

DEPARTMENT OF AEROSPACE ENGINEERING

COLLECTED DATA FOR TESTS ON A NACA 23012A AEROFOIL

by

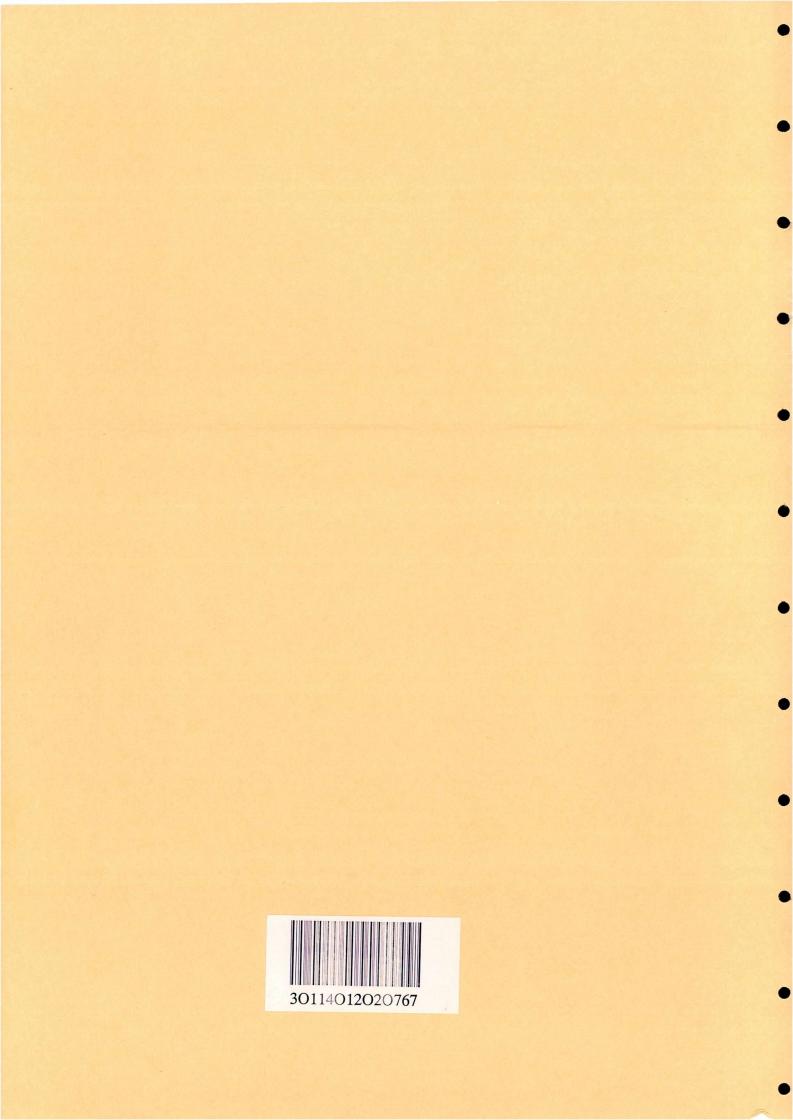
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April 1992



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Herein is presented the collected data for tests in which a NACA 23012A aerofoil was subjected to a variety of displacements in pitch about the quarter-chord location at low Reynolds numbers.

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NACA 23012A

CONTENTS

	Nomenclature	•	•	•	•	•	•	•	•	•	•	•	•	•	•	1
1	Introduction	•	•	•	•	•	•	•	•	•	•	•	•	•	•	1
2	Description of Test Fac														•	1
	2.1 Aerofoil and Wind Tunn															1
	2.2 Pitch-drive Mechanism		•		•				•			•				2
	2.2.1 Actuator 2.2.2 Command Signal .	•	÷	÷	•	·		•	•	·	·	•	·		•	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	2.3 Instrumentation and Da	ta I	Log	gin	g	1					÷.				÷.	2
	2.3.1 Pressure Transducers				<i>.</i>											2
	2.3.1 Pressure Transducers 2.3.2 Dynamic Pressure .					•										2
	2.3.3 Incidence													•		2
	2.3.4 Acquisition Unit .	•	•	•	•	٠	•	•	•	•	•	•	•	•	•	3
3	Test Series and Proced	ure	e.	•	•	•	•	•	•		•	•	•	•	•	3
	3.1 Static Experiment .	•	•	•		•	•	•	•	•	•	•	•	•	•	3
	3.2 Ramp Experiment .	•	•	·	•	•	•	•	•	•	•	•	•	•	•	4
	3.3 Sinusoidal Experiment	•		•		•	•	•	•	•	•	•		•	•	4
	3.4 Procedure		•	•	•	•	•		•	•	•		•	•	•	4
	3.5 Data Presentation .	•	·	•	•	•	•	•	•	·	•	•	•	•	•	4
4	Results and Discussion					1						÷.,	•		-	4
- 7	4.1 Tunnel Performance .															4
	4.2 Averaging of the Data															4
	4.3 Test Data	•		·	÷	÷	÷	÷	÷	÷		•	:	:		5
A	cknowledgements	•	•	•	•	•	•	•	•	•	•		•	•	•	5
R	eferences	•	•	•	•	•	•	•	•	•	•	•	•	•	•	5
Т	ables	•	•	•	•	•	•	•	•	•	•	•	•	•	•	6
-																

Figures

NOMENCLATURE

С	chord
Cm	pitching-moment coefficient
Cn	normal force coefficient
Cp	pressure coefficient
Ct	"thrust" force coefficient
D.P.	dynamic pressure ($\rho V^2/2$)
k	reduced frequency ($\omega c/2V$)
r	reduced pitch-rate (c/2V)da/dt
Re	Reynolds number
V	velocity
x/c	chordwise dimension
α	angle of attack
ω	rotational velocity

1 INTRODUCTION

The phenomenon of dynamic stall, the onset of which is largely controlled by the behaviour of the viscous boundary layer on the aerofoil surface, plays an important role in the successful design of the helicopter rotor. During high speed forward flight conditions, the blades on the retreating side of the rotor disc encounter a reduced dynamic pressure, and hence rotor trim requirements dictate a high aerofoil lift coefficient. These high lift coefficients are generated through large angles of incidence, often exceeding the maximum static stall value and so take advantage of the dynamic effects on the stalling process. Aerofoil dynamic stall is imprecisely understood and is currently the subject of extensive experimental and theoretical investigation by, amongst others, Beddoes¹. As has been shown by Harris and Pruyn², attempts to predict rotor performance without a mathematical model of retreating-blade stall have Furthermore, the met with little success. modelling is complicated by the highly threedimensional flowfield of the rotor. It is clear, however, that, in order to formulate modelling techniques for use in rotor airload calculations, a basic understanding of the unsteady stall process must be established.

An experimental investigation of retreatingblade stall, together with a boundary-layer analysis on a model rotor, by **McCroskey et al**^{3,4} pointed to the modelling of blade dynamic stall by an oscillating aerofoil in the nominally two-dimensional flow environment of a wind tunnel. Many such experiments of aerofoils oscillating through stall have since been performed, and data have been gathered for both the analysis of the fluid mechanics of the dynamic stall phenomenon itself and for use in mathematical model development.

As part of this investigation, in recent years, in the dynamic stall facility at the University of Glasgow^{5,6,7}, two-dimensional data have been acquired from experiments on a number of aerofoils under a variety of motion types. These aerofoils can be divided into two groups: the first is a family of cambered aerofoils generated from the NACA 23012 section and intended for the examination on helicopter blades of the transition from trailing-edge to leading-edge stall and the mechanism of reattachment; the second is a series of symmetrical sections for use on large-scale vertical-axis wind turbines. This report presents the collected data from tests performed on a model of a NACA 23012A aerofoil in steady and unsteady conditions. This aerofoil, which belongs to the first of these groups was designed by Niven and Galbraith⁸ by modifying the NACA 23012 aerofoil section downstream of the quarter-chord location in order to create a region of reflex camber at the trailing edge. The coordinates for the aerofoil section are listed in Table 1, and a brief descripton of the experimental apparatus and techniques is presented below.

2 DESCRIPTION OF TEST FACILITY

2.1 Aerofoil and Wind Tunnel

The general arrangement of the aerofoil in the wind tunnel was as shown in **Figure 1**. The aerofoil, of chord length 0.55m and span 1.61m, was constructed of fibre glass mounted on an aluminium spar and filled with an epoxy resin foam. The hand-finished surface was very smooth, and the profile accurate to better than 0.1mm. The instrumented model was fitted vertically into the University of Glasgow's "Handley Page" wind tunnel.

The "Handley Page" low-speed wind tunnel is an atmospheric-pressure closed-return type with a 1.61x2.13 octagonal working section (**Figure 2**) in which a wind velocity of 61ms⁻¹ can be attained. The model was pivoted about its quarter-chord axis on two tubular steel shafts connected to the main support via two selfaligning bearings. A single thrust bearing on

1

the top support beam took all the weight. The dynamic and aerodynamic loadings from the aerofoil were reacted to the tunnel framework by two transversely mounted beams.

2.2 Pitch Drive Mechanism

2.2.1 Actuator

Angular movement of the model was obtained using a linear hydraulic actuator and crank mechanism. The actuator was mounted horizontally below the tunnel working section on the supporting structure, with the crank rigidly connected to the tubular part of the spar by a welded sleeve and keyway. The acuator was a UNIDYNE 907/1 type with a normal dynamc thrust of 6.1KN operated from a supply pressure of 7.0MNm⁻². A MOOG 76 series 450 servo valve was used via a UNIDYNE servo controller unit to control the movement of the actuator. A suitable feedback signal for the controller was provided by a precision linear angular displacement transducer geared to the main spar of the model.

2.2.2 Command Signal

The model's angle of attack was incremented by the actuator controller. The input signal during the static tests was provided under software control by the data acquisition unit's own digital-to-analogue converter. This was possible because, during the sampling, the angle of attack was fixed and sufficient time was available between sampling to set the model at the required angle of attack. The two activities were separate and were performed sequentially.

Such was not the case during the unsteady tests, however, where sampling and control of were required motion model's the Therefore, during constantsimultaneously. pitch-rate "ramp" experiments, the input signal was provided by a separate function generator, comprised of an PET microcomputer and an 8bit digital-to-analogue converter. A ramp signal was obtained by simply incrementing the PET's output lines sequentially from 00000000 to 11111111, while the desired delay between increments was generated by software using a memory location as a counter. The input signal during oscillatory experiments was provided by an IEEE-controlled synthesised function generator, the amplitude and frequency of which was set via the MINC microcomputer at the start of each test condition.

2.3 Instrumentation and Data Logging

2.3.1 Pressure Transducers

To provide the chordwise pressure distribution at mid-span, thirty ultra-miniature silicon strain-gauge pressure transducers (ENTRAN EPI-080-5 and KULITE LSQ-57) were installed just below the surface of the centre section of the model. The transducers were of sealed-gauge type with one side of the pressure-sensitive diaphragm sealed to a reference pressure during manufacture. Each transducer was fitted with a temperature compensation module, which minimised the change in zero-offset and sensitivity with temperature. The locations of the pressure transducers in the model are illustrated in Figure 3.

The low voltage outputs from the thirty presure transducers were suitably amplified and conditioned by a bank of differential amplifiers. The conditioned signals were passed to a "sample and hold" unit^{5,9} to overcome the timeskew problem arising from the sequential conversion of the anlogue signals into digital form.

2.3.2 Dynamic Pressure

The dynamic pressure in the wind tunnel working section was determined by a pitot-static probe mounted on the tunnel side wall approximately one chord length upstream of the aerofoil's leading edge. The probe was connected to a FURNESS FC012 micromanometer, which provided an analogue signal suitable for the data acquisition unit's analogue-to-digital converter. This dynamic pressure was recorded as the sample-and-hold unit was triggered to sample the output from the pressure transducers.

2.3.3 Incidence

The instantaneous angle of attack of the aerofoil was determined by an angular displacement transducer geared to the model's main spar. The signal voltage from the transducer was fed into an amplifier/splitter to produce three signals for the following purposes:

- i) connection of the multiplexer for recording the aerofoil's angle of attack;
- ii) connection of the Schmitt trigger for initiation of data sampling when a preset incidence (voltage) was attained;
- iii) a feedback signal to the hydraulic actuator controller.

2.3.4 Acquisition Unit

The actual data acquisition unit was a DEC MINC-11 microcomputer, configured with an LSI-11/32 16-bit microprocessor and laboratory modules which included:

- i) an analogue-to-digital converter module, with a 16-channel multiplexer incorported. The converter was a 12-bit successive approximation type with a conversion time of of 30μ s, but the multiplexer's settling time and the need to transfer the data from the analogue-todigital converter into system memory increased the conversion time to 44μ s;
- ii) a multiplexer module, of 16 single-ended channels, which increased the number of channels that could be sampled to 32;
- iii) a real-time clock module, with two Schmitt triggers. This was used as a time-base generator to accurately set the For ramp sampling frequency. experiments, the sampling frequency was determined at run time from the pitch rate and the requirement that 128 sample sweeps should be obtained when the incidence was increasing and the same number when the aerofoil was sitting at its final incidence. However this specification was qualified by the fact that data were required to be recorded at the final incidence for no longer than 4 seconds and that the maximum sampling frequency which could be attained was 550Hz. One of the Shmitt triggers was used to initiate data sampling, by setting its reference voltage to a value corresponding to the angular

displacement transducer's output for the required starting angle of attack. For oscillatory tests, the sampling frequency was determined from the frequency of oscillation and the requirement that 128 sample sweeps should be obtained during each cycle;

iv) a digital-to-analogue converter module which housed four independent 12-bit digital to analogue converters. This was used to provide the command signal for the hydraulic actuator during static tests.

The path of data flow and system layout is shown diagrammatically in **Figure 4**. The main control programs for the tests were written in FORTRAN IV, as described by **Murray-Smith and Galbraith¹⁰**. The programs prompt the user for specific run information before calling a specialised subroutine written in MACRO-11 assembly language to receive and store the digitised data. The timing and control of the analogue-to-digital converter and associated circuitry was performed by the processor's hardware, but channel selection and data management were achieved under software control.

3 TEST SERIES AND PROCEDURE

3.1 Static Experiment

A number of experiments were performed under steady conditions. Once the wind velocity had reached the required value, the aerofoil was rotated about its quarter-chord axis until it was positioned at the incidence at which the first set of data were to be recorded. Usually, this was approximately -2° . The model's angle of attack was then increased in steps of approximately 0.5°. After each increment in incidence, the flow was allowed to stabilise for a few seconds before each transducer's output was sampled 100 times and the mean value for each was stored. After 64 sweeps of data had been recorded, the model was returned to its starting position. Data sampling was maintained at the same rate on the return arc in order to record any delay in the reattachment of flow.

3.2 Ramp Experiment

During a ramp test the aerofoil was rotated about its quarter-chord axis over a preset arc at a constant pitch-rate. Five cycles of 256 data sweeps were recorded during each experiment. Between each ramp, the model sat at the finishing angle for five seconds, moved smoothly back to the starting angle in five seconds and sat at this position for another five seconds. Experiments were performed both when the pitch-rate was positive ("ramp up") and when it was negative ("ramp down").

3.3 Sinusoidal Experiment

For this experiment, the model was rotated about its quarter-chord axis so that its angle of attack varied sinusoidally with time. The amplitude and frequency were controlled by the function generator. During each oscillatory cycle 128 data sweeps were recorded and logged, with data being sampled during ten cycles.

3.4 Procedure

Before each individual set of tests, the tunnel was shut down and the air flow allowed to cease before the transducer offsets were logged. Immediately after these values were recorded, the appropriate data acquisition routine was initiated whilst the tunnel was brought up to speed and thence data gathered as per the software prompts. The tunnel was then shut down, offsets logged again and further tests were performed in the manner described above.

3.5 Data Presentation

All data collected by the data acquisition routines were stored in unformatted form on magnetic tape. A library of programs (coded in FORTRAN 77) is available for the reduction, presentation and analysis of the data on a DEC MICROVAX 3400. By applying offsets, gains and calibrations, the data reduction programs convert the cycles of raw data into averaged or unaveraged non-dimensional pressure coefficients. As described by Leitch and Galbraith¹¹, these data are stored on the

University of Glasgow's aerofoil database. The airloads are determined by suitably integrating the pressure coefficient values.

4 RESULTS AND DISCUSSION

4.1 Tunnel Performance

Assessment of the quality of the data can only be made with a clear insight of the tunnel effects. Unfortunately the tunnel performance was such that, for the time scales of the model motion, it was not possible to hold the dynamic pressure in the working section constant whilst altering the blockage due to the pitching of the aerofoil. During the static tests (i.e. $\mathbf{k}=0.0$ and $\mathbf{r}=0.0$), this variation was as illustrated in **Figure 5**, where it can be seen that there was approximately a 30% reduction in dynamic pressure as the angle of attack was increased from 0° to 30°. As illustrated in **Figures 6** and **7**, this reduction in dynamic pressure decreased as reduced frequency increased.

Figure 8 reveals that, during ramps, there was a drastic reduction and subsequent unsteadiness in the dynamic pressure during a test. The model was pitched to an incidence of 40° so that uniform ramp conditions existed at stall. Once the aerofoil had stalled, however, all significant data had already been collected and the corresponding dynamic pressure reduction was only in the region of 10%. The subsequent data are of little relevance to the current work and is presented merely for completeness.

4.2 Averaging of the Data

The main data in this report are the average of a number of cycles. Individual cycles are presented in **Figures 9** and **10** where it may be seen that, whilst minor random differences do exist from cycle to cycle, the salient features are highlighted by the averaging process. In addition, the sweep at which any event occurred did not vary. Therefore the given data may be considered as typical of aerofoil performance during any given individual cycle. This is particularly relevant when considering the detailed flow phenomena of separation and reattachment.

4.3 Test Data

The test data are grouped for each motion type with compact details of the specific tests listed in **Tables 2** to **5**.

ACKNOWLEDGEMENTS

The authors wish to acknowledge the encouragement and support of their colleagues both academic and technical.

The research was performed with the financial support of the Science and Engineering Research Council and Westland Helicopters plc via SERC CASE award number 8051/3408, and the Royal Aircraft Establishment under MOD aggreement 2048/026.

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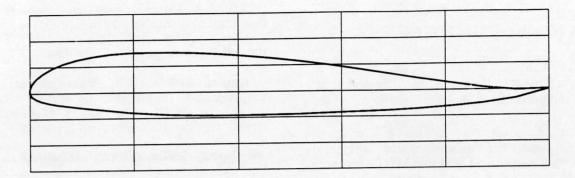
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NACA 23012A

TABLE 1 : NACA 23012A AEROFOIL PROFILE AND
COORDINATES



Upper S	Surface	Lower Surface					
Station	Ordinate	Station	Ordinate				
0.000	0.000	0.000	0.000				
-0.044	0.802	0.436	-0.681				
0.337	1.694	1.229	-1.226				
1.166	2.657	2.354	-1.658				
2.454	3.651	3.791	-2.008				
4.207	4.626	5.529	-2.308				
6.413	5.523	7.564	-2.588				
9.048	6.286	9.910	-2.874				
12.069	6.876	12.588	-3.180				
15.421	7.276	15.631	-3.508				
19.042	7.503	19.077	-3.838				
22.902	7.603	22.925	-4.123				
27.060	7.597	27.083	-4.333				
31.507	7.479	31.530	-4.471				
36.224	7.241	36.247	-4.540				
41.195	6.872	41.216	-4.547				
46.399	6.365	46.418	-4.498				
51.816	5.725	51.831	-4.401				
57.424	4.964	57.436	-4.261				
63.202	4.103	63.209	-4.077				
69.125	3.169	69.128	-3.843				
75.169	2.202	75.169	-3.544				
81.310	1.257	81.306	-3.147				
87.521	0.422	87.515	-2.587				
93.773	-0.125	93.768	-1.705				
100.031	0.051	100.027	-0.050				

Coordinates in %Chord

TABLE 2 : DETAILS OF STATIC TESTS

TABLE 2.1 : SUMMARY OF STATIC TESTS (nominal)

Reynolds Number	1.5x10 ⁶
Angle of Attack	-2° to 30°

TABLE 2.2 : LIST OF STATIC TESTS (actual)

Run	Start	Sweep	Reynolds
Number		(^)	No. x 10 ⁻⁶
00101	-2	32	1.51

TABLE 3 : DETAILS OF RAMP UP TESTS

TABLE 3.1 : SUMMARY OF RAMP UP TESTS (nominal)

Starting Incidence		-1°										
Finishing Incidence		40°										
	3.0	4.5	6.0	7.5	15.0	30.0	45.0					
Pitch Rate (°s ⁻¹)	60.0	75.0	90.0	100.0	115.0	130.0	145.0					
	160.0	175.0	190.0	200.0	230.0	245.0	260.0					
	275.0	290.0	300.0	315.0	330.0	345.0	360.0					
Reynolds Number	1 7 106											

(all permutations)

TABLE 3.2 : LIST OF RAMP UP TESTS (actual)

Run	Start	Arc	Pitch Rate	Reduced	Reynolds
Number	(°)	(°)	$(^{\circ}s^{-1})$	Pitch Rate	No. x 10 ⁻⁶
			2.9	0.0004	1.50
20031	-1	41			1.50
20041	-1	41	4.4	0.0006	
20051	-1	41	6.0	0.0007	1.50
20061	-1	41	7.4	0.0009	1.51
20071	-1	41	17.9	0.0018	1.53
20081	-1	41	30.0	0.0037	1.51
20091	-1	41	45.0	0.0055	1.53
20101	-1	41	60.0	0.0075	1.51
20111	-1	41	75.3	0.0092	1.53
20121	-1	41	89.9	0.0111	1.51
20131	-1	41	102.5	0.0125	1.53
20141	-1	41	115.1	0.0142	1.51
20151	-1	41	129.6	0.0158	1.53
20161	-1	41	146.4	0.0181	1.51
20171	-1	41	159.6	0.0195	1.53
20181	-1	41	173.6	0.0215	1.51
20191	-1	40	189.5	0.0232	1.53
20201	-1	40	199.8	0.0244	1.53
20221	-1	41	229.1	0.0282	1.52
20231	-1	41	242.6	0.0296	1.48
20241	-1	40	258.5	0.0311	1.48
20251	-1	41	263.6	0.0319	1.48
20261	-1	40	276.8	0.0335	1.47
20271	-1	41	286.6	0.0346	1.48
20281	-1	41	298.5	0.0358	1.49
20291	-1	40	315.9	0.0385	1.46
20301	-1	41	324.9	0.0181	0.81
20301	-1	41	337.2	0.0411	1.47

TABLE 4 : DETAILS OF RAMP DOWN TESTS

TABLE 4.1 : SUMMARY OF RAMP DOWN TESTS (nominal)

Starting Incidence			40°		and a planta a	
Finishing Incidence			1°			
Pitch Rate (°s ⁻¹)	-5.0	-15.0	-30.0	-45.0	-60.0	
	-75.0	-90.0	-150.0	-250.0	-350.0	
Reynolds Number			1.5x10 ⁶			

(all permutations)

TABLE 4.2 : LIST OF RAMP DOWN TESTS (actual)

Run Number	Start (°)	Arc (°)	Pitch Rate (°s ⁻¹)	Reduced Pitch Rate	Reynolds No. x 10 ⁻⁶
30321	40	-41	-325.2	-0.0403	1.47
30331	40	-41	-233.9	-0.0285	1.49
30341	40	-41	-148.6	-0.0185	1.46
30351	40	-41	-84.1	-0.0105	1.46
30361	40	-41	-71.1	-0.0088	1.48
30371	40	-41	-57.6	-0.0072	1.46
30381	40	-41	-43.5	-0.0054	1.48
30392	40	-41	-29.1	-0.0036	1.47
30402	40	-41	-14.6	-0.0018	1.47
30411	40	-41	-4.5	-0.0006	1.45

TABLE 5 : DETAILS OF SINUSOIDAL TESTS

TABLE 5.1 : SUMMARY OF OSCILLATIONS ABOUT 10° (nominal)

Mean Incidence		10°										
Amplitude	4	o	6	0	8	0	10°					
Reduced Frequency	0.010	0.025	0.050	0.075	0.100	0.125	0.150	0.175				
Reynolds Number	1.5x10 ⁶											

(all permutations)

TABLE 5.2 : SUMMARY OF OSCILLATIONS OF AMPLITUDE 10° (nominal)

Mean Incidence	44	0	6°	8	o	15°	2	0°
Amplitude	nplitude 10° duced Frequency 0.010 0.025 0.050 0.075 0.100 0.125 0.13							
Reduced Frequency	0.010	0.025	0.050	0.075	0.100	0.125	0.150	0.175
Reynolds Number				1.5	x10 ⁶			

(all permutations)

TABLE 5.3 : SUMMARY OF OSCILLATIONS OF AMPLITUDE 8° (nominal)

Mean Angle	4°	6°	8°	10°	12°	17°				
Amplitude		8°								
Reduced Frequency	0.100									
Reynolds Number	1.5x10 ⁶									

(all permutations)

Run	Mean	Amp'ude	Reduced	Reynolds		
Number	O	O	Frequency	No. x 10 ⁻⁶		
10011	10	4	0.011	1.42		
10021	10	4	0.025	1.48		
10031	10	4	0.051	1.48		
10041	10	4	0.080	1.44		
10051	10	4	0.104	1.49		
10061	10	4	0.128	1.51		
10071	10	4	0.155	1.50		
10081	10	4	0.180	1.51		
10111	10	6	0.025	1.49		
10121	10	6	0.052	1.50		
10131	10	6	0.078	1.50		
10141	10	6	0.103	1.51		
10151	10	6	0.130	1.49		
10161	10	6	0.156 1.49			
10171	10	6	0.181	1.49		
10191	10	8	0.010	1.49		
10201	10	8	0.026	1.49		
10211	10	8	0.052	1.49		
10221	10	8	0.032	1.50		
10221	10	8	0.103	1.50		
10231	10	8	0.103	1.50		
10251	10	8	0.128	1.48		
10251	10	8	0.137	1.48		
10201	10	10	0.026	1.50		
10201	10	10	0.020	1.50		
10301	10	10	0.031	1.49		
10311	10	10	0.128	1.49		
10331	10	10	0.128	1.48		
10341	10	10	0.133	1.48		
10351	4	10	0.010	1.49		
10301	4	10	0.010	1.49		
10371	4	10	0.020			
10381	4	10	0.049	1.43 1.51		
10391	4	10	0.103	1.49		
10401	4	10	0.103	1.49		
10411	4	10	0.128			
10421	4	10	0.135	1.49 1.49		
10451	6	10	0.181	1.49		
10451	and the second se	10	0.020	1.40		
10401	6 6	10	0.032			
	6			1.48		
10481	0	10	0.103	1.48		
10491	6	10	0.128	1.46		
10501	6	10	0.155	1.48		
10511	6	10	0.180	1.49		
10521	8 8 8 8	10	0.010	1.50		
10531	8	10	0.026	1.46		
10561	8	10	0.104	1.47		
10571	8	10	0.129	1.49		
10581	8 8	10	0.157	1.46		
10591	8	10	0.183	1.46		

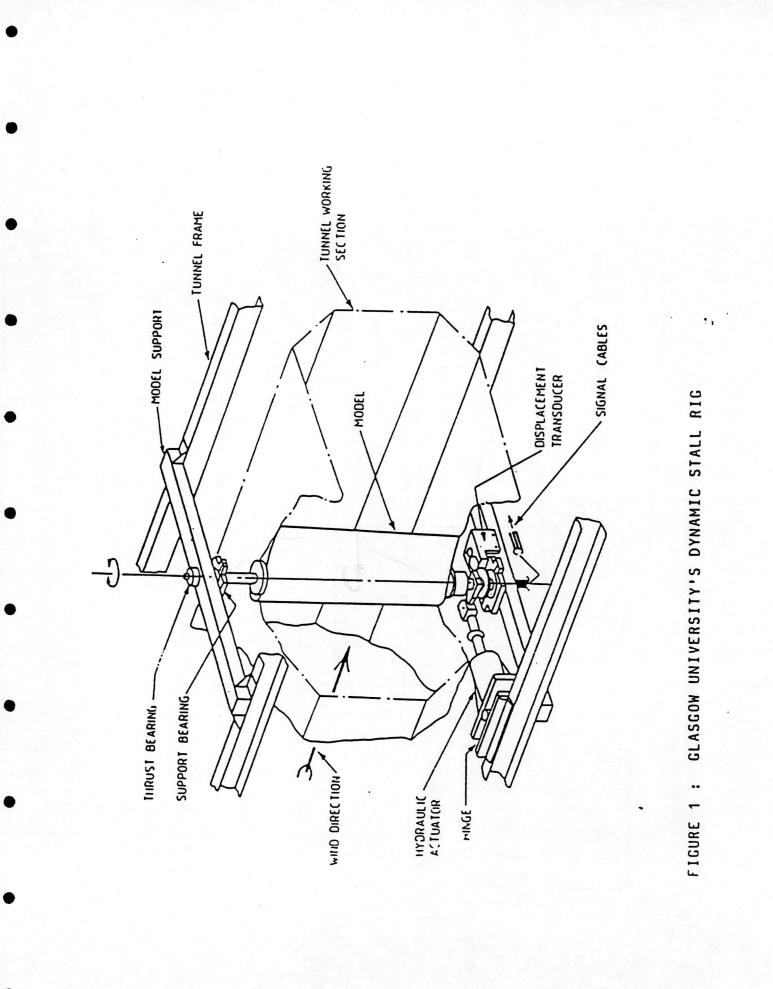
TABLE 5.4 : LIST OF OSCILLATORY TESTS (actual)

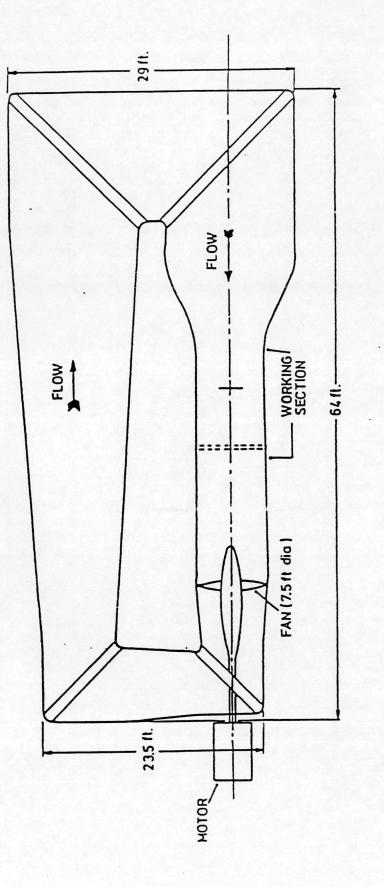
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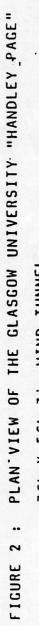
NACA 23012A

Run	Mean	Amp'ude	Reduced	Reynolds
Number	(°)	Ô	Frequency	No. x 10 ⁻⁶
10601	15	10	0.010	1.47
10611	15	10	0.026	1.46
10621	15	10	0.052	1.47
10631	15	10	0.078	1.48
10641	15	10	0.105	1.46
10651	15	10	0.130	1.48
10661	15	10	0.157	1.46
10671	15	10	0.181	1.47
10681	20	10	0.010	1.46
10691	20	10	0.026	1.46
10701	20	10	0.052	1.46
10711	20	10	0.078	1.47
10721	20	10	0.105	1.46
10731	20	10	0.130	1.47
10741	20	10	0.157	1.46
10751	20	10	0.181	1.47
10761	10	10	0.010	1.48
10771	10	10	0.026	1.50
10781	10	10	0.052	1.48
10791	10	10	0.078	1.49
10801	10	10	0.104	1.49
10811	10	10	0.131	1.48
10821	10	10	0.157	1.48
10831	10	10	0.182	1.49
10841	20	10	0.022	1.47
10851	20	10	0.032	1.48
10861	20	10	0.043	1.47
10871	20	10	0.054	1.48
10881	4	8	0.104	1.51
10891	6	8	0.105	1.50
10901	8	8	0.105	1.50
10911	10	8	0.102	1.54
10921	12	8	0.103	1.53
10931	17	8	0.103	1.53

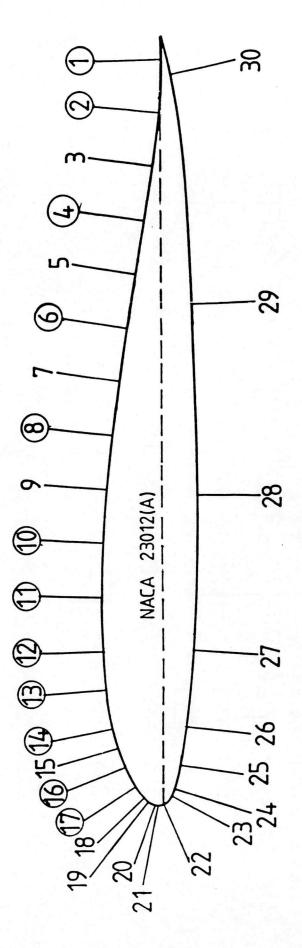
TABLE 5.4 : LIST OF OSCILLATORY TESTS (continued)







7ft X 5ft Jin WIND TUNNEL



HACA 23012(A)	To. x/c 0					25 0.05			04. ()		
	x/c I	27	50	15	10	0.075 2	05	025	01	005	0005
LOCATIO	No.	11	12	13	14	15	16	17	18	19	20
TRANSDUCK LUCATIONS	x/c	0.97	0.90	0.83	0.76	0.69	0.62	0.55	0.48	0.41	0.34
TKA	No.	1	~	8	-	2	9	4	8	0	10

FIGURE 3 : PRESSURE TRANSDUCER LOCATIONS FOR THE NACA 23012A.

