

# Numerical analysis of the manufacturing processes of a mock-up of the ITER NHF First Wall Panel

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## Abstract

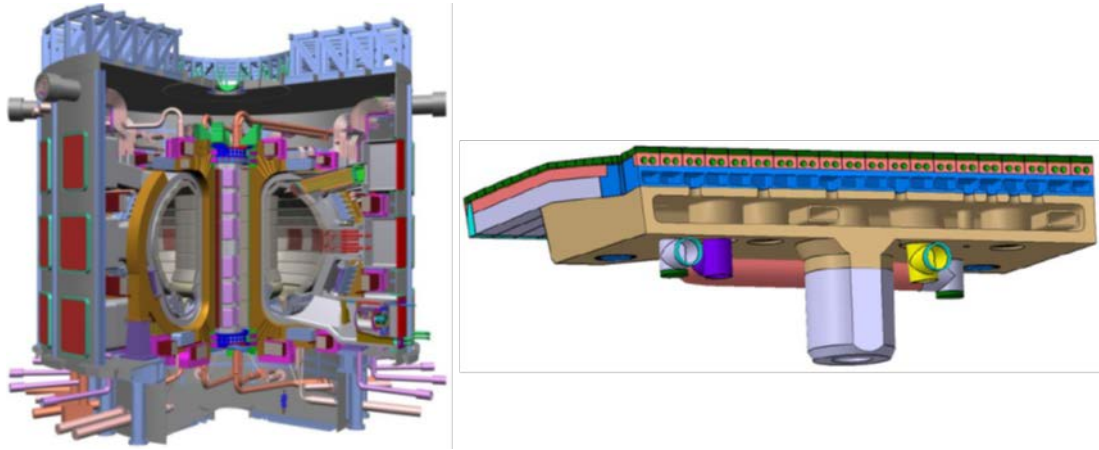
The objective of ITER is to build a new Tokamak, with the goal of demonstrating the scientific and technical feasibility of fusion power. The First Wall Panels are the inner component of the reactor, built with different materials that must support high heat flux levels inside the vacuum vessel. The manufacturing processes of the First Wall are a complex procedure including bending, hiping and cutting procedures which, in general, lead to residual stresses and distortions of the fabricated component. In this work, the analysis of the thermo-mechanical response of a simplified prototype of the ITER NHF First Wall Panel is presented from the numerical point of view. The experimental procedure within each phase of the whole manufacturing process is described. Residual stresses and distortions have been measured and analyzed. The numerical simulation of the manufacturing process includes the description of the main hypothesis, the applied loads and the boundary conditions assumed at every stage of the process. Special attention is paid to the simulation of machining and cutting by means of an *ad-hoc* element deactivation strategy. The numerical results are compared with the experimental evidence to show the prediction capability and the limitations of the proposed numerical model.

## 1. Introduction

ITER is an international project involving many research centers, universities and industrial companies from different countries worldwide to develop a new and clean energy source.

The ITER reactor is based on the *Tokamak* concept of magnetic confinement in which the plasma is contained in a doughnut-shaped vacuum vessel (Figure 1a). The fuel, a mixture of deuterium and tritium (two hydrogen isotopes) is heated to temperatures over 150 million °C forming the plasma. Strong magnetic fields are used to avoid the contact between the plasma and the vessel walls. The Blanket System of ITER is the inner component of the reactor directly exposed to the plasma. The main function of the Blanket System is to provide the main thermal and nuclear shielding to the vacuum vessel or any other reactor component. Depending on their location, the First Wall (FW) panels will be able to sustain two different levels of heating loads referred to as the Normal Heat Flux (NHF – design load up to 1 MW/m<sup>2</sup>) and the Enhanced Heat Flux (EHF – design load up to 4.7 MW/m<sup>2</sup>).

In order to reduce the eddy currents induced by the electromagnetic loading during ITER operations, the final design of the First Wall panel is cut into a number of longitudinal *fingers* as shown in Figure 1b. Each one of these fingers is cooled by pressurized water introduced into the cooling system at 70 °C and extracted at 110°C, approximately.



**Figure 1.-** a) Cross section of the ITER reactor b) Vertical cross section of the First Wall (F4E)

The First Wall panel is fabricated according to the following manufacturing sequence:

- Drilling operations
- Bending operations
- Machining operations
- Assembly procedures
- Hot Isostatic Pressure (HIP) cycles
- Heat Treatment (HT) and gas quenching
- Cutting operations
- Final Machining operations

The Hot Isostatic Pressure (HIP) cycles are used to join the Copper Chromium Zirconium (CuCrZr) alloy to the Stainless steel (SS) structure and later to the Beryllium (Be) layer of the final arrangement [7][15][19]. These are the most critical phases of the manufacturing route because of their influence on the final distortion and residual stresses accumulated by the component. Several works have been carried out on this issue, specially about the influence over the CuCrZr properties [13][16][4].

The experimental work presented in this paper has been carried out by *Fundación LEADING INNOVA*. They provided the geometry of the mock-up, as well as the characterization of the manufacturing processes and the corresponding results to support this study.

The features of the ITER reactor and the First Wall, as well as the material properties employed to build the prototype have been provided by Fusion for Energy (F4E), the European agency for the procurement of the FW.

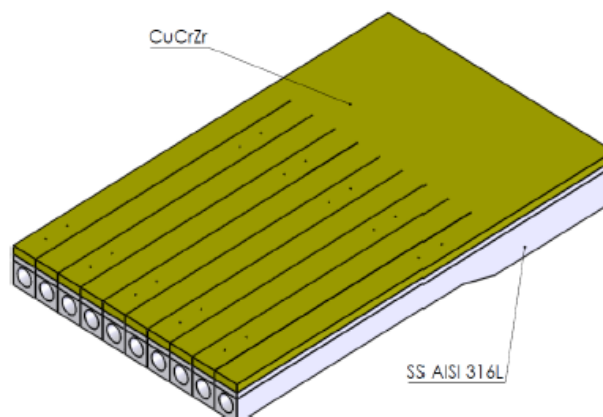
## 2. Description of the manufacturing process

Due to the geometrical complexity of the real components as well as the experimental and numerical strategy to study the manufacturing processes, the geometry of the First Wall Panel has been simplified [3].

