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COMPUTATIONAL FLUID DYNAMICS

*Original*

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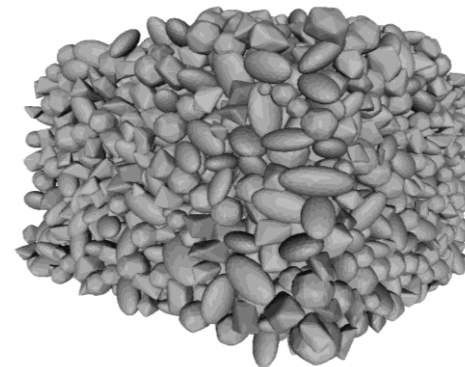
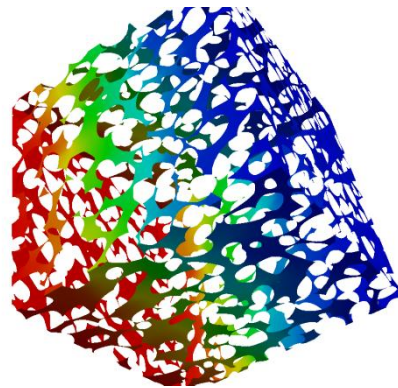
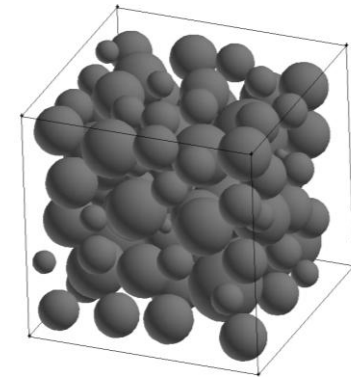
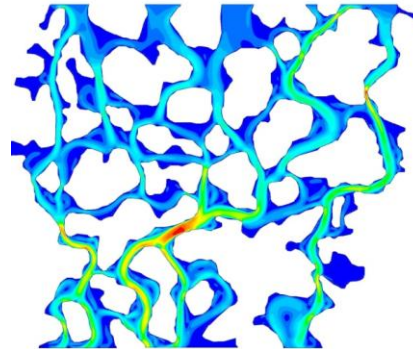
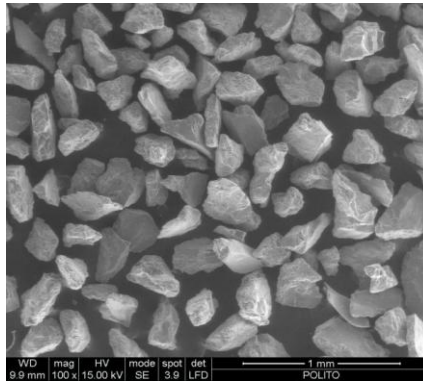
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# SIMULATION OF FLOW AND PARTICLE TRANSPORT AND DEPOSITION IN POROUS MEDIA WITH COMPUTATIONAL FLUID DYNAMICS



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ECCE9/ECAB2  
The Hague, Netherlands

# INTRODUCTION: MOTIVATION OF THE WORK

## MANY FIELDS OF INTEREST:

- PROCESS ENGG.:
  - Packed bed reactors
  - Filtration
  - Chromatographic separation
- ENVIRONMENTAL ENGG.:
  - Aquifer remediation

## PURPOSE

Results from  
microscale simulations ...



... used to develop  
macroscale models

*“.. since, depending on the right scale of observation, everything is porous. “*

# THEORETICAL BACKGROUND: FLUID FLOW

## MACROSCALE PSEUDO-CONTINUUM APPROACH

- Creeping flow ( $Re < 1$ ): linear relationship

DARCY'S LAW 
$$\frac{\Delta P}{L} = \frac{\mu}{k} q$$

- $Re > 1$ : nonlinear relationship

FORCHHEIMER'S LAW 
$$\frac{\Delta P}{L} = \frac{\mu}{k} q + \beta \rho q^2$$

- Packed beds filter law (wide range of  $Re$ )

