

Effect of faults and fractures on oilfield flow rate data: long-range correlations in a complex system

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*Results of ITF (Aberdeen) 'Coffers' project
Data provided by Statoil, sponsored by BP, Shell, Statoil,
Conoco-Phillips, Maersk, Total, Hess, BG group, DTI.*



References

- Main, I.G., L. Li, K. Heffer, O. Papasouliotis & T. Leonard (2006). Long-range, critical-point dynamics in oilfield flow rate data, *Geophys. Res. Lett.* 33, L18308, doi:10.1029/2006GL027357.
- Heffer, K., X. Zhang, N. Koutsabeloulis, I. Main and L. Li (2007). Identification of activated (therefore potentially conductive) faults and fractures through statistical correlations in production and injection rates and coupled flow-geomechanical modelling, *Society of Petroleum Engineers*, paper no. 107164, 9pp.

In press

- Main, I.G., L. Li, K. Heffer, O. Papasouliotis, T. Leonard, N. Koutsebaloulis & X. Zhang (2007). The Statistical reservoir model: Calibrating faults and fractures, and predicting reservoir response to water flood, in Jolley, S. (ed.), *Geol. Soc. Lond., special volume on Complex Reservoirs*.
- Zhang, X., N. Koutsebaloulis, K. Heffer, I. Main and L. Li (2007). Analysis of geomechanics and production data for critically-stressed reservoirs – generic characteristics and application to Gullfaks, in Jolley, S. (ed.), *Geol. Soc. Lond., special volume on Complex Reservoirs*.

Preamble: triggering phenomena

- **Earthquake-earthquake (Marsan et al, Huc & Main, Helmstetter & Sornette, Felzer & Brodsky)**
 - static or dynamic?
- **Pore pressure-earthquake (Segall, Kohl & Megel)**
 - poroelasticity and induced seismicity
- **Earthquake-pore pressure (Doan & Cornet)**
 - borehole response
- **Pore pressure-pore pressure? (Main et al, Heffer et al)**
 - flow rate-flow rate
- ⇒ **Reservoir modelling**

Monarch to get a face-lift

REPEREPIED of Singapore is to rebuild Diamond Offshore (listing) using Victory class semi-submersible. Caslen Bunka (now renamed Ocean Monarch), a deepwater unit with 6th-generation capabilities. The \$300million reconstruction will result in the rig being able to drill in up to 1500m of water using its mooring system. The revamped rig should be ready for work late 2008. This is the fourth in a series of 6th-generation Victory class upgrades that include the Ocean Harpoon, Ocean Rover and Ocean Defender. Monarch is currently docked at the Gulf of Mexico.

Big spender

MEXICAN state operator Pemex plans to invest \$100bn in the exploitation of deeper waters in Mexico's sector of the Gulf of Mexico over the next decade. The first 10 exploration wells have already been spudded offshore. Pemex says the first 100m will be followed by the Caspian pipeline. Pemex is planning 1100 wells this year alone onshore and says this year with a massive drilling programme planned. The target is 600 new wells.

Earthquake modelling technique provides reservoir pointers

IN THE PIPELINE

through the Aberdeen-based technology leader, IFF Duncan Anderson, IFF's subsurface technology manager, said: "The COFFRES project has made excellent progress in developing a methodology to model fluid flow in complex reservoirs. It will eventually be possible for operating companies to incorporate the software within their existing workflows to help optimise production strategies."

The COFFRES project will be presented at The Geological Society's Structural Complex Reservoirs conference, which is being held in London from February 24 until March 2. Instead, the three-day international conference was inspired by the IFF programme of the same name, of which the COFFRES project was part.

The conference includes leading contributions from industry and academic researchers, specialist presenters and practitioners with unique field case studies. The conference proceedings will be organised in a Geological Society Special Publication.

For more information, contact Duncan Anderson at IFF on d.anderson@iff.com



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




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The Press and Journal

Outline

-  **Background concepts: statistical forecasting, parsimony in model fitting, principal component analysis, geo-mechanics and permeability**
-  **The statistical reservoir model**
-  **Application to the Gullfaks field, North Sea**
-  **Application of a geo-mechanical model to the same field**
-  **Conclusions**

Statistical forecasting

Example: Buying a house

££ = ??



Buying a house: A statistical model

$$\text{££} = w_1 x_1 + \dots$$



Buying a house: A statistical model

Local School?

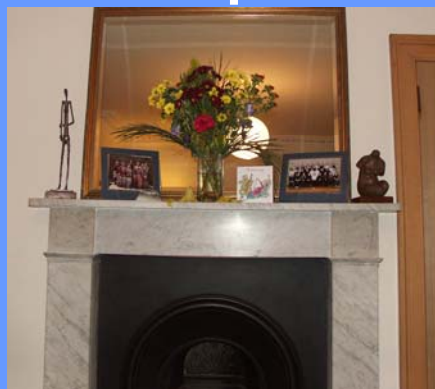
$$\text{££} = w_1 x_1 + w_2 x_2 + \dots$$



Buying a house: A statistical model

Local School? South Facing Garden?

$$\text{££} = w_1x_1 + w_2x_2 + \dots + w_ix_i + w_{i+1}x_{i+1} + \dots$$



Buying a house: A statistical model

Local School? South Facing Garden?

$$\text{££} = w_1x_1 + w_2x_2 + \dots + w_ix_i + w_{i+1}x_{i+1} + \dots + w_nx_n$$

Period features?



Buying a house: A statistical model

Local School? South Facing Garden?

$$w_i, i = 1, n$$

Define a set weights

$$\pounds\pounds = w_1x_1 + w_2x_2 + \dots + w_ix_i + w_{i+1}x_{i+1} + \dots + w_nx_n$$

Period features? Kitchen Sink

SIGNAL

NOISE

A History of Parsimony

- **William of Ockham:** “That which is accomplished by fewer (assumptions) is accomplished in vain with more”

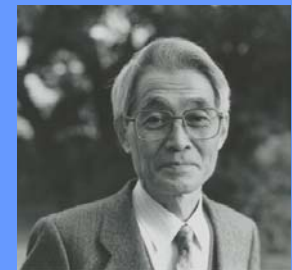
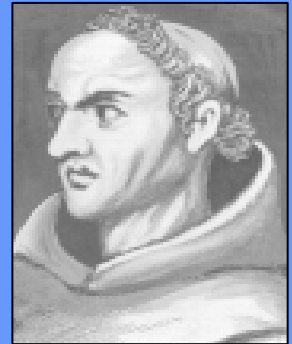
- **Carl Friedrich Gauss**

$$\sigma^2 = \sum_{i=1}^n [y_i - \hat{y}(x_i)]^2 / (n - p)$$

- **Hirotsugu Akaike**

$$AIC = n \ln \left\{ \sum_{i=1}^n [y_i - \hat{y}(x_i)]^2 / n \right\} - p$$

n = no. of data points
 p = no. of parameters



Information vs. goodness of fit

$$y = 1 + x - x^2 : \sigma^2 = 1$$

$$BIC = n \ln \left\{ \sum_{i=1}^n [y_i - \hat{y}(x_i)]^2 / n \right\} - p [\ln(n/2\pi)]$$

m	3	4	5	6	7	8	9
AIC	0	6.705	0.120	0.078	0.044	0.030	0.023
BIC	0	0.841	0.080	0.046	0.019	0.009	0.005

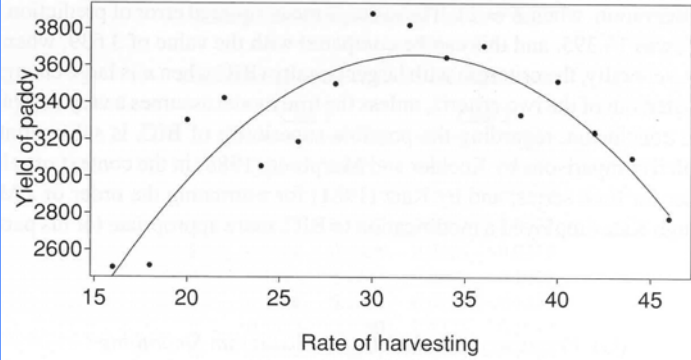


Figure 1.2.8. Fitting a quadratic regression curve.

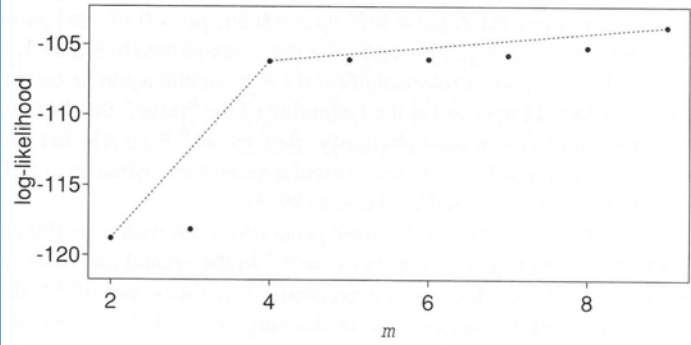


Figure 1.2.9. Log-likelihood plot for polynomial regression.

