

Advanced Measurement Systems to evaluate CSP Plants

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Knowledge for Tomorrow



Outline

- Challenges for measurements in CSP power plants
- Parabolic Trough Fields:
 - Airborne predictions of optical field performance
 - Hydrogen accumulation in parabolic trough receivers
 - Cloud shadow prediction in the solar field
- Solar Tower
 - Optical quality of heliostat field and flux distribution on receiver
 - Air return ratio in open volumetric receiver systems
- Summary

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Challenges for measurements in CSP power plants

- Measurement object extended or distributed over several square miles
- Limited access (e.g. tower)
- Measurement should not disturb operation
- Sensors preferably non invasive
- High measurement precision requirements



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QFly – airborne prediction of the optical performance of parabolic trough collector fields

QFly UAV

Failure Detection, Quality Control, Optimization

High resolution

Survey

Thermo

Mirror shape
HCE position

Mirror shape
Alignment
Torsion
Tracking

Defective HCEs
Heat loss

50 MW PTC solar field (Andasol I)

25%/day

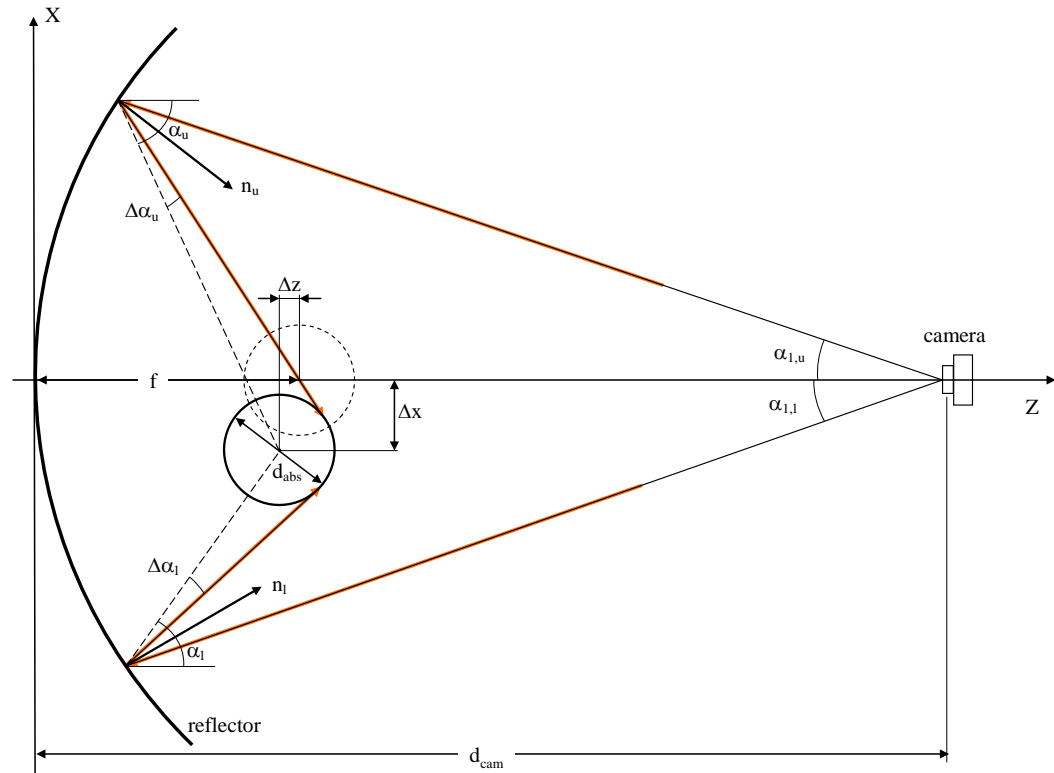
50%/day

5%/day



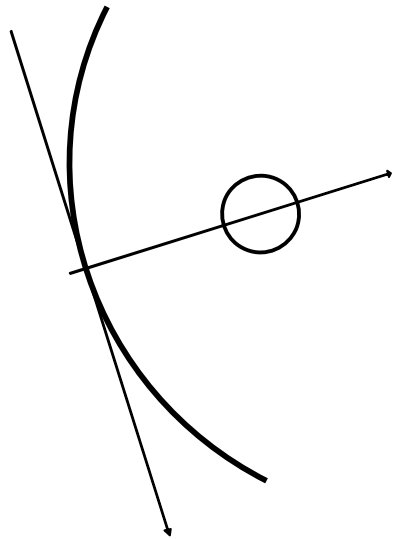
2. Qualification of Concentrators

Deflectometry



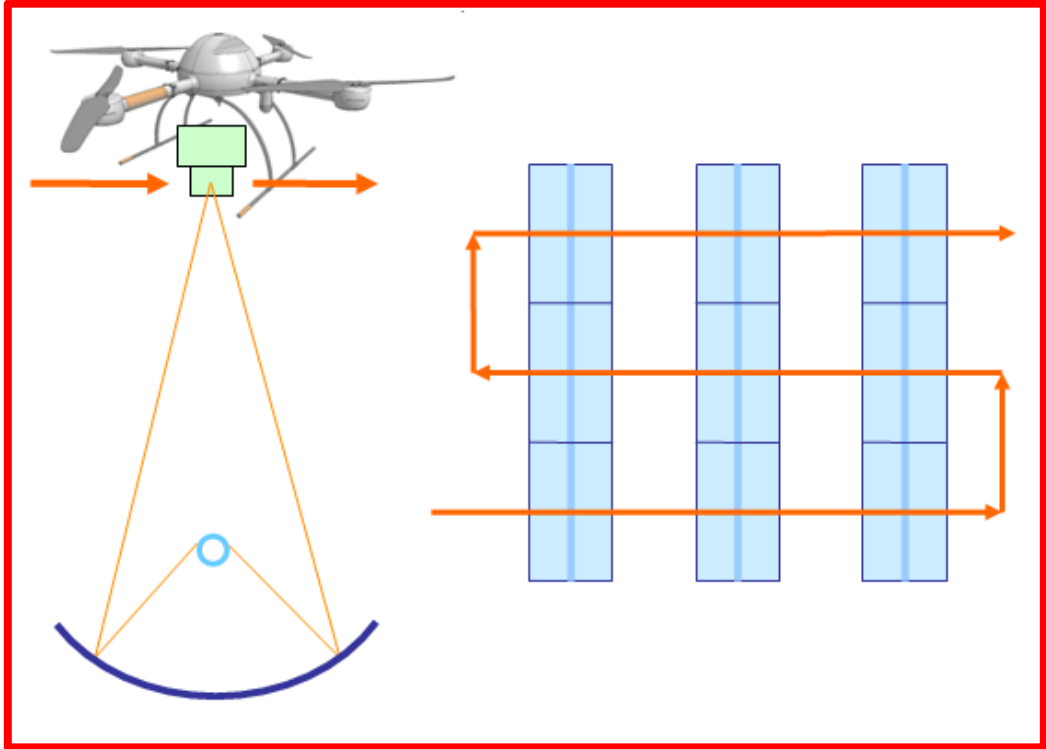
2. Qualification of Concentrators

Deflectometry – Image Acquisition



QFly measurement principle

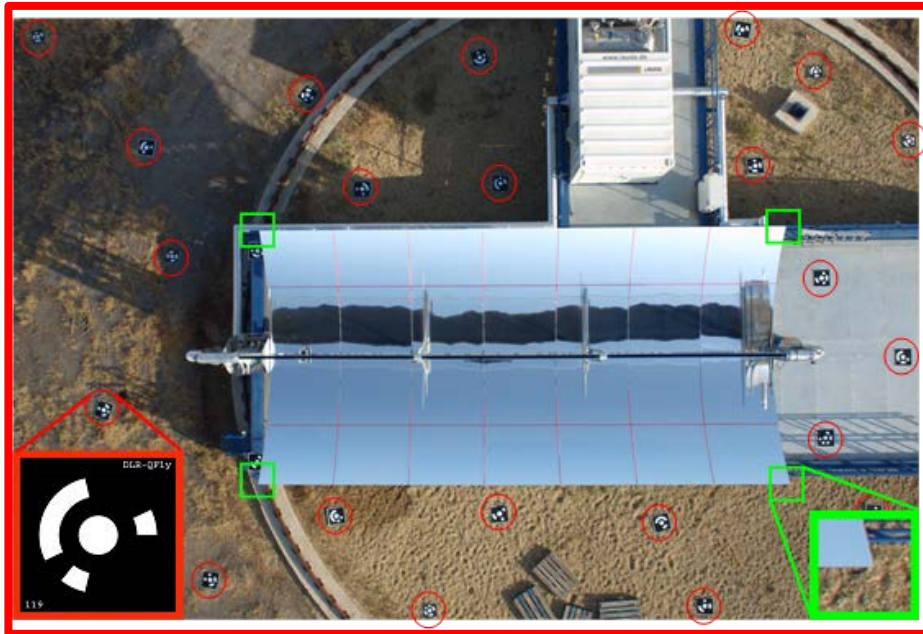
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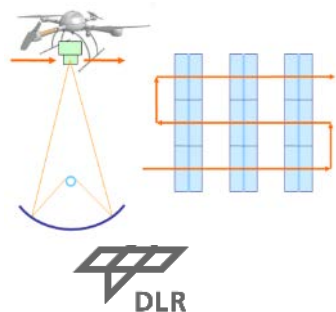
- Plan for Flight Route using GPS waypoints
- Aerial images showing absorber tube reflex
- Scaling/reference system for close-range photogrammetry