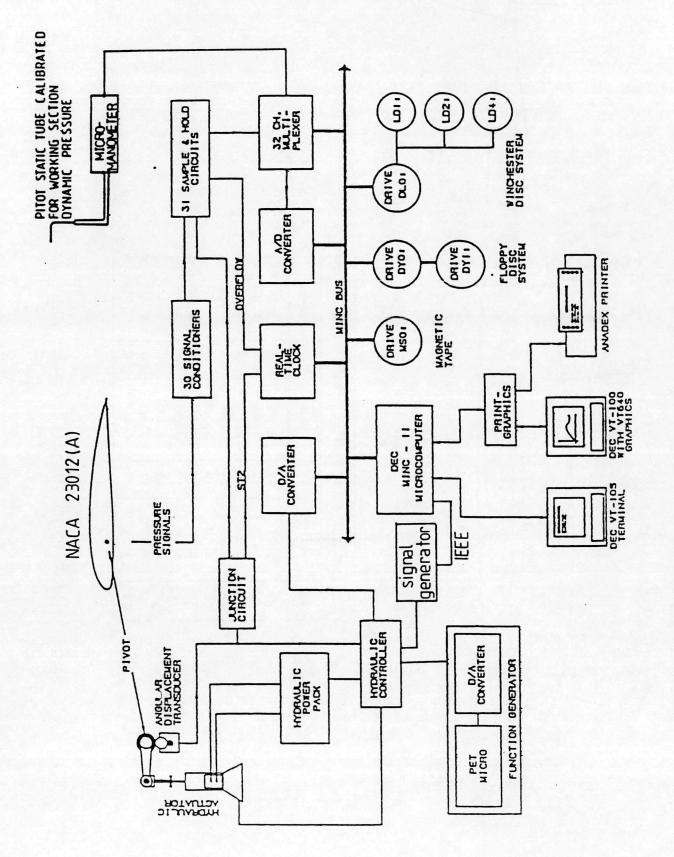
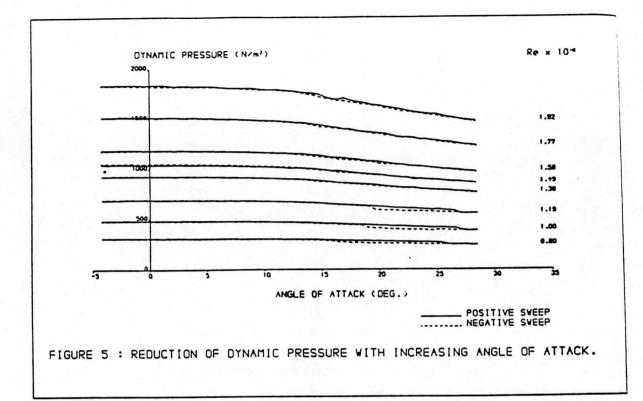
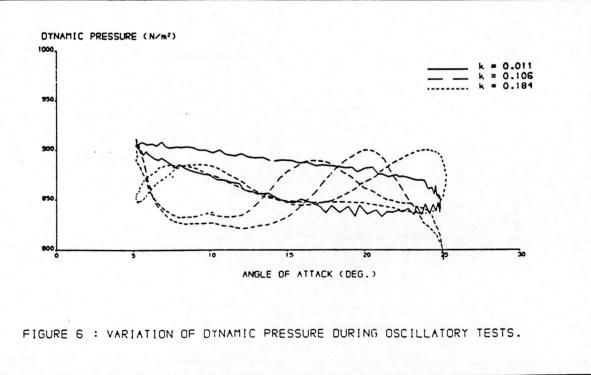
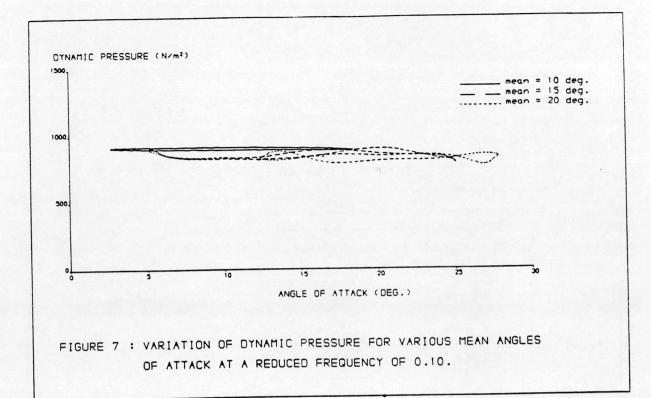


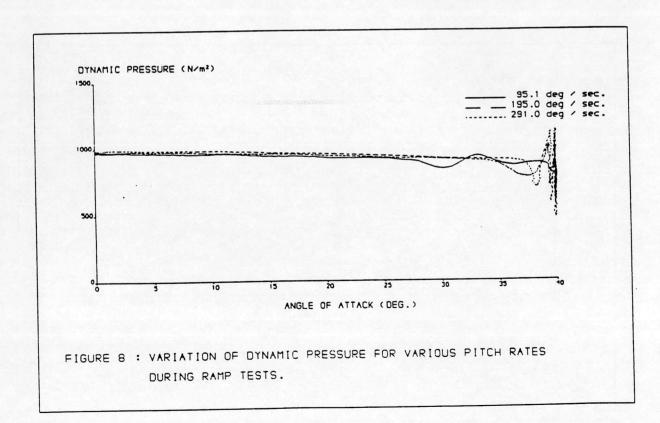
FIGURE 4 : SYSTEMATIC ARRANGEMENT OF DATA ACQUISITION AND CONTROL SYSTEM.

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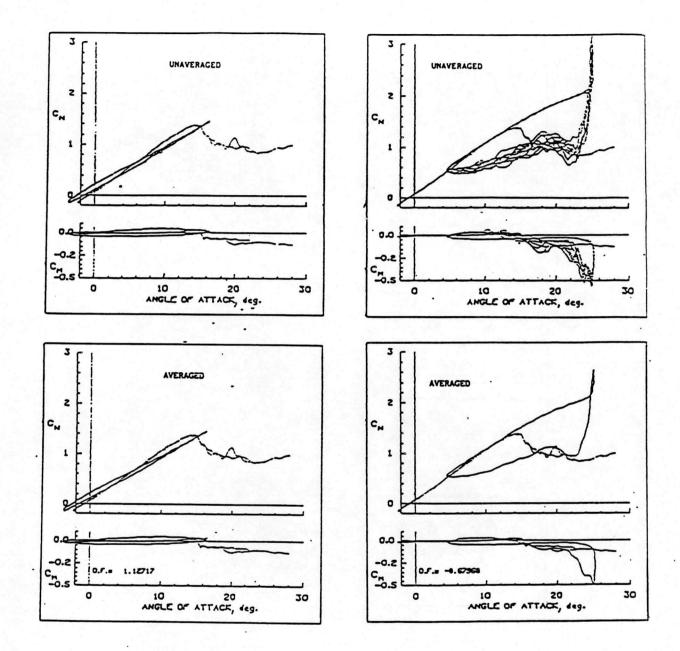


FIGURE 9: EFFECT OF AVERAGING ON THE NORMAL FORCE AND PITCHING MOMENT FOR OSCILLATORY TESTS.

and the second

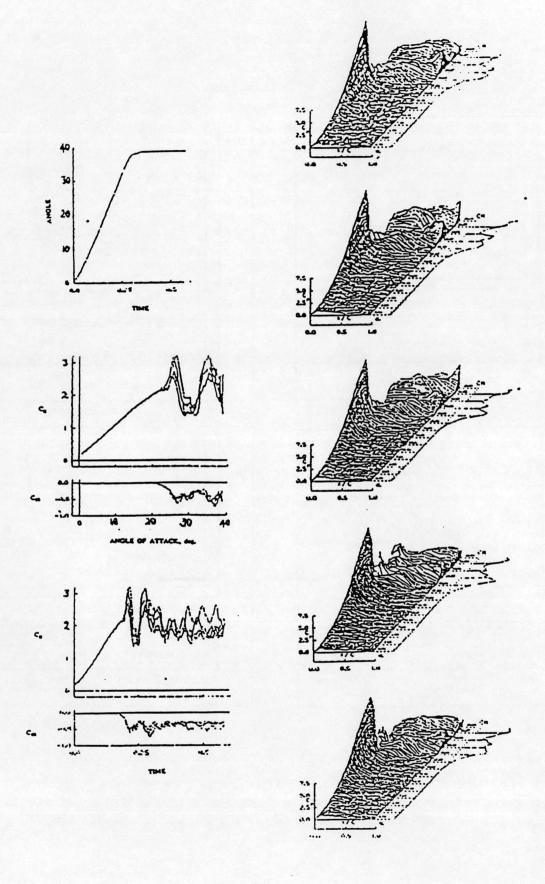


FIGURE 10: TYPICAL UNAVERAGED DATA FOR RAMP TESTS.

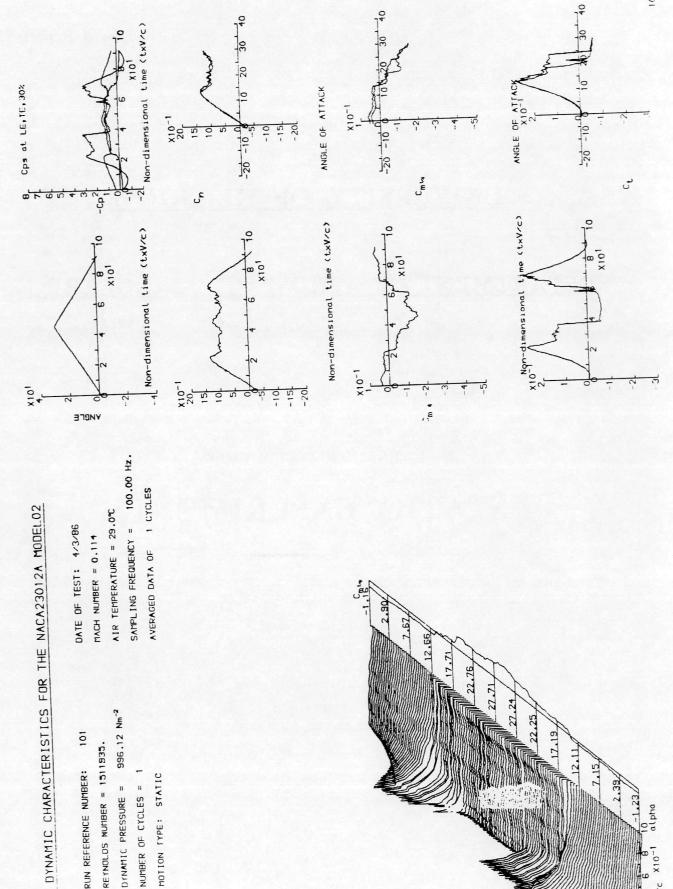
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PRESSURE DATA FROM

STATIC EXPERIMENTS



01

DrNAMIC PRESSURE = 996.12 Nm⁻² RETNOLDS NUMBER = 1511935. RUN REFERENCE NUMBER: NUMBER OF CYCLES = 1 MOTION TYPE: STATIC

0 × 0 0 + m N

7.15

1.23 alpha

X/C X10-

27

dy-

10

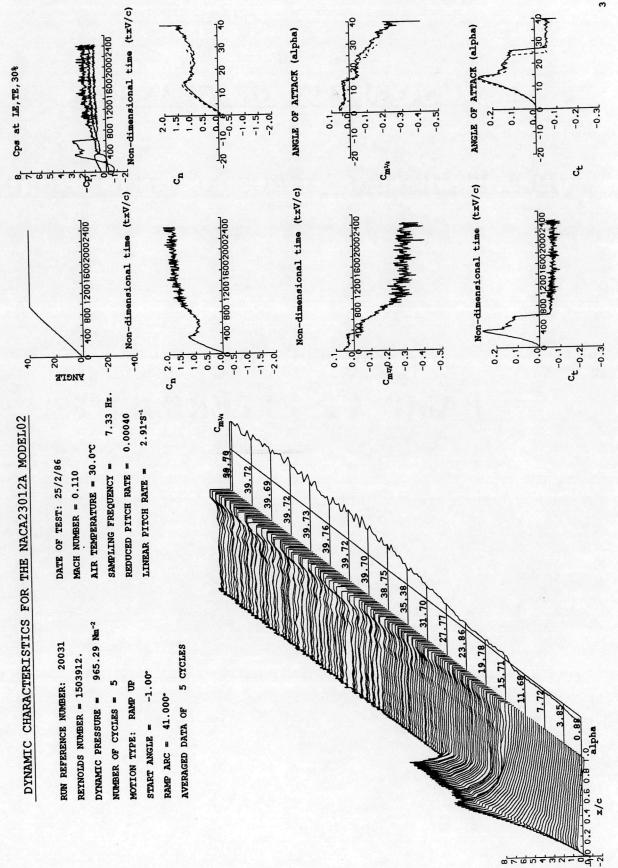
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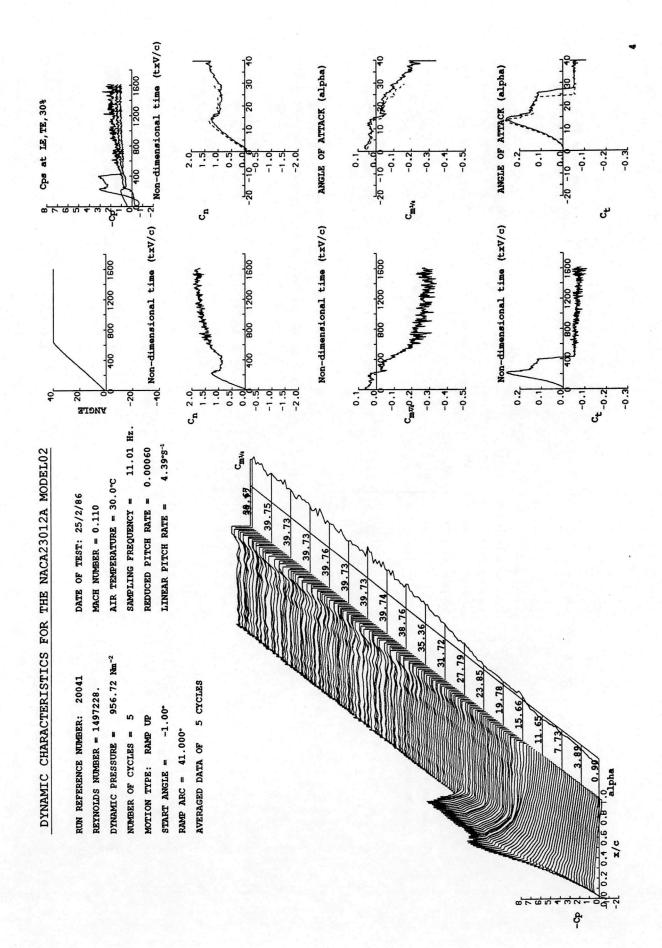
PRESSURE DATA FROM

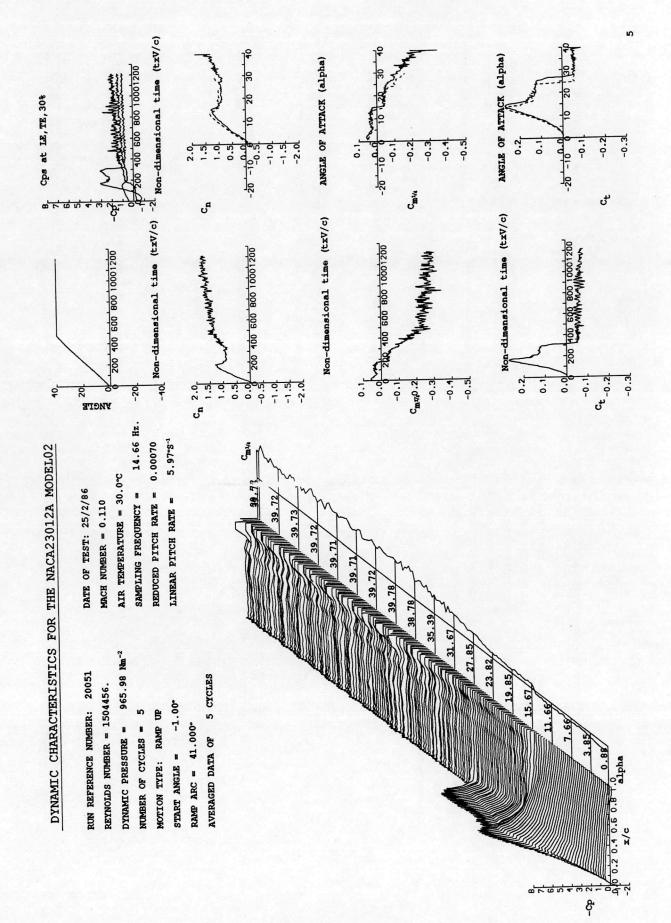
RAMP UP EXPERIMENTS



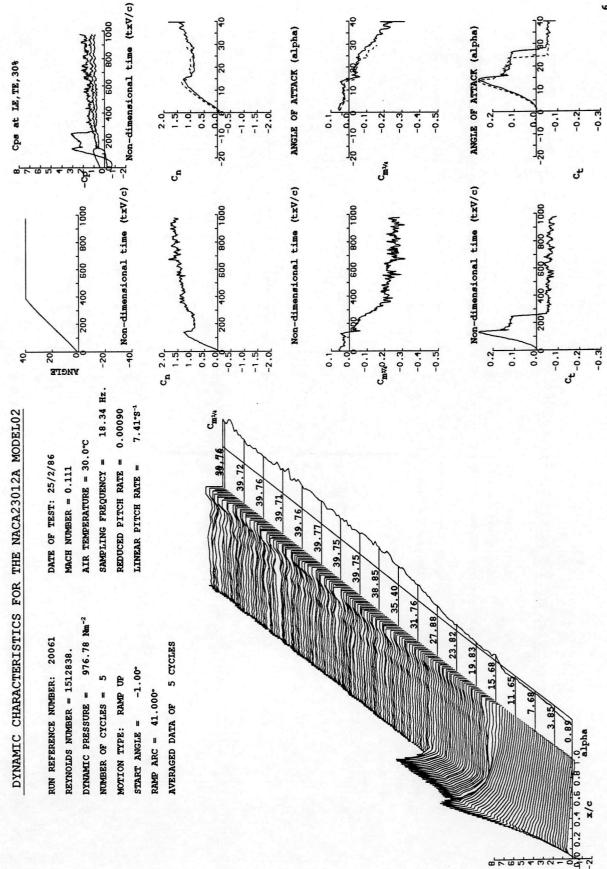
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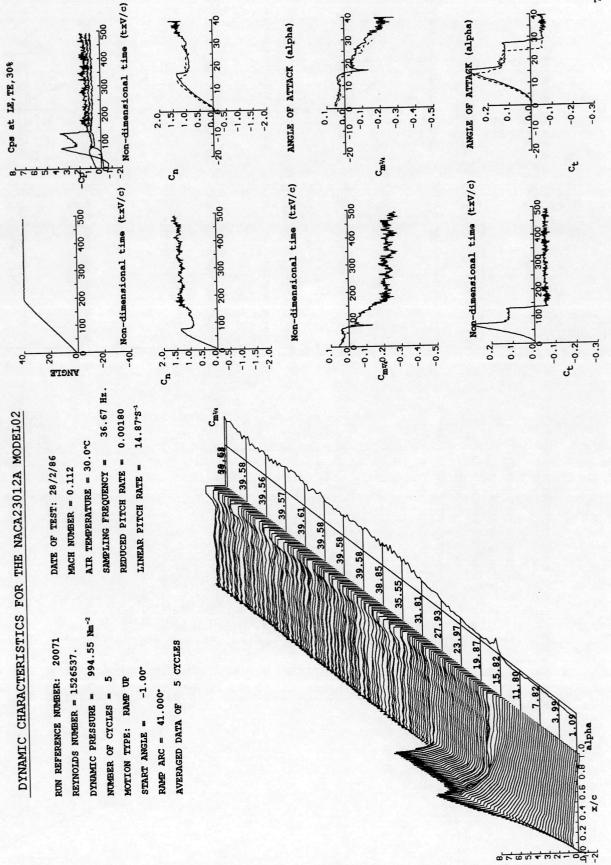




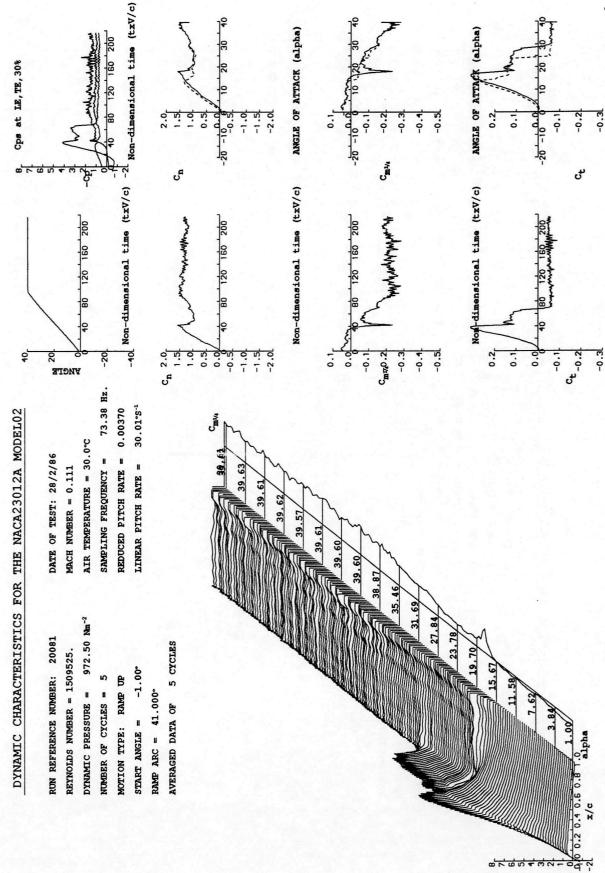
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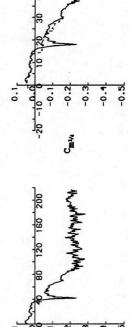
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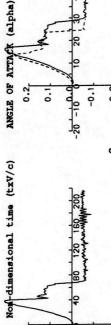


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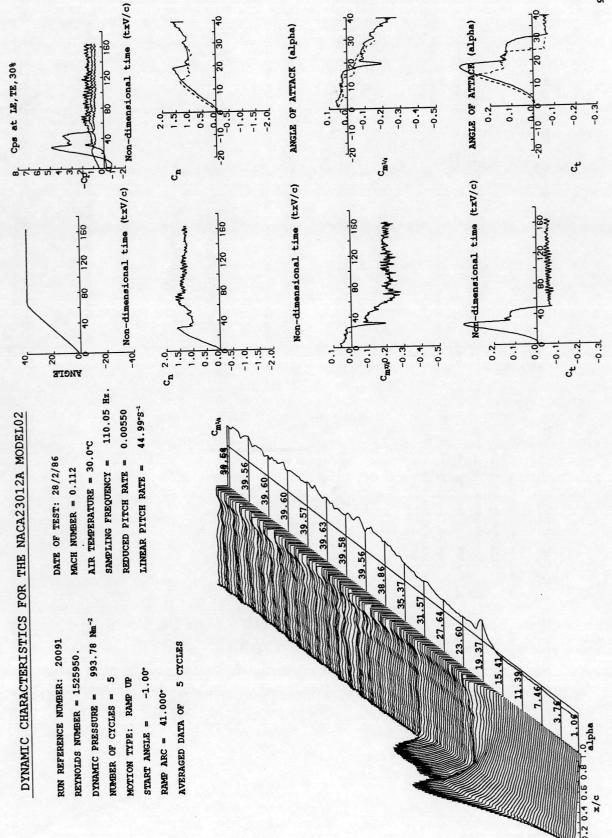


Cps at LE, TE, 30%





-CP 2

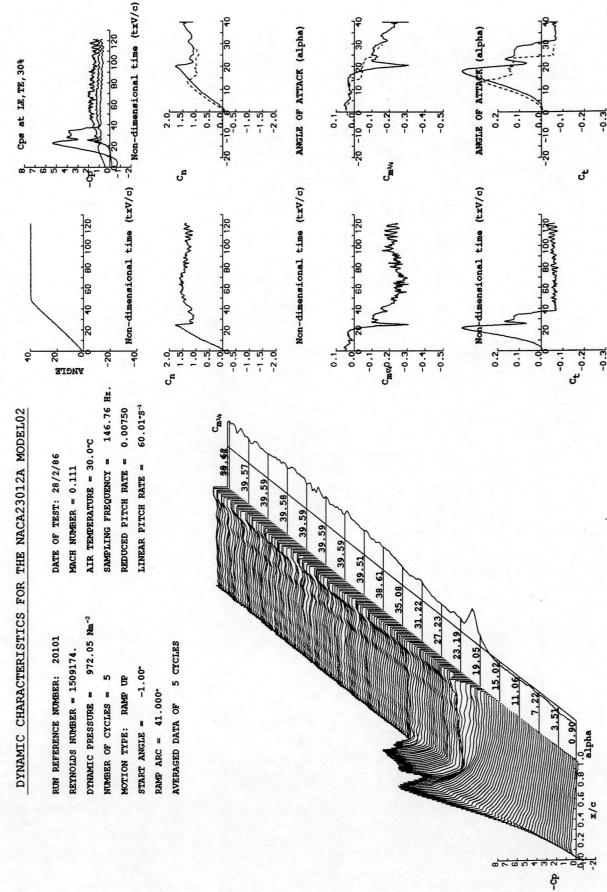


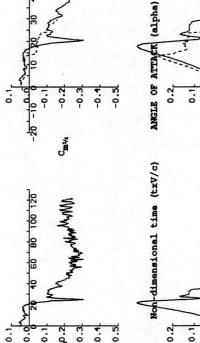
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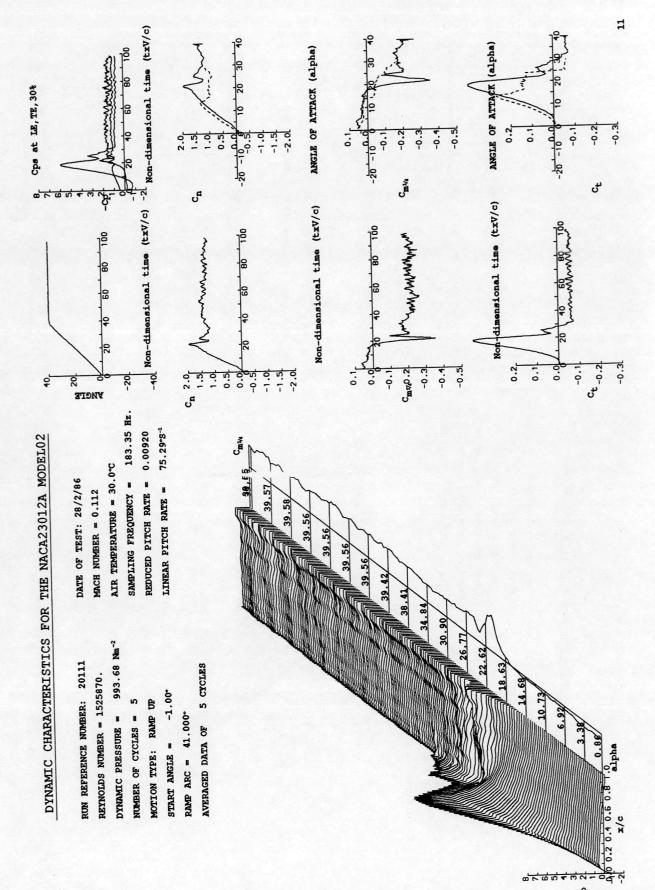
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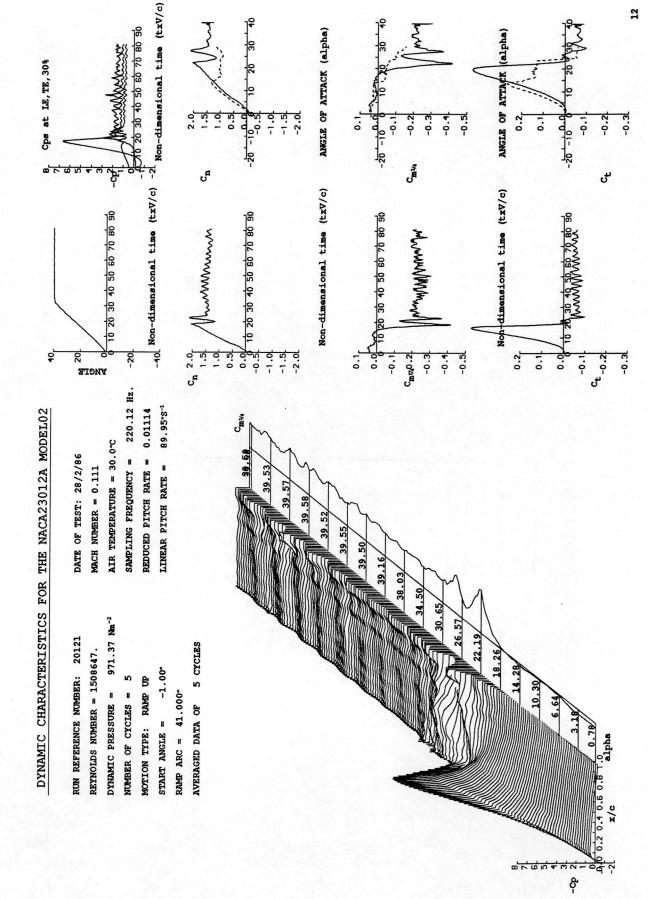


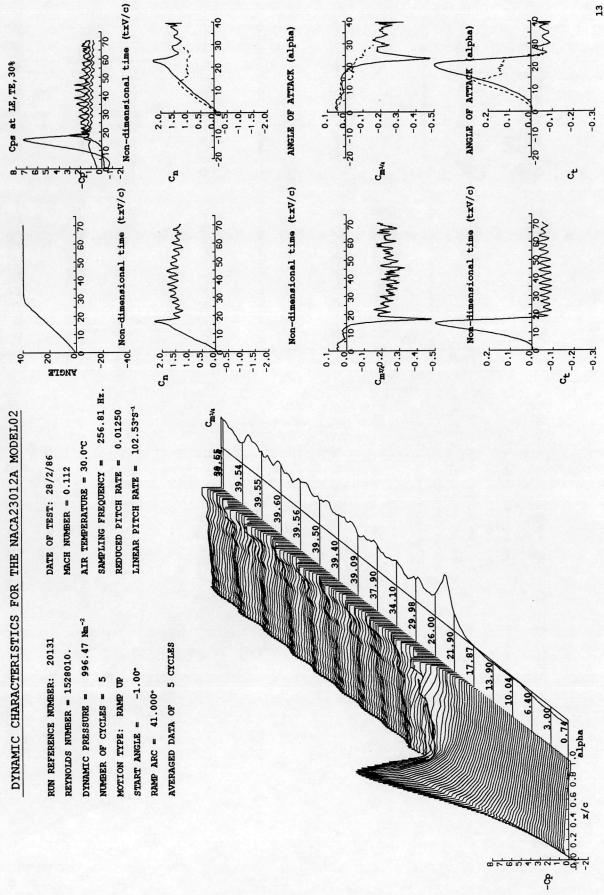


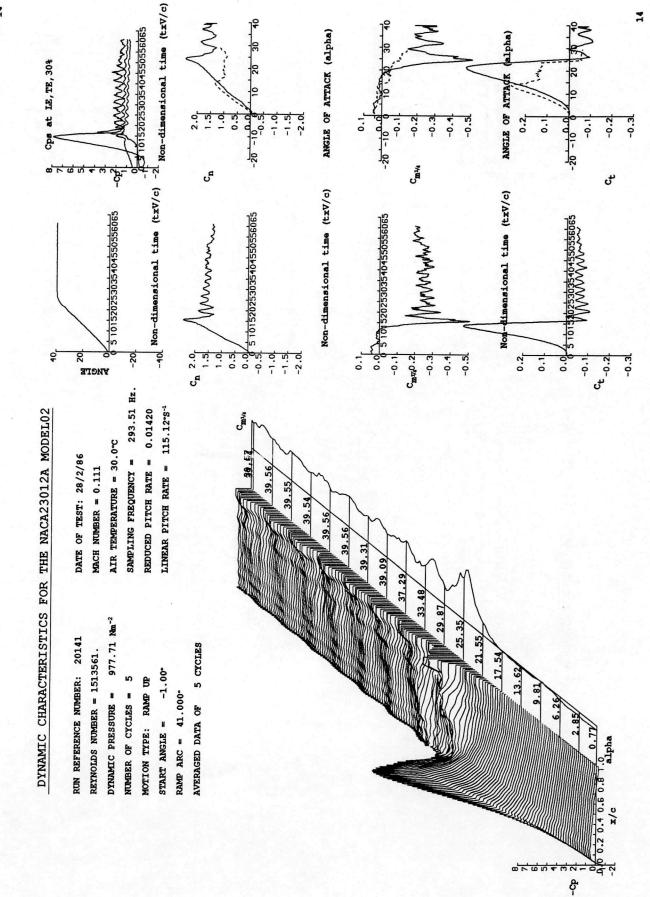


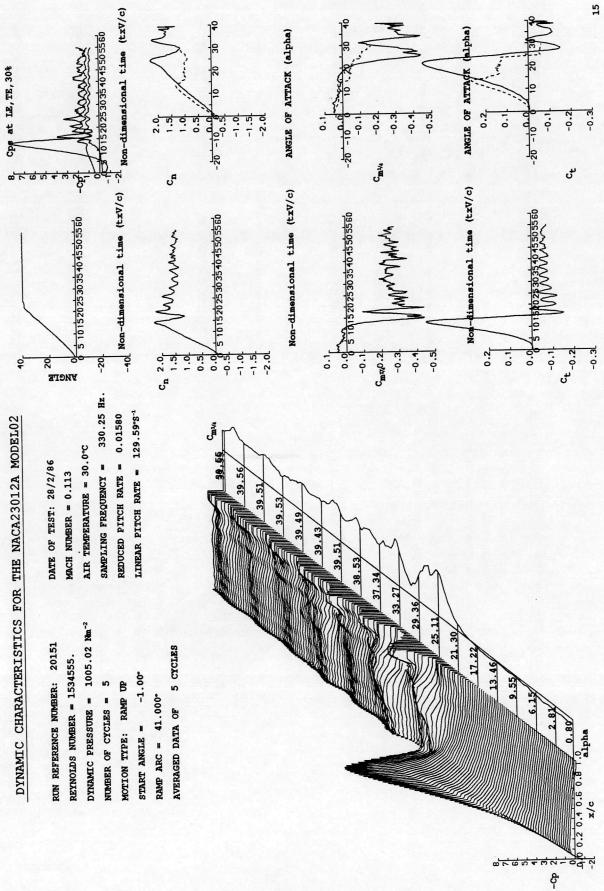
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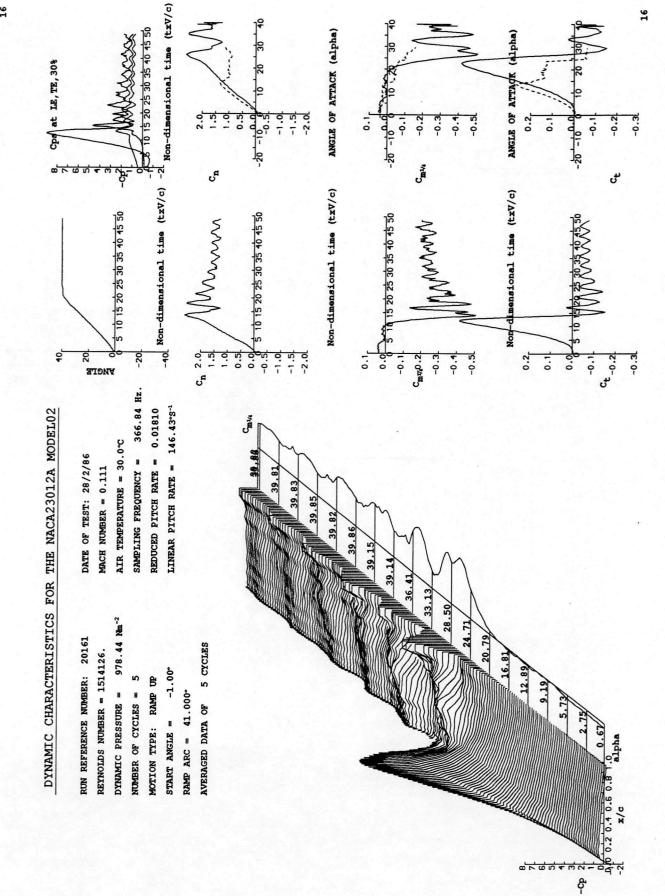
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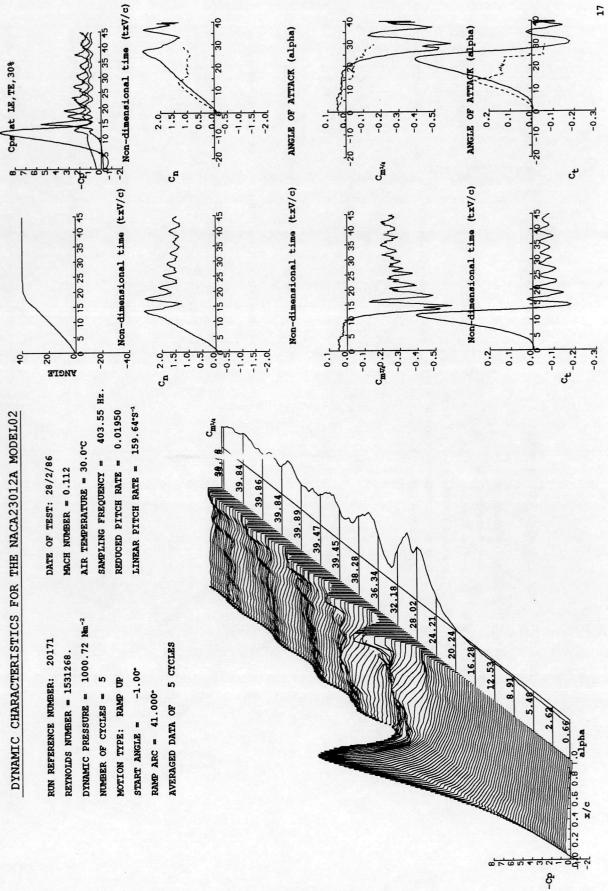


