

## Simulation Study on Material Property of Cantilever Piezoelectric Vibration Generator

<sup>1,\*</sup> Yan Zhen, <sup>1</sup> Liu Junfeng, <sup>2</sup> He Qing

<sup>1</sup> Mechanic & Electronic College, Agricultural University of Hebei, Hebei Baoding 071001, China

<sup>2</sup> School of Energy Power and Mechanical Engineering, North China Electric Power University, Beijing 102206, China

\* Tel.: 8603127526450

\* E-mail: qceftgh@126.com

*Received: 6 April 2014 /Accepted: 30 May 2014 /Published: 3 June 2014*

---

**Abstract:** For increasing generating capacity of cantilever piezoelectric vibration generator with limited volume, relation between output voltage, inherent frequency and material parameter of unimorph, bimorph in series type and bimorph in parallel type piezoelectric vibration generator is analyzed respectively by mechanical model and finite element modeling. The results indicate PZT-4, PZT-5A and PZT-5H piezoelectric materials and stainless steel, nickel alloy substrate material should be firstly chosen. Copyright © 2014 IFSA Publishing, S. L.

**Keywords:** Wireless sensor network, Vibration energy harvesting, Micro piezoelectric vibration generator, Finite element modeling.

---

### 1. Introduction

Piezoelectric vibration generator made in MEMS can infinite and continue to supply energy for low power electric device, which effectively solves the energy supply problem in rugged working condition of wireless sensor network [1-7]. However, output power of piezoelectric harvesting is still limited at present, which hinder seriously widespread use of the technology, and how to enhance effectively generating capacity of generating set is key problems needed to be solved currently. In recent years, research has shown that piezoelectric generating capacity mainly depends on material property, structure parameter, base frequency and incentive method. Ericka [8] design piezoelectric vibration generator bearing big load and its material is unimorph film. Wang [9] design drum type piezoelectric vibration generator which has high

output energy density, but resonant frequency of drum type generator general is beyond 200 Hz, and output power is low because it's difficult to resonant in low-frequency environment. Hu Hongping [10] adopt heliciform double piezoelectric ceramic piece as generating component, and its characteristic is small volume, micromation and good stability, and it can reduce effectively structure inherent frequency. But its area is small, so quantity of electric charge of collecting and output power is respectively few. Generating area of rectangle piezoelectric plate of cantilever piezoelectric vibration generator is big relative to heliciform piezoelectric piece, so quantity of electric charge of collecting and output power are enhanced, and it already become research hotspot of many countries all around the world. He Qing [11], Shad Roundy [12], Du Xiaozhen [13], Cheng Guangming [14] et al. respectively have researched structure optimization, mechanical model,

workmanship and experimental measurement system of cantilever piezoelectric generator, few researcher, however, have addressed the question of optimization research of cantilever piezoelectric generator's materials. So, in this article fem simulative analysis is apply to verify mechanical model precision based on electromechanical coupling distribution parameter, and influence rule of material parameter of cantilever piezoelectric generator to inherent frequency and output voltage respectively is studied, then material parameter is optimized analysis, and research foundation for enhancing generating capacity of cantilever piezoelectric generator with limited volume in working environment is laid.

## 2. Structure and Modeling

Cantilever piezoelectric generator form by piezoelectric ceramics, electrode, elastic substrate and fixed support. Piezoelectric ceramics cover and tightly integrated with substrate, and electrode cover on piezoelectric ceramics. One end of generator is fastened to support, another end vibrates freely with vibration source. Because generator's length and width are far greater than thickness, which belongs to thin walled beam structure and meets theoretical assumption of composite Euler–Bernoulli beam, so influence of shear deformation and rotational inertia can be neglected, and transformation regard as linear treatment under small amplitude condition.

When suffering persistent excitation, piezoelectric ceramics generate charge which move and deform with vibration source, and continuous load resistance current output is generated at load resistance, consequently, Mechanical vibration energy translate into electric energy. Structural representation of three essential cantilever piezoelectric generators are shown in Fig. 1. Fig. 1(a) is shown unimorph piezoelectric beam structure, and Fig. 1(b) is shown bimorph in series type beam structure, and Fig. 1(c) is shown bimorph in parallel type beam structure. Piezoelectric beam's length is indicated by  $l$ , width is indicated by  $b$ , thickness is indicated by  $h$ , superscript (or subscript)  $s$  and  $p$  respectively present substrate and piezoelectric layer, subscript  $u$ ,  $bs$ ,  $bp$  respectively present unimorph, bimorph in series type and bimorph in parallel type beam.

