



# Human Mars Entry, Descent, and Landing Architecture Study: Phase 3 Summary

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**Structural Sizing and Optimization**



Joseph Garcia

# OUTER MOLD LINE UPDATE



- **Mid Lift-to-Drag (Mid L/D) vehicle being considered by NASA to land large payloads on the surface of Mars**
- **During Entry, Descent, and Landing Architecture Study (EDLAS) phase 3, Mid L/D conceptual design advanced significantly**
  - Updated outer mold line (OML) shape
  - Conducted packaging feasibility study
  - Completed preliminary vehicle structure design and mass sizing

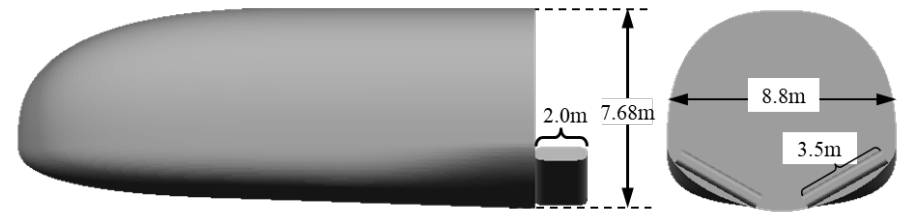
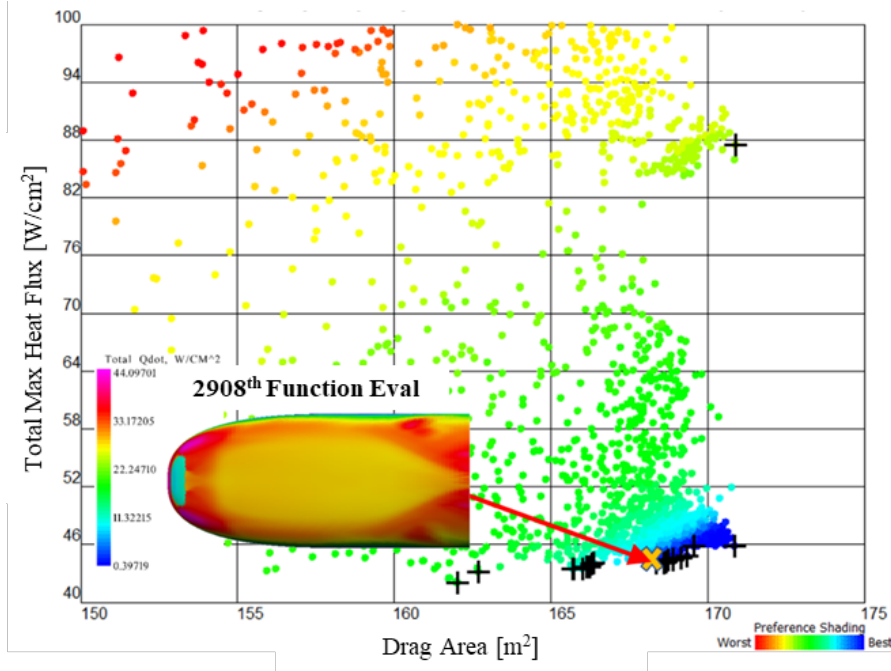


- **Co-Optimization Blunt-body Re-entry Analysis (COBRA)** has been used by NASA for the past decade to arrive at a shape for the Mid L/D rigid vehicle (MRV)
  - Goal to minimize surface heating, maximize drag area ( $C_d A$ )
- **Realistic body flap concept allowed integration of OML with body flap shape**

# COBRA Optimization



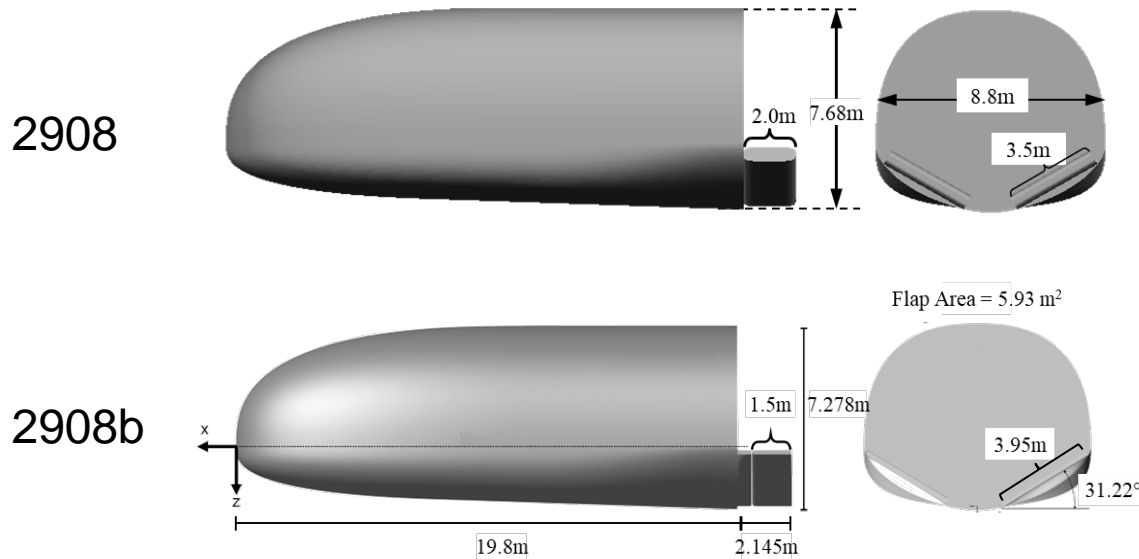
- Pareto front of multi-objective genetic algorithm (MOGA) shapes (left) used to down select CobraMRV2908 shape (right)



# COBRA Optimization



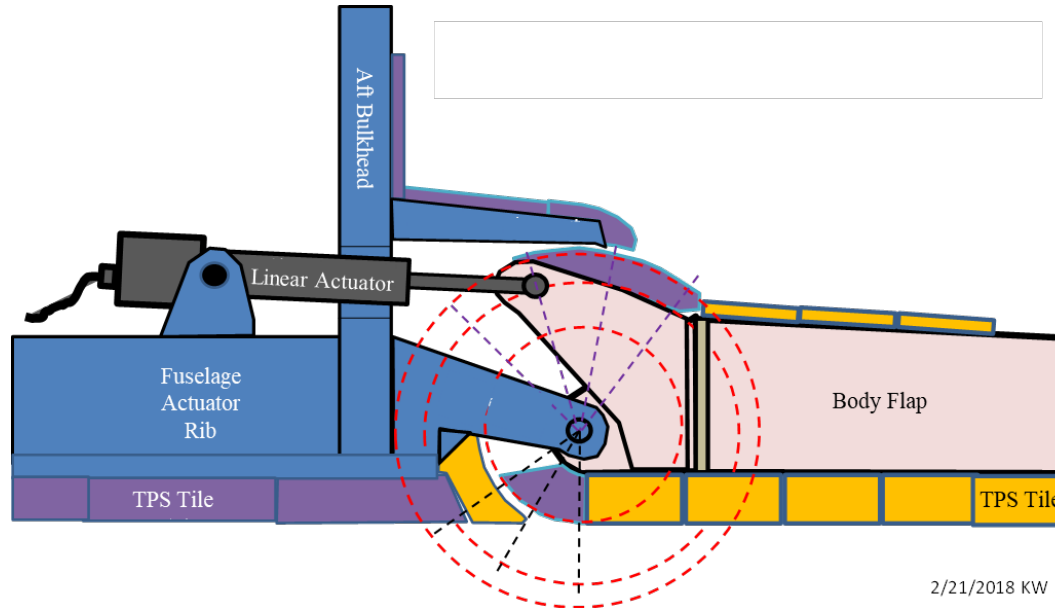
- **2908 shape was modified to 2908b**
  - Allowed fit within SLS 10m shroud (Ø9.1 m inner volume)
  - Reduced high heating and flow separation on body flaps



