

1
2 **ALTERNATIVE MODEL TO DETERMINE THE CHARACTERISTIC**
3 **STRENGTH VALUE OF WOOD IN THE COMPRESSION PARALLEL TO**
4 **THE GRAIN**

5 André Luis Christoforo¹, Vinicius Borges de Moura Aquino^{2*}, José Silvio Govone³,
6 Alfredo Manuel Pereira Geraldes Dias⁴, Tulio Hallak Panzera⁵, Francisco Antonio
7 Rocco Lahr⁶

8 ¹ Department of Civil Engineering, Federal University of São Carlos, São Carlos, São Paulo, Brazil.

9 ² Department of Civil Engineering, Federal University of South and Southeastern Pará, Santana do
10 Araguaia, Pará, Brazil.

11 ³ Department of Statistics, Applied Mathematics and Computation, Center of Environmental Studies, State
12 University of São Paulo, Rio Claro, São Paulo, Brazil.

13 ⁴ Department of Civil Engineering, University of Coimbra, Coimbra, Portugal.

14 ⁵ Department of Mechanical Engineering, Federal University of São João del-Rey, São João del-Rey,
15 Minas Gerais, Brazil.

16 ⁶ Department of Structures Engineering, University of São Paulo, São Carlos, São Paulo, Brazil.

17 *Corresponding author: aquino.vini@hotmail.com

18 **Received:** January 21, 2019

19 **Accepted:** February 25, 2020

20 **Posted online:** February 26, 2020

21 **ABSTRACT**

22 Wood strength values are calculated based on the characteristic value, which
23 corresponds to the 5 % percentile of a given probability distribution model. For a few
24 number of samples (12 samples), the Brazilian standard ABNT NBR (7190)
25 establishes an estimator of the characteristic compressive strength parallel to grain of
26 the wood, which may provide a different result when compared with the characteristic
27 value coming from a suitable probability distribution model. Considering the strength
28 results in the parallel compression to the grain of 45 wood species of the hardwood
29 group, Normal, LogNormal, Weibull and Exponential probability distribution models
30 were used for each specie with the purpose of determining the one with the highest
31 adhesion. Calculated the characteristic values by the best probability model
32 distribution, an analysis of variance (ANOVA) was performed in the estimation of the
33 characteristic value of compressive strength, making it possible to identify the most
34 significant terms of the models as well as the quality of the adjustment obtained on
35 such models. The proposed regression model (R^2 adj= 96,56 %) proved to be
36 equivalent to the empirical model of the Brazilian standard. The model proposed here
37 only depends on the mean and the lowest value obtained from the compressive
38 strength in the parallel direction to the grain.

39 **Keywords:** Characteristic value, mechanical properties, probability distribution,
40 *Tabebuia* spp., wood.

41

42

43

INTRODUCTION

44

45 The wood, a natural and renewable source material, presents a good relation
46 between mechanical strength and density (Arruda *et al.* 2015; Baar *et al.* 2015;
47 Cavalleiro *et al.* 2016), which makes it suitable for use in construction (Andrade Jr.
48 *et al.* 2014; Chen and Guo 2017; Lahr *et al.* 2017).

49 Brazil is a country with enormous potential for timber applications, since the
50 availability of wood species from the Amazon Forest is the order of 11194 wood
51 species, cataloged between the years 1707 and 2015 (Steege *et al.* 2016) these
52 conditions motivated the development of new researches with the purpose of
53 characterizing new species to replace those commonly used in civil construction
54 (Ferro *et al.* 2015; Freitas *et al.* 2016; Almeida *et al.* 2016; Christoforo *et al.* 2017).

55 In Brazil, timber structures projects are regulated by the Brazilian Standard ABNT
56 NBR 7190 (1997) "Wood Structures Project", and the structures are designed
57 assuming small displacements and therefore the principle of geometric linearity and
58 also to withstand satisfactorily and safely the action of the acting forces.

59 For reasons of structural design safety, the values of strength to the mechanical
60 stresses of the wood are obtained based on the characteristic value (and not on the
61 mean value), which corresponds to the 5 % percentile of the respective probability
62 distribution.

