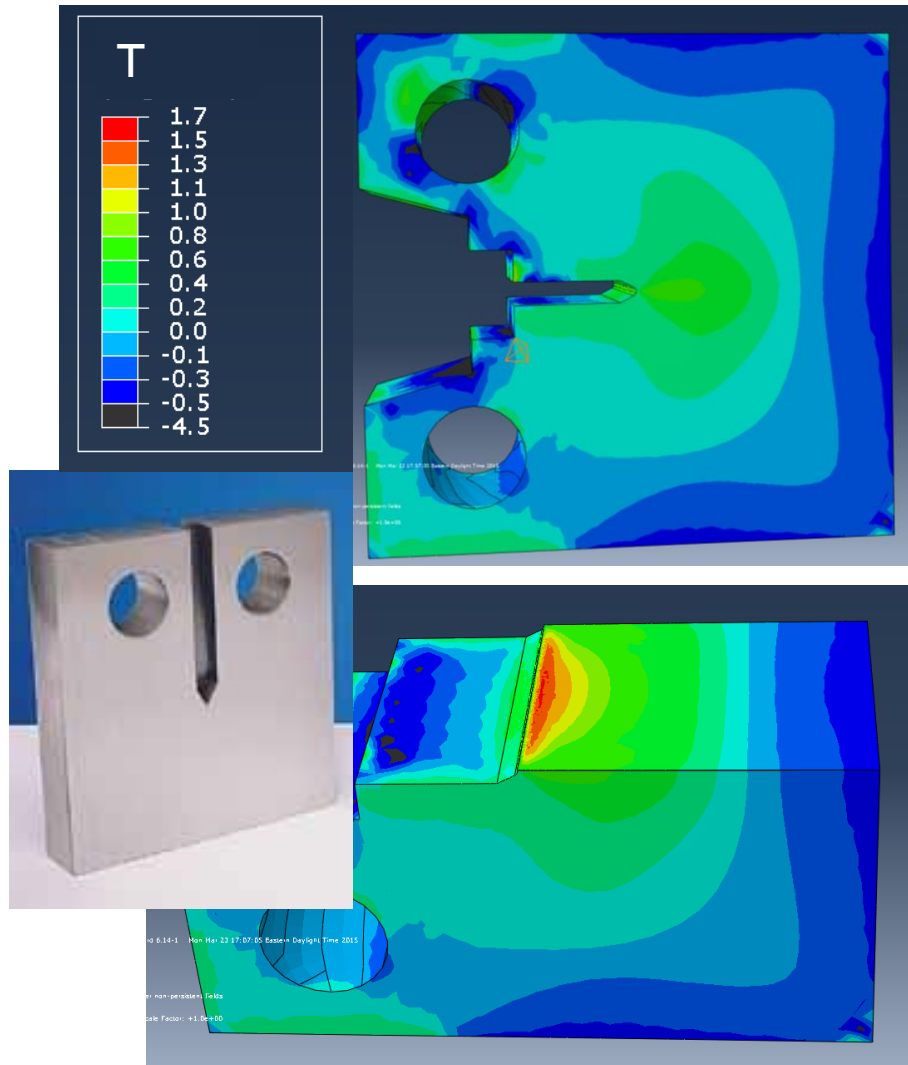
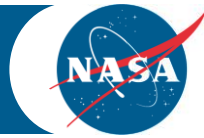


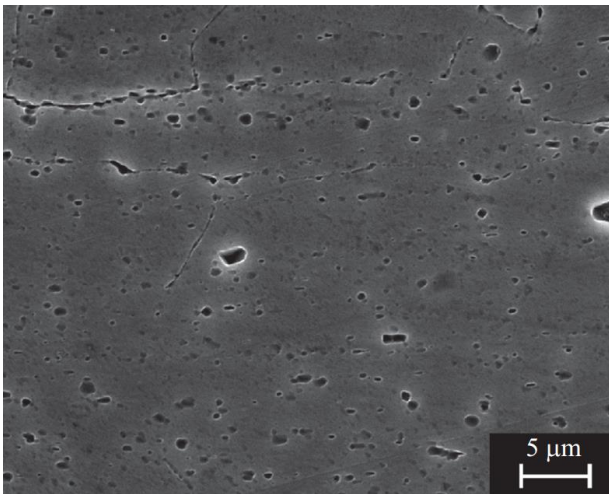
- Lode Parameter

- $L = \frac{27J_3}{2\sigma_e^3}$



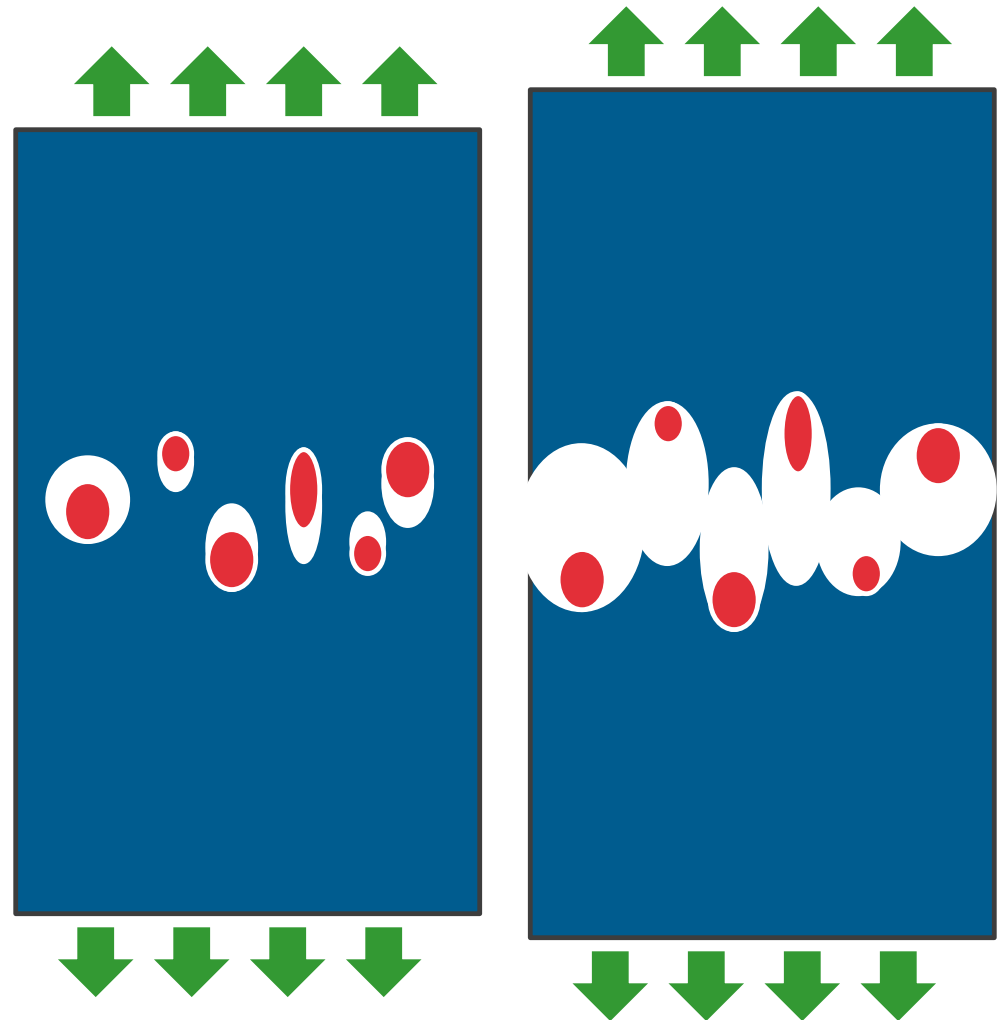
# VARIABILITY IN LOADING (MICRO-SCALE)



