



## Abstract

Monthly duration curves have been constructed from climate data across Europe to help address the relative frequency of ecologically critical low flow stages in temporary rivers, when flow persists only in disconnected pools in the river bed. The hydrological model is based on a partitioning of precipitation to estimate water available for evapotranspiration and plant growth and for residual runoff. The duration curve for monthly flows has then been analysed to give an estimate of bankfull flow based on recurrence interval. The corresponding frequency for pools is then based on the ratio of bank full discharge to pool flow, arguing from observed ratios of cross-sectional areas at flood and low flows to estimate pool flow as 0.1% of bankfull flow, and so estimate the frequency of the pool conditions that constrain survival of river-dwelling arthropods and fish. The methodology has been applied across Europe at 15 km resolution, and can equally be applied under future climatic scenarios.

## 1 Introduction

Many of our hopes (Sivapalan et al., 2003) of providing a basis for making predictions in ungauged drainage basins have stalled on the unexplained dissimilarities of apparently similar basins. Here we focus on the impact of climatic inputs on the hydrologic responses of catchments, paying particular attention to their low flow characteristics and how these are controlled by the seasonality of climate, the response of vegetation cover and the interactions with evapotranspiration and runoff throughout the year. It is hoped that differences in monthly duration curves, analysed here, can provide one tool for looking at and classifying the characteristic signatures of climate and the contrasting hydrological regimes that are driven by climatic differences. By looking for major differences across a wide range of catchments, we deliberately focus on the climatic signal that distinguishes between, for example, snow-dominated, humid and semi-arid

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five years to stabilise the hydrology and then run for the 50-year period to generate a synthetic monthly flow exceedance curve.

Although there are many local factors that influence hydrological response, including the presence of aquifers, variations in soil properties, imposed land use and water abstractions or return of treated wastewater, these have not been incorporated into the model presented here, allowing broad patterns of difference to emerge that are related to climatic differences and their impact on the hydrological regimes. The model has been developed in the context of the EU MIRAGE project, on water management in southern Europe, so that the examples used largely reflect concern with ecological status of temporary rivers, which is intimately linked to the presence or absence of disconnected or zero surface flow during the summer period.

## 2 Model structure

### 2.1 Construction of synthetic climate time series

The CRU European and Global 10-min databases (New et al., 2002; Mitchell et al., 2003) contain averages for monthly total precipitation and its standard deviation, and number of rain days per month. They also contain data for temperatures and mean values of vapour pressure or relative humidity. The European data base also contains year by year monthly values for 1901–2000, and these data are sufficient to estimate monthly potential ET, using the Hargreaves method (Hargreaves and Samani, 1982), for each month, and consequently mean and standard deviation for each month. This method estimates top of atmosphere radiation from latitude, and air temperature to modify this to make some correction for cloudiness. Additional ERA-40 data have been added (BADC) for the coefficient of variation of rain on rain-days, averaged for the same spatial grid.

These data have then been used to define distributions, and a 50-year time series has been generated by drawing independent samples from these distributions. Monthly

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loss by further ET from the saturated zone, calculated separately for vegetated and bare areas. Combining these components provides an estimate for total actual ET, plant water use (pro-rated to cover) and the several components of runoff by overland and subsurface pathways.

Plant water use is then used to estimate vegetation and soil organic matter biomass. Although a transient model might be desirable, it was recognised that times for equilibration, particularly for organic matter in potentially saturated environments, might be excessive, so that biomass was calculated for equilibrium conditions, updated annually to allow for minor changes in response to climate variability. Finally cover and biomass were used to update the runoff threshold, providing a dynamic link between overland flow runoff and vegetation in response to the prevailing climate.

### 2.3 Exceedance curves and other indicator tools

The model is based on runoff generation from source areas, and assumes that all runoff pathways contribute to stream flow downstream. Exceedance curves were generated from the combined total runoff contributions for each month, providing a basis that, in our experience, could be most reliably compared with observed data. These were sorted and presented as a plot of  $\log(\text{monthly discharge})$  against probability of exceedance, plotted on a probability scale or z-score, so that a log-normal distribution of discharges appears as a straight line. Since, we wish to analyse the frequency of low flow conditions, we have preferred to use the complete synthetic record, rather than partition it from the outset on the basis of dry periods, as has been proposed by Viola et al. (2011). Examples are shown in Fig. 4.

