



## A MIMO Optimization for Physical Layer Security

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# 1





- Introduction
- System Characterization for MIMO types
- MISO System specified for Directivity
- Conclusions



## Introduction



- 4G systems is demanding high data rates, improved performance and improved spectral efficiency
- Multi-antenna systems are used in order to push the performance or capacity/throughput limits as high as possible without an increase of the spectrum bandwidth, although at the cost of an obvious increase of complexity
- Multi-antenna systems are regarded as:
  - SISO (Single Input Single Output)
  - SIMO (Single Input Multiple Output)
  - MISO
  - MIMO







- Transmitters with **directivity introduced at information level** where the transmitted constellation is only optimized in the desired direction can be used for **security purposes**
- Severely time-dispersive channels in broadband wireless systems => Use MIMO to improve spectral efficiency
- The use of multilevel modulations in modern wireless standards leads to high peak-to-average power ratios and further drives the costs of power amplifiers while reducing their efficiency.

# MISO System specified for Directivity



- Power efficiency on Amplification can be improved, due to the fact that constellations are decomposed into several BPSK (Bi Phase Shift Keying) or QPSK components (Quadri-Phase Shift Keying), being each one separately amplified and transmitted independently by an antenna
- Several users can coexist since each user must know the configuration parameters associated to the constellation configuration, i.e., the direction in which the constellation is optimized, otherwise receives a degenerated constellation with useless data

# MISO System specified for Directivity



- FDE (Frequency-Domain Equalization) techniques are suitable for time-dispersive channels, namely the SC-FDE (Single Carrier – Frequency Domain Equalization) with multilevel modulations.
  - This leads to lower envelope fluctuations => efficient power amplification (OFDM signals present high envelope fluctuations)

 IB-DFE receiver (Iterative Block Decision Feedback Equalization) are suitable for SC-FDE with multilevel modulations

# Multilevel constellations



• The constellation symbols can be expressed as a function of the corresponding bits as follows:

$$a_{n} = g_{0} + g_{1}b_{n}^{(1)} + g_{2}b_{n}^{(2)} + g_{3}b_{n}^{(1)}b_{n}^{(2)} + g_{4}b_{n}^{(3)} + \dots = \sum_{i=0}^{M-1}g_{i}\prod_{m=1}^{\mu}(b_{n}^{(m)})^{\gamma_{m,i}}, \quad b_{n}^{(m)} = 2\beta_{n}^{(m)} - 1$$
  
for each  $s_{n} \in \mathfrak{S}$ 

 $(\gamma_{\mu,i} \gamma_{\mu-1,i} \dots \gamma_{2,i} \gamma_{1,i})$  is the binary representation of *i* 

In matrix format we have

$$\mathbf{s} = \mathbf{W}\mathbf{g},$$

where

$$\mathbf{s} = [s_1 \ s_2 \ \dots \ s_M]^T \quad \mathbf{g} = [g_0 \ g_1 \ \dots \ g_{\mu-1}]^T$$

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### Multilevel constellations



- Examples:
  - optimal 16-Voronoi constellation (linear)

 $g_0 = 0$   $g_1 = -0.58 + j0.57$   $g_2 = -0.712 + j0.545$   $g_3 = -0.014 - j0.124$   $g_4 = 0.028 + j0.248$ 

 $g_5 = -0.186 + j0.273$   $g_6 = -0.2 + j0.149$   $g_7 = -0.014 - j0.124$   $g_8 = -0.1 + j0.074$ 

 $g_9 = 0.085 - j0.198$   $g_{10} = 0.358 + j0.272$   $g_{11} = 0.859 - j0.198$   $g_{12} = -0.1 + j0.074$ 

 $g_{13} = -0.085 - j0.198$   $g_{14} = -0.1 + j0.074$   $g_{15} = 0.085 - j0.198$ 

• 16-OQAM can be decomposed as a sum of **four BPSK signals** with the mapping rule defined by the set of non null complex coefficients