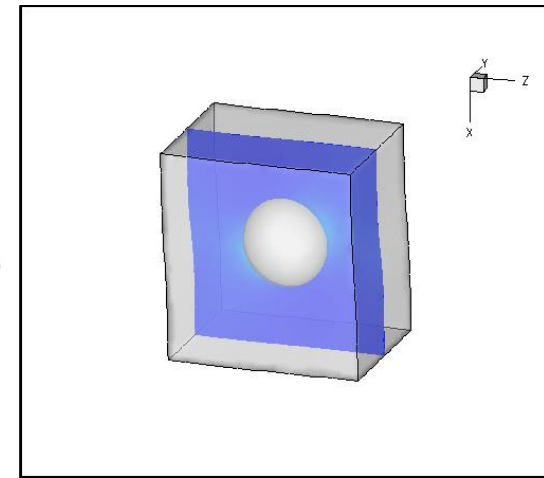
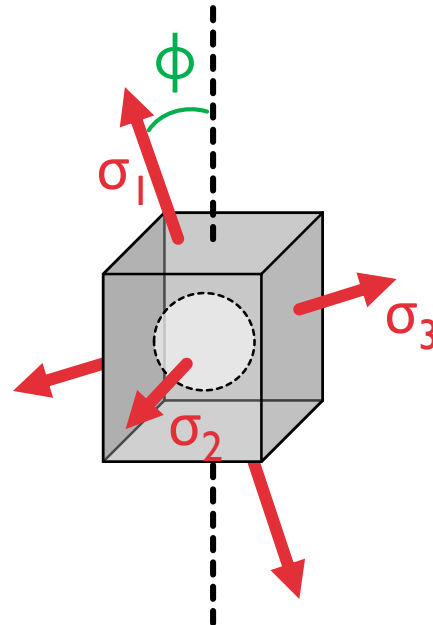
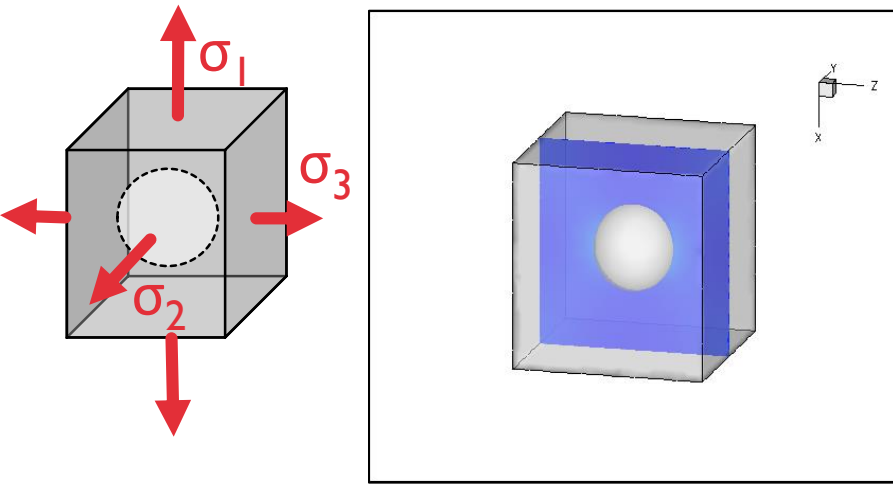
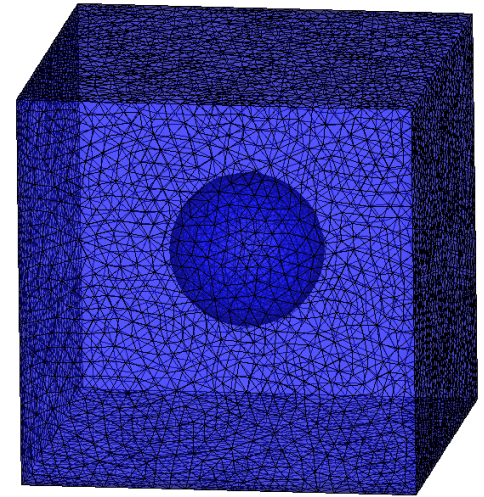


Chen and Lai (2014)

- Assume second phase particles act as voids
- Assume local porosity to be the defining microstructural feature



- 3D FEM
- Initial porosity ( $f_0$ ) defines geometry
- $T$  and  $L$  define the loading ratios:  $\frac{\sigma_2}{\sigma_1}$  and  $\frac{\sigma_3}{\sigma_1}$
- Allow for different localization modes