According to piezoelectrics theory, surface of piezoelectric beam which suffer continuous bending deformation will generate free charge. The stress and electric field of piezoelectrics obey piezoelectric equation:

$$\begin{cases} \{D\} = [d]\{T\} + [\varepsilon^T]\{E\} \\ \{S\} = [s^E]\{T\} + [d]^t\{E\} \end{cases}, \quad (1)$$

where  $\{D\}$  express electric displacement,  $\{E\}$  express electric field intensity,  $[d]$  express piezoelectric constant matrix,  $\{S\}$  and  $\{T\}$  respectively express strain and stress,  $[\varepsilon^T]$  express

free dielectric constant matrix at stress constant,  $[s^E]$  express short circuit elastic compliance ratio matrix at electric field constant.

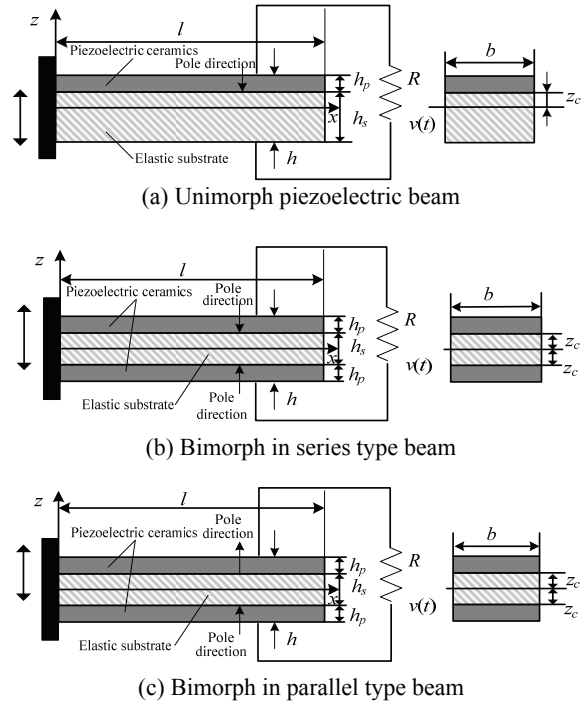


Fig. 1. Unimorph beam and bimorph beam.

Under piezoelectric beam suffer harmonic excitation, when excitation frequency is close by  $r$ -order inherent frequency, voltage response of unimorph, bimorph in series type and bimorph in parallel type respectively is [15, 16]:

$$\hat{v}_u(t) = \frac{j\omega R k_r^u F_r e^{j\omega t}}{(1 + j\omega R C_p^u)(\omega_r^2 - \omega^2 + j2\zeta_r \omega_r \omega) + j\omega R k_r^u \chi_r^u}, \quad (2)$$

$$\hat{v}_{bs}(t) = \frac{j2\omega R k_r^{bs} F_r e^{j\omega t}}{(2 + j\omega R C_p^{bs})(\omega_r^2 - \omega^2 + j2\zeta_r \omega_r \omega) + j2\omega R k_r^{bs} \chi_r^{bs}}, \quad (3)$$

$$\hat{v}_{bp}(t) = \frac{j2\omega R k_r^{bp} F_r e^{j\omega t}}{(1 + j2\omega R C_p^{bp})(\omega_r^2 - \omega^2 + j2\zeta_r \omega_r \omega) + j2\omega R k_r^{bp} \chi_r^{bp}}, \quad (4)$$

where  $R$  indicates load resistance,  $k_r$  indicates modal coupling item,  $F_r$  indicates amplitude excitation function,  $C_p$  indicates piezoelectric capacitance,  $\zeta_r$  indicates mechanical damping ratio,  $\chi_r$  indicates electromechanical coupling item.

$R$ -order inherent frequency  $\omega_{rd}$  is expressed as [14, 15]:

$$\omega_{rd} = \lambda_r^2 \sqrt{\frac{YI}{mI^4}} \sqrt{1 - \zeta_r^2}, \quad (5)$$

where  $\lambda_r$  indicates nondimensional frequency,  $Y$  indicates elastic module,  $I$  indicates moment of inertia,  $m$  indicates mass of per unit length.

