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## Overview of Kizildere Geothermal Power Plant in Turkey

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### Abstract

Achieving sustainable development is a target that is now widely seen as important in worldwide public opinion. In this context, the utilization of renewable energy resources such as solar, geothermal and wind energy appears to be one of the most efficient and effective ways of achieving this target. Recently, power generation from geothermal energy has become of big importance in Turkey, which is located on the Mediterranean sector of the Alpine-Himalayan Tectonic Belt and is among the first seven countries in abundance of geothermal resources around the world. The main objective in doing the present study is twofold, namely: (a) to investigate Turkey's geothermal energy potential for power generation and (b) to overview the Denizli-Kizildere geothermal power plant (DKGPP) with an installed capacity of 20.4 MW<sub>e</sub>, which is at present the only operating geothermal power plant of Turkey. Based on the drilling data, which have been gathered to date, Turkey's geothermal energy potential for power generation is determined to be 764.81 MW<sub>e</sub>. Electricity generation projections of Turkey are also 500 MW<sub>e</sub> from Germencik, Kizildere, Tuzla and several of the other fields by the year 2010 and 1000 MW<sub>e</sub> by 2020. The Denizli-Kizildere geothermal field has an estimated capacity of 200 MW<sub>e</sub>. The DKGPP was put into operation in 1984 and has been operated since then. It produced an electrical energy of 89,597 MWh in 2001, representing an electric power of 10.6 MW<sub>e</sub> in the same year. Present applications have shown that in Turkey, geothermal energy is a promising alternative and can make a significant contribution towards reducing the emission of greenhouse gases. As the public recognizes the projects, the progress will continue.

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**Keywords:** Electricity generation; Geothermal energy; Geothermal fields; Power generation; Power plant; Renewable energy; Kizildere; Turkey

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## 1. Introduction

Despite the limitations of Planet Earth's conventional energy resources, the demand for energy is continuously rising as a result of increasing population and industrialization. The utilization of fossil energy resources is presently causing increasingly disastrous effects on the global environment. In this regard, there is urgent need to deploy sustainable and environmentally clean energy sources. An important contribution could be made by rapidly expanding the use of renewable energy sources, such as geothermal energy [1].

Geothermal energy is the energy contained as heat (the thermal energy) within the Earth's interior. The origin of this heat is linked to the internal structure of our planet and the physical processes occurring there. Geothermal energy, is to some extent, a renewable energy source, since a geothermal resource usually has a projected life of 30–50 years. The life of a resource may be prolonged by a reinjection process, which may compensate for at least part of the fluid extracted by production [2–4].

Table 1 illustrates installed geothermal generating capacities in the top 10 countries and Turkey between 1995 and 2000. Hutterer [5,6] has reviewed the world wide application of geothermal energy for power generation and reported the following: (a) geothermally fueled electric power is being generated in 21 nations as of February 2000, (b) the installed capacity has reached 7974 MW<sub>e</sub> in 2000, which is a 16.7% increase since 1995, (c) the total energy generated during the last 5 years has been at least 49,261 GWh, (d) about 1165 wells more than 100 m deep have been drilled. Hutterer [6] also concluded that greater increases in the total international installed geothermal power generation capacity were inhibited by the economic crisis that occurred in southeast Asia, by the low petroleum prices that prevailed during the 5 year period from 1995 to 2000 and by serious capacity declines at The Geysers field in California, USA.

The share of the top three countries, namely the US, The Philippines and Italy, in total installed capacity of 7974 MW<sub>e</sub> in 2000 (with the generation of 49.3 billion kWh in the same year) was about 27.94%, 23.94% and 9.8%, respectively, followed by Mexico at 9.47%, Indonesia at 7.39%,

Table 1  
Installed geothermal generating capacities in the top 10 countries and Turkey between 1995 and 2000 [5,6]

Country	1995 (MW <sub>e</sub> )	2000 (MW <sub>e</sub> )	2005 (estimated MW <sub>e</sub> )	1995–2000 (MW <sub>e</sub> increase)	% Increase
USA	2816.7	2228	2376	–588	n/a
Philippines	1227	1909	2673	682	55.8
Italy	631.7	785	946	153.3	24.3
Mexico	753	755	1080	2	0.3
Indonesia	309.75	589.5	1987.5	279.75	90.3
Japan	13.705	549.6	566.9	133.195	32.2
New Zealand	286	437	437	151	52.8
Iceland	50	170	186	120	240
El Salvador	105	161	200	56	53.3
China	28.78	9.17	n/a	0.39	1.35
Turkey	20.4	20.4	250	0	0
Total <sup>a</sup>	6833	7974	11,414	1141	17

<sup>a</sup> This total includes 22 countries, while in Argentina there were no installed capacities in 2000.

Japan at 6.85%, New Zealand at 5.48% and others at 9.13%. By comparison, Turkey accounted for about 0.256% of the total [4–6].