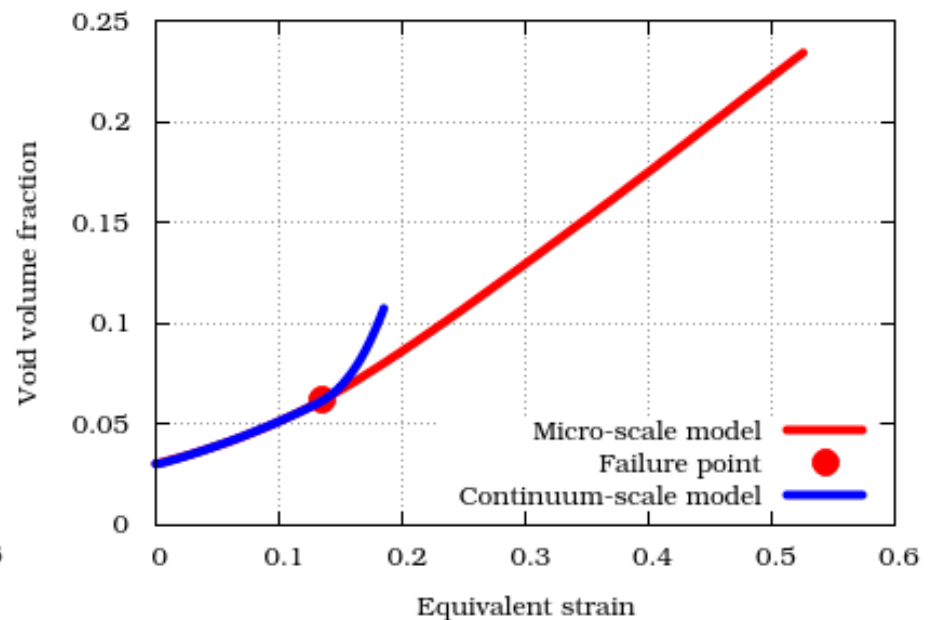
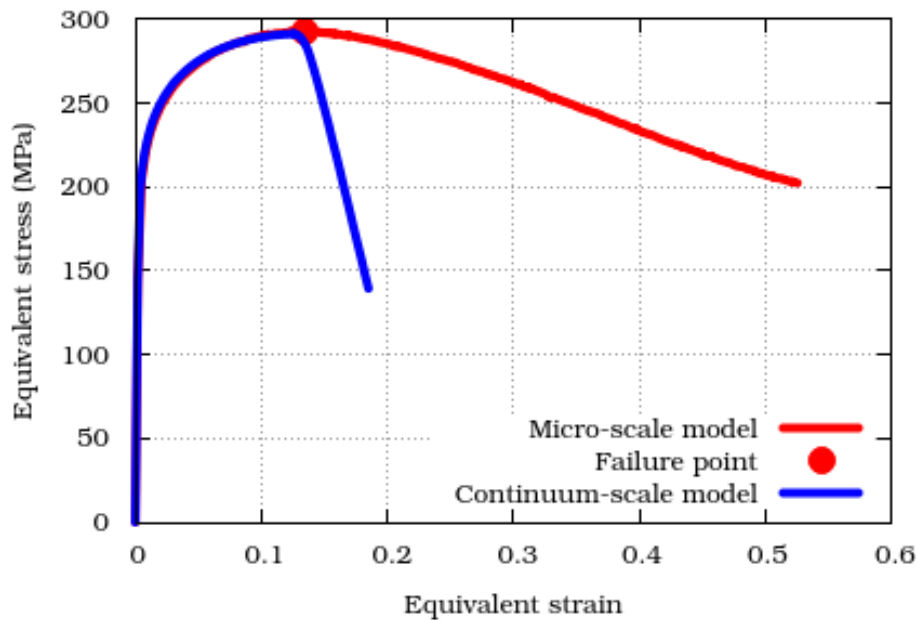
# THE MODEL: CONTINUUM-SCALE



$$\Phi = \left( \frac{\bar{\sigma}}{\sigma_y} \right)^2 + 2q_1 f^* \cosh \left( \frac{3}{2} q_2 \frac{\sigma_h}{\sigma_y} \right) - (1 + q_1 f^*)^2$$

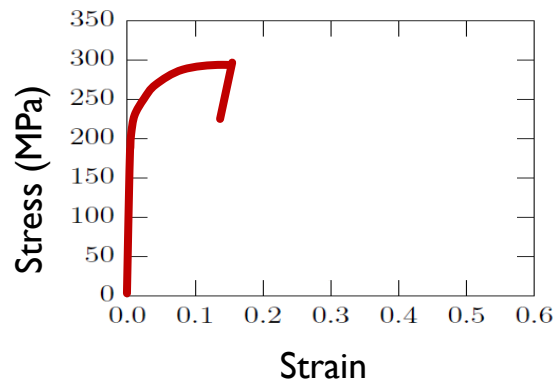
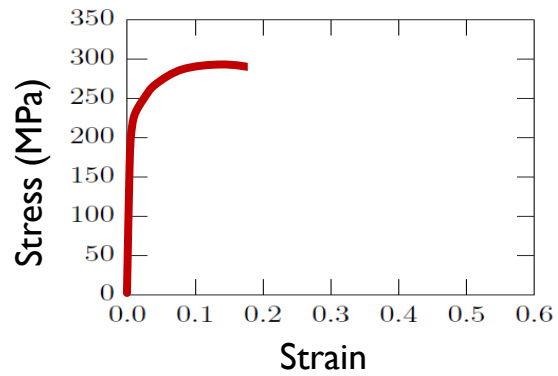
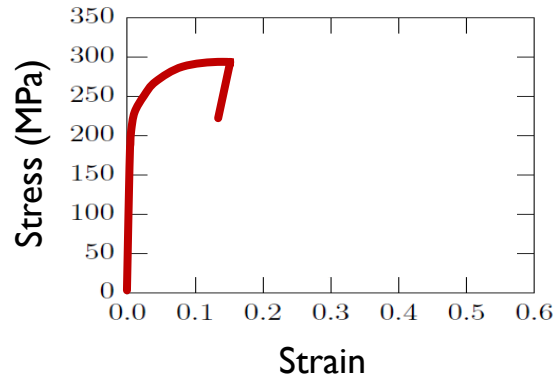
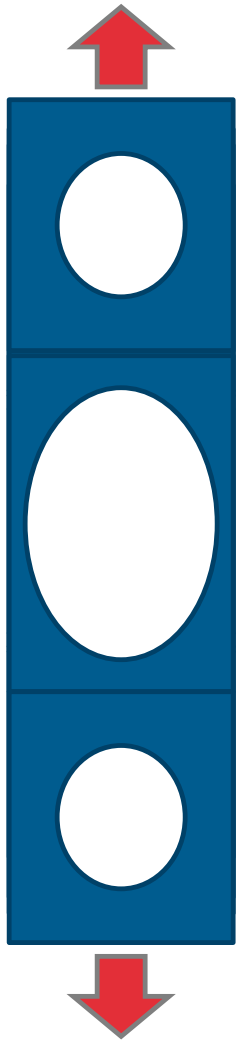
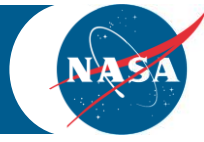
$$f^* = \begin{cases} f & : f \leq f_c \\ f_c + \kappa(f - f_c) & : f > f_c \end{cases}$$