63 According to the probabilistic method of the Brazilian standard ABNT NBR 7190
64 (1997), a normal distribution is assumed of the strength values. Such hypothesis is
65 based on the consideration of large number of samples (30 or more test specimens)

66 together with a value limit of 18 % of the coefficient of variation. Given the average
67 value of the strength (\bar{f}) and its standard deviation (sd), the characteristic value (f_{wk})
68 of the property is determined using Equation 1.

$$f_{wk} = \bar{f} - 1,645 \cdot sd \quad (1)$$

69 For a small number (n) of samples ($n < 30$), the Brazilian standard establishes
70 the use of Equation 2 to estimate the characteristic strength value.

$$f_{wk} = \left(2 \cdot \frac{f_1 + f_2 + f_2 + \dots + f_{(n/2)-1}}{(n/2) - 1} - f_{n/2} \right) \cdot 1,10 \quad (2)$$

71 From Equation 2, n is the number of samples used in the mechanical tests and f_i
72 consists of the strength values of the sample, and the results must be arranged in
73 ascending order ($f_1 \leq f_2 \leq f_3 \dots \leq f_n$), neglecting the largest value of the strength if the
74 number of specimens is odd and not assumed to be less than f_i and not less than 70 %
75 of the average value of the strength. It should be noted that the Brazilian standard
76 ABNT NBR 7190 (1997) establishes 12 specimens for determining the physical and
77 mechanical properties of the wood, and that, therefore, the characteristic value is
78 calculated based on twelve strength values.

79 The adoption of Equation 2 for the estimation of the characteristic value can
80 result in values different from the characteristic value associated to a certain
81 probability density function, and it should be noted that there are several existing
82 probability density functions (Pinto *et al.* 2004), and found the one of best adherence
83 to the set of strength values, it can obtain the characteristic value with greater
84 reliability. Being higher than the characteristic value estimated by the expression of
85 the standard in relation to that obtained by a given model of probability distribution,
86 this implies in the possibility of overestimating the strength of the wood, condition

87 usually unfavorable to the project, and of underestimating it otherwise, which
88 motivates the development of researches in this area.

89 This research aimed to identify the characteristic value ($f_{c0,k}$) per wood specie
90 associated with the best probability distribution model and relate, using a multilinear
91 regression model, with the mean values, coefficients of variation and with the lowest
92 and highest value of the property per species, using four probability distribution
93 models (Normal, LogNormal, Weibull and Exponential) and 45 species of wood from
94 the group of hardwood. By the adjusted coefficient of determination (R^2) obtained
95 from the regression model, it will be possible to evaluate the precision in the
96 estimation of the characteristic value of $f_{c0,k}$, a precision that is unknown with the use
97 of Equation 2 established by the Brazilian standard.

98 MATERIAL AND METHODS

99 The values of strength in compression parallel to the grain (f_{c0}) of the wood were
100 obtained following the assumptions and the methods of testing and calculation of the
101 Brazilian standard ABNT NBR 7190 (1997) on its Annex B. Twelve specimens were
102 manufactured and tested for each wood species, from which were obtained the mean
103 values, the highest and the lowest values, the coefficient of variation, the standard
104 deviation and also the characteristic values, the latter determined by Equation 2
105 (Brazilian standard) and the probability distribution models.

106 The 45 species of wood used in the development of this project were: Angelim
107 Amargoso (*Vatairea fusca*); Angelim Araroba (*Vataireopsis araroba*); Angelim
108 Ferro (*Hymenolobium* sp.); Angelim Pedra (*Hymenolobium petraeum*); Angelim Saia