Geothermal energy utilization may be divided into two categories, namely electric energy production and direct uses. Direct or non-electric utilization of geothermal energy refers to the immediate use of the heat energy rather than to its conversion to some other form, such as electrical energy. The geothermal energy source that can be easily converted into electrical power is generally considered renewable, because reservoirs may be recharged by rain and by reinjection of the spent water. In general, the geothermal fluid temperatures required for direct heat use are lower than those for economic electric power generation [7,8]. In this context, the main uses of geothermal energy in Turkey are: space heating and domestic water supply, greenhouse heating, balneology, CO<sub>2</sub> and dry ice production process, heat pumps and electricity generation.

Turkey has a place among the first seven countries in abundance of geothermal resources around the world [9,10]. To date, wells were drilled in 105 geothermal fields although there are 170 geothermal fields in Turkey. The General Directorate of Mineral Research and Exploitation (MTA) has conducted geothermal energy explorations in Turkey. The inventorial works and chemical analyses of the hot springs and mineral waters started in 1962 [11,12]. The existence of more than 600 hot springs indicates that Turkey has an important geothermal energy potential, as given in detail elsewhere [13]. The data accumulated since 1962 show that the estimated direct use potential is about 31,500 MW, of which 10% is apparent. However, only 2–3% of this potential has so far been utilized [13–15].

## 2. Turkey's geothermal energy potential for power generation

About 95% of the 170 geothermal fields in Turkey are low–medium enthalpy fields, which are suitable for direct use applications. Among the remaining 9 fields, Denizli-Kizildere (200–242 °C), Aydin-Germencik (232 °C), Canakkale-Tuzla (174 °C), Aydin-Salavatli (171 °C), Kutahya-Simav (162 °C), Manisa-Salihli (150 °C) and Izmir-Seferihisar (153 °C) are high enthalpy fields, which are suitable for electrical energy production [12,13]. The locations of the nine geothermal fields are illustrated in Fig. 1, while the four fields of highest temperature are summarized below.

The only operating geothermal power plant of Turkey is the Denizli-Kizildere geothermal power plant (DKGPP) located near Denizli City in Western Anatolia with an installed capacity of 20.4 MW<sub>e</sub>. The total capacity of the field is estimated to be 200 MW<sub>e</sub>, as given in Table 2.

The exploration stage is completed in the Aydin-Germencik field, which is located to the west of Kizildere. Nine wells have been drilled into a 216–232 °C reservoir within marbles and quartzites at depths ranging from 285 to 1500 m. The field capacity is estimated to be 100 MW<sub>e</sub>. The first stage of the field development is planned to build a 25 MW<sub>e</sub> single flash plus binary power plant [16].

The third field with power generation potential is the Canakkale-Tuzla field in northwest Anatolia. The first well was drilled in 1982. The temperature encountered was 174 °C in a reservoir at a depth of 333–553 m in volcanic rocks. A second well was drilled to 1020 m. Temperatures up to 174 °C were recorded, but the permeability was low. Another two shallow wells (81 and 128 m) also produced fluid at 146 and 165 °C.

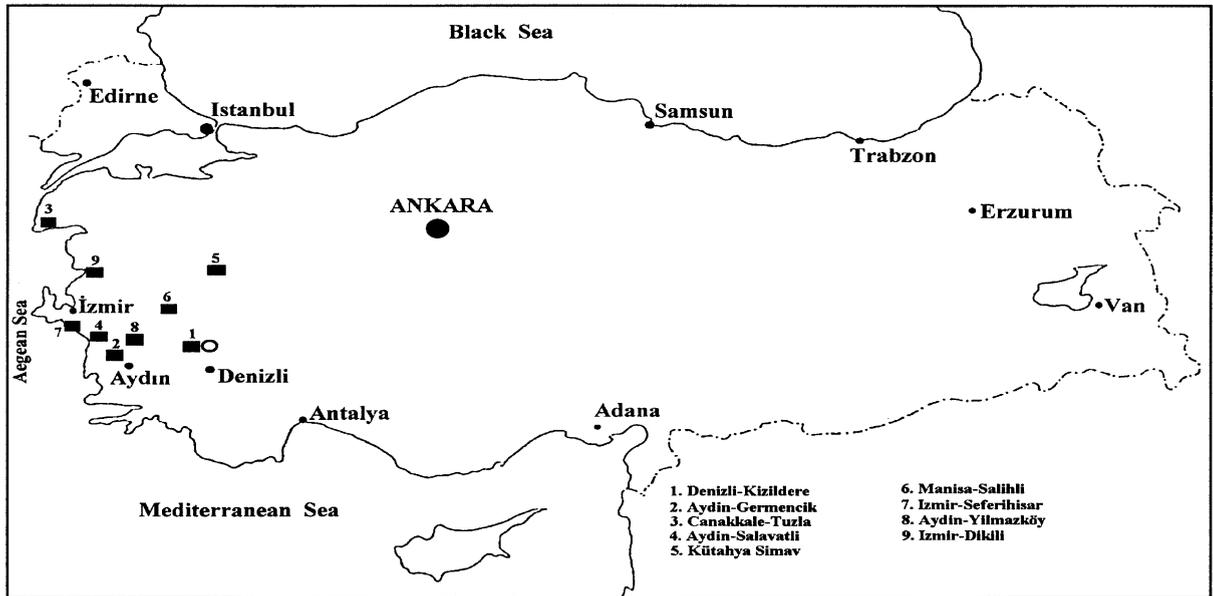


Fig. 1. Map indicating Turkey's geothermal fields suitable for power generation (o): the location of Turkey's only operating geothermal power plant (GPP): Denizli-Kizildere GPP.