# Body Flap Concept



- **Conceptual design for body flap structure and actuators enabled more realistic modelling**
  - Below concept was based on Space Shuttle Orbiter design

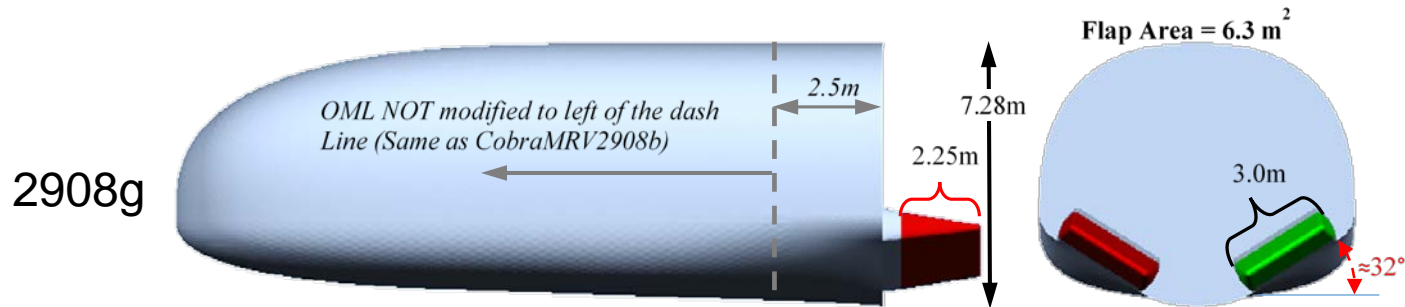




# COBRA Iteration



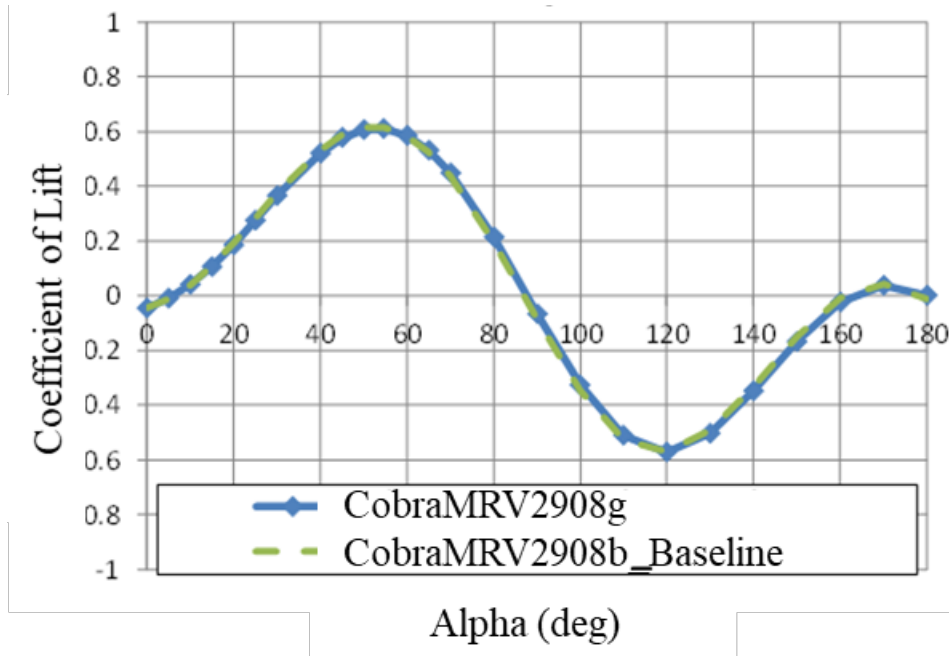
- **2908c → 2908d → 2908e → 2908f → 2908g**
  - Re-lofted aft 2.5 m of OML to smooth body flap transition
  - Changed to trapezoidal flaps
  - Increased cant angle and planform area of flaps
  - Increased aft body base corner radii to reduce heating



# 2908g Comparison



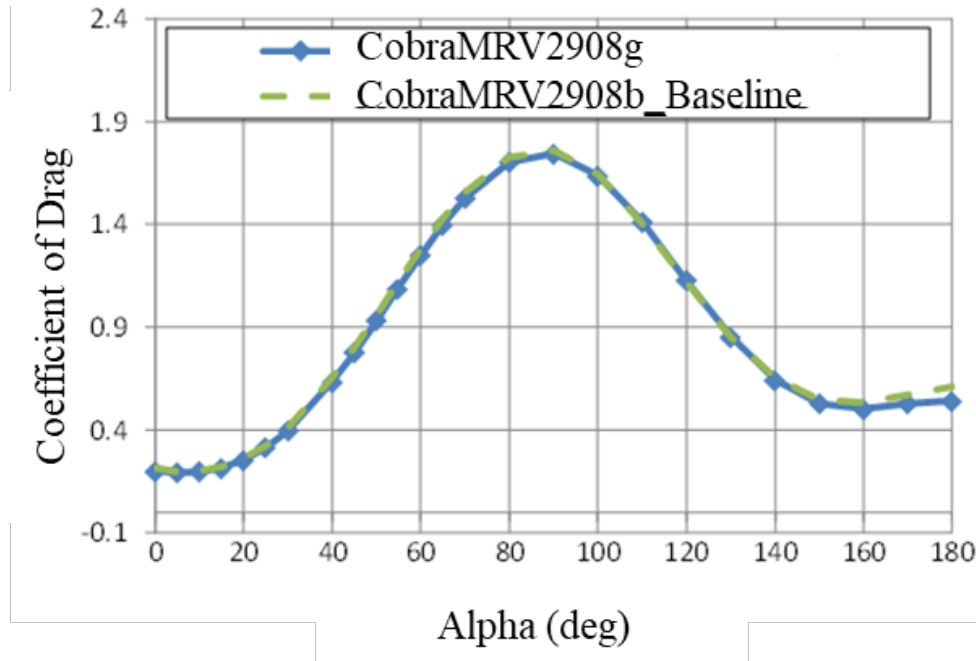
- Used CBAERO Newtonian aerodynamic tool to compare 2908g to 2908b
  - Similar Coefficient of Lift



# 2908g Comparison



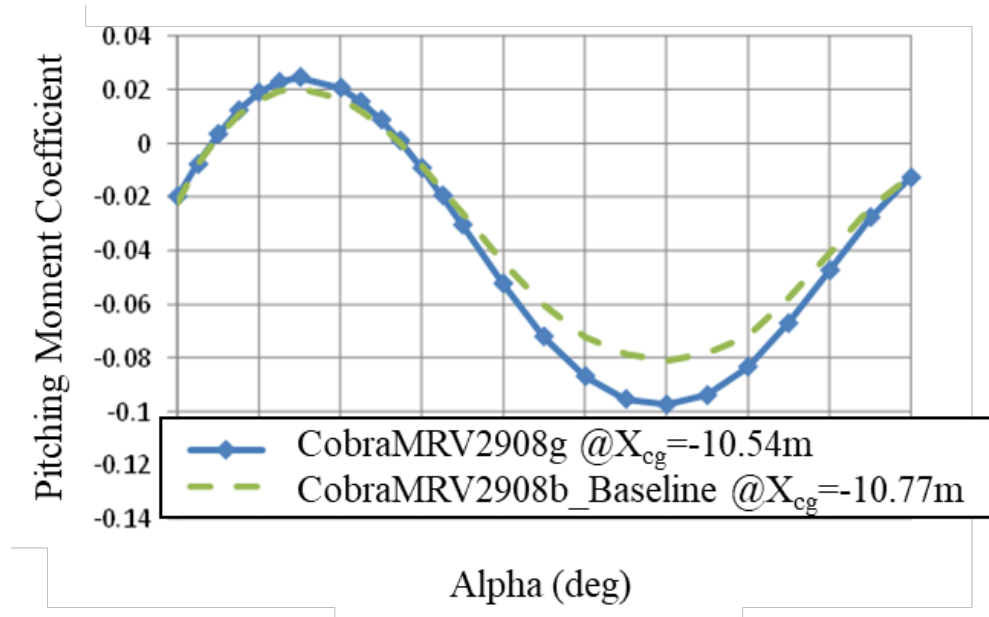
- Used CBAERO Newtonian aerodynamic tool to compare 2908g to 2908b
  - Similar Coefficient of Drag