109 (*Dinizia excelsa*); Angelim Vermelho (*Dinizia excelsa* Ducke); Angico Branco
110 (*Anadenanthera colubrina*); Angico Preto (*Piptadenia macrocarpa*); Branquilha
111 (*Terminalia* sp.); Cafearana (*Andira* sp.); Cambará Rosa (*Erisma* sp.); Canafístula
112 (*Cássia ferruginea* Schrad); Casca Grossa (*Ocotea odorifera*); Castanheira
113 (*Bertholletia excelsa*); Castelo (*Gossypiospermum praecox*); Catanudo (*Calophyllum*
114 sp.); Cedro Amargo (*Cedrela odorata*); Cedro Doce (*Cedrela* sp.); Cedroarana
115 (*Cedrelinga cateniformis* Ducke); Champanhe (*Dipteryx odorata* (Aublet.) Willd);
116 Copaíba (*Copaifera* sp.); Cutiúba (*Copaifera* sp.); Garapa (*Apuleia leiocarpa*);
117 Goiabão (*Planchonella pachycarpa*); Guaiçara (*Luetzelburgia* sp.); Guajará
118 (*Micropholis venulosai*); Guarucaia (*Peltophorum vogelianum*); Itaúba (*Mezilaurus*
119 *itauba*); Jatobá (*Hymenea* sp.); Louro Preto (*Ocotea* sp.); Louro Verde (*Laurus*
120 *nobilis*); Maçaranduba (*Manilkara* sp.); Mandioqueira (*Qualea* sp.); Oiticica Amarela
121 (*Clarisia racemosa*); Oiuchu (*Rapanea* sp.); Parinari (*Parinari rodolph* Huber); Pau-
122 óleo (*Copaifera* sp.); Piolho (*Tapirira guianensis*); Quarubarana (*Erisma uncinatum*);
123 Quina Rosa (*Chinchona* sp.); Rabo de Arraia (*Vochysia* sp.); Sucupira (*Diploptropis*
124 sp.); Tachi (*Tachinalia* sp.); Tatajuba (*Bagassa guianensis*) and Umirana (*Qualea*
125 *retusa*). It should be noted that they were tested with moisture content close to 12 %,
126 which consists of equilibrium moisture content according to the Brazilian standard.

127 The probability distributions considered in this research to determine the
128 characteristic values were Normal, LogNormal, Weibull and Exponential, whose
129 probability density functions (f) on the random variable X are expressed in Equations
130 3, 4, 5 and 6, respectively.

$$f(x) = \frac{1}{\sqrt{2 \cdot \pi \cdot \sigma^2}} \cdot e^{-\frac{1}{2} \left(\frac{x-\mu}{\sigma}\right)^2}, x \in (-\infty, \infty) \quad (3)$$

$$f(x) = \begin{cases} \frac{1}{x \cdot \sigma \cdot \sqrt{2 \cdot \pi}} \cdot e^{-\frac{1}{2} \frac{(\log(x)-\mu)^2}{\sigma^2}}, & \text{if } x > 0 \\ 0, & \text{otherwise} \end{cases} \quad (4)$$

$$f(x) = \begin{cases} \frac{\delta}{\alpha^\delta} \cdot x^{\delta-1} \cdot e^{-\left(\frac{x}{\alpha}\right)^\delta}, & \text{if } x \geq 0 \\ 0 & \text{if } x < 0 \end{cases} \quad (5)$$

$$f(x) = \begin{cases} \lambda \cdot e^{-\lambda \cdot x}, & x \geq 0 \\ 0 & \text{if } x < 0 \end{cases} \quad (6)$$

131

132 From Equation 3, σ and μ consist of the standard deviation and the population mean,
 133 respectively. In Equation 4, σ is the standard deviation and μ is the population mean of
 134 the logarithm. From the Weibull probability density function (Equation 5), δ and α are
 135 the form and scale parameters, respectively, and λ is the Exponential function
 136 distribution rate parameter (Equation 6).

137 The adhesion tests (at the 95 % level of reliability) used to verify the best
 138 distribution model were obtained by the Least Squares Method, with the aid of
 139 Minitab® software version 18.

