## 1 Static stress drop associated with brittle slip events on exhumed 2 faults

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## 9 Abstract

10 We estimate the static stress drop on small exhumed strike-slip faults in the Lake Edison 11 granodiorite of the central Sierra Nevada (California). The sub-vertical strike-slip faults were 12 exhumed from 4-15 km depth, and were chosen because they are exposed in outcrop along their 13 entire tip-to-tip lengths of 8-12 m. Slip nucleated on joints and accumulated by ductile shearing (forming quartz mylonites from early quartz vein filling in joints) and successive brittle faulting 14 15 (forming epidote-bearing cataclasites). The occurrence of thin, < 1 mm wide, pseudotachylytes 16 along some small faults throughout the study area suggests that some portion of the brittle slip 17 was seismic. We suggest that the contribution of seismic slip to the total slip along the studied 18 cataclasite-bearing small faults may be estimated by the length of epidote-filled, rhombohedral 19 dilatational jogs (rhombochasms) distributed semi-periodically along the length of the faults.

20 The interpretation that slip recorded by rhombochasms occurred in single events is based 21 on evidence that: 1) epidote crystals are randomly oriented and undeformed within the 22 rhombochasm; and 2) cataclasite structure in principal slip zones does not include clasts of 23 previous cataclasite. We thereby constrain *both* the rupture length and slip. Based on these 24 measurements, we calculate stress drops ranging over 90-250 MPa, i.e., one to two orders of 25 magnitude larger than typical seismological estimates for earthquakes, but similar in magnitude 26 to recent observations of small (< M2) earthquakes from the San Andreas Fault Observatory at 27 Depth (SAFOD). These inferred seismic ruptures occurred along small, deep-seated faults, and,

given the calculated stress drops and observations that brittle faults exploited joints sealed by quartz-bearing mylonite, we conclude that these were "strong" faults.

## 30 Introduction

#### 31 Statement of the problem

32 The static shear stress drop associated with earthquakes is a fundamental quantity that 33 scales linearly with slip, particle velocity and acceleration [Scholz, 2002], and is typically 34 calculated using a characteristic source dimension (e.g., fault radius for a circular fault), average 35 slip, and the estimated shear modulus of the host rock. The stress drop  $(\Delta \sigma)$  is defined as the difference between  $\sigma_{zx}^r$ , the peak shear stress in the remote field, and  $\sigma_{zx}^c$ , the shear stress 36 37 resolved on the fault after slip, where slip is in the x direction and z is normal to the fault. Kanamori [1994] distinguishes two end-member characteristic faults based on the stress  $\sigma_{zx}^r$  at 38 which they fail: (1) weak faults for which  $\sigma_{x}^{r} \approx 20$ MPa; and (2) strong faults for which 39  $\sigma_{zx}^{r} \approx 200 \text{MPa.}$ 40

41 Stress drops measured in triaxial experiments of shear failure of intact rocks are typically 42 on the order of hundreds of MPa to GPa [e.g., Brace and Byerlee, 1966]. Triaxial experiments 43 with sawcut samples have yielded slightly smaller stress drops in the range from tens to hundreds 44 of MPa [Brace and Byerlee, 1966]. These results indicate that, at least in the laboratory, faults in 45 geomaterials are strong. In both types of experiments, the shear stress drop was a fraction of the 46 peak yield stress; however stress drops on the order of hundreds of MPa in the upper crust would constitute a near total stress drop ( $\sigma_{zx}^c \approx 0$ ). Laboratory stress drops stand in stark contrast to 47 seismologically observed stress drops, typically on the order of 0.1-100 MPa, a fraction of the 48 49 shear strength of intact rock at seismogenic depths [e.g., Kanamori, 1994; Abercrombie, 1995].

50 The earthquake rupture process has long been considered to follow a self-similar scaling 51 relationship, as stress drop has been observed to be independent of magnitude [Aki, 1967]; 52 however this scale independence has been observed to break down for earthquakes below  $M_{L} \sim 3$ , 53 as small earthquakes appear to be associated with smaller stress drops [e.g., Archuleta et al., 54 1982; Hanks, 1982]. Minimum source dimensions on the order of 100 m have been inferred for 55 earthquakes, offering one solution for the apparent deviation in scaling [Archuleta et al., 1982, 56 Guo et al., 1992]. If 100 m is truly a minimum source dimension (presumably controlled by 57 geometry or nucleation length), then smaller observed moments must be attributed to a lower 58 values of average fault slip leading to smaller calculated stress drops. More recently, however, 59 this breakdown in scaling for small earthquakes has been established to be an artifact of severe 60 near surface attenuation of high frequency waves [e.g., Hanks, 1982]. Attenuation of high 61 frequency waves artificially distorts the amplitude spectrum, making interpretation of the corner 62 frequency difficult [e.g., Hanks, 1982; Hough and Anderson, 1988; Abercrombie, 1995; Prejean 63 and Ellsworth, 2001].