Principal component analysis

Example: stress rotation

$$\begin{bmatrix} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{bmatrix} = R^T(\theta, \phi) \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} R(\theta, \phi)$$

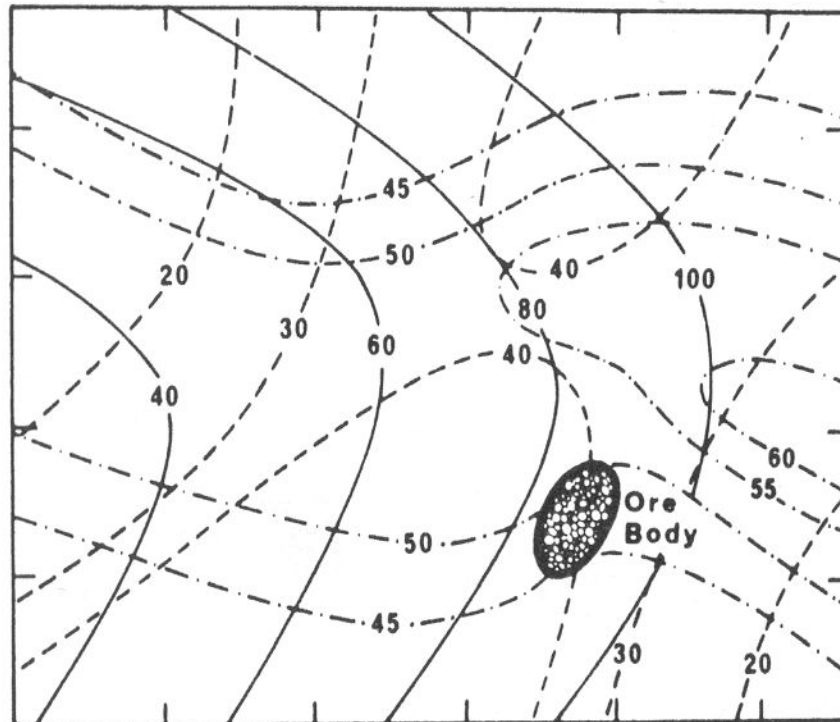
$$\sigma_1 \geq \sigma_2 \geq \sigma_3$$

Second Example: mineral prospecting

Table 1.1. The raw data matrix for the lead-zinc prospecting problem

				Geological properties										
				Mg in calcite	Fe in sphalerite	Na in muscovite	Sulfide	Crystal size of carbonates	Spacing of cleavage	Elongation of ooliths	Tightness of folds	Vein material per m ²	Fractures per m ²	
Causes				<i>T</i>	0.95	0.75	0.75	0.33	-0.20	0.05	0.20	0.10	0.00	0.05
				<i>D</i>	0.00	0.10	0.20	0.33	0.60	0.95	0.70	0.85	0.10	0.25
				<i>P</i>	0.05	0.15	0.05	0.34	0.60	0.00	0.10	0.05	0.90	0.70
Local-ity	<i>T</i>	<i>D</i>	<i>P</i>	Data matrix										
1	121	21	46	117.25	99.75	97.25	62.50	16.00	26.00	43.50	32.25	43.50	43.50	
2	96	35	42	93.30	81.80	81.10	57.51	27.00	38.05	47.90	41.45	41.30	42.95	
3	78	54	49	76.55	71.25	71.75	60.22	46.20	55.20	58.30	56.15	49.50	51.70	
4	63	51	49	62.30	59.70	59.90	54.28	47.40	51.60	53.20	52.10	49.20	50.20	
5	42	44	44	42.10	42.50	42.50	43.34	44.40	43.90	43.60	43.80	44.00	43.90	
6	39	26	54	39.75	39.95	37.15	39.81	40.20	26.65	31.40	28.70	51.20	46.25	
7	52	36	52	52.00	50.40	48.80	46.72	42.40	36.80	40.80	38.40	50.40	48.00	
8	67	46	54	66.35	62.95	62.15	55.65	46.60	47.05	51.00	48.50	53.20	52.65	
9	90	37	51	88.05	78.85	77.45	59.25	34.80	39.65	49.00	43.00	49.60	49.45	
10	108	27	61	105.65	92.85	89.45	65.29	31.20	31.05	46.60	36.80	57.60	54.85	
11	112	33	59	109.35	96.15	93.55	67.91	32.80	36.95	51.40	42.20	56.40	55.15	
12	91	38	59	89.40	80.90	78.80	62.63	40.00	40.65	50.70	44.35	56.90	55.35	
13	76	39	54	74.90	69.00	67.50	56.31	40.60	40.85	47.90	43.45	52.50	51.35	
14	63	30	51	62.40	57.90	55.80	48.03	36.00	31.65	38.70	34.35	48.90	46.35	
15	43	19	55	43.60	42.40	38.80	39.16	35.80	20.20	27.40	23.20	51.40	45.40	
16	68	16	42	66.70	58.90	56.30	42.00	21.20	18.60	29.00	22.50	39.40	36.80	
17	77	27	41	75.20	66.60	65.20	48.26	25.40	29.50	38.40	32.70	39.60	39.30	
18	93	37	43	90.50	79.90	79.30	57.52	29.40	39.80	48.80	42.90	42.40	44.00	
19	102	47	48	99.30	88.40	88.30	65.49	36.60	49.75	58.10	52.55	47.90	50.45	
20	120	36	46	116.30	100.50	99.50	67.12	25.20	40.20	53.80	44.90	45.00	47.20	

