

## Improved thermoelectrical properties of Bi-M-Co-O (M=Sr, Ca) misfit compounds by laser directional solidification

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### ABSTRACT

In this work it is reported the improvement of the thermoelectrical properties of bulk samples of composition  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$  and  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$ , when they are properly textured by a directional solidification process, assisted by laser (laser floating zone melting method). Samples composition and microstructure aspects have been studied using X-ray diffraction and scanning electron microscopy. Thermoelectric properties have been measured between 4 and 300K by the simultaneous determination of the electrical resistivity and the thermopower. All the textured samples show a remarkable increase of the power factor values, as compared to the conventional sintered ceramics.

Keywords: thermoelectric oxides, misfit cobaltites, thermoelectric properties, directional solidification, laser floating zone

## INTRODUCTION

In response to escalating energy crisis and related pollution problems, we urgently need to adopt new technologies that utilize energy sources in a more efficient and environmentally friendly manner. Thermoelectric power generation has been recognized as one of the innovative and promising energy conservation and environmentally friendly technologies.<sup>1</sup> It allows converting a thermal gradient originated, for example, in exhaust emissions, into an electrical energy output by the well known Seebeck effect. Between other advantages, thermoelectric generation is reliable, clean and silent. On the other hand, big efforts must be still done to obtain more efficient thermoelectric materials and devices.

Since the discovery of a large room temperature thermopower in  $\text{NaCo}_2\text{O}_4$ ,<sup>2</sup> other layered cobalt oxides, such as  $\text{Ca-Co-O}$ ,<sup>3</sup>  $\text{Bi-Ca-Co-O}$ ,<sup>4</sup> and  $\text{Bi-Sr-Co-O}$ ,<sup>5</sup> have attracted much attention. Their crystal structure is composed of an alternate stacking of a common conductive  $\text{CdI}_2$ -type  $\text{CoO}_2$  layer with a two-dimensional triangular lattice and a block layer, composed of insulating rock-salt-type (RS) layers.<sup>4,6,7</sup> This structure shows a high crystal anisotropy, which is reflected in both, thermoelectric properties as well as a preferential grain growth along the  $ab$  planes, matching up with the conductive ones.

The performance of a thermoelectric material is evaluated through a dimensionless parameter, the figure of merit ( $ZT=S^2T/\rho\kappa$ ). An easy way for raising this figure of merit is the use of materials with high working temperature. This can be performed by using thermoelectric ceramics, which possess the advantages of higher thermal stability at high temperature and lower toxicity when compared with conventional semiconducting compounds and alloys. In this context, those cobalt oxides seem to be an alternative for thermoelectric power generation devices.

Another way to raise the  $ZT$  values for these cobalt oxide families is the improvement of the grain orientation using different techniques. Some of them, involving solid state reactions, have been successfully applied in order to obtain well oriented grains, as hot forging<sup>8</sup> and template grain growth.<sup>9</sup> On the other hand, it is possible to get a

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4 good grain orientation by directional growth from the molten material, as it can be  
5 performed by a directional solidification from the melt, induced by laser.<sup>10</sup>  
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9 In this paper, we report the main microstructural and thermoelectrical results obtained  
10 on  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$  and  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  misfit cobaltites textured by a directional  
11 solidification process assisted by laser in the same conditions.  
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## 17 **EXPERIMENTAL**