64 Researchers have attempted to circumvent the problem of small source resolution by 65 examining data recorded by seismometers closer to the source, in deep boreholes [Abercrombie, 66 1995], or in deep South African gold mines [e.g., *Richardson and Jordan*, 2002]. Recent studies 67 suggest that using borehole seismometers may not effectively alleviate problems with high frequency attenuation [Ide and Beroza, 2001; Imanishi and Ellsworth, 2006]. Using a stable 68 69 spectral ratio method to analyze microearthquakes from the San Andreas Fault Observatory at 70 Depth (SAFOD) seismic array in Parkfield, CA, Imanishi and Ellsworth [2006] showed that 71 there is no scaling breakdown for stress drop or apparent stress and found that half of the 72 microearthquakes examined had static stress drops greater than 10 MPa.

73	An alternative approach to studying the source of small earthquakes, which effectively
74	removes any spatial ambiguity introduced by inferring earthquake source dimensions, is to study
75	the earthquake source by direct examination of ancient earthquake ruptures along faults exhumed
76	from hypocentral depths. Detailed investigation of faults at the outcrop and microscopic scale
77	can resolve to high precision the spatial extent and geometry of rupture in two dimensions and
78	the fault slip. Given these parameters and the shear modulus of the fault host rocks the stress
79	drop can be calculated with the same elastic dislocation models commonly employed by
80	earthquake seismologists. Unfortunately, such estimates have been difficult to come by because a
81	number of factors need to be present in outcrop to successfully estimate the stress drop:
82	1) The fault must be exposed along its entire length in order to measure the source

dimension, and the fault must be isolated from nearby faults to lessen the potential forfault interaction;

85 2) Slip must be measured for a single slip event;

86 3) Evidence of seismic slip must be present if the slip is interpreted to be related to
87 ancient earthquakes. For exhumed faults, this means that pseudotachylyte (solidified
88 friction-induced melts produced during seismic slip; *Sibson*, 1975) must be present
89 within the slipping zone [*Cowan*, 1999].

Complete slip distributions have been measured along the entire length of faults exposed at the Earth's surface via remote sensing and field mapping [e.g., *Maerten et al.*, 2001; *Manighetti et al.*, 2001], and 3D seismic datasets [e.g., *Willemse*, 1997; *Kattenhorn and Pollard*, 2001]. Slip estimates along small exhumed faults most typically consist of sparse (one or two) measurements of piercing points along the fault representing only the relative particle displacement at the point of measurement [e.g., *Shipton et al.*, 2006]. With few exceptions [e.g., *Di Toro et al.*, 2005], slip measurements along natural faults almost always represent the total
accumulated slip (representing multiple slip episodes) during the history of fault activity.

Here we attempt to use geological observations to calculate the stress drops for slip events along small exhumed faults by describing deformation associated with single seismic slip events which can be mapped in two dimensions from one tip of the fault to the other. The results of these calculations are compared to data from the seismological record. This approach effectively removes ambiguity about the source dimensions and geometry inherent in the seismological inverse problem by affording direct observation of the source.

104

#### **Bear Creek Faults**

Fracturing and faulting has been documented in the Bear Creek drainage, in the southern half of the Mount Abbot quadrangle in the Sierra Nevada batholith [e.g., *Lockwood and Lydon*, 1975; *Segall and Pollard*, 1983a, 1983b; *Martel et al.*, 1988]. These studies have concentrated on the Lake Edison Granodiorite (~88 Ma) whose depth of emplacement is estimated at 4-15 km based on amphibole geobarometry [*Ague and Brimhall*, 1988]. K-Ar ages from muscovite in the fractures date the Bear Creek faults at 79 Ma, and these faults have been interpreted as having grown soon after pluton emplacement [*Segall et al.*, 1990].

Post-magmatic structures in Bear Creek include nearly vertical joints and faults [e.g., *Segall and Pollard*, 1983*a*, 1983*b*; *Martel et al.*, 1988]. Initial fracturing produced a single set of joints (Figure 1I) striking predominantly ENE [Segall and Pollard, 1983a; Martel et al., 1988]. Subsequent crystal-plastic shearing localized on the joints, producing quartz (from former quartz veins filling the joints) and granodiorite mylonites (Figure 1II, A). As pluton cooling progressed, cataclasis became the dominant deformation mechanism. Brittle slip localized on the boundaries between tabular quartz mylonites and host granodiorites (Figure 1II-III, B). *Griffith et al.* [2008] 119 showed that some of these brittle slip zones are associated with thin ( $<300 \mu m$ ), discontinuous 120 pseudotachylyte veins (Figure 1II-III, C). The pseudotachylytes are typically found in small 121 patches in narrow (< 200 µm) slip zones where cataclasite is either poorly developed or 122 completely absent [Griffith et al., 2008]. This observation suggests that pseudotachylyte was 123 either not formed in thicker (>200 µm) cataclasite slip zones due to distributed shear (and thus 124 broadened frictional heat generation), or were poorly preserved due to enhanced permeability of 125 the thicker granular cataclasite during exhumation. The presence of pseudotachylyte veins along 126 the Bear Creek faults suggests that these faults were seismic during the brittle phase of their 127 evolution.