Five catchments have been chosen across a range of environments to examine the response of the exceedance curves to climate. Table 1 summarizes their characteristics, showing their position, precipitation and estimated potential ET. It can be seen that the catchments range from semi arid, with precipitation less than half potential ET, to humid with precipitation exceeding potential ET, and with a range of seasonality.

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These test catchments have been used to test whether the hydrological model is able to distinguish broad differences in duration curve characteristics without specific optimisation of parameters for each site.

The model is driven by three significantly changeable parameters. The first of these is the TOPmodel “ $m$ ” parameters, which describes the rate at which subsurface drainage decreases as saturation deficit increases, and has the dimensions of depth (mm of water). High values of  $m$  provide some subsurface flow even at high deficits, and give long-tailed recession curves. Whereas low values of  $m$  give flashy response, with negligible flow at high saturation deficit. The value of  $m$  scales the deficits (and implicitly depths) to which water will drain.

The second control parameter is the rooting depth under vegetation,  $R$ , which is also expressed as a water deficit. Vegetation is able to extract transpiration water readily under conditions when the deficit is less than the rooting depth, and progressively less as the deficit increases. Bare soil evaporation is also allowed, but with a small (5 mm) scale depth, and total transpiration loss combines bare soil and plant transpiration according to the prevailing crown and root cover.

The third parameter is the subsurface runoff at saturation,  $j_*$ . This is important for partitioning between subsurface and saturation excess overland flow, and is increasingly important as the simulation time step is reduced, but has little impact on total runoff for the monthly time steps used here. Other parameters control the rate of conversion of plant transpiration to biomass, respiration, leaf etc. fall and decomposition, and these have been taken from values used in the PESERA model, and taken from the literature without further adjustment.

For suitable climatic areas, the model shows three main response zones to the two primary parameters. First a zone in which rooting depth is much less than TOP-model  $m$ . Here the response is dominated by subsurface and saturation excess overland flow, with little sensitivity to the vegetation. In humid areas, the soil is frequently close to saturation, and plant growth is unrestricted by water. In more arid areas, few of these shallow-rotted plants are able to survive. In a second zone, where rooting depth

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is substantially greater than TOPmodel  $m$ , the hydrology is dominated by root extraction, with minimal lateral subsurface drainage. Under humid conditions, most runoff occurs as saturation excess overland flow, while in semi-arid conditions deep-rooted plants exploit percolating storm rainfall. However, the response of the catchments investigated all lay between these extremes, in a zone where both subsurface flow and plant transpiration play a part. Where the climate is seasonal, then dry seasons are typically dominated by root extraction, and wet seasons by increased subsurface flow.

For the five test catchments, the goodness of fit of the modelled duration curve was estimated from the average root mean square (RMS) difference between observed and estimated log(discharge) across the range of non-zero values. To minimise inconsistencies, the same climate realisation was used for each parameter pair, and each different realisation produces a slightly different error map. Figure 3a shows an example for the Hozgarganta catchment, over the ranges  $m = 2\text{--}52$  mm;  $R = 10\text{--}210$  mm. It can be seen that there is a weakly defined optimum at  $m = 6$  mm;  $R = 54$  mm, within a trough-shaped region in which  $m$  and  $R$  increase together, maintaining moderately low values of the RMS error. Similar mappings can be made for the other catchments, and Fig. 4 shows the optimum values of  $m$  and  $R$  for each. Comparing these values, it can be seen that higher values of  $m$  are generally associated with higher values of  $R$ . It is therefore suggested that a single global parameter set might encapsulate much of the significant climatic difference across all sites.

To estimate the best global values, individual error maps for each site (similar to Fig. 3a) have been normalised to  $(\text{RMS value} - \text{Minimum value}) / (\text{Maximum value} - \text{Minimum Value})$ , so that each error map is linearly transformed to the range  $[0, 1]$ . Figure 3b is then obtained as the average of the five normalised error maps, and itself shows a minimum, with an average of 13.4% deviation from the individual optima. This minimum sets the global parameter values at  $m = 6$  mm;  $R = 50$  mm. An alternative criterion is, for each parameter set, to map the largest of the normalised errors for the test catchments; and select the least maximum (27%), a minimax solution that gives parameter values of  $m = 6$  mm;  $R = 60$  mm. The former values have been used, giving

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a minimax normalised error of 32%.