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20  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  and  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$  polycrystalline samples were prepared by the  
21 conventional solid state route using commercial  $\text{Bi}_2\text{O}_3$  (Panreac, 98 + %),  $\text{CaCO}_3$   
22 (Panreac, 98 + %),  $\text{SrCO}_3$  (Panreac, 98 + %), and  $\text{Co}_2\text{O}_3$  (Aldrich, 98 + %) powders  
23 as starting materials. They were weighed in the appropriate proportions, mixed and  
24 ball milled for 30 minutes at 300 rpm in an agate mortar. In order to assure the total  
25 decomposition of carbonates, the mixed powders were thermally treated twice at 750  
26 and 800°C for 12h under air, with an intermediate manual milling. This thermal  
27 treatment is of the main importance, as it has been designed to decompose the  
28 calcium and strontium carbonates, avoiding their presence in the Laser Floating Zone  
29 (LFZ) process. Otherwise they would decompose in the melting process, leading to  
30 bubble formation inside the liquid phase and, more important, disturbing the  
31 crystallization front. The so obtained powders were then isostatically pressed at 200  
32 MPa for 1 minute in order to obtain green cylindrical ceramic bars, which were  
33 subsequently used as feed in a LFZ device equipped with a continuous power  
34 Nd:YAG solid state laser (1.06  $\mu\text{m}$ ) and described elsewhere.<sup>11</sup>  
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49 The texturing processes have been performed downwards with a growth speed of 30  
50 mm/h. In order to assure the compositional homogeneity of the molten zone and  
51 maintaining constant the textured rod diameter, the feed has been rotated at 15 rpm.  
52 The use of this relatively high crystallization rate implies that the growth process is  
53 not produced in a totally equilibrium condition. For this reason, the obtained textured  
54 cylinders are formed by the most stable phase, but also accompanied by other  
55 phases (secondary phases). In spite of that multiphasic composition, the LFZ process  
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4 produces long (more than 20 cm) textured cylinders have been obtained, with c.a. 2  
5 mm diameter. These bars were finally cut to obtain samples having the adequate  
6 dimensions for their characterization.  
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10 Powder X-ray diffraction (XRD) patterns have been systematically recorded in order  
11 to identify the different phases in the thermoelectric textured materials. Data have  
12 been collected at room temperature, with  $2\theta$  ranging between 10 and 40 degrees,  
13 using a Siemens Kristalloflex diffractometer working with  $K\alpha$  Cu radiation.  
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18 Microstructures have been observed by scanning electron microscopy JEOL 6000  
19 equipped with an energy dispersive spectroscopy (EDS) device used for phase  
20 identification. On the one hand, micrographs of longitudinal fractured sections have  
21 been recorded to observe the grain orientation. Longitudinal and transversal polished  
22 sections of the samples have been observed to analyze the different phases.  
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28 Electrical resistivity measurements were performed longitudinally on textured  
29 cylinders using the standard dc four-probe technique at temperatures between 5 and  
30 400K, with no applied external field, in a Physical Properties Measurement System  
31 (PPMS) from Quantum Design. Thermopower (TEP or S) measurements were  
32 performed at temperatures between 5 and 300K in an experimental setup described  
33 elsewhere.<sup>12</sup> With the electrical resistivity and thermopower data, the power factor  
34 (PF) has been calculated ( $PF = S^2/\rho$ ) in order to determine the samples  
35 thermoelectric performances.  
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## 47 **RESULTS AND DICUSSION**