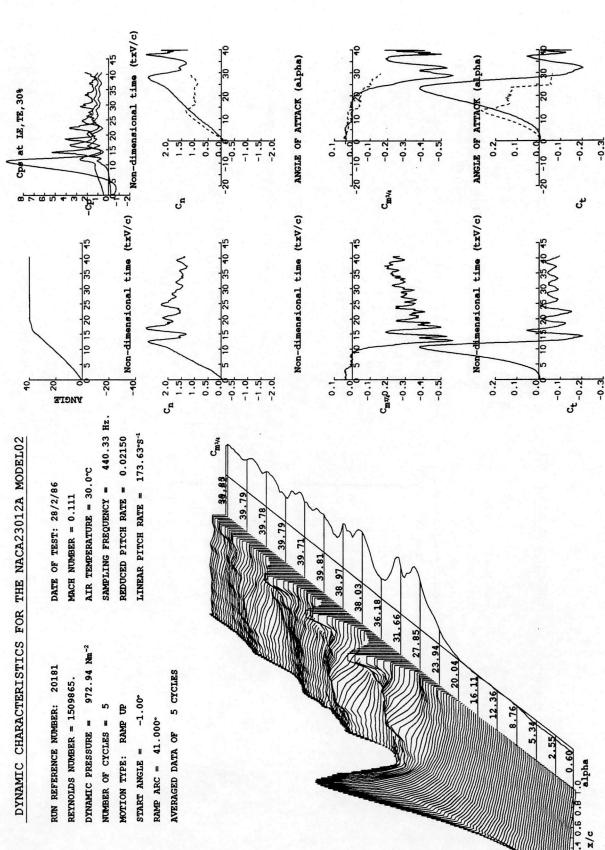


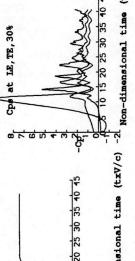


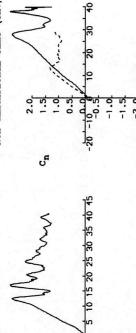


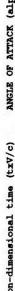


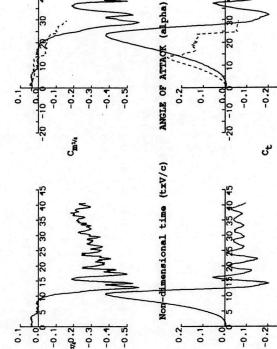




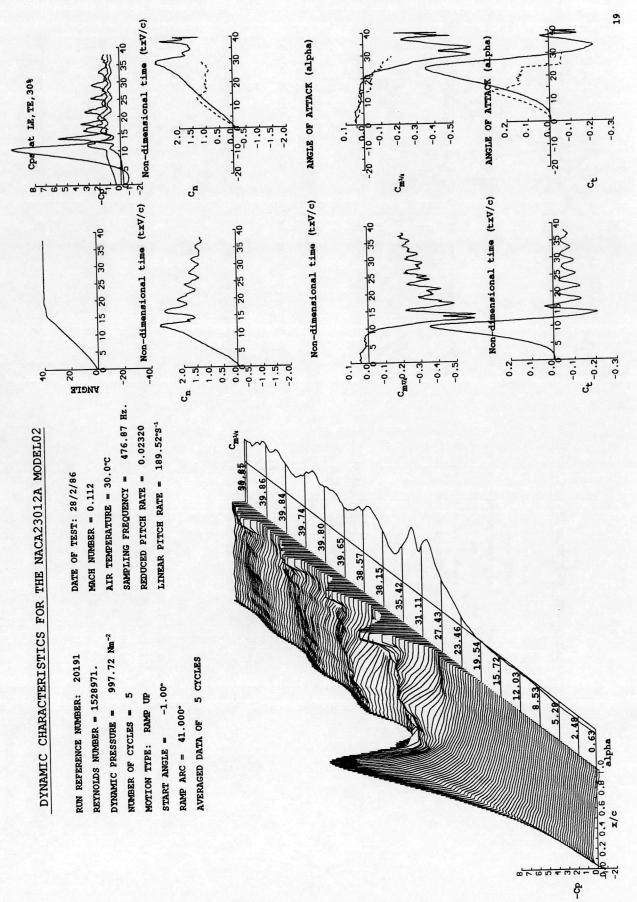


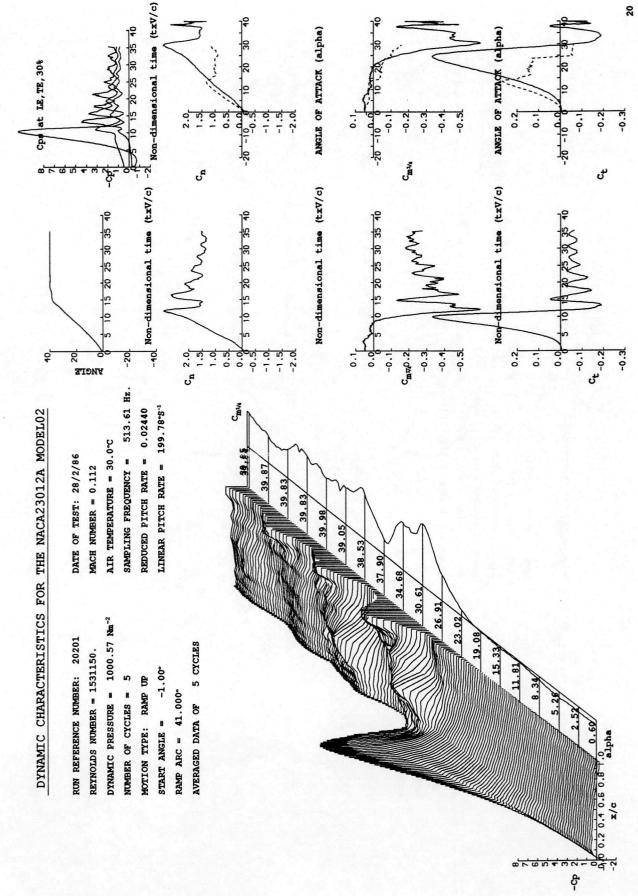


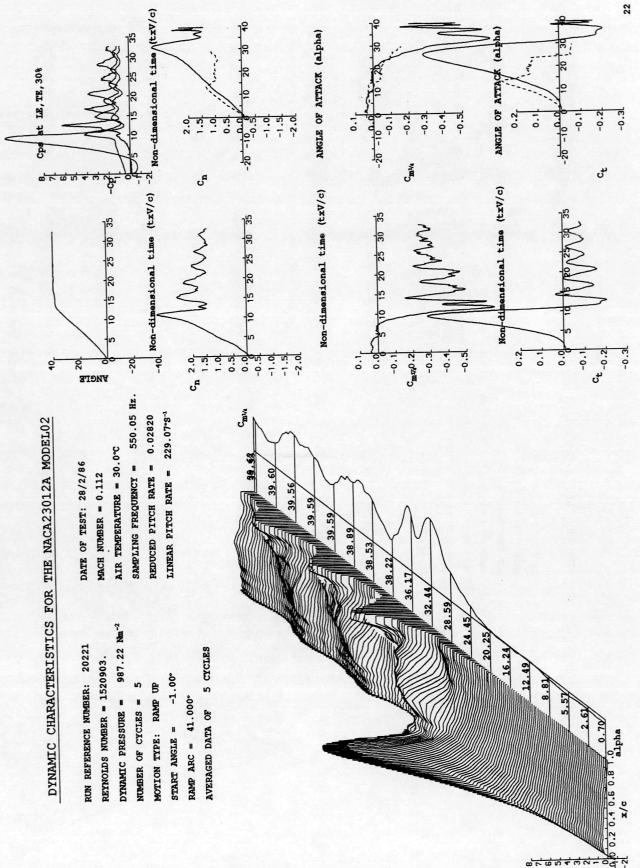




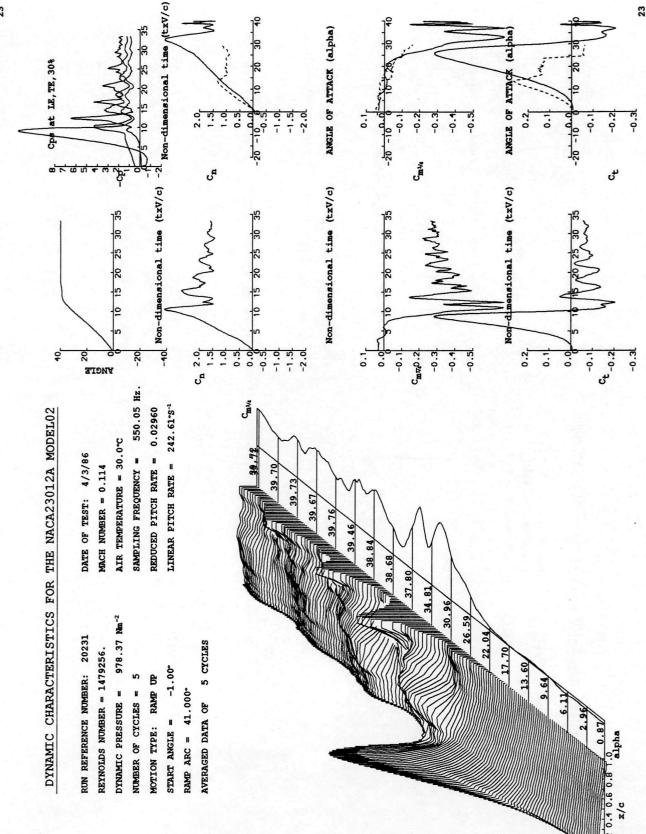
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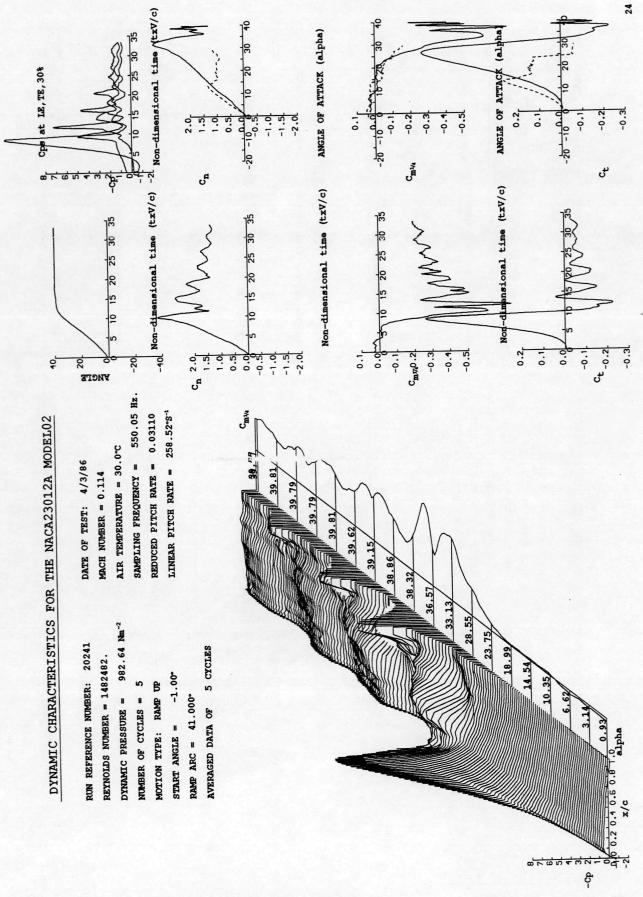


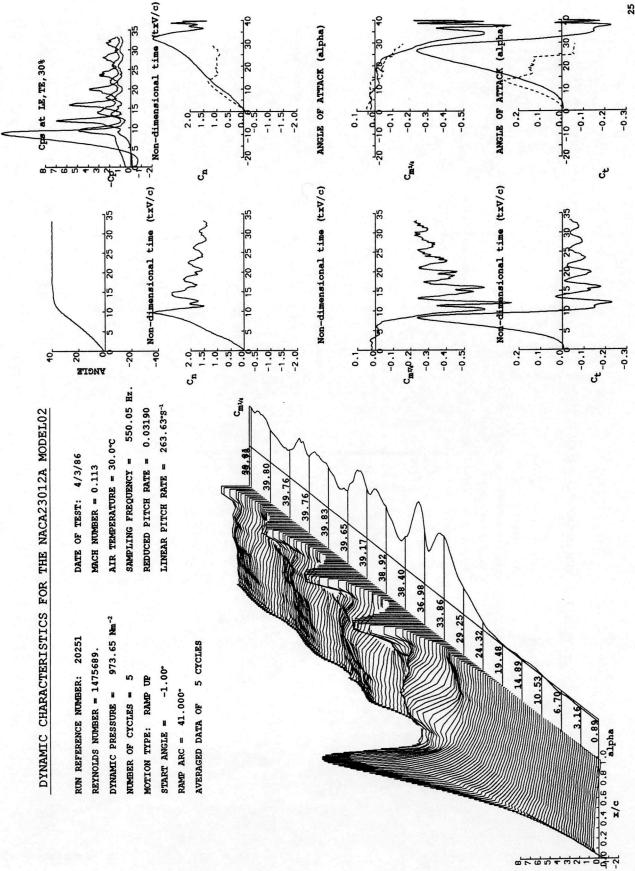


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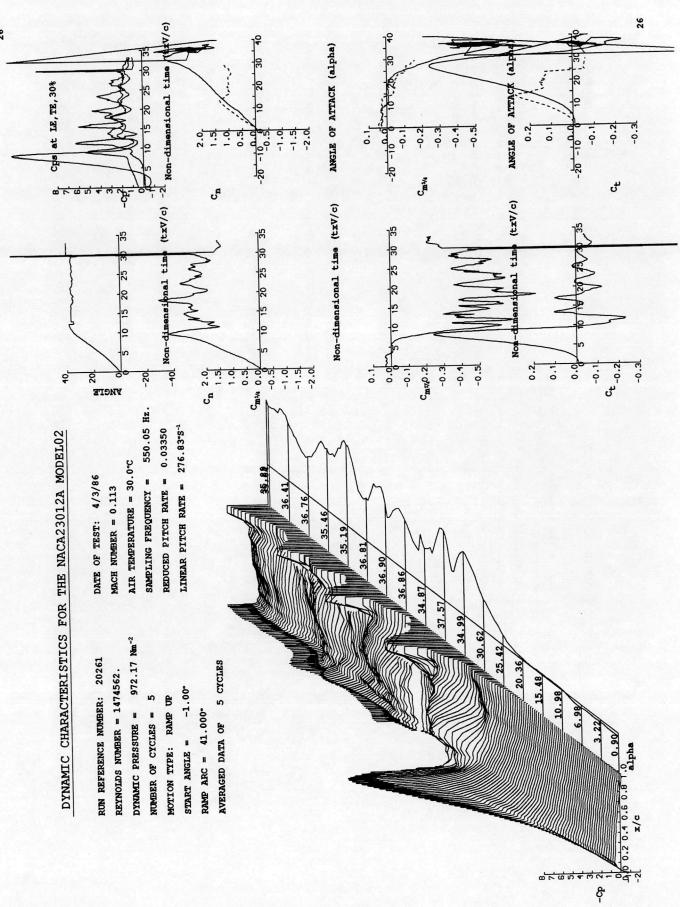
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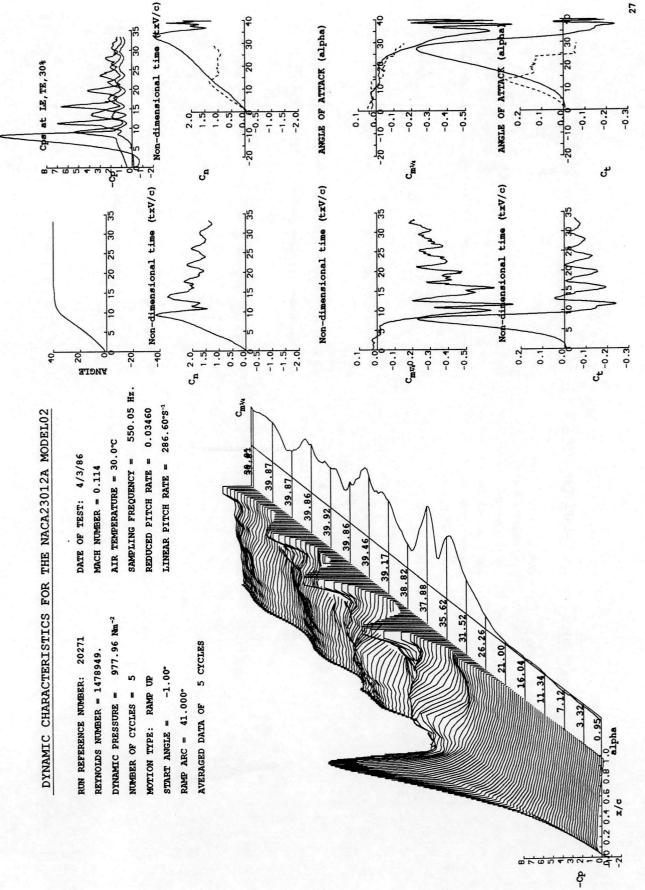


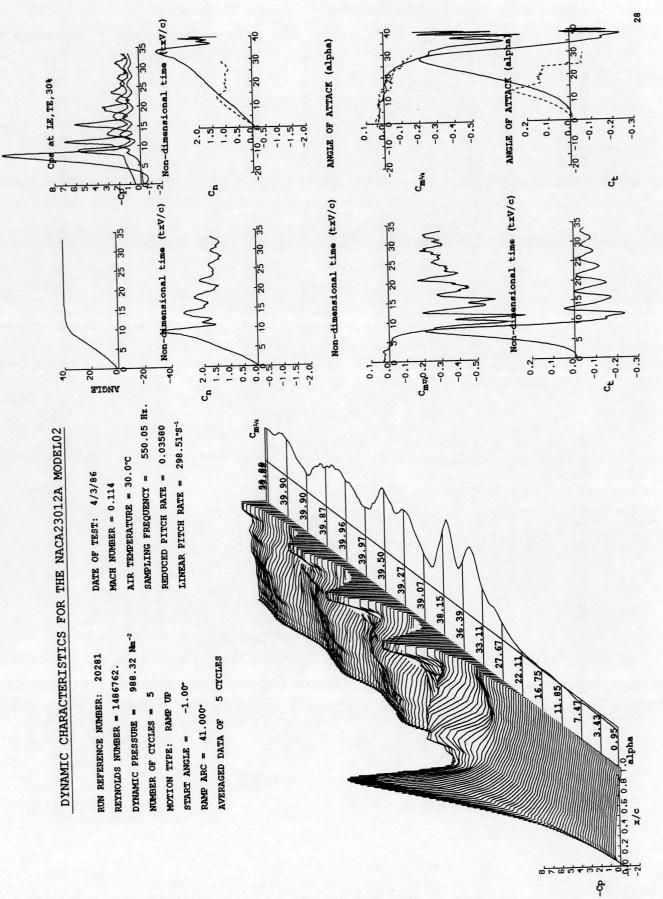


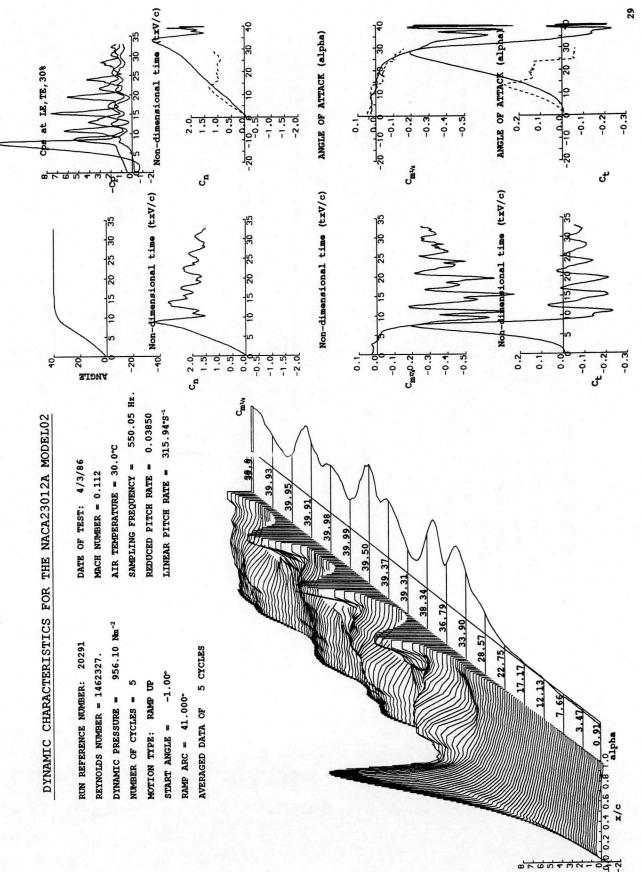
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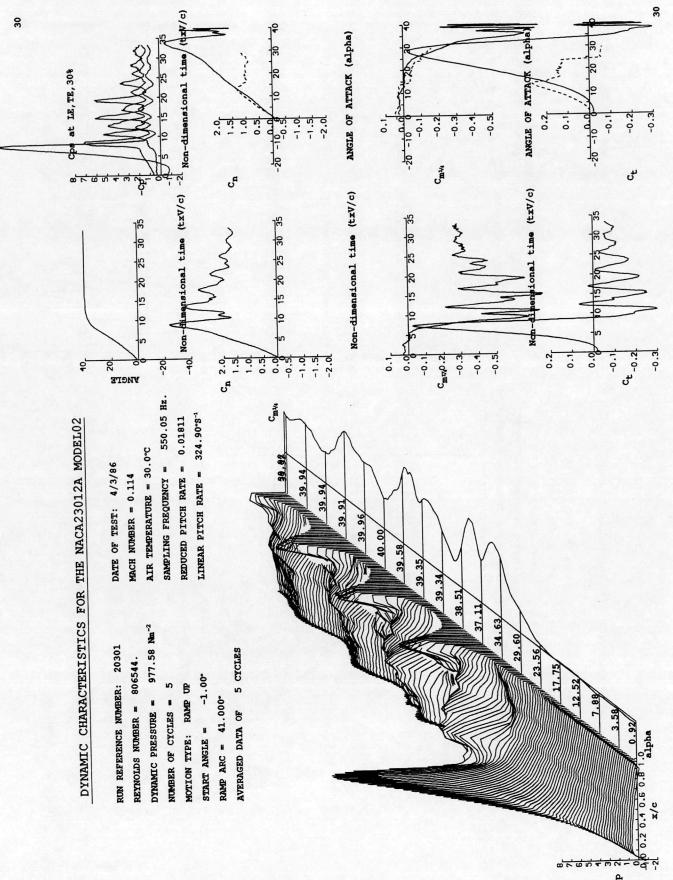




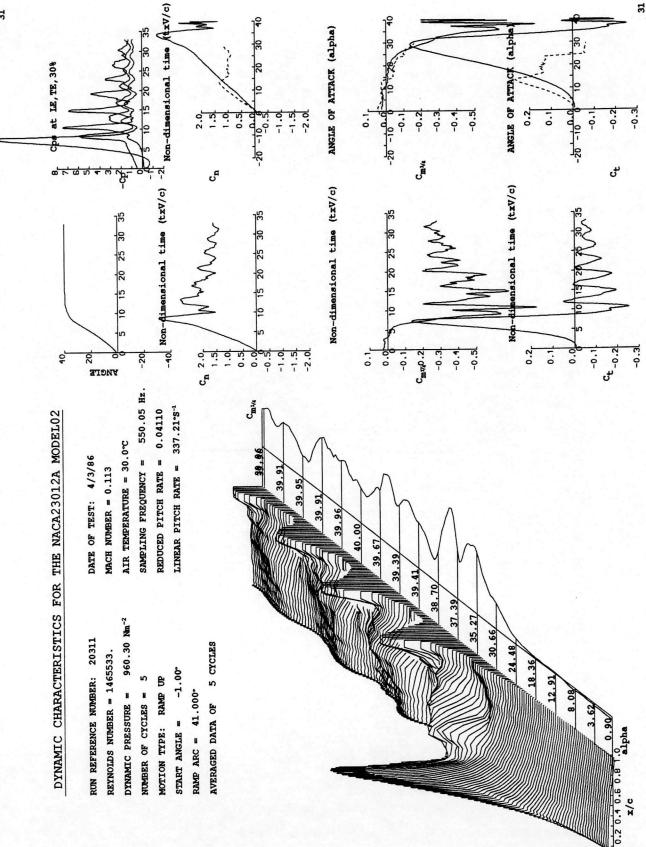




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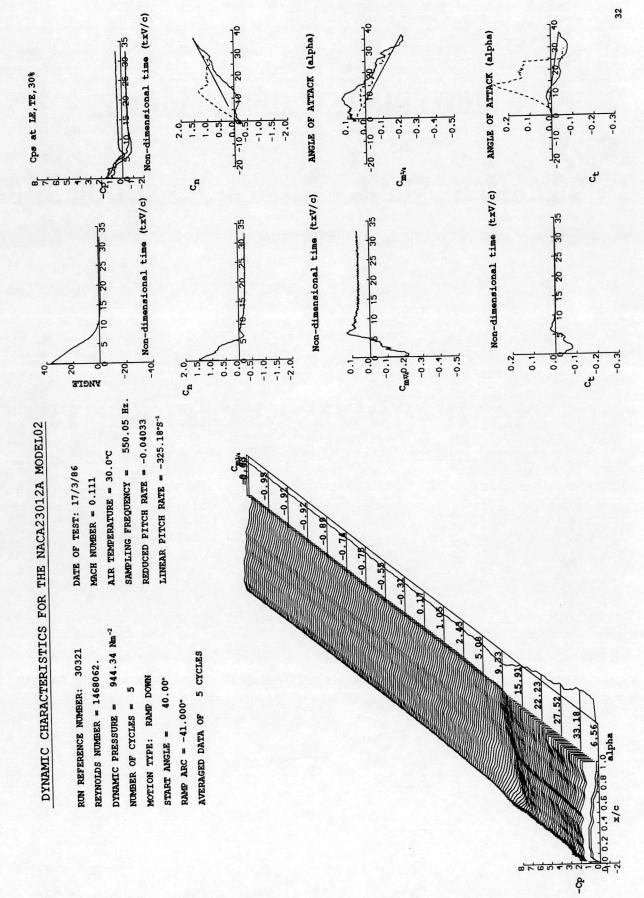
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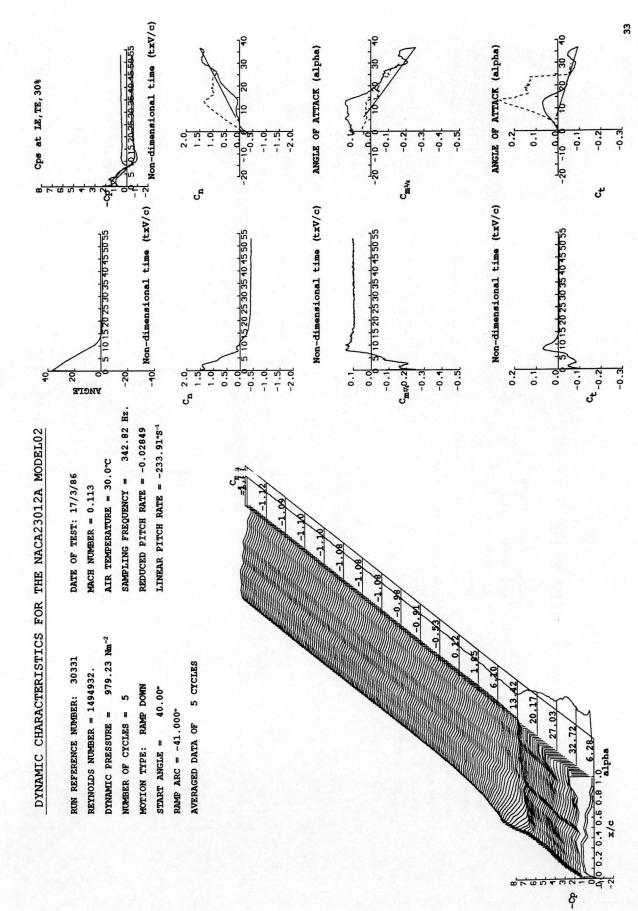
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PRESSURE DATA FROM