Table 2

Utilization of geothermal energy for electricity generation in Turkey

Name of geothermal power plant	Year commissioned	Status	Type of unit	Unit rating			
				Potential (MW <sub>e</sub> )	Operational (MW <sub>e</sub> )	Under construction or planned (MW <sub>e</sub> )	Annual production in 2001 (GWh/yr)
Denizli-Kizildere	1984	O	SF + C	200	20.4	–	89.6
Aydin-Germencik	–	P	SF + B	100		25	–
Aydin-Salavatli	–	P	B or K	N/A		5	–

SF, single flash; C, condensing; B, binary; K, kalina; O, operational; P, planned; UC, under construction; N/A, no data.

The Aydin-Salavatli field has a reservoir temperature of 171 °C. It was planned to build a 5 MW<sub>e</sub> binary or Kalina cycle plant in the field, but this has not been realized yet [15].

Some attempts have been made towards installation of geothermal power plants in the fields of Aydin-Germencik-Omerbeyli, Canakkale-Tuzla and Manisa-Salihli-Caferbey. Besides this, there are also some investment attempts for electricity generation in Aydin-Salavatli by applying the autoproduction model [12], which is defined as the production of electricity by industrial facilities for their own use in Turkey based on the Turkish Trade Law [17].

The number of wells in the two geothermal fields, Denizli-Kizildere and Aydin-Germencik, is relatively more than that of the remaining fields. Besides this, the geothermal wells drilled are insufficient in the other 7 geothermal fields. Therefore, studies on the determination of the potential of these fields are still in progress [12,16]. Based on the drilling data, which have been

gathered to date, Turkey's geothermal energy potential for power generation is determined to be 764.81 MW<sub>e</sub> [12]. Electricity generation projections of Turkey are also 500 MW<sub>e</sub> from Germencik, Kizildere, Tuzla and several of the other fields by the year 2010 and 1000 MW<sub>e</sub> by 2020 [5].

### 3. Brief historical development of the Denizli-Kizildere geothermal power plant

The Denizli-Kizildere geothermal field (DKGF) is located 30 km away from the province of Denizli, Western Anatolia, Turkey, as can be seen in Fig. 2. This field is the first and only geothermal field developed in Turkey. The first geological, geochemical, and geophysical studies were conducted with the support of the United Nations Development Program (UNDP) in 1966. Two stratigraphically separate zones in the field were initially identified as first and second reservoirs during the exploration stage. The shallow reservoir has a temperature of 190–200 °C, a depth of up to 706 m, a steam fraction of 10% and moderate permeability. The deeper one has 200–212 °C