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49 XRD has confirmed that the cobaltite phase is the major one, independently of the  
50 composition, showing very intense peaks for the (002l) planes. These diffractions  
51 indicate that the cobaltite grains have a plate-like shape, with preferential growth  
52 along the ab plane. This growth habit is clearly confirmed with the micrograph  
53 displayed in Fig. 1, showing a representative fractured longitudinal section of a  
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4 textured sample. In this figure, it is possible to observe that grain lengths in the ab  
5 plane can easily exceed 100  $\mu\text{m}$ .  
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9 The polished longitudinal surfaces of the textured bars are shown in Fig. 2, for the  
10 different compositions, where Fig. 2a corresponds to the  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  sample and  
11 Fig. 2b to  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$ . In a first sight, it is clear that the second one is formed by  
12 bigger and better oriented grains than the first one. When this figure is analysed more  
13 in detail, it is possible to find some more differences between the two compositions.  
14 In Fig. 2a, it is possible to distinguish three main different contrasts. A black contrast,  
15 with a relatively small size, compared with the other phases, showing a dendritic-like  
16 structure, and identified as CoO through EDS analysis. The major phases are the  
17 gray ones, which appear with a preferential orientation along the growth direction,  
18 and stacked as alternate layers. Dark grey contrast has been associated to the  
19  $\text{Bi}_2\text{Ca}_2\text{Co}_2\text{O}_y$  cobaltite, while the light grey one is a non thermoelectric phase  
20 corresponding to the Bi-Ca-O solid solution. On the other hand, in Fig. 2b it can be  
21 observed four different contrasts. As it was indicated for the Ca-containing samples,  
22 black phase correspond to CoO and the white phase is identified as the Bi-Sr-O solid  
23 solution. Despite the presence of these secondary phases, the samples are mainly  
24 composed of highly textured Bi-Sr-Co-O grains alternatively stacked, with  
25 compositions  $\text{Bi}_2\text{Sr}_2\text{Co}_2\text{O}_y$  and  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.3}\text{O}_y$ , and corresponding to the dark and light  
26 grey contrasts, respectively. Moreover, the relative proportion of secondary phases is  
27 also reduced from the Ca-containing samples (about 35%) to the Sr ones (about  
28 10%), measured as the relative areas of the different phases obtained from SEM  
29 micrographs.  
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48 The temperature (T) dependence of the resistivity ( $\rho$ ) of the textured materials, as a  
49 function of the composition, is shown in Fig. 3. As it can be easily seen, the  $\rho(T)$   
50 curves exhibit a semiconductor-like behaviour from low to high temperature,  
51 characterised by a  $d\rho/dT < 0$ , independently of the nominal composition. This  
52 semiconducting behaviour is in agreement with earlier reports on these cobaltite  
53 systems.<sup>7,13</sup> The resistivity values decrease from the Ca-containing samples (about  
54 91  $\text{m}\Omega\text{ cm}$  at RT) to the Sr ones (about 24  $\text{m}\Omega\text{ cm}$  at RT), which are very similar to  
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4 the values reported in the literature for these type of materials. These apparently  
5 contradictory results for these highly textured materials can be associated to the  
6 presence of secondary phases (normally not present in adequately sintered  
7 materials), and to a different oxygen content compared to the sintered specimens. On  
8 the other hand, a more detailed observation of the graph shows a slight deviation  
9 from that behaviour for the Sr-containing samples, between 150 and 250K, where a  
10 change on the sign of  $d\rho/dT$  is produced, which is in agreement with a more metallic-  
11 like behaviour, as it has been previously reported, as a function of the size of the  
12 alkaline-earth cation.<sup>14,15</sup> In both cases the samples show a three dimensional Mott  
13 variable range hopping (VRH),  $\ln \rho \propto T^{-1/4}$  in the low temperature range.  
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23 Fig. 4 shows the variation of the thermopower with the temperature as a function of  
24 the nominal composition. The sign of the thermopower is positive for the entire  
25 measured temperature range, which confirms a mechanism involving holes  
26 conduction. The values of the thermopower increase with the temperature, with very  
27 similar behaviour in both cases. In the low temperature range (until about 150K), a  
28 good agreement with  $S \propto T^{1/2}$ , which is also described by the three dimensional Mott  
29 VRH conduction mechanism. From 150K to room temperature, the S values remain  
30 practically constant, as previously reported in this cobaltite family.<sup>16</sup> This more  
31 metallic behaviour found for the Sr-containing samples, displayed in resistivity  
32 measurements, is confirmed by the lower thermopower values in the plateau-like  
33 region. At room temperature, the S values for both samples are about 205  $\mu\text{V/K}$  for  
34 the Ca samples and 130  $\mu\text{V/K}$  for the Sr ones, which are higher than those reported  
35 in the literature.<sup>6</sup> The high value of the thermopower obtained for these textured bulk  
36 materials, prepared by the Laser Floating Zone Melting method, is not common in  
37 this system but we can assume that the LFZ growth can probably generate oxygen  
38 vacancies in larger content than in bulk samples synthesized in a classic solid state  
39 reaction. This reduction on the oxygen content has been confirmed by  
40 thermogravimetical measurements and estimated in around 1-2 wt.%. As a  
41 consequence, the carriers concentration (holes) is decreased due to the reduction of  
42 the  $\text{Co}^{+4}$  to  $\text{Co}^{+3}$  and an increase on the TEP is produced.<sup>15</sup> It has already been  
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4 evidenced that, in reduced conditions, the misfit phase  $[\text{Ca}_2\text{CoO}_3][\text{CoO}_2]_{1.62}$  is not  
5 oxygen stoichiometric but contains considerable amounts of oxygen vacancies.<sup>17</sup>  
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9 In order to evaluate the thermoelectric performance of these materials, the power  
10 factor,  $S^2/\rho$ , has been calculated. The temperature and composition dependences of  
11 the power factor (PF) are calculated from the data represented in Figs. 3 and 4, and  
12 displayed in Fig. 5. The variation of PF with temperature is similar for both  
13 compositions, reaching the maximum values at room temperature, about 0.05  
14  $\text{mW/K}^2\text{m}$  for the  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  samples, and 0.06  $\text{mW/K}^2\text{m}$  for the  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$   
15 ones, which are higher than the usual values for sintered specimens.  
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## 25 **CONCLUSIONS**