140 The characteristic values of each wood species ($f_{c0,k}$) for distribution models
 141 suitable probability were obtained, these results were related to the mean value (x_m),
 142 coefficient of variation (CV), the smallest (Min) and highest (Max) value of f_{c0} by
 143 means of a multilinear regression model (Equation 7) evaluated based on analysis of
 144 variance (ANOVA), at the level of 5 % of significance, whose quality of fit was
 145 evaluated by means of the adjusted coefficient of determination (R^2_{adj}).

$$f_{c0,k}(MPa) = \beta_0 + \beta_1 \cdot x_m + \beta_2 \cdot CV + \beta_3 \cdot Min + \beta_4 \cdot Max + \varepsilon \quad (7)$$

146 From Equation 7, β_i consist of the coefficients adjusted by the least square method

147 and ϵ is the random error. By the ANOVA formulation of the regression model, P-
148 value (Probability P) equal to or greater than the significance level (5 %) implies in
149 the model or its coefficients are not representative (null hypothesis H_0 - factor
150 variations do not explain the variations in dependent variable), and significant
151 otherwise (alternative hypothesis H_1 - P-value $<0,05$).

152 Because twelve specimens were used to determine the characteristic strength value
153 by both Equation 2 and the probability distribution models, the Equation 7 should
154 strictly consider a maximum of 12 values.

155 The Anderson-Darling test (Weerahandi 1995) was used to evaluate the normality
156 in the ANOVA residue distribution of the regression models, and the graph of
157 residuals versus fitted values was used to assess the homogeneity of the residues,
158 making possible validate the results of the analysis of variance.

159 The multilinear regression model was compared with the empirical model
160 (Equation 2) proposed by the Brazilian standard, allowing to evaluate the precision of
161 the model proposed in this standard.

162 **RESULTS AND DISCUSSION**

163 The confidence interval (CI) of the mean (at the 5 % level of significance) for $f_{c0,k}$
164 calculated by the Brazilian standard equation resulted in IC = (49,74; 60,28 MPa),
165 being 31,90% the coefficient of variation obtained. The values of the compressive
166 strength parallel to the grain determined by the standard ranged from 25,52 MPa to
167 96,58 MPa, thus evidencing the coverage of the results due to all strength classes for
168 the hardwood group were accounted for.

169 The confidence interval (CI) of the mean (at the 5 % level of significance) for $f_{c0,k}$
170 calculated by the probability distribution models resulted in CI = (45,88; 55,56 MPa),
171 31,77 % coefficient of variation obtained. The lowest and the highest value of the
172 property were equal to 19,32 MPa and 85,50 MPa, respectively.

173 From 45 wood species evaluated by the probability distribution models in $f_{c0,k}$, 40
174 % (18/45) of the species were better represented by the LogNormal model, 17,78 %
175 (8/45) were better adjusted by the Normal distribution model and 42,22 % (19/45) by
176 the Weibull model, and it should be noted that the Exponential model did not provide
177 a significant adjustment for $f_{c0,k}$ in any of the evaluated species. Even though the
178 Normal probability distribution model was not the one with the best adhesion, yet all
179 the wood species presented Normal distribution, a result that favors the use of the
180 empirical equation of the Brazilian standard.

181 The regression model for estimating the characteristic value of resistance in
182 compression parallel to the grain is expressed by Equation 8, and the results of
183 ANOVA and their validation (normality, independence and homogeneity of
184 variances) are presented in Table 1 and in Figure 1, respectively.

$$f_{c0,k}(\text{MPa}) = -1,21 + 0,49 \cdot x_m - 0,04 \cdot Cv + 0,67 \cdot \text{Min} - 0,16 \cdot \text{Max}$$
$$[R^2_{\text{adj}} = 97,08 \%]$$

(8)

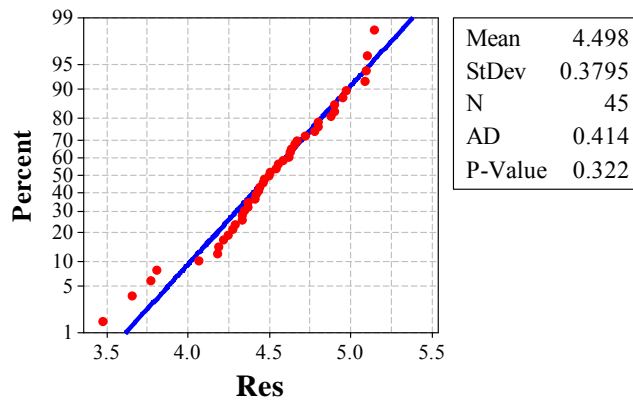
185

Table 1: Results of the ANOVA of the regression model.