### 3. Performance Simulation Analysis

Software of finite element analysis ANSYS is applied to model and simulate for cantilever piezoelectric generator, and computed result of mechanical model is further validated. For bearing more deformation, phosphor bronze with larger elasticity modulus is selected as substrate material, and PZT-5H is selected as piezoelectric ceramics material, and performance parameter of unimorph beam is shown in Table 1. For comparing generating capacity of unimorph with bimorph in series type and bimorph in parallel type in same volume, thickness of each of bimorph is same which is half with unimorph.

**Table 1.** Structural and material parameters of unimorph piezoelectric beam.

Parameter	Piezoelectric layer (PZT-5H)	Phosphor bronze substrate
Density $\rho$ (kg/m <sup>3</sup> )	7600	8860
Elastic module $E$ (GPa)	60.6	110.0
Poisson's ratio $\mu$	0.289	0.330
piezoelectric constant $d_{31}$ (10 <sup>-12</sup> m/V)	-274	—
dielectric constant $\epsilon_{33}^s$ (F/m)	1470 $\epsilon_0$	—
Length $l$ (mm)	50	50
Width $w$ (mm)	15	15
Thickness $h$ (mm)	0.4	0.4

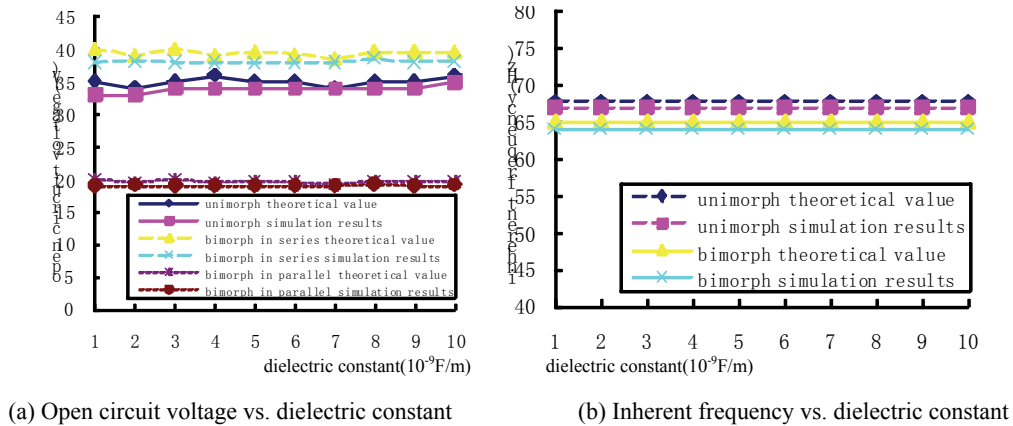
Influence of dielectric constant, density, elasticity modulus and piezoelectric constant of piezoelectric layer to open circuit voltage and inherent frequency respectively is shown from Fig. 2 to Fig. 5.

Sees from the Fig. 2, open circuit voltage and first order inherent frequency aren't basic influenced by dielectric constant.

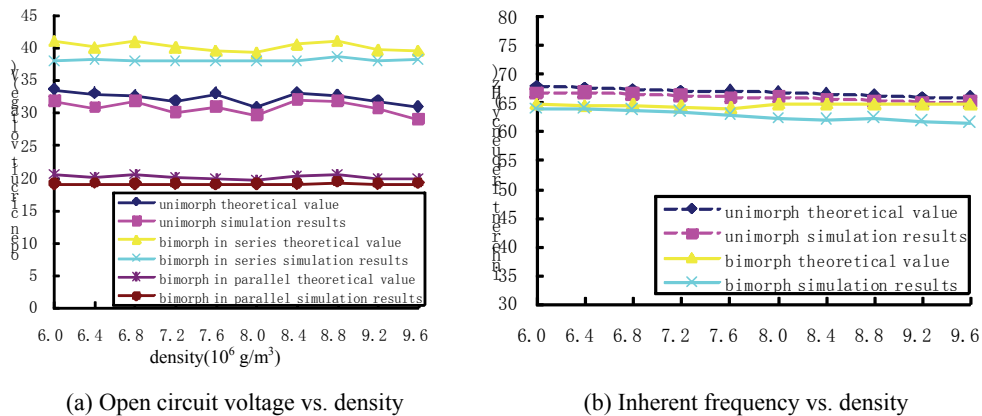
Sees from the Fig. 3, influence of density to open circuit voltage is small too, but first order inherent frequency of unimorph and bimorph beam are slightly lower with increasing of density.