QFly measurement principle

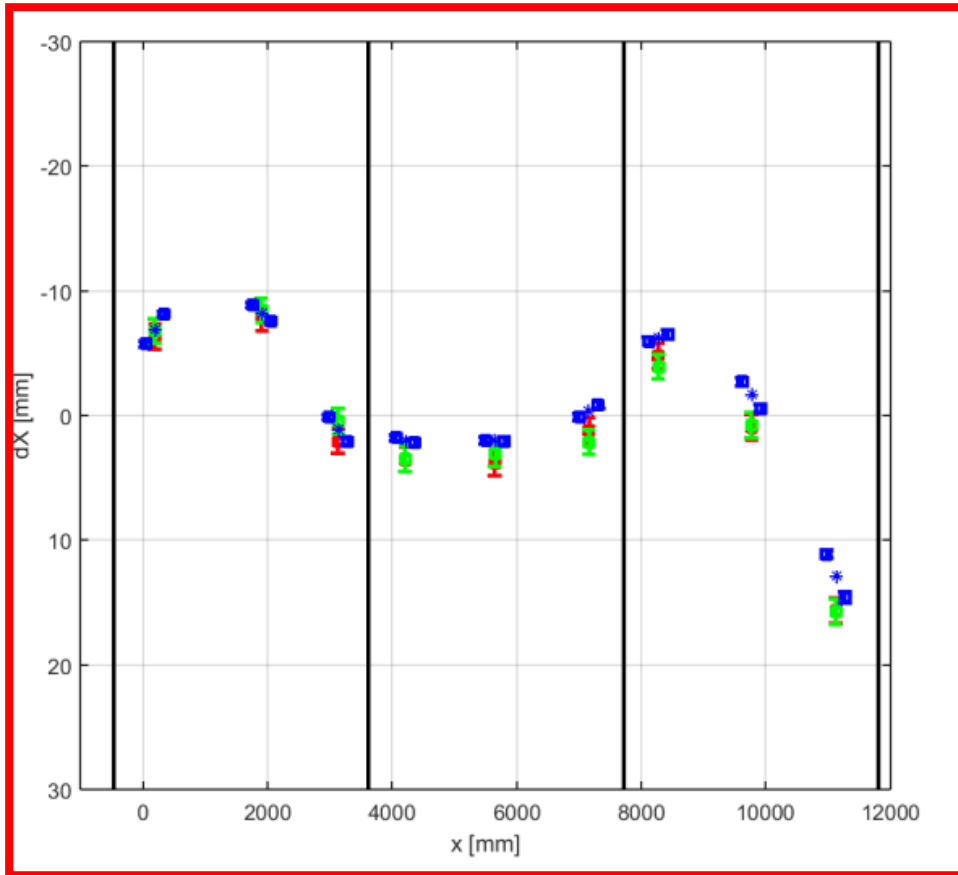


- Calculation of camera positions relative to each collector via photogrammetry
- Artificial, coded and natural markers
- Accuracy of 3D coordinates ~ 5 mm



QFly measurement principle

3

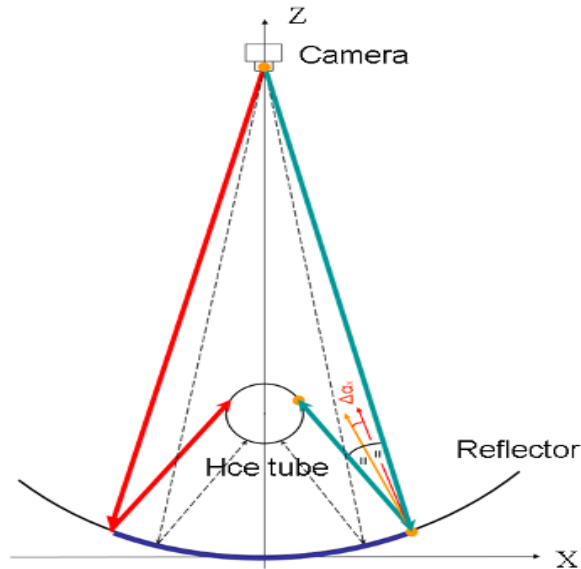


- Calculation of lateral and vertical HCE deviation from focal line via photogrammetric approach
- Deviations Q_{fly} to reference:
 - RMS $dX < 2.0$ mm

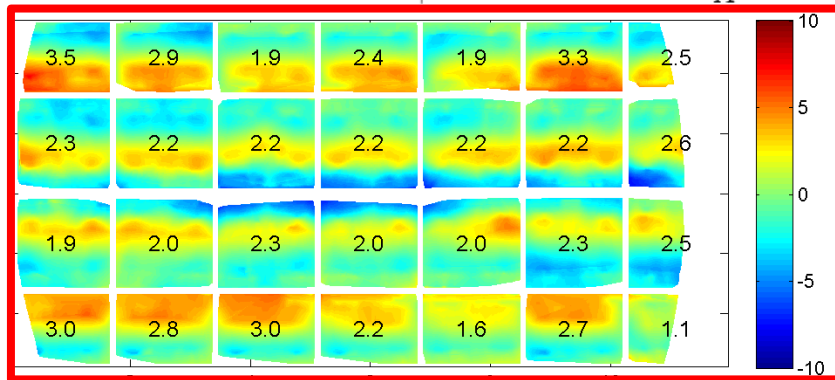


QFly measurement principle

4

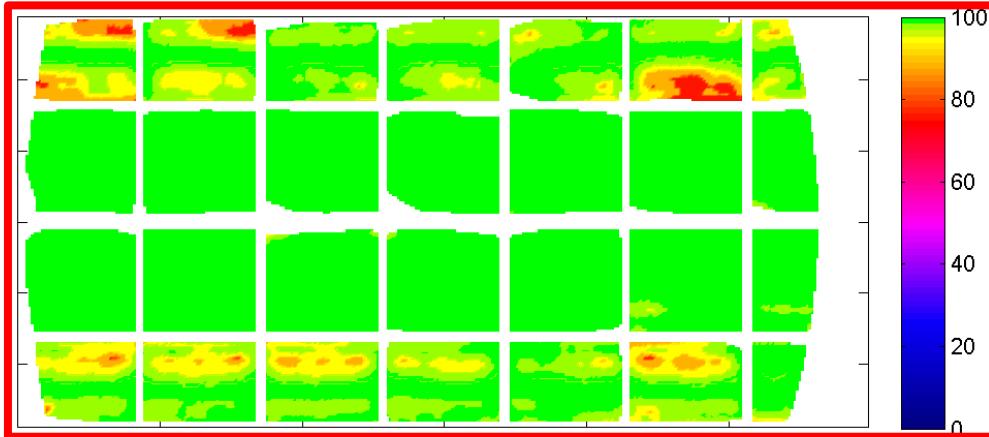


- Calculation of slope deviations in curvature direction (SD_x , in mrad) from absorber reflex, camera positions and absorber position



QFly measurement principle

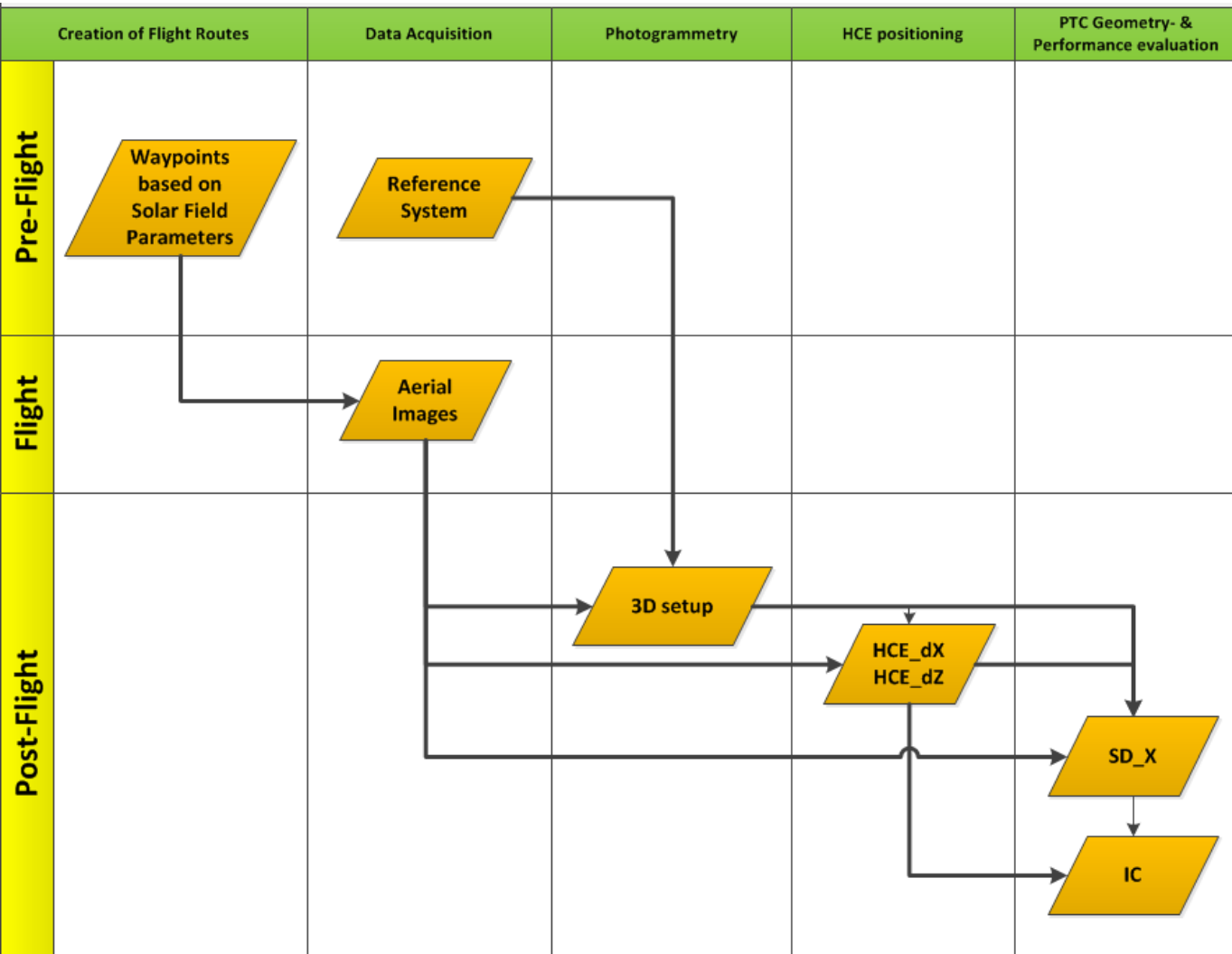
6



- Intercept factor via ray-tracing based on measured geometry
- Includes blocking and shading effects
- Assumptions on other error sources



QFly measurement principle



Effort per collector (SCA) 150 m:

2 hours

0.5 hours

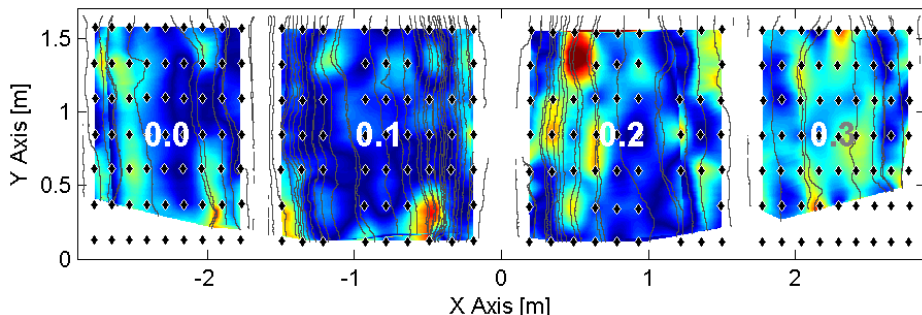
4 hours



Validation

Optical:

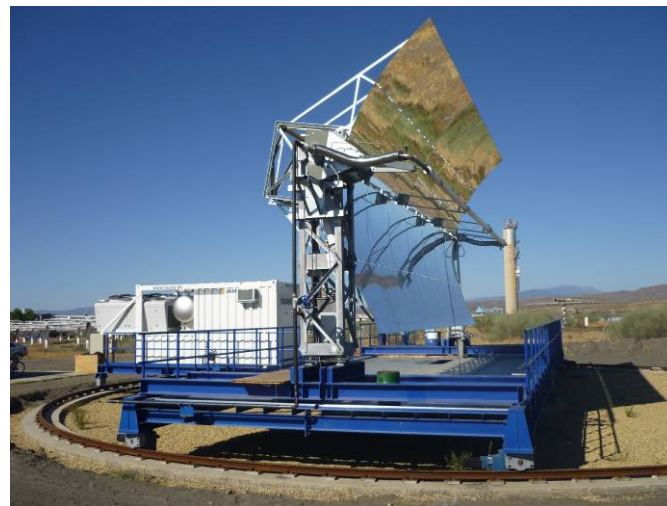
- Comparison with reference data from photogrammetry
- Mirror:
 - Difference of SDx
RMS values < 0.4 mrad (due to limited spatial resolution of photogrammetry)



- Absorber tube position
RMS of differences:
 - < 2.0 mm horizontal
 - < 2.1 mm vertical

Thermal:

- Comparison with thermal efficiency of EuroTrough module on Kontas test-bench (PSA Almeria)
- Good agreement between η_{opt} :
 - via thermal measurement
 - via QFly measurement

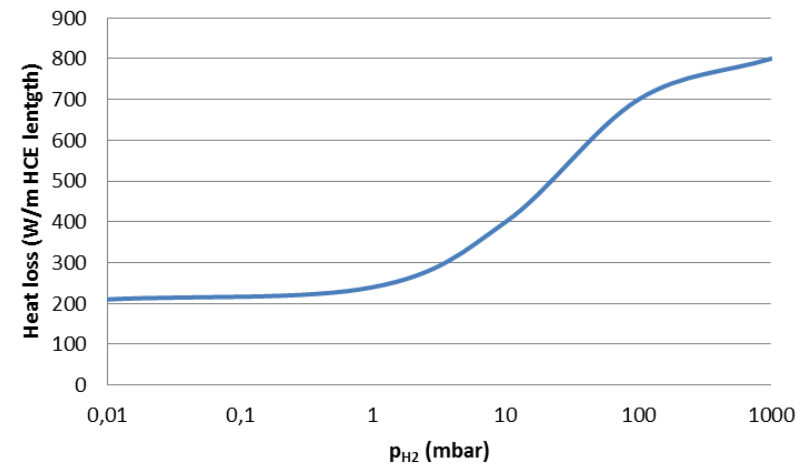
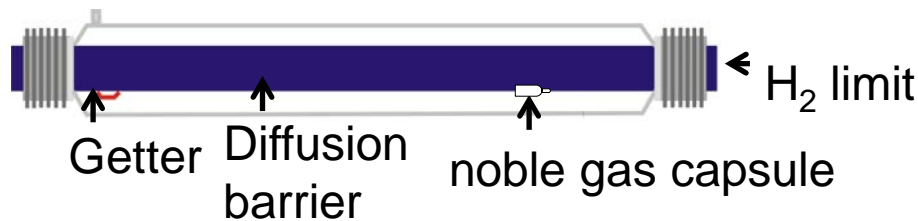


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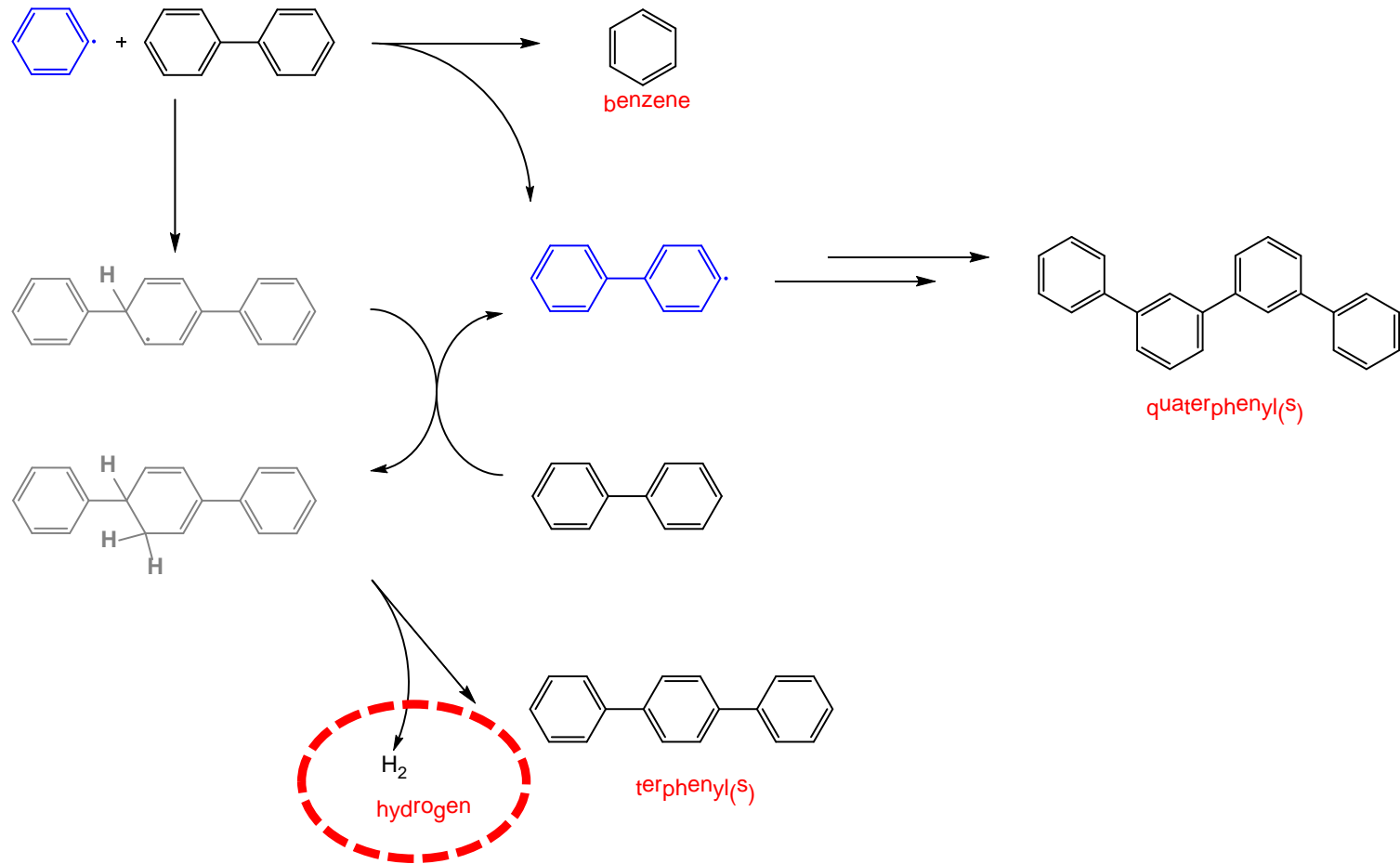
Hydrogen accumulation in parabolic trough receivers: Effects and Counteractions



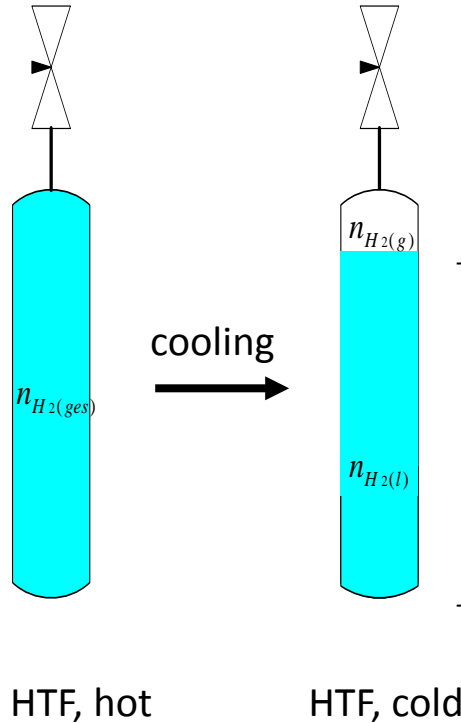
- Hydrogen accumulation would deteriorate vacuum insulation of receivers
- Counteractions against hydrogen in receiver (getter, barrier coating) designed for H₂ limit concentration / pressure in heat transfer fluid (HTF)
- H₂ monitoring and HTF processing focussed on H₂ removal, required to keep H₂ level below deterioration limit



Thermal aging of HTF causes slow hydrogen formation



Measurement of hydrogen in oil samples in solar field



Hydrogen in gas phase

$$n_{H_2(g)} = \frac{p_{H_2} \left(V_{ges} - \frac{m_{HTF}}{\rho_{HTF}} \right)}{RT}$$