Source	GL	SQ (Aj.)	QM (Aj.)	F-Value	P-Value
Regression	4	11123,1	2780,78	366,79	0,000
x_m	1	62,0	61,96	8,17	0,007
Cv	1	0,4	0,43	0,06	0,813
Mín	1	1627,5	1627,49	214,67	0,000
Máx	1	8,4	8,41	1,11	0,298
Error	40	303,3	7,58		
Fault of adjust	39	303,1	7,77	46,20	0,116
Pure error	1	0,2	0,17	*	*
Total	44	11426,4			

* *GL* – freedom degrees, *SQ(Aj)* – sum of squares; *QM(Aj)* – mean squares

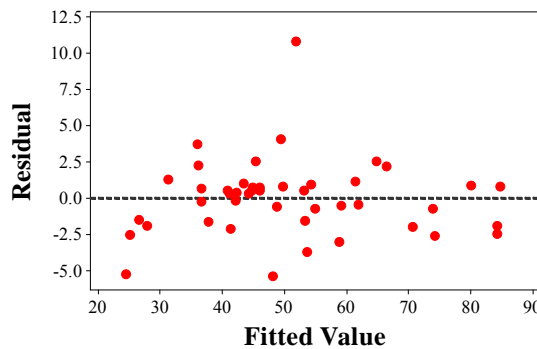
186



187

188

Figure 1: Anderson-Darling normality test of residues for ANOVA validation.



189

190

191

192

Figure 2: Residue graph versus adjusted values for ANOVA validation.

Figure 1 shows normality in the distribution of residues ($P\text{-value} > 0,05$), and

193 Figure 2 shows that residues (randomly distributed) are grouped around 0 (evidence
194 of homogeneity of variances), thus validating the model of ANOVA. It should be
195 noted that the three points located at -5 and at +10 on the axis of the ordinates (Res)
196 in the graph of Figure 2 are considered as outliers, and that ended up impacting
197 negatively the quality of the adjustment, but they were preserved in order to conserve
198 the variability in the wood physical and mechanical properties (Christoforo *et al.*
199 2017).

200 Table 1 shows that the regression model obtained was significant (P-value < 0,05),
201 with a good accuracy of the adjustment by the adjusted coefficient of determination
202 (97,08 %). From the coefficients of the model, only the mean (x_m) and the lower value
203 of the compressive strength parallel to the grain (f_{c0}) significantly affected the
204 characteristic values ($f_{c0,k}$) of compressive strength parallel to the grain, implying that
205 the coefficient of variation (Cv) and the highest value (Max) of f_{c0} have little effect
206 on the estimate of $f_{c0,k}$.

207 The exclusion of the Cv and Max factors from Equation 8 resulted in the regression
208 model expressed by Equation 9, whose adjusted coefficient of determination was
209 96,56 %, only 0,52 % difference with the complete model, which reinforces the small
210 influence of CV and Max factors.

$$f_{c0,k}(\text{MPa}) = -4,24 + 0,35 \cdot x_m + 0,65 \cdot \text{Min} \quad [R^2_{\text{adj}} = 96,56 \%] \quad (9)$$

211 Table 2 shows the ANOVA results of the regression model of Equation 9 and in
212 Figure 2 the validation tests of the analysis of variance.

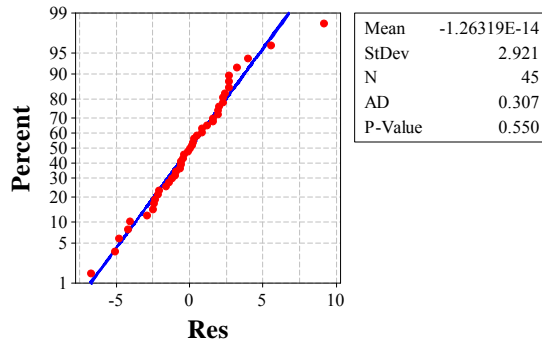
213

214

Table 2: Results of the ANOVA of the regression model of Equation 9.