From Fig. 4, influence of elastic module to generating capacity is larger, open circuit voltage and first order inherent frequency of unimorph and bimorph beam increase with increasing piezoelectric elasticity modulus.

From Fig. 5(a), influence of piezoelectric constant to open circuit voltage is larger too, and open circuit voltage increases first, and then decreases with increasing piezoelectric constant, and open circuit voltage of bimorph beam is the largest when piezoelectric constant is about -180 pm/V, so the best piezoelectric constant of bimorph beam is about -180 pm/V; open circuit voltage of unimorph beam is the largest when piezoelectric constant is about -210 pm/V, so the best piezoelectric constant of unimorph beam is about -210 pm/V. From Fig. 5(b), first order inherent frequency isn't basic influenced by piezoelectric constant.



**Fig. 2.** Generating performance vs. dielectric constant of piezoelectric layer.



**Fig. 3.** Generating performance vs. density of piezoelectric layer.

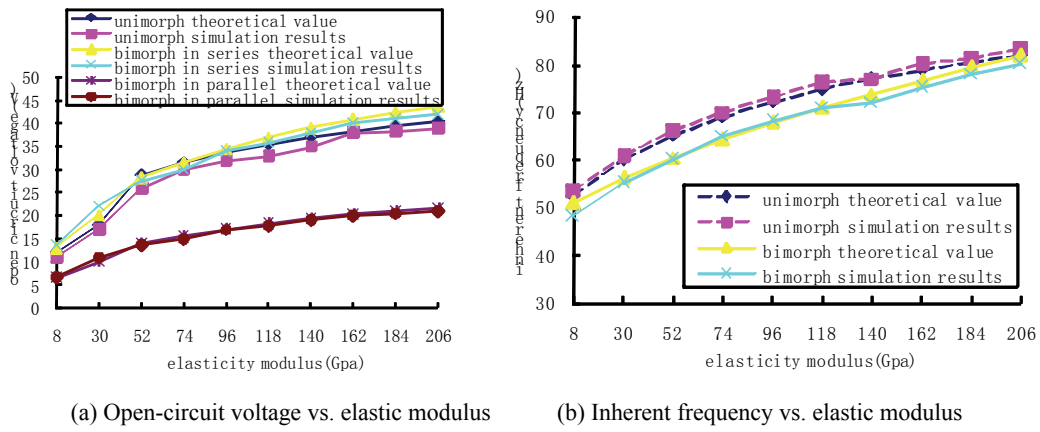


Fig. 4. Generating performance vs. elastic modulus of piezoelectric layer.

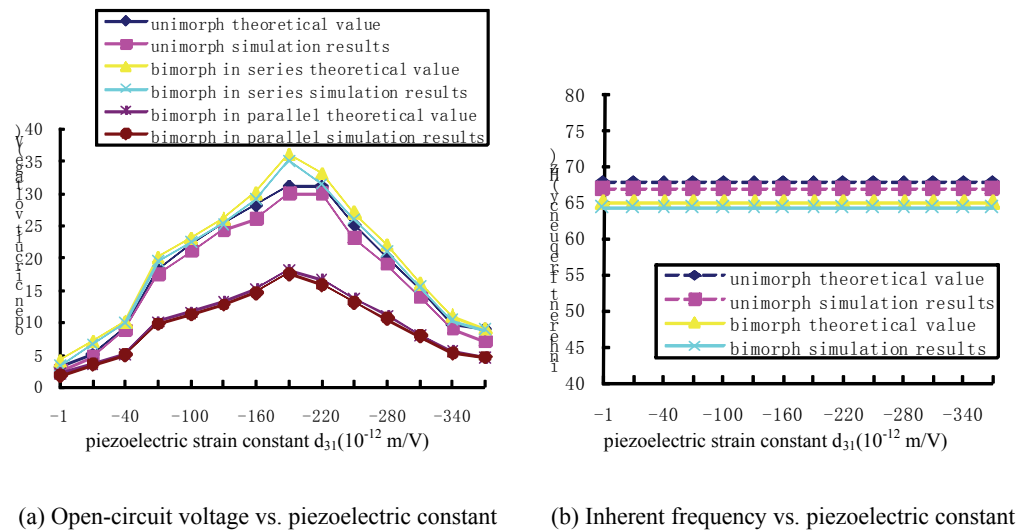


Fig. 5. Generating performance vs. piezoelectric constant of piezoelectric layer.