For each of the five test catchments, Fig. 4 shows the exceedance curves plotted from the observed data, and with simulated curves generated with the local best fit parameter set and the global set. It can be seen that differences between the three curves for each site are much smaller than the differences between the five sites, and this encourages us to use the global parameter values to simulate regional patterns of natural variation in the exceedance curves. It is recognised that many factors are not taken into account in this analysis, including the impact of non-natural vegetation, abstraction of water for irrigation, domestic use and industry, return of urban waste water and exchange with aquifers, particularly karst aquifers.

### 3 Analysis of low flow conditions from exceedance curves

To interpret low flow conditions for streams in different climates, we have used the concept of bank full discharge to provide a generalised measure of channel dimensions, and have used the well known, although not necessarily totally reliable, method of associating bank full discharge with a frequency of occurrence. An exceedance with a z-score of  $-2.5$ , corresponding to a probability of 0.62%, or 3.7 months in 50 years. Here we are using a rarer event than that normally used to define bank full flows (1–5–10 year Recurrence interval) to compensate for the use of monthly total flows (Leopold, 1994; Pickup and Warner, 1975), but which is still within the range of flows observed and modelled with a 50 year synthetic climate series. This discharge is used to indicate the cross sectional area of the bank full channel. Since at-a-station discharge is approximately proportional to Cross sectional area to a power, typically 0.6 (Leopold and Maddock, 1953), then reductions in discharge correspond to reductions in wetted cross-sectional area. Table 2 shows observed ratios between bank full discharges and discharges at which disconnected pools are present for a set of catchments in southern Europe studied in the MIRAGE project. The geometric mean of the listed flood:pool discharge ratios is 1100, and the median is 950. From these data it is proposed to use

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a discharge ratio of 1000 as an indicator of pool conditions, and this should correspond to a cross-sectional ratio of  $1000^{1/0.6}$ , i.e.  $10^5$ . An intermediate “riffle” stage has also been used for illustrative purposes, corresponding to a discharge ration of  $\sqrt{(1000)}$ , or a cross-sectional area ratio of 300. At this level continuous flow is anticipated, but without drowning out riffles and similar features.

Figures 5 and 6 show the regional aridity and the predicted frequency of pools under the current climate. In Fig. 5, aridity is indicated by the average number of months per year with precipitation less than 60% of potential evapotranspiration. There is a clear north south gradient with many Mediterranean areas having more than 4.5 dry months in the summer. In Fig. 6, the model has been applied to show the frequency of “pool” conditions throughout the year. It can be seen that the forecast pattern, although identifying the same north south differences, has a much sharper concentration towards the south.

Figure 7 shows the corresponding distribution with a uniform 2 °C rise in temperature. It can be seen that the differences are small, but generally in the direction of a small reduction in the frequency of pool conditions. The temperature rise increases potential ET, and this has some effect on natural vegetation biomass, which increase where there is adequate rainfall. There is a consequent reduction in runoff, which decreases both flood and low flows. It is therefore argued that the short term impact of a step rise in temperature may be some increase in low flow (pool) frequency but that, after a while, bankfull channel dimensions will decrease, largely counteracting the initial change.

Although there is substantial variability, there is a general relationship between the mean value of forecast pool frequency and the number of dry months per year, and this relationship is little changed by a 2 °C temperature rise. Figure 8 shows that this average behaviour is non-linear with a more rapid increase in pool frequency above about 4 dry months per year, which is consistent with the strong concentration apparent in Figs. 6 and 7 towards southern Europe and the Mediterranean.

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## 4 Conclusions

The model presented shows some potential for estimating the hydrological impact of climate in time and space, containing a number of feedback paths, mainly through vegetation, that influence the partition of precipitation between evapotranspiration and runoff. The use of the monthly duration curve provides a rather stable indicator of overall behaviour, particularly at low flows, and has been shown to allow the use of global parameter sets, in the first instance, rather than requiring individual optimisation for each site.