Source	GL	SQ (Aj.)	QM (Aj.)	F-Value	P-Value
Regression	2	11050,9	5525,47	618,15	0,000
x_m	1	646,3	646,30	72,30	0,000
Min	1	1665,4	1665,40	186,31	0,000
Error	42	375,4	8,94		
Fault of adjust	41	375,3	9,15	54,42	0,107
Pure Error	1	0,2	0,17	*	*
Total	44	11426,4			

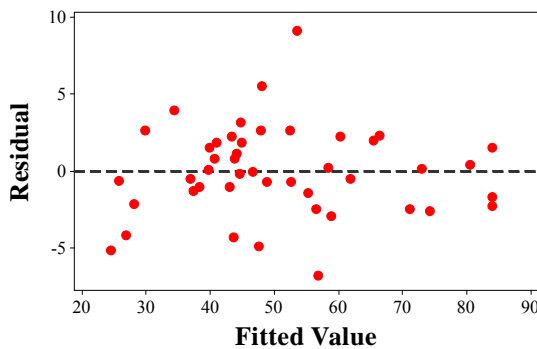
* GL – freedom degrees, SQ(Aj) – sum of squares; QM(Aj) – mean squares.



215

216

Figure 3: Anderson-Darling normality test of residues for ANOVA validation.



217

218

219

Figure 4: Residue graph versus adjusted values (b) for ANOVA validation.

220

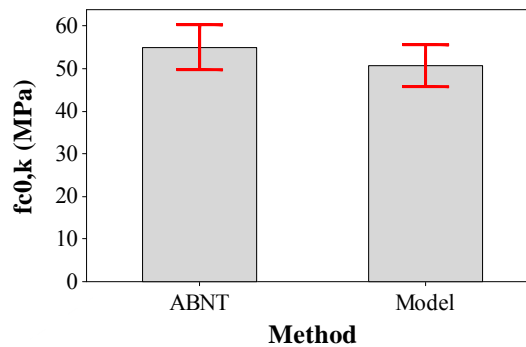
221

The results of Figure 3 and 4 show the validity of the ANOVA model, and from Table 2, it is evident that the two factors x_m and Min are significant. Again, it is

222 verified that the lack of adjustment is not significant and that the obtained model is
 223 significant.

224 The analysis of variance (at 5 % level of significance) was also used as a way of
 225 comparing the results of the model proposed (Equation 9) with the results of the use
 226 of Equation 2 established by the Brazilian standard to obtain $f_{c0,k}$. Figure 5 shows the
 227 mean values and confidence intervals of the mean (at the 95 % confidence level) of
 228 the values of $f_{c0,k}$ obtained by both calculation methods, and Table 3 and Figura 6
 229 shows the ANOVA results and validation, respectively.

230



231

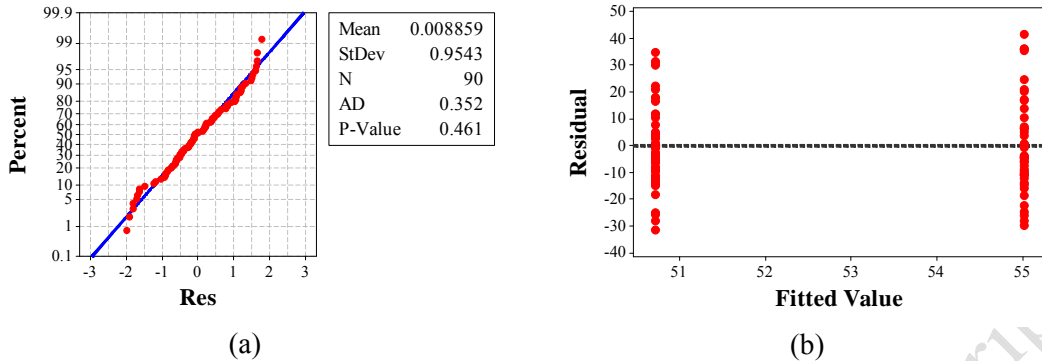
232 **Figure 5:** Mean values and confidence intervals for $f_{c0,k}$ obtained by both calculation
 233 methods.