# 2908g Comparison



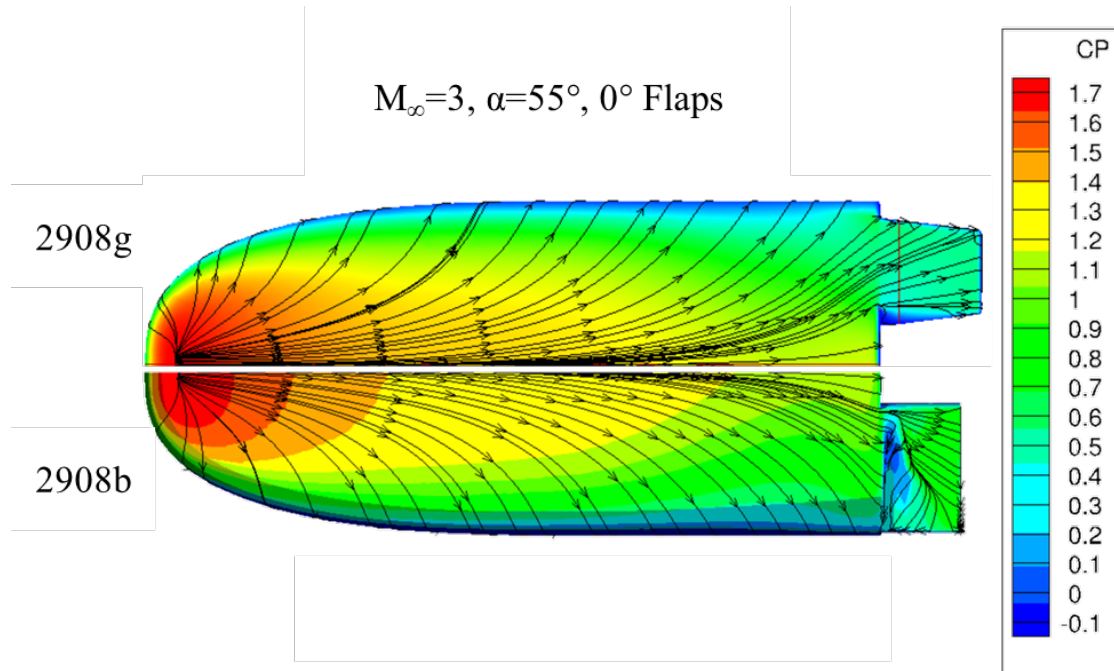
- Used CBAERO Newtonian aerodynamic tool to compare 2908g to 2908b
  - Improved pitching moment coefficient at high angles of attack



# 2908g Comparison



- Used Kestrel computational fluid dynamics software to verify flow improvements
  - Improved flow onto body flaps





Joseph Amar, Holly Newton, Zachery Wiens

# MANIFEST PACKAGING



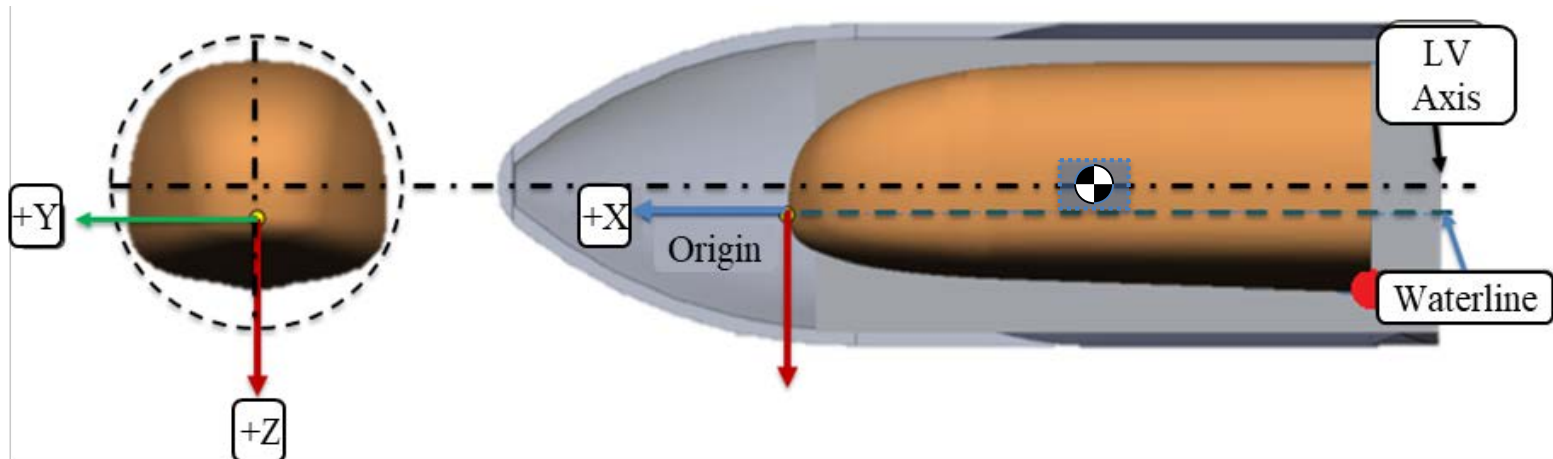
- **Assumed 22T Payload manifest for Crew Expedition 1 Mission**
  - Cargo-1, Cargo-2, Crew-1
  - Common items across manifest would be identically placed
- **Used the 2908G OML, manifest packaging for Cargo 2 for sizing**
  - Modeled frame to match OML form
- **Creo Parametric software used to conduct packaging and CG estimation**