## 128 Rhombochasms

#### 129 Field Observations

130 The Bear Creek small faults are commonly associated with epidote veins in extensional 131 domains along the faults (Figure 2), as for example: (1) at releasing bends along faults (Figure 132 2A); (2) where two fault segments link in dilational steps (e.g. left step for left-lateral faults; 133 Figure 2B); and (3) at fault tips as extensional splays [Segall and Pollard, 1983a]. A fourth 134 structure, distinctly different from the former three, occurs where the cataclastic slip zone jumps 135 from one side of a quartz mylonite to the other (Figure 2C). In this latter case the veins have a 136 typical rhomboidal shape and are referred to as *rhombochasms* throughout the following 137 sections. Where rhombochasms are present, they are often distributed semi-periodically along a 138 fault (Figure 3). The rhombochasms and the epidote-veins are often associated with bleached 139 halos in the adjacent host rock (Figure 2A-C), a result of plagioclase and biotite alteration to 140 saussurite and chlorite, respectively. In outcrops orthogonal to faults and parallel to the fault 141 slickenlines (approximately the case in the Bear Creek subhorizontal outcrops) the length of rhombochasms sides that are parallel to the fault provide a direct estimate of the fault slip as therhombochasm formed (e.g., Figure 3).

Minerals in the rhombochasms typically appear to be uniform in color and texture (prismatic epidote grains with no apparent preferred orientation, and minor chlorite). In some cases epidote are interspersed with brecciated subangular clasts of quartz and the host granodiorite (Figure 2C) resembling implosion breccias [*Sibson*, 1985; 1986].

#### 148 Microstructural Observations

149 Rhombochasms are filled principally with randomly oriented columnar (~0.1 to 2.5 mm 150 in length) epidote and variably with chlorite embedding subangular quartz clasts (Figure 4A-C). 151 The vein microstructure indicates growth in an open fluid-filled cavity without evidence of 152 incremental growth by the crack-seal mechanism [Ramsay, 1980] (Figure 4A). Crystals are not 153 deformed or broken (Figure 4C). Slip zones (generally <1mm thick) entering and departing on 154 the opposite sides of the rhombochasm (Figure 4B) are always left-stepped, switching from the 155 one boundary between quartz vein and host granodiorite to the other, consistent with the left-156 lateral sense of shear. Rhombochasms along the same fault consistently show the same stepping 157 asymmetry. We interpret this observation to mean that the length of each rhombochasm 158 approximates the brittle slip magnitude that occurred at the corresponding position along the 159 fault.

In some cases, thin (<200 μm), veins outline the slip zones and extend partly into the rhombochasms (Figure 4B, D). In Figure 4B, these veins overlap the rhombochasm by approximately 9 mm along the northeast boundary and approximately 5 mm on the southwest boundary. Thin epidote veins on the upper left and lower right corners of rhombochasms also extend for a short distance (a few cm) along the granodiorite-mylonite interface, but these

165 terminate at the rhombochasm opening (Figure 4B). The typical rhombochasm boundary is 166 knife-edged with no cataclasis of the host rock or the minerals in the rhombochasm at the 167 boundary (Figure 4E), whereas slip zones that penetrate into the rhombochasm form a contact 168 between undeformed rhombochasm mineral fillings and the host granodiorite. In some places, 169 slip zones penetrating into rhombochasms can be seen to truncate clasts within the rhombochasm, 170 while these slip zones are truncated at their tips by undeformed epidote crystals, suggesting that 171 rhombochasm mineral infilling was synchronous with slip (Figure 4F). In other cases the slip 172 zone terminates at the rhombochasm opening (Figure 4G).

173

# **Conceptual Model**

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175 The component of brittle slip along small faults resulting in cataclasite formation may be 176 distinguished from the slip contribution from previous ductile shearing because epidote-filled, 177 rhombohedron-shaped dilational jogs opened at bends and step-overs during brittle slip, and are 178 distributed along the length of the faults. We argue that brittle slip occurred along the measured 179 fault lengths in single slip events. Epidote crystals are randomly oriented and undeformed within 180 the rhombochasms (Figure 4C). The epidotes were not broken after initial opening and 181 precipitation as should be expected if the rhombochasms opened incrementally, as epidote 182 precipitation was coincident with slip along the faults. Also, some small faults in the Bear Creek 183 area contain pseudotachylytes [Griffith et al., 2008] suggesting that seismic slip occurred during 184 brittle deformation along these faults. However, as previously noted, pseudotachylytes are only 185 developed (or preserved) locally along small faults and tend to be absent in cataclasite slip zones 186 thicker than ~ 200  $\mu$ m [Griffith et al., 2008]. Because cataclasites along these faults are 187 consistently thicker than 200 µm, we should not expect to see pseudotachylyte if our previous 188 observations are predictive. However pseudotachylytes described by Griffith et al., 2008 do

189 show common static overgrowths of epidote. This suggests that the rhombochasm-bearing small 190 faults investigated in this study may also have developed during the same ambient conditions as 191 the pseudotachylyte-bearing faults, and is evidence that the rhombochasm-bearing faults may 192 also have been seismic. In some places rhombochasms contain breccias resembling implosion 193 breccias [e.g., Sibson, 1985; Sibson, 1986] that also point toward a fast rate of deformation. Slickenlines on faults commonly plunge less than 15° on studied faults and the offset measured 194 195 from the rhombohedron lengths on subhorizontal outcrop should underestimate the actual slip by 196 at most 4% (error =  $1 - \cos 15^{\circ}$ ).