At a first level of simplification, in the so called *semi-prototype*, the actual size has been reduced and many of the functional details have been neglected or simplified. Nevertheless, the main dimensions are kept unchanged as the length of the fingers and their section.

At a further level of simplification, the *FW simple mock-up* has more reduced dimensions, reduced model details and a lower number of manufacturing phases: the bending operation and the final HIP cycle used to add the Beryllium layer have not been considered.

Figure 2 shows a view of the simple mock-up and the location of the different materials used. The initial configuration is a parallelepiped-like volume, 434,4 mm wide and 718 mm long. The thickness varies between 61 mm and 77 mm. The diameter of the holes is 26 mm.



**Figure 2.-** Simple mock-up geometry and materials

The manufacturing phases to fabricate the mock-up for the First wall panel are the following:

- Machining of individual pieces
- Assembling and sealing operations
- HIP cycle for SS/CuCrZr joining
- Heat treatment (HT)
- Machining operation: top, lateral and back parts
- Fingers cutting: ten fingers 41 mm wide each.
- Final machining: front and back side

The objective of this paper is to study the influence of the different manufacturing stages required for the fabrication of the FW simple mock-up, and compare the numerical results obtained with the experimental evidence. To achieve such objective the component has been fabricated and both residual stresses and distortions have been measured at the end of the HIP and HT phases (once extracted from the HIP chamber) and after the machining/cutting operations at the end of the manufacturing process.

Some authors have presented a numerical approach to the HIP cycle [21][22] to support the experimental work. In this study, all the manufacturing phases have been simulated numerically by means of in-house Finite Element (FE) software adapted for this purpose. The hypothesis as well as the constitutive model adopted for the material characterization is presented in Section 4.3. Finally, Section 4.5 shows the comparison between the experimental evidence and the numerical predictions.

## 2.1 The HIP cycle

The objective of the HIP cycle is the joint between the stainless steel and CuCrZr alloy by diffusion bonding in the interphase of both materials. This is achieved by applying simultaneously the isotropic pressure and a high temperature field according to a prescribed loading function. In a first phase, both temperature and pressure are increased simultaneously until their maximum values are reached; these values are 1040 °C and 140 MPa for the temperature field and the isostatic pressure, respectively. The temperature and the pressure are kept constant during the second interval of 120 min.

Finally, the applied pressure and temperature decrease to reach the initial conditions. The total duration of the HIP cycle is about 320 minutes. At the end of the HIP cycle, the joining between the SS casing and the CuCrZr alloy by diffusion bonding is achieved.

## 2.2 The heat treatment process

After the HIP cycle, the mock-up goes through the Heat Treatment (HT) process. The objective of this treatment is to induce the solution annealing condition to improve both mechanical and thermal properties of the CuCrZr [5].

The HT process consists of a furnace chamber where the mock-up is placed. The temperature is increased to a peak of 1020°C±10°C and kept constant during 60 min ±5 min. Finally, a rapid cooling phase is enforced by gas quenching using nitrogen at 10 bar. The peak temperature is slightly higher than 980°C has been prescribed to improve the quenching rate.

The cooling rate is determinant for the phase transformations of the material properties of the CuCrZr alloy as reported by to several studies [14][18]. This heat treatment has been carried out following ITER specifications that establish a minimum cooling rate of 1°C/sec between the peak temperature and 450°C, to avoid excessive grain growth in the alloy by precipitation of the Cr, leading to a higher strength of the CuCrZr alloy.

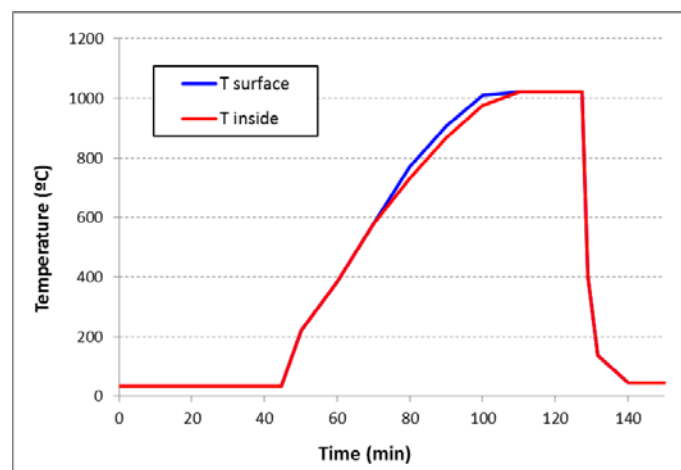


Figure 3.- Temperature evolution in the heat treatment cycle (Leading Innova)

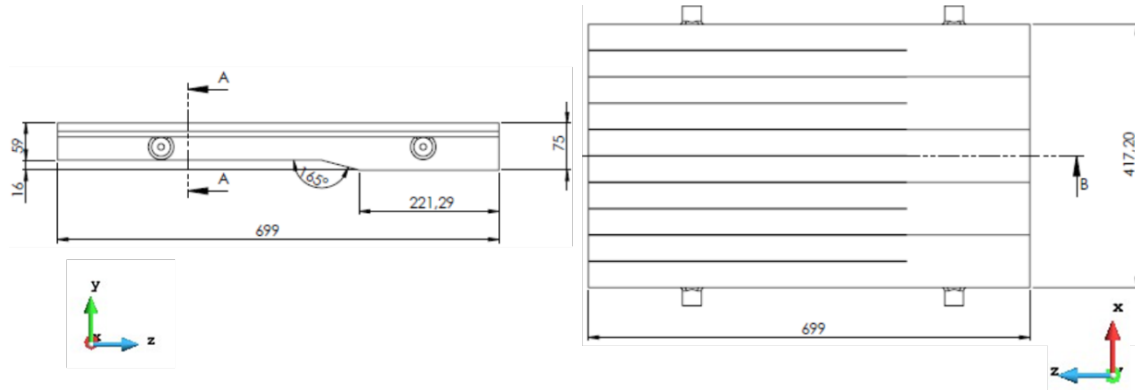
Several measures for the temperature have been obtained in the furnace, in the surface and inside the mock-up. Three holes have been drilled in the mock-up 6 mm far from the bottom of

the CuCrZr alloy. Thermocouples have been installed to measure the evolution of the temperature and specially the gradient between inside and outside. Both temperature curves in the mock-up during the heat treatment are shown in Figure 3.