# CG Requirement



- CG should be mid-body of MRV, along launch vehicle (LV) axis

Axis	Minimum (m)	Maximum (m)
X	-10.747	-10.347
Y	-0.050	0.050
Z	-1.100	0.000

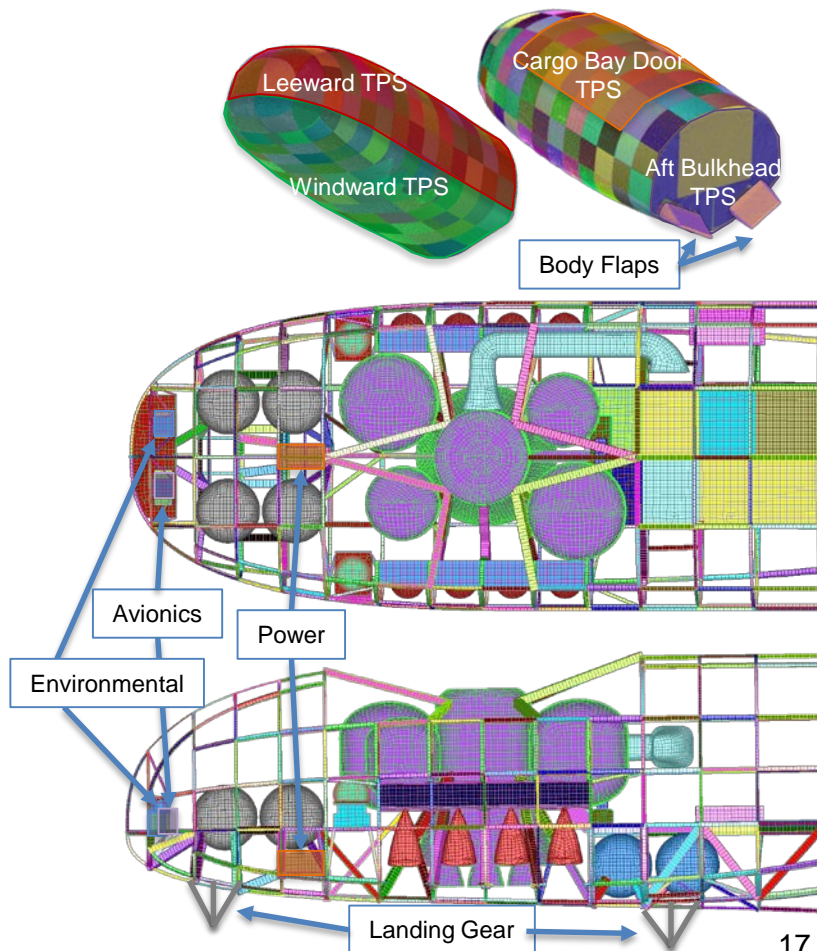




# Expedition 1 Common Subsystems



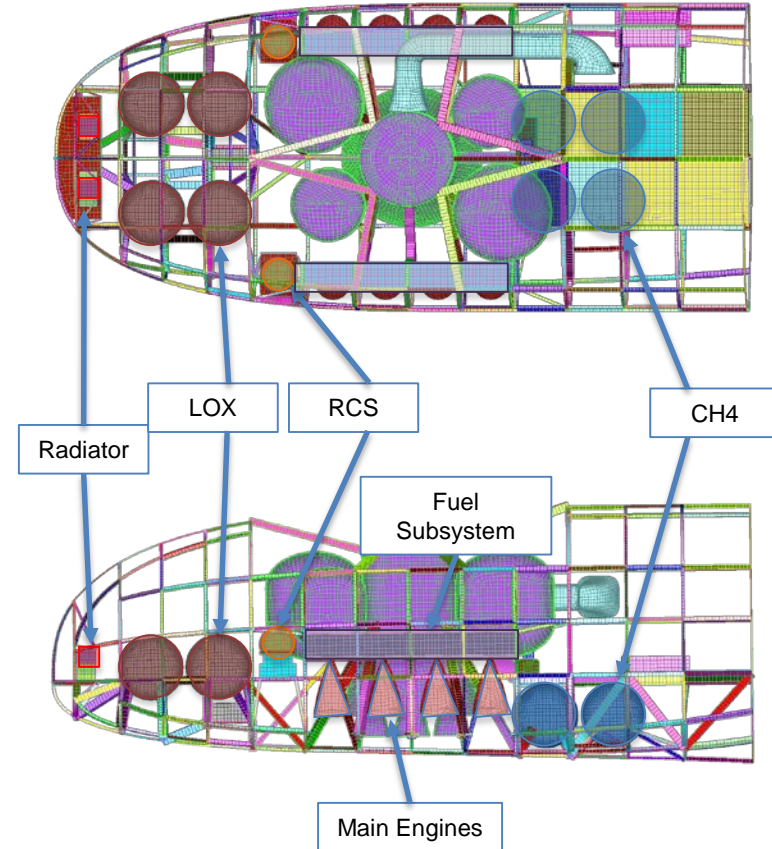
Component	Qty.	Mass Each (kg)	Mass Total
<b>Thermal Protection System (TPS)</b>			<b>4624</b>
Windward	1	3590	3590.21
Aft Bulkhead	1	65	64.75
Aft Door	1	73	73.40
Leeward	1	653	653.13
Cargo Bay Doors	2	121	242.50
<b>Acoustic Thermal Protection – Dist.</b>			<b>635</b>
IML Blankets	1	459	458.80
IML Radiant Barrier - MLI	1	65	65.10
Lightning Protection	1	111	110.90
<b>Power</b>			<b>470.00</b>
Power Distribution	1	400	400.00
Power Cable (1 km) spool	1	70	70.00
<b>Body Flaps</b>	<b>2</b>	<b>298</b>	<b>595.40</b>
<b>Landing Gear</b>	<b>3</b>	<b>388</b>	<b>1164.60</b>
<b>Avionics</b>			<b>333.00</b>
Command and Data Handling	1	141	141.00
Communications and Tracking	1	76	76.00
Guidance, Navigation, & Control	1	116	116.00
<b>Environmental Cabin</b>			<b>212.50</b>
Active Cooling Loops	1	200	200.00
Heaters	1	13	12.50



# Expedition 1 Common Subsystems



Component	Qty.	Mass Each (kg)	Mass Total
<b>In-Space Radiator</b>	<b>1</b>	<b>191</b>	<b>191</b>
<b>Other – Dist.</b>			<b>379</b>
Purge System	1	301	301
Umbilicals Interfaces	1	78	78
<b>Methane + Tank</b>	<b>4</b>	<b>1080</b>	<b>4322</b>
<b>LOX + Tank</b>	<b>4</b>	<b>3274</b>	<b>13095</b>
<b>Fuel Subsystem</b>	<b>2</b>	<b>328</b>	<b>656</b>
<b>RCS Prop Distribution</b>	<b>2</b>	<b>205</b>	<b>411</b>
<b>RCS Cluster</b>	<b>2</b>	<b>506</b>	<b>1013</b>
<b>Main Engine</b>	<b>8</b>	<b>250</b>	<b>2000</b>
<b>Aft Ramp System</b>			<b>469</b>
Strut	2	8	16
Hard stop	1	49	49
Hinges	1	22	22
Perimeter Seal	1	41	41
Ramp	1	175	175
Mechanism	1	166	166
<b>Cargo Bay Doors Mech.</b>			<b>360</b>
Power Drive Units	10	10	96
Rotary Actuators	8	6	46
Latches	22	8	168
Hinges	16	3	50