It can be seen from the above analysis that for obtaining larger open circuit voltage and lower first order inherent frequency, larger density and piezoelectric constant between -180 to -210 pm/V should be selected, and elasticity modulus should be overall consideration according to requisite output voltage and environmental vibration frequency. But material parameter of specific piezoelectric materials is inherent attribute which don't random match, and material performance parameter of common PZT piezoelectric material is shown in Table 2. Influencing characteristic of common PZT piezoelectric material to open circuit voltage and inherent frequency are analyzed to find that open circuit voltage of piezoelectric ceramics PZT-4, PZT-5A and PZT-5H is larger, the result is shown in Fig. 6. So cantilever piezoelectric generator is made to select firstly above three piezoelectric materials.

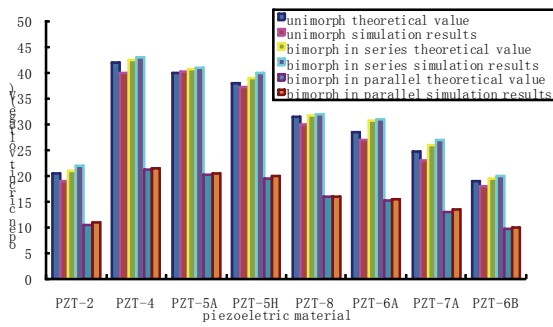
Influence of substrate material parameter to generating performance is analyzed to discover that open circuit voltage and first order inherent frequency is increase with the increasing substrate elasticity modulus, and result is shown in Fig. 7. So, substrate elasticity modulus is selected which take

into account demands of vibration source frequency and output voltage value.

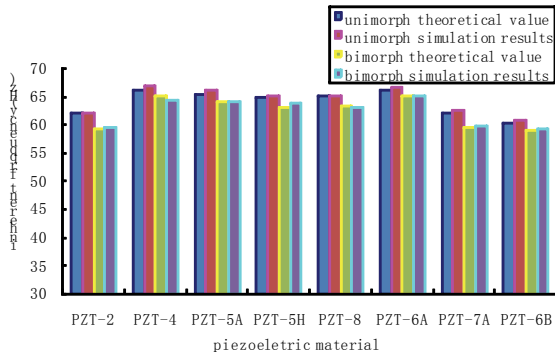
Influence of substrate density to open circuit voltage and first order inherent frequency are shown in Fig. 8. From Fig. 8, influence of substrate density to open circuit voltage is little, but first order inherent frequency is reducing with increasing substrate density. So, substrate material should be larger density for obtaining high generating performance.

Table 2. Common PZT piezoelectric material parameters.

Material parameter Piezoelectric material	$\epsilon_{33}^s / \epsilon_0$	$d_{31}(10^{-12}$ m/V)	$s_{11}^E(10^{-12}$ m <sup>2</sup> /N)	$\rho(10^3$ kg/m <sup>3</sup> )
PZT-2	260	-60	11.6	7.50
PZT-4	635	-123	12.3	7.50
PZT-5A	830	-171	16.4	7.75
PZT-5H	1470	-274	16.5	7.50
PAT-6A	730	-80	10.7	7.45
PZT-6B	386	-27	9.0	7.55
PZT-7A	235	-60	10.7	7.60
PZT-8	600	-93	12.0	7.60