As observed, in the heating branch in the inner points the rate of temperature is lower than outside. In the quenching, the cooling rate in the reference range of temperatures is about 3°C/sec or higher. On the other hand, in this same quenching branch no significant differences are observed in the experimental text between inner and outer measures.

### 2.3 Machining and cutting processes

After the heat treatment, the mock-up goes through the machining process to remove the exceeding material as the top canister covering the CuCrZr alloy and both the lateral and back sides of the mock-up. The cutting operation to create the fingers is performed by means of Wire Electron Discharge Machining (WEDM). Observe that both cutting and machining operations are performed in isothermal conditions. In fact, the component is submerged in a water cooling pool at constant temperature. The dimensions of the mock-up after machining and cutting operations are depicted in Figure 4:



**Figure 4.-** Final dimensions of the mock-up after machining and cutting operations (F4E)

### 3. Materials

The materials used to fabricate the simple mock-up are stainless steel (SS) 316L and CuCrZr alloy (CuCrZr-IG). The material properties of both materials are assumed as temperature dependent as shown in Figure 5.

At high temperatures, it is also important to take into account the rate-dependency of both elastic and plastic behaviors. Hence, visco-elastic and-visco-plastic constitutive laws are defined for both materials as described in Section 4.

Finally, to account for the phase transformation occurring during the HT process, the material properties are modified through a saturation law defined as:

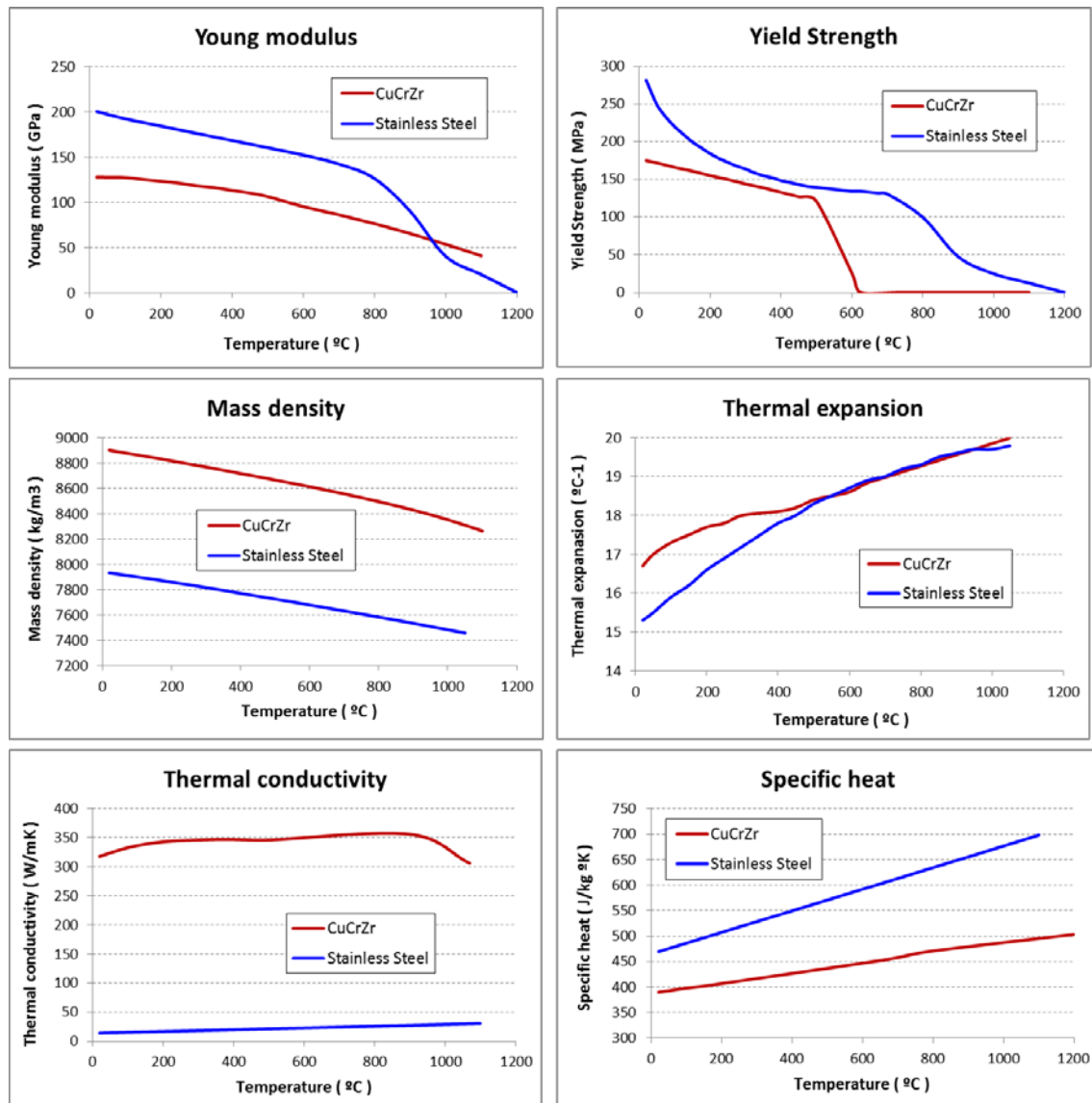
$$p(t) = p_0 + (p_f - p_0)[1 - e^{-\delta(t-t_0)}] \quad (1)$$

where  $p(t)$  is the generic material property (e.g. material stiffness or strength) as a function of the transformation time  $t$  of the process (e.g. the HT or HIP).  $p_0$  and  $p_f$  are the initial and the final values of the material property at time  $t_0$  and  $t_f$ , respectively, while  $\delta$  defines the transformation rate.