ERGUN'S LAW 
$$\Delta P^* = \frac{150}{Re^*} + 1.75$$

$$\Delta P^* = \frac{\Delta P \rho D_g \varepsilon^3}{L G_0^2 (1 - \varepsilon^3)}$$

$$Re^* = \frac{D_g G_0}{(1 - \varepsilon) \mu}$$

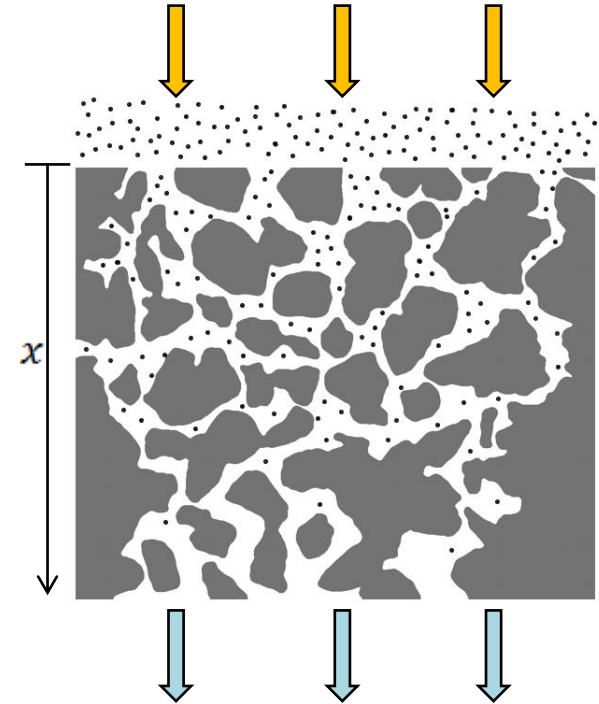
# THEORETICAL BACKGROUND: PARTICLE DEPOSITION

## MACROSCALE 1D ADVECTIVE-DIFFUSIVE EQUATION

$$\frac{\partial C}{\partial t} + q \frac{\partial C}{\partial x} - D \frac{\partial^2 C}{\partial x^2} = \textit{Source}$$

$$\textit{Source} = -K_d C$$

$$K_d = \frac{3}{2} \frac{1 - \varepsilon}{\varepsilon} \frac{q}{D_g} \alpha \eta$$



$\eta$ : COLLECTOR DEPOSITION EFFICIENCY

# THEORETICAL BACKGROUND: PARTICLE DEPOSITION

## DEPOSITION EFFICIENCY

- BROWNIAN DIFFUSION

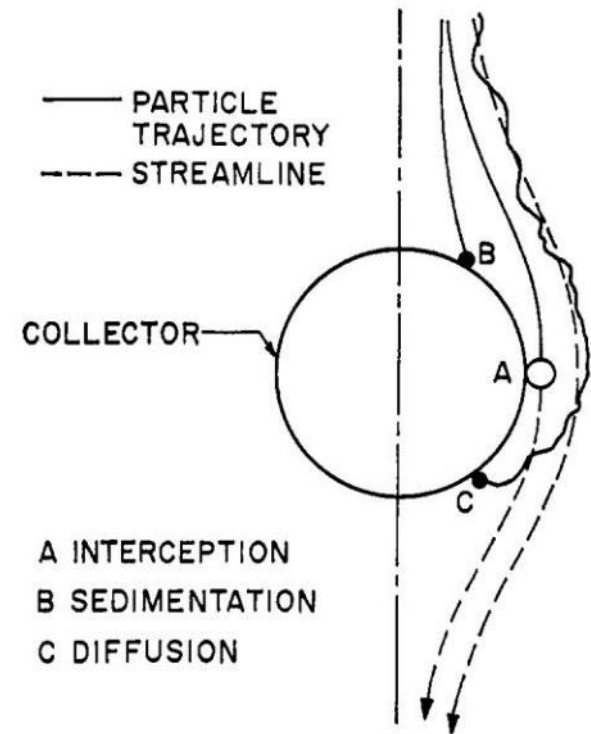
$$\eta_B = 4.04 Pe^{-\frac{2}{3}} \quad \text{LEVICH}$$

$$\eta_B = 4 As^{\frac{1}{3}} Pe^{-\frac{2}{3}} \quad \text{HAPPEL}$$

- INTERCEPTION

$$\eta_I = \frac{3}{2} \left( \frac{d_p}{D_g} \right)^2 = \frac{3}{2} N_R^2 \quad \text{YAO}$$