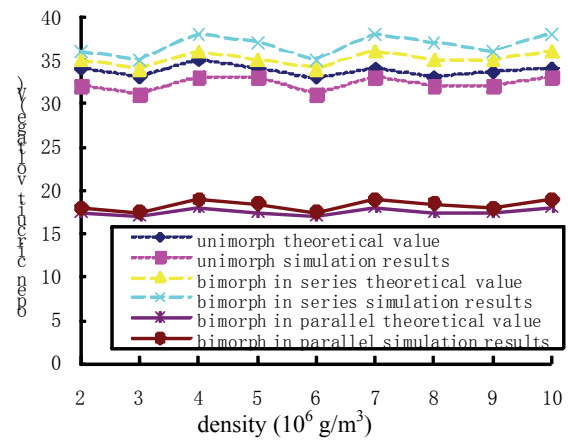


(a) Open circuit voltage vs. piezoelectric material

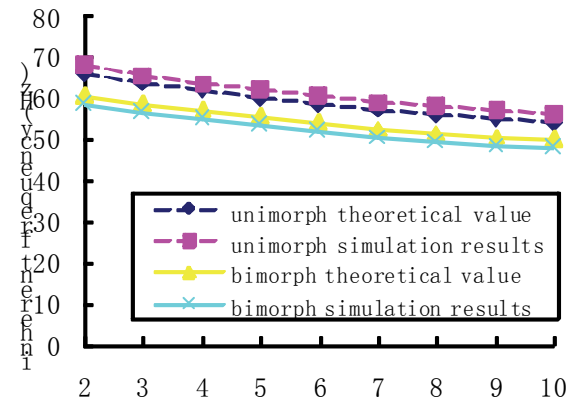


(b) Inherent frequency vs. piezoelectric material

Fig. 6. Generating performance vs. common piezoelectric material.

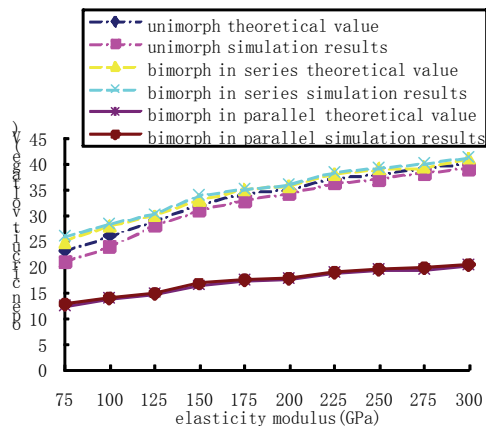


(a) Open circuit voltage vs. density

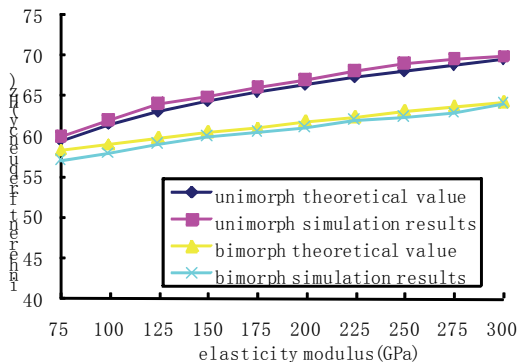


(b) Inherent frequency vs. density

Fig. 8. Generating performance vs. density of substrate.



(a) Open-circuit voltage vs. elasticity modulus



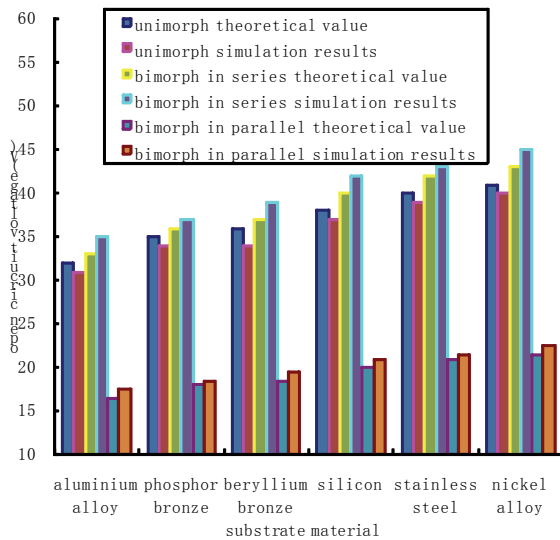
(b) Inherent frequency vs. elasticity modulus

Fig. 7. Generating performance vs. elasticity modulus of substrate.