$q_1$   
 $q_2$   
 $f_c$

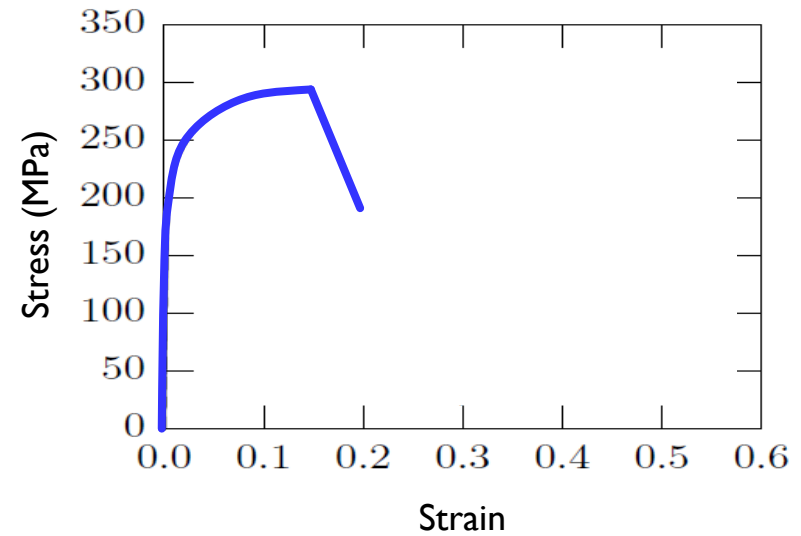




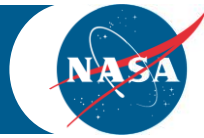
# POST-FAILURE RESPONSE



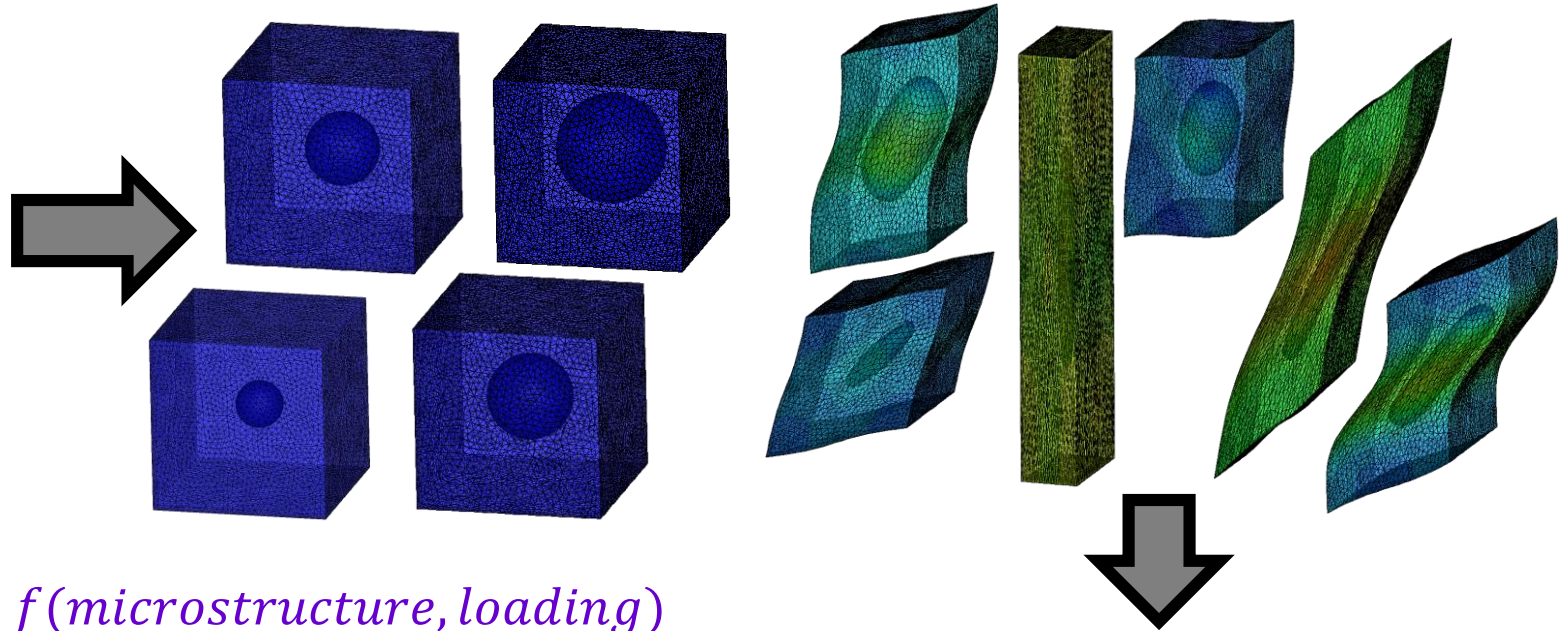
## Composite



# RECAP ON MECHANICAL RESPONSE



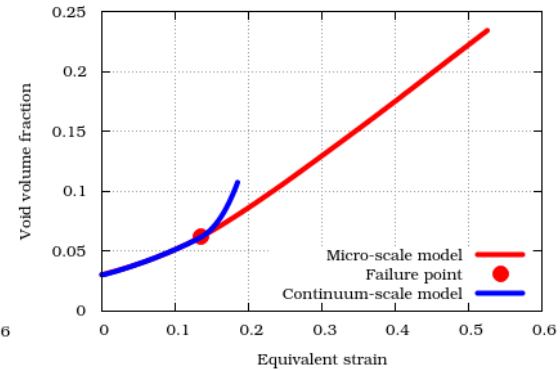
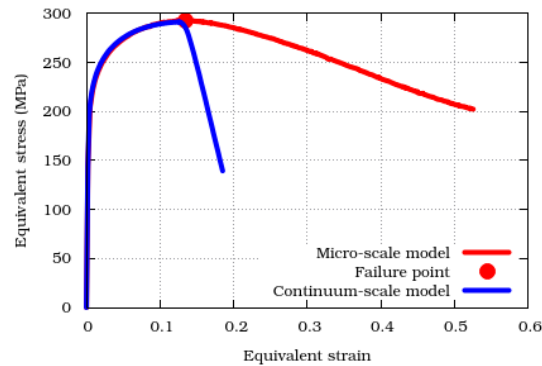
Given:  
 $f_0, T, L$