$$g_2 = 2j$$
  $g_3 = j$   $g_8 = 2$   $g_{12} = 1$ 



#### Transmitter



Sort=LINEAR			Sort=CENTER		
Gain	QAM	VORONOI	Gain	QAM	VORONOI
$g_0$	2j	0,717+j 0,546	$g_0$	0	-0,100+j 0,075
$g_1$	2	-0,588+j 0,572	$g_1$	0	-0,014-j 0,124
$g_2$	j	0,359+j 0,273	$g_2$	0	-0,014-j 0,124
$g_3$	1	-0,186+j 0,273	$g_3$	0	0,086-j 0,199
$g_4$	0	-0,201+j 0,149	$g_4$	0	0,086-j 0,199
$g_5$	0	0,029+j 0,248	$g_5$	0	-0,201+j 0,149
$g_6$	0	0,086-j 0,199	$g_6$	j	0,359+j 0,273
$g_7$	0	0,086-j 0,199	$g_7$	2j	0,717+j 0,546
$g_8$	0	0,086-j 0,199	$g_8$	2	-0,588+j 0,572
$g_9$	0	0,086-j 0,199	$g_9$	1	-0,186+j 0,273
$g_{10}$	0	-0,014-j 0,124	$g_{10}$	0	0,029+j 0,248
$g_{11}$	0	-0,100+j 0,075	$g_{11}$	0	0,086-j 0,199
$g_{12}$	0	-0,014-j 0,124	$g_{12}$	0	0,086-j 0,199
$g_{13}$	0	-0,100+j 0,075	$g_{13}$	0	-0,100+j 0,075
$g_{14}$	0	-0,100+j 0,075	$g_{14}$	0	-0,100+j 0,075
$g_{15}$	0	0,000	$g_{15}$	0	0,000

Linear and Centered arrangements of sub-constellations in transmitter's antennas for 16-QAM and 16 Voronoi





The receiver does not require any processing, as the multiple components of the modulation are summed over-the-air, and combined in terms of phase, as long as the receiver is in the desired DoA (alternatively, regular receive diversity can be employed).

## MISO System specified for Directivity Simulation Environment



• SC-FDE systems with multilevel modulations.

•We considered 16-QAM, 64-QAM or Voronoi constellations, decomposed as as a sum of  $N_m$  BPSK components.

• Antennas are equally spaced by  $d=\lambda/4$  and the constellations are optimized for  $\theta=75^{\circ}$  (under these conditions the directivity in the transmitted constellation is assured by phase rotations of the BPSK components).

- AWGN channel and a severely time-dispersive channel are considered
  - Channel is modeled as a frequency selective fading Rayleigh channel characterized by an uniform PDP (Power Delay Profile), with 32 equal-power taps, with uncorrelated Rayleigh fading on each tap.

# MISO System specified for Directivity



#### Simulation results

•The symbols s<sub>n</sub> are selected with equal probability from a M-QAM constellation (dimensions of M=16 and M=64 are considered).

•The transmitter based on 16-QAM with gray mapping is characterized by the set of non null coefficients 2j, 1, 2 and j, associated to the antennas 1, 2, 3 and 4, respectively. 64-QAM uses 6 non-null coefficients with values 2j, 1, 2, j, 4 and 4j associated to the antennas 1, 2, 3, 4, 5 and 6, respectively.

#### **MISO** System specified for UNIVERSIDADE AUTÓNOMA DE LISBOA Directivity 10 10 BER 16QAM Centered 10 16 Voronoi Centered 16 Voronoi Linear 16QAM Linear 10 10 10 12 16 20 2 8 14 18 Δθ

Impact of an angle error regarding the transmission direction  $\theta$  in BER performance of size-16 constellations using linear and centered arrangements.



Impact of an angle error regarding the transmission direction  $\theta$  in BER performance of size-64 constellations using linear and centered arrangements

# MISO System specified for Directivity



#### Analysis of Simulation Results

• The impact of constellation's directivity on system's performance increases with the constellation's size.

Higher directivity is assured by Voronoi constellations with a linear arrangement (uses 16 antennas, instead of 4 [16-QAM] or 6 [64-QAM]).

Increasing system's spectral efficiency / higher modulation orders assures a better separation of the data streams transmitted for the different users.

Higher impact of angle errors for constellations that are decomposed in a higher number of sub-constellations (i.e. the case of Voronoi constellations).





Linear array: BER performance for size-64 constellations with a frequency selective channel and an angle error against to transmission direction  $\theta$ .

# MISO System specified for Directivity



#### Analysis of Simulation Results

• When the angle error is null for 3 iterations of IB-DFE the performance is close to the Matched Filter Bound (MFB).

•Due directivity errors (see 4° of error) other users are unable to decode efficiently the transmitted data (the constellation symbol is degenerated)

Voronoi constellations are the best choice.

Voronoi constellations achieves higher directivity but worse performance.



#### Conclusions



Results show that the proposed MIMO / MISO system achieves directivity, while degenerating the constellation signals in the other directions.

 Directivity can increase with higher spectral efficiencies / higher order modulations.

**•**Constellation shaping implemented by a MISO transmission structure achieves physical layer security.

 Besides the aspects already mentioned, this approach also improves the power efficiency given the decomposition of multilevel constellations into constant envelope signals.

• This facilitates the use of simplified non-linear amplifiers.





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