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27 Microstructural and thermoelectric characteristics of misfit cobaltites, with  
28 compositions  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$  and  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$ , directionally grown from the melt by  
29 the technique LFZ (laser floating zone) have been studied. The following conclusions  
30 can be drawn from the present study:  
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- 34 1. Bulk samples of these misfit cobaltites can be properly grown by the laser floating  
35 zone method (LFZ). Highly textured samples with homogeneous dimensions and  
36 phase distribution are obtained.  
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- 38 2. Larger and better oriented grains are obtained for the Sr-containing samples. In  
39 addition, the amount of secondary phases is lower for these samples.  
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- 41 3. Thermopower values are, in both cases, higher to those found in sintered  
42 ceramics. On the other hand, their values are in agreement with the evolution  
43 reported in the literature, taking into account the alkaline earth cation size.  
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- 45 4. Electrical resistivity values, in both types of cobaltites, are similar to those  
46 obtained for sintered bulk ceramics.  
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- 48 5. An important increase of the power factor (PF) has been obtained in all cases, as  
49 a result of raising the thermopower.  
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4 6. The use of the laser floating zone (LFZ) melting method seems to be a very useful  
5 and promising technique in order to obtain well textured bulk misfit cobaltites with  
6 improved thermoelectrical properties.  
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## 10 11 12 **ACKNOWLEDGEMENTS**

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4 **FIGURE CAPTIONS**  
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9 Fig. 1. SEM micrograph of a longitudinal fractured sample ( $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$ ), showing  
10 the typical orientation of the misfit platelike grains. The arrow indicates the growth  
11 direction.  
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14 Fig. 2 SEM micrographs of longitudinal polished sections of the textured samples: a)  
15  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  and b)  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$ .  
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18 Fig. 3 Temperature dependence of the electrical resistivity,  $\rho$ , for the different  
19 compositions: (●)  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  and (◆)  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$ .  
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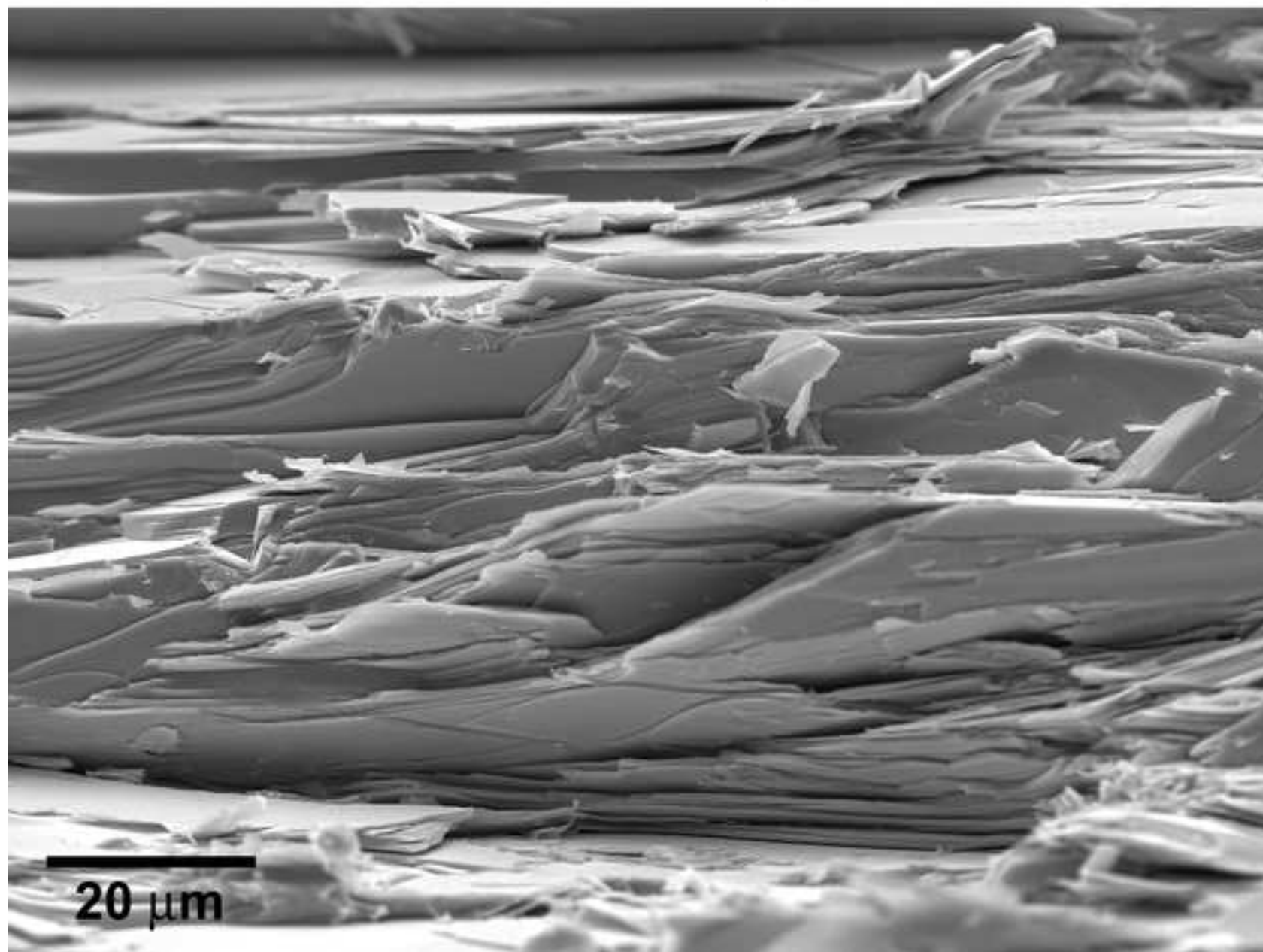
22 Fig. 4 Temperature dependence of the thermopower, TEP, for the different  
23 compositions: (●)  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  and (◆)  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$ .  
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26 Fig. 5 Temperature dependence of the power factor, PF, for the different  
27 compositions: (●)  $\text{Bi}_2\text{Ca}_2\text{Co}_{1.7}\text{O}_y$  and (◆)  $\text{Bi}_2\text{Sr}_2\text{Co}_{1.8}\text{O}_y$ .  
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Figure