Response =  $f(\text{microstructure}, \text{loading})$

$q_1(f_0, T, L)$   
 $q_2(f_0, T, L)$   
 $f_c(f_0, T, L)$

$q_1$   
 $q_2$   
 $f_c$

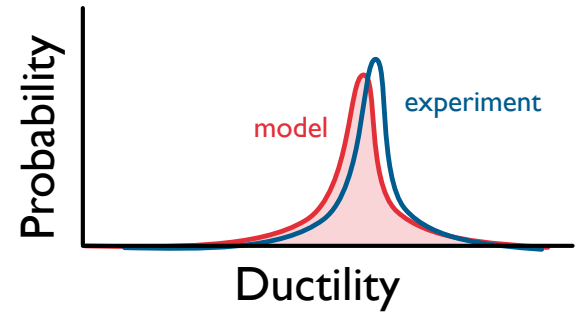
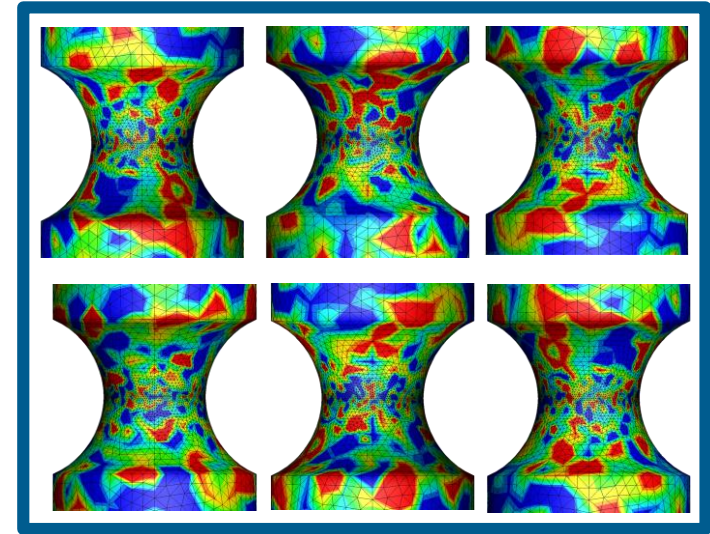
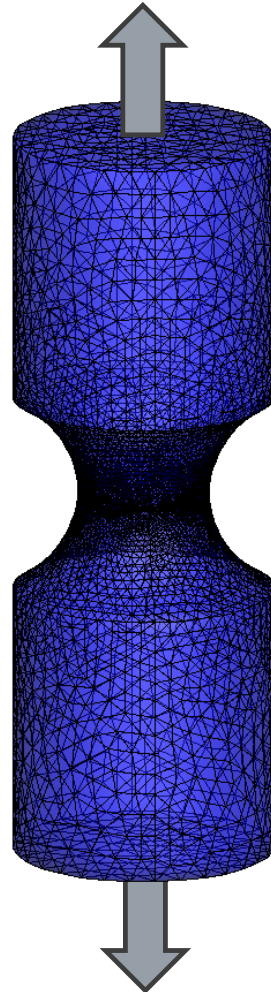
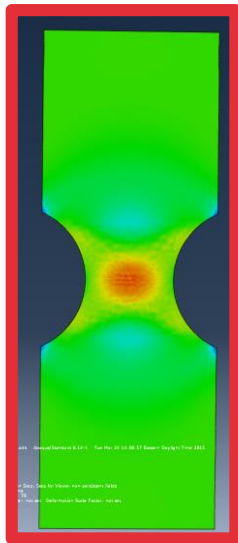


# UNCERTAINTY QUANTIFICATION



Response =  $f(\text{microstructure}, \text{loading})$

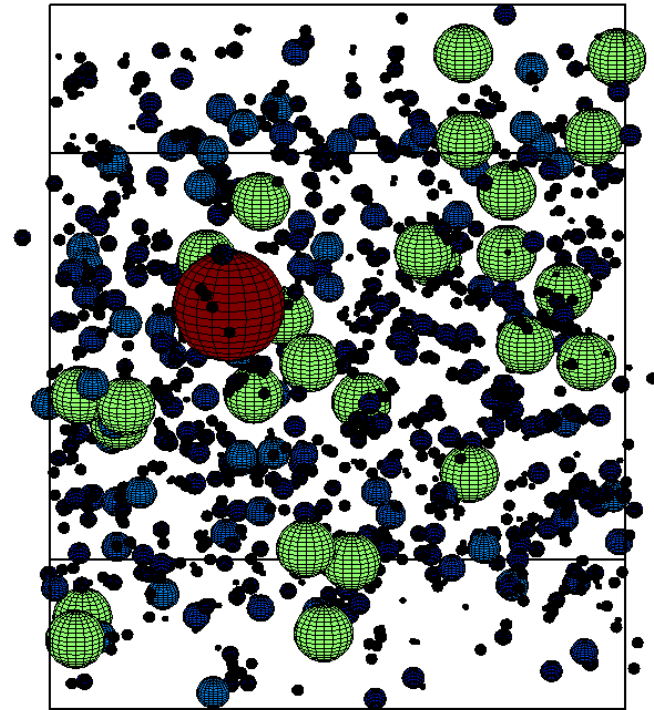
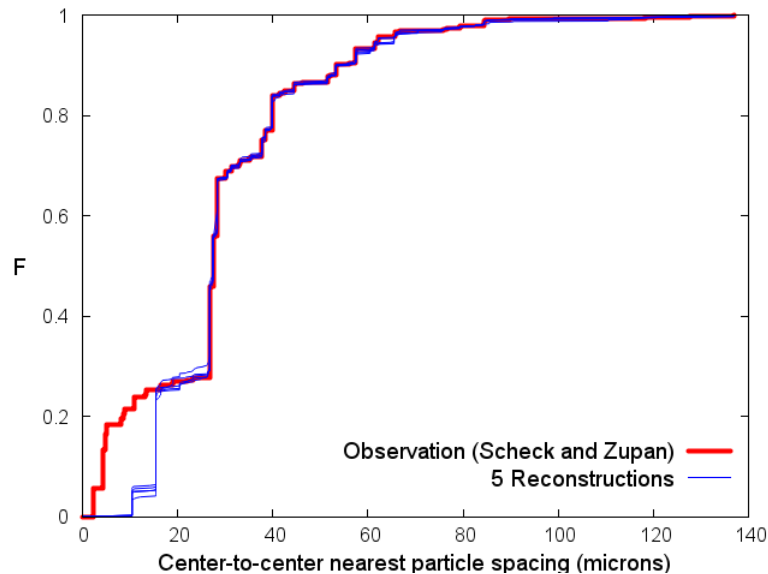
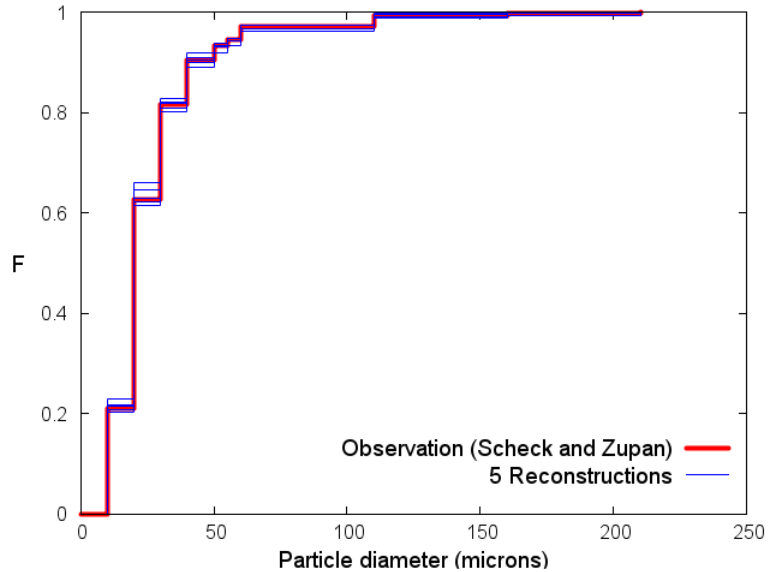
$$\begin{matrix} q_1(f_0, T, L) \\ q_2(f_0, T, L) \\ f_c(f_0, T, L) \end{matrix}$$