#### 4. Numerical simulation of the manufacturing process

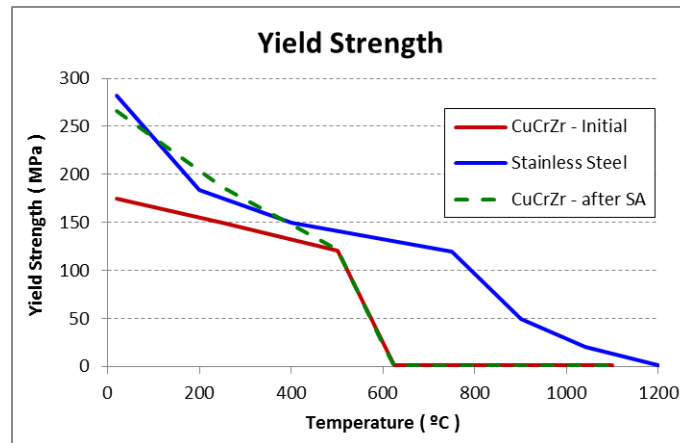
##### 4.1 Geometry and mesh discretization

The geometrical model of the simple mock-up is presented in Figure 7. The actual model has been simplified by omitting all the geometrical details that do not contribute to the structural behavior of the mock-up such as the supporting devices on the lateral walls. Symmetry conditions have been considered to perform the numerical analyses on half of the geometrical model.



**Figure 5.-** Material properties for CuCrZr alloy and the stainless steel (F4E)

- a) Young's modulus
- b) Yield strength
- c) Density
- d) Thermal expansion
- e) Conductivity
- f) Specific heat

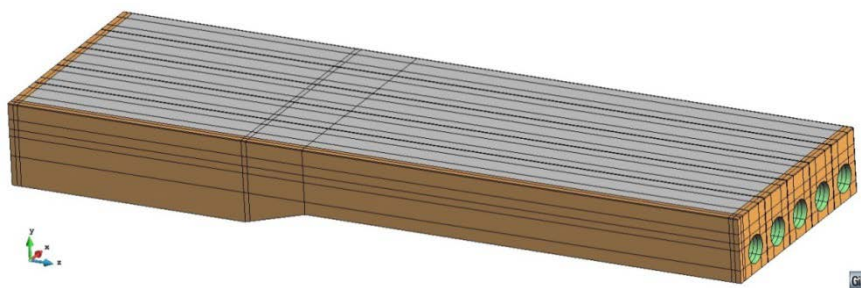


**Figure 6.-** Material properties for CuCrZr alloy and stainless steel. Variation of the yield surface due to heat treatment

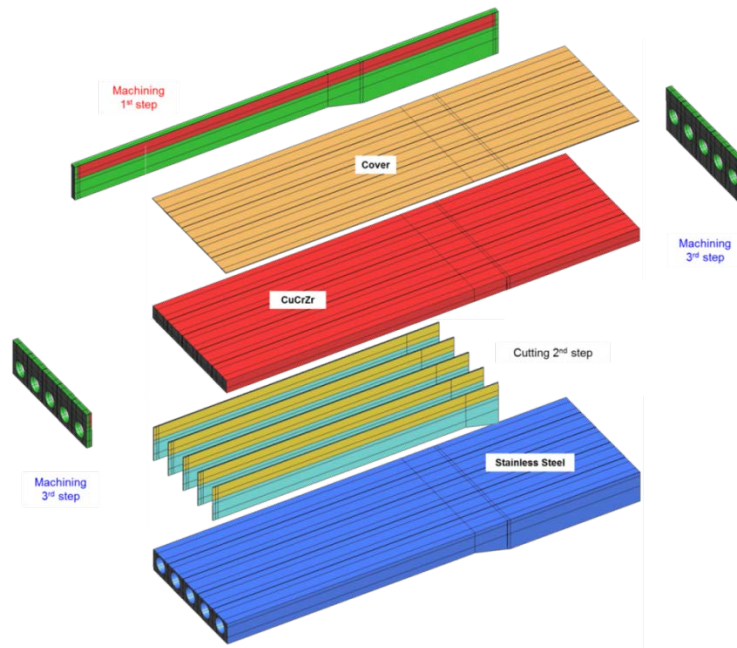
The original model has been divided into different volumes to allow for the material removal during the cutting and the machining operations (see Figure 8).

The steel body is shown with blue color while the CuCrZr bars are depicted with the red color. The canister lid (top cover) is made of stainless steel (light brown color). It is removed after the HT. The lateral sides, made of stainless steel (green) and CuCrZr alloy (red color), are prepared to be removed by the machining operation.

Five vertical slim layers, 0.8 mm wide, are inserted among the fingers allowing for the cutting process. These layers are made of both CuCrZr alloy (yellow) and stainless steel (light blue). Finally, the front and back sides of the mock-up, in green and red colors, respectively, are also ready to be removed by the final machining operations.