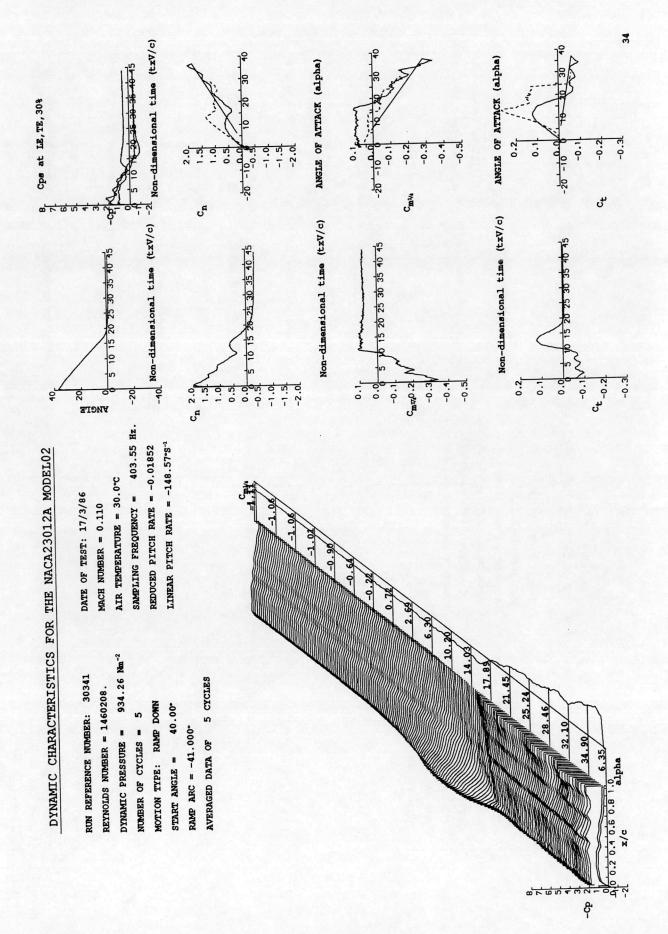
RAMP DOWN EXPERIMENTS



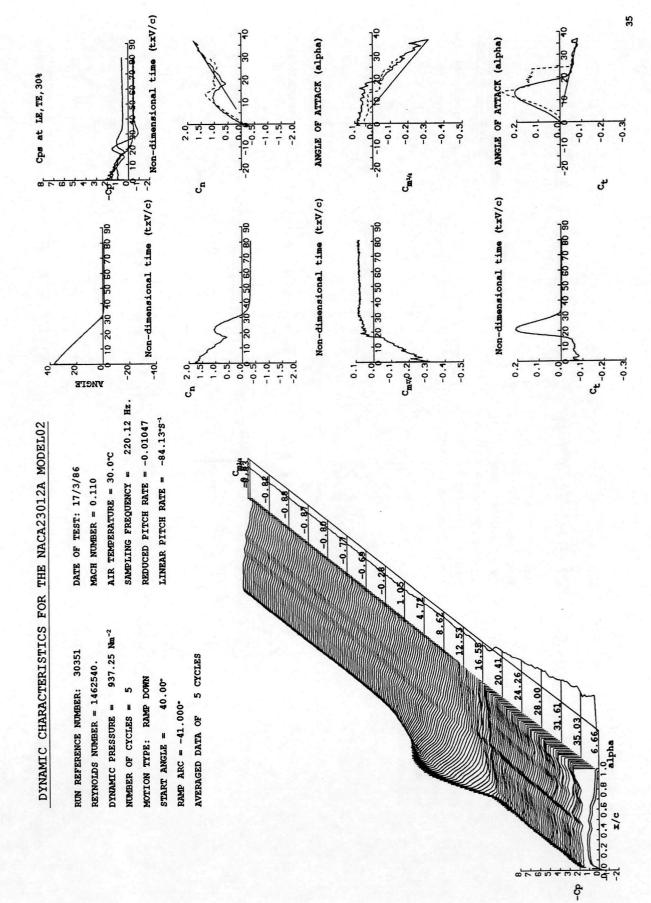


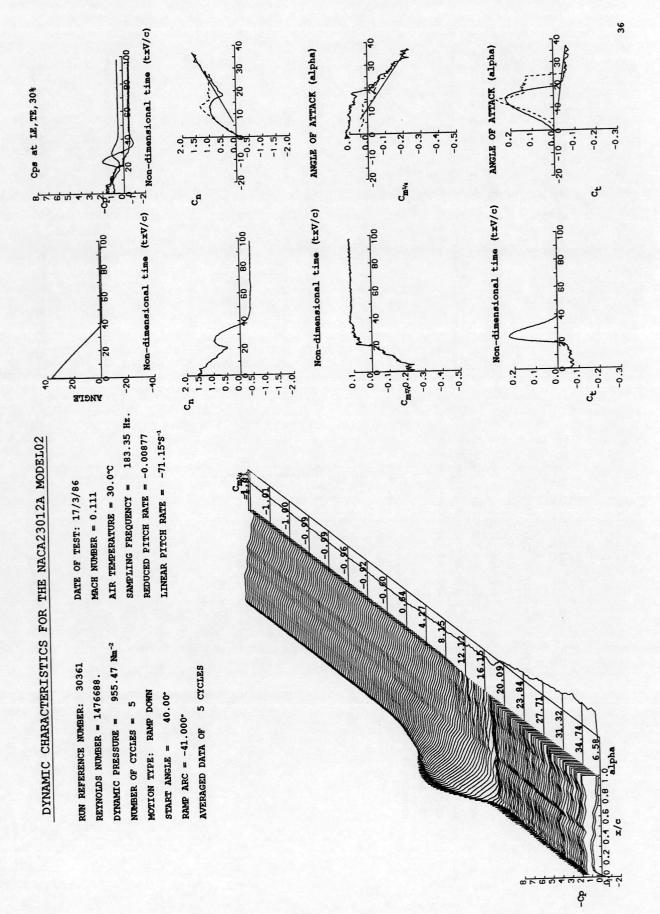
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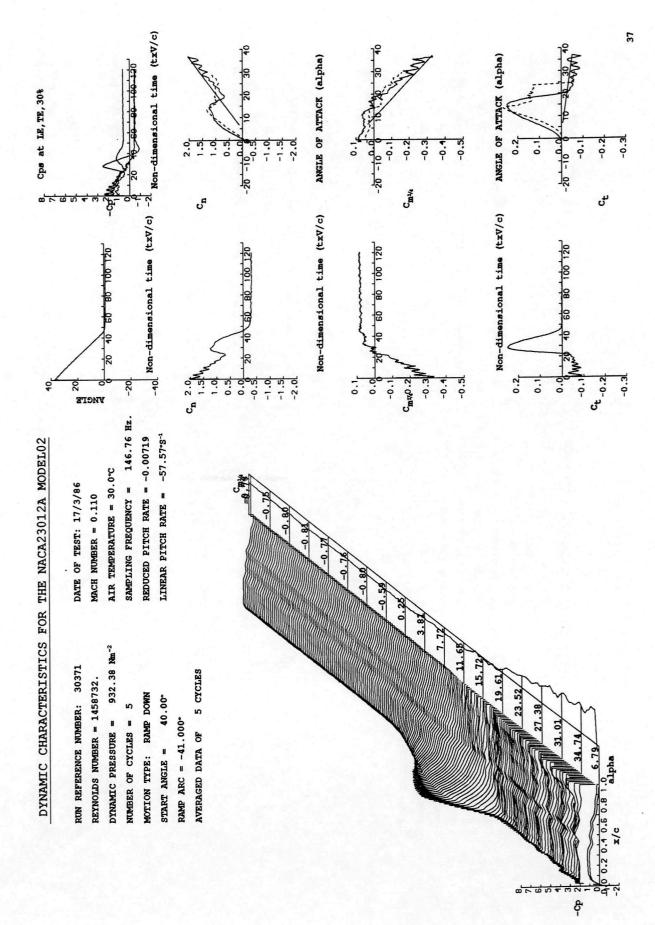
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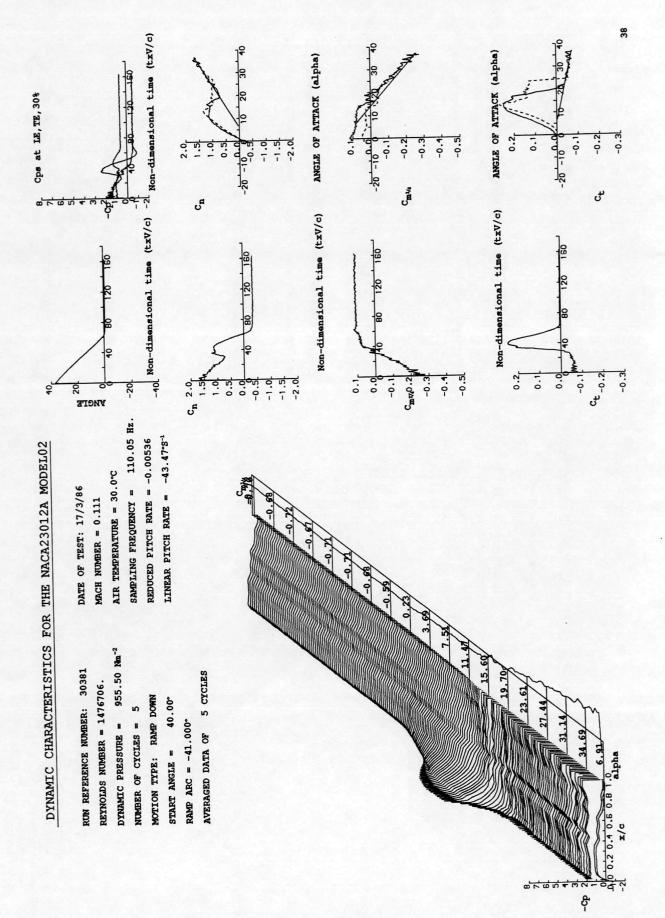
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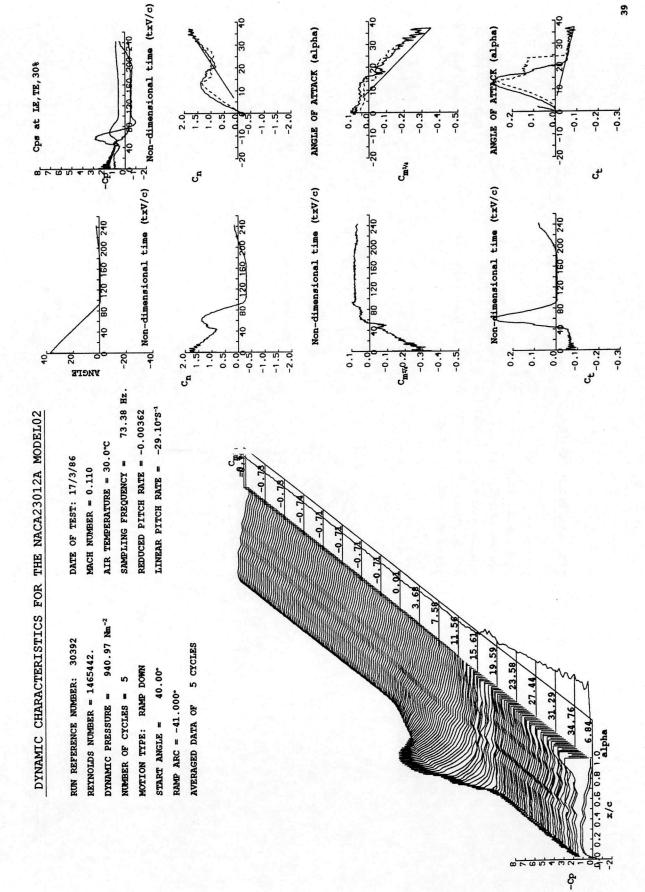


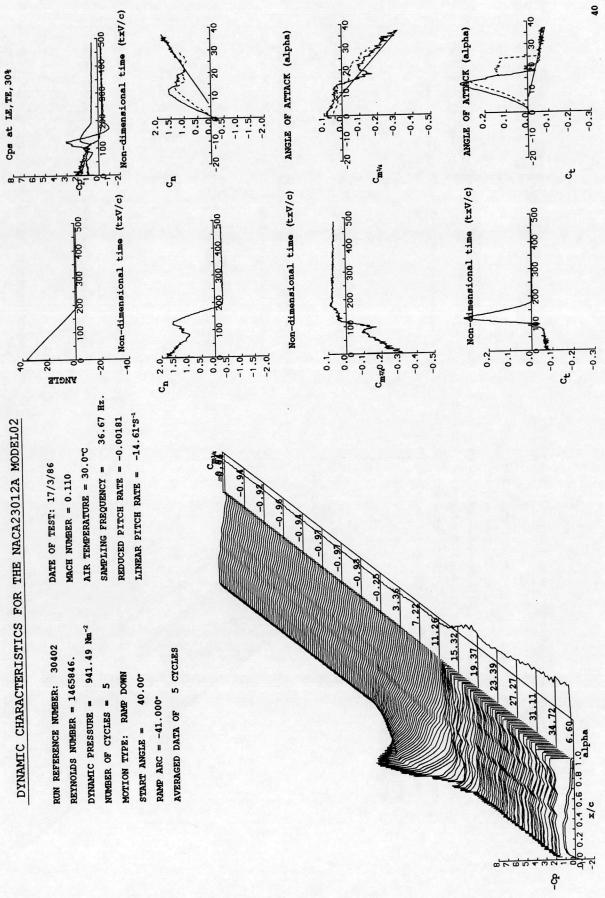


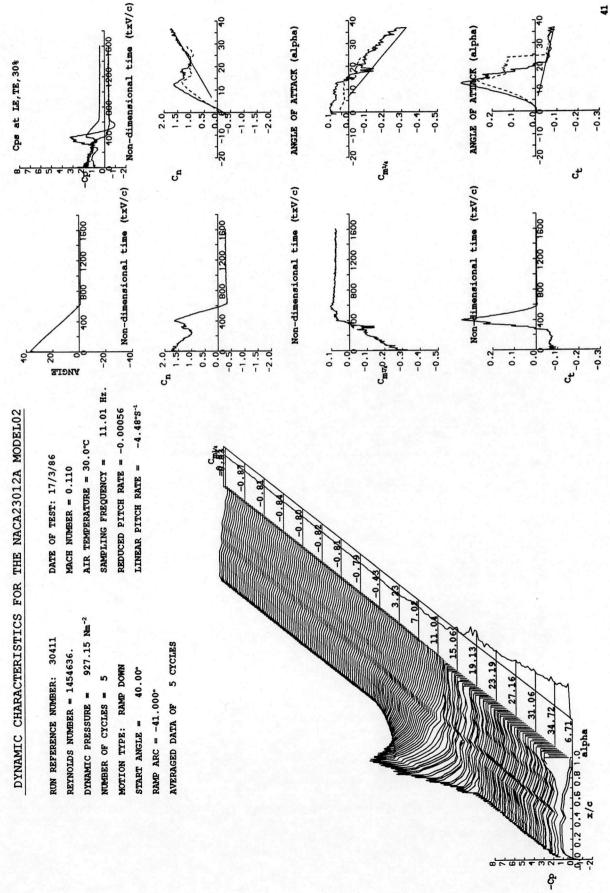


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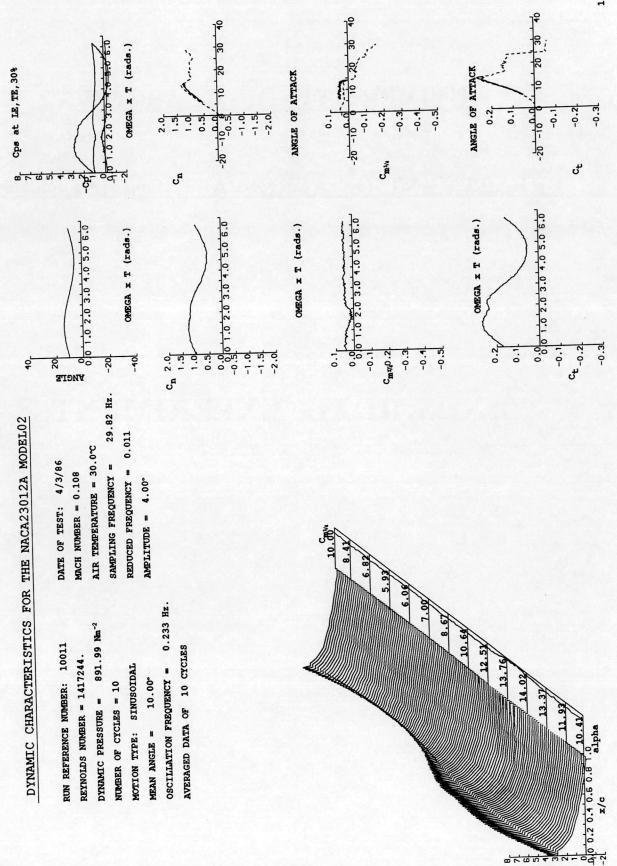
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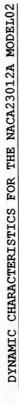
PRESSURE DATA FROM

SINUSOIDAL EXPERIMENTS

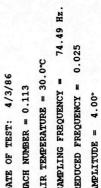


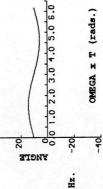
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RUN REFERENCE NUMBER: 10021	DATE
REYNOLDS NUMBER = 1483306.	MACH
DYNAMIC PRESSURE = 977.08 Nm ⁻²	AIR
NUMBER OF CYCLES = 10	SAMP
MOTION TYPE: SINUSOIDAL	REDU
MEAN ANGLE = 10.00°	AMPL
OSCILLATION FREQUENCY = 0.582 Hz.	
AVERAGED DATA OF 10 CYCLES	





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Cps at LE, TE, 30%

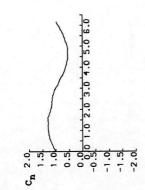
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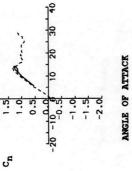
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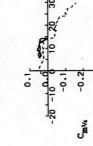
OMEGA x T (rads.)

2.0

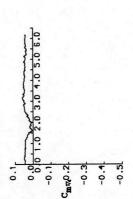
1.5







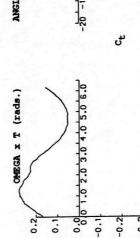
OMEGA x T (rads.)

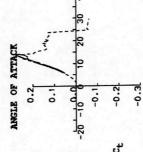


-0.5L

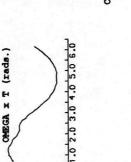
E.0-

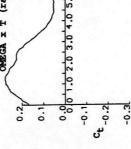
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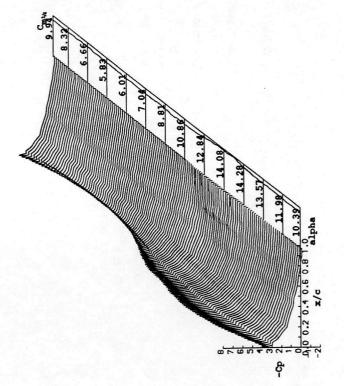


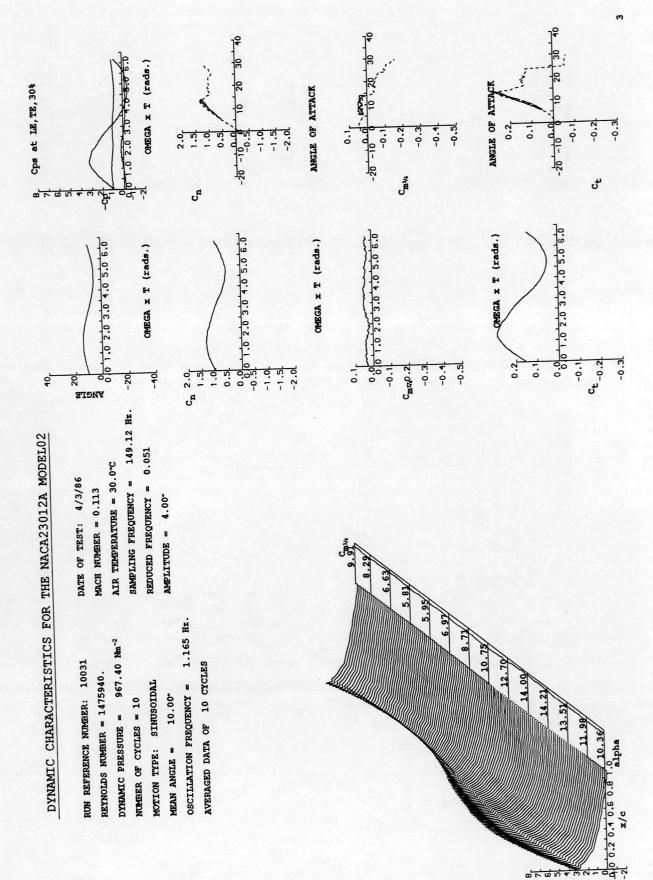


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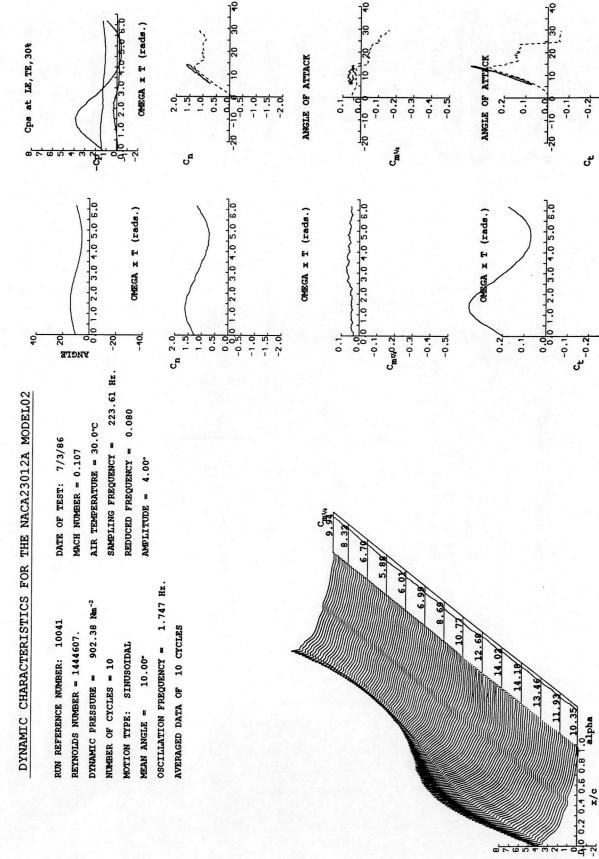


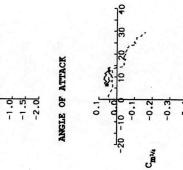


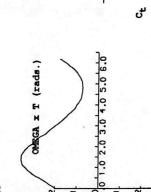


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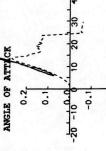
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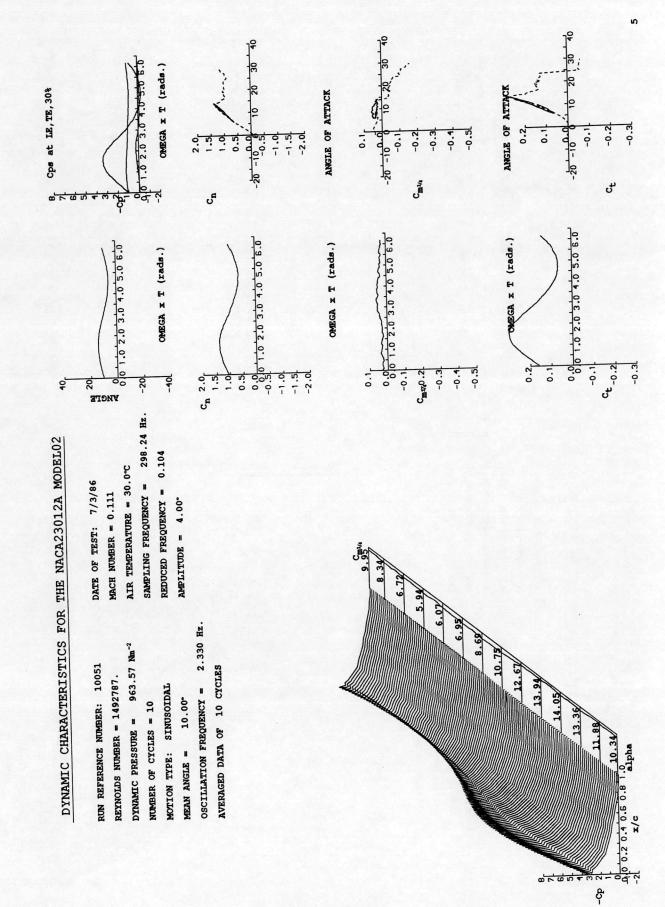


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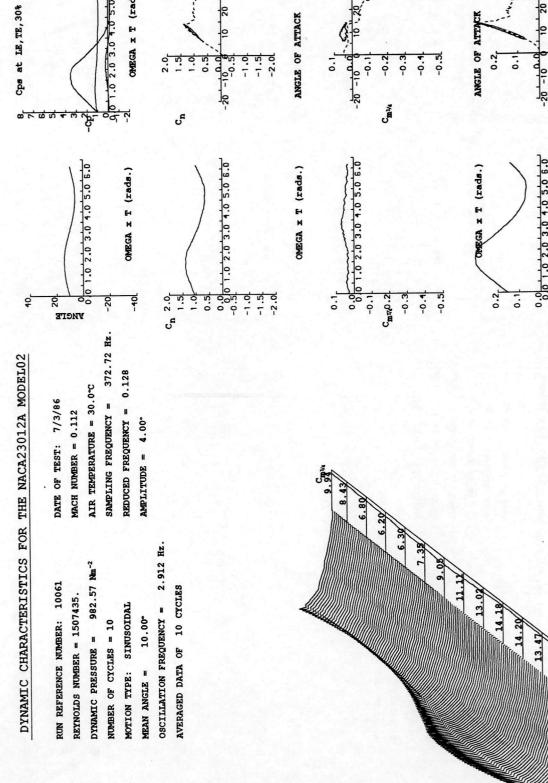


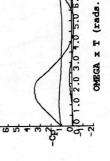
-0.3

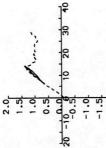
16.0-

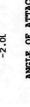


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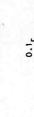


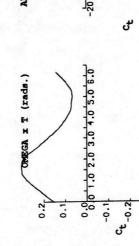


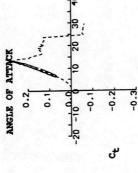


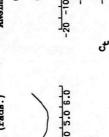








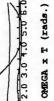














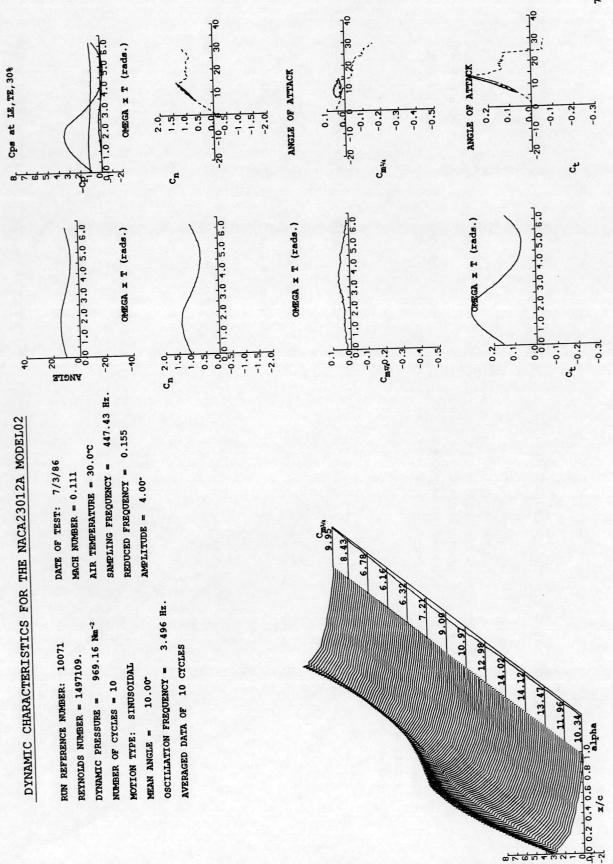
30 40

-0.3

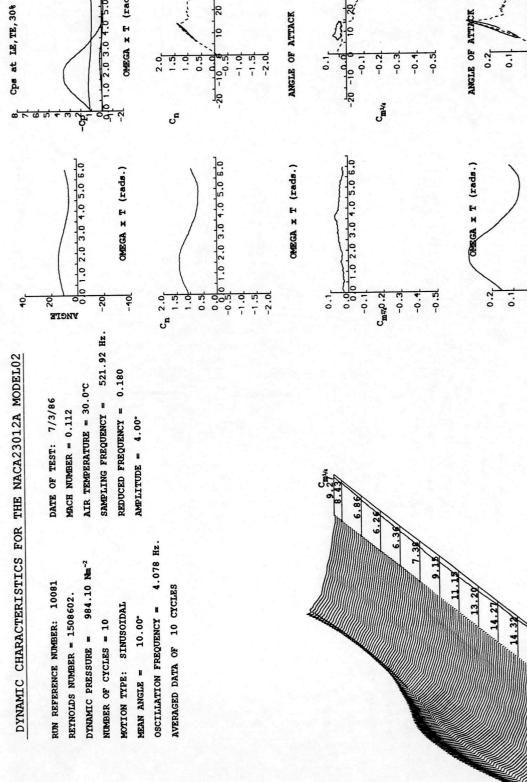
10.38/ alpha

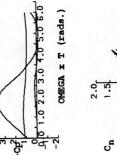
> 0 0.2 0.4 0.6 0.8 x/c

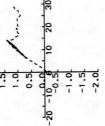
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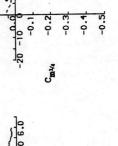


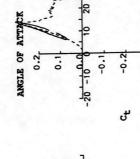






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16.0-

ct -0.2 -0.3

-0.1

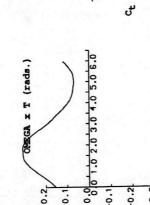
13.6

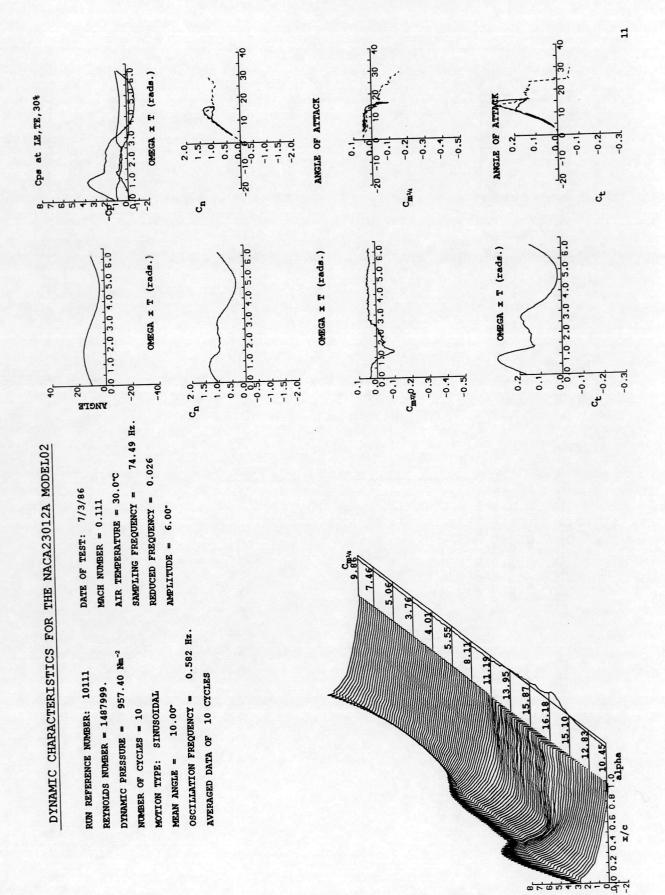
30 65 10.42/ alpha

> 0.2 0.4 0.6 0.8 X/C

0.

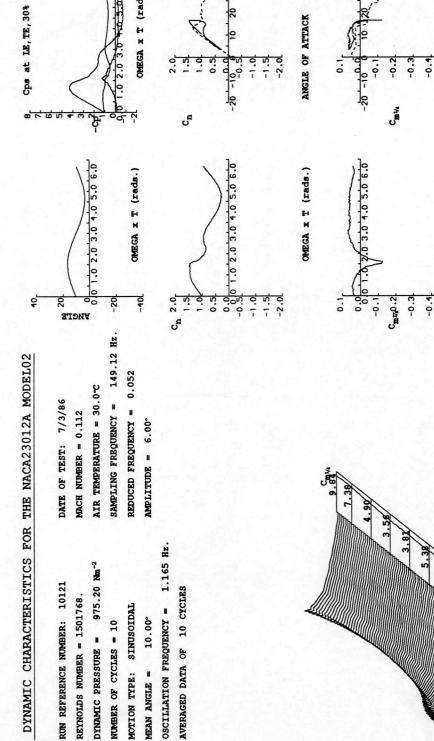
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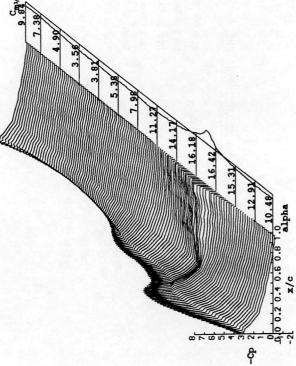


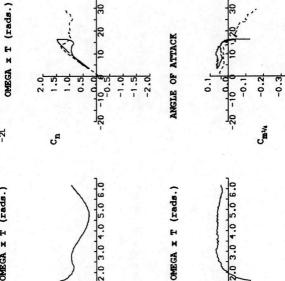


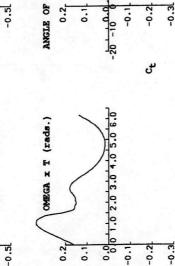
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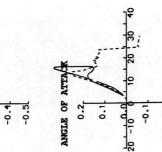




0.2

0.1

-0.5



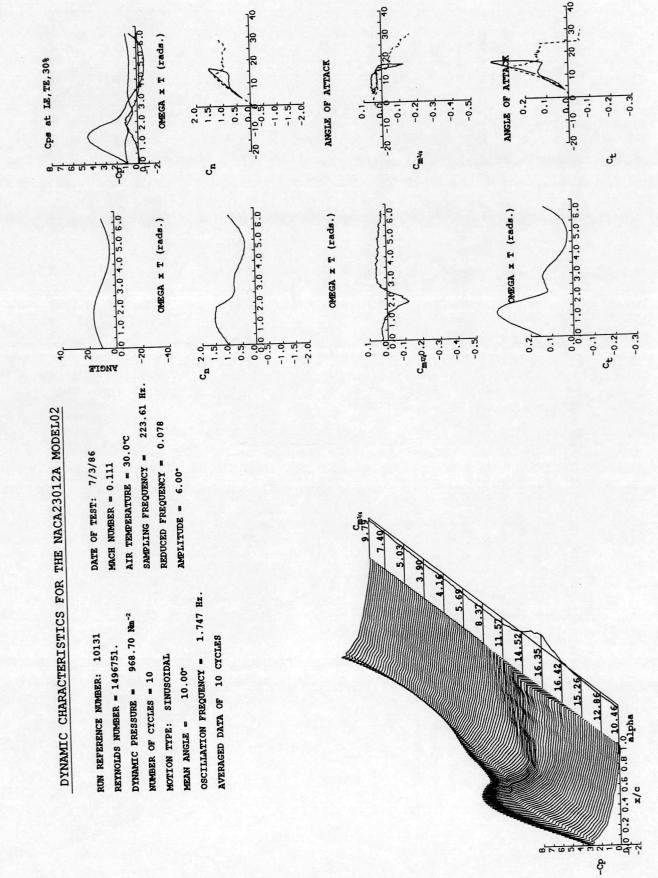
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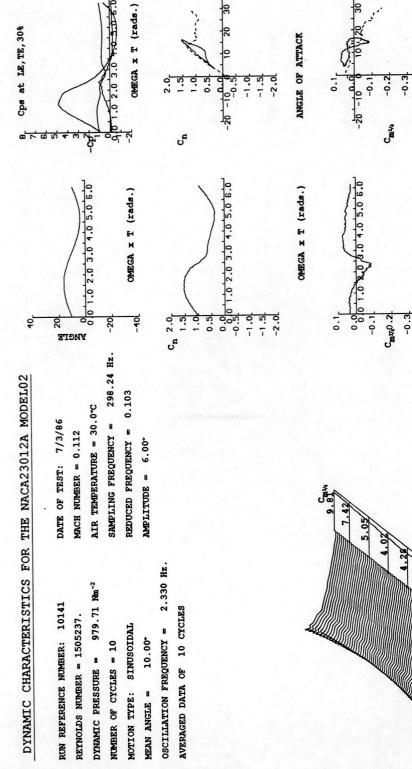
12

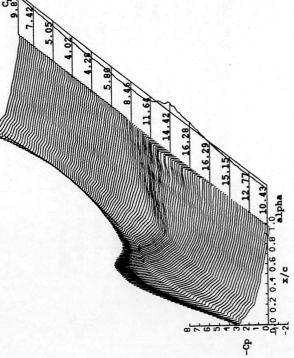
ct -0.2

-0.1

-0.3







ANGLE OF ATT

EGA x T (rads.)