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**Growth direction**



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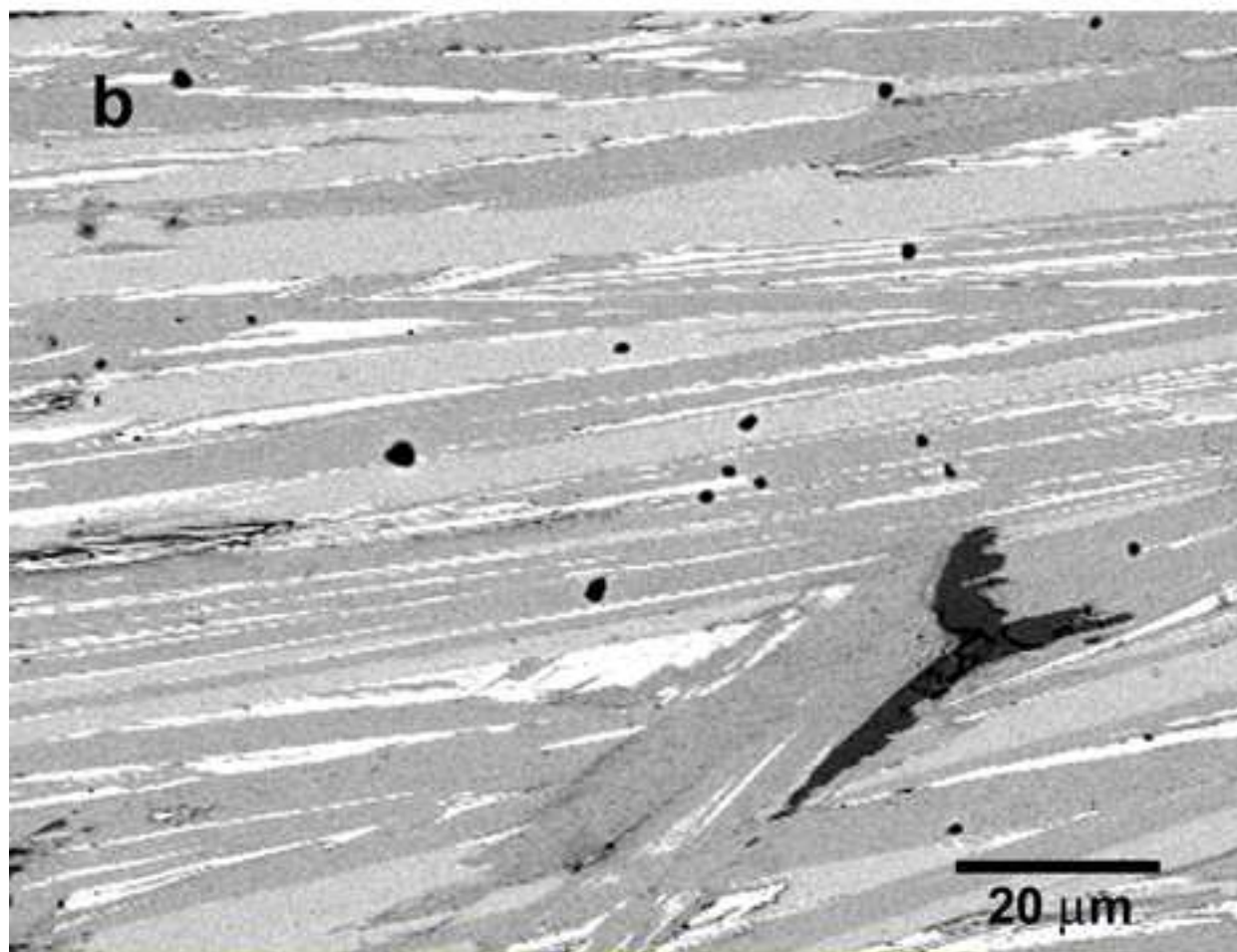
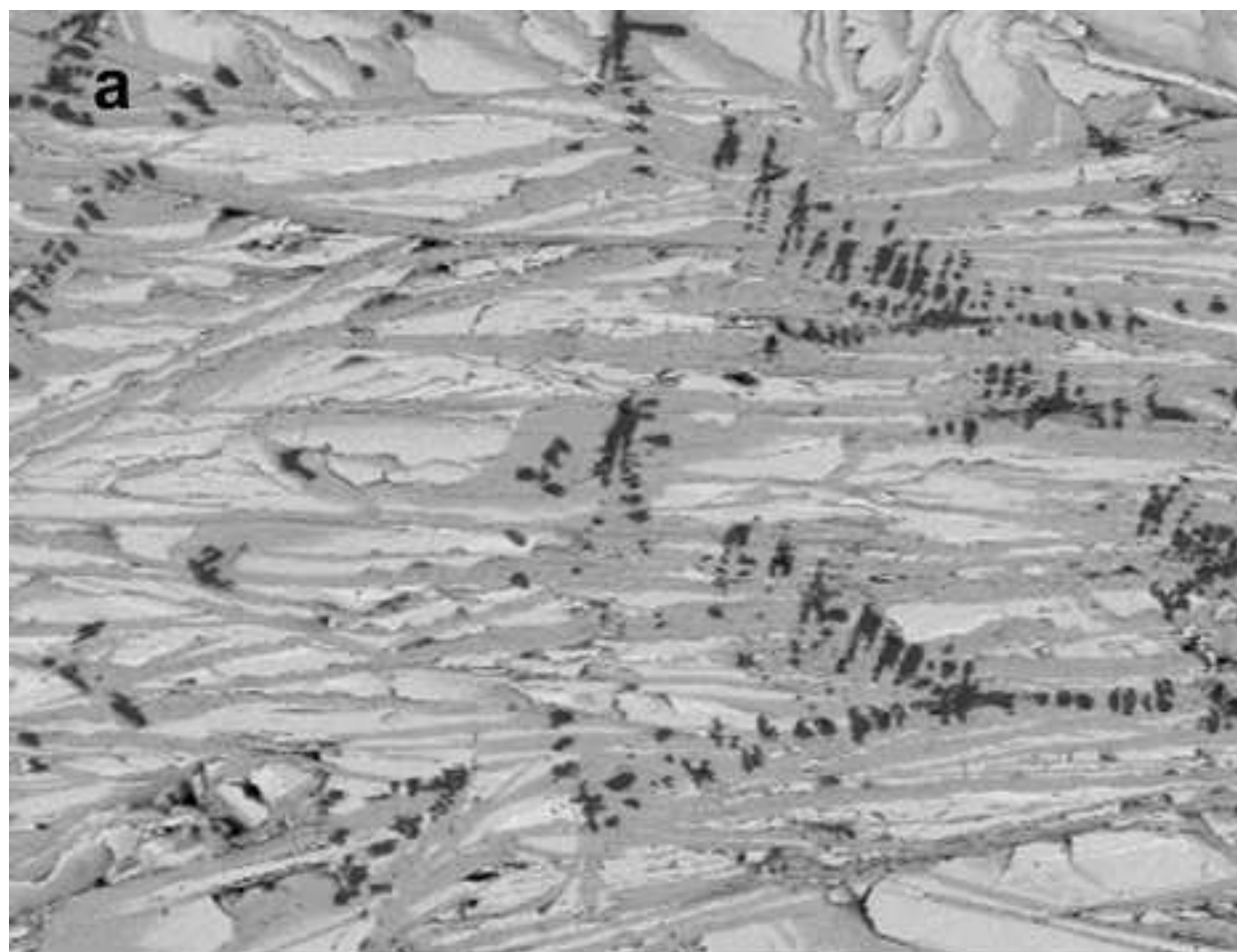