# Expedition 1 Payload Manifest



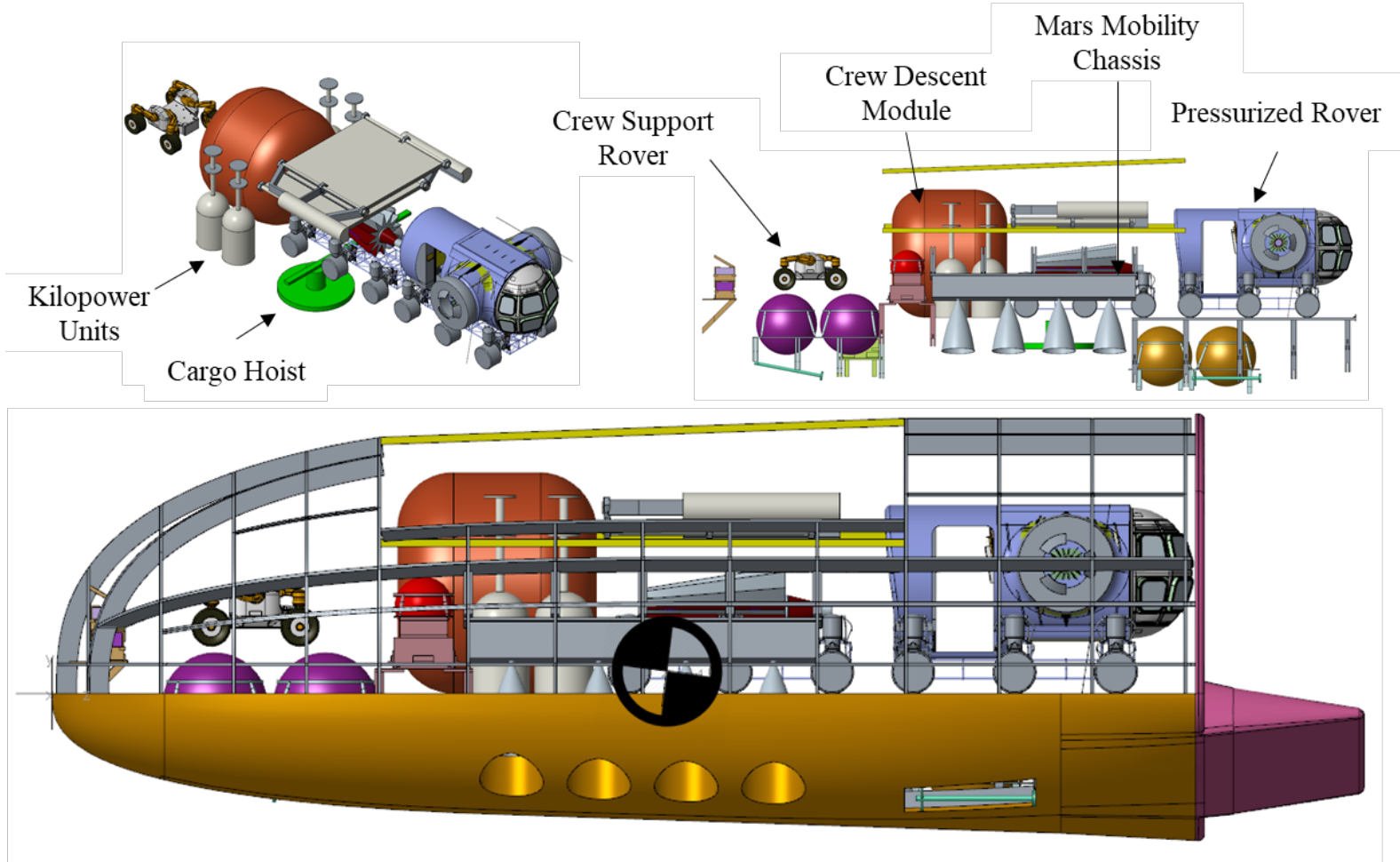
- **Cargo-1**

<b>Manifested Item</b>	<b>Mass (kg)</b>	<b>Qty</b>	<b>Mass (kg)</b>
<b>Kilopower, 10 kW each</b>	1544	5	7720
<b>Power Management/Distribution</b>	400	1	400
<b>Power cable (1 km) spool</b>	70	1	70
<b>Crew Support Rover</b>	1225	1	1225
<b>Cargo Hoist</b>	600	1	600
<b>Crew Descent Module</b>	3516	1	3516
<b>Mars Mobility Chassis</b>	2457	1	2457
<b>Pressurized Rover</b>	6021	1	6021
<b>Total Payload Mass</b>			22009

# Cargo-1 Packaging



Zachery Wiens



# Expedition 1 Payload Manifest



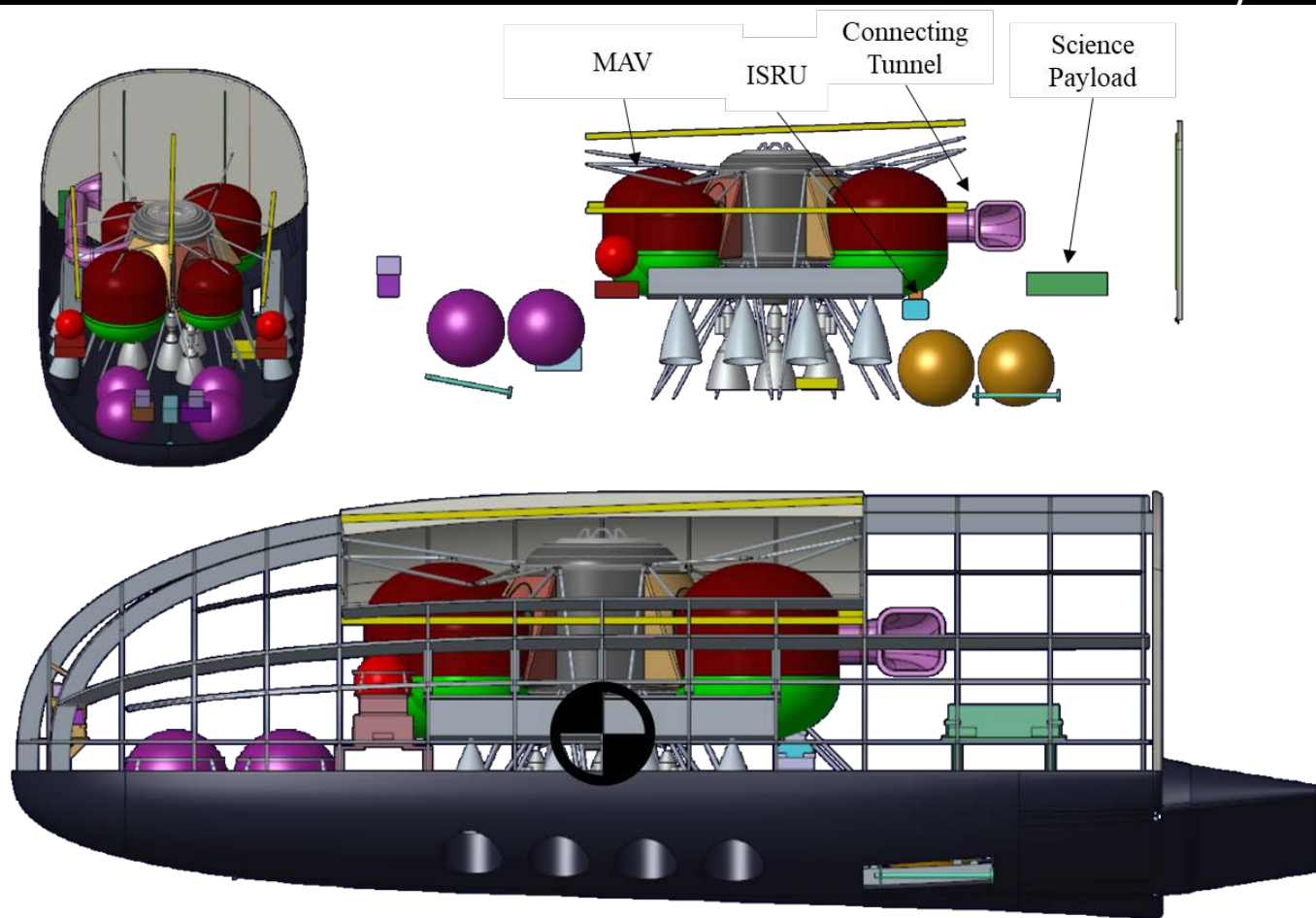
- **Cargo-2**

<b>Manifested Item</b>	<b>Mass (kg)</b>	<b>Qty</b>	<b>Mass (kg)</b>
<b>Atmospheric Production Plant</b>	1032	1	1032
<b>Part of ISRU radiator mass</b>	478	1	478
<b>ISRU Deployment</b>	130	1	130
<b>Power Management/Distribution</b>	400	1	400
<b>Power cable (1 km) spool</b>	70	1	70
<b>Connecting Tunnel</b>	237	1	237
<b>Allocated Science Payload</b>	1000	0.2	200
<b>MAV (5 sol, wet)</b>	18868	1	18868
<b>Part of MAV Radiator</b>	212	1	212
<b>MPS Tank Cryocoolers/BAC charged to MAV</b>	141	1	141
<b>MDM-to-MAV Adapter</b>	200	1	200
<b>Total Payload Mass</b>			21968