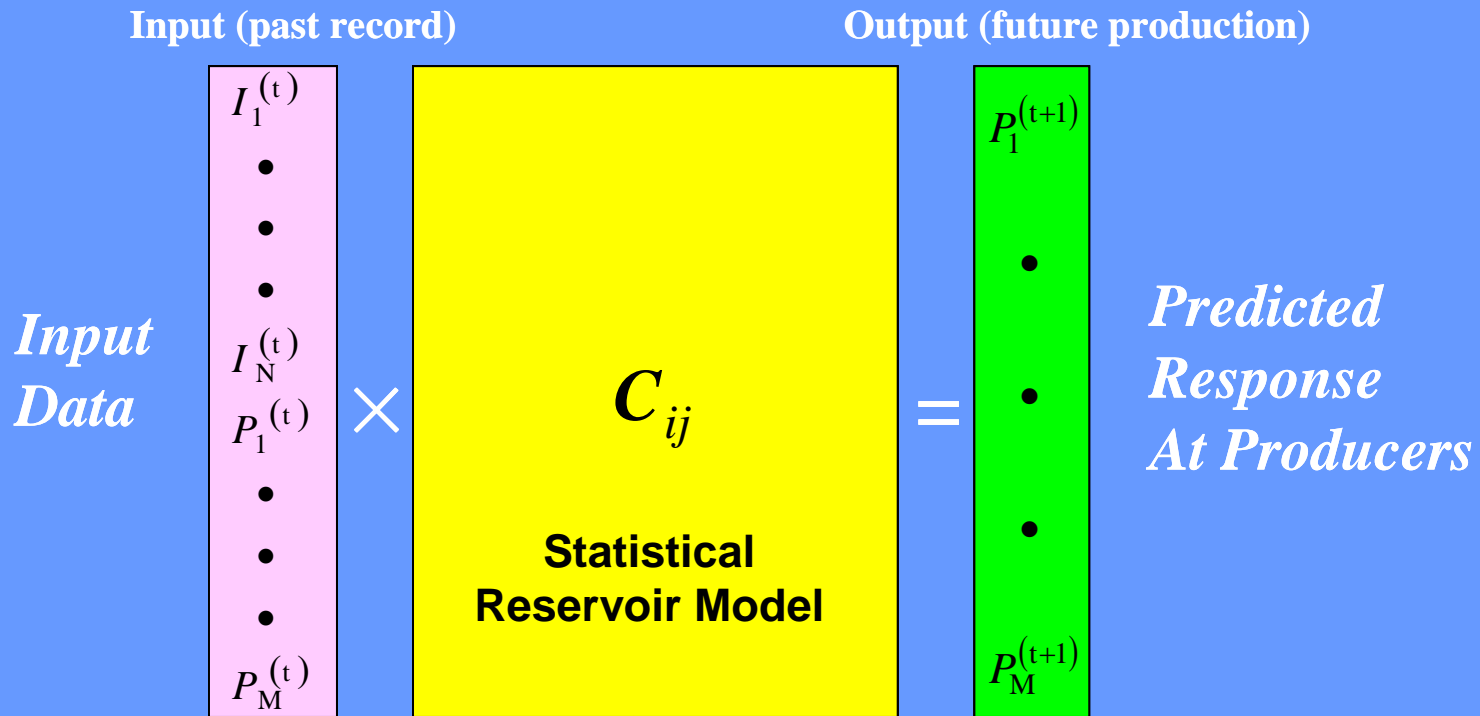
Map of first three principal components



- DISTRIBUTION OF PALEOTEMPERATURES
- · - · - DISTRIBUTION OF PERMEABILITY
- - - - DISTRIBUTION OF DEFORMATION

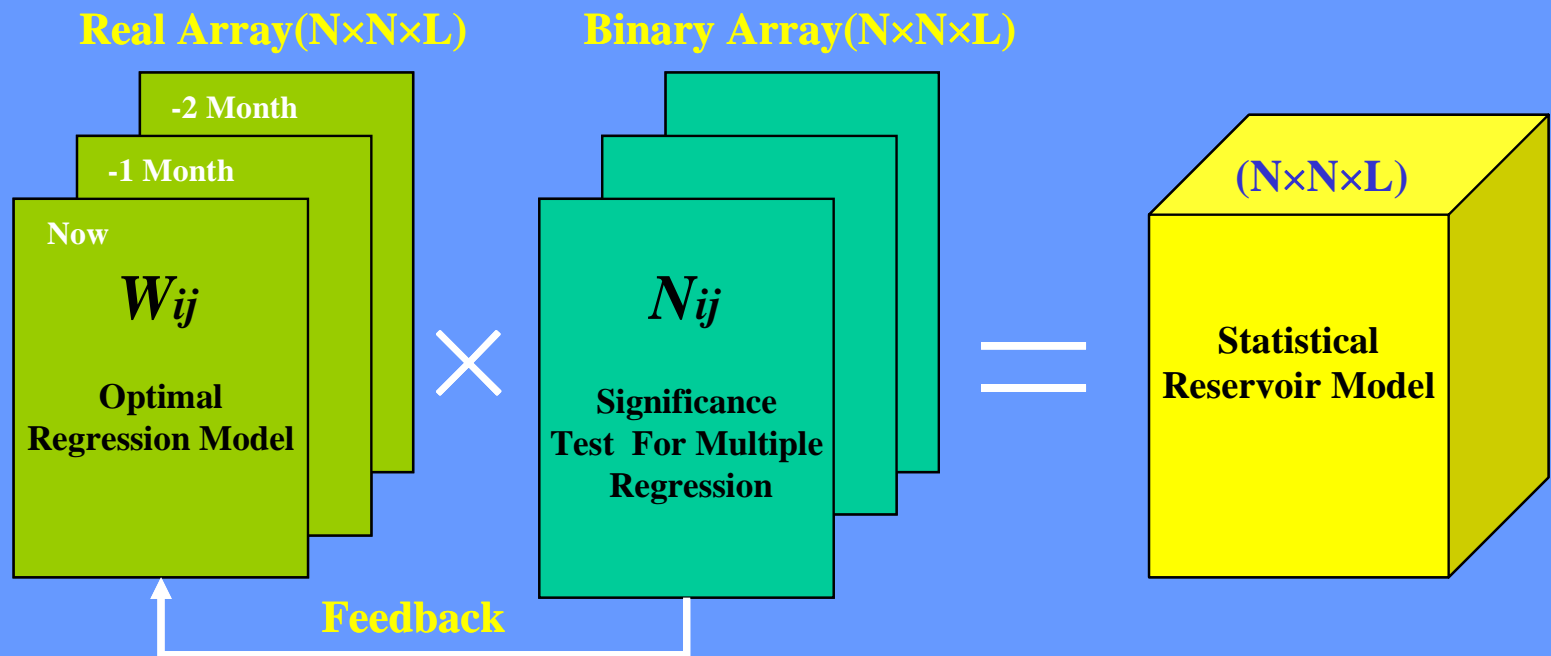
Figure 1.2. Distribution of controls imposed at the locations of the samples.

The statistical Reservoir Model



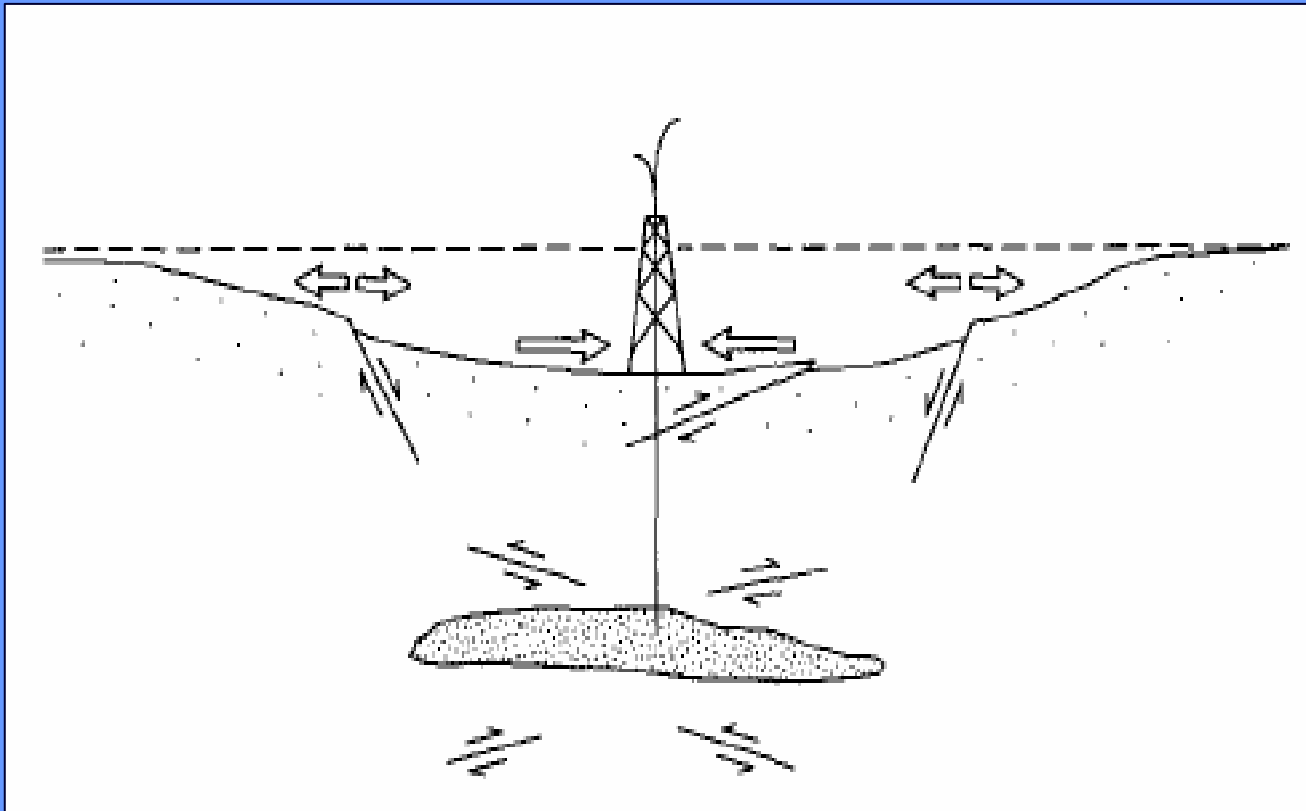
How the reservoir responds

Separating signal from noise: a parsimonious model



UK patent application 0524134.4 filed 26/11/2005

Geo-mechanical model: long-range poro-elasticity



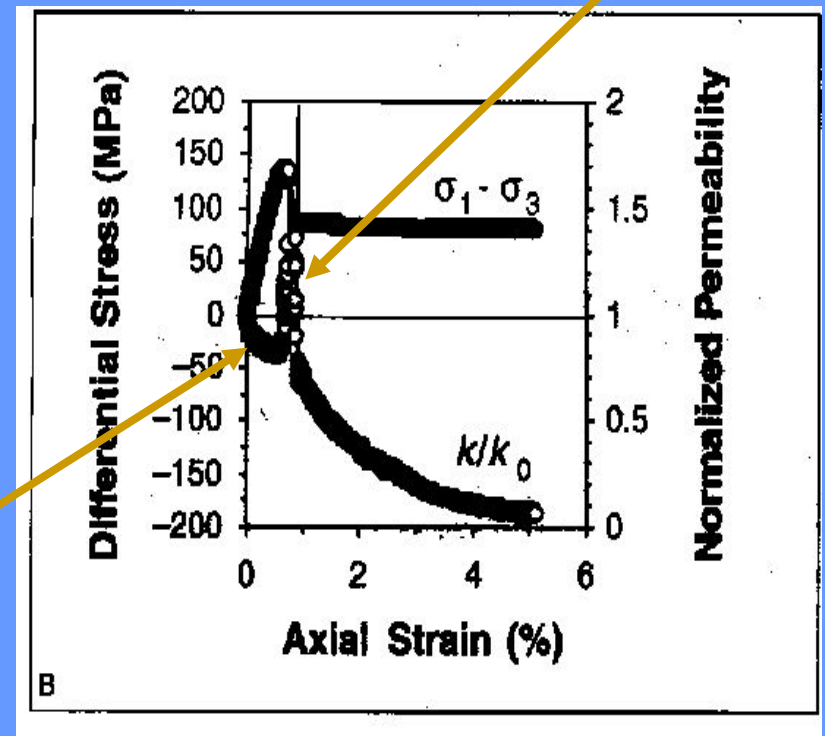
Deformation and faulting associated with fluid extraction (Segall, 1989)