## Appendix A

### Model equations

Monthly infiltration excess overland flow is summed over distribution of daily rainfalls for which rainfall  $r$  is greater than the runoff threshold  $h_C$ .

$$q_{OF} = N \int_{h_C}^{\infty} (r - h_C) \cdot \frac{r^{\alpha-1}}{\beta \Gamma(\alpha)} \exp\left(-\frac{r}{\beta}\right) dr \quad (A1)$$

where  $N$  is the number of rain days,

$h_C$  is the current runoff threshold,

$r$  is the daily effective rainfall,

$\alpha$  is the Gamma parameter = (Mean daily rainfall)/(standard deviation of rain on rain days),

$\beta$  is the ratio (mean rain per rain day)/ $\alpha$ .

And  $\Gamma$  represents the Gamma function.

Monthly near-surface evapotranspiration is similarly summed for days when effective rainfall is greater than the potential ET demand.

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$$aet_S = N \left[ \int_0^e r \cdot \frac{r^{\alpha-1}}{\beta \Gamma(\alpha)} \exp\left(-\frac{r}{\beta}\right) dr + e \int_e^\infty \frac{r^{\alpha-1}}{\beta \Gamma(\alpha)} \exp\left(-\frac{r}{\beta}\right) dr \right] \quad (A2)$$

where  $e$  is the lesser of daily evaporative demand or the runoff threshold,  $h_c$ .  
The ET from the saturated zone is estimated from the relationship

$$aet_d = 1/\sqrt{(1/A^2 + 1/E^2)} \quad (A3)$$

5 where the available water,

$$A = R \exp(-D/R), \quad (A4)$$

In which  $R$  is the rooting depth and  $D$  is the saturation deficit (or zero if it is negative).  
And  $E$  is the (residual) potential ET demand.

This subsurface ET component is calculated separately for vegetated and bare frac-  
10 tions of the surface, and combined to provide the total actual ET, and the plant water uptake.

Subsurface deficit is updated by solving the TOPmodel equations:

$$\frac{dj}{dt} = \frac{j \cdot (i - j)}{m} \quad (A5)$$

$$j = j_* \exp(-D/m)$$

15 where  $j$  is the subsurface runoff rate,  $i$  is the net rate of percolation to the saturated zone = Net Rainfall–Overland flow–Actual ET and  $m$  is the TOPmodel soil depth parameter. Equations (3)–(5) are normally solved by subdividing the month into five, progressively updating each component to its monthly total. Cover is modified monthly,

always converging towards the value  $\sqrt{\frac{\text{Plant water uptake}}{\text{Potential ET}}}$ , but with 50% inertia, and Root cover, which is taken to be more complete than surface cover, is estimated as  $\sqrt{(\text{Cover})}$ .

20 Equilibrium Plant and Soil organic matter biomass are estimated annually, from the equations:

Gross primary productivity = respiration + Leaf Fall

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Leaf Fall = SOM decomposition  
where  $GPP \sim \text{Plant Water Uptake}$ ,

$$\text{Respiration} \sim \exp\left(\frac{T - 10}{8}\right) \quad (\text{A6})$$

In which  $T$  is temperature in  $^{\circ}\text{C}$ ,

$$\text{Leaf fall} \sim \frac{V}{\log(V + 1.4)} \quad (\text{A7})$$

In which Vegetation biomass,  $V$ , is in  $\text{kg m}^{-2}$ , and

$$\text{Annual decomposition} = \{\exp[0.05 \exp(0.12 T)] - 1\} H \quad (\text{A8})$$

In which  $H$  is the SOM biomass.

Finally the runoff threshold  $h_c$ , is estimated as

$$h_c = 10 + 40 C + 50[1 - \exp(-H/10)] C, \quad (\text{A9})$$

where  $C$  is the fractional crown cover.

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**Table 1.** Summary characteristics of catchments studied.

Name	Latitude (° N)	Longitude (° E)	Precipitation (mm)	Potential evapo- transpiration
Hozgarganta, Spain	36.4	−5.4	699	1053
Cal Rodo, Spain	42.2	1.9	989	776
Algali, Portugal	39.1	−7.2	640	1170
Kendal, UK	54.4	−2.7	2064	577
Celone San Vincenzo, Italy	41.3	15.5	465	991



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**Table 2.** Ratios of flood to pool discharges reported for some MIRAGE catchments.