# Cargo-2 Packaging



Holly Newton



# Expedition 1 Payload Manifest



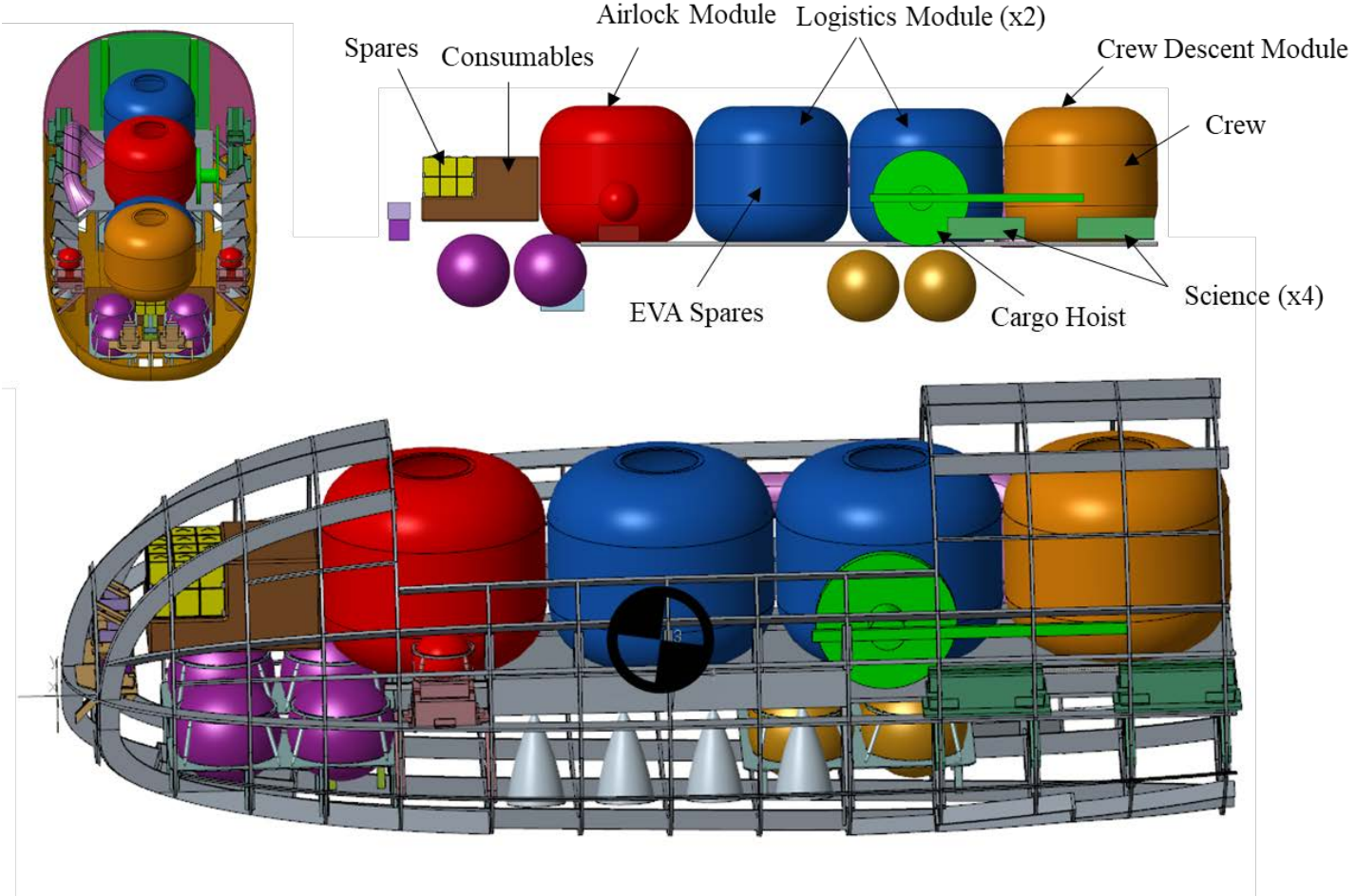
- Crew-1**

Manifested Item	Mass (kg)	Qty	Mass (kg)
Crew (each)	100	4	400
Power Management/Distribution	400	1	400
Power cable (1 km) spool	70	1	70
Cargo Hoist	600	1	600
Logistics Module (Dual Hatch 3500 kg capacity)	2600	2	5200
Crew Descent Module	3516	1	3516
Airlock Module	3500	1	3500
Connecting Tunnel	237	1	237
Consumables (4.02 kg/person/sol + 97.57)	4.02	163	2719
Spares and Other Logistics (2.946 kg/sol + 2112.9 kg)	2.946	163	2593
Maintenance Equipment	70	1	70
EVA Suit + Primary Life Support System	693	1	693
Launch-Entry Assembly Suits	104	1	104
Spares (1.73 kg/sol/crew + 796.8)	4 crew	163	1079
Allocated Science Payload	1000	0.8	800
			21981

# Crew-1 Packaging



Joseph Amar





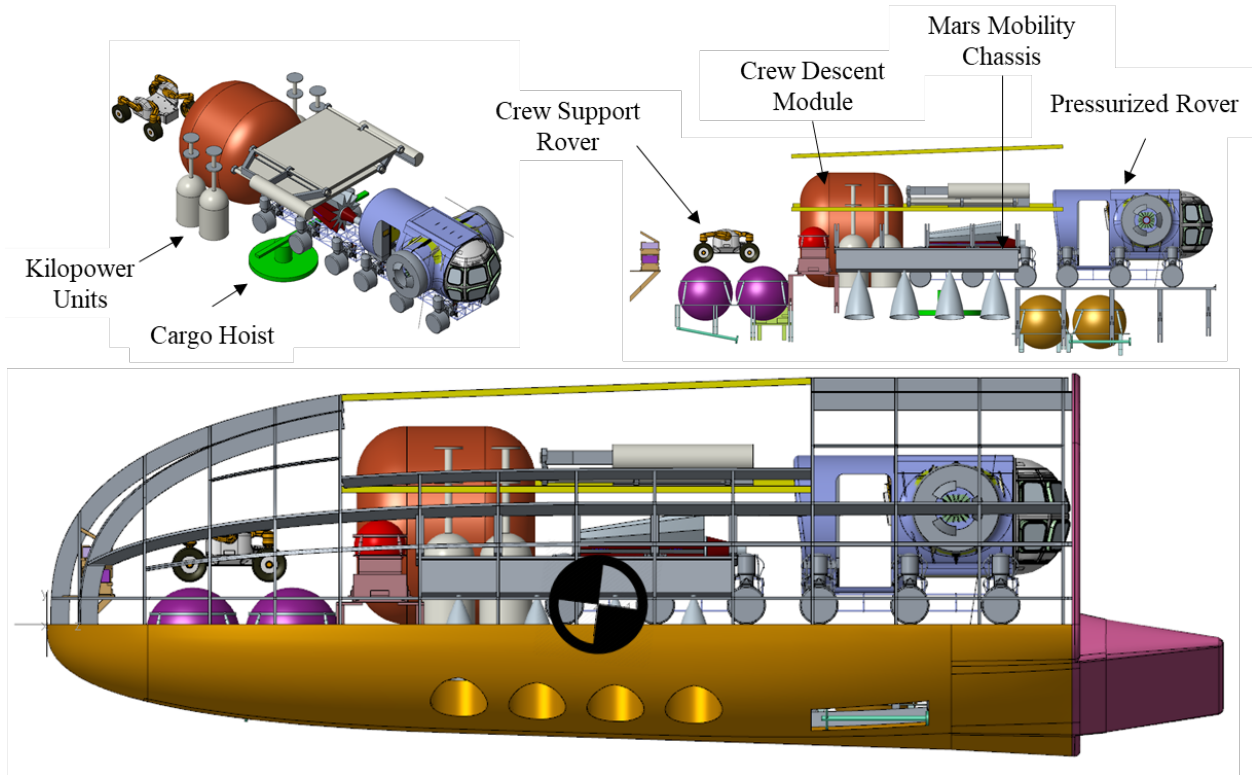
# CG Cargo 1



Zachery Wiens

- **Calculated CG with all Cargo-1 items:**

- X: 10.557 m
- Y: -0.0139 m
- Z: 0.393 m



# CG Estimations



- All configurations meet CG requirements

Manifest	$X_{CG}$ (m)	$Y_{CG}$ (m)	$Z_{CG}$ (m)
Cargo-1	-10.557	-0.014	-0.393
Cargo-2	-10.446	0.001	-1.009
Crew-1	-10.380	-0.006	-0.013



Damien Calderon

# STRUCTURAL SIZING AND OPTIMIZATION

# Initial Assumptions



- **Used the 2908G OML, manifest packaging for Cargo 2 for sizing**
  - Modeled frame to match OML form
  - Modified substructure to support cargo packaging, dynamic constraints
- **MSC Nastran used as a linear solver (SOL 101)**
- **Collier Research Hypersizer used for sizing optimization**
- **All sized structure assumes Aluminum 2024 construction**