Geo-mechanical model: Permeability response to deformation

Non-linear,
near critical

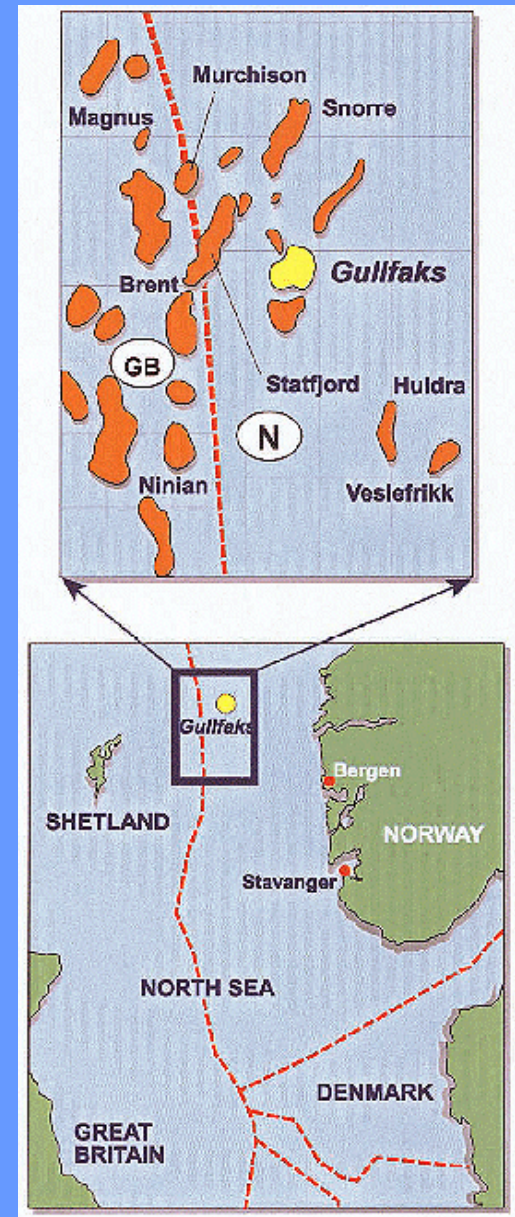


Linear

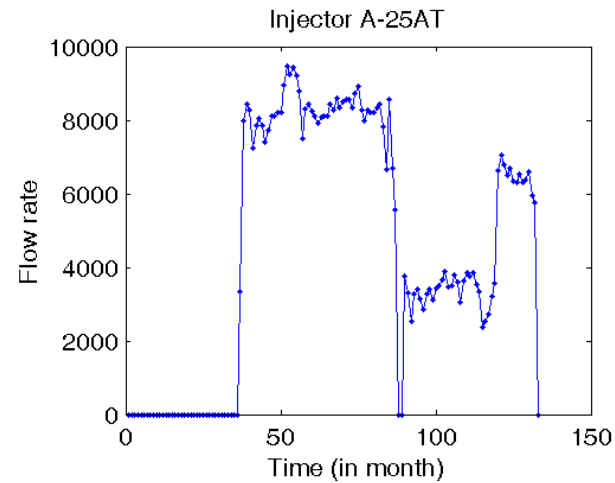
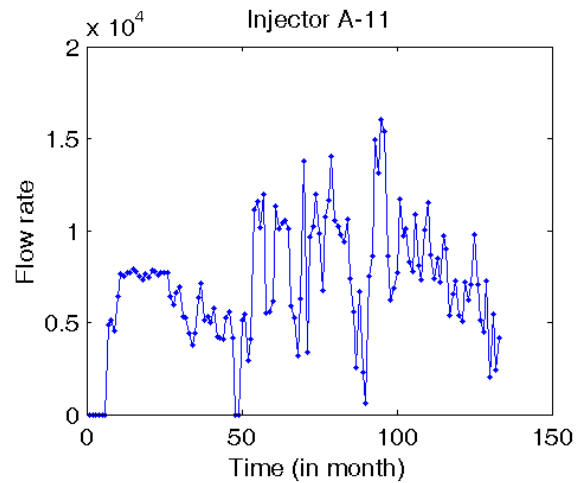
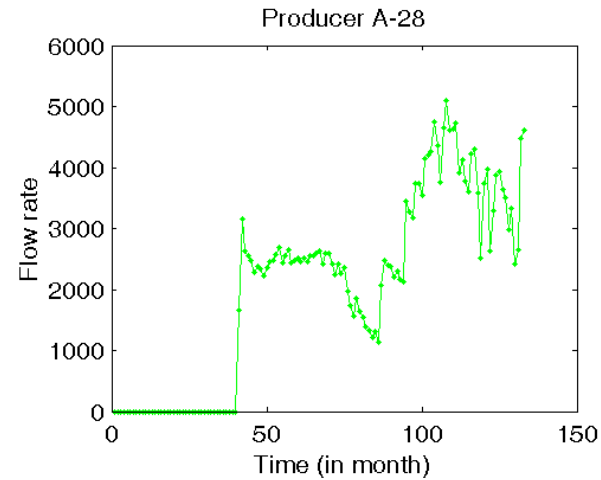
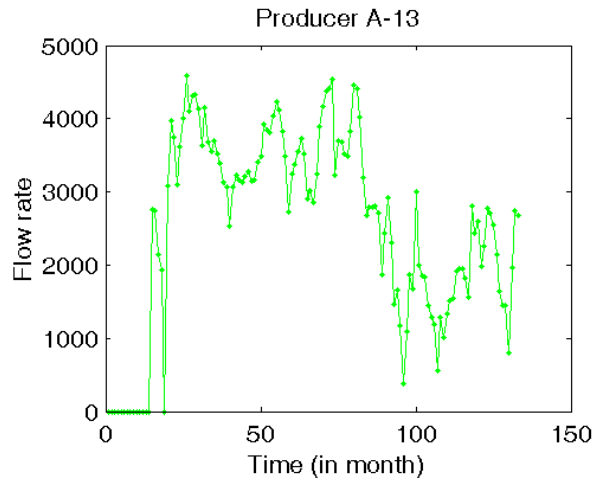


Test case: The Gullfaks field (after Arild Hesjedal)

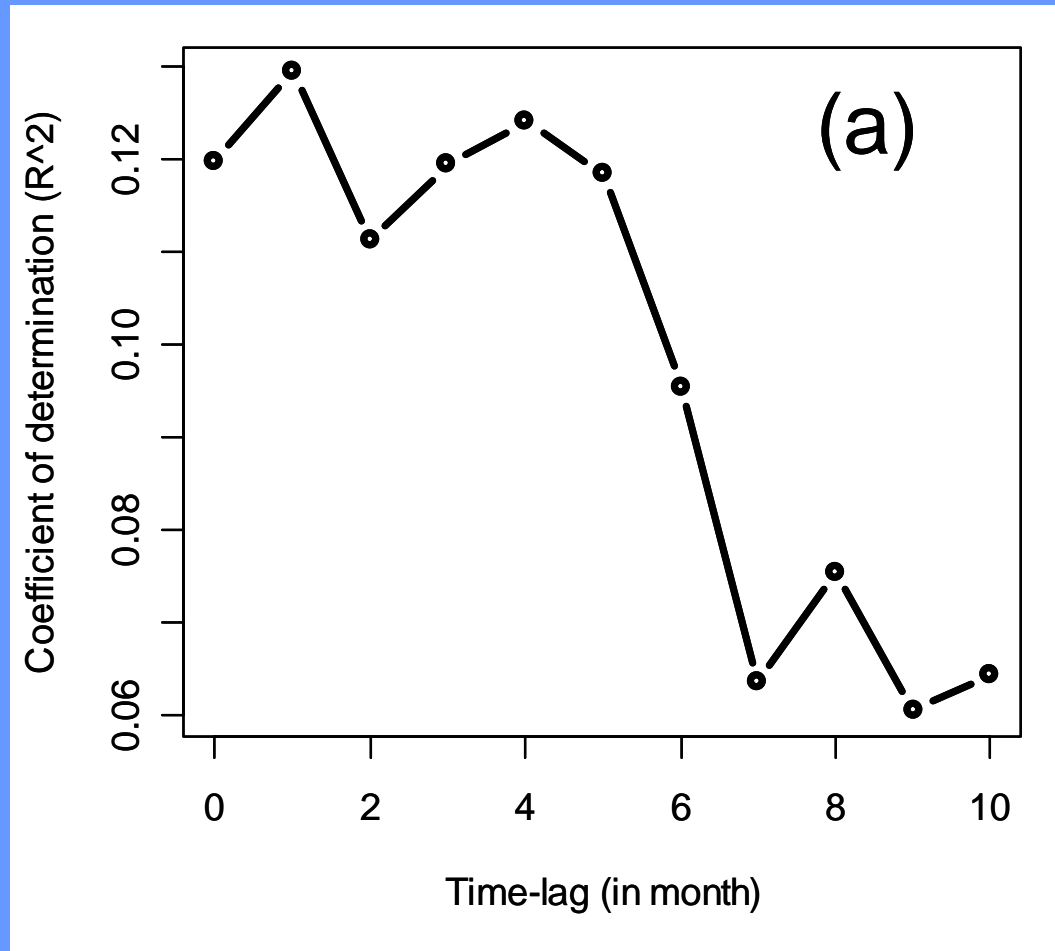
- Complex, faulted reservoir
- In block 34/10 in the northern part of the Norwegian North Sea.
- Total of 133 months data 1986-1997
- 106 platform wells (79 producers +27 injectors >24 months) used
- Data provided free for academic use