Catchment	Flood: Pool discharge ratio
Salsola – Casanova, Italy	400
Salsola – Ponte Foggia, Italy	400
Celone – S. Vincenzo, Italy	1500
Celone – Ponte Foggia, S. Severo, Italy	2000
Vrontanno, Greece	20000
Tordera, Spain	200

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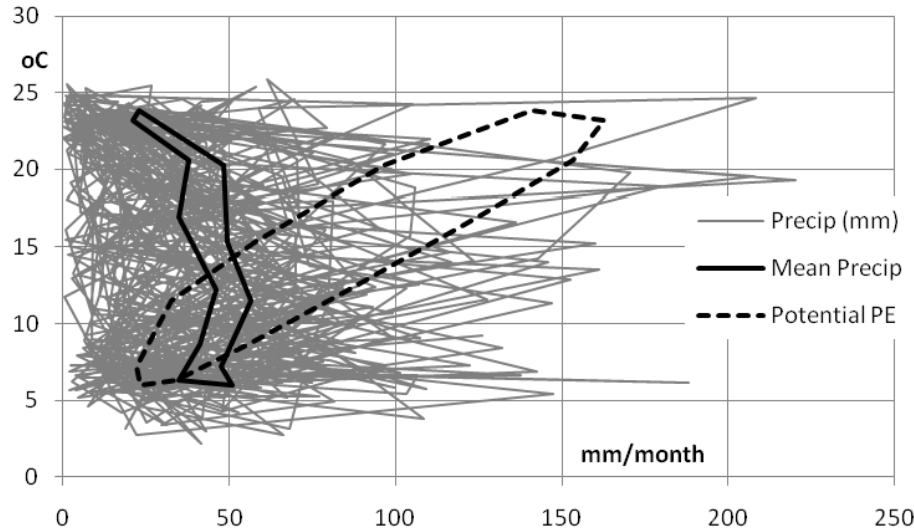
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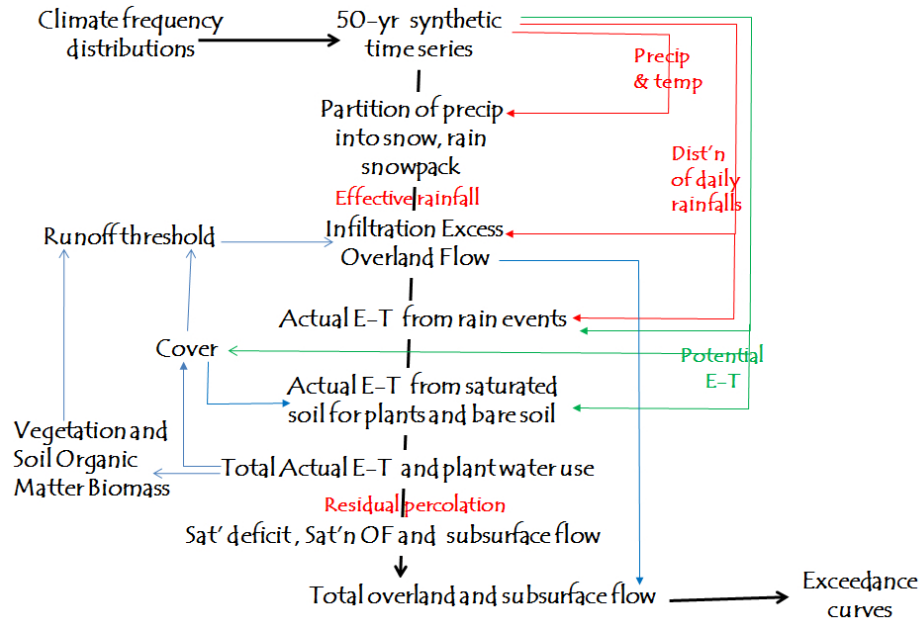
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**Fig. 1.** Example of 50-year synthetic climate realisation for the Celone catchment, near Foggia.