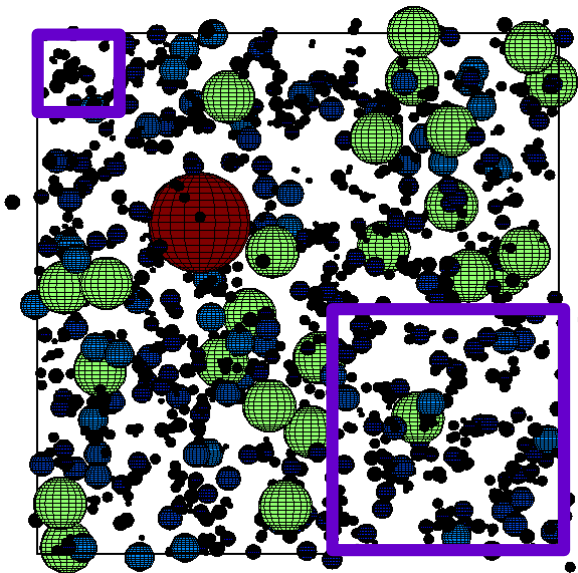
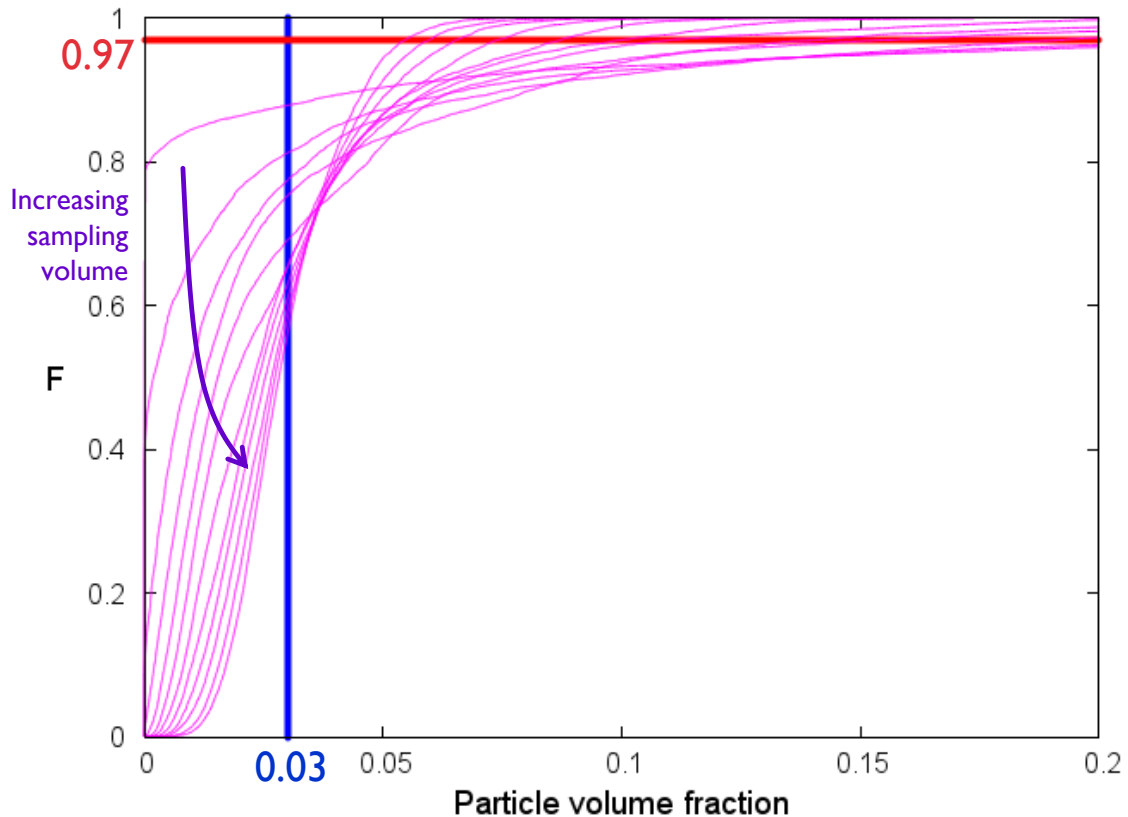
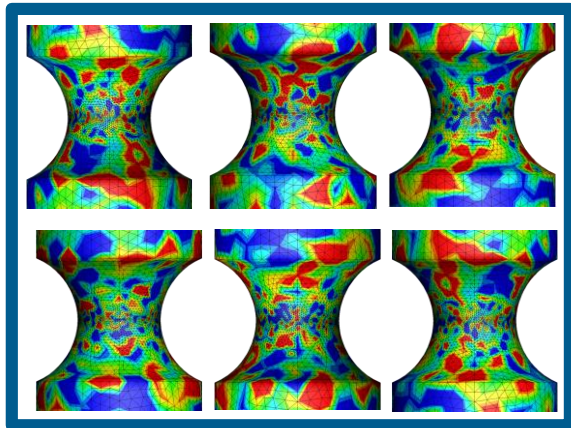
# CREATION OF REPRESENTATIVE MICROSTRUCTURES