Time series for flow rate

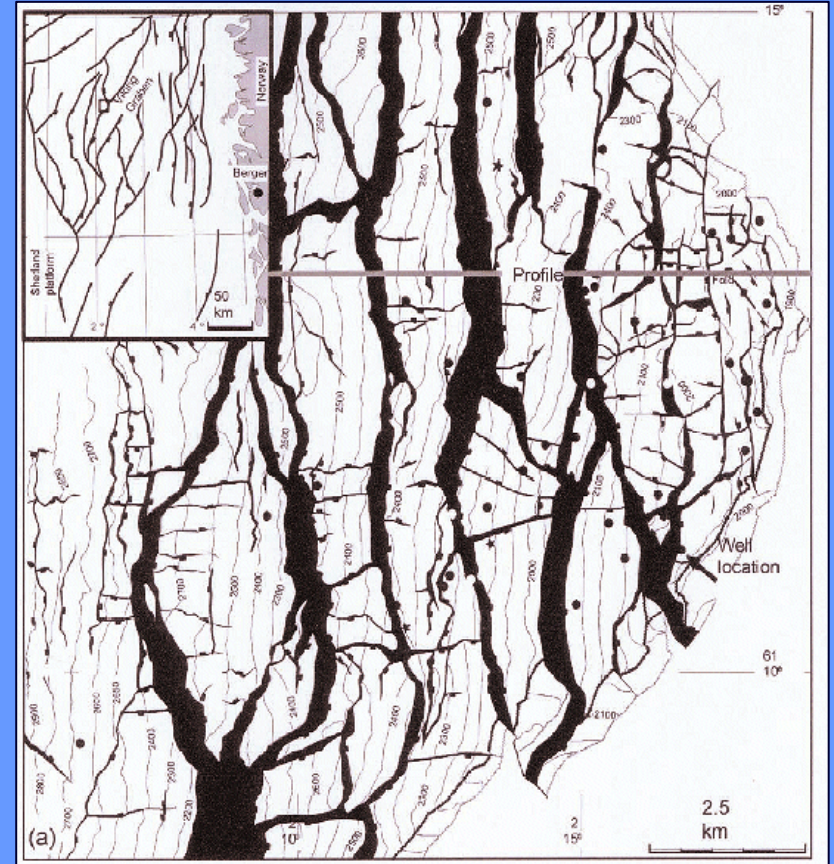
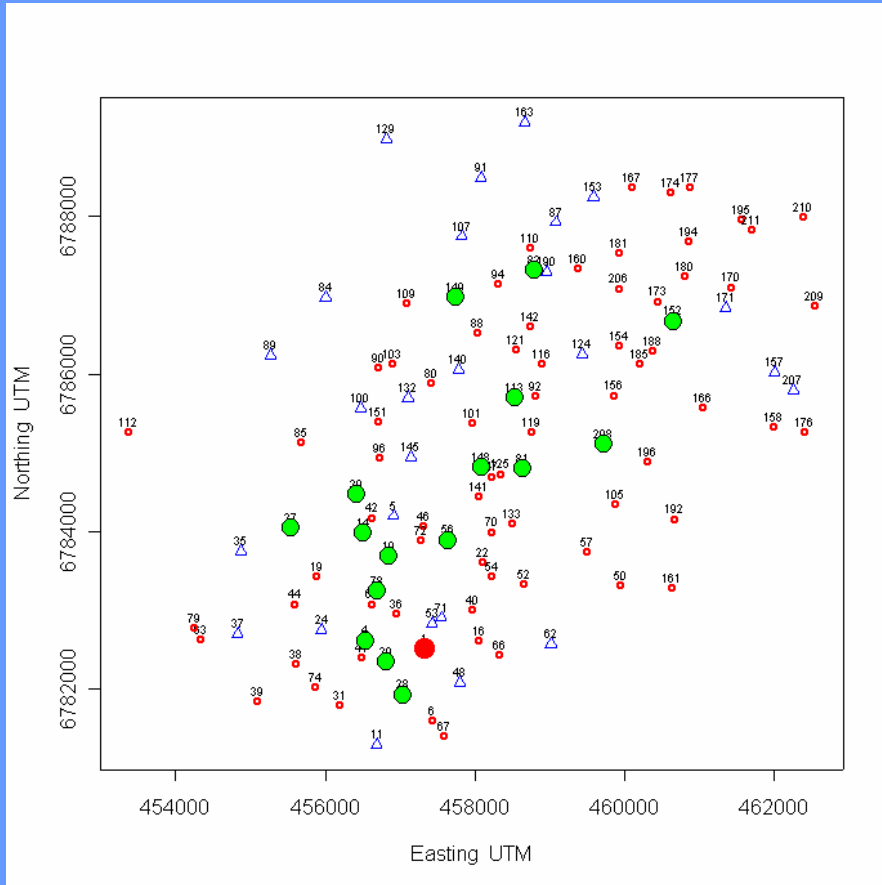


Cross-correlation function



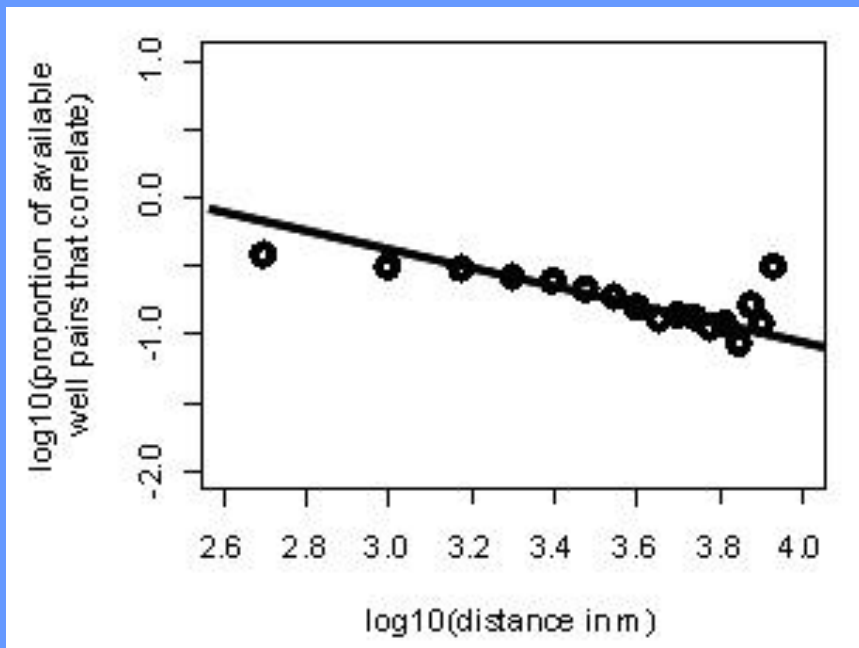
‘Direct’ and time-delayed effects seen over a few months

Significantly correlated wells

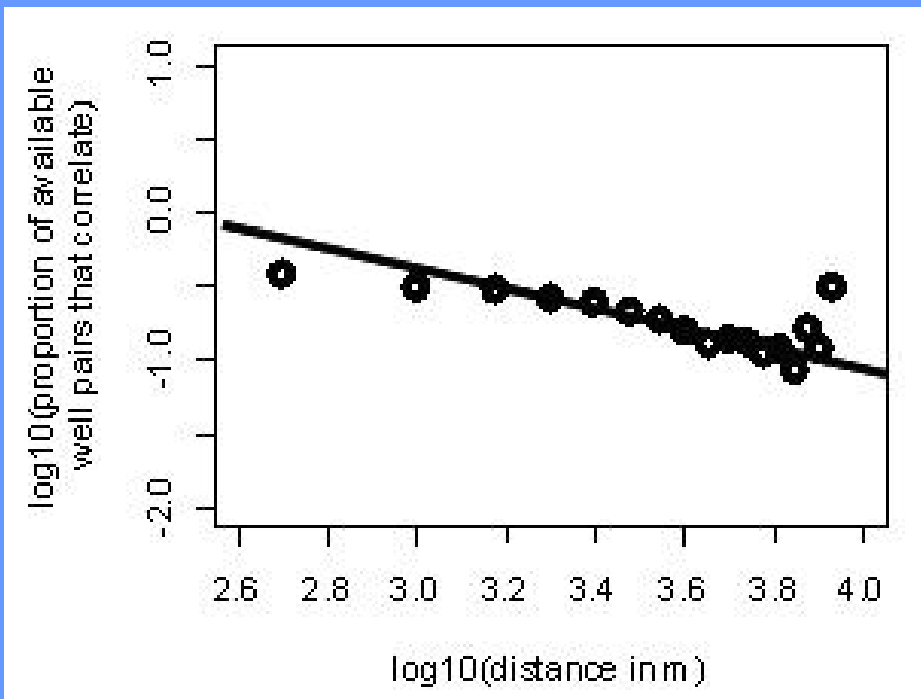


Fault map of the Gullfaks Field (*Fossen et al., 1998*).

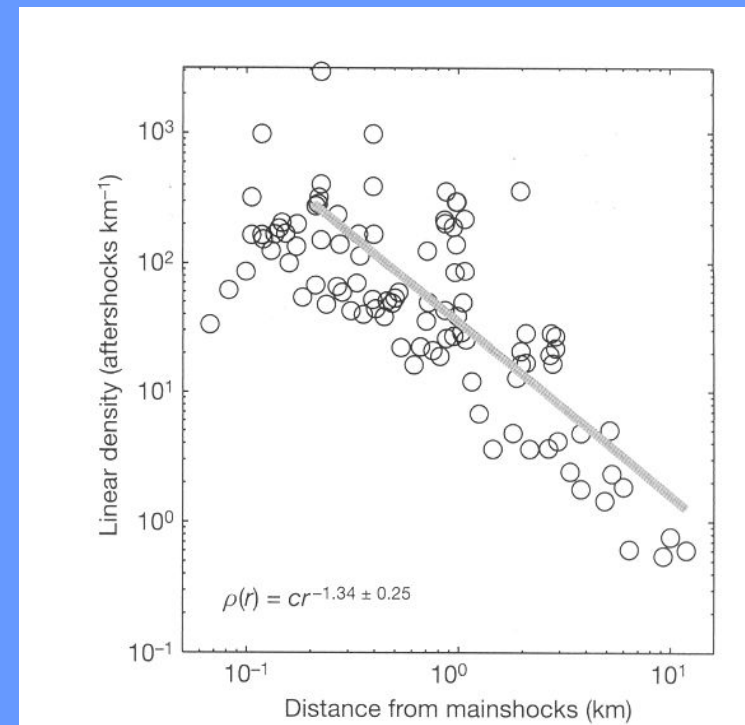
Correlation function for significantly correlated wells