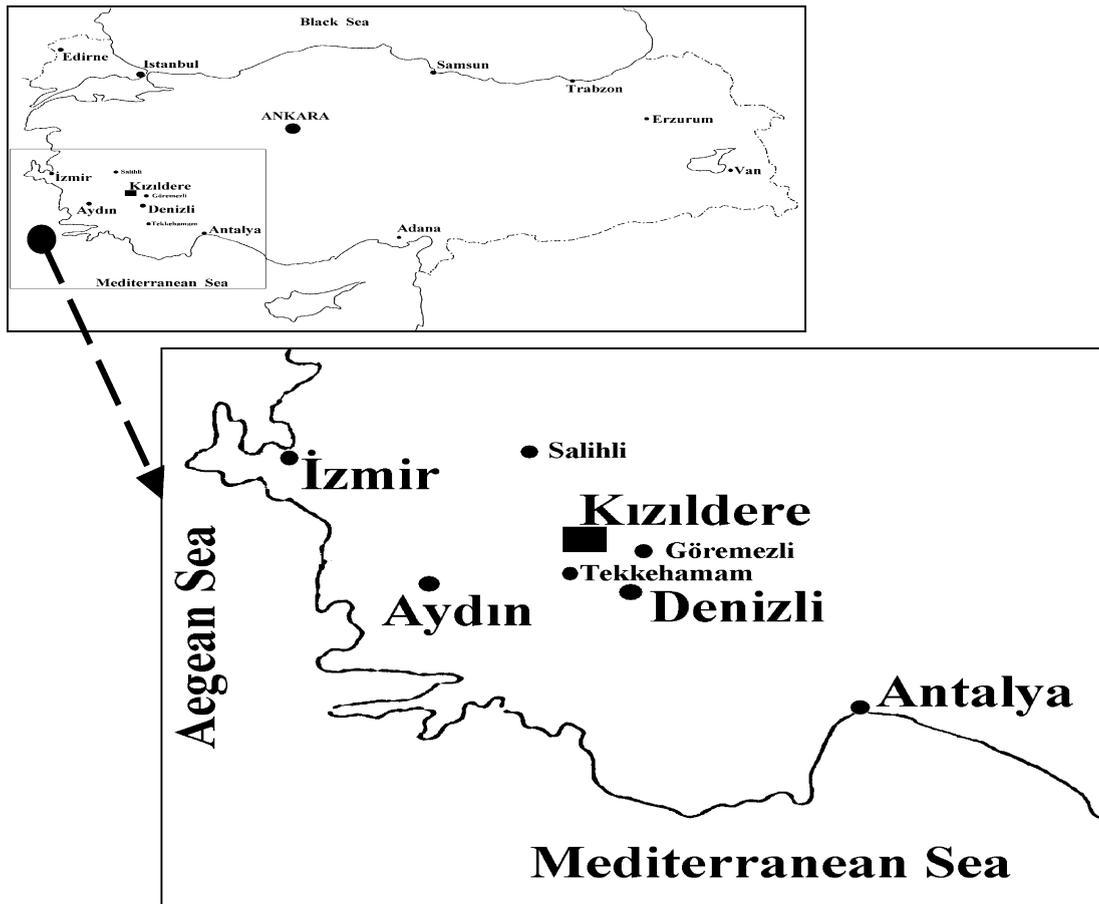


Fig. 2. Location of the Denizli-Kizildere geothermal field.

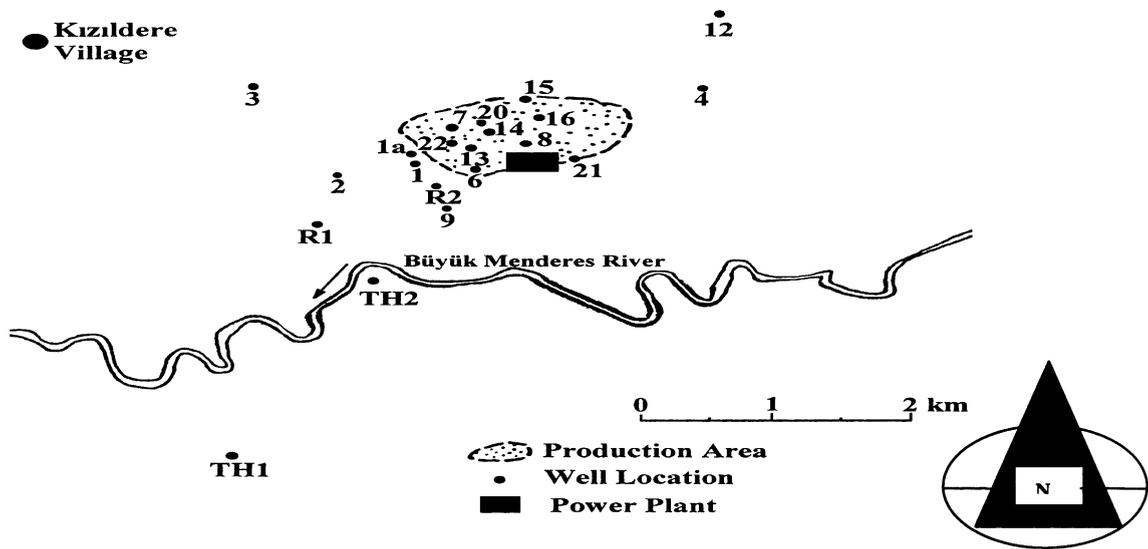


Fig. 3. Well locations of the Denizli-Kizildere geothermal field [18].

temperature, a depth of up to 1241 m, a steam fraction of 10–12% and a higher permeability. So, the second reservoir was chosen as the production zone.

Fig. 3 illustrates the well locations of the DKGf [18]. The first well (the so-called KD-1) was drilled in 1968, and the temperature measured was 198 °C at a depth of 540 m. A total of 14 wells were drilled between 1968 and 1973, while the encountered temperatures were in the range of 170–212 °C. A 0.5 MW<sub>e</sub> pilot plant, which was fed from the KD-13 well, was installed in 1974 in the field. The electricity generated had met the demand of the villages around the field for a long time period. The MTA reported that 6 (KD-6, 7, 13, 14, 15, 16) out of 13 wells were suitable for electricity generation. The DKGPP was installed on February 14, 1984 with an installed capacity of 20.4 MW<sub>e</sub>. Then, 3 (KD-20, 21, 22) more production wells were drilled in two years, and the total number of production wells reached 9 [19]. In 1997, the R-1 well was drilled for injection purposes [20]. A liquid CO<sub>2</sub> and dry ice production process with a capacity of 40,000 tons/yr was built adjacent to the field in 1986. The capacity of the process was increased to 120,000 tons/yr in 1999. Besides electricity and dry ice production, the resources of the field have also been used for greenhouse heating and space heating of offices and staff houses of the plant [21,22]. In Turkey, the first geothermal greenhouse heating system of 4.5 da was applied in the DKGf in 1985 [13].