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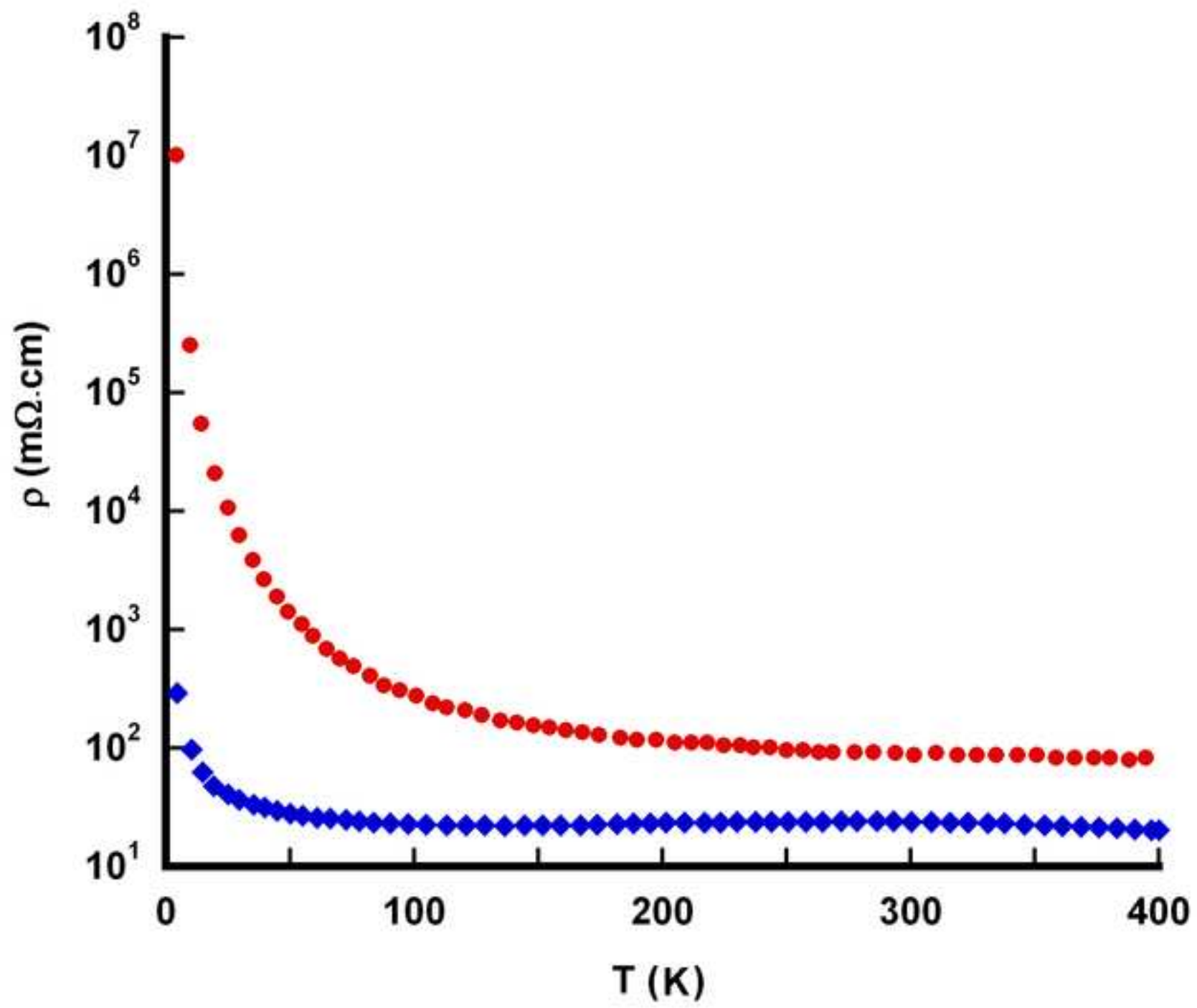