197 The unique combination of factors listed above distinguishes these observations from 198 previous attempts to estimate coseismic parameters such as stress drop from exhumed faults 199 because we can constrain *both* the rupture length and slip [e.g., *Sibson*, 1975; *Di Toro et al.*, 200 2005].

## 201 Slip Distributions

Figure 3 shows the profiles of four small faults in the Bear Creek area exposed along their entire lengths, ranging from 8 to 12 m. We measured the total slip (from aplite dike offset) and the distributions of rhombochasm lengths for two faults, the Bear Creek Meadows Fault (BCMF) and the Upper Hilgard Fault (UHF) (Figure 5).

The BCMF consist of an en-echelon array of highly overlapping, right-stepping fault segments. We estimated brittle slip using seven rhombochasms distributed along the central segment (Figure 3, BCMF). No hard linkage was observed along the overlapping echelon segments on BCMF, nor was any macroscopic evidence evident for brittle reactivation of the mylonite fracture fillings on these segments overlapping the central one. The zero slip data points on either side of the slip distribution (Figure 5A) correspond to the tips of the central fault segment. Rhombochasms occur within the data gaps (e.g. position ranges 590-770 cm and 870-1350 cm), but they were too complicated in shape to use as slip markers. The presence of rhombochasms along the length of the BCMF does indicate that brittle slip occurred along the entire length of the fault segment; therefore the measured length of the fault segment accurately represents the source dimension. The slip maximum occurs slightly west of center and appears to taper toward the fault tips. The average measured brittle slip on the fault is 2.1 cm.

218 The UHF consists of two hard-linked fault segments (i.e. the fault segments are linked by 219 fractures across the relay zone). In the case of the UHF, only the easternmost fault tip is exposed. 220 The westernmost fault tip is buried under debris. This debris cover is approximately 2-3 m wide, 221 and the fault does not continue on the other side. Near the debris cover, splay cracks are 222 concentrated on the southern side of the fault. These two observations suggest that the fault length is no more than a couple of meters greater than the visible length. Rhombochasms are 223 224 distributed more evenly than in the BCMF, therefore the slip distribution is more clearly 225 discernable (Figure 5B). The slip distribution appears to be flat along most of the fault and 226 tapers sharply at the western end. Slip tapers more gently on each segment in the relay zone. 227 The average measured brittle slip on the UHF is 2.0 cm.

As suggested previously, the rhombochasm length distribution measured from outcrop maps should closely approximate the brittle slip distribution, and possibly the seismic slip distribution, along these faults. The observed offset of an aplite dike on the BCMF is approximately 35 cm, while that measured along the UHF is 42 cm. Both of these are significantly greater than the measured brittle slips. This gives us an indirect way to estimate the ductile (i.e., crystal-plastic shear of quartz) contribution to slip. The discrepancy between brittle

slip and total slip should approximate the offset from ductile shearing of the tabular quartzmylonites extending much of the length of the faults.

#### 236 Stress Drop

The constant stress drop model used to calculate the stress drops of ruptures on the rhombochasm-bearing Bear Creek faults, and in many seismological models [e.g., *Kanamori and Anderson*, 1975], is a special case of the *Eshelby* [1957] analytical solution for the elastic field of an ellipsoidal inclusion. The circular "penny-shaped crack" model assumes that the principal ellipsoidal axis *c* is much smaller than the other principal axes, *a* and *b* (Figure 6). If the elliptical fault can be approximated as a circle (a = b) the slip distribution is given by [*Eshelby*, 1957, eq. 5.7]:

244 
$$\pm D(r) = \frac{\Delta\sigma}{\mu} \frac{4(2-\nu)}{\pi(1-\nu)} R \sqrt{1-\frac{r^2}{R^2}} = \frac{1}{2} \Delta D(r)$$
(1)

where *D* is the particle displacement on either side of the fault and  $\Delta D$  is the displacement discontinuity (slip) across the fault at each point *r*,  $\Delta \sigma$  is the stress drop,  $\mu$  is the elastic shear modulus of the medium and *v* the Poisson ratio. The model assumes a constant stress drop on a circular fault of radius *R* in a linear elastic whole space. The expression for  $\Delta \sigma$  of an earthquake given the average slip  $\Delta \overline{D}$  across the fault and assuming a Poisson solid (*v* = 0.25) is [e.g., *Keilis Borok*, 1959; *Kanamori and Anderson*, 1975]:

$$251 \qquad \Delta\sigma = \frac{7\pi}{16}\mu \frac{\Delta D}{R} \tag{2}$$

252 The assumption of a Poisson solid is a good approximation for granodiorite based on laboratory 253 tests [*Gercek*, 2007]. Using this relationship, a shear modulus of  $\mu = 30$ GPa, average slip  $\Delta \overline{D} \approx$ 254 2.1 cm, and radius R = 5.75 m (Table 1) the coseismic static stress drop on the BCMF is approximately  $\Delta \sigma \approx 150$  MPa. A similar calculation based on the UHF yields a stress drop of 130 MPa. These are large stress drop values relative to the expected range 0.1 to 100 MPa. Before we discuss the implications of these findings, we first analyze potential sources of error in the analysis.