Currently, the DKGPP employs 98 people including engineers, technicians and workers. The plant operates 8000 h/yr. The rest of the time is spent for maintenance such as cleaning the wells and overhaul. Electricity production cost was calculated as 1.75 cents/kWh in 2001.

#### 4. Denizli-Kizildere geothermal field

The main characteristics of the DKGf are given in Table 3 [19,23]. This field is a liquid dominated system with a steam fraction of 10–12%. The steam field has an area of 550 m × 650 m,

Table 3  
Main characteristics of the Denizli-Kizildere geothermal field [19,23]

Description	Unit	Value
Reservoir temperature	°C	200–242
Wellhead steam fraction	%	10–12
CO <sub>2</sub> partial pressure ( $P_{CO_2}$ )	MPa	3.0–5.0
Total dissolved solid (TDS)	ppm	2500–3200
NCG content in steam (by wt.)	%	10–21
CO <sub>2</sub> content	%	96–99
H <sub>2</sub> S content	ppm	100–200

Table 4  
Gas analysis of some production and observation wells [23]

Well no.	Date	H <sub>2</sub> (vol.%)	O <sub>2</sub> –Ar (vol.%)	N <sub>2</sub> (vol.%)	CH <sub>4</sub> (vol.%)	CO <sub>2</sub> (vol.%)	H <sub>2</sub> S (vol.%)	He (ppm)
KD 6	May 9, 1988	0.3	0.1	1.8	0.3	97.5	<0.1	5.4
KD 6	June 15, 1988	<0.1	2.7	11.8	<0.1	85.5	<0.1	5.9
KD 6	June 6, 1988	<0.1	2.1	8.5	<0.1	89.4	<0.1	8.2
KD 7 <sup>a</sup>	May 8, 1988	<0.1	0.1	0.5	0.1	89.3	<0.1	15.6
KD 7 <sup>a</sup>	June 29, 1988	<0.1	2.4	8.8	<0.1	88.8	<0.1	7.7
KD 14	June 30, 1988	<0.1	11.6	42.6	<0.1	45.8	0.1	11.6
KD 16	June 29, 1988	<0.1	2.4	9.2	<0.1	88.4	<0.1	10.9
KD 21	June 23, 1988	<0.1	1.6	3.6	<0.2	94.8	<0.1	14
KD 22	May 8, 1988	<0.1	0.6	1.7	0.1	97.5	<0.1	15

<sup>a</sup> Observation well.

while the calculated reservoir area is 100 km<sup>2</sup>. The depth of the wells changes from 370 to 2261 m. The reservoir temperature is between 200 and 242 °C. The estimated capacity of the field is 200 MW<sub>e</sub>. The most significant characteristic of the field is the high amount of non-condensable gases (2.5% in the reservoir, 5% by volume of steam, 10–21% by weight of steam and average 13% by weight of steam at the turbine inlet) with a CO<sub>2</sub> content of 96–99%, H<sub>2</sub>S content of 100–200 ppm and NH<sub>3</sub> content of 72 ppm. A gas analysis of some production and observation wells is given in Table 4 [23]. The specific steam consumption of the plant is 10.96 kg/kWh. The first law efficiency of the plant is determined to be 11.98%.

A geothermal power plant can be divided into two sections, namely (a) steam field and (b) power generation unit including turbine house, cooling tower and related systems.

The major components of a steam field are:

- (a) The wellbore,
- (b) The wellhead with its valves,
- (c) Separators if it is a liquid dominated system,
- (d) A silencer,
- (e) A ball check valve,
- (f) A steam transmission system,
- (g) A waste water system, and/or
- (h) An injection system.



Table 5  
Production well data [24]

Well no.	Drilling date	Well-head temperature (°C)	Well-head pressure (MPa)	Depth (m)	Total flow rate (kg/s)	Separator pressure (MPa)	Separator temperature (°C)	Steam flow rate (kg/s)	CO <sub>2</sub> content (by wt. of steam) (%)	Liquid flow rate (kg/s)
KD-6	1970	194	1.356	851	23.32	0.367	147	2.80	20	20.52
KD-13	1971	198	1.387	760	26.31	0.377	145	3.16	17.4	23.15
KD-14	1970	210	1.356	597	29.13	0.387	148	3.50	10	25.63
KD-15	1971	208	1.387	510	31.59	0.377	147	3.79	17.5	27.80
KD-16	1975	212	1.427	666.5	45.45	0.387	148	5.45	12	40.00
KD-20	1986	204	1.448	810	30.48	0.377	147	3.66	13.7	26.82
KD-21	1985	205	1.101	898	32.03	0.387	147	3.84	10.6	28.19
KD-22	1985	204	1.386	888	28.24	0.367	147	3.39	14	24.85
R-1	1997	242	1.409	2261	44.44	0.369	148	5.33	21	39.10

Table 6  
Injection well data [24]

Well no.	Wellhead temperature (°C)	Wellhead pressure (MPa)	Depth (m)	Total flow rate (kg/s)	Status
TH-2	168	N/A	2001	11.67	Abandoned
R-1	242	1.962	2261	103.05	Converted to production well
R-2	197	1.478	1371	55.55	Injection

discharges the wastewater over a measuring weir to determine the well output characteristics before its disposal to the wastewater channel. From May to August 2002, two wells were connected to the injection well for injection trials. So, the silencers are only used to by-pass the well output when it is necessary.