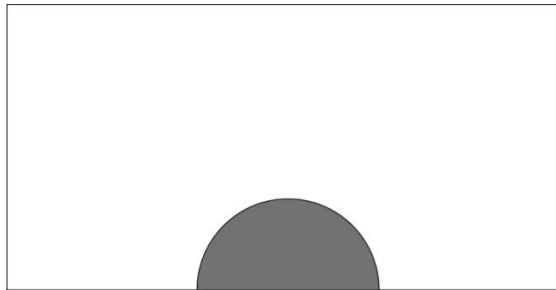
$$\eta_I = \frac{3}{2} As N_R^2 \quad \text{HAPPEL}$$



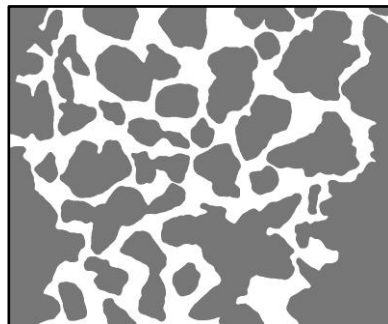
# METHODOLOGY: MICROSCALE GEOMETRIC MODELS

## INCREASING COMPLEXITY

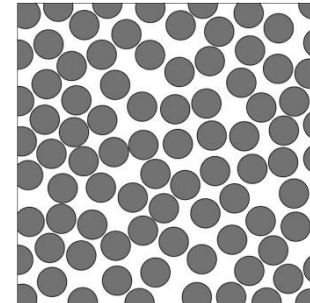
- SINGLE COLLECTOR
- CIRCULAR SHAPE  
(under axial simmetry)



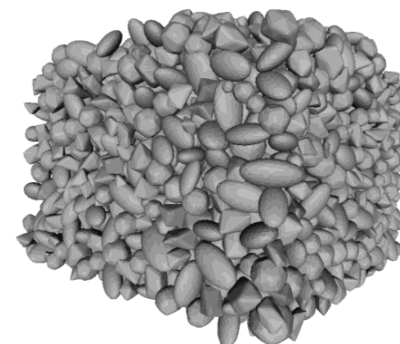
- IRREGULAR SHAPES
- REALISTIC  $\mu$ -CT/SEM SCANS  
(planar geometry)