#### 259 **Discussion**

260

## 261 Uncertainty and Analysis Limitations

Here we identify and attempt to quantify the sources of error for the stress drops calculated in the previous section. Possible sources of error are divided into two groups: (1) assumption of the source geometry (2) differentiation between seismic and aseismic slip; and (3) measurement of slip. The calculated stress drops for the BCMF and the UHF are summarized in Table 1.

267 (1) Source Dimensions

Eshelby's general solution for slip on an elliptical crack with aspect ratio a/b on which slip is parallel to the *a* axis is given by:

270 
$$\pm D(x, y) = \frac{b\Delta\sigma}{C_1\mu}\sqrt{1 - \frac{x^2}{a^2} - \frac{y^2}{b^2}} = \frac{1}{2}\Delta D(x, y)$$
 (3)

This is the more general form of eq. (1) in Cartesian coordinates where slip is parallel to the *x*axis. The coefficient  $C_1$  is a function of the aspect ratio of the elliptical fault geometry and is given by *Eshelby* [1957, eq. 5.3]:

$$C_{1} = E(k) + \frac{v}{1-v} \frac{K(k) - E(k)}{k^{2}}; \qquad a > b, k = \sqrt{1-b^{2}/a^{2}}$$

$$274 \qquad = \frac{b}{a} \left[ E(k) + \frac{v}{1-v} \frac{K(k) - a^{2}/b^{2} E(k)}{k^{2}} \right]; \quad b > a, k = \sqrt{1-a^{2}/b^{2}}$$

$$= \frac{\pi (2-v)}{4(1-v)}; \qquad a = b$$
(4)

275 Here E(k) and K(k) are complete elliptical integrals of the first and second kind respectively. 276 Madariaga [1977] evaluated similar expressions for the stress drop in terms of the average slip,  $\Delta \overline{D}$ : 277

278 
$$\Delta \sigma = \frac{\mu}{C_2} \frac{\Delta D}{W}$$
(5)

279 Where W is the shortest principal axis of the fault model (i.e. W=R for the circular fault). For the circular ('penny-shaped') fault the commonly cited result for the coefficient  $C_2$  is 16/7 $\pi$  [e.g., 280 Kanamori and Anderson, 1975].  $C_2$  can be calculated for elliptical model faults of a variety of 281 282 aspect ratios using [Madariaga, 1977]:

$$C_{2} = 4 \left[ 3E(k) + \frac{K(k) - b^{2}/a^{2} E(k)}{k^{2}} \right]^{-1}; \quad a > b, k = \sqrt{1 - b^{2}/a^{2}}$$

$$= 4 \left[ 3E(k) + \frac{a^{2}}{b^{2}} \frac{K(k) - E(k)}{k^{2}} \right]^{-1}; \quad b > a, k = \sqrt{1 - a^{2}/b^{2}}$$
(6)

284 In calculating the stress drop, we previously made the simplifying assumptions that (i) the fault 285 mapped in two dimensions with measured half length  $R_a$  can be represented in three dimension 286 by a circular fault; and (ii) that the radius R of the fault is equivalent to the measured half length  $R_a$ . Below we assess the net effect of each of these assumptions. 287

288 First, we keep the assumption that the fault is circular, but we relax the assumption that 289 the apparent radius  $R_a$  exposed at the earth's surface is equal to the actual radius R of the crack. 290 Let the line A-B (Figure 6A) be the intersection of the circular fault with the Earth's surface. 291 Because the slip maximum according to eq. 1 occurs at the center of the fault (r=R), the stress 292 drop can be expressed as a function of the maximum slip,  $\Delta D_{max}$ :

293 
$$\Delta \sigma = C_1 \mu \frac{\Delta D_{\text{max}}}{R}$$
(7)

With no knowledge of the actual size, using the apparent radius  $R_a$  and the maximum apparent slip  $D_a$  measured at point *m*, an apparent stress drop  $\Delta \sigma_a$  is obtained:

296 
$$\Delta \sigma_a = C_1 \mu \frac{\Delta D_a}{R_a}$$
(8)

However, according to Figure 6A we may replace  $r = R \sin \theta$  in eq. 1 to obtain:

298 
$$D(r) = \frac{\Delta\sigma}{C_1\mu} R\sqrt{1-\sin^2\theta}$$
(9)

299 and using the fact that  $R_a = R \cos \theta$  we obtain:.

$$300 \quad \Delta\sigma_a = \frac{\Delta\sigma\sqrt{1-\sin^2\theta}}{\cos\theta} = \Delta\sigma \quad . \tag{10}$$

In conclusion, the ratio  $D_a/R_a$  remains identical to D/R; as a consequence, measurement of apparent maximum slip and radius along any arbitrary section of a circular model fault yields the correct stress drop estimate through eq. (3). The same observations apply when using average apparent slip, instead of the maximum apparent slip: the correct scaling with stress drop is maintained through any section of the model fault. It can also be shown that the apparent half length, *a*, of any elliptical fault scales linearly with slip.