0.2

0.1

-0.5L

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-0.2 E.0-

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ct _0.2

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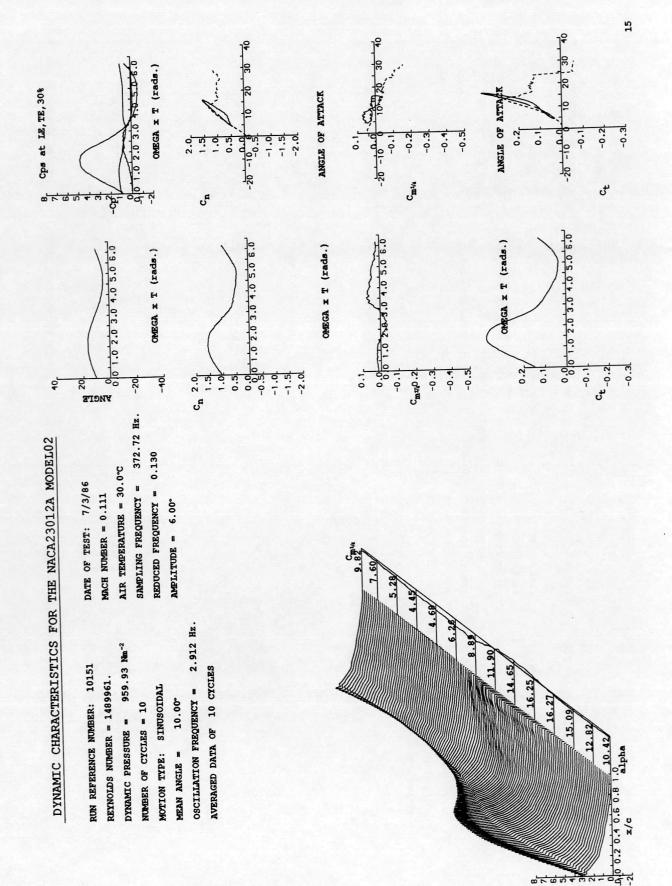
E.0-

10

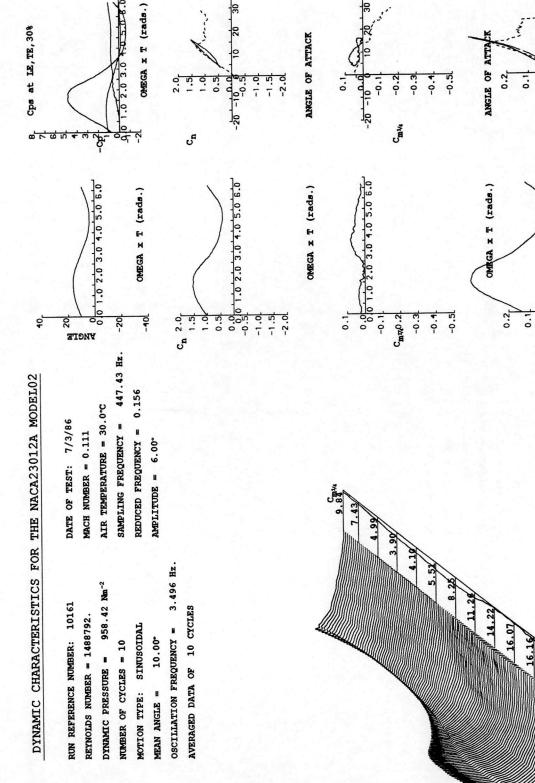
-0-

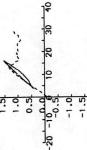
-20 -10

0.001.01.01.2.013.014.015.016.0

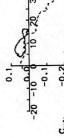


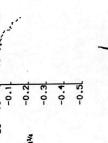
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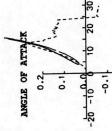


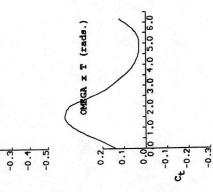












15.1 12.7 10.43 alpha

0000

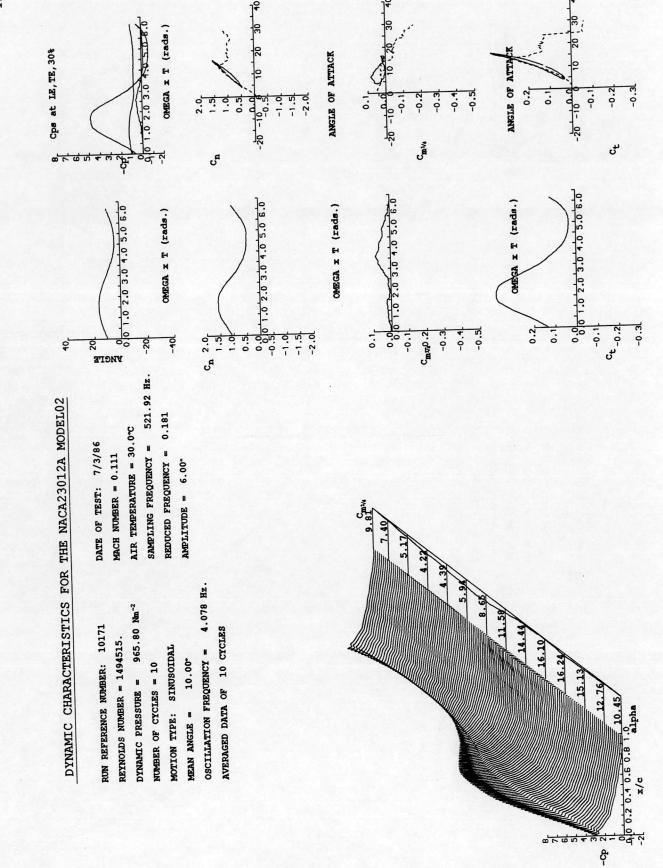
0.2 0.4 0.6 0.8 x/c

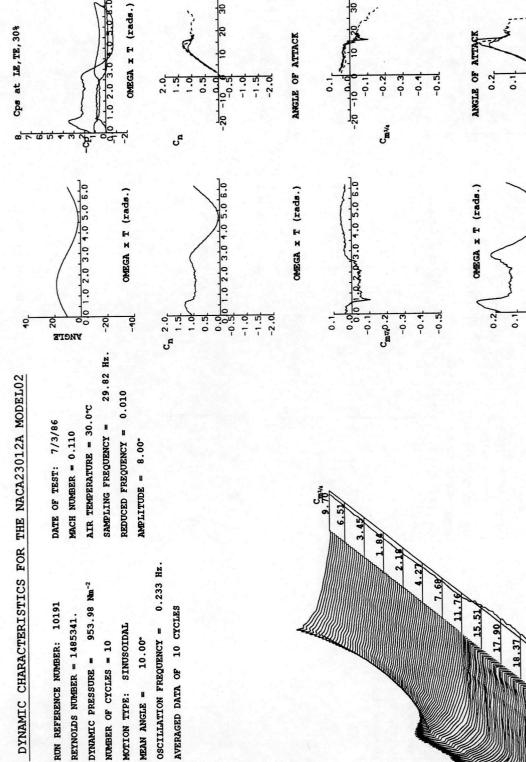
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-0.3

-0.2

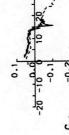
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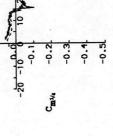


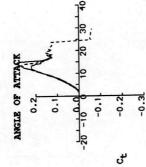


30 40 0.1-

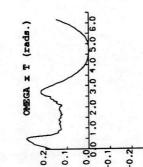
ANGLE OF ATTACK

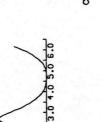




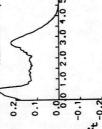


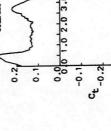
19





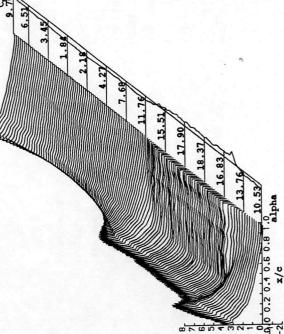


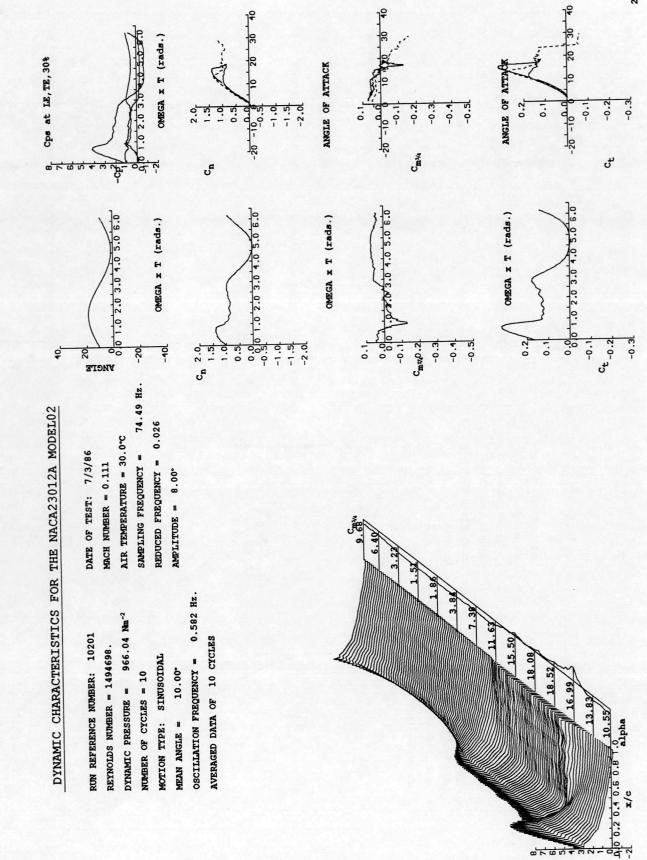




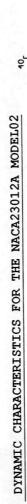
ę

-0.3





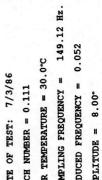
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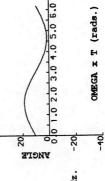


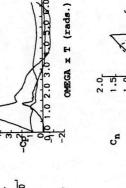
Cps at LE, TE, 30%

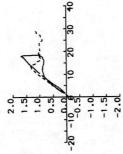
8 5

RUN REFERENCE NUMBER: 10211	DATE
REYNOLDS NUMBER = 1489783.	MACH 1
DYNAMIC PRESSURE = 959.70 Mm^{-2}	AIR T
NUMBER OF CYCLES = 10	SAMPL
MOTION TYPE: SINUSOIDAL	REDUC
MEAN ANGLE = 10.00°	AMPLIT
OSCILLATION FREQUENCY = 1.165 Hz	Нz.
AVERAGED DATA OF 10 CYCLES	









1.0 2.0 3.0 4.0 5.0 6.0

0.00

cn 2.0

1.01

0.5



OMEGA x T (rads.)

m M

-1.5

-1.0

0.1

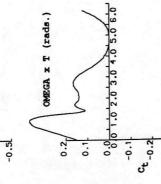


-0.2

Cm44

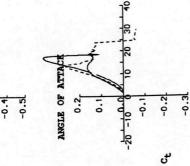
9

10



18. 91 18. 91 13. 76 13. 10 13. 10 13. 10 13. 10 13. 10 13. 10 13. 10 13. 10 13. 10 13. 10 13. 10 13. 10 14. 10 15

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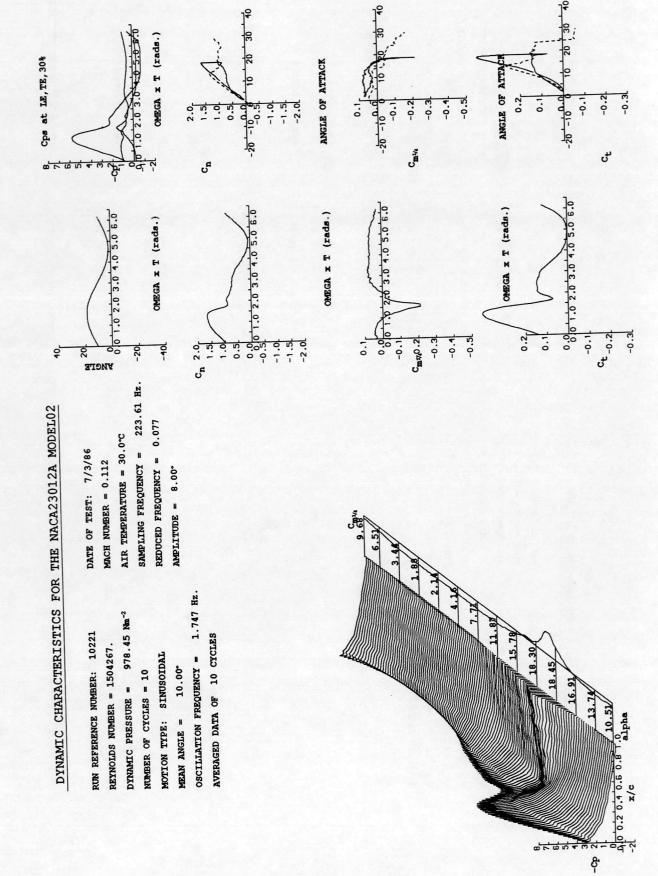


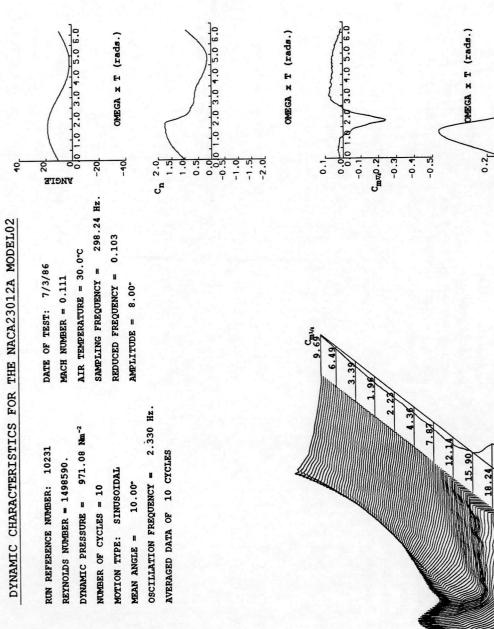
21

-0.3

0,0.2 0.4 0.6 0.8 -2[x/c

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Cps at LE, TE, 30%

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10

-10-51

-20 -1

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-1.5

OMEGA x T (rads.)

2.0

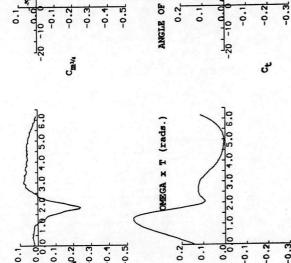
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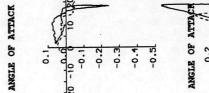
1.0 2.0 3.0

P.

-2

ANGLE OF ATTR -0.5 0.2 -0.2 -0.2 0-0 -0.4 0 -20 -10 ė -20 -10 CIII'





10

ct -0.2 JE.0-

-0.1

0.1

18.40 16.8

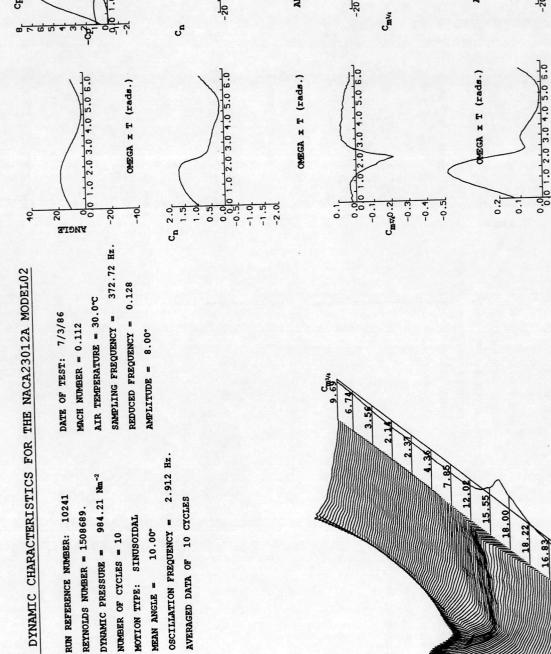
0000

10.51 alpha

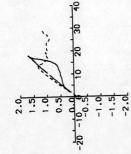
> 0 0.2 0.4 0.6 0.8 x/c

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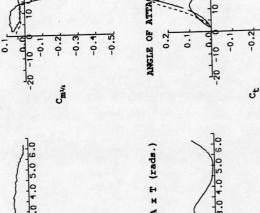
2-2



0.2.0.2.0 OMEGA x T (rads.) Cps at LE, TE, 30% 1.0 2.0 3.



ANGLE OF ATTACK



30 40

24

-0.3

ct -0.2 -0.3

-0.1

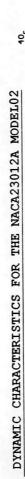
13.6 10.51

ę

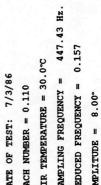
0 N 0 0 4

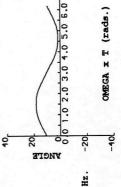
alpha

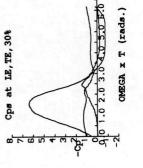
0,0.2 0.4 0.5 -2[x/c

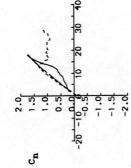


RUN REFERENCE NUMBER: 10251	DAT
REYNOLDS NUMBER = 1482170.	MAG
DYNAMIC PRESSURE = 949.91 Nm ⁻²	AII
NUMBER OF CYCLES = 10	SA
MOTION TYPE: SINUSOIDAL	REI
MEAN ANGLE = 10.00°	AM
OSCILLATION FREQUENCY = 3.496 Hz.	
AVERAGED DATA OF 10 CYCLES	









0.00 -0.5--0.5-

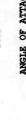
-2.0

-1.5

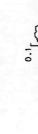
-1.0

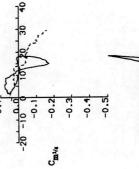
cn 2.0

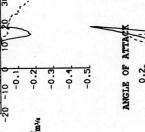
1.0 0.5

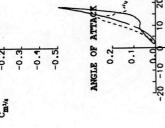


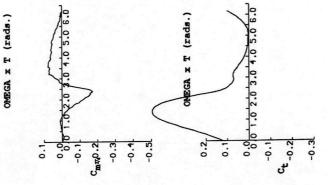


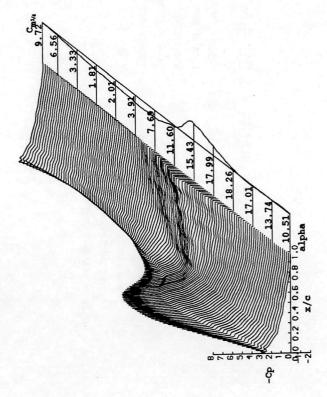












25

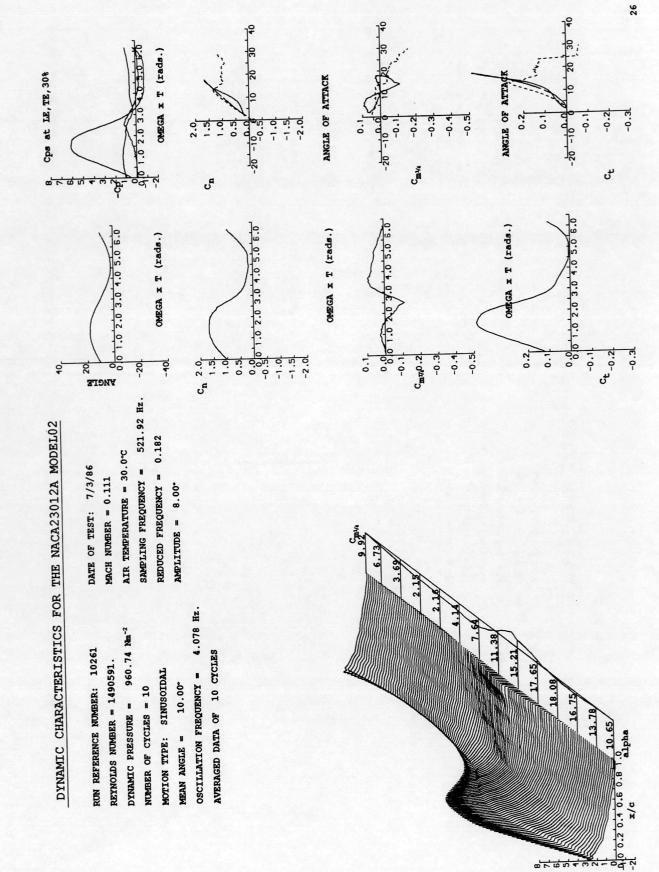
25

-0.2 -0.3

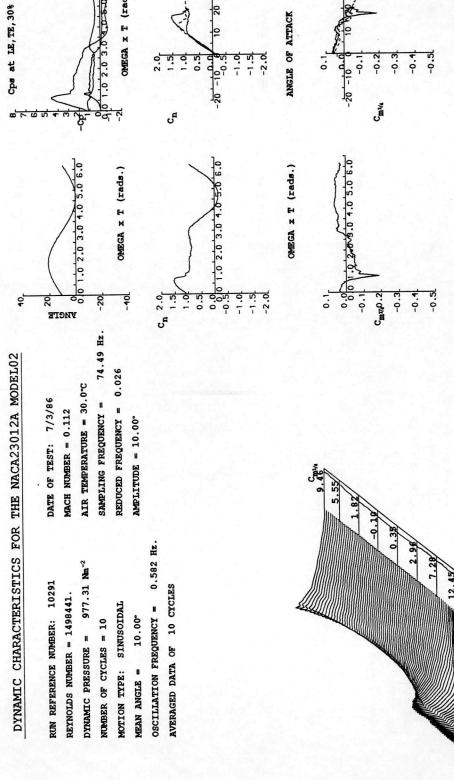
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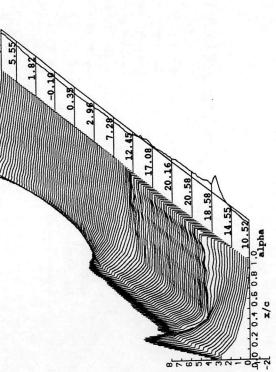
-0.1

40

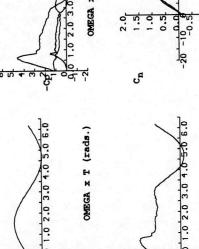


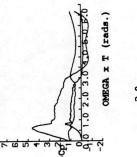
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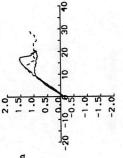




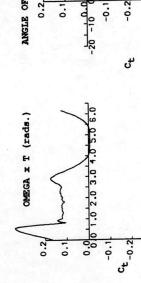
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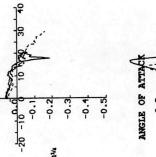


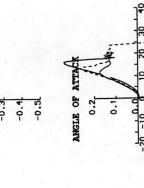


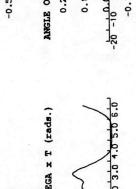










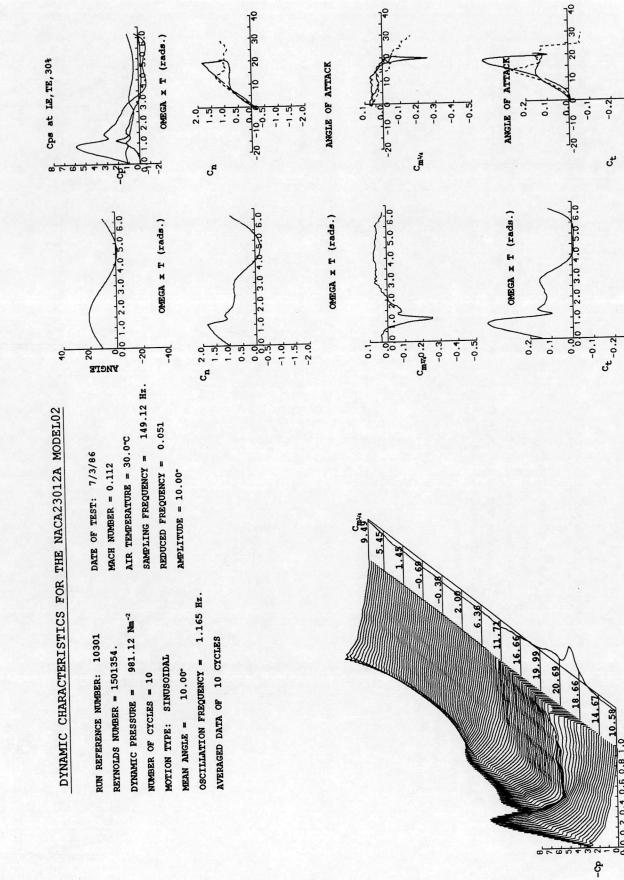




29

-0.3

-0.3



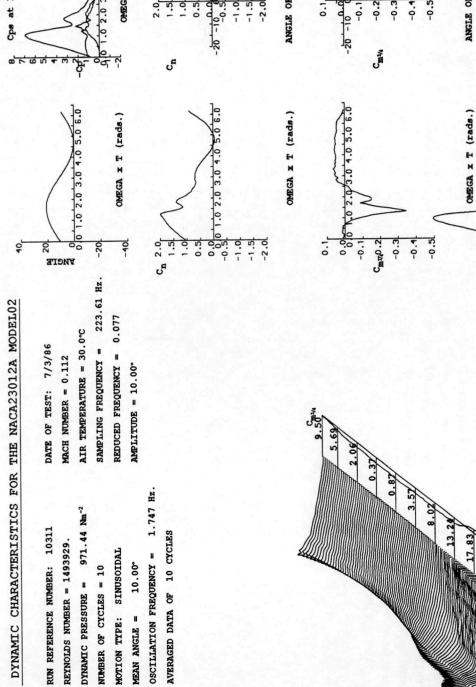
-0.3L

-0.3

alpha

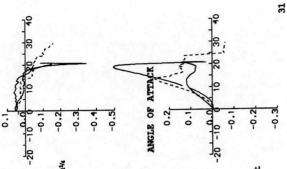
0.4 0.6 0.8 x/c

-21

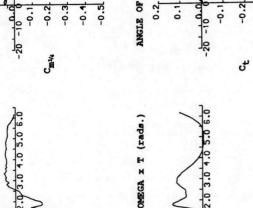


ANGLE OF ATTACK

-1.5



0.1 0.0



0.24

0.1

Cps at LE, TE, 30%

31

OMEGA x T (rads.)

2.0

1.5

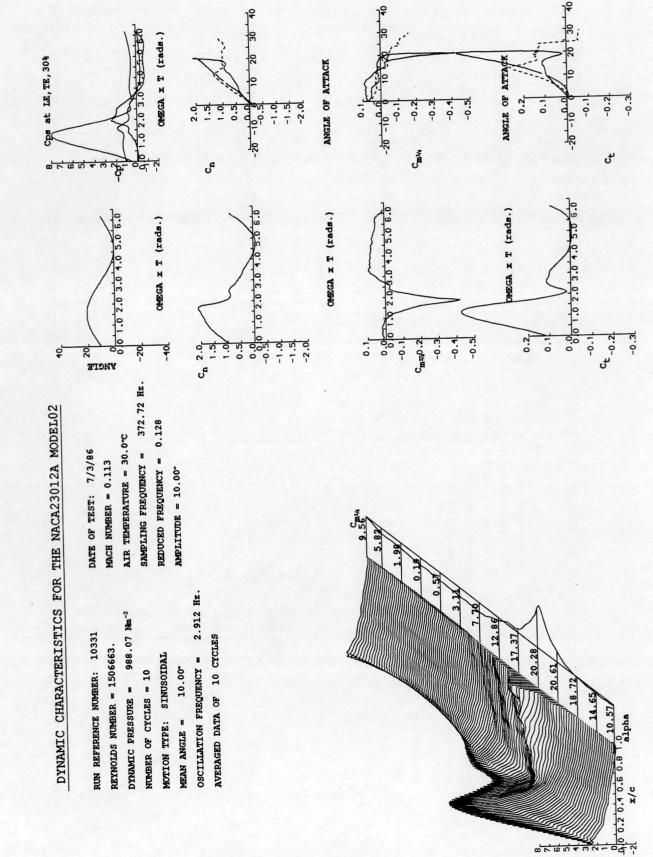
0.5

ct -0.2

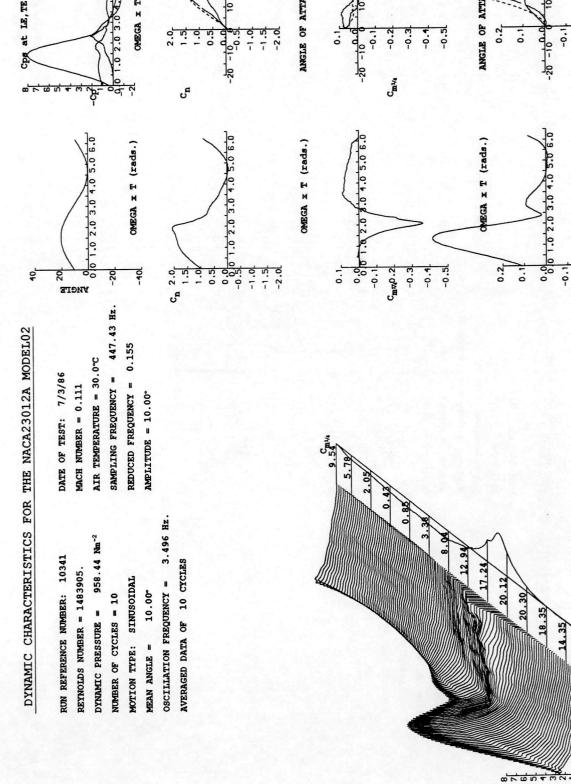
-0.1

16.0-

20.80 20.70 18.64 10.54 alpha 0 0.2 0.4 0.6 0.8 -2 x/c

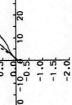


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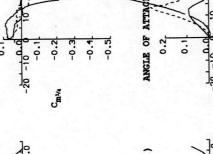
Cpg at LE, TE, 30%

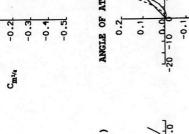


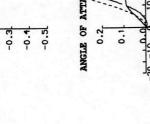


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34

-0.3 -0.2

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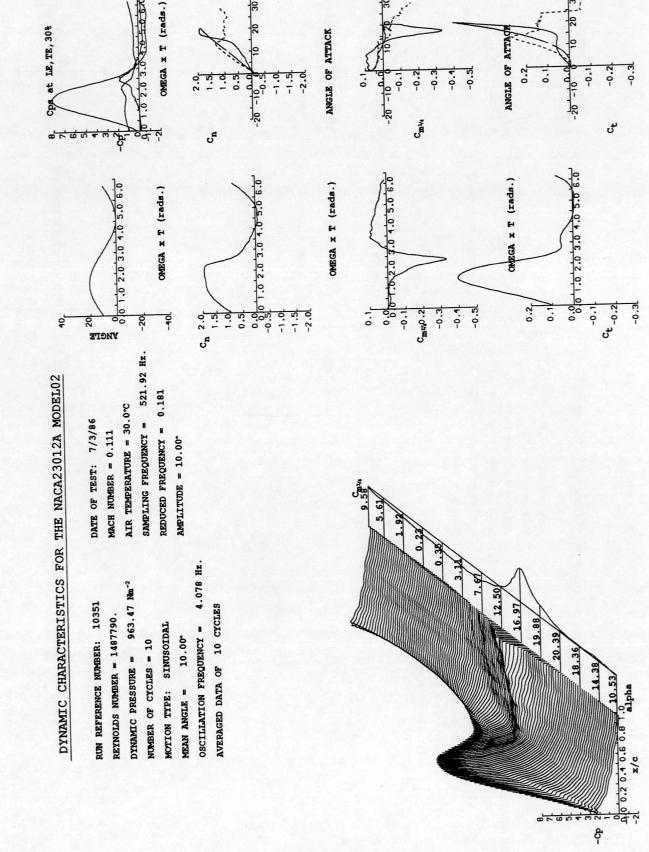
ct -0.2

10.50 alpha

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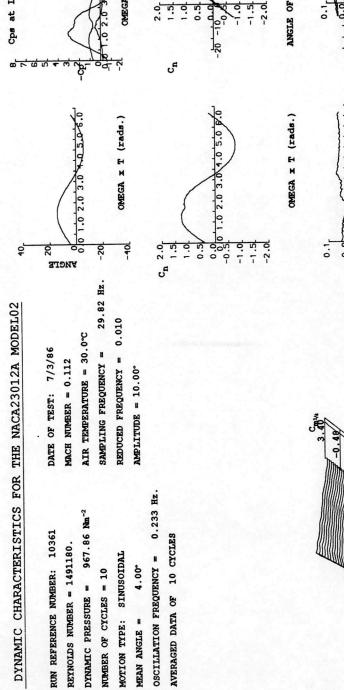
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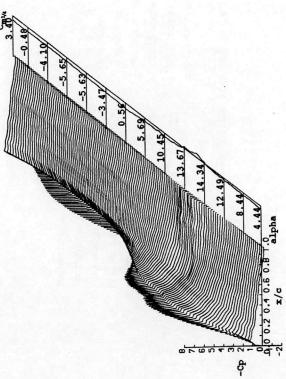


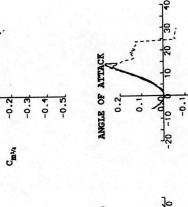
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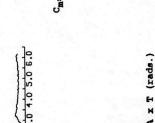
32

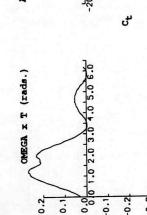
30 40



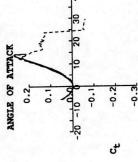


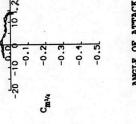


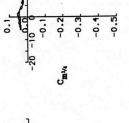


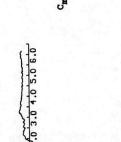


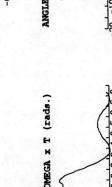
0.1

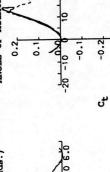


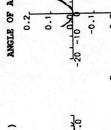












18

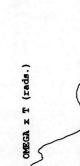
-2.0

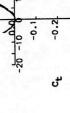




Cm40.2

-0.1

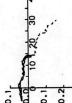


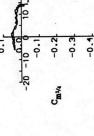


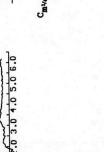
Ct -0.2 -0.3

-0.1

36









36

Cps at LE, TE, 30%

OMEGA x T (rads.)