(e) *Ball check valve*. The steam from the separator is first sent to a safety unit, which employs a ball check valve to prevent water entrance to the steam line. If water moves with the steam, the ball ascends and seals the flow.

(f) *Steam transmission system*. The wells are connected individually through a wellhead separator via a steam branch line to the main steam transmission line with a length of 1171 m to the power plant. The pipeline is insulated to reduce heat loss and to conserve the enthalpy of the fluid. Condensation traps achieve control of the condensate in the bottom of the pipe, which is caused by heat loss. This also ensures adequate scrubbing, particularly of the salts, and a clean fluid is presented to the turbine.

(g) *Waste water system*. Only 10–12% of the brine extracted from the ground turns into steam after the separation process, while the remainder (88–90%) has been disposed to the Menderes river through a 1.8-km long channel at an average temperature of 147 °C and a total flow rate of 277.7 kg/s since 1984.

(h) *Injection system.* The commonly acceptable method of dealing with wastewater is to inject it back into a part of the reservoir.

The first pilot injection test in the DKGf was conducted in 1976 and lasted for 29 weeks. The water produced from well KD-15 was injected into well KD-1A at an average rate of 23.61 kg/s. The injected water temperature varied from 70 to 80 °C. Well KD-1, which is 68 m away from KD-1A, was chosen as an observation well. The cooling effect was encountered at the observation well. A heat flow model describing the non-isothermal fluid flow in naturally fractured reservoirs is applied, and the temperature behavior in the observation well is predicted.

The second test lasted for 45 days in 1995. The water produced from KD-20 was injected into well KD-7 by gravity. The wellhead injection temperature was 100 °C. The decline in injectivity is related to the possible plugging by scale deposition in the injector. The producer well KD-20 also served as an observation well for monitoring the produced water temperature and chloride ( $\text{Cl}^-$ ) concentration. Some change in the chloride content but no change in the temperature of the produced water was observed. Because of the limitations in technical conveniences at that time, the actual reasons for the plugging difficulty have never been revealed [25].

After those trials, an injection well (TH-2) was designed to drill on the other side of the Menderes river in the Tekkehamam field, which is 3 km away from the DKGf. The injectivity of the well was poor, and hence, it was abandoned.

According to the injection program of the MTA, another injection well (R-1) was drilled in the DKGf boundary in 1997. R-1 indicated that a third reservoir with a temperature range of 235–245 °C exists in the DKGf. Taking into account the completion test results, it may be concluded that the well has a high productivity with figures of 103.05 kg/s and 6 MW<sub>e</sub> with the highest temperature in the field having a bottomhole temperature of 242 °C at 2261 m. Based on the data obtained, the R-1 well was converted to a production well in 2001, and the production of the plant increased by 6.5%. The production rate of the plant between 1984 and 2001 is illustrated in Fig. 5 [24,26].

Following the R-1 well drilling, the MTA conducted some injection trials at abandoned wells in the field in 1998–99, but a drastic temperature drop was observed in the production wells. In 2000, a new injection well (R-2) was initiated to drill and was completed in 2001 with a depth of 1371 m.

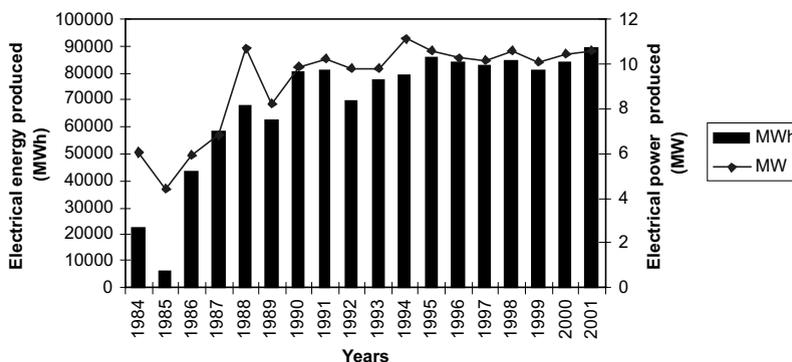


Fig. 5. Electricity generation of the Denizli-Kizildere geothermal power plant between 1984 and 2001 [24,26].

Injection trials in R-2 have been conducted for 3 months from May to August 2002. Separated liquid from 2 production wells at a flow rate of 55.55 kg/s and a temperature of 125–135 °C were injected by gravity. The results of the trials have not been reported yet.