Average particle volume fraction = 3%

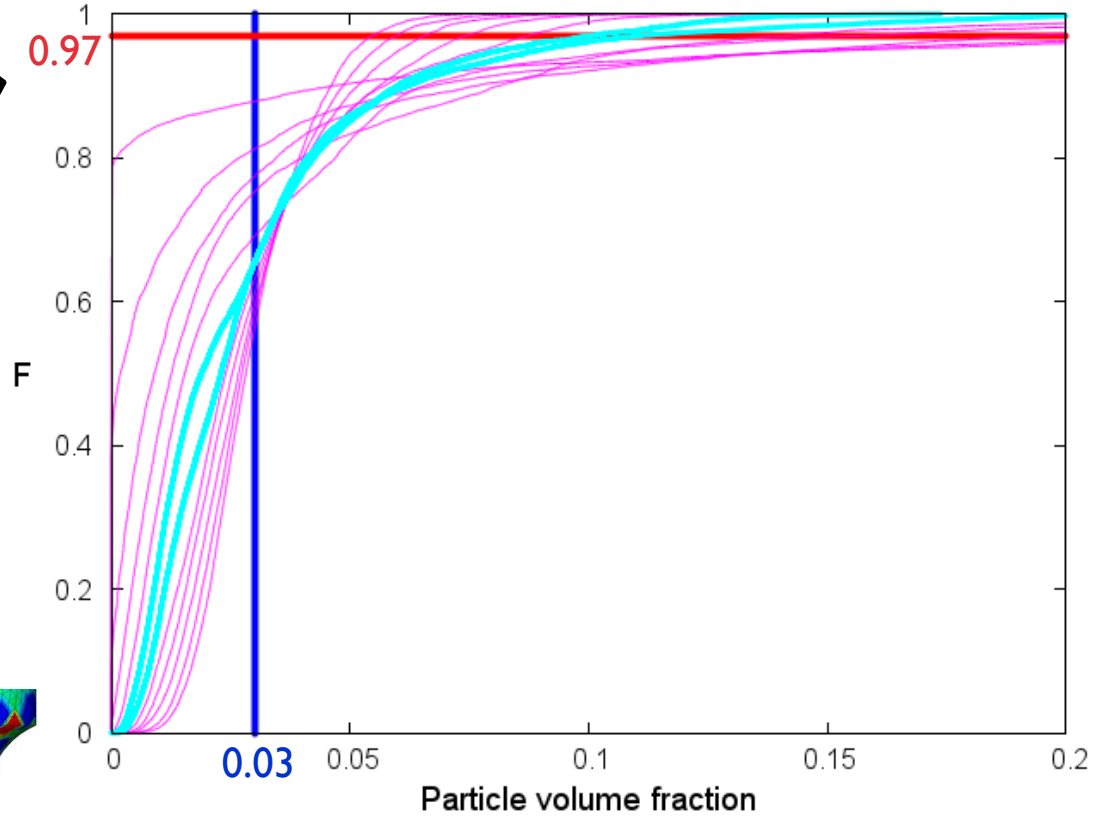
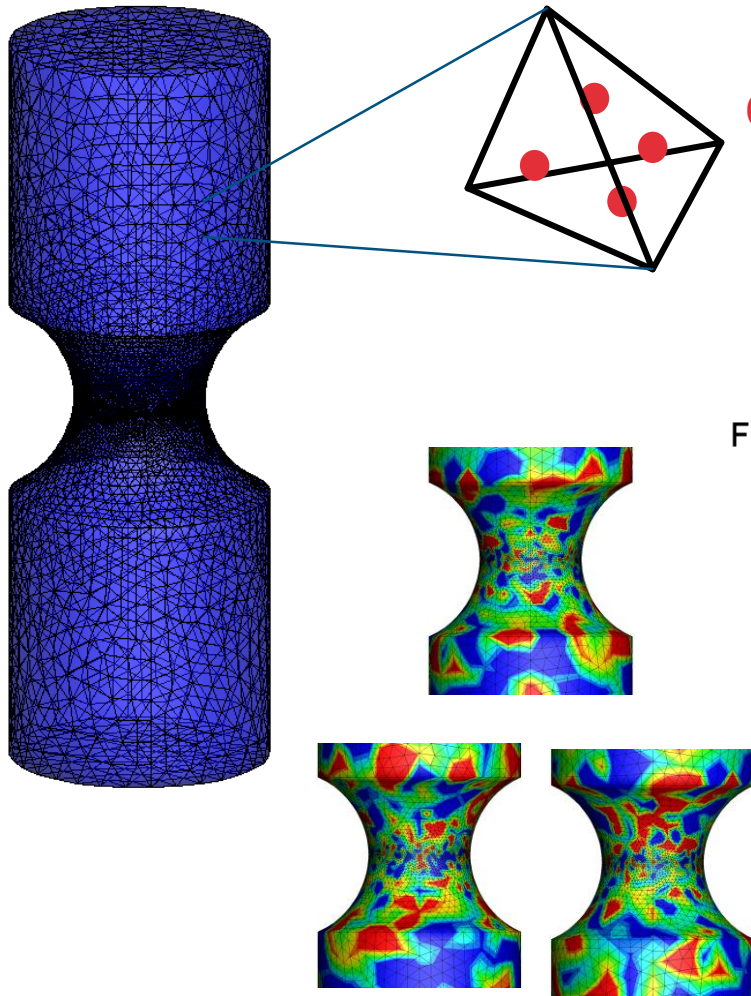
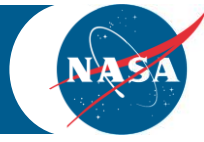


Looking for statistics on particle volume fraction ( $f_0$ )  
-dependent upon sampling volume!

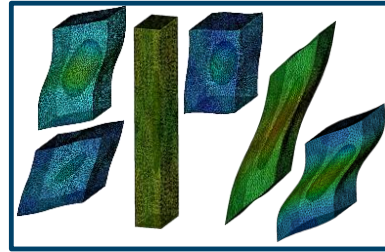
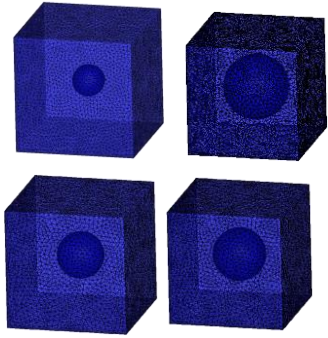




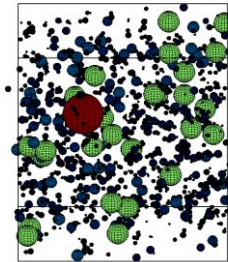
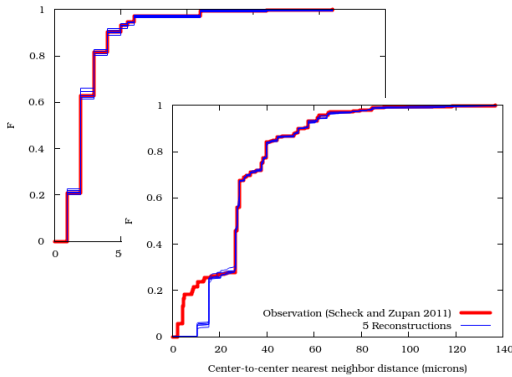
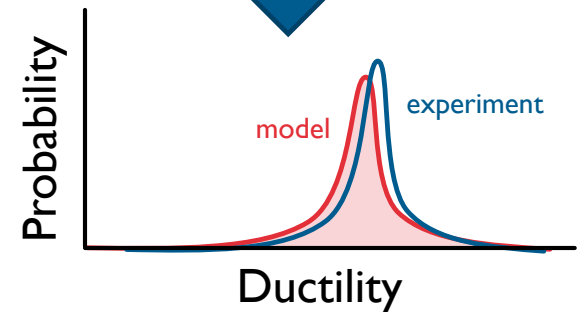
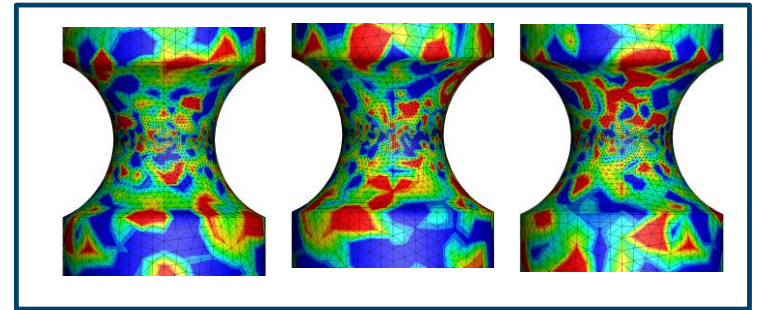
# ASSIGNING LOCAL MICROSTRUCTURE