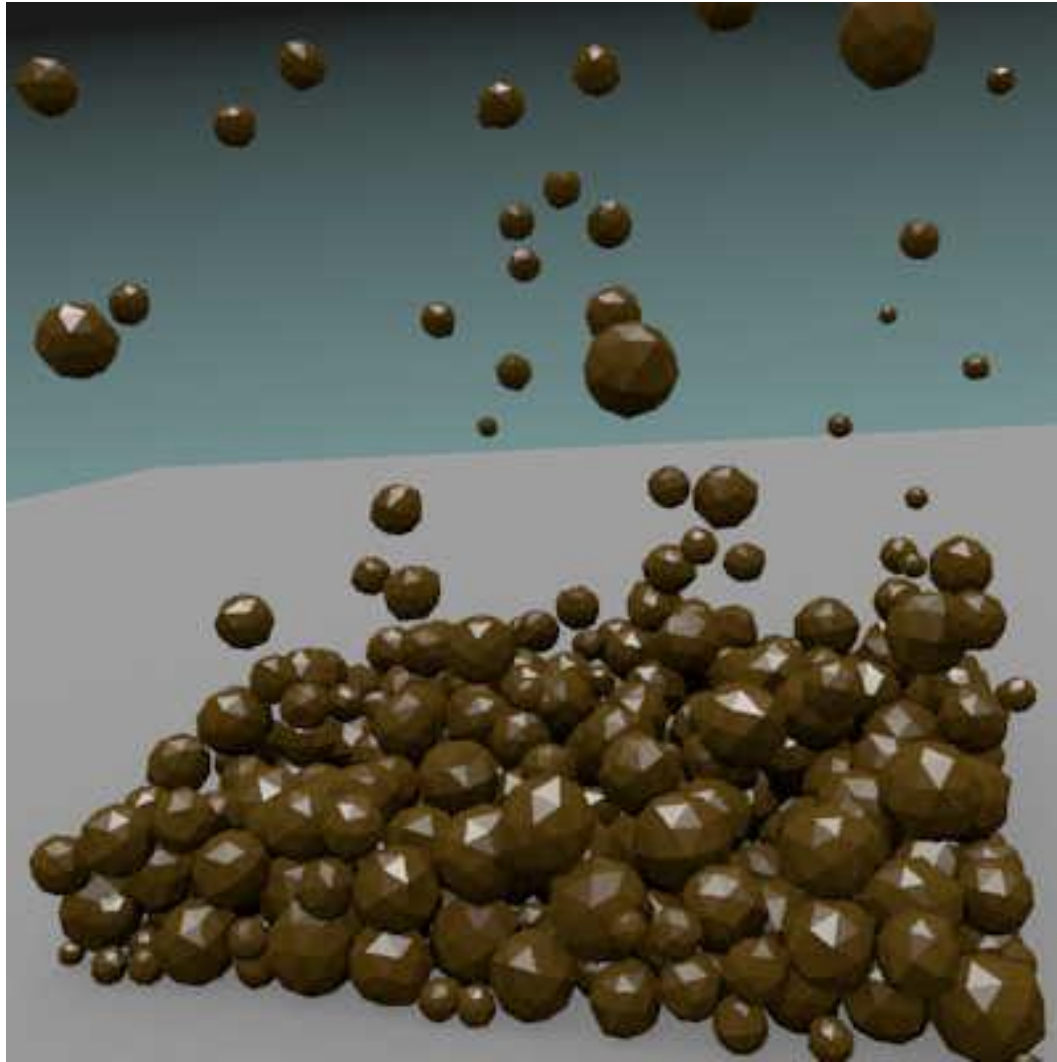
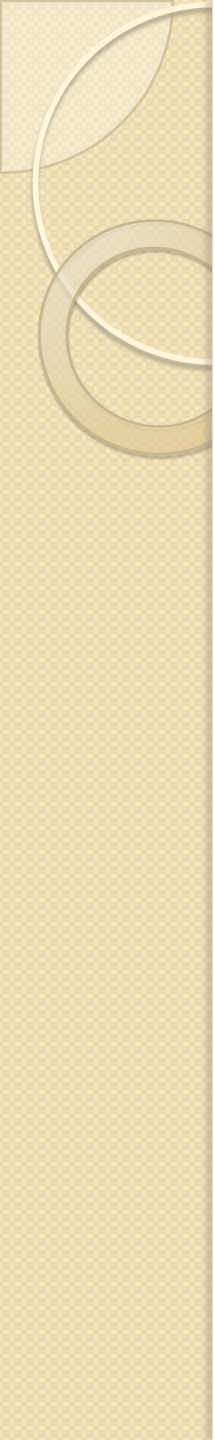
- CIRCULAR SHAPE
- ARTIFICIAL PACKING  
(planar geometry)



- IRREGULAR SHAPES
- ARTIFICIAL PACKING









# METHODOLOGY: OPERATING CONDITIONS

## SOLVERS AND MESHING

- Finite volume CFD codes:

FLUENT, OPENFOAM

- Body-fitted meshers:

GAMBIT, SNAPPYHEXMESH

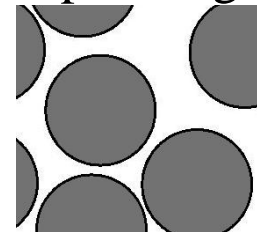
## OPERATING CONDITIONS

- $D_g = 100 \text{ m} \div 300 \text{ m}$
- $\epsilon = 0,3 \div 0,5$
- $q = 10^{-6}, 10^{-5}, \dots, 10^{-1} \text{ m s}^{-1}$
- Laminar model
- $T = 293 \text{ K}$
- Viscosity  $\mu = 0.00103 \text{ Kg m}^{-1}\text{s}^{-1}$

- 8 realistic geometries

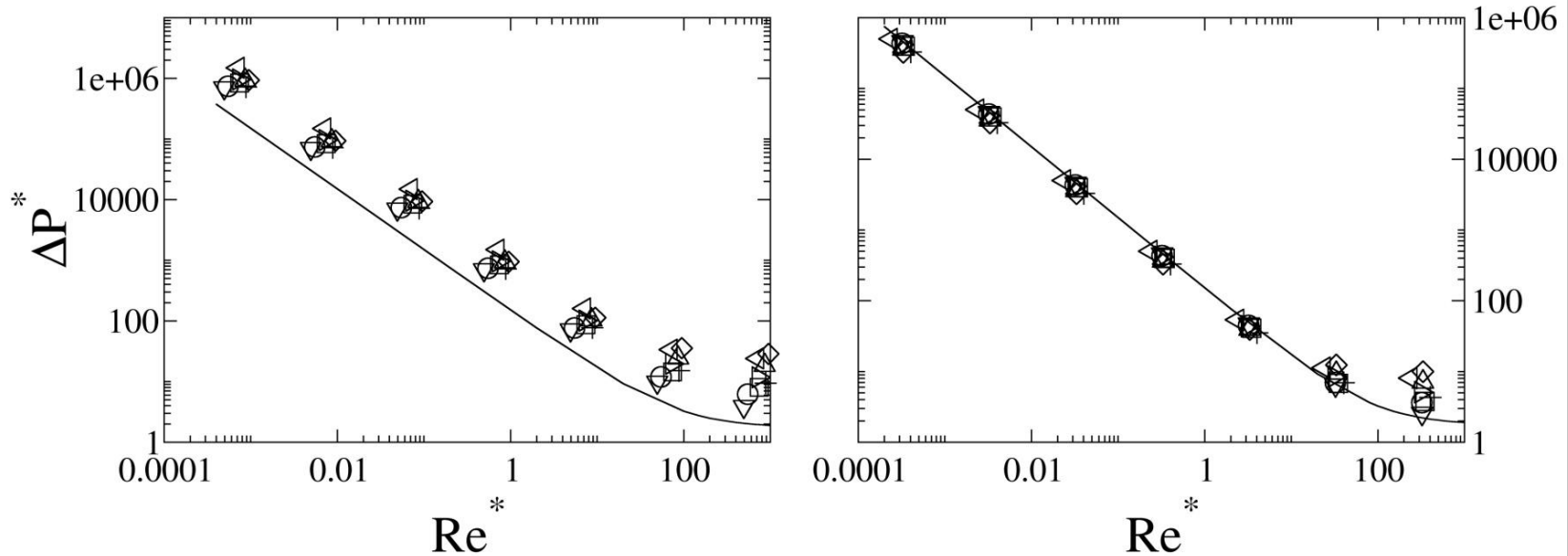


- 4 simplified geometries



# RESULTS: FLUID FLOW

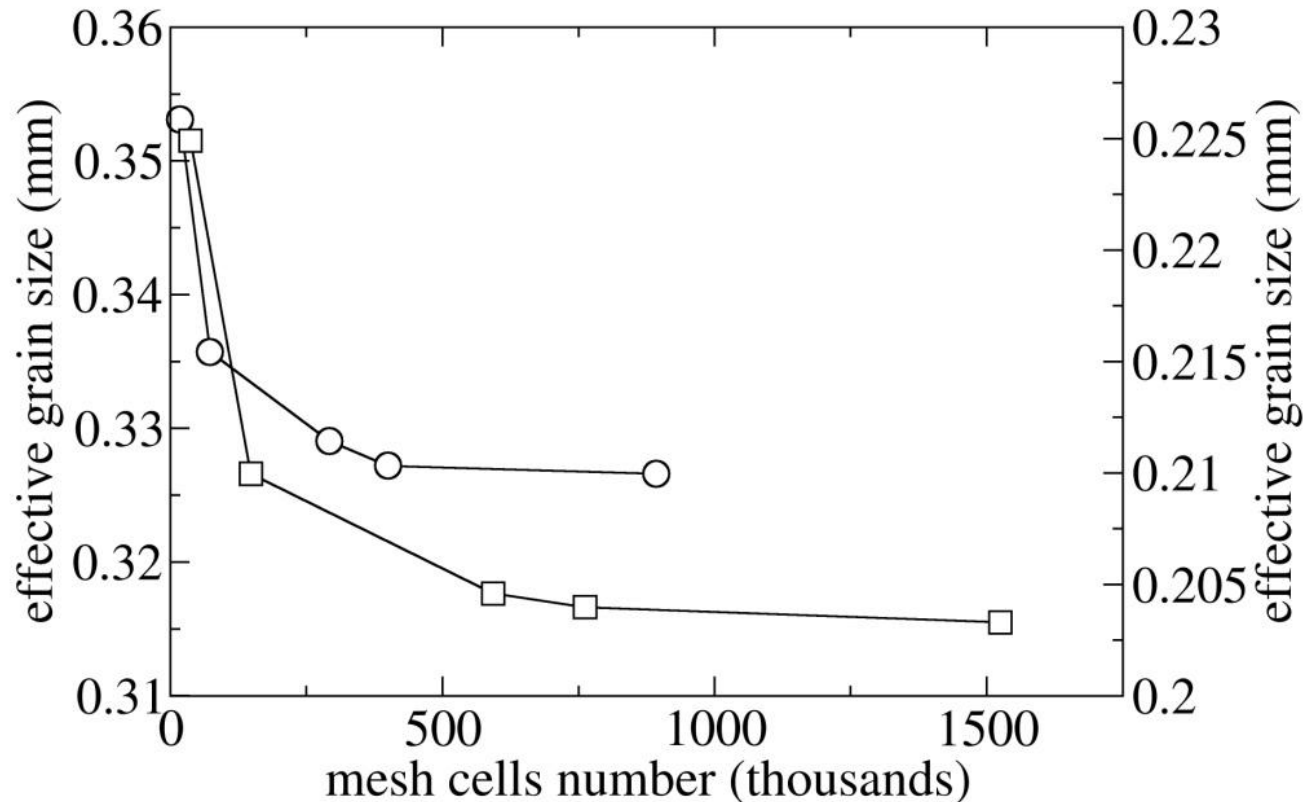
## COMPARISON WITH ERGUN'S LAW



- Results show good agreement with Ergun's law
- Fitting on Ergun's law to obtain an effective grain diameter,  $D_g^*$