Based upon the injection strategy recommended by Serpen and Satman [20], the Kizildere system would produce from the deeper and hotter third reservoir and inject to the shallow reservoir. Since the third reservoir produces more steam than the second reservoir, which is used as a production zone, the amount of water to inject will decrease approximately by half.

## 5. Denizli-Kizildere geothermal power plant

The DKGPP is a single flash system with a condensing low pressure double flow turbine. The plant operates with a 90% load factor. The main characteristics of the DKGPP are given in Table 7 [19,24,27], while the major components of the power generation unit are as follows:

- (a) Scrubber (main moisture separator),
- (b) Turbine-generator unit,
- (c) Condenser,
- (d) Gas removal system,
- (e) Cooling tower,
- (f) Auxiliary equipment (parasitic loads).

Table 7  
Main characteristics of the Denizli-Kizildere geothermal power plant [19,24,27]

Description	Unit	Value
Number of production wells		9
Optimum wellhead pressure	MPa	1.6 (because of scaling)
Wellhead operation pressure	MPa	1.28–1.58
Wellhead temperature	°C	180–190
Total flow rate	kg/s	320.83
Separator pressure	MPa	0.367–0.387
Separator temperature	°C	145–148
Steam flow rate	kg/s	25–38.88 (av. 33.34)
Steam pressure at safety valve	MPa	0.35
Steam temperature at safety valve	°C	147.2
Turbine pressure	MPa	0.378
Turbine temperature	°C	147
Back pressure at turbine exhaust	MPa	0.01
Steam wetness at turbine exhaust	%	9.5
NCG flow rate	kg/s	6.1345
Capacity	MW <sub>e</sub>	Installed 20.4 Gross 14.0 Net 11.2
Compressor consumption	MW <sub>e</sub>	2.38 (12% of installed capacity, 17% of gross capacity)

Table 8  
Main characteristics of turbine-generator unit [19]

Description	Unit	Value
Turbine inlet temperature	°C	147
Turbine inlet pressure	MPa	0.378
Turbine inlet enthalpy	kJ/kg	2742.35
Steam flow rate (average)	kg/s	33.34
Steam flow rate (at maximum output)	kg/s	42.42
Turbine exit temperature	°C	42–44
Turbine exit pressure	MPa	0.01019
Turbine exit enthalpy	kJ/kg	2357.6
Water enthalpy at condenser pressure	kJ/kg	190
Turbine rotor speed	rpm	3000
Rated output	kW	17,800
Maximum output	kW	17,800
Compressor power	kW	2380
Thermal efficiency	%	11.98
Turbine-generator efficiency	%	71.2

(a) *Scrubber*. Outside of the turbine house, the steam enters a scrubber to remove the impurities and condensate. At the exit of the scrubber, the steam goes to a demister to remove the moisture and splits into two branches that are sent to the double flow turbine.

(b) *Turbine-generator unit*. The double flow turbine used in the DKGPP consists of two turbines on the same shaft with steam flowing in opposite directions. It is preferred because of its lower capital cost and the balance on the thrust loads. The turbine has seven reaction stages on both sides. The main characteristics of the turbine-generator system of the DKGPP are illustrated in Table 8 [19]. The pressure and temperature of the turbine are 0.378 MPa and 147 °C, respectively. The total steam flow rate, including NCG's, enters the turbine at a flow rate of 33.34 kg/s, expands to 0.01019 MPa and flows to the condenser. To protect the leading edge of the last blades of the turbine from erosion and corrosion by water droplets, stellite erosion shields coat the blades, and to remove the condensate, drain channels are added. The turbine is protected by safety discs against excess pressure differentiation during drainage. The turbine-generator efficiency is determined to be 71.2%.

(c) *Condenser*. A direct contact condenser with barometric leg, situated under the turbine, is used in the DKGPP. Direct contact condensers are the least affected condensers from harmful physical and chemical impacts of the fluid. The heat transfer coefficient is also higher than with surface type condensers.

The condenser consists of two sections: the first one is a co-current horizontal section where the cooling water contacts steam, while the second one is a vertical barometric leg where NCG's and a small fraction of uncondensed steam are accumulated and the condensate flows down to be pumped to the cooling tower. The cooling water (2375 kg/s) is sucked from the cooling tower by vacuum in the condenser at 29 °C temperature and flow rate and then sprayed over the steam by nozzles. Two centrifugal pumps are used to pump the condensate with a temperature of 36.6 °C. The condenser is manufactured of stainless steel for corrosion protection. To prevent plugging of the nozzles, the nozzle diameters are kept as wide as 50 mm. The condenser-turbine coupling is made of stainless steel to absorb the vibration and thermal expansions.

(d) *Gas removal system.* In the DKGPP, NCG's are extracted from the condenser by a compressor and passed to the dry ice production plant, which produces dry ice and liquid CO<sub>2</sub> at a rate of 120,000 tons/yr. The capacity of the gas extraction system is 2.38 MW<sub>e</sub> (17% of the gross capacity) due to a high NCG content.