$$p_{H_2} = p_{ges} x_{H_2} \quad x_{H_2} \text{ via GC}$$

Hydrogen in liquid phase

$$p_{H_2} = \frac{n_{H_2(l)}}{n_{HTF}} H_{H_2}$$

$$n_{H_2(l)} = \frac{p_{H_2} n_{HTF}}{H_2}$$

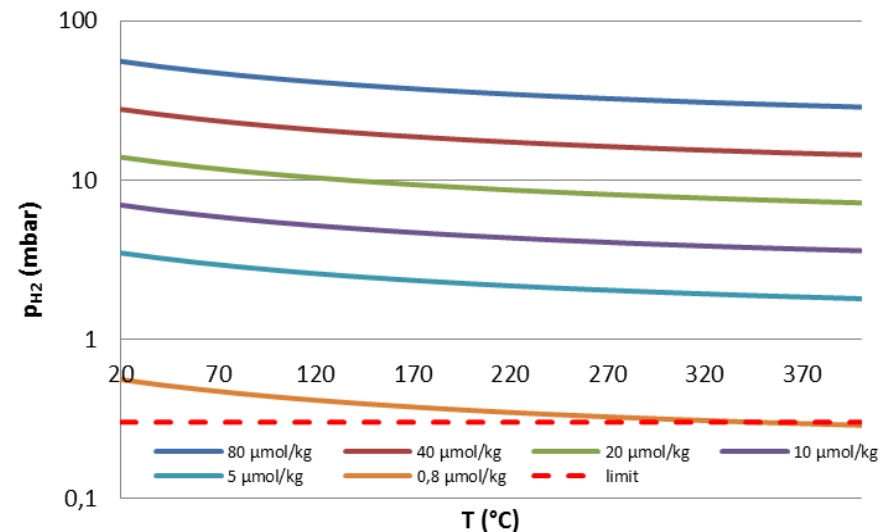
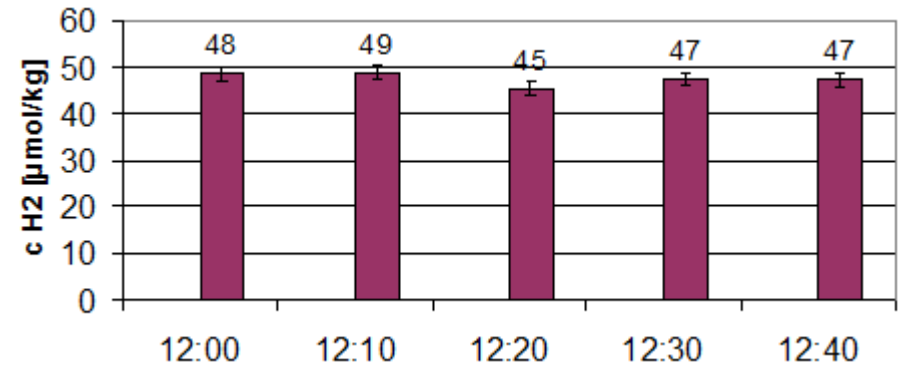
- Sampling of liquid and gas phase with steel cylinders inline (pressurized & hot)
- Analysis of (all) dissolved gases offline (lab)



Gas Content: Concentration vs. Pressure

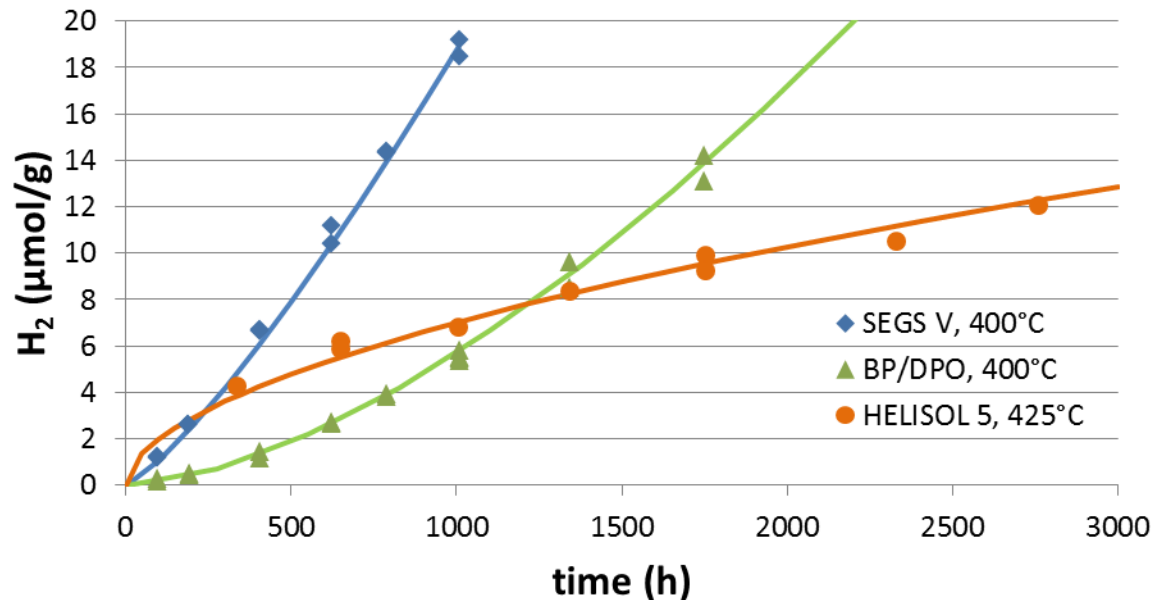
- Direct result of measurement: $\mu\text{mol/kg}$ hydrogen in oil
- Receiver manufacturer's hydrogen limit: e. g. 0.3 mbar
- Conversion from concentration to pressure via Henry coefficient (gas solubility, H , from gas dissolution experiments)

$$p_{\text{H}_2} = H_{\text{H}_2}(T) * x_{\text{H}_2}$$



Hydrogen in Heat Transfer Fluid

Reduced Formation using Silicone Fluids?



- Eutectic mixture of biphenyl (BP) and diphenyl oxide (DPO) forms hydrogen at increasing rate on prolonged operation
- New silicone fluids form less hydrogen on prolonged operation at elevated temperature



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Cloud shadow prediction in CSP Plants

Optimize energetic and financial yield & plant life time

- CSP plant operation involves decisions, e.g.
 - selection of operation mode
 - tower plants: mirror focus control (avoid fast temperature changes of receiver, avoid overload dumping with dynamic aim-point selection)
 - trough plants: individual heat transfer fluid mass flow in different parts of the solar field



Cloud Movement Analysis

irradiance maps with high temporal and spatial resolution (nowcasts and live information) from cloud camera system

ground observation from camera on solar tower (90 m)



- Challenges:
 - High variability
 - Complex cloud formation/motion
- Captured at PSA
2014- 05-28, 10:00 - 17:00

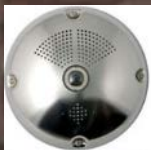
Whole Sky Imager (WSI)



Mobotix Q24



+ Rotating Shadowband Irradiometers (inside PSA & 2km south)



pyranometers

2 Mobotix Allround M25



100 m



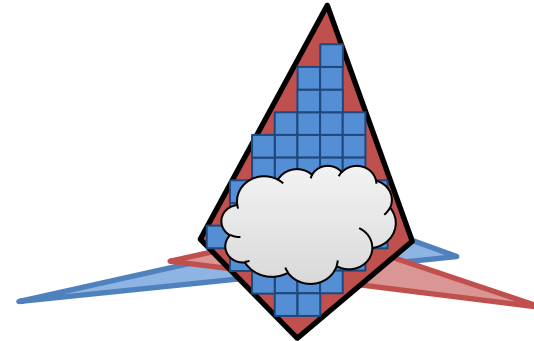
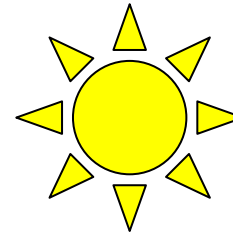
Automatic solar trackers with pyrheliometer