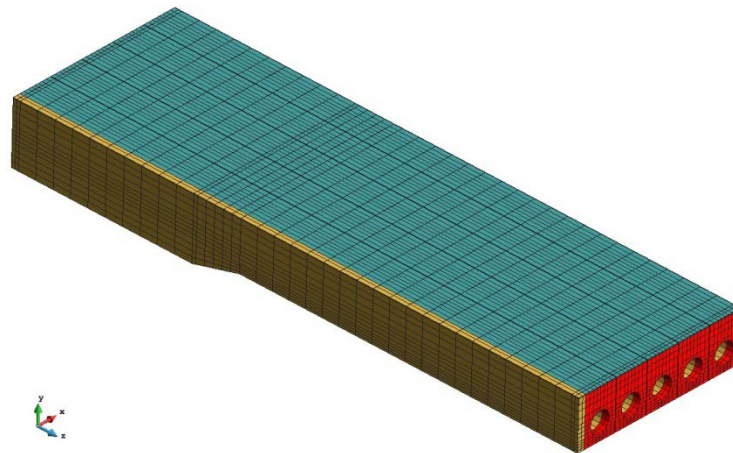


**Figure 7.-** Model of the mock-up used for the numerical analysis



**Figure 8.-** Subdomains defined for the numerical simulation of the different process operations

The volume partition defined at geometrical level is preserved during the meshing strategy. To achieve optimal numerical accuracy, a structured mesh made of 23,320 hexahedral elements has been generated with a maximum allowed element distortion of 1/5. Figure 9 shows the FE mesh used to discretize the geometrical model and used for the simulation of the manufacturing process of the simple mock-up.



**Figure 9.-** Finite element mesh of the mock-up

An ad-hoc FE technology to deal with the isochoric material behavior is mandatory when the plastic deformations are purely deviatoric. This is the case for J2 visco-plastic constitutive models to describe the material behavior of metallic materials. In our work, the mixed Q1P0 FE technology is adopted to overcome the locking phenomena observed in the pressure field when standard displacement-based elements are used (see [10][20]).

## 4.2 Constitutive model



A thermo-mechanical framework is adopted for the numerical simulation of the different manufacturing phases to be considered. The governing equations as well as the constitutive equations of the model assumed in the numerical simulation are summarized in Table 1. Further details can be found in [1].

A fractional step method is used to solve in a staggered form the balance of momentum and the balance of energy equations.

Fourier's law is adopted to deal with the heat conduction being  $k(T)$  the temperature-dependent heat conductivity.

The heat absorption as well as the heat losses, are due to the heat convection and radiation mechanisms. The effects induced by the heat convection can be taken into account using Newton's law as:

$$q_{conv} = h_{conv}(T - T_{env}) \quad (2)$$

where  $h_{conv}$  is the Heat Transfer Coefficient (HTC) by convection between the component and the surrounding environment while  $T_{env}$  is the temperature. The heat loss by radiation is described by the radiation law:

$$q_{rad} = \sigma_{rad}\epsilon_{rad}(T^4 - T_{env}^4) \quad (3)$$

where  $\epsilon_{rad}$  is the emissivity parameter while  $\sigma_{rad}$  is the Stefan-Boltzmann constant.

Both models are needed to account for the temperature field evolution applied to both HIP and HT chambers.

A visco-elasto-visco-plastic constitutive model including both isotropic hardening and thermal softening has been used to characterize both the stainless steel and the CuCrZr alloy. Figure 10 shows a schematic representation of the mechanical rheological model. Both visco-elastic and visco-plastic responses have been included to deal with the rate-dependency of the material behavior at the high temperature (see [2][8][9]).

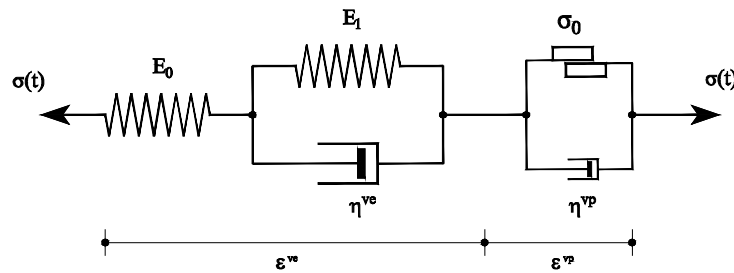


Figure 10.- Rheological scheme for the visco-elastic-viscoplastic model

The visco-elastic model depends on the elastic viscosity  $\eta^{ve}$  so that the material stiffness can vary from its initial value  $E_0$  ( $t=0$ ) to the final stiffness  $E_\infty$  ( $t \rightarrow \infty$ ) defined as:

$$E_\infty = \frac{E_0 + E_1}{E_0 E_1} \quad (4)$$

The elastic limit  $\sigma_0$  is a critical temperature-dependent material parameter that is progressively reducing while the temperature is increased. When the temperature is close to the melting temperature the yield surface radius vanishes and the mechanical response for both mushy and liquid-like phases is purely viscous being  $\eta^{vp}$  the associated plastic viscosity.

The isotropic hardening is defined by the saturation stress  $\sigma_\infty$  and the linear hardening coefficient  $H$ . Note that the melting temperature is assumed as annealing temperature. Hence, the strain hardening is reset above such temperature.

Finally, the thermal shrinkage depends on the thermal expansion coefficient  $\alpha(T)$  and the initial temperature  $T_0$  defined for each material.

<b>Thermal model</b>	
▪ Balance of energy equation	$\dot{H} = -\nabla \cdot \mathbf{q}$
▪ Enthalpy rate	$\dot{H}(T) = C(T)\dot{T}$
▪ Fourier's law for heat conduction	$\mathbf{q} = -k(T)\nabla T$
▪ Convection heat flux	$q_{conv} = h_{conv}(T - T_{env})$
▪ Radiation heat flux	$q_{rad} = \sigma_{rad}\epsilon_{rad}(T^4 - T_{env}^4)$
<b>Mechanical model</b>	
▪ Total strain	$\boldsymbol{\varepsilon} = \nabla^S \mathbf{u}$
▪ Thermal deformation	$\boldsymbol{\varepsilon}^\theta = 3[\alpha(T)(T - T_{ref}) - \alpha(T_0)(T_0 - T_{ref})]$
▪ Stress tensor decomposition	$\boldsymbol{\sigma} = p\mathbf{I} + \mathbf{s}(\mathbf{u})$
▪ Balance of momentum equation (split format)	$\nabla \cdot \mathbf{s}(\mathbf{u}) + \nabla p + \mathbf{f} = \mathbf{0} \quad \text{in } \Omega$
▪ Strain tensor decomposition	$\boldsymbol{\varepsilon} = \mathbf{e} + \varepsilon_v \mathbf{I}$
▪ Deviatoric strain tensor split	$\mathbf{e} = \mathbf{e}^{ve} + \mathbf{e}^{vp}$
▪ Volumetric constitutive equation	$p = K(\nabla \cdot \mathbf{u} - \varepsilon^\theta)$
▪ Deviatoric constitutive equation	$\mathbf{s}(\mathbf{u}) = 2G\mathbf{e}^{ve} + \eta\dot{\mathbf{e}}^{ve}$
▪ Yield surface	$\Phi(\mathbf{s}, q, T) = \ \mathbf{s}\  - R(q, T)$
▪ Von Mises yield surface radius	$R(q, T) = \sqrt{\frac{2}{3}}[\sigma_0(T) - q]$
▪ Isotropic hardening	$q = -[\sigma_\infty - \sigma_0](1 - e^{-\delta\xi}) - H\xi$
▪ Evolution law for the plastic deformation	$\dot{\boldsymbol{\varepsilon}}^{vp} = \gamma^{vp} \frac{\mathbf{s}}{\ \mathbf{s}\ }$
▪ Isotropic strain hardening	$\dot{\xi} = \sqrt{\frac{2}{3}} \left\langle \frac{\Phi(\mathbf{s}, q, T)}{\eta_p} \right\rangle = \sqrt{\frac{2}{3}} \gamma^{vp}$