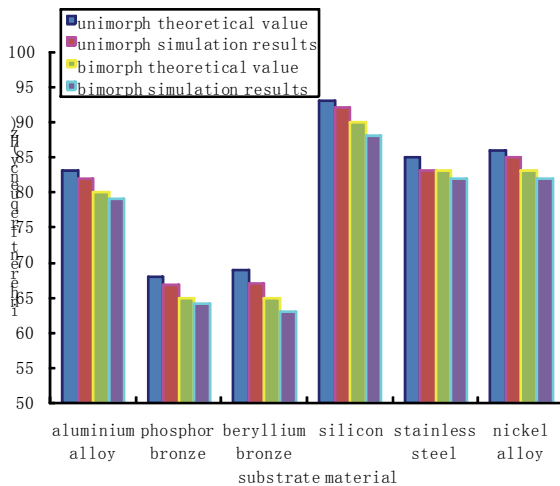
Based on substrate material of beryllium bronze, stainless steel, nickel alloy and phosphor bronze, which parameters are shown in Table 3, and influence of substrate material to open circuit voltage and first order inherent frequency are analyzed which is similar to analytical method of piezoelectric layer above, and results are shown in Fig. 9. From Fig. 9, output voltage of unimorph and bimorph beam with stainless steel and nickel alloy substrate material are larger, and first order inherent frequency of unimorph and bimorph beam with phosphor bronze and beryllium bronze substrate material are lower, which work well with low frequency incentive environment.

Table 3. Common substrate material parameters.

Material parameter Substrate material	elasticity modulus $Y_s$ (GPa)	Poisson's ratio $\gamma$	Density $\rho$ ( $\text{kg/m}^3$ )
Beryllium bronze	118	0.35	8920
Stainless steel	197	0.28	7800
Aluminium alloy	75	0.33	2700
Nickel alloy	210	0.32	8800
Silicon	170	0.28	2328
Phosphor bronze	110	0.33	8860



(a) Open-circuit voltage vs. substrate material



(b) Inherent frequency vs. substrate material

**Fig. 9.** Generating performance vs. common substrate material.

## 4. Conclusions

Mechanical model accuracy is verified which apply ANSYS finite element simulation, and influence rule of material parameter of cantilever piezoelectric generator to inherent frequency and output voltage are studied, and material parameter is optimized analysis aiming maximum output electric energy with minimum volume. The results indicate PZT-4, PZT-5A and PZT-5H piezoelectric materials and stainless steel, nickel alloy substrate material should be firstly chosen.

## Acknowledgements

The authors would like to acknowledge the support of Provincial Natural Science Foundation of Hebei of China (Grant E2013204069), Special Fund

for Agro-scientific Research in the Public Interest (Grant 201203016), Science and Technology Projects of Baoding of Hebei (Grant 13ZG020).

## References

- [1]. T. Galchev, E. E. Aktakka, K. Najafi, et al, A piezoelectric parametric frequency increased generator for harvesting low-frequency vibrations, *Journal of Micro Electro-mechanical Systems*, Vol. 21, No. 6, 2012, pp. 1311-1320.
- [2]. Choong Hyo Park, Jong Wook Kim, Jung Hoon Lim et al, Increase of generating power of cantilever type piezoelectric generators by interconnecting the generators, *Integrated Ferroelectrics*, Vol. 134, 2012, pp. 88-101.
- [3]. J. H. Lim, S. S. Jeong, N. R. Kim et al, A study on the resonance frequency of the cross-shaped piezoelectric generator according to change in elastic body thickness and tip mass, *Integrated Ferroelectrics*, Vol. 139, 2012, pp. 32-39.
- [4]. E. Arroyo, A. Badel, F. Formosa, et al, Comparison of electromagnetic and piezoelectric vibration energy harvesters: model and experiments, *Sensors and Actuators. A, Physical*, Vol. 183, 2012, pp. 148-156.
- [5]. Yan Zhen, He Qing, Performance analysis on incentive environment of micro cantilever piezoelectric vibration generator, in *Proceedings of the Chinese Society for Electrical Engineering*, Vol. 31, No. 30, 2011, pp. 140-145.
- [6]. He Qing, Lan Lan, Yan Zhen, et al, Modeling and simulation of piezoelectric vibration generator for powering wireless sensor networks, *Sensors and Transducers*, Vol. 22, Special Issue, 2013, pp. 133-138.
- [7]. Chang-Il Kim, Yong-Ho Jang, Young Hun Jeong, et al., Performance enhancement of elastic-spring-supported piezoelectric cantilever generator by a 2-degree-of-freedom system, *Applied Physics Express*, Vol. 5, Issue 3, 2012, pp. 37101.1-37101.3.
- [8]. M. Ericka, D. Vasic, F. Costa, et al., Energy harvesting from vibration using a piezoelectric membrane, *Journal De Physique Iv*, Vol. 128, 2005, pp. 187-193.
- [9]. S. Wang, H. L. Kwok, C. L. Sun, et al, Energy harvesting with piezoelectric drum transducer, *Applied Physics Letters*, Vol. 90, Issue 11, 2007, pp. 113506-113509.
- [10]. Hu Hongping, Gao Farong, Xue Huan, et al, Analysis on structure and performance of a low frequency piezoelectric power harvester using a spiral-shaped bimorph, *Acta Mechanica Solida Sinica*, Vol. 8, Issue 1, 2007, pp. 87-92.
- [11]. He Qing, Yan Zhen, On piezoelectric vibration generator for self-powered wireless sensor network, *Sensor Letters*, Vol. 9, Issue 5, 2011, pp. 1869-1873.
- [12]. S. Roundy, K. W. Ringt, A piezoelectric vibration based generator for wireless electronics, *Smart Materials & Structures*, Vol. 13, Issue 5, 2004, pp. 1131-1142.
- [13]. Du Xiaozhen, Micro piezoelectric power generator driven by ambient vibration, *Dalian University of Technology*, Dalian, 2008.
- [14]. Cheng Guangming, Pang Jianzhi, Tang Kehong, et al, development of measuring system for electricity generating capacity of piezoelectric ceramics,