ARFRISOL



Approach: Voxel carving

1. Cloud-segmentation
2. Back-projection of detected clouds view cone
3. Intersection of view cones = cloud



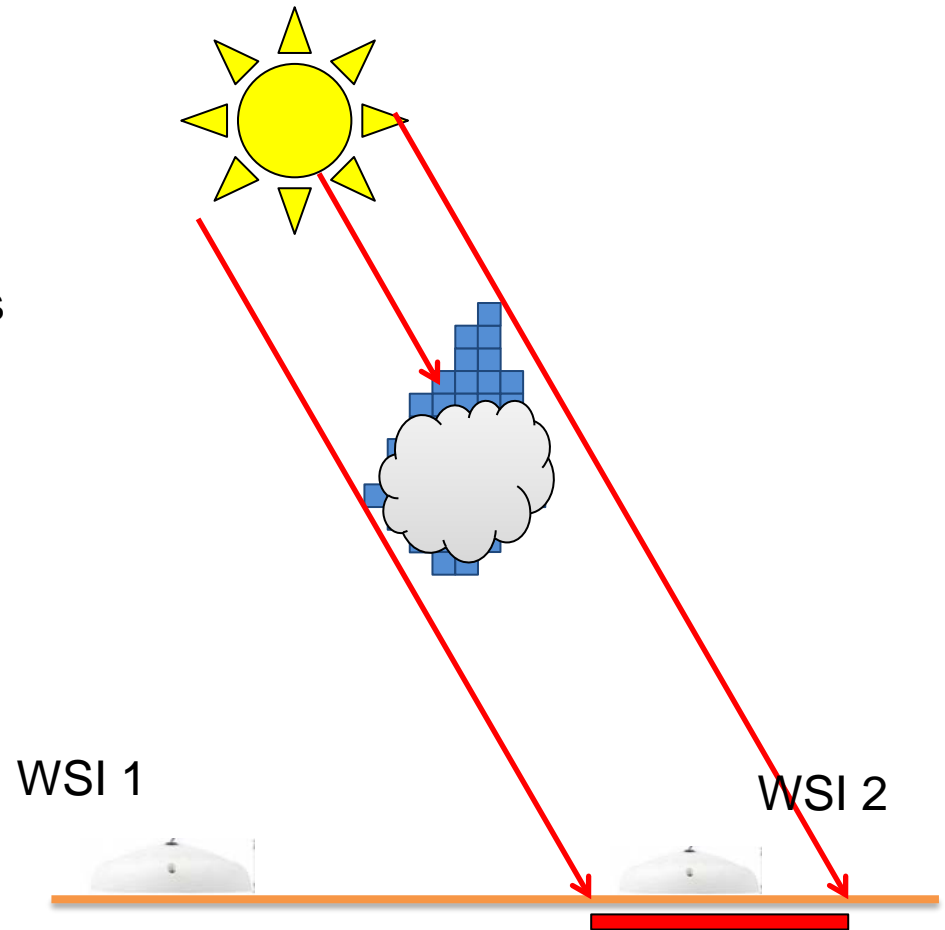
WSI 1

WSI 2



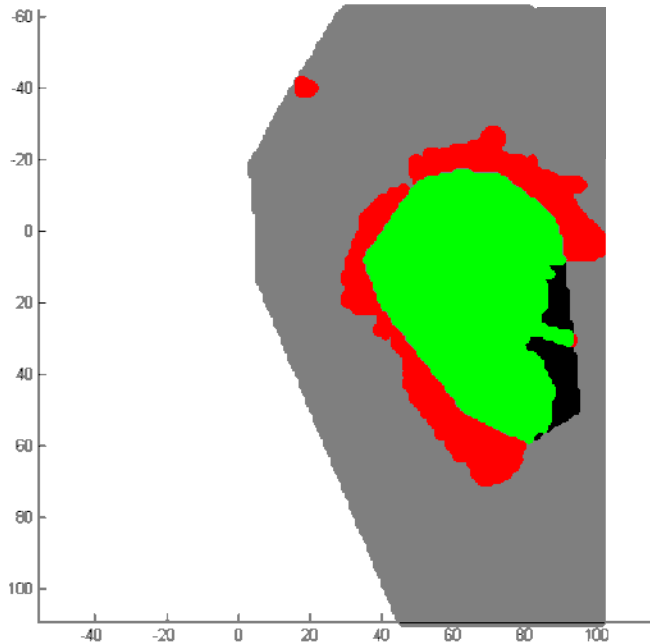
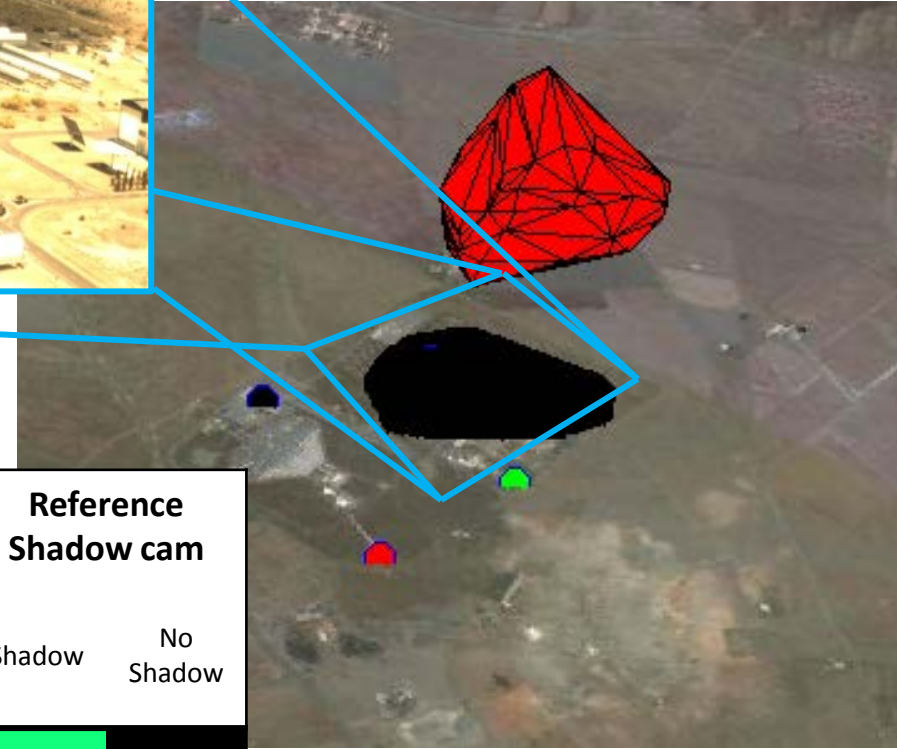
Approach: Voxel carving

1. Cloud-segmentation
2. Back-projection of detected clouds view cone
3. Intersection of view cones = cloud
4. Calculation of **modeled shadow**



- Tested with ~100 cases with average ACC = 0,72
- Prototype of system (hardware + processing) running live at PSA

Validation of modeled shadow



		Reference Shadow cam	
		Shadow	No Shadow
Model Voxel Carv.	Shadow	TP	FP
	No shadow	FN	TN

$$ACC = (TP + TN) / \text{surface} = 0.76$$



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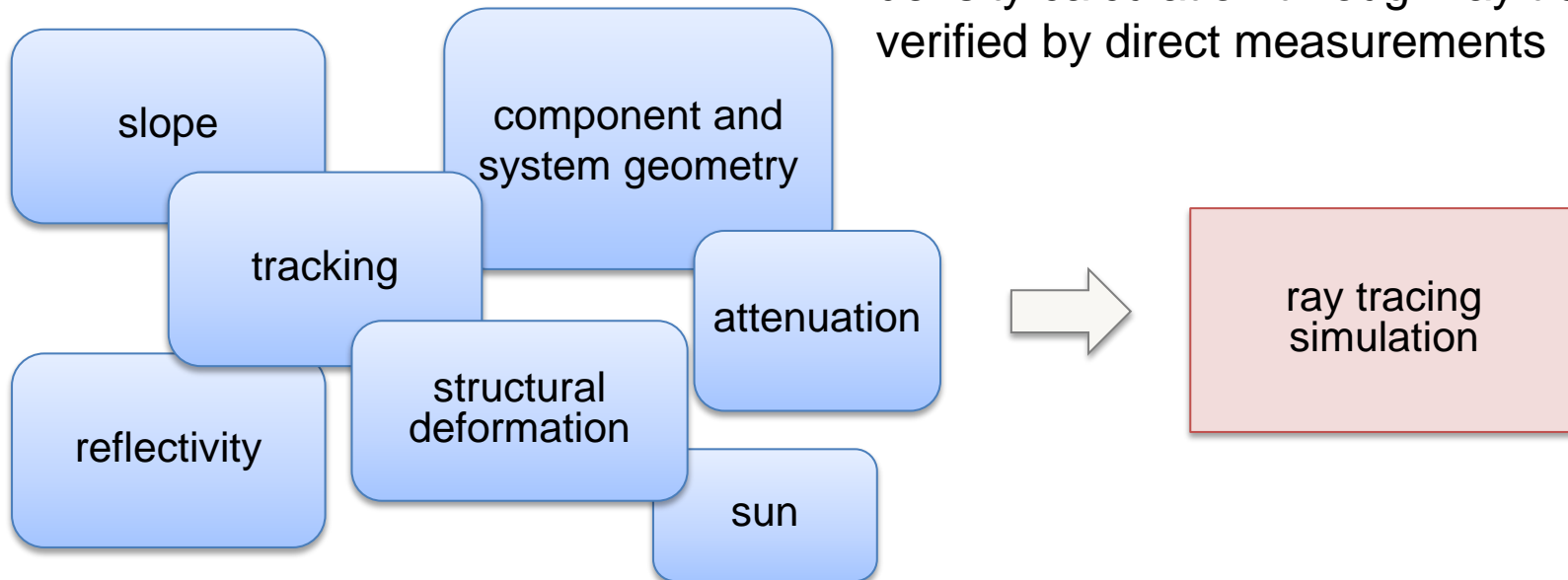
Evaluation of Heliostat Field Optical Quality

Problem:

Measurement of flux density distribution on aperture is not practical for large commercial (external) receivers

Solution:

Measurement supported simulation = Assessment of field parameters by qualification of entire heliostat field (or random samples) as basis for flux density calculation through ray tracing, verified by direct measurements



Assessment of Heliostat Field Parameters

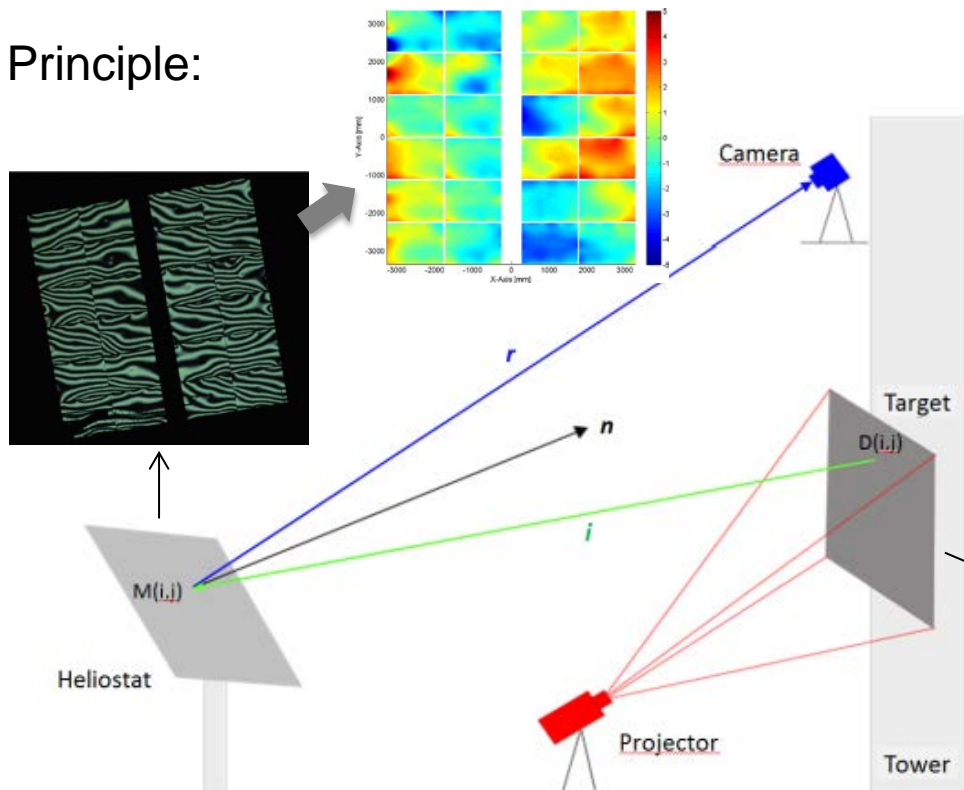
parameter(s)	assessment method	coverage
slope (mirror shape and canting)	automated deflectometry	total/ sample
structural deformation	on-site photogrammetry	sample
component and system geometry (size and positions of heliostats and receiver)	triangulation, stereo camera	sample
reflectance	on-site reflectometer device	sample
tracking accuracy	calibration (camera/target)	total
sun (DNI, sunshape)	on-site pyrhelimeter and CCD camera	total
atmospheric attenuation	transmissometer, scatterometer	sample



Automated Deflectometry Measurement

Deflectometry (= fringe reflection): observation of deformation of regular stripe patterns through reflection

Principle:

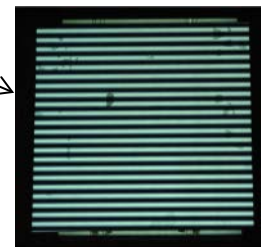


- resolution: 10^6 points per heliostat
- accuracy: < 0.2 mrad*

can be used for

- prototype testing
- qualification during production

*Ulmer, S. et al. Automated high resolution measurement of heliostat slope errors. Sol. Energy (2010)