**Table 1.-** Governing equations, constitutive laws and evolution law describing the thermo-visco-elasto-visco-plastic constitutive model

Table 2 shows a list with the material properties to define the constitutive model, their notation and temperature dependence.

<b>Property name</b>	<b>Notation</b>
Specific heat	$C(T)$
Conductivity	$k(T)$
Emissivity	$\epsilon_{rad}$
Convection coefficient	$h_{conv}$
Young's modulus	$E(T)$

Poisson's ratio	$\nu(T)$
Thermal expansion coefficient	$\alpha(T)$
Elastic viscosity	$\eta_{ve}(T)$
Plastic viscosity	$\eta_{vp}(T)$
Initial flow stress limit	$\sigma_0(T)$
Saturation stress limit	$\sigma_\infty(T)$
Linear hardening parameter	H

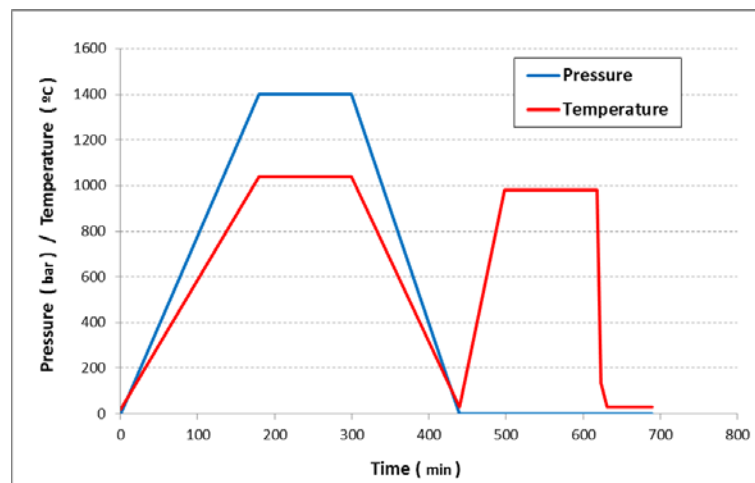
**Table 2.-** Material properties in the thermo-visco-elasto-visco-plastic constitutive model

### 4.3 Simulation of the HIP and HT processes

A fully coupled thermo-mechanical analysis is considered to analyze both the HIP and HT cycles. Figure 11 shows the pressure and temperature functions used in the experiment. The same thermo-mechanical loading is applied in the numerical model.

The following assumptions have been made for the numerical modeling of the HIP phase:

- 1) Stress-free thermal expansion of the stainless steel casing is ensured by the isostatic boundary condition of the supporting structure used to fix the mock-up in the HIP chamber.
- 2) Free dilatation of the stainless steel with respect to the CuCrZr bar during the heating phase.
- 3) Perfect bonding between stainless steel and CuCrZr alloy is assumed at the end of the HIP plateau when the highest temperature and pressure field is applied in the HIP chamber. This is imposed by linking the surface nodes at the contact interface between the steel and the CuCrZr alloy.
- 4) When the maximum temperature is reached for both HIP and HT phases, the CuCrZr alloy is in a mushy phase [6]. Its yield strength is negligible and the annealing effect resets the phase transformation hardening due to previous plastic deformations as shown in Figure 5b.
- 5) The residual stresses are generated during the cooling phase of both HIP and HT cycles due to the different thermal expansion coefficients of the two materials once the joining is completed by diffusion bonding. Note that these stresses take place below 600°C when the strength of the CuCrZr alloy is reestablished.
- 6) In case of high cooling rates (that's HT process) the material properties of the CuCrZr alloy are modified to take into account the phase transformation. Hence, a different set of material properties is used during cooling if compared to the one used during the heating phase (see Eq. 1).



**Figure 11.-** Evolution of the pressure [bars] and temperature [°C] applied to the mock-up during the HIP process and the HT treatment. (F4E)

#### 4.4 Simulation of the machining and cutting phases

The final dimensions of the mock-up are obtained after machining and cutting operations. Both of them take place in isothermal conditions: the component is submerged in a water cooling pool at constant temperature. Hence, a purely mechanical analysis is performed according to the following hypotheses:

- 1) The residual stresses and distortions induced by HIP and HT cycles are the starting point for machining and cutting process.
- 2) The same mesh is assumed for the next phases without requiring any data transfer or smoothing techniques.
- 3) The machining and cutting processes are performed by deactivating the elements in the sets that correspond to the volumes removed during such operations [11]. The cutting planes have been previously inserted as part of the CAD geometry and preserved during the meshing operation as described in Section 4.1.
- 4) Cutting and machining operations are very local processes. The global response (distortion) of the component is only affected by the stress redistribution and stress relaxation while removing the material.
- 5) At room temperature and very slow cutting speed the material behavior can be assumed as temperature and rate independent. Consequently, the cutting speed does not affect the final results.