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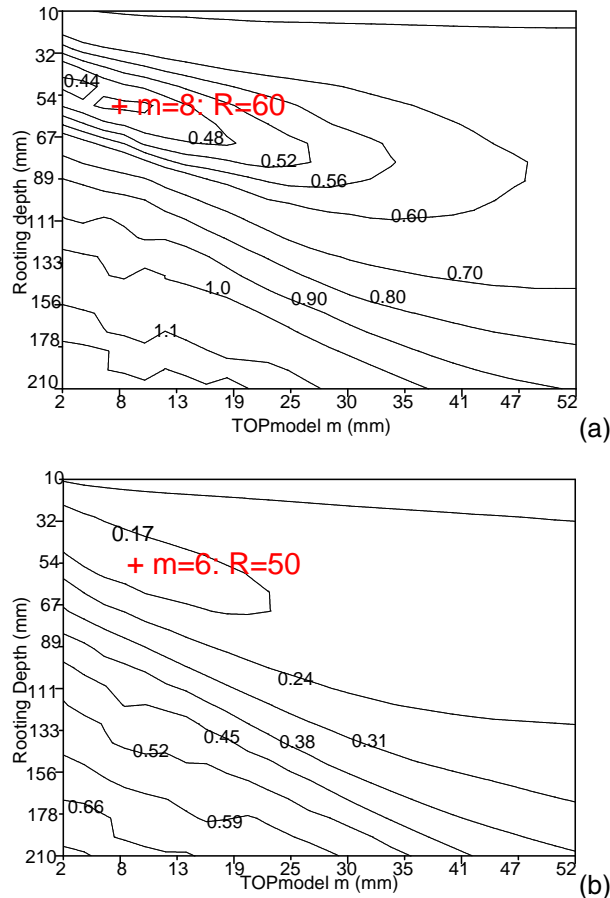


**Fig. 2.** Schematic for hydrological model.

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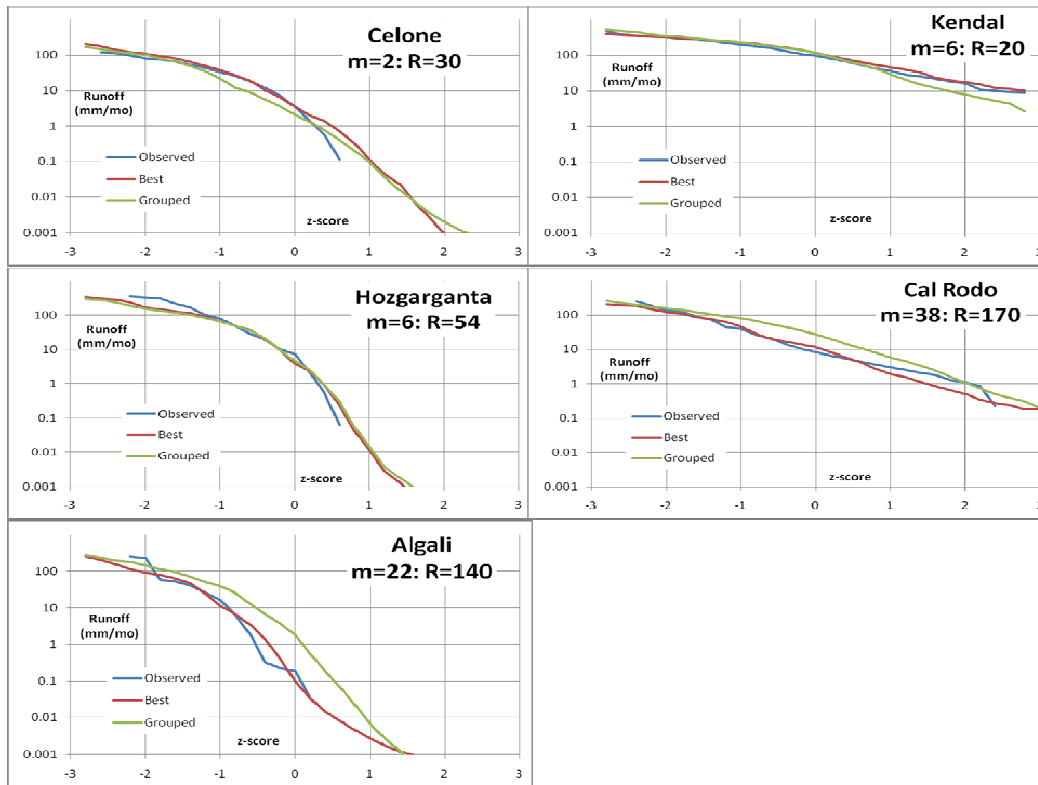


**Fig. 3.** (a) RMS mean difference between observed and simulated exceedance curves for R. Hozgarganta, S. Spain.  $\Delta$  shows catchment optimum. (b) Average normalized departure averaged across five test catchments from their individual minimum RMS error.  $\Delta$  shows global optimum.