307 If the assumption that the crack is circular is dropped, and the possibility is considered 308 that the fault may approximate an ellipse, the resulting stress drop will vary depending on the 309 aspect ratio of the fault and the length of the semi-minor axis. We can calculate the stress drop 310 for elliptical faults using eq. (5) and (6). If we assume that a reasonable range of elliptical fault 311 aspect ratios is in the range  $0.5 \le a/b \le 2$ , then we can calculate the range of possible stress drops 312 represented by two dimensional fault exposures. Faults of aspect ratios less than one, on which 313 the slip direction is parallel to the semi-minor axis (Figure 6B), were called 'transversal slip' 314 faults by *Madariaga* [1977] while faults with aspect ratios greater than one, on which slip is

315 parallel to the semi-major axis, were classified as 'longitudinal slip' faults (Figure 6C). If the 316 BCMF is a transversal slip fault with an aspect ratio equal to 0.5, the corresponding stress drop is 317 reduced to  $\Delta \sigma \approx 110$  MPa. Assuming the BCMF is a longitudinal slip fault with an aspect ratio 318 equal to 2 implies that the semi-minor axis is vertical, and the apparent length of the semi-minor 319 axis is half the measured length of the fault in the field. Correspondingly, using the value 320 W=b=3m, and the appropriate expression from eq. (6), the corresponding stress drop is  $\Delta\sigma \approx 250$ 321 Thus, taking into account the geometric error introduced by extrapolating the two MPa. 322 dimensional map to three dimensions extends the range of possible stress drop values to 110 323 MPa  $\leq \Delta \sigma \leq 250$  MPa. Similar estimates for the stress drop on the UHF yield stress drops of 90 324 MPa  $\leq \Delta \sigma \leq 230$  MPa.

## 325 (2) Differentiation between seismic and aseismic slip

326 Ultimately, stress drop and slip under brittle conditions should not be very different 327 whether they occurred quasi-statically or seismically. Due to dynamic overshoot, slip (and stress 328 drop, may be as much as 30% larger during seismic slip [Madariaga, 1976]. The recognition of 329 seismic slip from outcrop observations along faults remains a difficult and controversial topic 330 [e.g., *Cowan*, 1999]. We argue that the slip recorded by rhombochasms may have been seismic 331 based on two lines of evidence: i) textures within the opening rhombochasms suggest that the 332 associated slip was nearly instantaneous. These textures include randomly oriented epidote 333 grains in all rhombochasms as well as implosion breccias. The fact that these textures show no 334 post-formation shearing disruption suggest that they formed in a single event. (ii) Thin (<1mm) 335 pseudotachylyte veins are found on nearby Bear Creek faults [Griffith et al., 2008]. These 336 observations support the interpretation that brittle slip along these faults was seismic.

337 *(3) Measurement of slip* 

338 Here we present a kinematic model for the rhombochasm formation (Figure 7) to justify 339 in more detail our assumption that the length of the rhombochasm represents the magnitude of 340 slip in a single event. The faulting begins as a tabular quartz mylonite with distributed crystal-341 plastic shearing across its thickness and bounded on either side by granodiorite (Figure 7i). 342 Shearing across the quartz mylonite involves no slip at the mylonite-granodiorite interfaces. 343 Subsequently, more localized brittle shearing develops at the interfaces forming cataclasite slip 344 zones in a left stepping configuration (Figure 7ii). A small amount of localized shearing 345 continues until the tensile strength of the quartz mylonite in the relay zone is exceeded [e.g., 346 Segall and Pollard, 1980; Martel and Pollard, 1989; Mutlu and Pollard, 2008], and a tensile 347 opening fracture forms, linking the two cataclastic slip zones (Figure 7iii). This linking fracture 348 cuts the cataclastic slip zones into short, abandoned, non-shearing zones including the tips, and 349 actively shearing echelon zones on either side of the tabular quartz mylonite. As slip progresses 350 in the echelon cataclastic zones, deformation in the quartz mylonite is primarily ascribed to 351 opening of the rhombochasm (Figure 7iv). On the interface between the granodiorite and 352 rhombochasm interior, there is no new cataclasite generation, thus cataclasite thins from the 353 actively slipping zone to the distal edge of the rhombochasm. As slip progresses, thin cataclasite 354 far from the actively shearing zone is spalled into the rhombochasm and/or dissolved as fluids 355 are sucked into the rhombochasm from the adjacent granodiorite (Figure 7v). As shearing ceases, 356 within the rhombochasm only the portion of the cataclastic zone closest to the actively shearing 357 cataclasite zone if any at all is preserved. Epidote is precipitated and fills the rhombochasm with 358 euhedral, randomly oriented crystals. In this model, the length of the rhombochasm should 359 approximate the magnitude of slip,  $\Delta D$ , of a single slipping event.