#### 4.5 Numerical results

##### 4.5.1 Quality control measurements during manufacturing

In this section the results obtained through the numerical simulation are compared with those coming from the experimental measurements. Particular attention is focused on the values of the residual stresses and the distortion of the mockup at the end of the manufacturing process.

A dimensional control is performed after HIP and HT phases once the mock-up is extracted from the HIP chamber. Once the steel canister is removed, stresses and strains have been measured using 3 strain-gauges placed on the top surface of the CuCrZr alloy. The measurements took place during the entire cutting/machining phase to monitor the stress released during to the cutting operation.

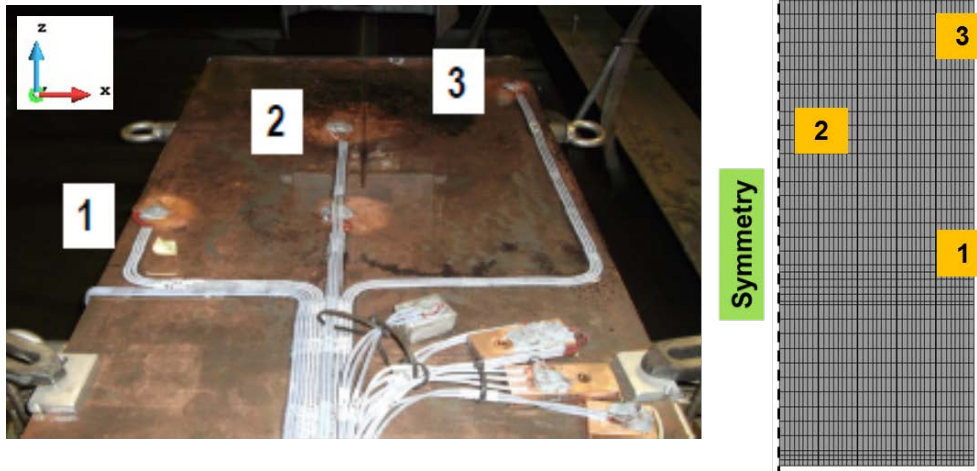
A further dimensional control is used to check the effects induced by the cutting process as well as to assess the final distortions induced by the entire manufacturing chain.

##### 4.5.2 Residual stress evolution

Before cutting of the fingers, a set of strain-gauges has been placed over the CuCrZr surface. The location of the gauges is shown in Figure 12a. The evolution of the in-plane stresses  $\{\sigma_x, \sigma_z\}$  have been measured during the cutting phase. Figure 12b shows the location where the normal stresses have been obtained from the numerical simulation. The comparison between experimental measurements and numerical results are shown in Figure 13.

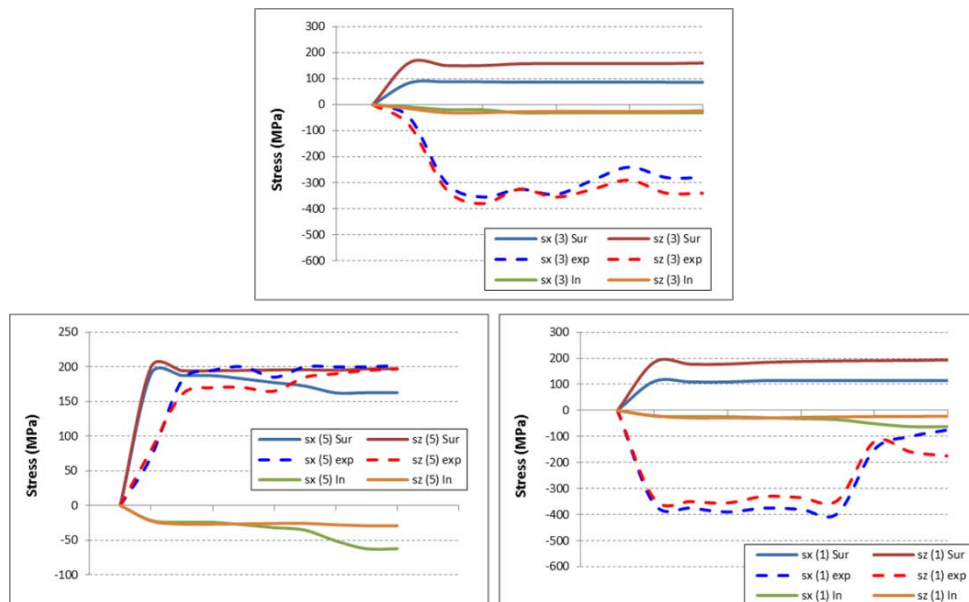
Note that the stresses reported are relative to the values before cutting (after HIP and HT). The in-plane stresses are presented using two curves: the first one on the CuCrZr surface just after the upper canister is machined ( $\sigma_{x,z}$ -Sur). The second one, in the same location but obtained by

hole-drilling through the CuCrZr bars ( $\sigma_{x,z}$ -In). Shear stresses are negligible as shown by the very low values obtained through the experimental measurements and the numerical simulation.



**Figure 12.-** Location of the strain gauges over the simple mock-up before machining/cutting phase  
 a) Experimental setup b) Numerical postprocess points

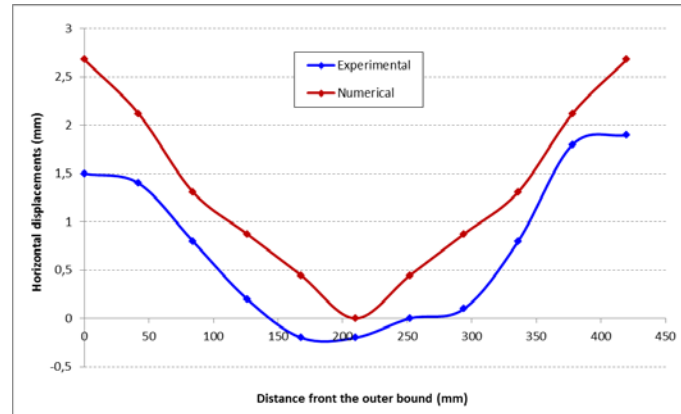
It can be observed that even if the global trend is somehow captured, the actual values are quite different. This is probably due to the large variation of the residual stresses through the thickness of the mockup as can be appreciated comparing surface and inside curves. This stress gradient cannot be captured by the hole-drilling method which returns an average value based on the stress release once the hole is made. The solution is quite different in the numerical model, because the FE representation is able to return the corresponding stress values once defined the exact locations to be extracted. The numerical analysis clearly shows the high stress gradient varying from the external surface to the actual penetration of the drill.