The general configuration consists of a two body compressor with two inter-coolers. The first unit rotor (LP) is directly coupled to the turbo-generator and, hence, rotates at 3000 rpm. The second unit (HP) is driven from the first, via a speed increasing gear and rotates at 3900 rpm. The characteristics of the centrifugal compressor in the plant are given in Table 9 [24].

(e) *Cooling tower.* A wet mechanical draft cooling tower is used to cool the condensate, which is used in the condenser as cooling water. The cooling tower employs four motor driven fans, each consuming 110 kWh. The fans are located at a height of 11.5 m. The condensate is pumped to a height of 8.5 m, distributed through headers and falls to the basin. Each cell is a separate unit with its own fan and louvered openings on only two sides. The cells are arranged side by side in a long row. The cell dimension is 15 m × 15 m. The width, length and height of the cooling tower are 15, 60 and 15 m, respectively. Airflow is counter-current, and the construction material is concrete. The condensate at 36.6 °C is cooled to 29 °C by evaporation. The feed water to substitute for the evaporated water (1.7%) and leakage losses comes from the Menderes river.

(f) *Auxiliary equipment.* The parasitic load in the plant accounts for about 20% of its gross capacity. The highest portion of the parasitic load is the compressor consumption, which

Table 9  
Main characteristics of gas compressors in the Denizli-Kizildere geothermal power plant [24]

Description	Unit	Value
Gas content	%	99.9 CO <sub>2</sub> , 0.1 H <sub>2</sub> S
Gas flow rate (Including 500 kg/h air leakage)	kg/s	6.44
Steam flow rate (LP suction)	kg/s	2.47
Total gas flow rate (suction)	kg/s	8.91
Compressor suction capacity	m <sup>3</sup> /h	293,500
Cooling water inlet temperature	°C	29
Cooling water flow rate	m <sup>3</sup> /h	900
LP compressor rotor speed	rpm	3000
LP suction temperature	°C	53
LP suction pressure	MPa	0.08
LP discharge temperature	°C	50–52
LP discharge pressure	MPa	0.1013
HP compressor rotor speed	rpm	3900
HP suction temperature	°C	50–52
HP suction pressure	MPa	0.093
HP discharge temperature	°C	35–40
HP discharge pressure	MPa	0.34
Critical speed LP rotor (calculated) HP rotor	rpm	1986 1730
No. of bodies		2
No. of inter coolers		2
Power	(kW)	2380

Table 10  
Power consumption of auxiliary equipment in the Denizli-Kizildere geothermal power plant [19]

Equipment	Unit power (kW <sub>e</sub> )	No. of units	Total power (kW <sub>e</sub> )
Compressor	2380.0	1	2380
Main lubrication pump	37.3	1	37.3
Drill collar pumps	0.185	2	0.37
Emergency bearing lubrication pump	37.3	1	37.3
Demister	2.24	1	2.24
Cooling tower fan motor	37.285	4	149.14
Water pump (domestic use and cooling water)	37.0	2	74.0
Sand filters water pump	7.5	2	15.0
Sand filters back wash pump	3.0	2	6.0
Dosage pump	0.25	3	0.75
Chlorinated water pump	37.0	2	74.0
Service air compressor	37.0	2	74.0
Air drier	1.5	1	1.5
Grand total			2851.6

constitutes 83% of the total parasitic load and 17% of gross capacity. The auxiliary equipment consumption is given in Table 10 [19].

## 6. Conclusions

Geothermal utilization is commonly divided into two categories, namely electric energy production and direct (or non-electric) uses. This study focused on the former, namely power generation. The main conclusions derived from the present study may be summarized as follows:

- In Turkey, there are nine geothermal fields suitable for generating electricity.
- Based on the values for wells drilled, Turkey's geothermal power production potential is estimated to be 764.81 MW<sub>e</sub>.
- The only operating geothermal power plant of Turkey is the Denizli-Kizildere geothermal power plant with an installed capacity of 20.4 MW<sub>e</sub>, while the total capacity of the field is estimated to be 200 MW<sub>e</sub>.
- There is not any 'geothermal law in Turkey' as yet. There is, however, a 'draft geothermal law'. It is expected that geothermal energy development will significantly increase in the country if this law becomes effective.
- The first law efficiency of the DKGPP is determined to be 11.98%. By comparison, the efficiency of generation of electricity from geothermal steam is generally in the range of 10 to 17% [4].
- Only 10–12% of the brine extracted from the ground turns into steam after the separation process, while the remainder (88–90%) has been discharged to the Menderes river at an average temperature of 147 °C and a total flow rate of 277.7 kg/s since 1984. Therefore, the plant efficiency may be improved by using the brine instead of discharging it to the Menderes river. In this regard, the existing plant may be combined with a binary geothermal power plant,

which is especially suitable for operating temperatures at around 150 °C. The use of the brine for heating purposes also consists of another alternative.

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