# Load Cases



## Four load cases envelope the design:

### 1. Earth Launch/Ascent

- +5g Axial, +/-2g Lateral
- 0-0.5 psig Vent Pressure

### 2. Mars Entry

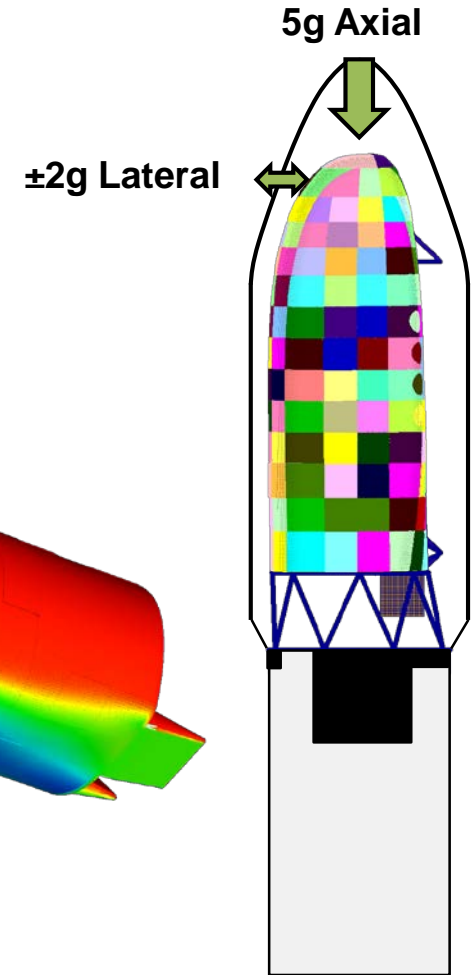
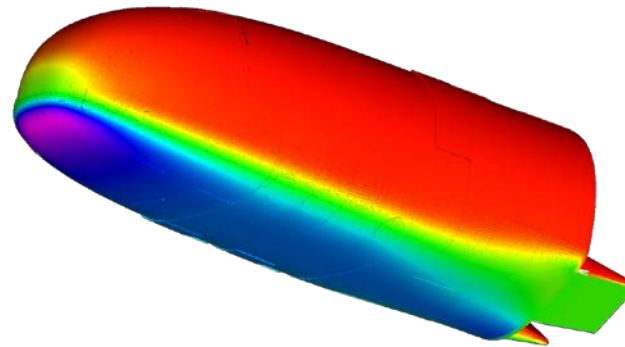
- Peak Dynamic Pressure

### 3. Mars Propulsive Descent

- 800 kN

### 4. Mars Landing

- 3g



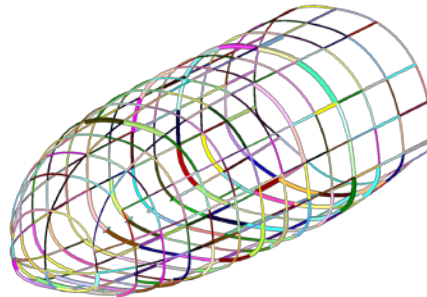
# Structural Architecture



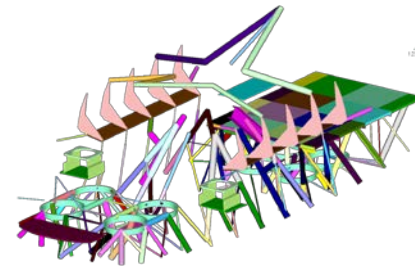
- **Skin, Airframe (Ring, Longeron), Substructure**
- **Components modeled as discrete members, sized independently to allow for optimum mass**



**OML Skin**



**Airframe**

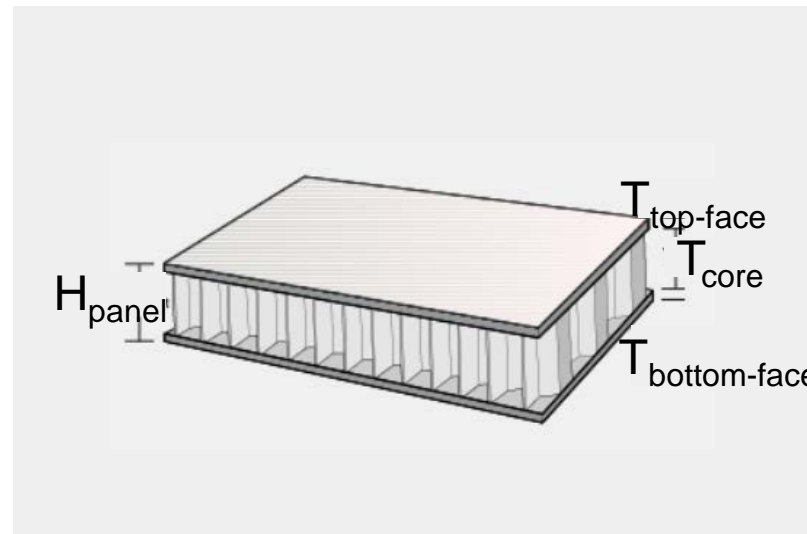


**Substructure**

# Honeycomb Sandwich Panels

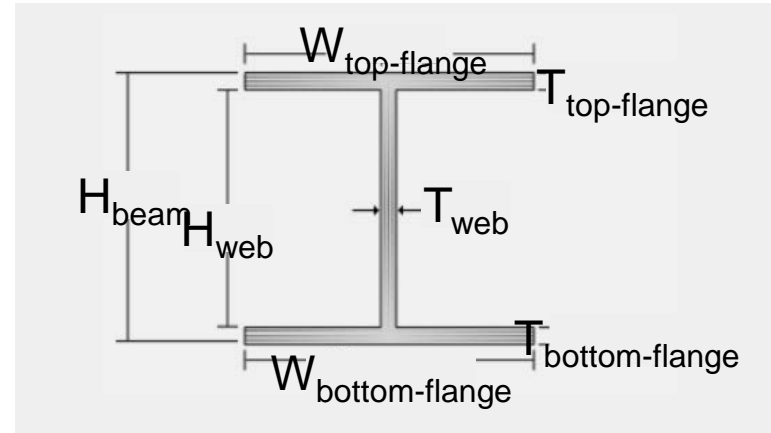
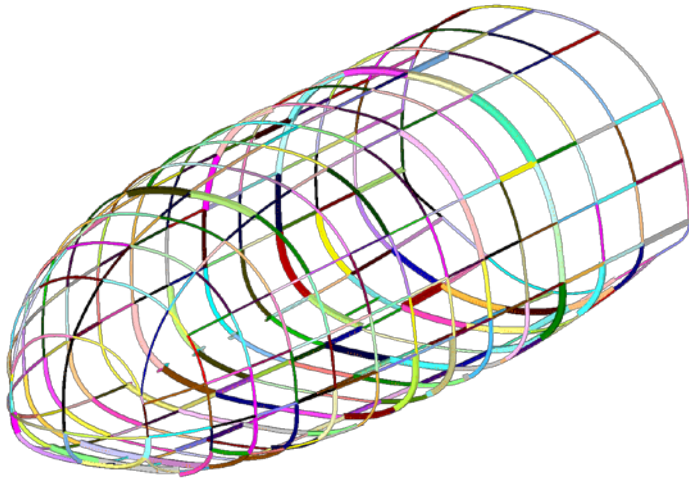


## OML Skin and Cargo Doors



Dimension	Min (mm)	Max (mm)
$T_{\text{bottom}}$	0.3	3.0
$T_{\text{core}}$	20.0	100.0
$T_{\text{top}}$	0.3	3.0