0.5

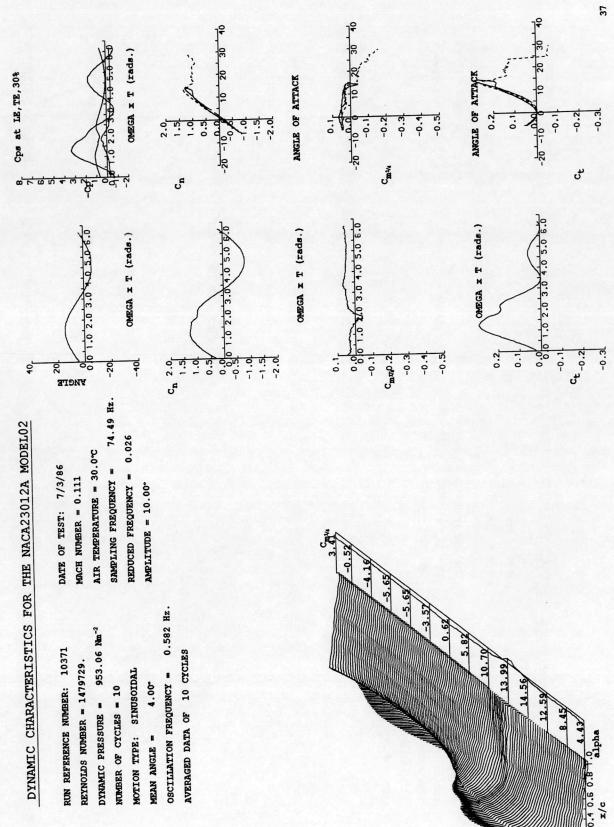
+.0--0.5

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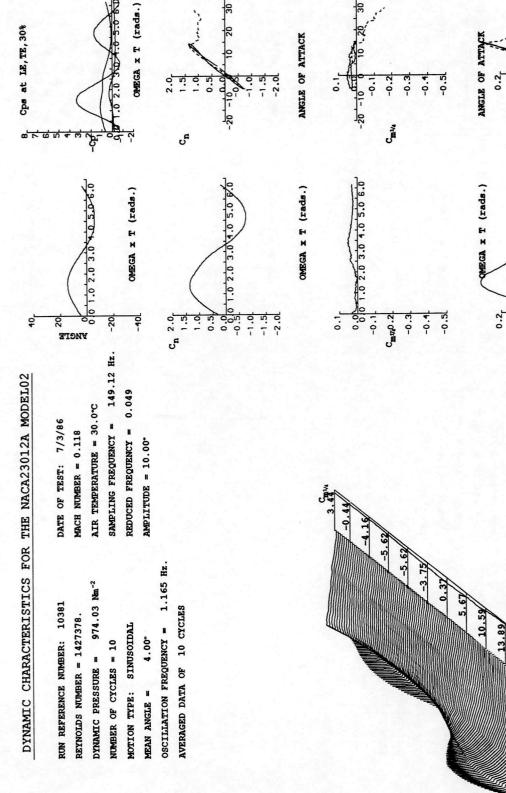
ANGLE OF ATTACK

-1.5



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38 ANGLE OF ATT -0.3L -0.2 0 -20 -10

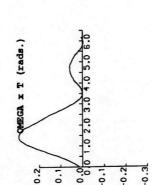
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0.1

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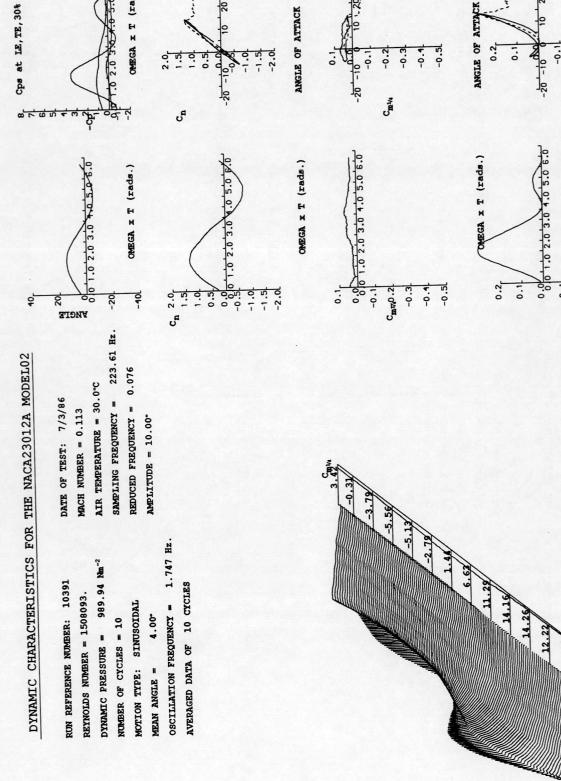
0000

4.47 alpha

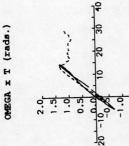
> X/C 0.2 0.4

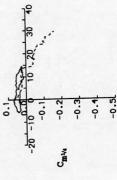
0.0

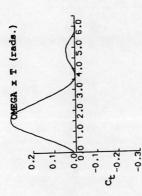
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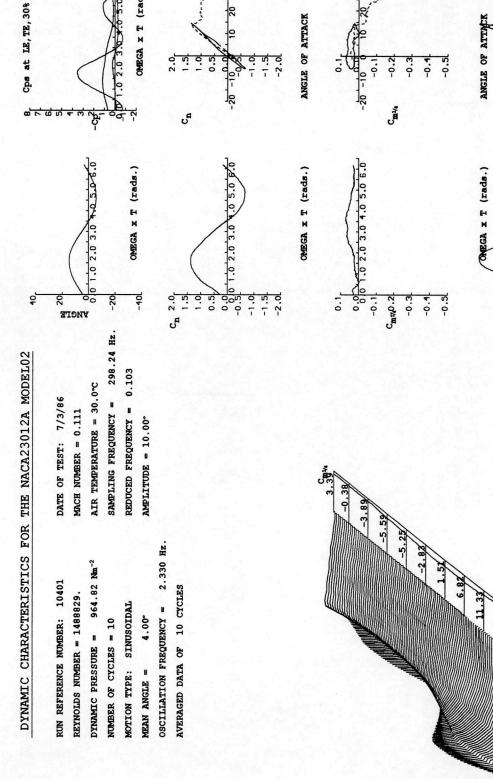
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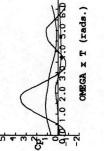
8 60 ė

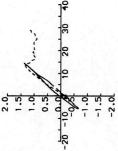
ANGLE OF ATTACK -2.01 - 22



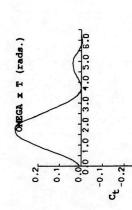


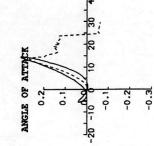






ANGLE OF ATTACK





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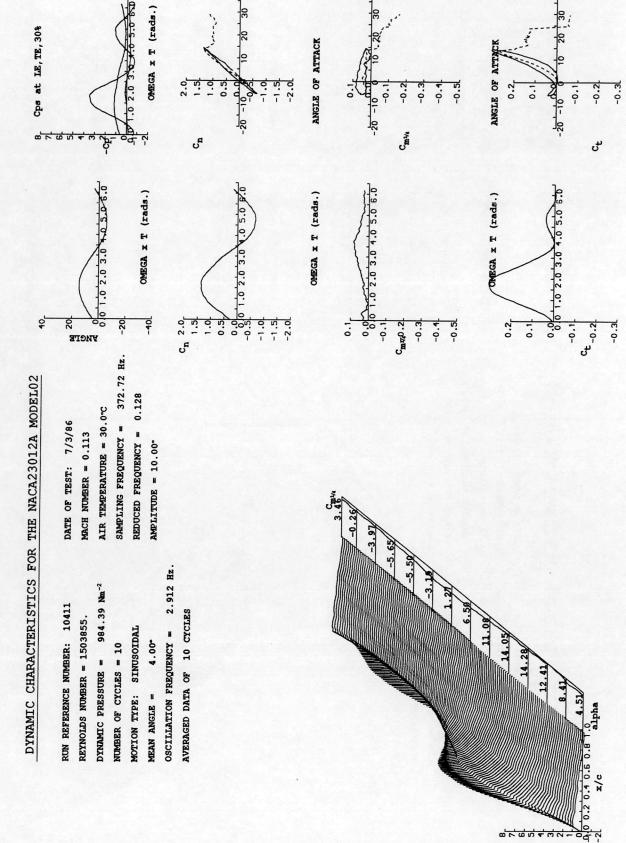
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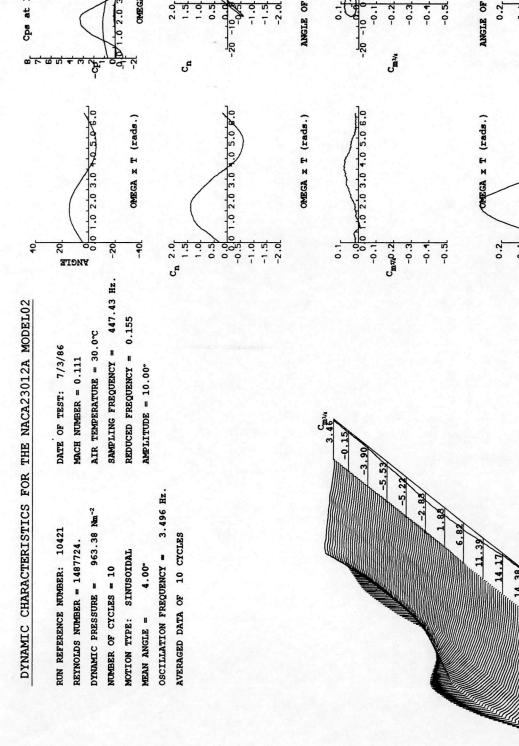
2018

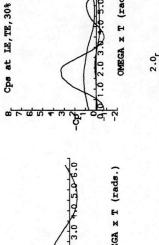


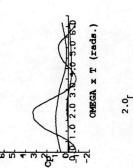
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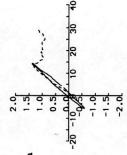
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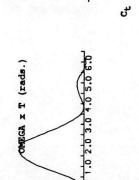


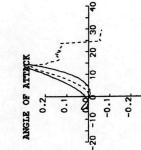


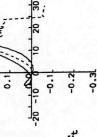




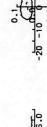


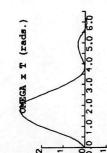






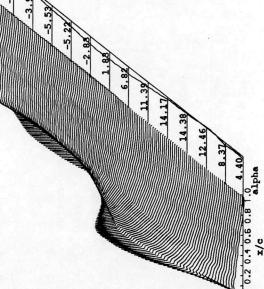
ANGLE OF ATTACK





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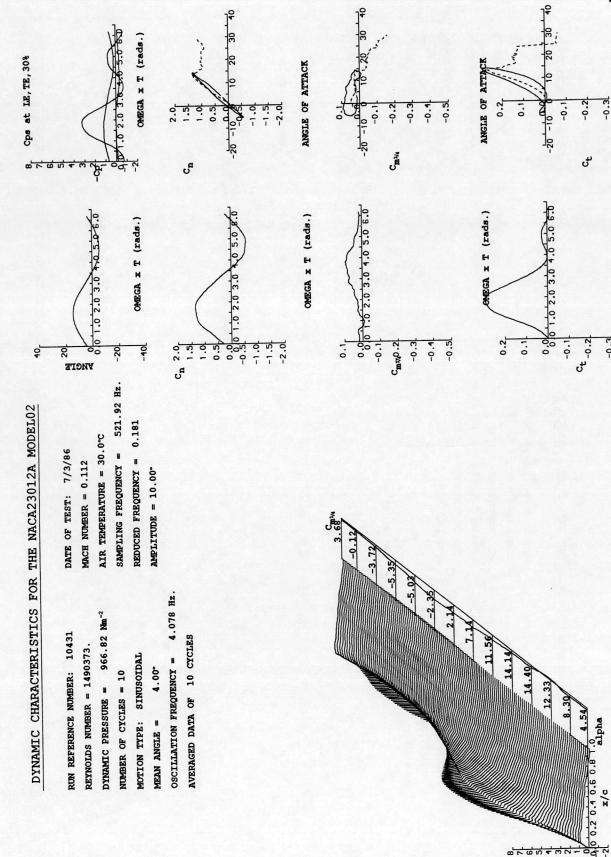
ct -0.2 0.0 JE. 0--0.1



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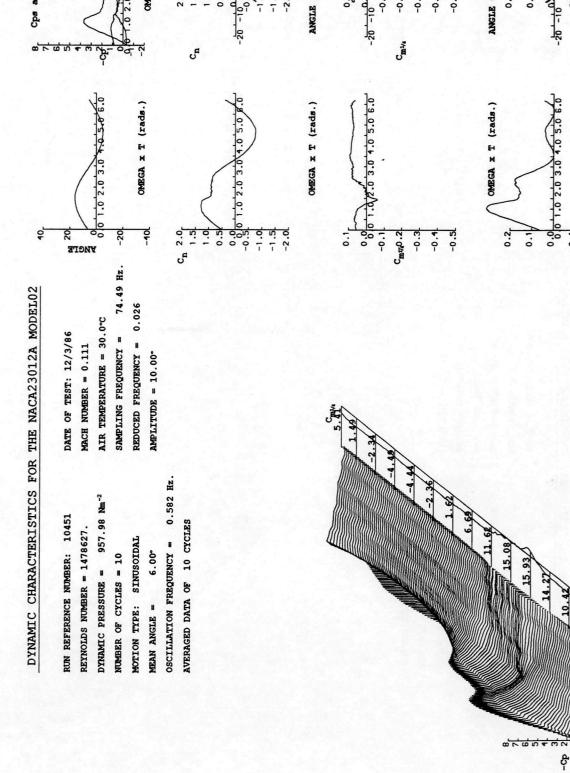
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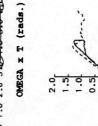
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-0.31



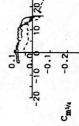
Cps at LE, TE, 30%



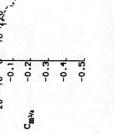


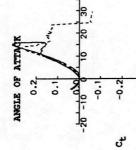


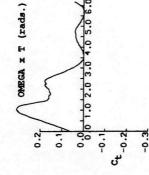


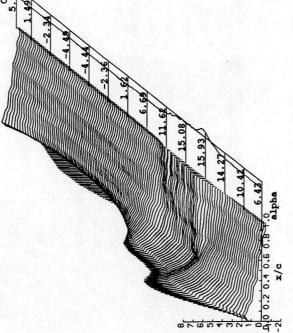


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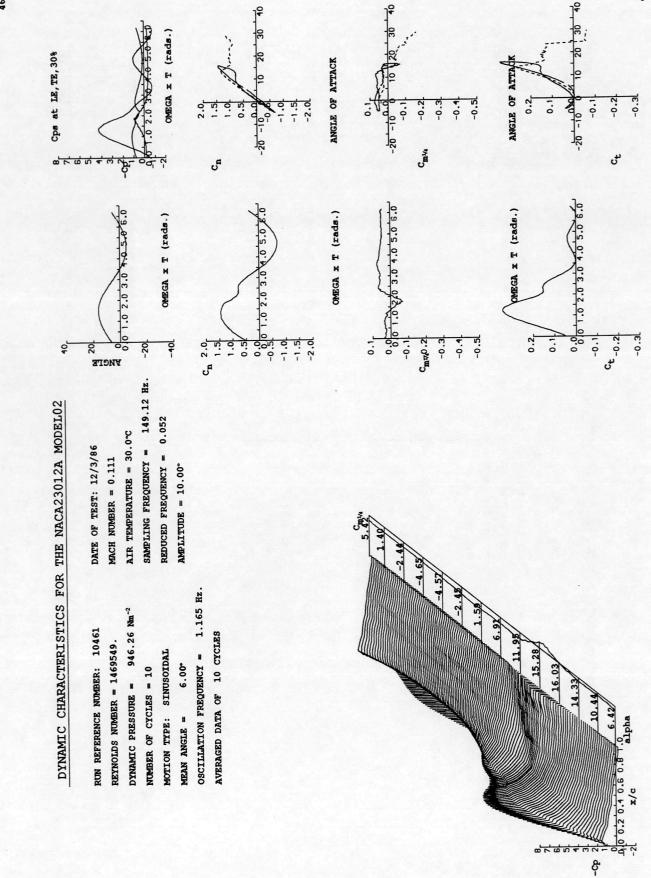


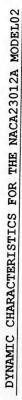


45

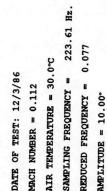
-0.3

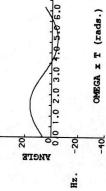
-21

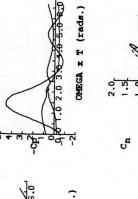


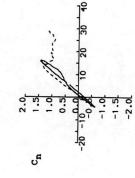


RUN REFERENCE NUMBER: 10471	DATE OF TEST:
REYNOLDS NUMBER = 1483809.	MACH NUMBER =
DYNAMIC PRESSURE = 964.71 Nm ⁻²	AIR TEMPERATU
NUMBER OF CYCLES = 10	SAMPLING FREC
MOTION TYPE: SINUSOIDAL	REDUCED FREQU
MEAN ANGLE = 6.00°	AMPLITUDE = 1
OSCILLATION FREQUENCY = 1.747 Hz.	
AVERAGED DATA OF 10 CYCLES	









0 5.0 8.0

-0.5 -0.5

-1.5

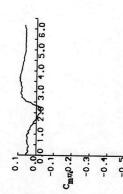
-1.0

cn 2.0

1.0

0.5





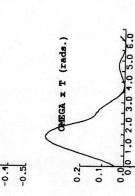
-0.2 E.0-

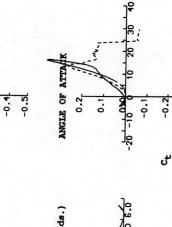
C.m.v.

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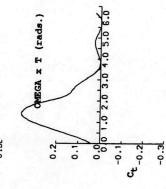
-20 -100-0

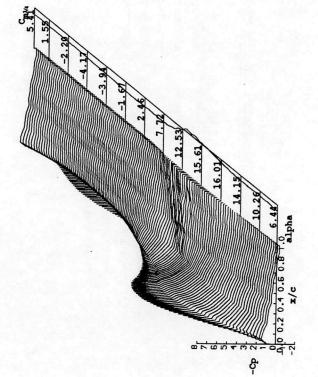




47

-0.3



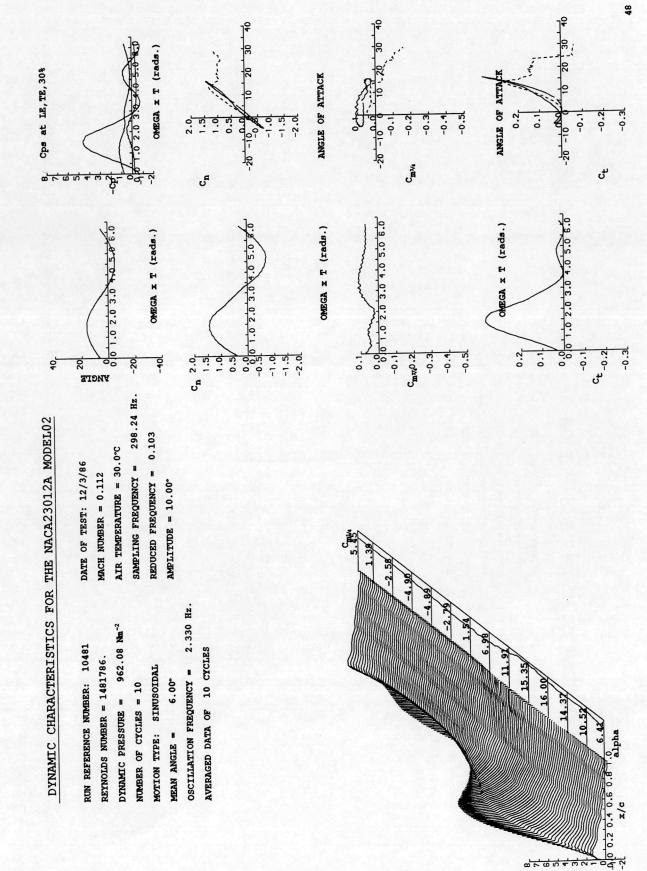


47

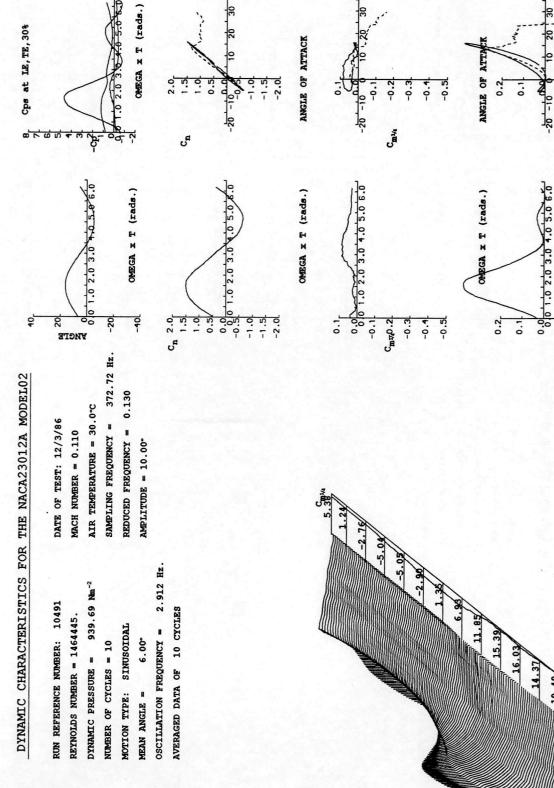
Cps at LE, TE, 30%

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A,0 0.2 0.4 0.6 0.8 -2 x/c

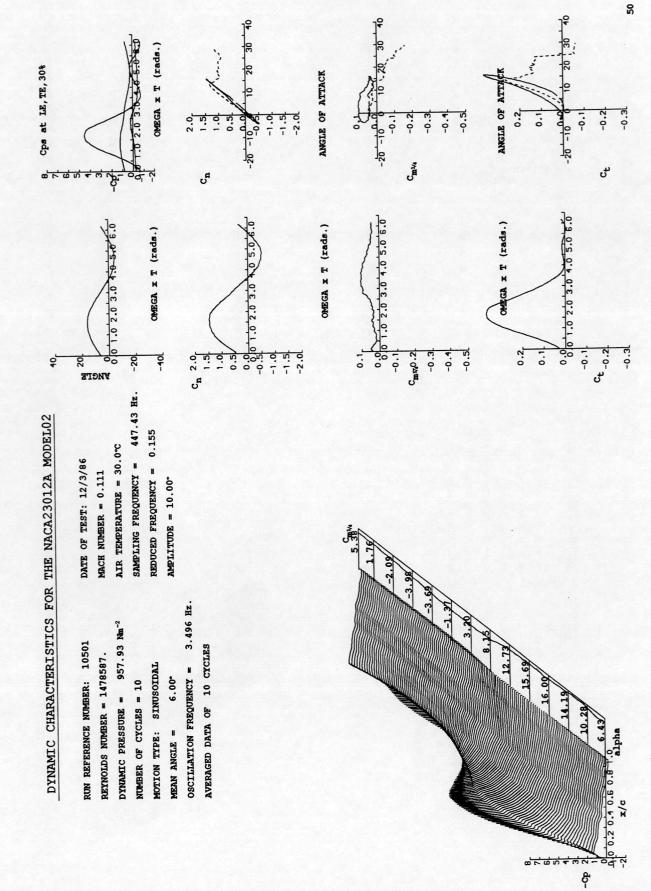
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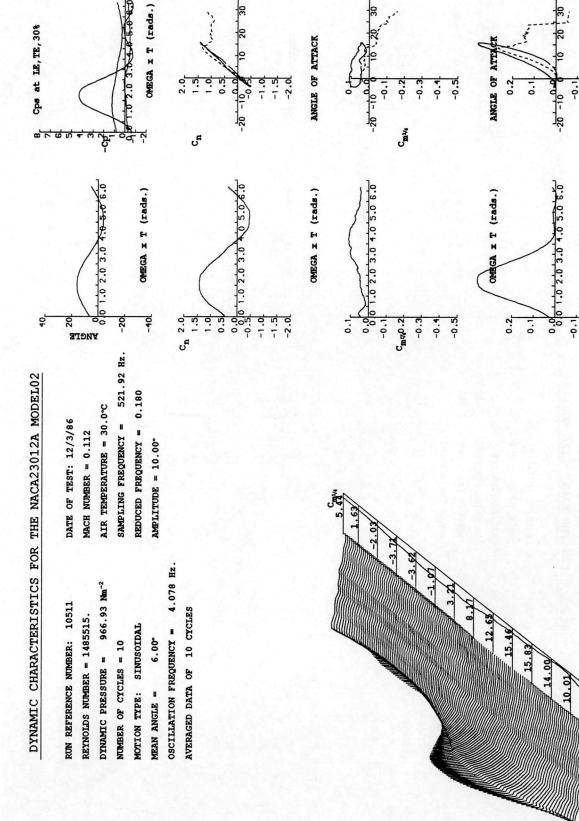
8 1 0

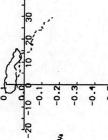
-0.1

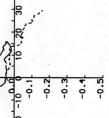
-0.3

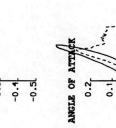
-0-1

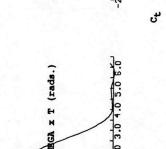


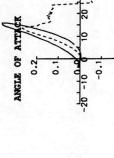


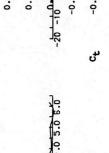












Ct -0.2

6.36 alpha

> 0.2 0.4 0.6 0.8 x/c

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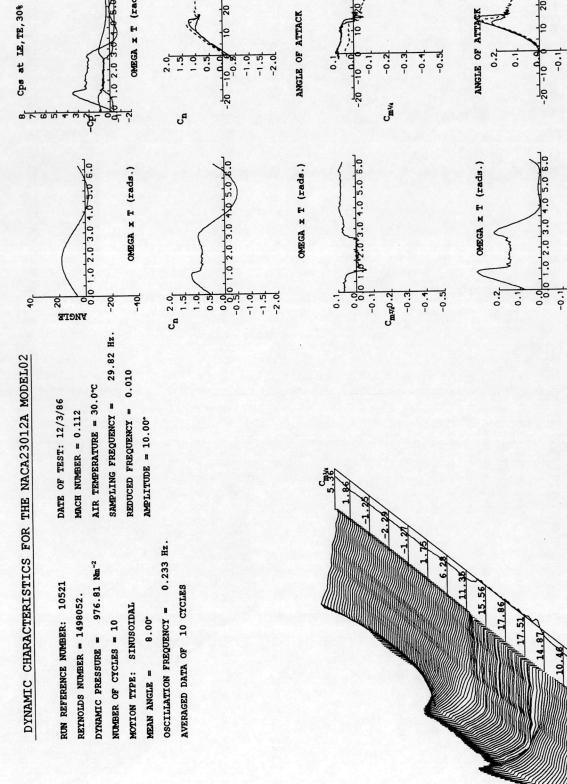
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OMEGA x T (rads.)