Correlation function for significantly correlated wells

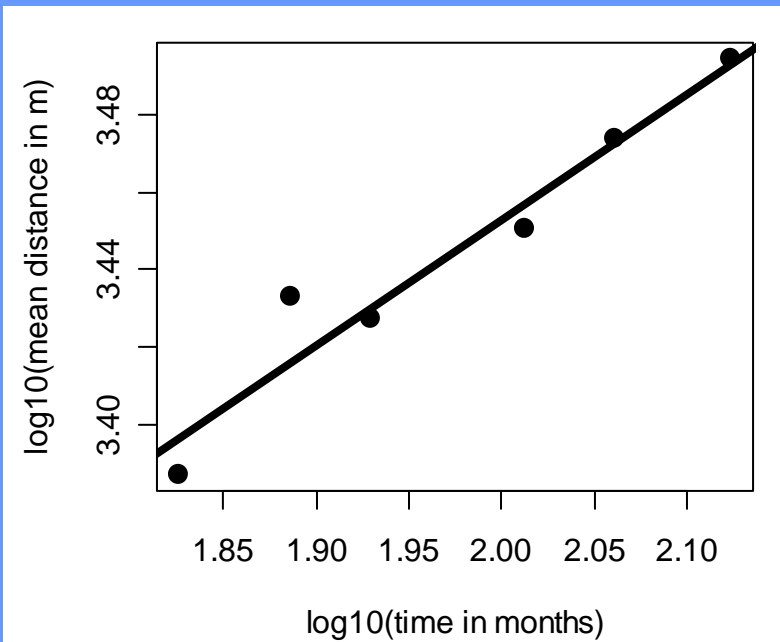


Flow rate correlations



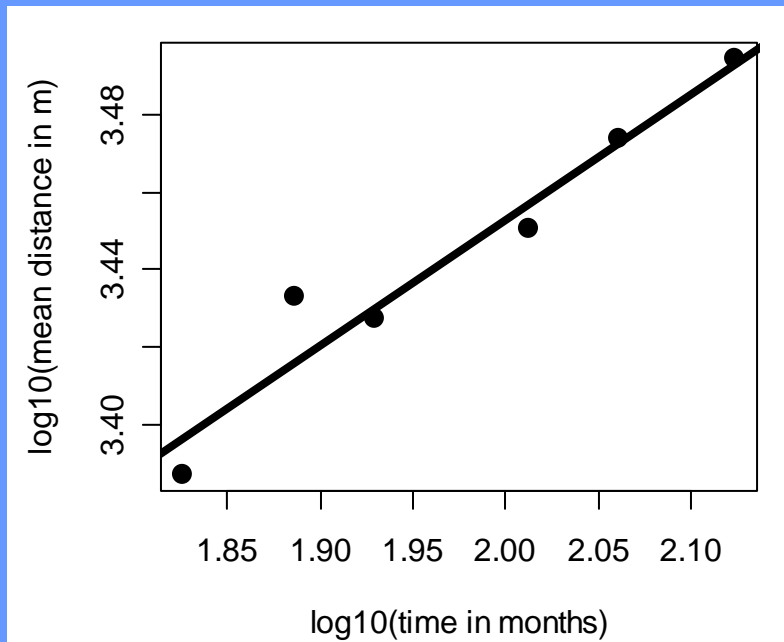
Earthquake aftershocks
(Felzer & Brodsky, 2006)

Anomalous (slow) diffusion

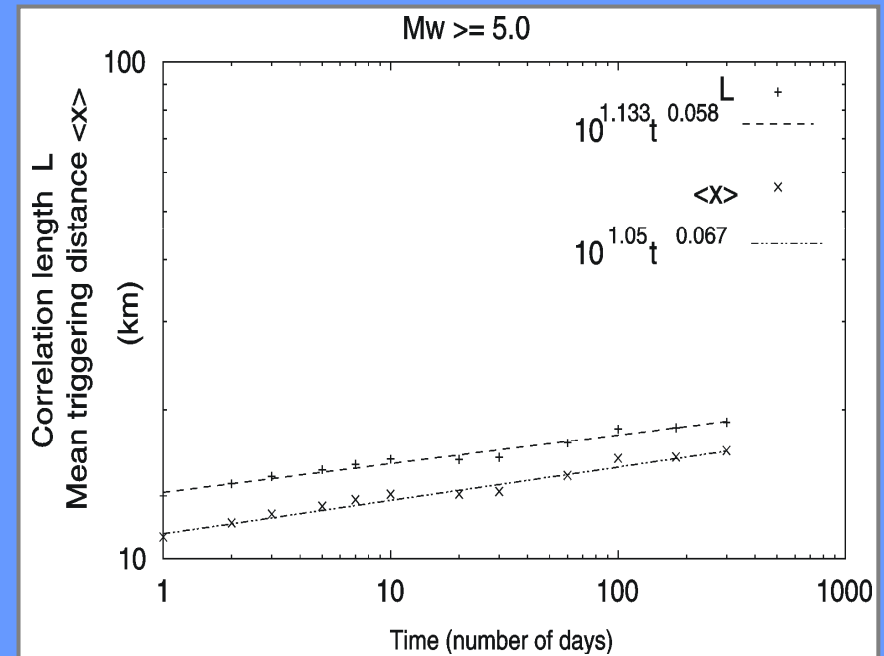


$\langle x \rangle \sim t^{0.3}$ for significantly correlated well pairs

Anomalous (slow) diffusion

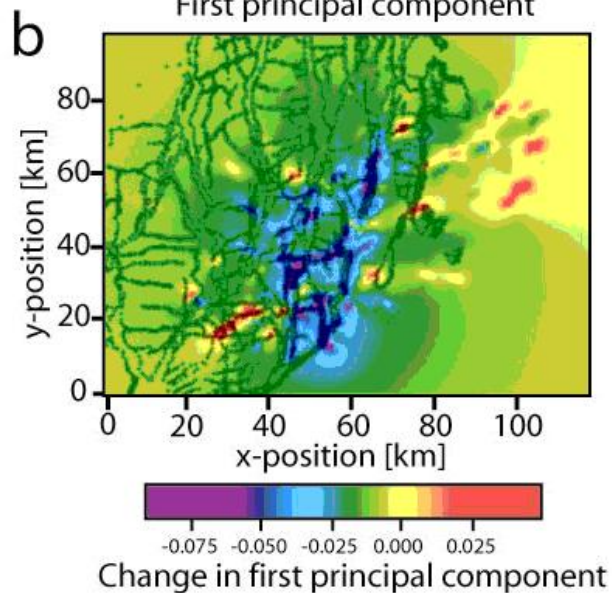
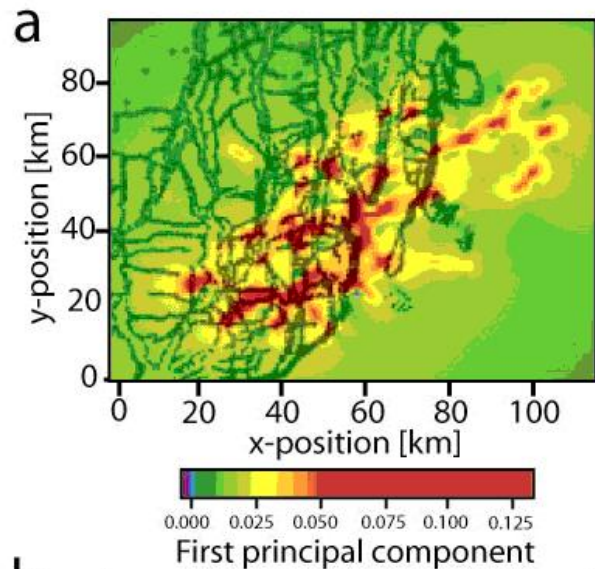
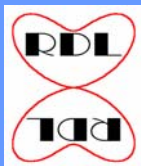


$\langle x \rangle \sim t^{0.3}$ for significantly correlated well pairs

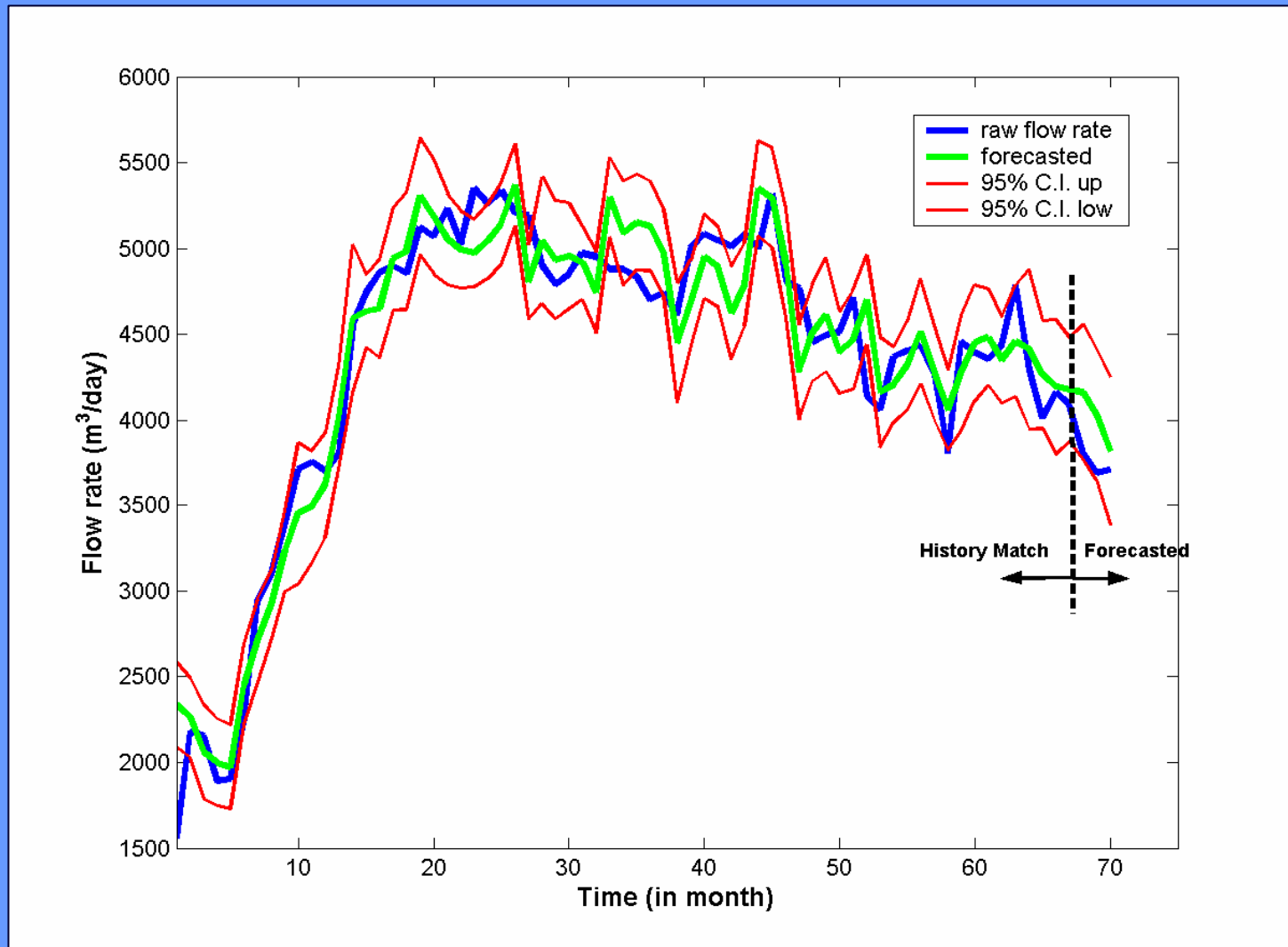


$\langle x \rangle \sim t^{0.07}$ for earthquakes ($M_w \geq 5.0$)
(Huc & Main, 2003)