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**Fig. 4.** Exceedance curves for the five test catchments. Each graph shows the observed data, the individual best fit model and the global best fit model.

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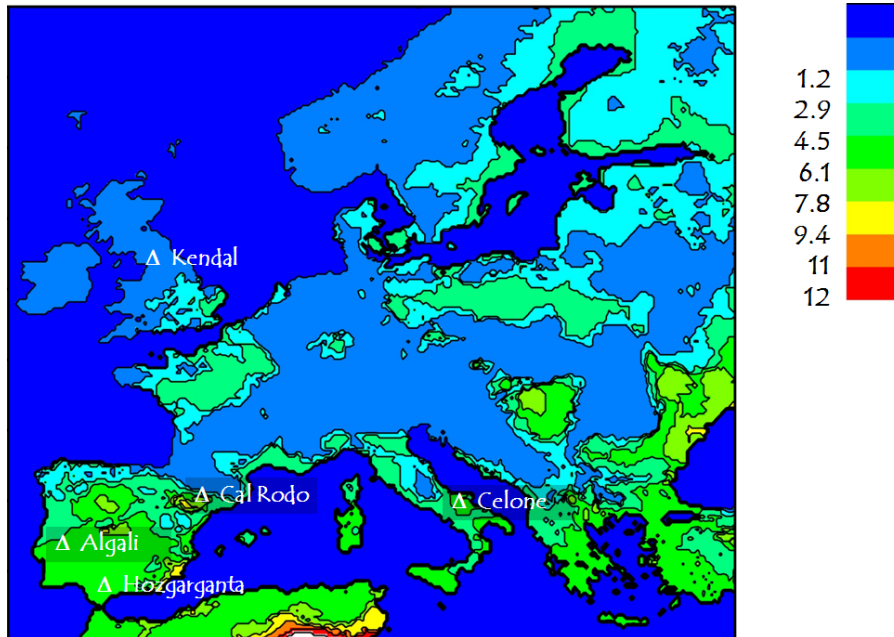
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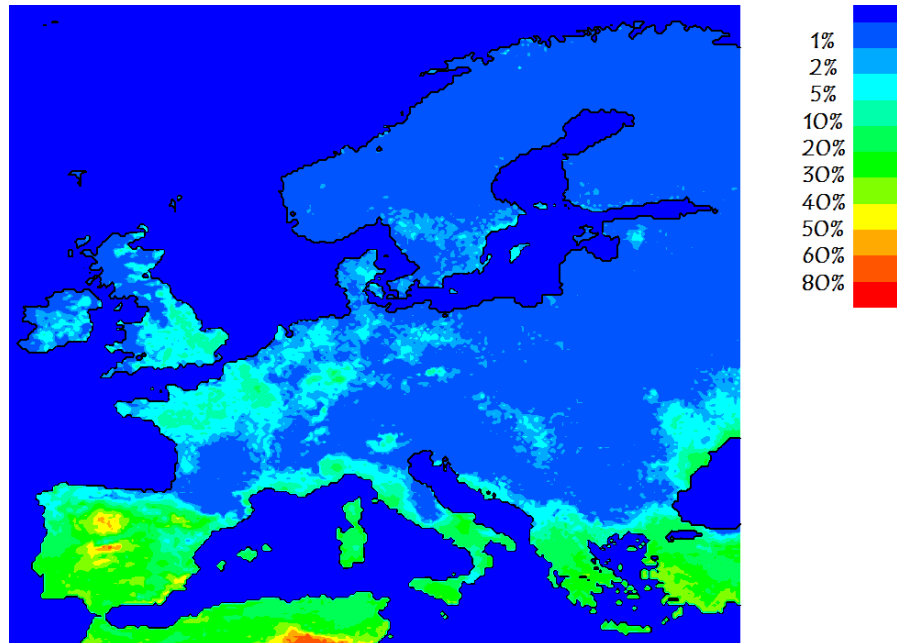


**Fig. 5.** Average number of months with Precipitation  $< 0.6$  Potential ET. Figure also shows location of test catchments.