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alpha

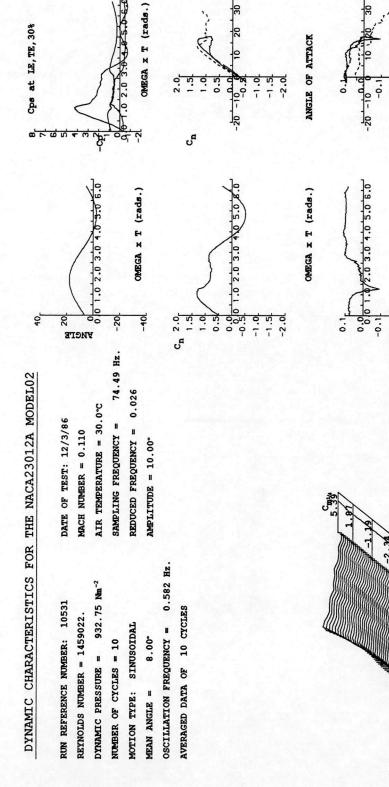
x/c

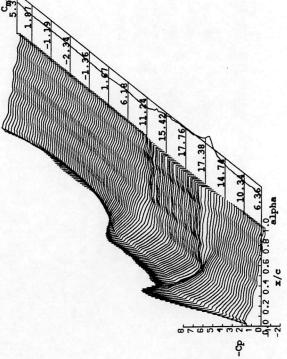
0.0 0.2 0 -2

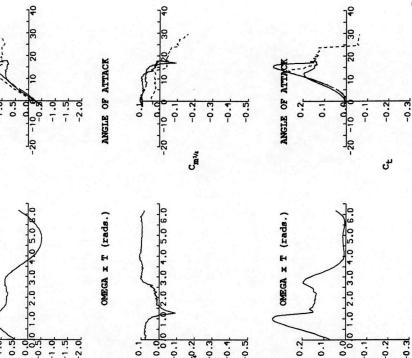
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53

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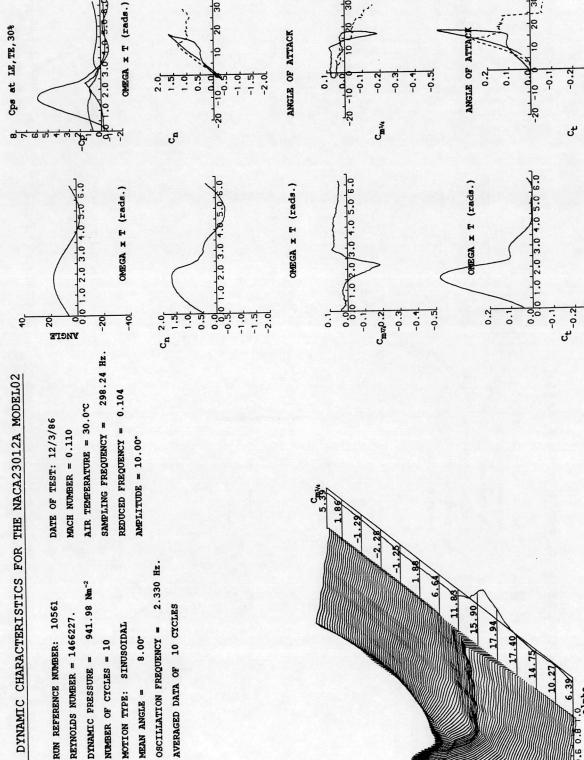
0.2

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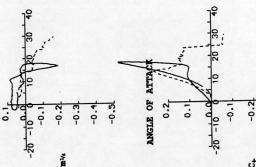
9



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26

DYNAMIC PRESSURE = 941.98 Nm⁻² REYNOLDS NUMBER = 1466227. MOTION TYPE: SINUSOIDAL NUMBER OF CYCLES = 10



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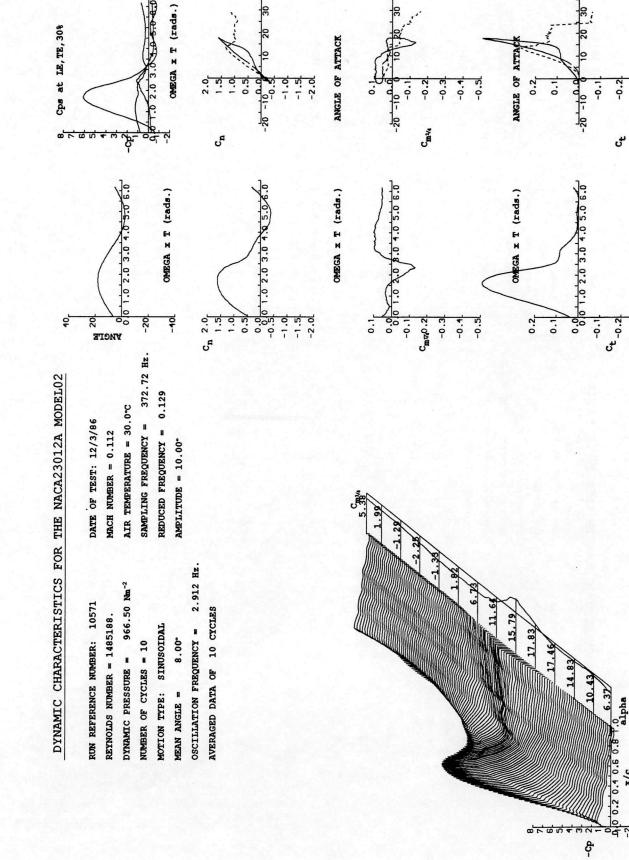
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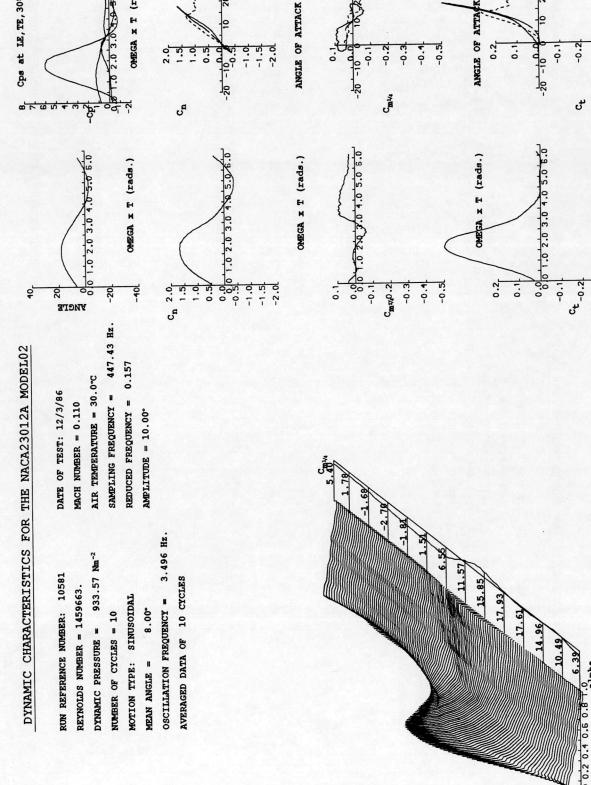
51

-0.3 -0.2

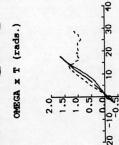
-0.3L

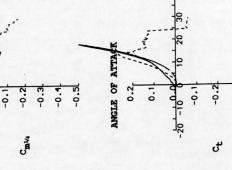
alpha

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0.00 OMEGA x T (rads.) Cps at LE, TE, 30%





18



58

8º

85

alpha

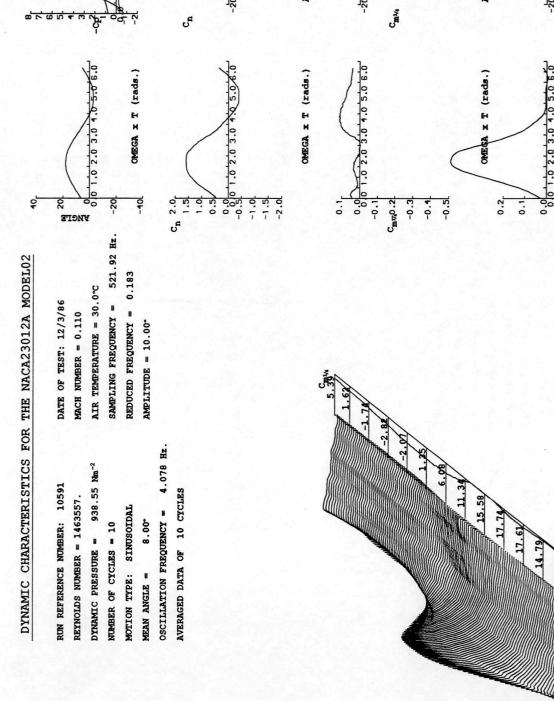
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0.2 -2-0

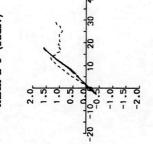
28

-0.3

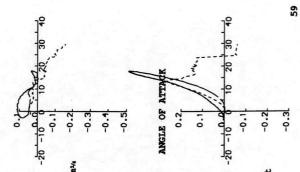
-0.3



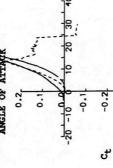
OMEGA x T (rads.) Cps at LE, TE, 30% 0 2.0 3.0 2.0



ANGLE OF ATTACK



ೆ 0 1.0 2.0 3.0 4.0 5.0 6.0



ct -0.2

6.39 alpha

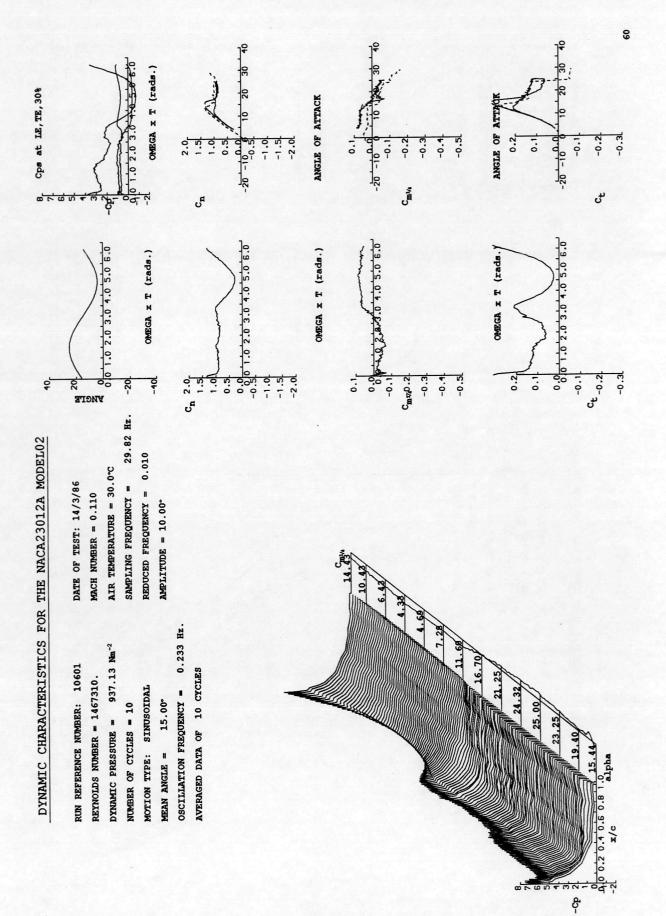
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X/C

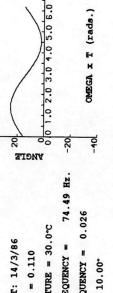
-0.1

-0.3





RUN REFERENCE NUMBER: 10611	DATE OF TEST
REYNOLDS NUMBER = 1459166.	MACH NUMBER
DYNAMIC PRESSURE = 932.93 Nm ⁻²	AIR TEMPERAT
NUMBER OF CYCLES = 10	SAMPLING FRE
MOTION TYPE: SINUSOIDAL	REDUCED FREQ
MEAN ANGLE = 15.00°	AMPLITUDE =
OSCILLATION FREQUENCY = 0.582 Hz.	
AVERAGED DATA OF 10 CYCLES	

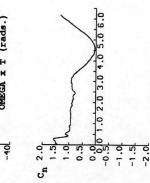


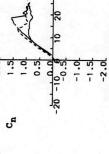
OMEGA X T (rads.)

10 5.0

1.0 2.0 3.0

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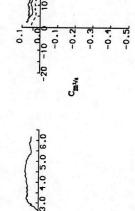


OMEGA x T (rads.)

0.1

0.0

-0.1

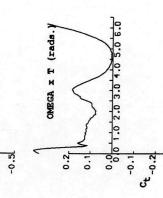


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-0.3

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ANGLE OF ATTA

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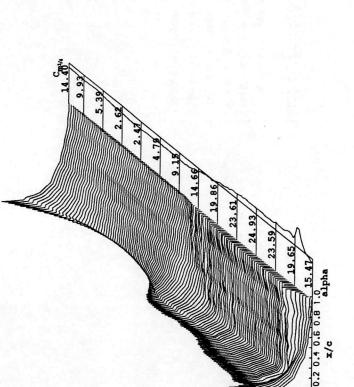
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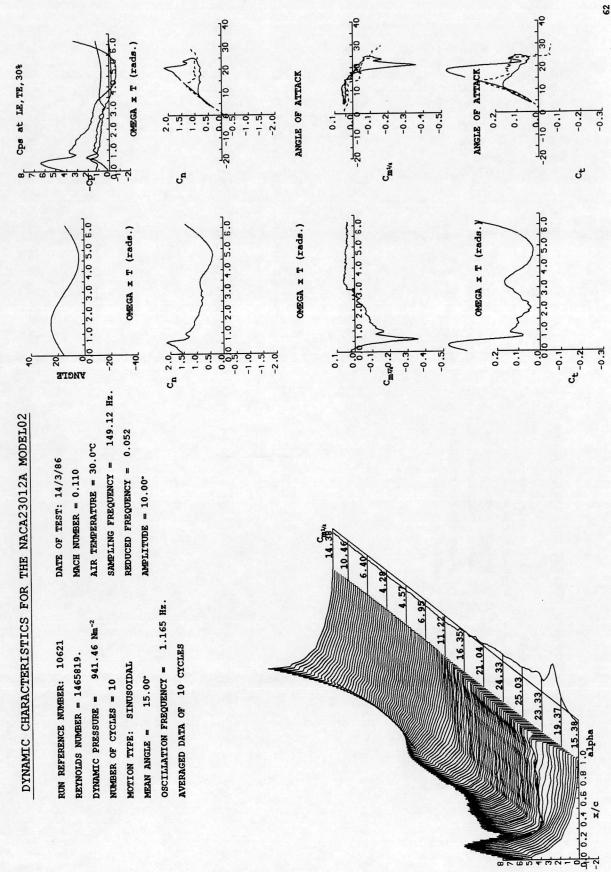
Cps at LE, TE, 30%

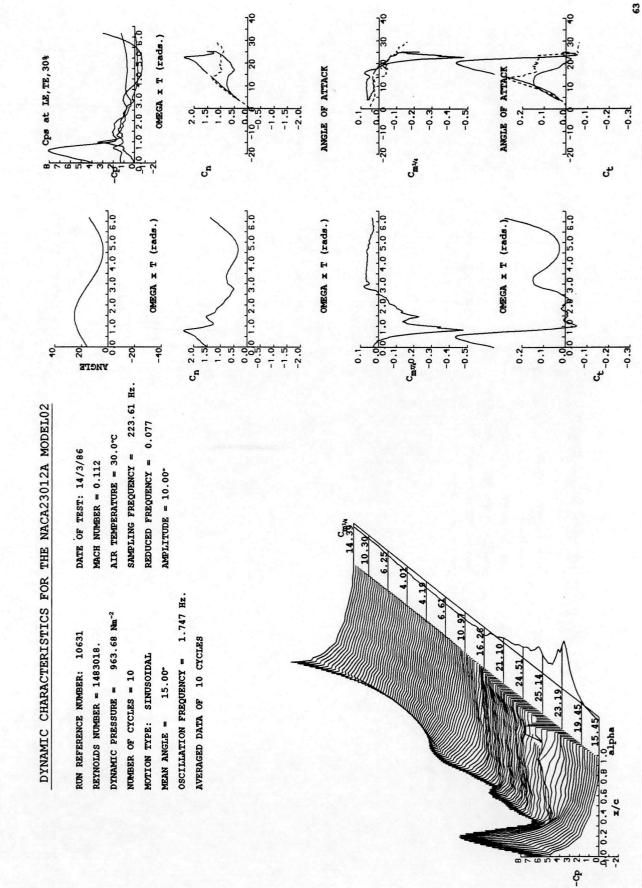
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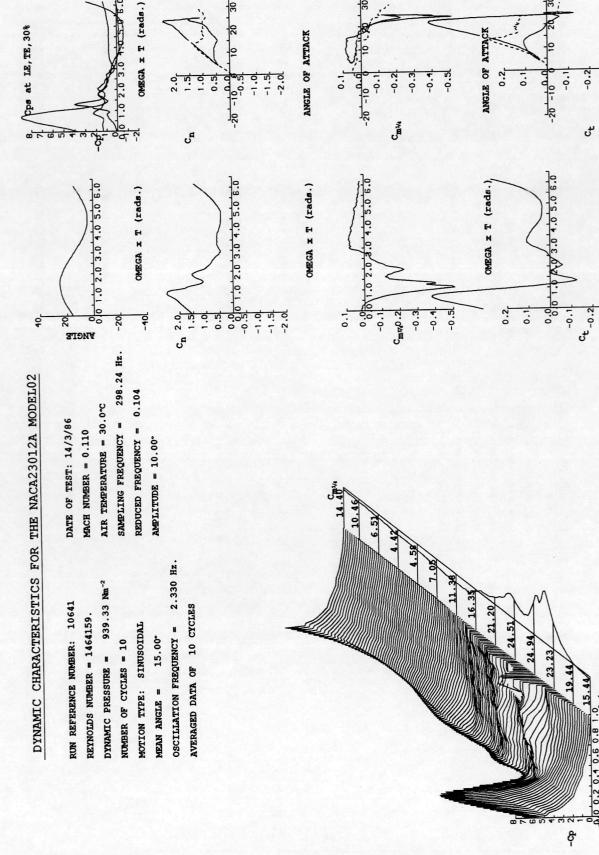
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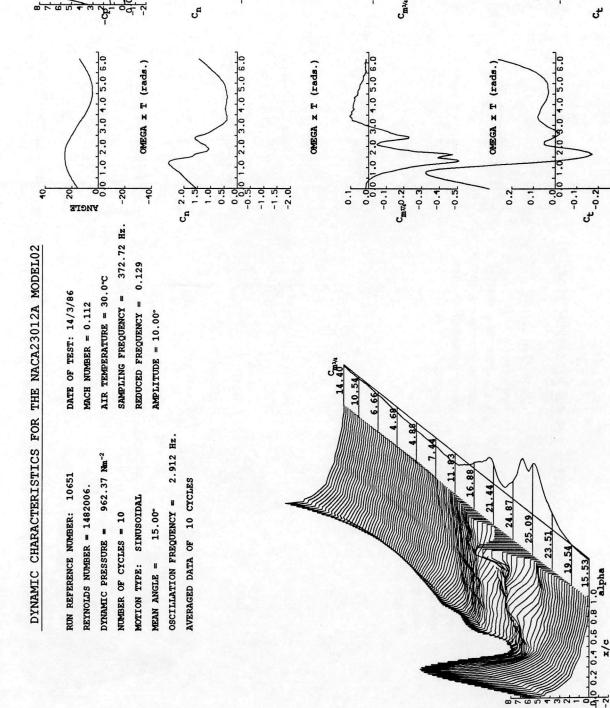
-0.31

15.44 alpha

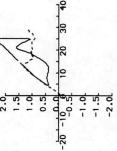
0,0 0.2 0.4 0.6 0.8 -2[**素/c**

-0.2

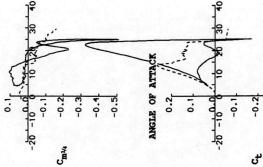
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OMEGA x T (rads.) at LE, TE, 30% 2.0 0 2 2 2 2



ANGLE OF ATTACK



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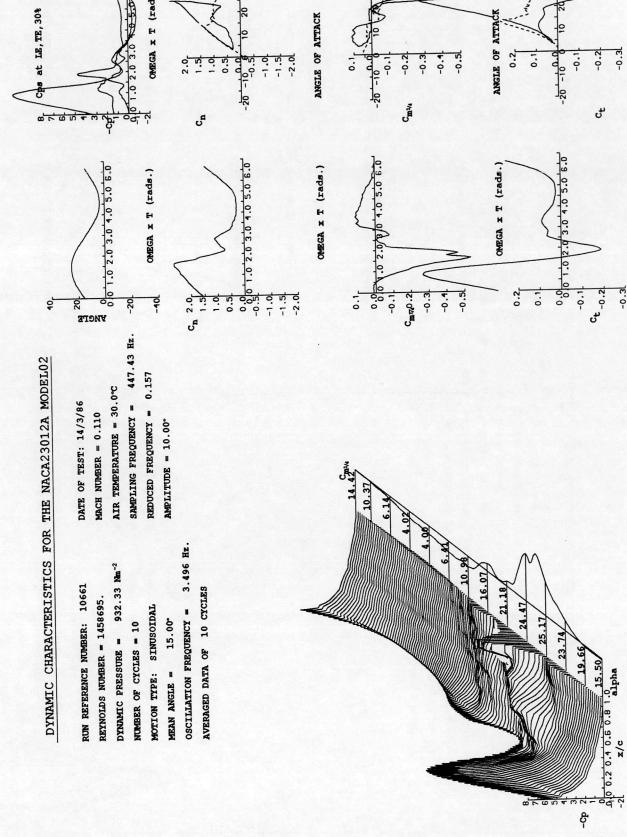
-0.3

E.0-

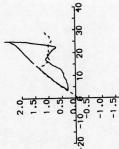
alpha

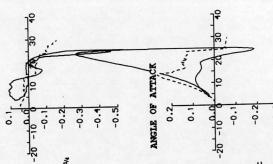
x/c

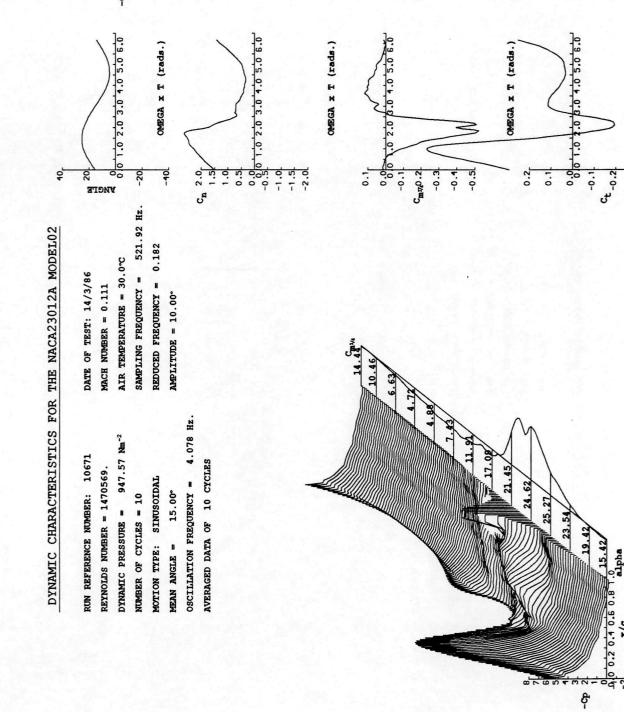
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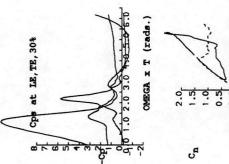


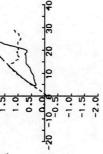
OMEGA x T (rads.)

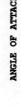


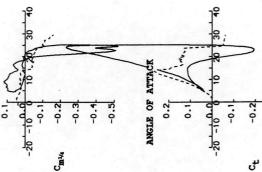












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ANGLE OF ATTACK

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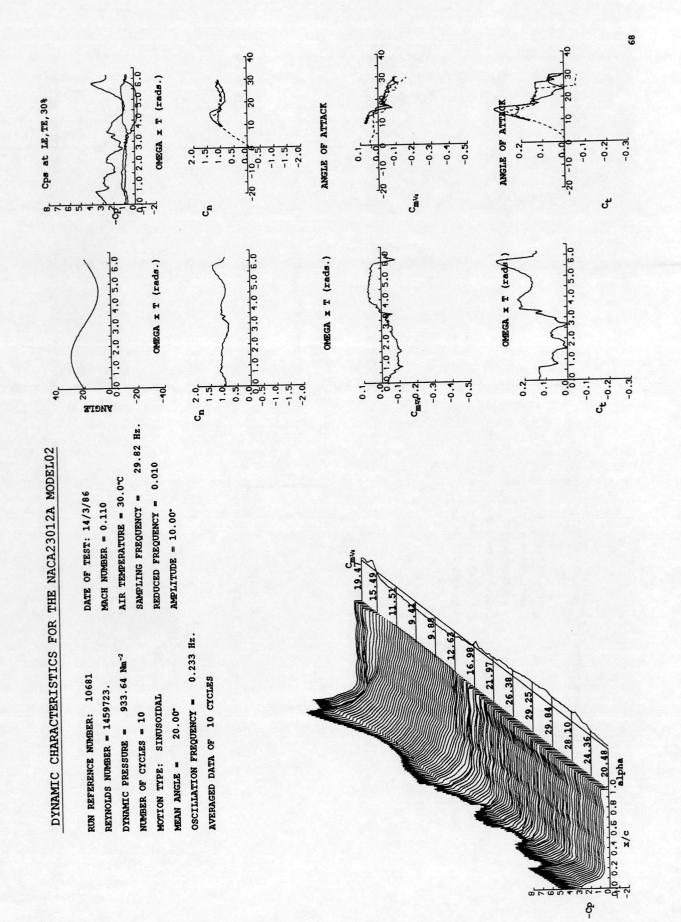
-0.3

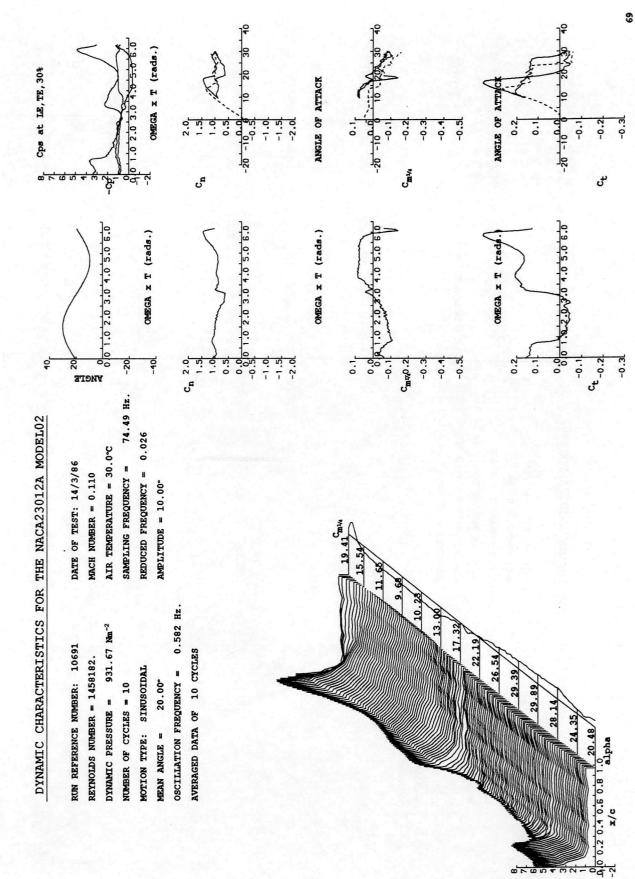
-0.3

alpha

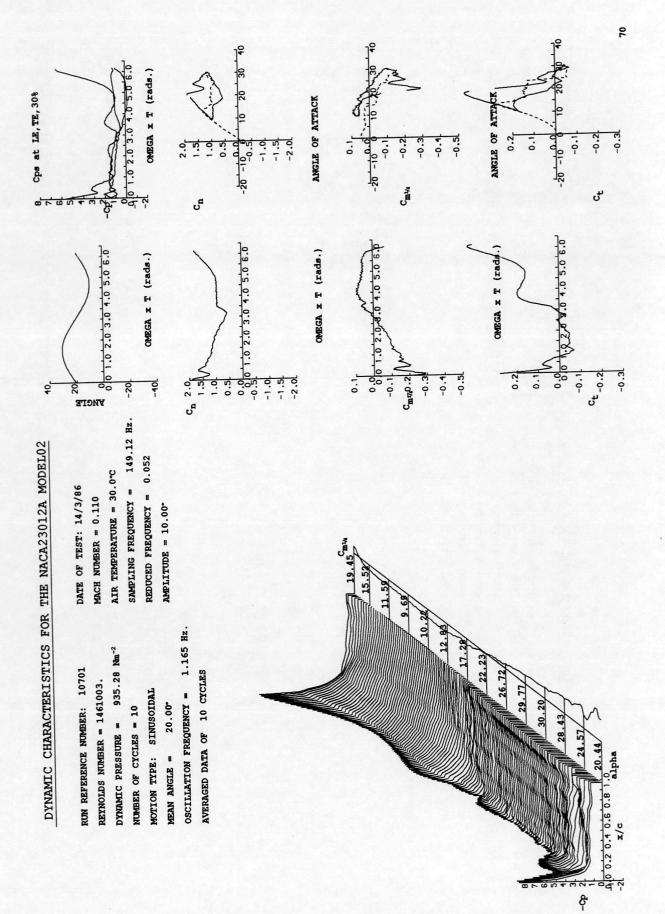
x/c

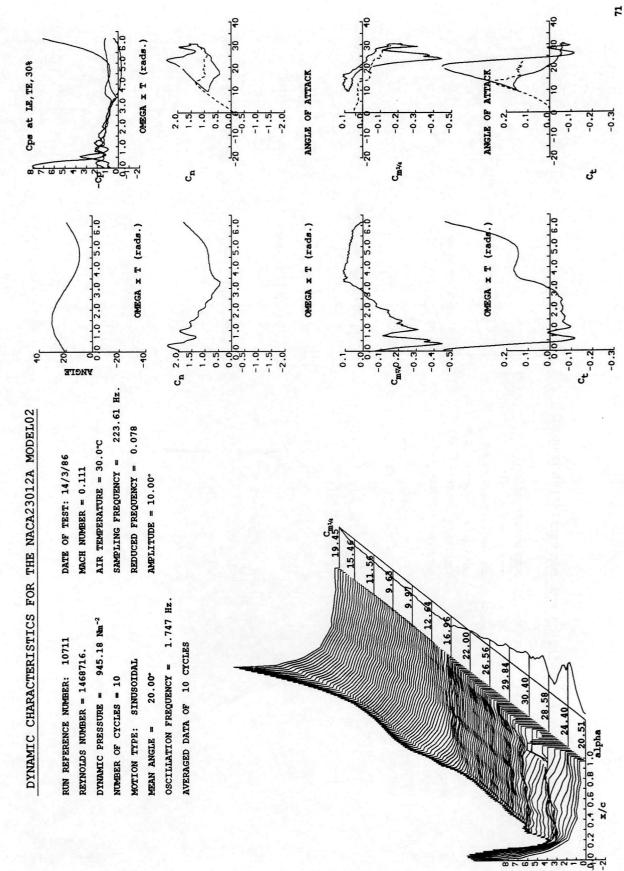
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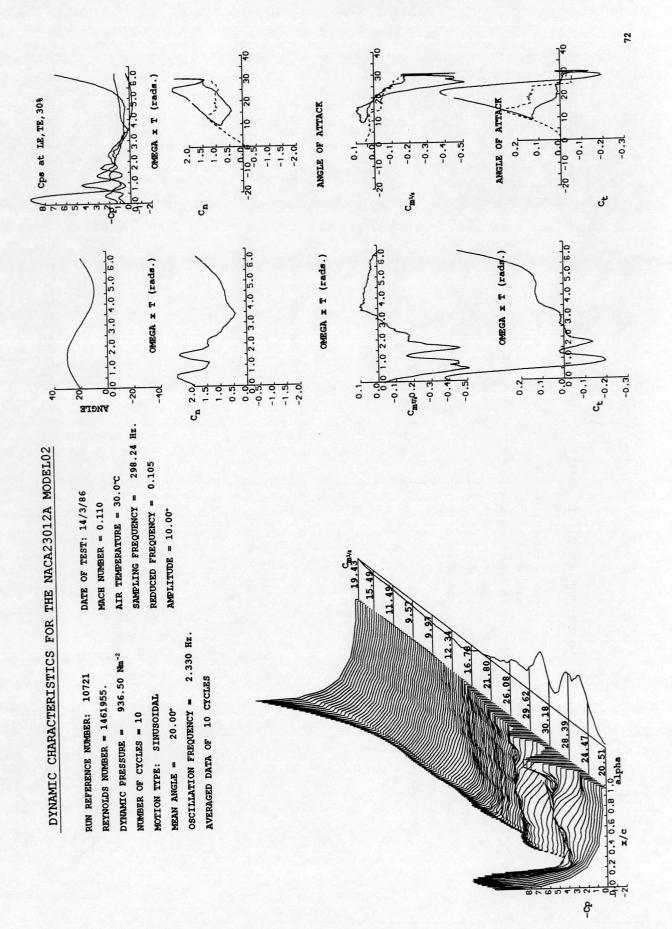


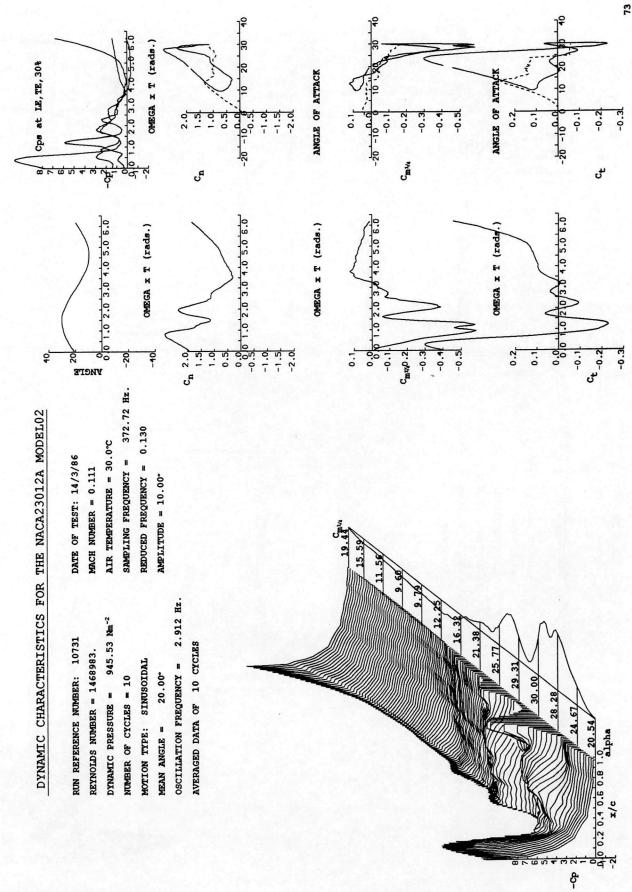


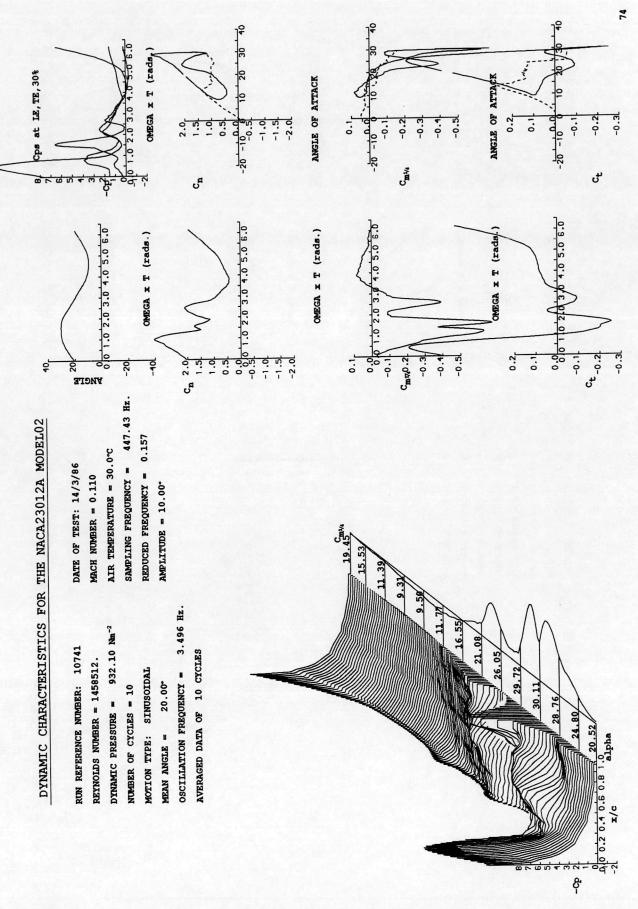
Nę

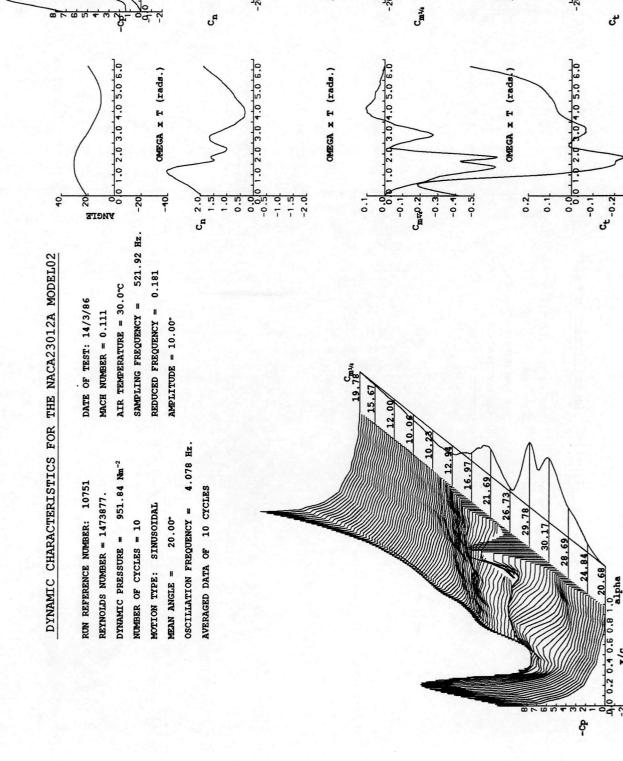




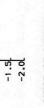




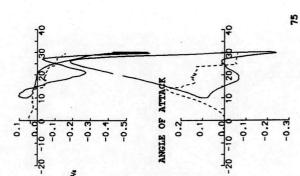




75 20 30 40 2 OMEGA x T (rads, at LE, TE, 30% -20 -10 6 2.0 1.5 0. -1.0 0.5 .