360 We note that a small amount of underestimation is introduced by assumption that this 361 process can be approximated by the kinematic block model summarized above. In Figure 7iii, a 362 small amount of slip must accumulate along the cataclastic zones before the tensile strength in 363 the relay zone is exceeded [e.g. Segall and Pollard, 1980]. This slip is not recorded by the 364 rhombochasm opening; however we expect the amount of slip necessary to breach the relay zone 365 to be very small relative to the rhombochasm length. Also of note is that average measured 366 rhombochasm length measured on the Bear Creek faults is approximately 2 cm, within the range 367 of single slip values estimated for nearby pseudotachylyte-bearing faults based on conductive 368 heat transfer calculations [Griffith et al., 2008].

## 369 Stress Drop Implications

370 The stress drops estimated here are large relative to the majority of data available in the 371 seismological literature [e.g., Abercrombie, 1995]; however they are not without precedent. 372 Stress drops on the order of hundreds of MPa appear to be rare, but have been observed using 373 seismology [Kanamori, 1994]. Munguia and Brune [1984] calculated stress drops in excess of 374 200 MPa for events in the Victoria, Baja California earthquake swarm of 1978. Kanamori et al [, 375 1990; 1993] estimated stress drops for a small earthquake in Pasadena, CA between 30 and 200 376 MPa. Imanishi and Ellsworth [2006] studied 34 M-0.2-M2.1 earthquakes near Parkfield, CA 377 from the SAFOD Pilot Hole Array and found that half had stress drops greater than 10 MPa, with 378 some exceeding 50 MPa. Nadeau and Johnson [1998] estimated stress drops on the order of 100 379 MPa and greater for repeating micro-earthquakes near Parkfield. They found that stress drops increased with decreasing seismic moment up to  $\Delta \sigma \approx 2000$  MPa for the smallest earthquakes 380 381 (W≈0.5) [Nadeau and Johnson, 1998]. This is approximately the lattice shear strength of an 382 asperity in granitoid rocks with no unhealed flaws [Sammis et al., 2001].

Stress drops calculated using values from field mapping of the BCMF and UHF are in the range 90 MPa  $\leq \Delta \sigma \leq 250$  MPa considering a range of three dimensional source geometries. These values are near the upper bound of scaling relationships based on the bulk of seismological data available [*Kanamori*, 1994; *Abercrombie*, 1995], yet they lie within observed ranges of microearthquakes near Parkfield. Because they are on the order of hundreds of MPa, we suggest that these were "strong" faults as defined by *Kanamori* [1994].

The interpretation that the Bear Creek faults represent "strong" faults is consistent with 389 390 interpretations regarding observations of pseudotachylyte-bearing faults in other locations [e.g., 391 Di Toro and Pennacchioni, 2005; Sibson and Toy, 2006]. Our observations indicate that the 392 stress drop associated with earthquake ruptures along these faults represent a large percentage of 393 total fault strength. The reason for this may lie in the nature of the interface on which the slip 394 events occurred. All of the brittle slip that took place on the rhombochasm-bearing faults 395 occurred on the interface between mylonitized quartz veins and the adjacent host granodiorite. 396 This interface may have represented an at least partially healed asperity, stronger than a typical 397 frictional fault, yet weaker than the surrounding undamaged granodiorite such that flaws 398 concentrated and grew along the quartz mylonite-granodiorite interface.

## 399 **Conclusions**

400 Using detailed mapping of small faults in the Bear Creek drainage of the central Sierra 401 Nevada, we estimate coseismic stress drops for ancient earthquakes using rhombochasms as slip 402 markers. This method constrains, with high resolution in two dimensions, the source dimensions 403 of ancient brittle slip events. Errors introduced in the stress drop calculations by inferring the 404 three dimensional fault geometry from the mapped geometry is approximately a factor of two. 405 The total range of possible stress drops is 90 MPa  $\leq \Delta \sigma \leq$  250 MPa. This is larger than typical

- 406 estimates for small earthquakes, and at the upper limit of self-similar scaling laws for all
- 407 earthquakes. Therefore we suggest that faults of the Bear Creek area were strong faults, and
- 408 earthquakes along these faults represented static stress drops that were a large fraction of the
- 409 total fault strength.