Journal of Jilin University (Engineering and Technology Edition), Vol. 37, No. 2, 2007, pp. 367-371.

- [15]. A. Erturk, D. J. Inman, On mechanical modeling of cantilevered piezoelectric vibration energy harvesters, *Journal of Intelligent Material Systems*

and Structures, Vol. 19, No. 11, 2008, pp. 1311-1325.

- [16]. A. Erturk, D. J. Inman, A distributed parameter electromechanical model for cantilevered piezoelectric energy harvesters, *Journal of Vibration and Acoustics*, Vol. 130, No. 4, 2008, pp. 1-15.

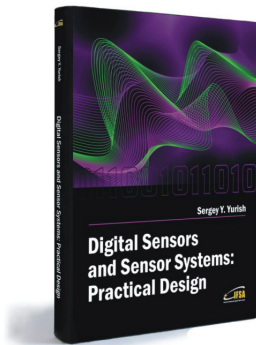
2014 Copyright ©, International Frequency Sensor Association (IFSA) Publishing, S. L. All rights reserved. (<http://www.sensorsportal.com>)



International Frequency Sensor Association (IFSA) Publishing

## Digital Sensors and Sensor Systems: Practical Design

Sergey Y. Yurish



Formats: printable pdf (Acrobat) and print (hardcover), 419 pages

ISBN: 978-84-616-0652-8,  
e-ISBN: 978-84-615-6957-1

The goal of this book is to help the practitioners achieve the best metrological and technical performances of digital sensors and sensor systems at low cost, and significantly to reduce time-to-market. It should be also useful for students, lectures and professors to provide a solid background of the novel concepts and design approach.

### Book features include:

- Each of chapter can be used independently and contains its own detailed list of references
- Easy-to-repeat experiments
- Practical orientation
- Dozens examples of various complete sensors and sensor systems for physical and chemical, electrical and non-electrical values
- Detailed description of technology driven and coming alternative to the ADC a frequency (time)-to-digital conversion

*Digital Sensors and Sensor Systems: Practical Design* will greatly benefit undergraduate and at PhD students, engineers, scientists and researchers in both industry and academia. It is especially suited as a reference guide for practitioners, working for Original Equipment Manufacturers (OEM) electronics market (electronics/hardware), sensor industry, and using commercial-off-the-shelf components

[http://sensorsportal.com/HTML/BOOKSTORE/Digital\\_Sensors.htm](http://sensorsportal.com/HTML/BOOKSTORE/Digital_Sensors.htm)

Promoted by IFSA

## MEMS for Cell Phones & Tablets Report up to 2017

Market dynamics, technical trends, key players, market forecasts for accelerometers, gyroscopes, magnetometers, combos, pressure sensors, microphones, BAW filters, duplexers, switches and variable capacitors, oscillators / resonators and micromirrors.

Order online:

[http://www.sensorsportal.com/HTML/MEMS\\_for\\_Cell\\_Phones\\_and\\_Tablets.htm](http://www.sensorsportal.com/HTML/MEMS_for_Cell_Phones_and_Tablets.htm)