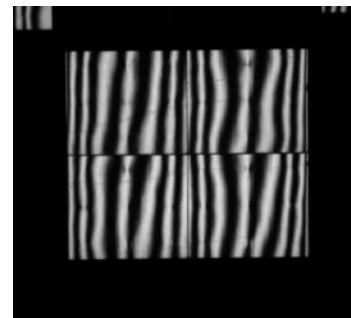
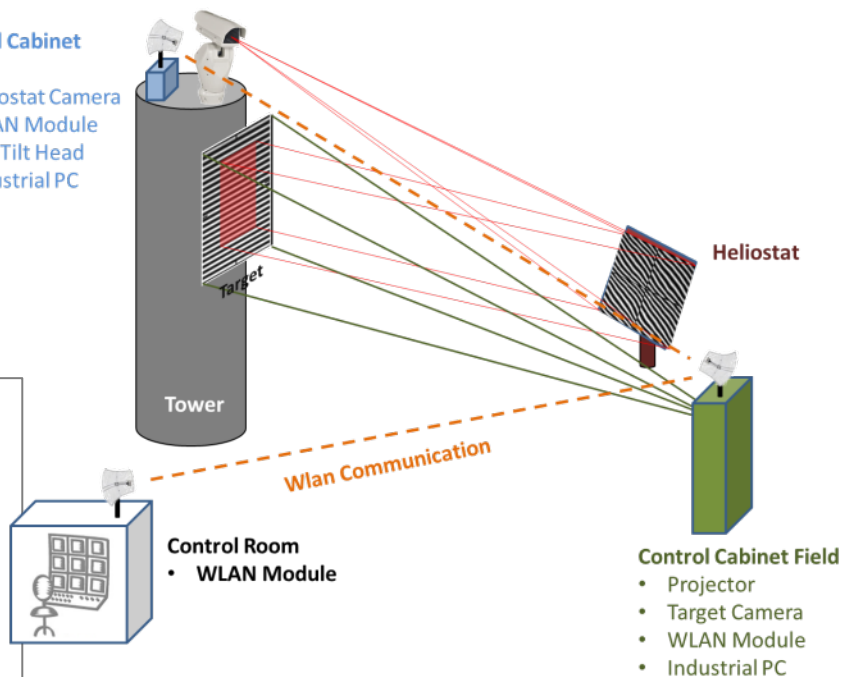
Automated Deflectometry Measurement

Automated deflectometry measurement of existing heliostat field (total/samples)



Jülich
2014/15

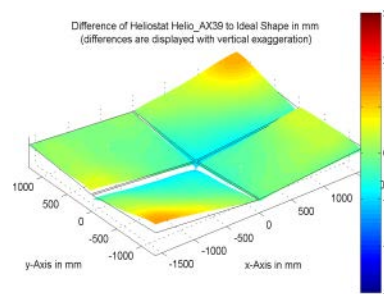
- Control Cabinet Tower**
- Heliostat Camera
 - WLAN Module
 - Pan Tilt Head
 - Industrial PC



- automatic selection of single heliostats/groups
- automatic measurement and data processing
- output of report and input data file for ray tracing
- performance: ~60sec./hel.

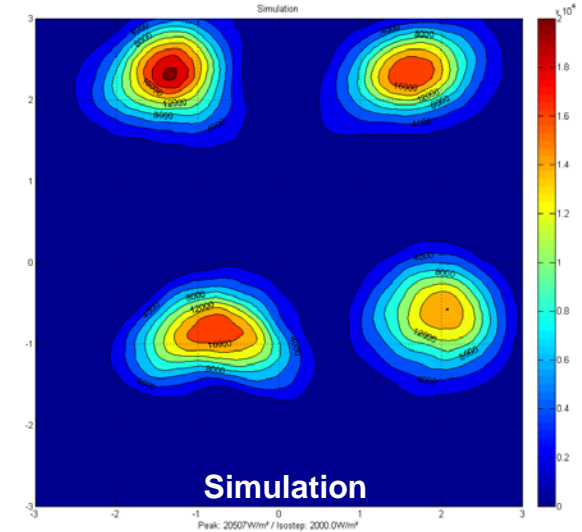
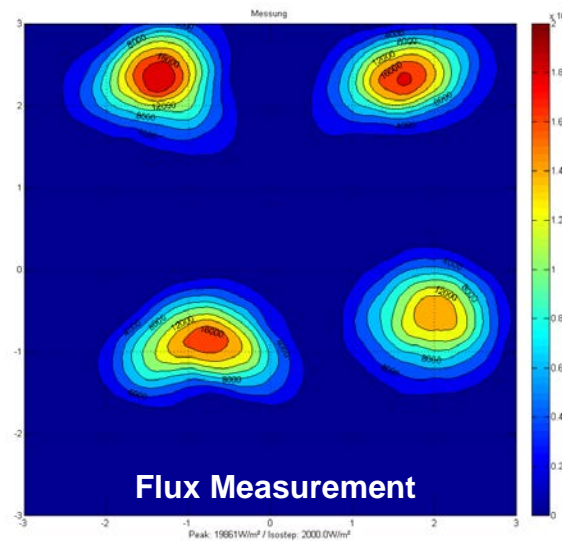
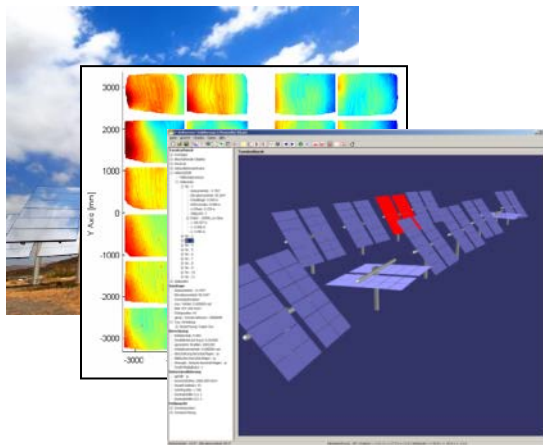
can be used for:

- field qualification during commissioning
- regular assessment of field quality during operation



High Precision Ray-Tracing of Heliostat Field

- ray tracing using deflectometry surface data in original resolution
- efficient ray generation and usage; utilization of modern cpu capabilities (SIMD, multi-threading)
→ calculation performance: $> 60 \cdot 10^6$ rays/sec using a standard pc (8 cores)
- successful validation by comparison with flux measurement*

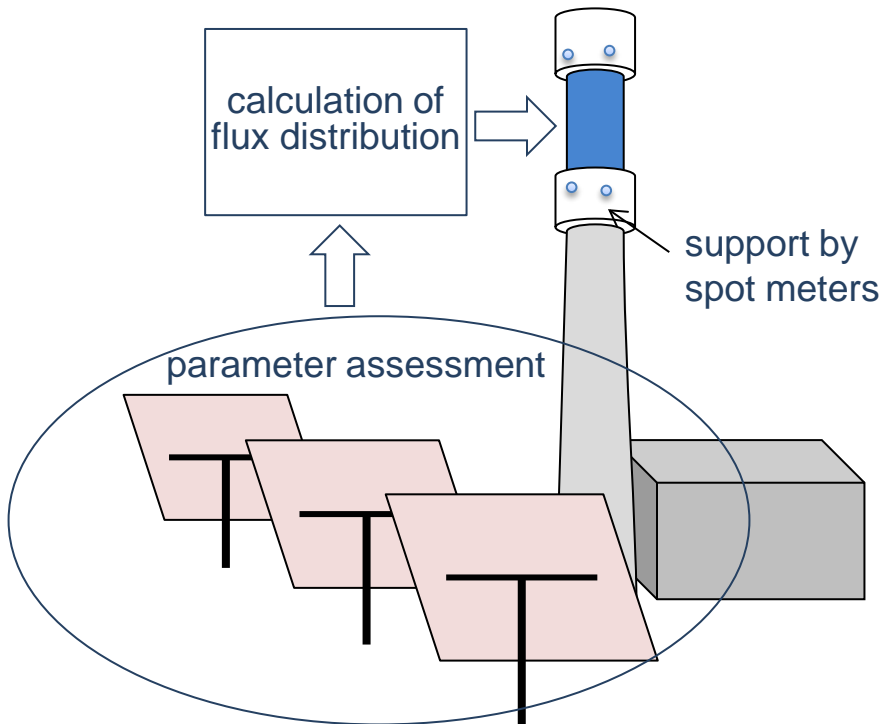


*Belhomme et al.
A New Fast Ray Tracing Tool for High-Precision Simulation of Heliostat Fields
ASME J. Sol. Energy Eng., (2009)



Measurement Supported Simulation of Heliostat Field

- high precision measurement systems
- calculation model covering all influence parameters
- reliability (confidence) improved by
 - high sampling rate
 - direct measurements



Application

1. During hot commissioning:

Which component is not meeting the contracted specifications?

- up to 100% measurement of guaranteed values
- calculation of intercept power with certain confidence level
- assessment of field and receiver efficiency

requirement: agree on measurement method and simulation model during contract negotiations

2. During commercial operation:

Why do we perform below expectation?
(... and what can we do to improve?)

- applicable to existing systems
- continuous / repeated measurements
- updated calculation every 15-60 minutes (for monitoring)

use gathered data to optimize aim point distribution on receiver surface (next slide)



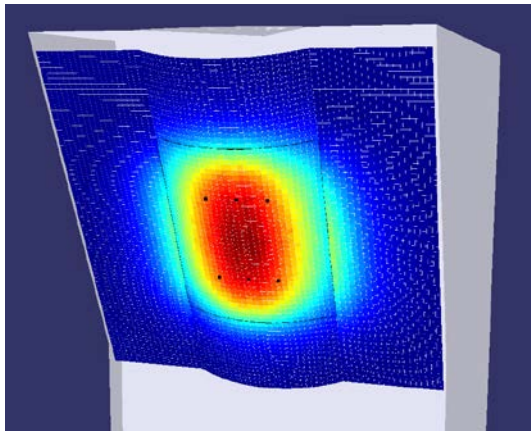
Plant owner



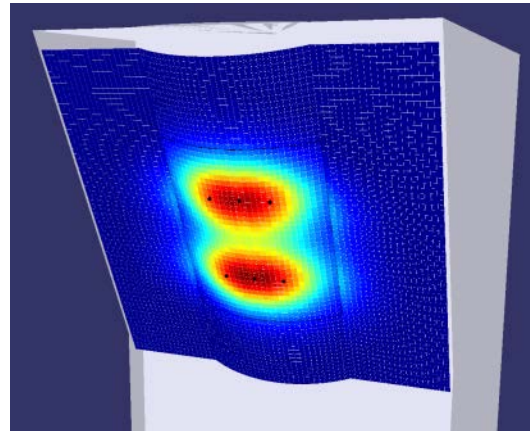
Simulation-Based Aim Point Optimization

Example: improvement of Solar Tower Jülich field performance

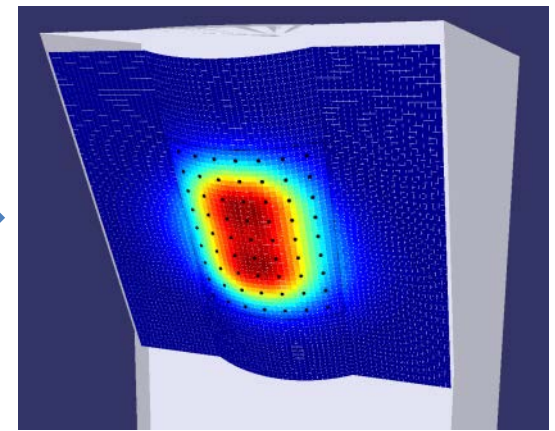
Ray tracing simulations based on deflectometry measurement of random samples