# RESULTS: FLUID FLOW

## GRID INDEPENDENCE VERIFICATION

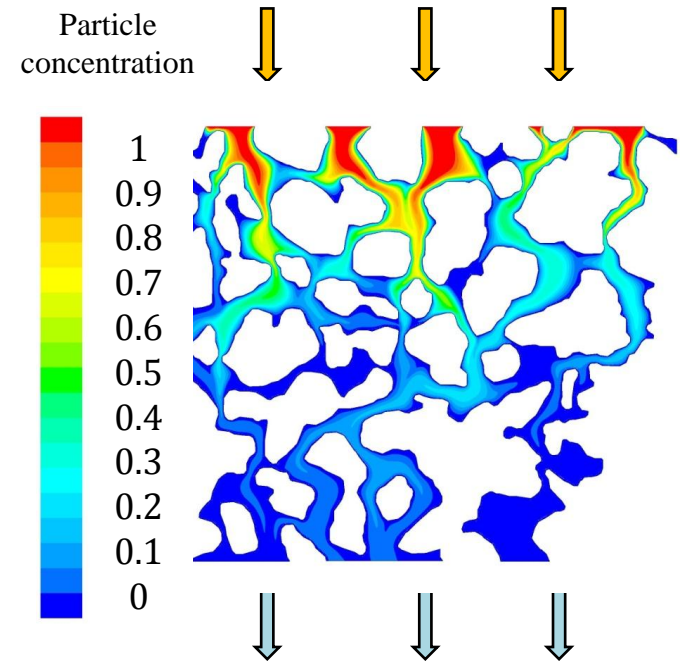


- Need for a single parameter summarizing fluid flow results
- Grid independence assessed with changes in  $D_g^*$

# METHODOLOGY: OPERATING CONDITIONS

## PARTICLES MODELING

- Particles are transported by convective and diffusive phenomena
- $C = 1$  at inlet
- $C = 0$  on grain surface
  - Assumed “perfect sink” condition
- Particle diameter
  - $d_p = 1, 10, 100, 200, 500, 625, 750, 875, 1000$  nm

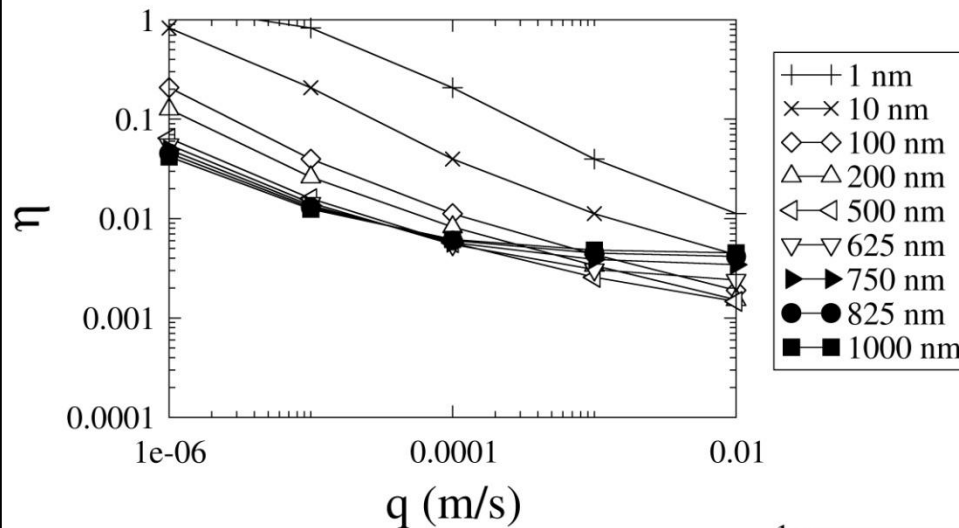


Collector deposition efficiency,  $\eta$   
calculated with packed bed performance equation