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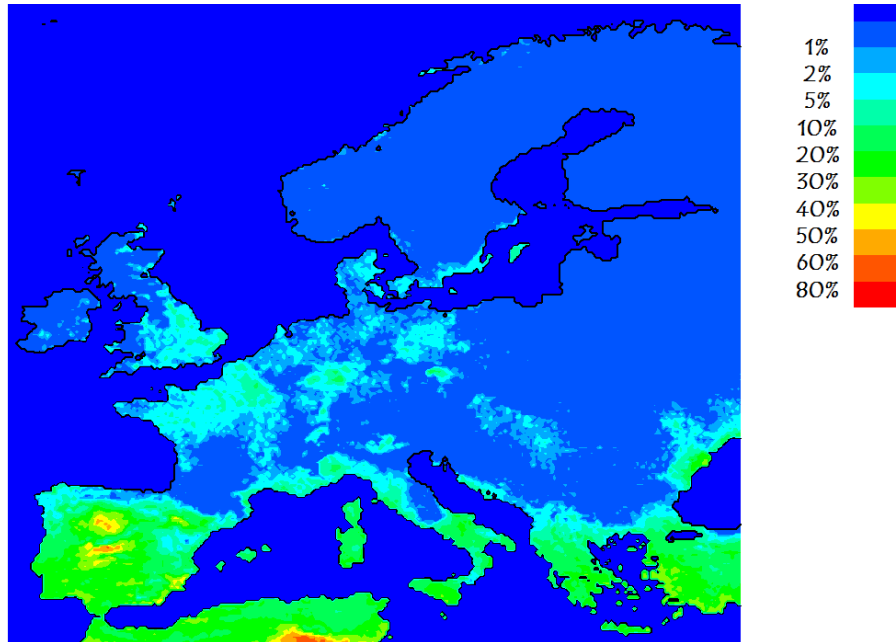
**Fig. 6.** Percentage of time with low flow “pool” conditions, derived from monthly duration curves for present climate.

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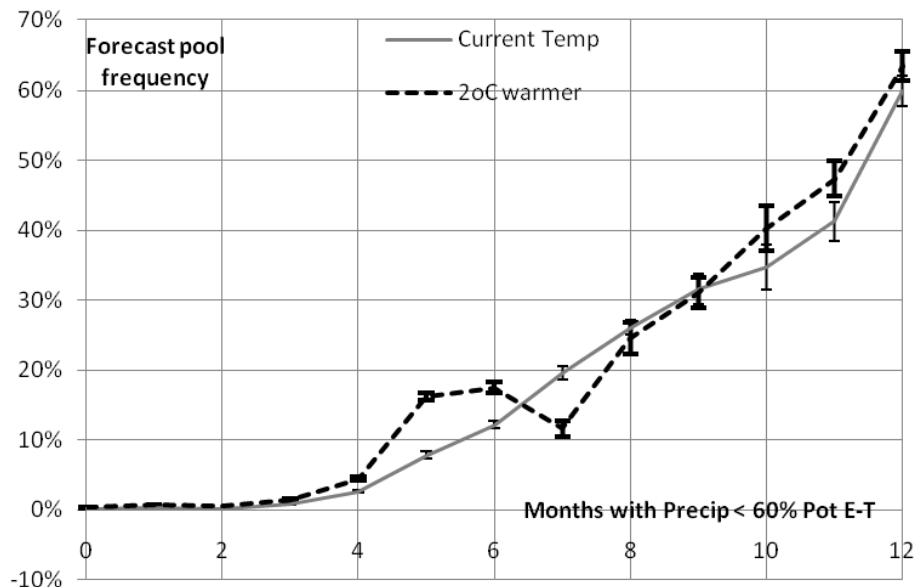
**Fig. 7.** Percentage of time with low flow “pool” conditions, derived from monthly duration curves with 2 °C warming.

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**Characterizing temporary hydrological regimes at a European scale**

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**Fig. 8.** Empirical relationship between forecast pool frequency and the average number of dry months (Precip < 0.6 Pot ET) for current climate and with a 2°C temperature rise.

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