234 **Table 3:** Result of ANOVA referring to the comparison of the models to obtain $f_{c0,k}$.

Source	GL	SQ (Aj.)	QM (Aj.)	Valor F	Valor-P
Method	1	413,9	413,9	1,48	0,227
Error	88	24602,1	279,6		
Total	89	25016,0			

* GL – freedom degrees, SQ(Aj) – sum of squares; QM(Aj) – mean squares.

235



236 **Figure 6:** Validation of ANOVA between the models - Anderson Darling normality
237 test (a) and graph of residuals versus adjusted values (b).

238

239 Based on the results of Table 3, the calculation model of the Brazilian standard
240 and the regression model proposed in this research for estimating the values of $f_{c0,k}$
241 are statistically equivalent, even though the mean of the values of $f_{c0,k}$ obtained by the
242 regression model smaller when compared to the average of the values of $f_{c0,k}$, coming
243 from the standard model (Figure 5).

244 From Equation 9, it should be pointed out that for a given species of wood, the
245 average value (x_m) of f_{c0} and the lowest value of this property of the respective set of
246 sample results, the characteristic value ($f_{c0,k}$) can be easily determined, unlike the way
247 of obtaining this property using the equation of the Brazilian standard (Equation 2),
248 which initially requires the ordering and exclusion of part of the set of experimental
249 results for later realization of the accounts.

250 To verify the accuracy of Equation 9, a new species of wood (Ipê Amarelo -
251 *Tabebuia* spp., *Bignoniaceae*) was characterized in compression parallel to the grain.
252 The average f_{c0} value for twelve specimens was equal to 81,73 MPa, and the lowest
253 sample value obtained was 71,90 MPa. By Equation 2 of the Brazilian standard, the

254 characteristic strength value resulted in 78,63 MPa. According to the probability
255 distribution models considered, the one with the best adherence was Normal, with a
256 characteristic strength value equal to 69,75 MPa. Using Equation 9, the characteristic
257 strength value of the Ipê Amarelo wood was equal to 71,10 MPa. Considering the
258 probability distribution model as a reference (of greater precision), the relative error
259 made with the use of Equation 9 was 1,94 %, which shows the excellent precision of
260 the proposed alternative model.

261 CONCLUSIONS

262 The results of the regression model proposed here, with excellent accuracy (R^2 aj
263 greater than 96 %) and dependent only on the mean and minimum value of the
264 compressive strength parallel to the grain of the set of results, were statistically
265 equivalent to the model proposed by the Brazilian standard, evidencing the good
266 precision contained in the calculation model of this standard. However, the use of the
267 regression model proposed in this research is justified for the ease in calculating the
268 characteristic strength value and also for providing an accuracy, suitable to be
269 incorporated in future versions of the Brazilian standard.

270 REFERENCES

- 271 **Almeida, T.H.; Almeida, D.H.; Christoforo, A.L.; Chahud, E.; Branco,**
272 **L.A.M.N.; Lahr, F.A.R. 2016.** Density as estimator of strength in compression
273 parallel to the grain in wood. *Int J Mat Eng* 6(3): 67-71.
274 <https://doi.org/10.5923/j.ijme.20160603.01>
275 **Andrade JR. J.R.; Almeida, D.H.; Almeida, T.H.; Christoforo, A.L.; Stamato,**
276 **G.C.; Lahr, F.A.R. 2014.** Avaliação das estruturas de cobertura em madeira de um
277 galpão de estoques de produtos químicos. *Amb Constr* 14(3): 75-85.