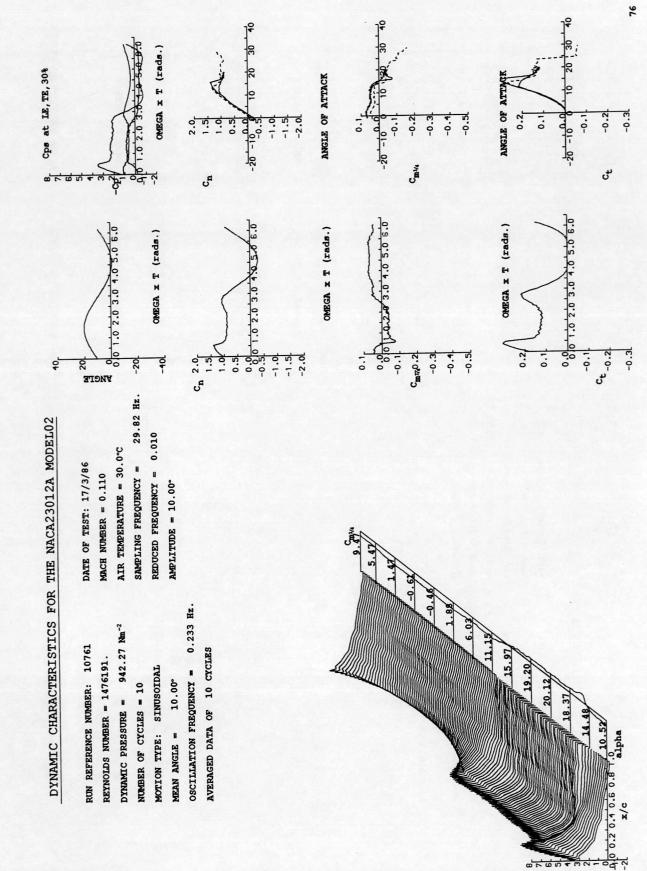


ANGLE OF ATTACK

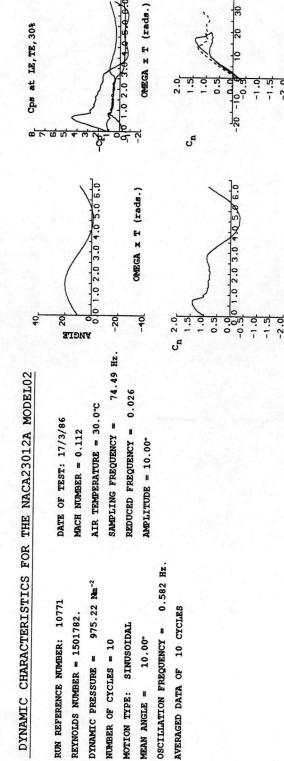


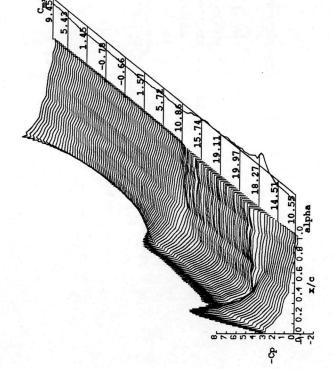
E.0-

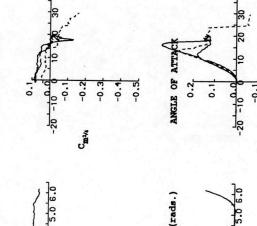
×/G

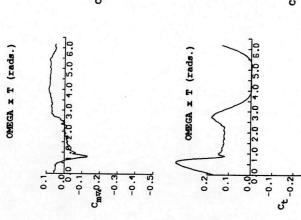


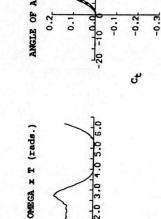
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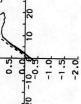


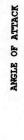
0.1

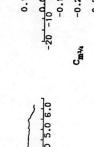
F

16.0-

-0.1





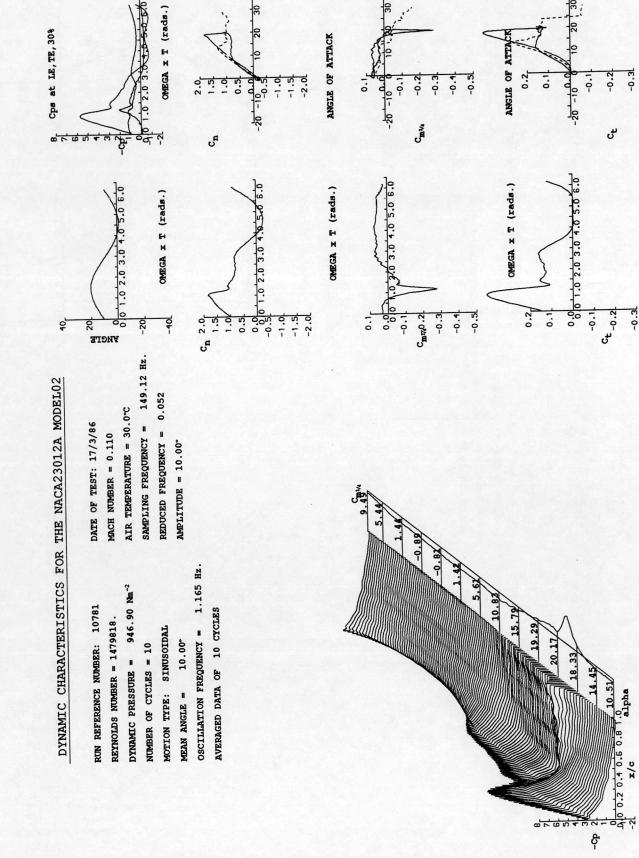


..

-0.1

-0.3

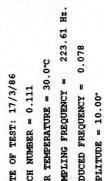
F

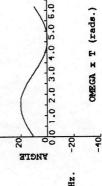


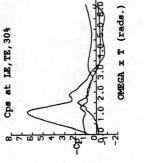
30 40



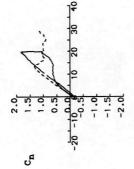
RUN REFERENCE NUMBER: 10791	DAT
REYNOLDS NUMBER = 1491382.	MAC
DYNAMIC PRESSURE = 961.76 Nm ⁻²	AIR
NUMBER OF CYCLES = 10	SAM
MOTION TYPE: SINUSOIDAL	RED
MEAN ANGLE = 10.00°	AMP
OSCILLATION FREQUENCY = 1.747 Hz.	
AVERAGED DATA OF 10 CYCLES	







19



0.001.012.013.014.045.06.0

0.5

1.0

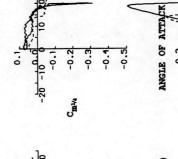
cn 2.0

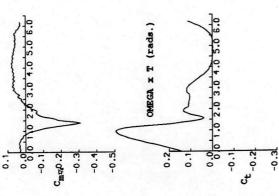


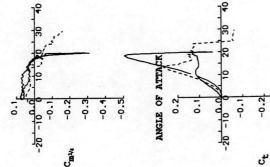
OMEGA X T (rads.)

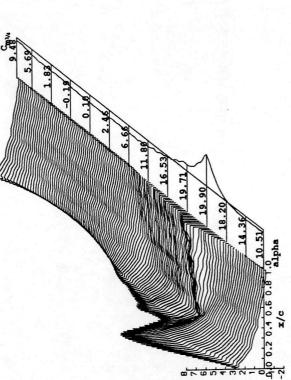
-1.5

-1.0









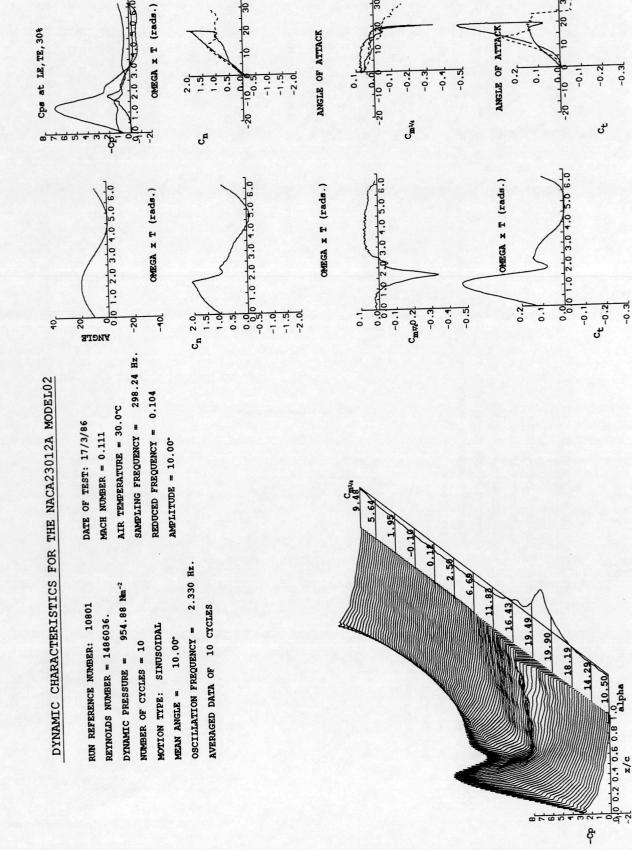
0000

-21

d'

19

-0.3



30 40

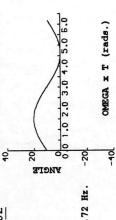
80

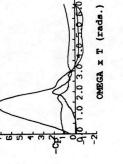
8

-0.3



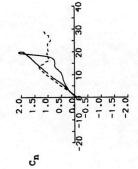
RUN REFERENCE NUMBER: 10811	DATE OF TEST: 17/3/86
REYNOLDS NUMBER = 1482537.	MACH NUMBER = 0.110
DYNAMIC PRESSURE = 950.38 Nm ⁻²	AIR TEMPERATURE = 30.0°C
NUMBER OF CYCLES = 10	SAMPLING FREQUENCY = 372.
MOTION TYPE: SINUSOIDAL	REDUCED FREQUENCY = 0.131
MEAN ANGLE = 10.00°	AMPLITUDE = 10.00°
OSCILLATION FREQUENCY = 2.912 Hz.	
AVERAGED DATA OF 10 CYCLES	





Cps at LE, TE, 30%

8



1.0 2.0 3.0 4.0 5.0 6.0

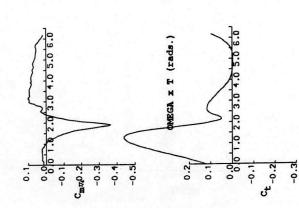
0.00

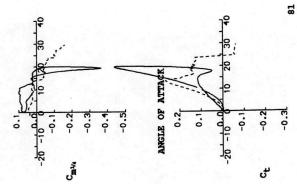
0.5

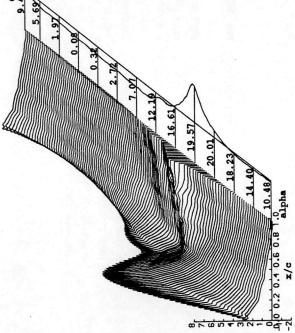
-1.0 -1.5 -2.0

cn 2.0

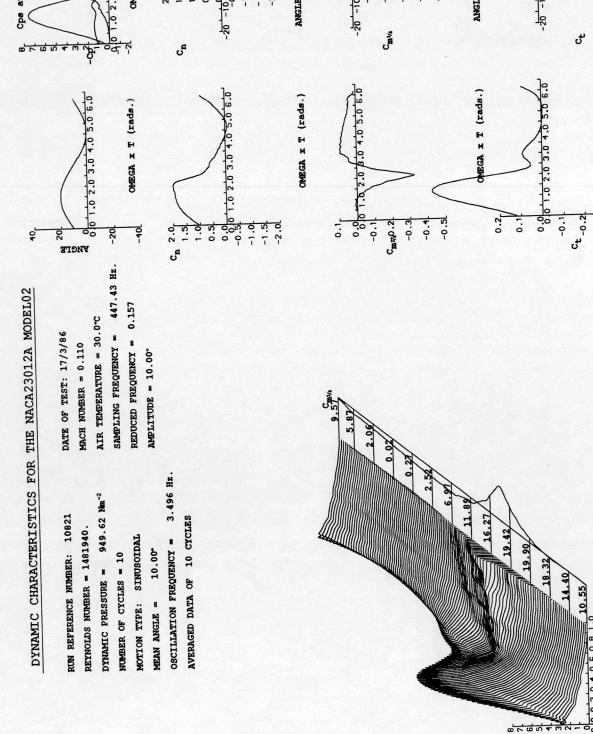




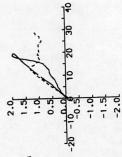




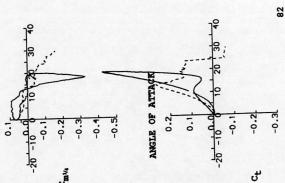
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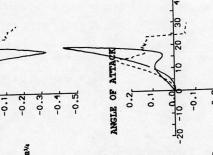


OMEGA x T (rads.) Cps at LE, TE, 30% 1.0 2.0 3.



ANGLE OF ATTACK





-0.3

10.55

alpha

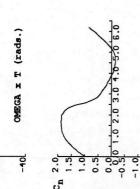
X/C

A 0 0.2

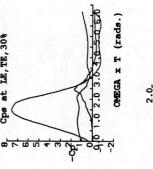
ę

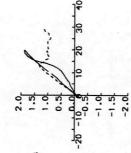


20- 0-1-0-2-0-3-0-4-0-5-0-6-0		-20. -40. OMEGA x T (rads.)				cn 2.0	
DATE OF TEST: 17/3/86	MACH NUMBER = 0.111	AIR TEMPERATURE = 30.0°C	SAMPLING FREQUENCY = 521.92 Hz.	REDUCED FREQUENCY = 0.182	AMPLITUDE = 10.00°		u D
RUN REFERENCE NUMBER: 10831	REYNOLDS NUMBER = 1488742.	DYNAMIC PRESSURE = 958.36 Nm ⁻²	NUMBER OF CYCLES = 10	MOTION TYPE: SINUSOIDAL	MEAN ANGLE = 10.00°	OSCILLIATION FREQUENCY = 4.078 Hz.	AVERAGED DATA OF 10 CYCLES



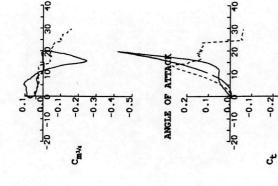
ď

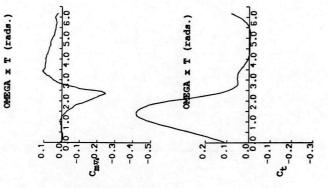


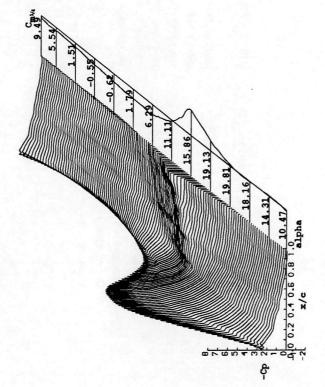




-1.5







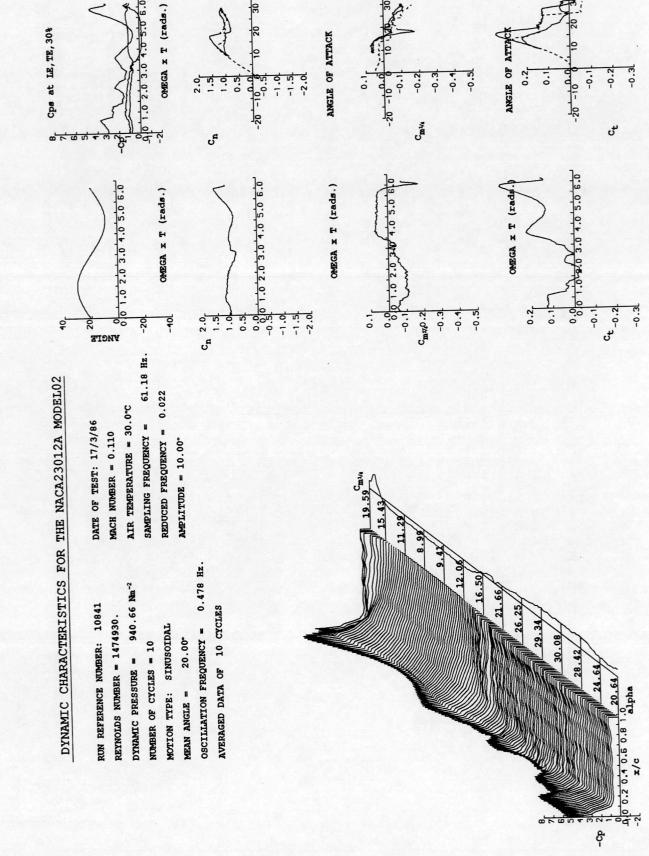
83

Cps at LE, TE, 30%

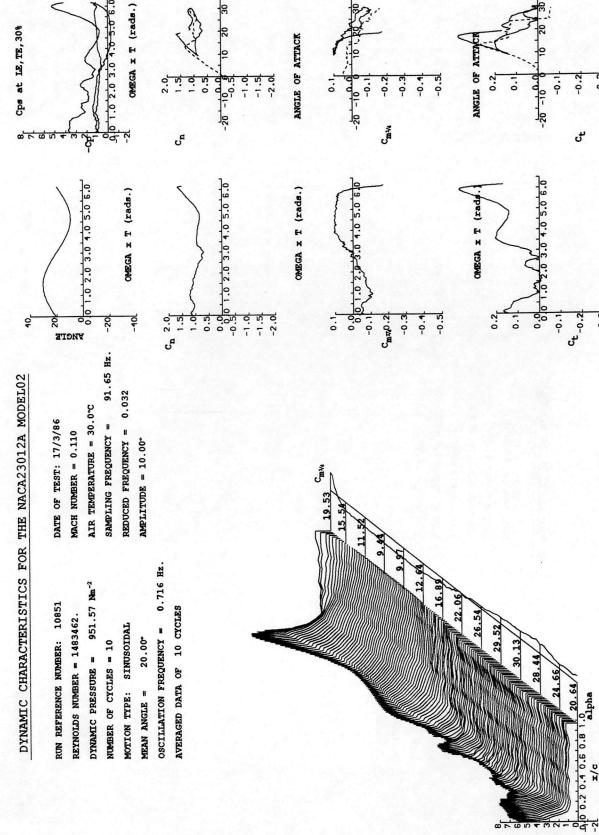
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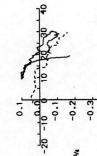
83

-0.3

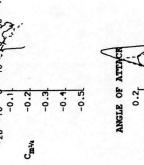


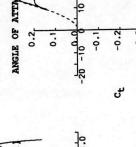
30 40



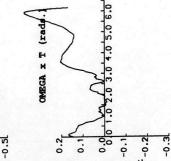


30 40





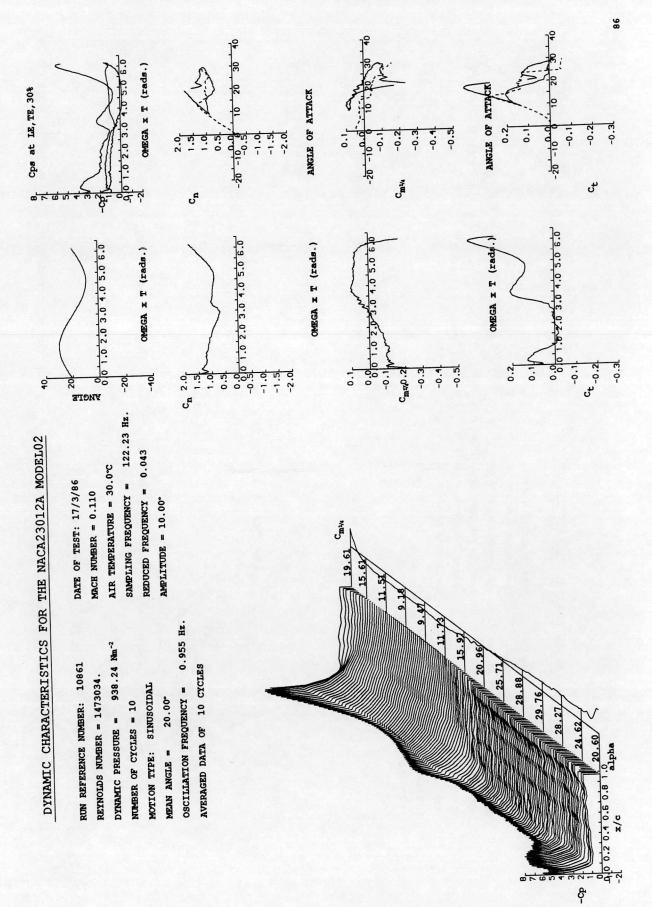
10

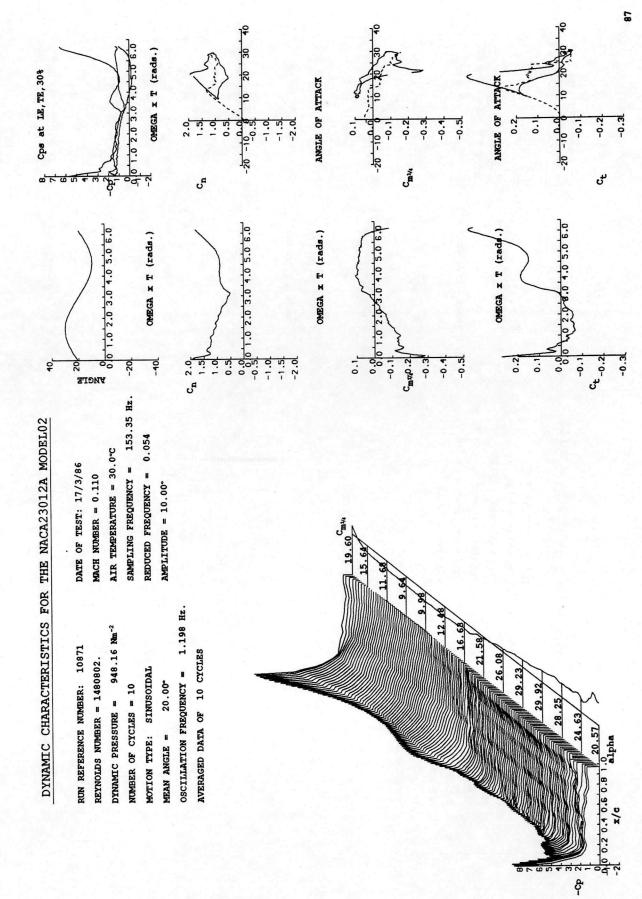


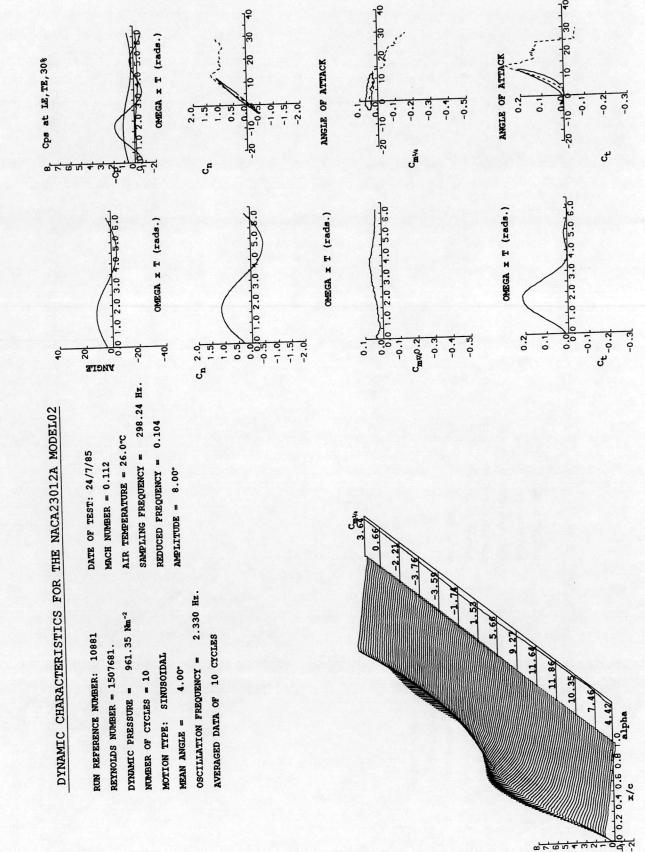
x/c

ę

-0.3



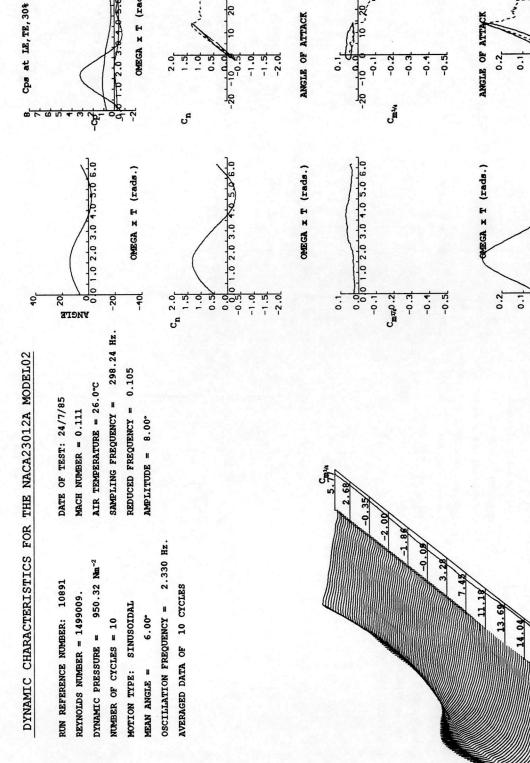


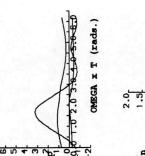


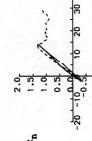
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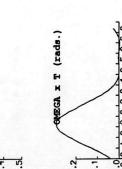


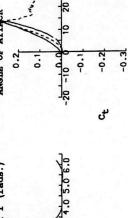


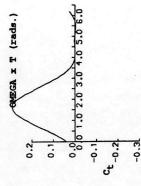




P





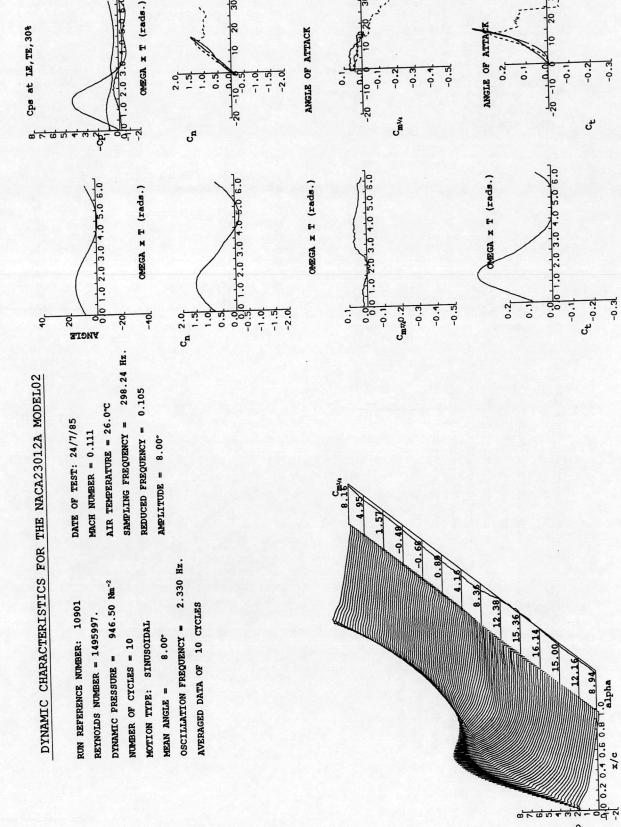


2.5

0.4 0.6 x/c 0.2 0.0 01004 n n

ę

6.51 addla



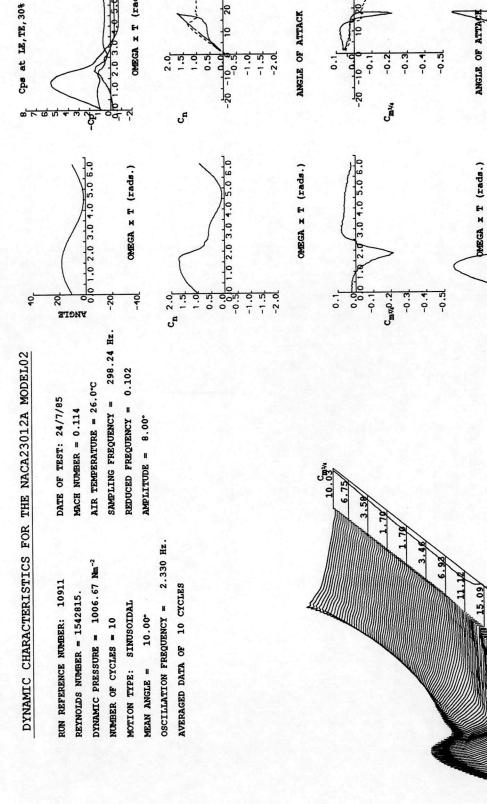
18

6

-Cp 2

8×00×0

8

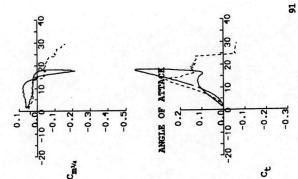


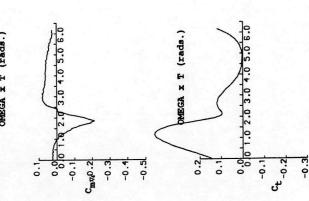
0.1 0.5 -2.01

-1.5

-1.0

OMEGA x T (rads.)





0.2

17.7

18.25

0000

16.9

10.77 alpha

0 0.2 0.4 0.6 0.6 -2 x/c

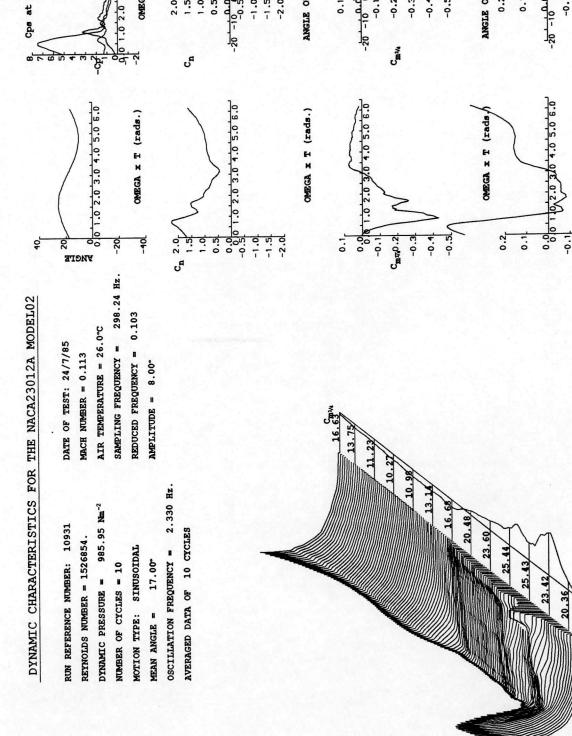
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0.1

-0.1

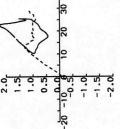
Cn 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	ANGLE OF ATTACK -20-10-0-0-1-0-10-100-30-40 -0.30-10-0-0-10-20-30-40 -0.30-10-0-0-10-20-30-40 -0.30-10-0-0-10-20-30-40 -0.2-0-10-0-0-0-10-20-30-40 -0.2-0-10-0-0-0-0-10-20-30-40 -0.2-0-0-10-0-0-0-0-20-30-40 -0.2-0-0-0-0-0-0-0-20-30-40 -0.2-0-0-0-0-0-0-0-20-30-40 -0.2-0-0-0-0-0-0-0-20-30-40 -0.2-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0
$ \begin{array}{c} \text{DELO2} \\ \text{C} \\ \text{C}$	OMEGA X T (rade.) 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0
DYNAMIC CHARACTERISTICS FOR THE NACA3012A MODEL02 RUN REFERENCE NUMBER: 10921 DATE OF TEST: 24/7/85 RUN REFERENCE NUMBER: 10921 DATE OF TEST: 24/7/85 REYNOLDS NUMBER = 1527392. DATE OF TEST: 24/7/85 DYNAMIC PRESSURE = 986.65 Nm ⁻² DATE TEMPERATURE = 26.0°C DYNAMIC PRESSURE = 986.65 Nm ⁻² AIR TEMPERATURE = 26.0°C NUMBER OF CYCLES = 10 REDUCED FREQUENCY = 298.24 MOTION TYPE: SINUSOIDAL REDUCED FREQUENCY = 0.103 MOTION TYPE: SINUSOIDAL REDUCED FREQUENCY = 0.103 MOTION TYPE: SINUSOIDAL REDUCED FREQUENCY = 0.103 MOTION TYPE: SINUSOIDAL AMFLITUDE = 8.00° MOTION TYPE: SINUSOIDAL AMFLITUDE = 8.00° MOTION TYPE: SINUSOIDAL AMFLITUDE = 8.00° MEAN ANGLE = 12.00° AMFLITUDE = 8.00° MEAN ANGLE = 12.00° AMFLITUDE = 8.00° MEAN ANGLE = 12.00° AMFLITUDE = 8.00° MEAN ANGLE = 10.0°° AMFLITUDE = 8.00°	d_{1}

92



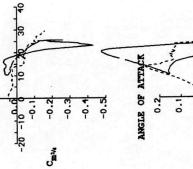
Cps at LE, TE, 30%

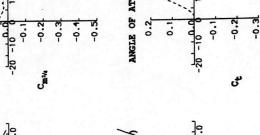
1.0 2.0 3.0 4.0 5.0 6.0 OMEGA x T (rads.)



]²

ANGLE OF ATTACK





6

Ct -0.2

17.40

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-2 x/c 0.2 0.4 0.6 0.8 1.0

16.0-