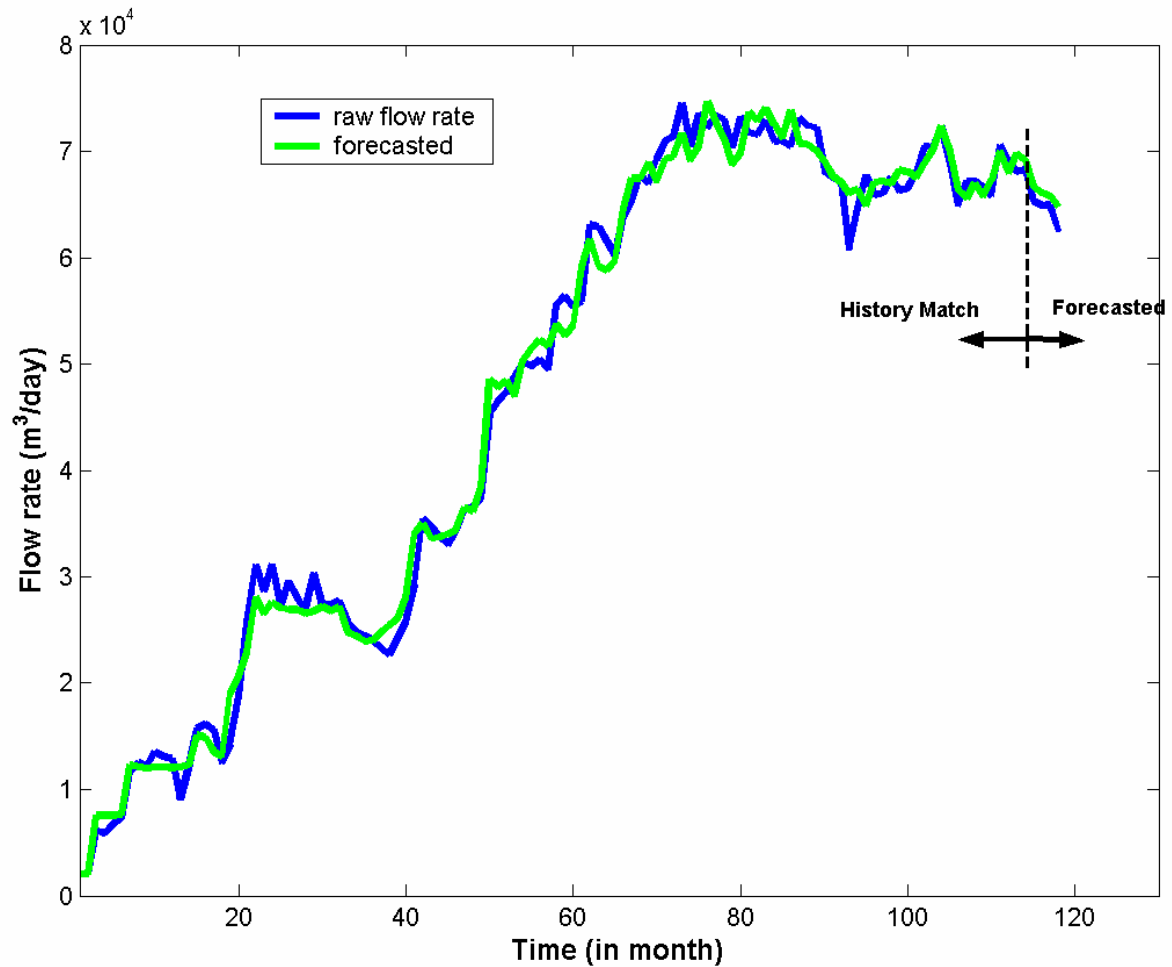
Principal component analysis



Predictive trial for a single well



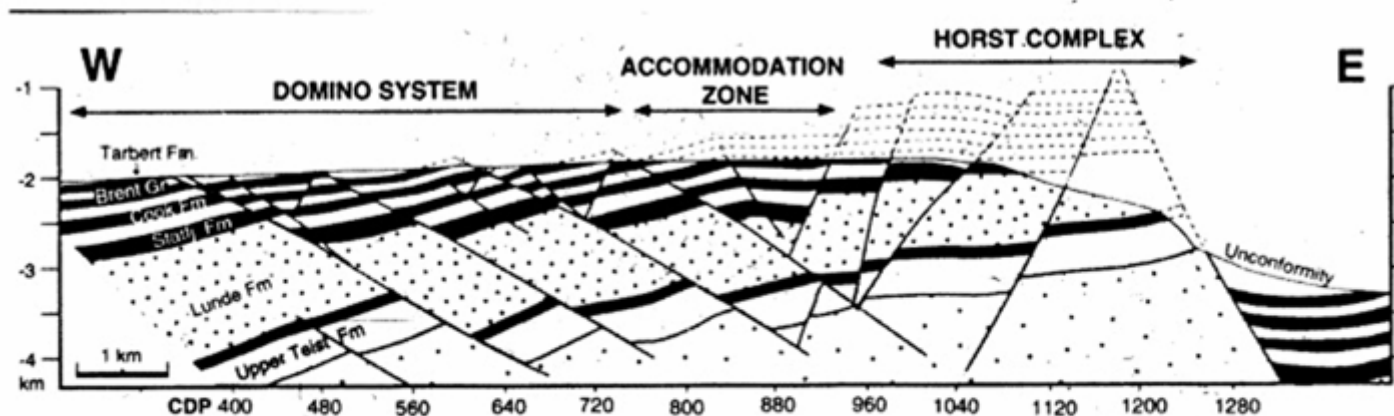
Predictive trial for a group of wells



Note good
statistical
averaging

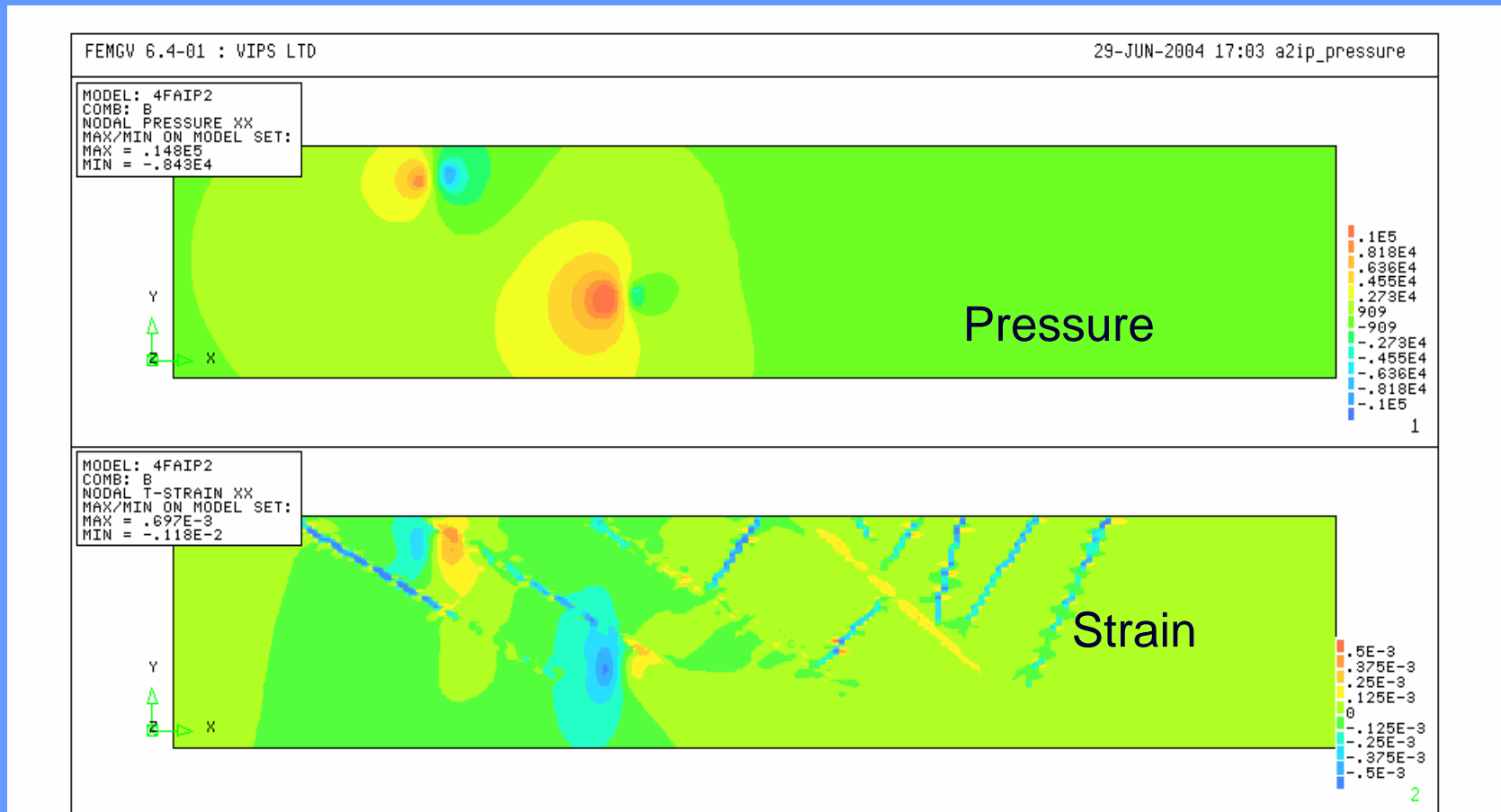
Geo-mechanical model: Reservoir architecture