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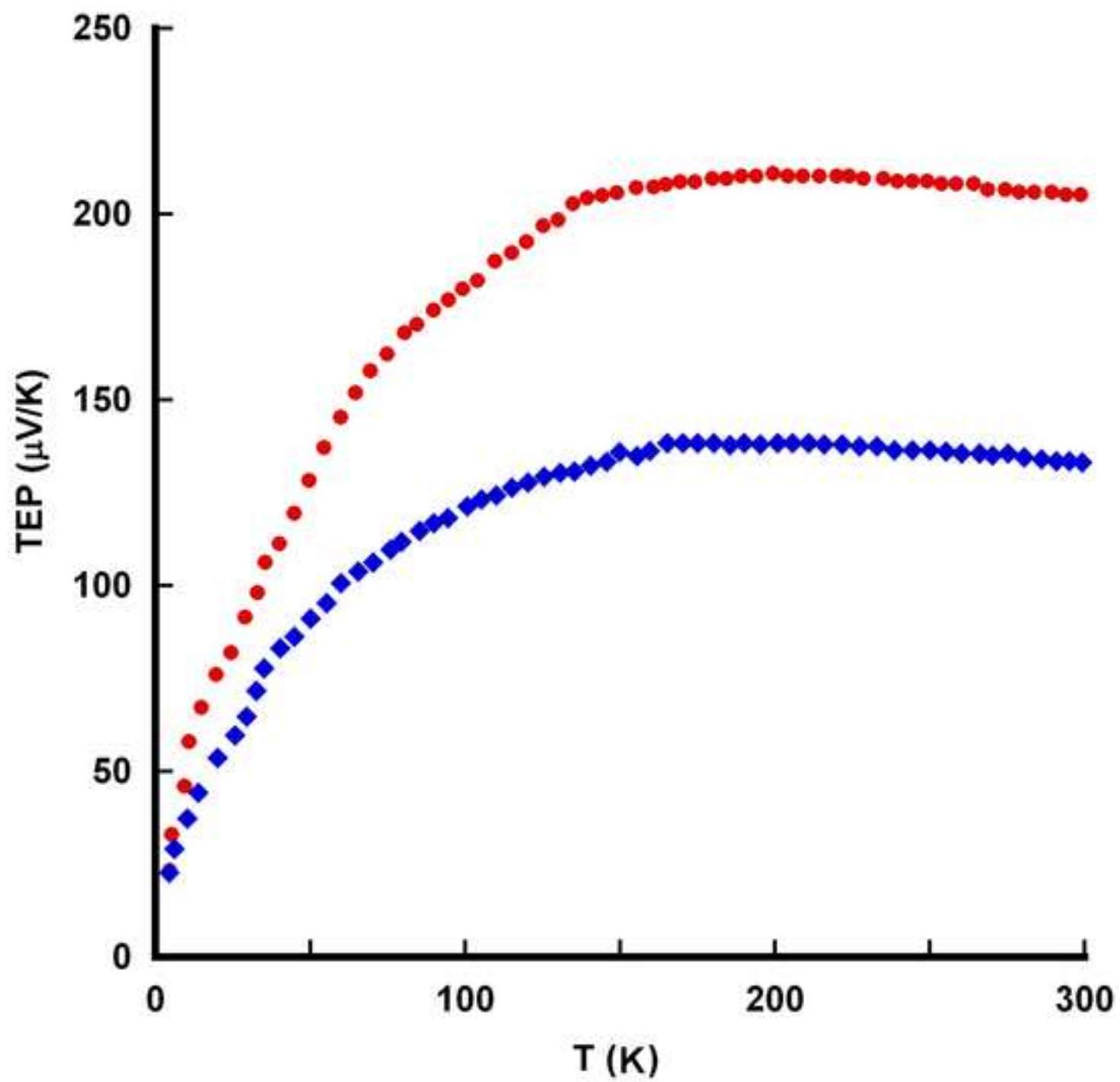


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