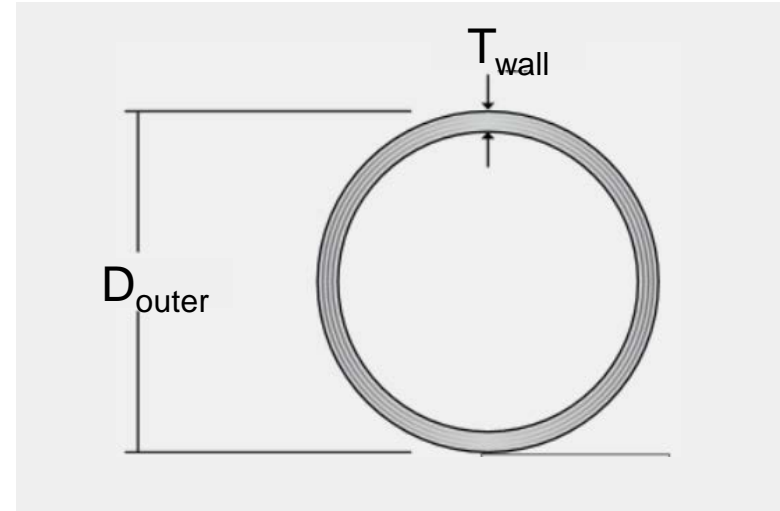
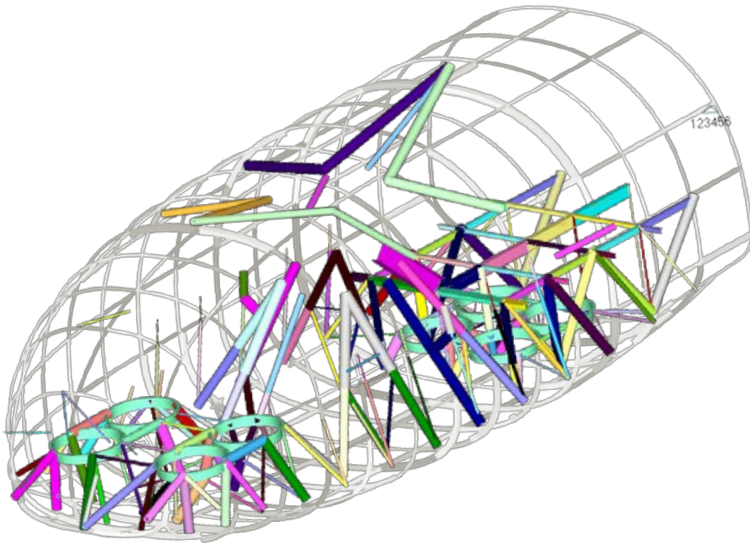
## Longerons and Ring Frame



Dimension	Min (mm)	Max (mm)
$T_{\text{top}}$	2.0	20.0
$T_{\text{web}}$	2.0	20.0
$T_{\text{bottom}}$	2.0	20.0
$W_{\text{top}}$	30.0	200.0
$W_{\text{bottom}}$	30.0	200.0
$H_{\text{beam}}$	30.0	200.0



## Cargo Support Struts

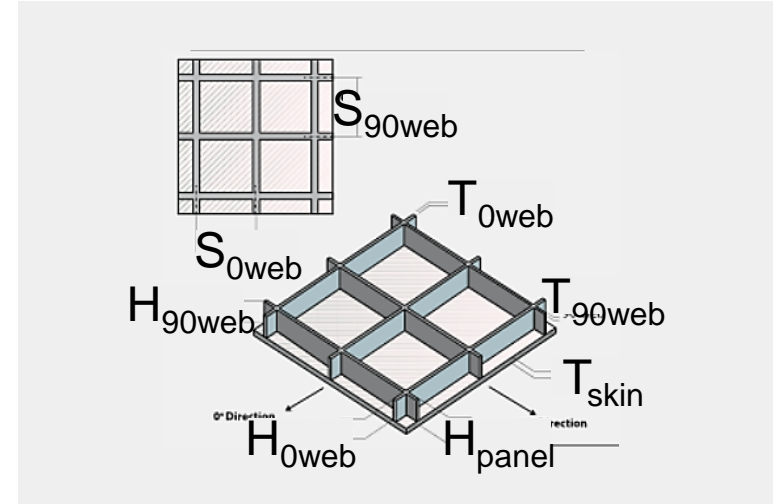
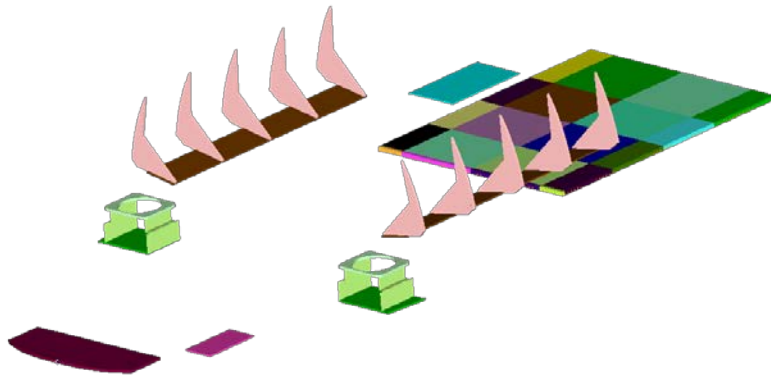


Dimension	Min (mm)	Max (mm)
$D_{outer}$	1.0	15.0
$T_{wall}$	30.0	250.0

# Grid Stiffened Panels



## Substructure



Dimension	Min (mm)	Max (mm)
$T_{skin}$	1.0	10.0
$T_{0web}$	2.0	20.0
$T_{90web}$	2.0	20.0
$H_{0web}$	20.0	100.0
$H_{90web}$	20.0	100.0
$S_{0web}$	50.0	800.0
$S_{90web}$	50.0	800.0

# Basic Mass Results



**Baseline predicted structural mass: 10281 kg**

<b>Assembly</b>	<b>Basic Mass (kg)</b>	<b>20% MGA (kg)</b>	<b>Predicted Mass (kg)</b>
Skin	4111	822	4933
Frame	1483	297	1780
Substructure	2973	595	3568
<i>Total Structural Mass</i>	<i>8567</i>	<i>1714</i>	<i>10281</i>



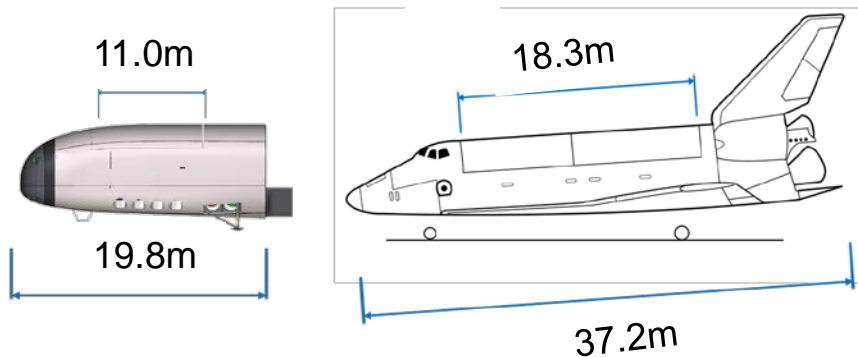
**BACKUP**

# Cargo Bay Doors (CBD)



Theodore Christian/JSC

- Orbiter payload bay door (PLBD) system actuator was 0.66 t (1446.2 lbm)
- Assume system mass scales with area PLBD:CBD ~ 1.83:1
- Estimated mass of CobraMRV CBD mechanisms and associated structure is 0.36 t (793.7 lbm)



## Predicted CobraMRV

Major Components	
Power Drive Units	10
Rotary Actuators	8
Latches	22
Hinges	16

Total number of parts: 56

- **Assumptions**

- Single Use Deployment
- Vent Pressure of 0.5psi



- **Design Background – C130 Hercules cargo ramp**

- Frangible nuts to secure door, blown upon deployment
- Pin/Hammer system to encourage door deployment
- Struts, hard stop to control drop of door
- Pin system to release support ramp

# Aft Door/Ramp (cont)



Amy Quartaro/JSC

- Estimated door/ramp mass ~177 kg (389 lbs)
- Estimated mechanisms and seal mass ~209 kg (460 lbs)