**Figure 13.-** Evolution of the stresses  $\{\sigma_x, \sigma_z\}$  at two strain-gauge locations during the machining/cutting phase: experimental measurements (Leading Innova) vs numerical analysis.

#### 4.5.3 Transversal displacements

The transversal displacements of the front side of the mock-up of the mock-up fingers obtained after the cutting/machining operations are shown in Figure 14. The experimental measurement is taken over the top surface of the mock-up, in the mid-point of each finger.



**Figure 14.-** Transversal distortion of the mock-up in terms of horizontal displacements of the fingers: experimental measurements (Leading Innova) vs. numerical analysis

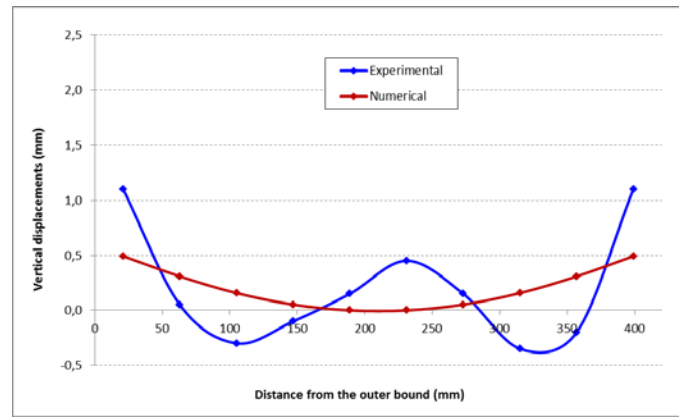
The numerical analysis results in good agreement with the experimental measurements. It must be pointed out that the numerical results take advantage from the symmetry plane with respect to the longitudinal mid-plane of the mock-up. The experimental evidence shows a different behavior on the two sides of the component. This could be attributed to either the non-identical clamping conditions during the manufacturing operation or to the cutting sequence which generates a non-symmetric stress release.

#### 4.5.4 Vertical displacements

The distortion of the mock-up along the vertical direction is very relevant for the final performance of the component. Also in this case, the cutting procedure results in a differential movement among fingers. The numerical analysis shows that the maximum vertical displacement corresponds to the more external fingers while reducing its amplitude for the more internal ones. Figure 15 compares the numerical results with the experimental evidence. Once again the comparison is not fully satisfactory.

The experimental measurements show how the more external fingers present the larger vertical movement as predicted by the numerical model. However, an inverted curvature of the inner part is an unexpected result. Due to the simplification made on the geometry proposed for the mock-up, it is difficult to expect such a structural response. Moreover, previous fabrications of semi-prototypes have induced a final distortion very similar to the result of the numerical analysis shown in this work.

A possible explication for the actual distortion obtained could be either a non-perfect diffusion bonding after the HIP process at the contact interface between Stainless Steel and CuCrZr alloy or non-homogeneous material properties induced by the HT process. Hence, after cutting, the inner part of the mock-up presents a different structural behavior compared to the more external zones. Those possibilities have not been accounted for in the numerical model. In fact, the diffusion bonding has been simulated as perfect sticking between the surfaces of the 2 materials in contact at the end of the HIP plateau, and homogeneous properties have been assumed for each material.



**Figure 15.-** Vertical distortion of the mock-up in terms of vertical displacements of the fingers: experimental measurements (Leading Innova) vs. numerical analysis

## 5. Conclusions

The simplified prototype of the ITER First Wall has been fabricated. The numerical analysis of the different phases of the entire manufacturing process has been presented making use of a fully coupled thermo-mechanical solution. HIP, heat treatment, machining and cutting operations have been simulated. A suitable fully temperature dependent visco-elastic visco-plastic constitutive model has been proposed, including strain hardening, thermal softening, annealing and phase transformation contributions.

The thermo-mechanical loading in terms of temperature and pressure evolution has been prescribed as for the actual processing. The machining and cutting sequences have been considered following the fabrication procedure.

Perfect sticking between stainless steel casing and CuCrZr alloy due to diffusion bonding has been assumed at the end of the HIP plateau.

The phase transformation induced by the rapid cooling during HT has been modeled by a saturation law able to modify the material properties from their initial values (before HT) to their final values (higher stiffness and strength induced by the the HT process).

Both cutting and machining operations have been modeled by an element deactivation process which removes the material according to the cutting sequence.

Experimental measurements have been carried out by LEADING INNOVA to understand the consequences induced to the mock-up by the subsequent manufacturing phases in terms of the final distortion and residual stresses. Hence, the hole-drilling method has been used to measure the stress/strain evolution during the entire cutting process. Moreover, a dimensional control after HIP and HT processes and after the cutting/machining operations has been recorded.

The comparison between the numerical results and the experimental evidence has demonstrated the prediction capabilities of the numerical procedure proposed. Nevertheless, the agreement with the experimental evidence was not always fulfilled. It must be remarked the complexity of both the fabrication processes as well as the difficulties encountered while simulating the entire fabrication chain. Moreover, on one hand, more precise techniques are necessary to improve the measurements of residual stresses such as neutron diffraction methods. On the other hand, more sophisticated constitutive models including microstructure evolution law are welcome to tackle both the diffusion bonding during HIP and the phase transformation during the HT process.

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