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# 530 Figure Captions

- 531
- 532 Figure 1: Conceptual model of macroscopic and microscopic evolution of faults in Bear Creek.
- 533 I-III correspond to the macroscopic evolution of faults suggested by Martel et al (1988), where
- in stage I joints form in response to thermal stresses; stage II is marked by slip nucleation along

535 joints and subsequent linkage to form small faults; and in stage III simple fault zones composed 536 of paired small faults linked by secondary fractures form due to interaction of neighbouring 537 faults. Martel (1990) also proposed a fourth stage of development in which simple fault zones 538 coalesce to form large, complex fault zones, but the fourth stage has been omitted from this 539 figure for simplicity. Dashed circles in II and III indicate the location of A, B, C, and D. A-D 540 represent the microstructural evolution of faults from the time that shearing commences to the 541 transition from shearing deformation to zeolite veining. (A) Quartz precipitated in dilatational 542 regions along faults is sheared at temperatures greater than  $400^{\circ}$ C producing quartz mylonites. (B) 543 Boundaries between mylonites and granodiorites are filled with epidote veins and reactivated by 544 cataclasites cemented by epidote. Locally cataclasites and epidote veins cut across mylonites. (C) 545 Thin, discontinuous pseudotachylyte veins form due to seismic slip, and locally cut mylonites 546 and cataclasites. (D) The termination of shear deformation is signified by opening of faults and 547 zeolite mineralization.

548

Figure 2: Field photographs (left side) and schematic drawings (right side) of three different types of epidote-filled dilational jogs found along Bear Creek faults. (A) A releasing bend in a fault. (B) A dilational stepover between two small faults. (C) A dilational stepover between two cataclastic slip surfaces localized on the boundary between tabular quartz mylonites and host granodiorite. The configurations shown in B and C produce rhombohedron-shaped openings (rhombochasms) which can be used as slip markers along the faults. Gray = granodiorite; green = epidote; white = quartz mylonite; and bleached/speckled = altered granodiorite.

556

Figure 3: Trace maps of rhombochasm-bearing faults. (BCMF) Bear Creek Meadows Fault;.
(UHF) Upper Hilgard Meadows Fault with segments 1 and 2 from Figure 5B; (LHF); Lower
Hilgard Meadows Fault; (BJF) Big Juniper Fault.

560

561 Figure 4: Rhombocham microstructures. (A) Field photograph of rhombochasm pictured in B. (B) 562 Photomosaic of a rhombochasm on the Bear Creek Meadows Rhomb Fault (Fig. 3, BCMF) 563 (optical photomicrograph, plane polarized light). (C) Epidote crystals and quartz grains from 564 Lower Hilgard Meadows Fault (Figure. 3, LHF) (optical photomicrograph, plane polarized light). 565 (D) Dark vein penetrating into the rhombochasm from BCMF (see Figure 4G). This vein is part 566 of the slip zone extending into the rhombochasm, and has some identifying characteristics of 567 pseudotachylyte (injection vein, aphanitic, optically cloudy), but upon closer inspection consists 568 of ultrafine-grained epidote. The dark vein is truncated by a later zeolite-bearing vein (optical 569 photomicrograph, plane polarized light). (E) Contact between rhombochasm filling and 570 granodiorite. No evidence of slip is preserved along this contact (SEM backscattered electron 571 image). (F) The ~0.2-0.4 mm thick slip zone separating rhombochasm filling and granodiorite 572 (SEM backscattered electron image). Images E and F were taken along the same (upper "slip 573 zone"??) rhombochasm-granodiorite contact from fault BCM. (G) Slip zone along the BCMF 574 which does not penetrate into the rhombochasm. Note that fabric formed by epidotes is seamless 575 between the rhombochasm and the slip zone. Image is taken from a rhombochasm several 576 centimeters from the rhombochasm from Figure 4 E & F along the BCMF.

578 Figure 5: Slip distributions along (A) the Bear Creek Meadows Rhomb Fault (BCMF) and (B) 579 the Upper Hilgard Rhomb Fault (UHF), as determined by measuring the length of 580 rhombochasms (brittle slip) and dike offset (ductile slip).

581

Figure 6: Constant stress dropped models for elliptical faults with aspect ratios (a/b) varying from 0.5 to 2. For each model, the upper diagram shows the coordinate system and the hypothetical erosional surface exposed in outcrop is shown by the line A-B. The lower plot in each diagram shows predicted slip distributions for a given constant stress drop. Note that the horizontal axis a is equal in all plots. Only the unknown b axis varies in each plot. (A) Penny shaped-crack model (a/b=1). (B) Transversal slip fault (a < b). (C) Longitudinal slip fault (a > b). See text for more detail.

589

Figure 7: Kinematic model for rhombochasm formation where stages in (A) indicate the steps of rhombocasm initiation and (B) and (C) illustrate possible stages during the rhombochasm evolution. See text for complete discussion.

## 593 **Tables**

594 Table 1: Summary of Fault Source Parameters

			$\Delta D_{ave}$	$\Delta D_{max}$	Dike	offset	
Fault	W (m)	a/b	(cm)	(cm)	(cm)		$\Delta \sigma$ (MPa)
BCMF	5.75	1	0.8-2.1	4.5	35		150
BCMF	5.75	0.5	0.8-2.1	4.5	35		110
BCMF	2.88	2	0.8-2.1	4.5	35		250
UHF	6.25	1	0.8-2.0	3.6	42		130
UHF	6.25	0.5	0.8-2.0	3.6	42		90
UHF	3.13	2	0.8-2.0	3.6	42		220
LHF	-	-	2.6	5.1	14		-
BJF	-	-	1.2	2.6	4.8		-