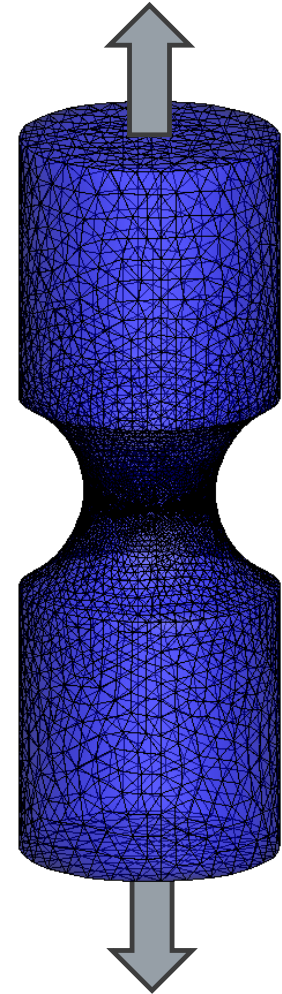
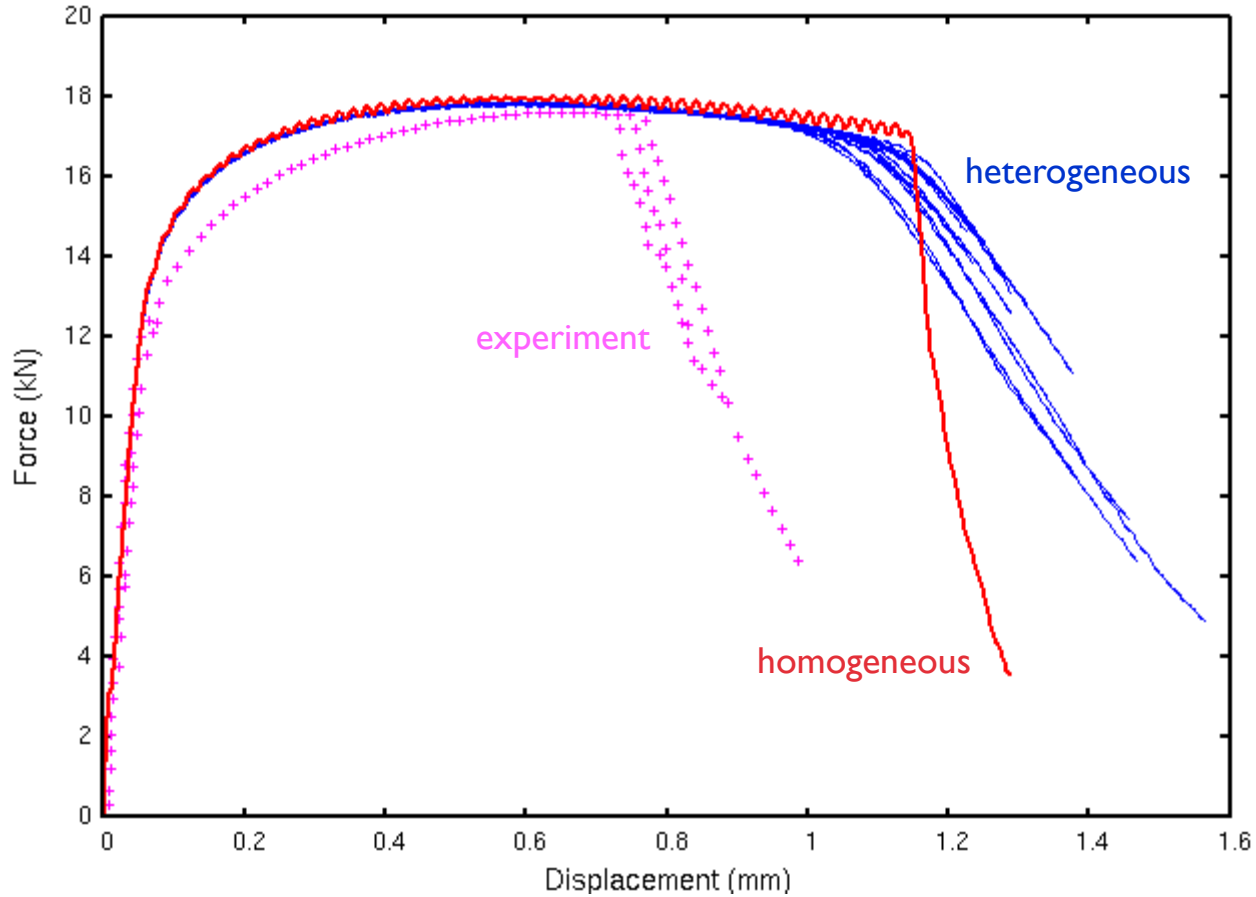


# RECAP ON SEEDING RANDOM MICROSTRUCTURES



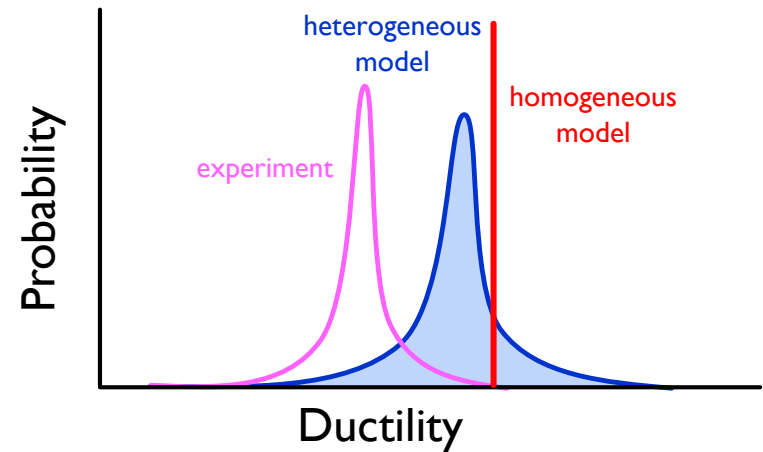
Response =  
 $f(\text{microstructure}, \text{loading})$







- Failure initiation in a homogeneous material over predicts ductility
- Microstructural heterogeneity leads to macro-scale uncertainty
- Better statistics on microstructure (from observation rather than reconstruction) are needed
- Incorporation of more microstructural features could yield improvements



THANK YOU!

ARE THERE ANY QUESTIONS?