- 278 <https://doi.org/10.1590/S1678-86212014000300006>
- 279 **Arruda, L.M.; Del Menezzi, C.H.S.; Andrade, A. 2015.** Utilization of a
280 thermomechanical process to enhance properties of a hardwood used for flooring.
281 *Braz J Wood Sci* 6(3): 223-231. <http://dx.doi.org/10.15210/cmadv6i3.7144>
- 282 **Baar, J; Tippner, J.; Rademacher, P. 2015.** Prediction of mechanical properties –
283 modulus of rupture and modulus of elasticity of five tropical species by
284 nondestructive methods. *Maderas-Cienc Tecnol* 17(2): 239-252.
285 <http://dx.doi.org/10.4067/S0718-221X2015005000023>
- 286 **Cavalheiro, R.S.; Almeida, D.H.; Almeida, T.H.; Christoforo, A.L.; Lahr, F.A.R.**
287 **2016.** Density as estimator of shrinkage for some Brazilian Wood species. *Int J Mater*
288 *Eng* 6(3):107-112. <https://doi.org/107-112.10.5923/j.ijme.20160603.08>
- 289 **Chen, Y.; Guo, W.; 2017.** Nondestructive evaluation and reliability analysis for
290 determining the mechanical properties of old wood of ancient timber structure.
291 *BioResources* 12(2): 2310-2325.
292 [https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_12_2_2310_Chen_N](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_12_2_2310_Chen_Nondestructive_Evaluation_Reliability_Analysis)
293 [ondestructive_Evaluation_Reliability_Analysis](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_12_2_2310_Chen_Nondestructive_Evaluation_Reliability_Analysis)
- 294 **Christoforo, A.L.; Aftimus, B.H.C.; Panzera, T.H.; Machado, G.O.; Lahr,**
295 **F.A.R. 2017.** Physico-mechanical characterization of the *Anadenanthera columbrina*
296 Wood specie. *Eng Agric* 37(2): 376-384. [https://doi.org/10.1590/1809-4430-](https://doi.org/10.1590/1809-4430-eng.agric.v37n2p376-384/2017)
297 [eng.agric.v37n2p376-384/2017](https://doi.org/10.1590/1809-4430-eng.agric.v37n2p376-384/2017)
- 298 **Ferro, F.S.; Icimoto, F.H.; Almeida, D.H.; Christoforo, A.L.; Lahr, F.A.R. 2015.**
299 Influência da posição dos instrumentos de medida na determinação do módulo de
300 elasticidade da madeira na compressão paralela às fibras (E_{c0}). *Rev Árvore* 39(4): 743-
301 749. <https://doi.org/10.1590/0100-67622015000400017>
- 302 **Freitas, A.S.; Gonçalez, J.C.; Del Menezzi, C.H. 2016.** Tratamento termomecânico
303 e seus efeitos nas propriedades da *Simarouba amara* (Aubl.). *FLORAM* 23(4): 565-
304 572. <https://doi.org/10.1590/2179-8087.144115>
- 305 **Lahr, F.A.R.; Christoforo, A.L.; Varanda, L.D.; Araujo, V.A.; Chahud, E.;**
306 **Branco, L.A.M.N.; 2017.** Shear and longitudinal modulus of elasticity in wood.
307 relations based on static bending tests. *Acta Sci-Techol* 39: 433-437.

- 308 <https://doi.org/10.4025/actascitechnol.v39i4.30512>
- 309 **Minitab. 2017.** Minitab software version 18. MINITAB, State College, PA, United
310 States of America. <https://www.minitab.com/>
- 311 **Pinto, E.M.; Espinosa, M.M.; Calil JR, C. 2004.** Métodos para Determinação do
312 Valor Característico da Resistência à Compressão Paralela às Fibras da Madeira.
313 *Madeira: Arquitetura e Engenharia* 5(14): 1-6.
314 <http://madeira.set.eesc.usp.br/article/view/264>
- 315 **Steege, H.; Vaessen, R.W.; Lopez, D.C.; Sabatier, D.; Antonelli, A.; Oliveira, S.**
316 **M.; Pitman, N.C.A.; Jorgensen, P.M.; Salomão, R.P. 2016.** The discovery of the
317 Amazonian tree flora with an update checklist of all known tree taxa. *Sci Rep*
318 6(29549): 1-15. <https://doi.org/10.1038/srep29549>
- 319 **Weerahandi, S. 1995.** ANOVA under Unequal Error Variances. *Biometrics* 51(2):
320 589-599. <https://doi.org/10.2307/2532947>