original heliostats
6 aim points
intercept: **0.706**



new heliostat facets
same aim points
intercept: **0.828**



new heliostat facets
aim point optimization
intercept: **0.861**

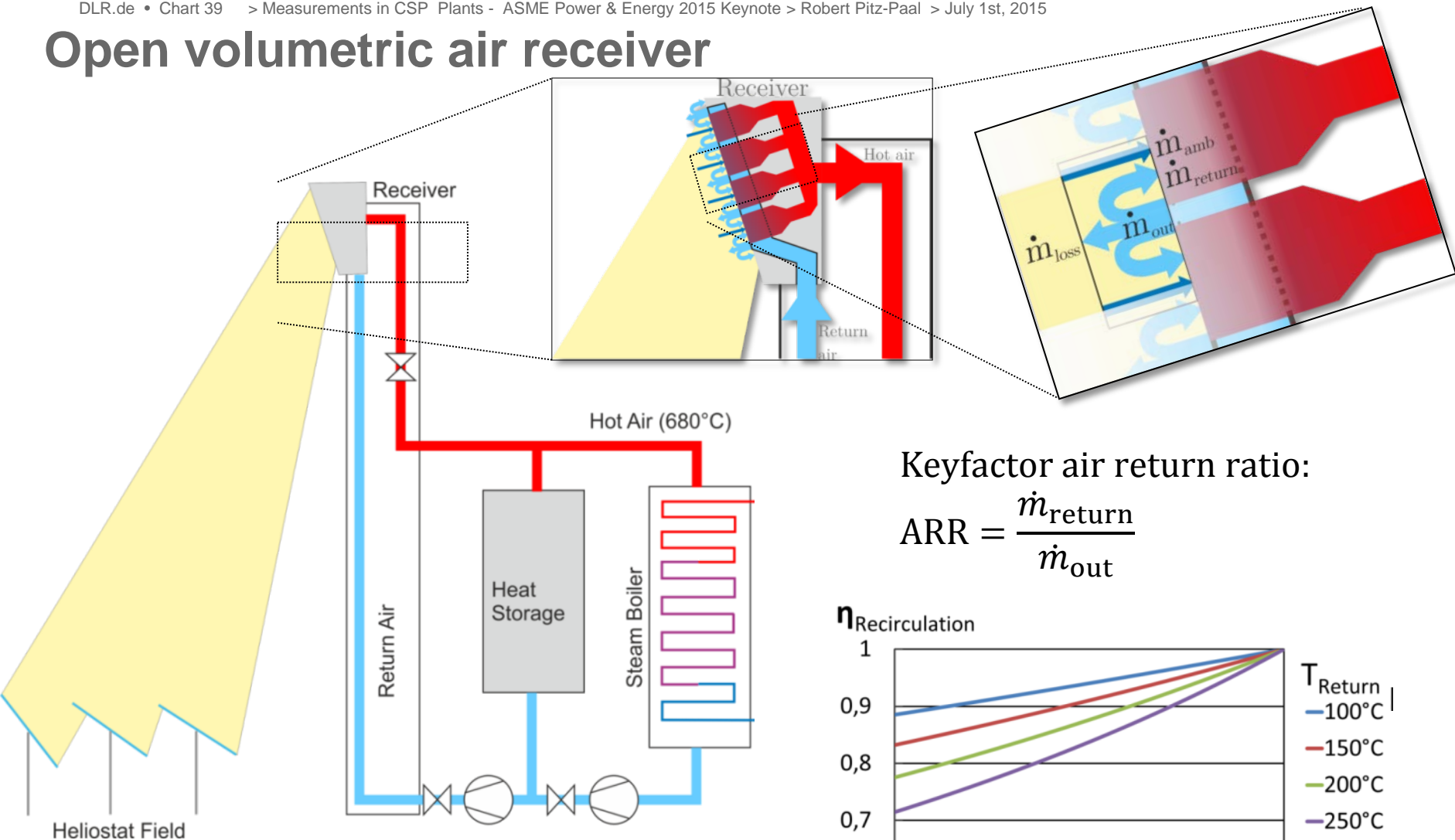


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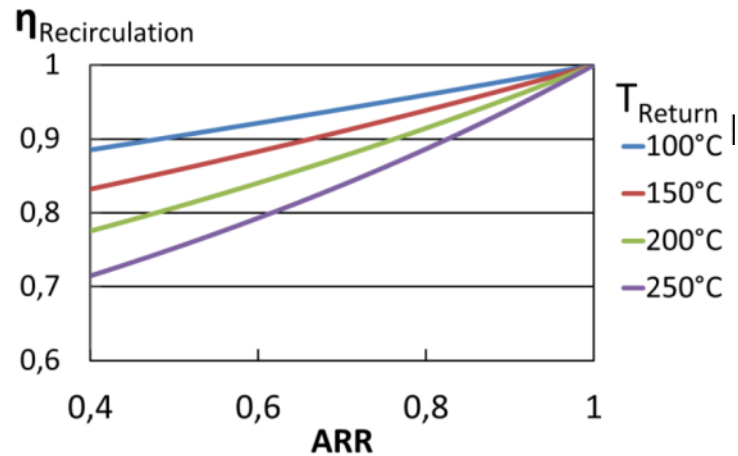


Open volumetric air receiver

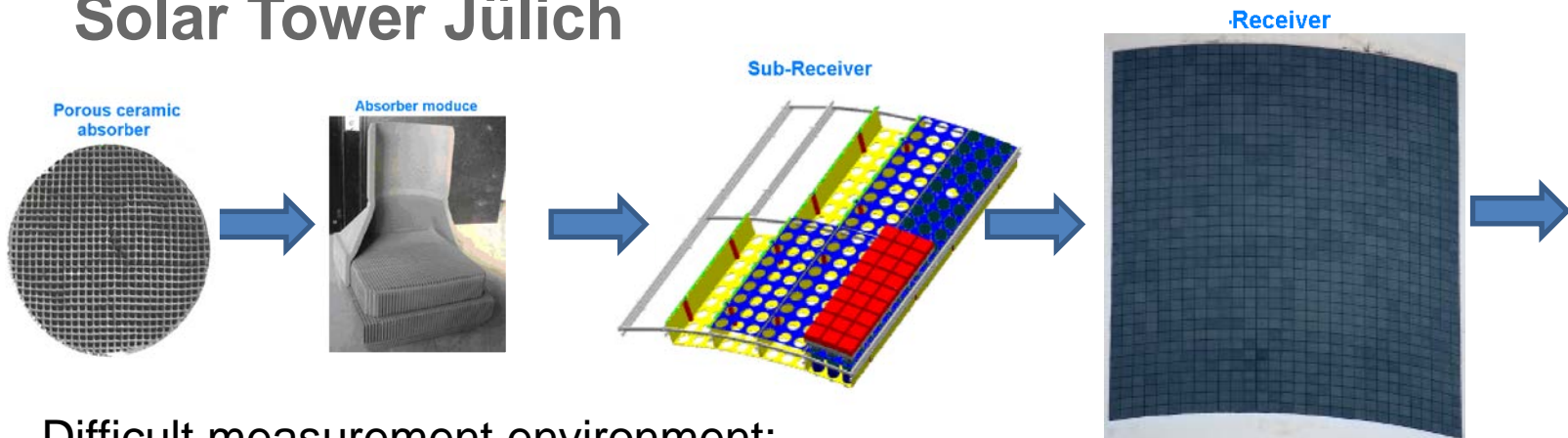


Keyfactor air return ratio:

$$ARR = \frac{\dot{m}_{return}}{\dot{m}_{out}}$$



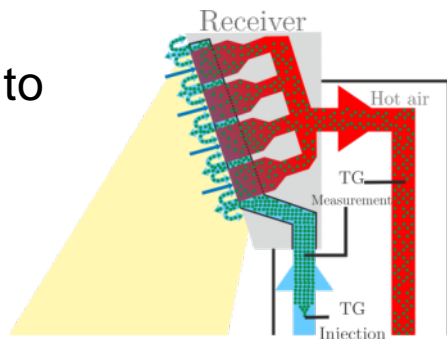
Solar Tower Jülich



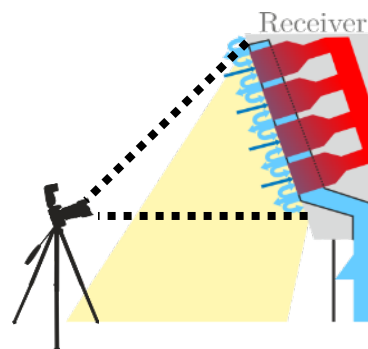
Difficult measurement environment:

- High air mass flows
- High surface temperatures
- Concentrated solar radiation
- Large scales

Two approaches to measure ARR:



Quantitative ARR measurement with tracer gas

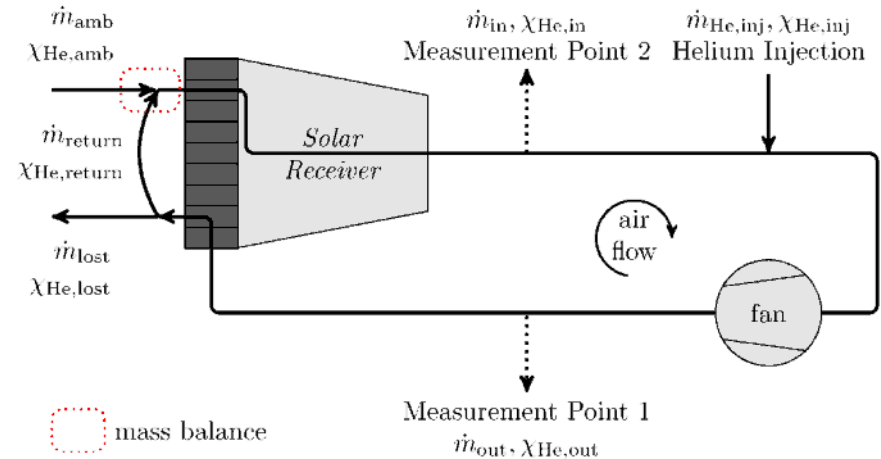


Qualitative ARR measurement with Induced Infrared Thermography

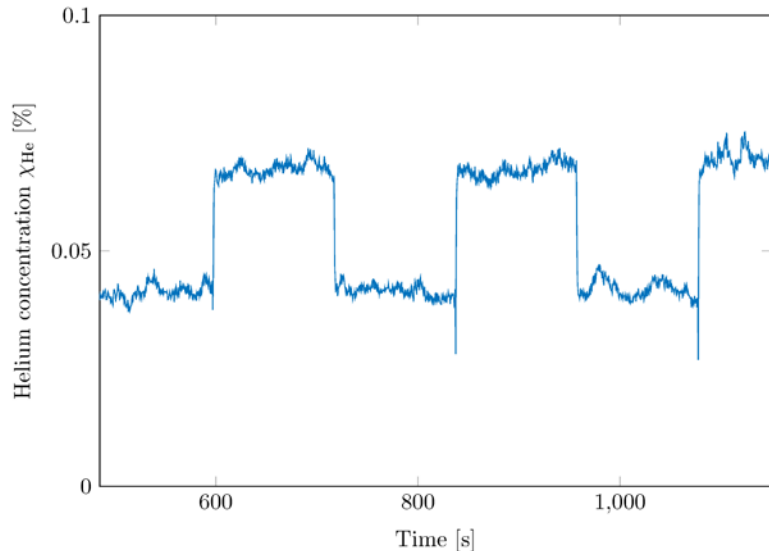


Tracer Gas Measurement

- Helium is used as tracer gas
- Helium is added to the system
 - Statically
 - Dynamically
- The Helium concentration response χ_{He} is measured using a mass spectrometer



Static Tracer Gas Measurement



- Both measuring points needed
- Straight forward measurement

$$ARR_{stat} = \frac{\chi_{He,in}}{\chi_{He,out}}$$

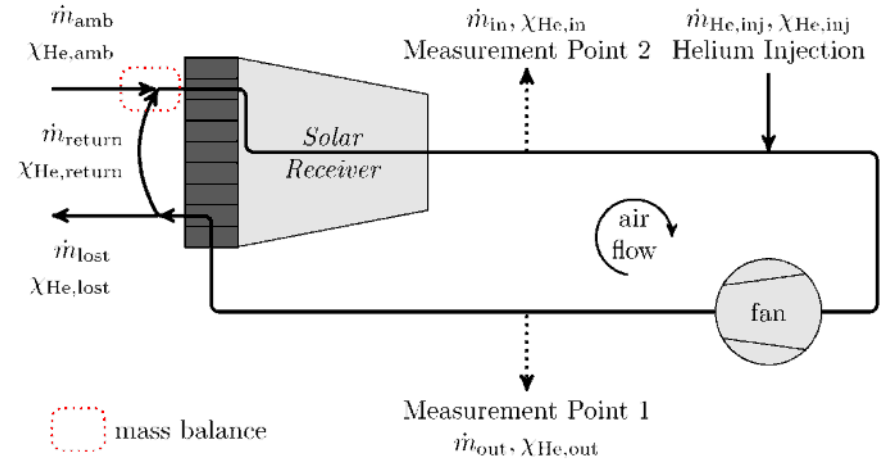
Measurement at receiver model:

$$ARR_{stat} = (61.5 \pm 2.5)\%$$

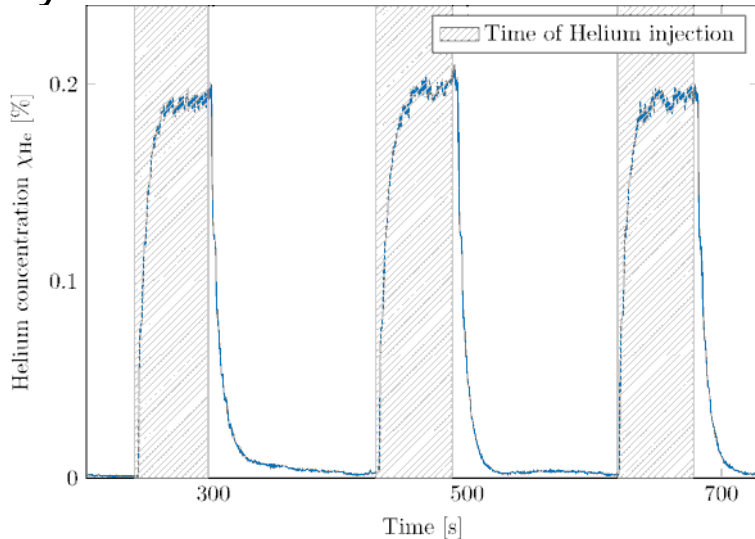


Tracer Gas Measurement

- Helium is used as tracer gas
- Helium is added to the system
 - Statically
 - Dynamically
- The Helium concentration response χ_{He} is measured using a mass spectrometer



Dynamic Tracer Gas Measurement



- Only one measuring point needed
- ARR from dynamic response

$$\chi_{He,leading}(t) = A(1 - ARR^{t/T})$$

$$\chi_{He,trailing}(t) = A \cdot ARR^{t/T}$$

Further measurements needed:

- Circulation period T
- Transfer function for dynamic error correction using system identification

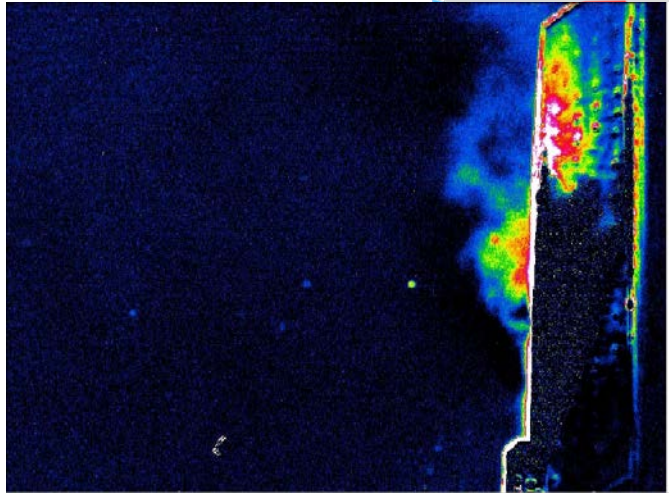
Measurement at receiver model:

$$ARR_{dyn} = (63.2 \pm 4.0)\%$$



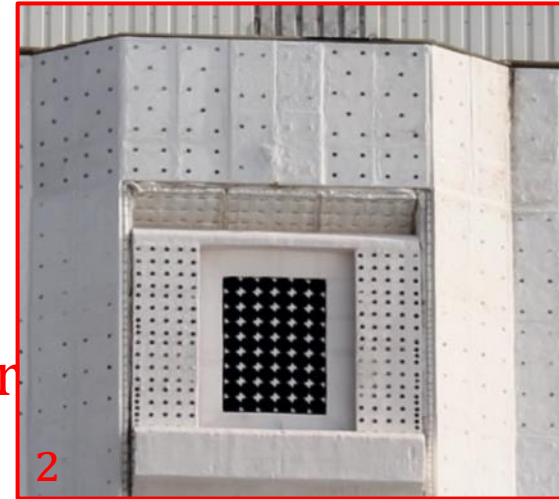
Induced Infrared Thermography (IIT)

Side view Receiver



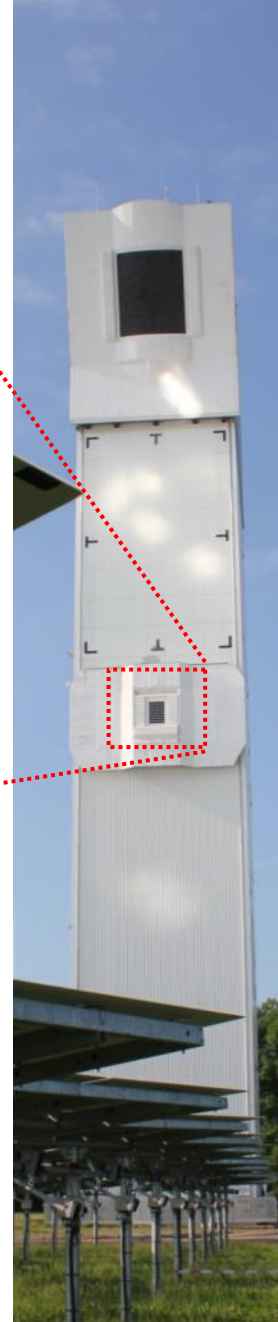
IR-Camera

Front view



Tracer
Gas

2



Summary and Conclusion

- DLR has developed a variety of tools in order to perform measurements in commercial scale trough and tower systems that go far beyond simple heat balance measurements
- All measurements have been validated in large scale facilities like the Plataforma Solar de Almería or the Research Facility Solar Tower Jülich
- Some of the measurements have been applied already in commercial full scale power plants in cooperation with the DLR Spin-off company CSP Services
- Commercial CSP applications require new methods under commercial conditions DLR and partners have the tools and validations to provide solutions

In addition we have extensive laboratory testing facilities for industrial components



QUARZ Test and Qualification Center Performance and Durability Testing

Mirror Panels

- Shape accuracy (also sag under different load conditions)
- Reflectance (specular and spectral hemispheric)
- Corrosion and abrasion tests
- Outdoor exposure at desert and coastal sites

Parabolic Trough Receiver

- Optical efficiency
- Thermal power loss
- Overheating & thermal cycling (aging of coating)
- Bellow fatigue tests (mechanical aging)
- Anti-reflective coating of glass envelope
- Operability tests under real solar conditions

Collectors

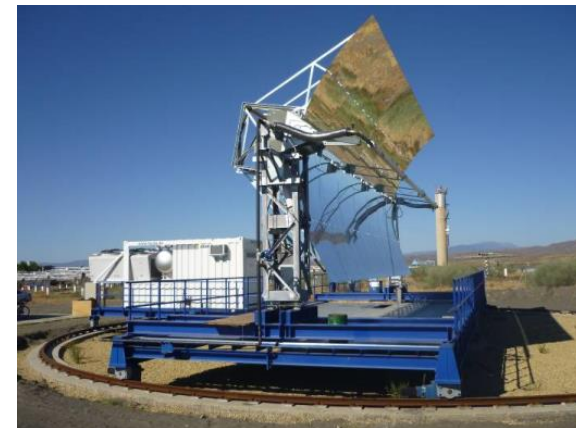
- Peak efficiency, Thermal characteristics, Incident angle modifier, behavior under different load conditions, Torsion



Mirror shape measurement



Receiver optical performance test



Rotary collector test bench (KONTAS)





Thank you for your attention

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