Cross-section through Gullfaks



Fossen & Hesthammer (1998) 2D cross section

Geo-mechanical simulation (2D model in cross section)



Pressure change and volumetric strain: critical case

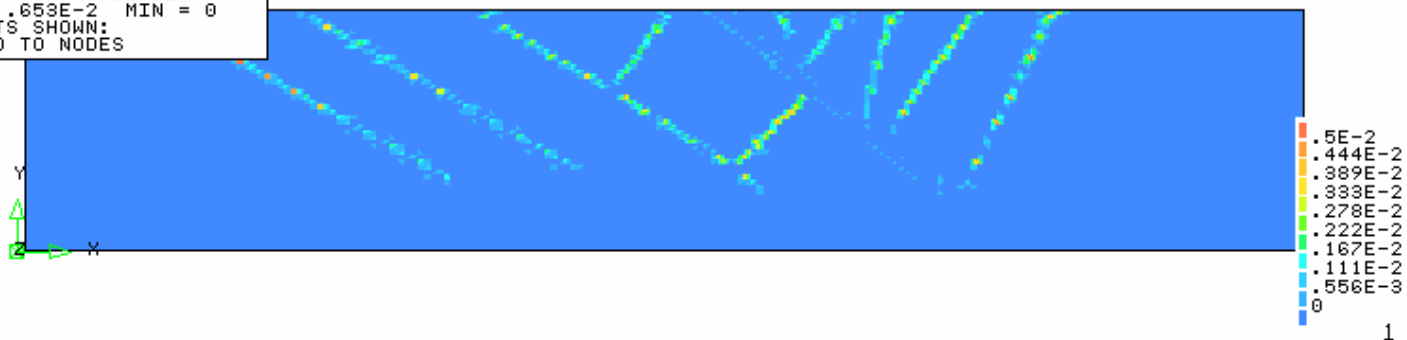
Geo-mechanical simulation

FEMGW 6.4-01 : VIPS LTD

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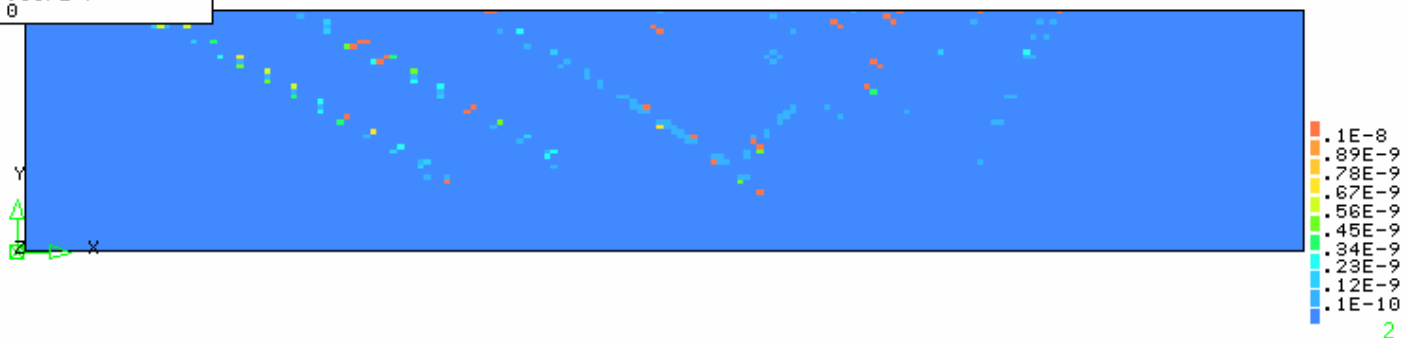
MODEL: 4FAIP2
COMB: B
GAUSS PRINC SHEAR MAX
CALCULATED FROM: TPSTRAIN
MAX/MIN ON MODEL SET:
MAX = .653E-2 MIN = 0
RESULTS SHOWN:
MAPPED TO NODES

Shear strain changes



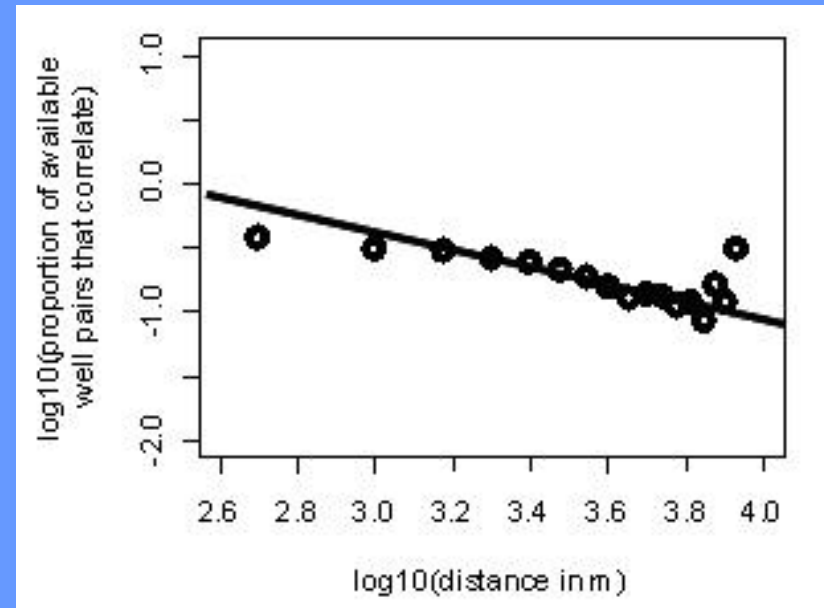
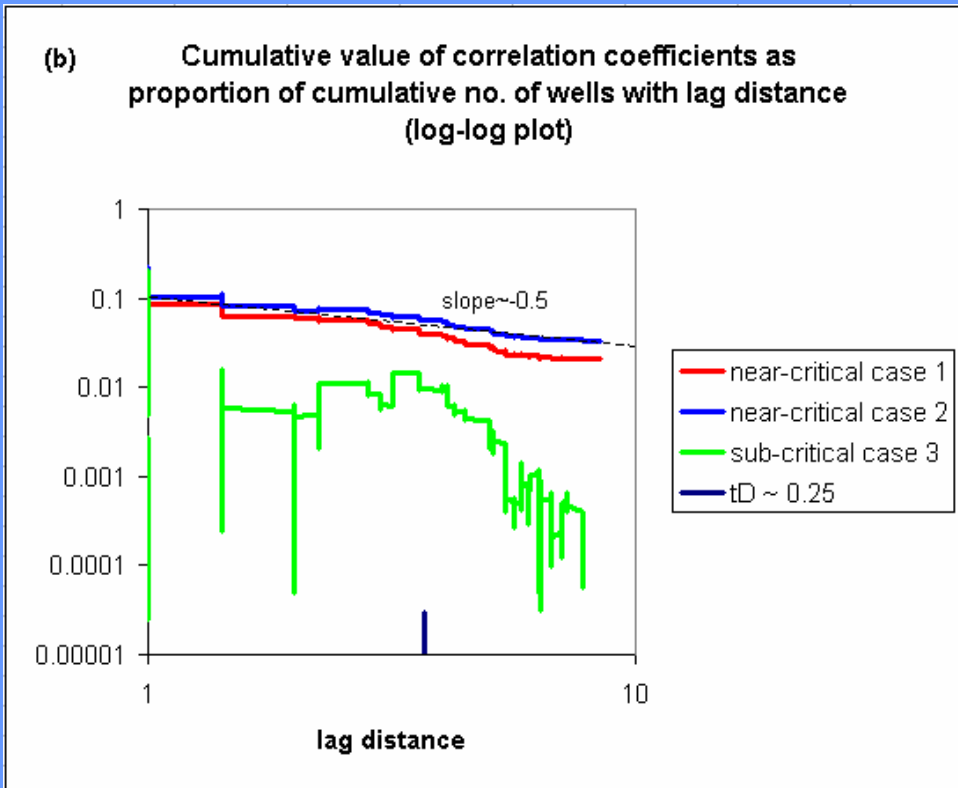
MODEL: 4FAIP2
COMB: B
INVARIANT PERMIJ K11
MAX/MIN ON MODEL SET:
MAX = .107E-7
MIN = 0

Permeability changes



Geo-mechanical simulation






(2D model in plan view for a synthetic regular grid of wells)



c.f. data from Gullfaks

Schlumberger

Conclusion

-  Oilfield flow rate correlations behave very similarly to earthquake-earthquake triggering
-  The results agree with deterministic geo-mechanical simulations *iff* the system is critical
-  The first principal component agrees with fault architecture
-  Good short-term predictability
-  Many potential applications

Next steps...

- Further field trials (DTI 'RESURGE' project)
- more data welcome
- Calibration and interpretation of principal components
- Compare with induced seismicity response (independent validation of geo-mechanical simulations)
- Apply to earthquake-earthquake triggering (EU 'TRIGS' network)