$$\frac{dC}{dx} = -\frac{3}{2} \frac{1 - \varepsilon}{\varepsilon D_g} \eta C$$

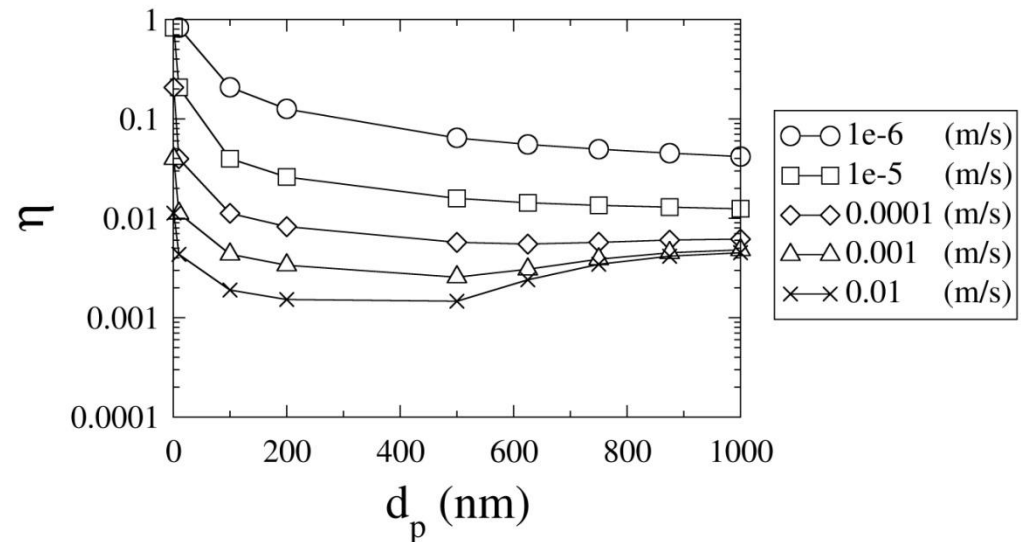
# RESULTS: PARTICLE DEPOSITION

## DEPOSITION EFFICIENCY: OVERVIEW



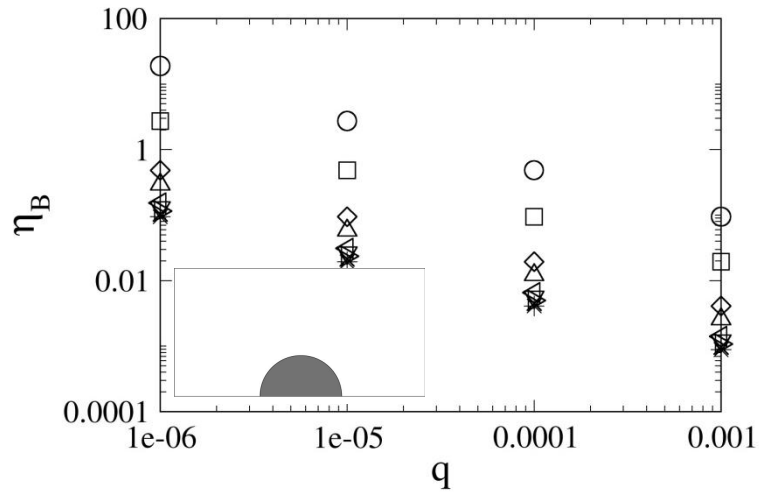
Efficiency  $\eta$  decreases for higher superficial velocities  $q$  (low residency times)

Efficiency  $\eta$  decreases for higher particle diameter (low diffusivity) until a certain  $d_p$  value, then increases for the steric interception effect.



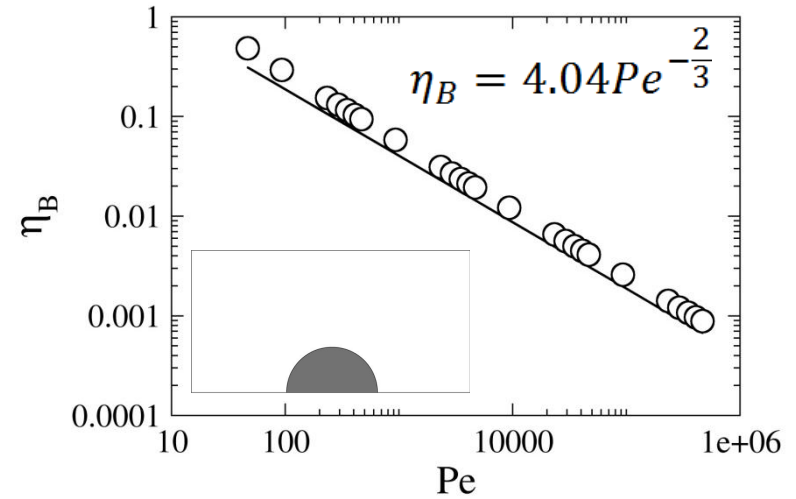
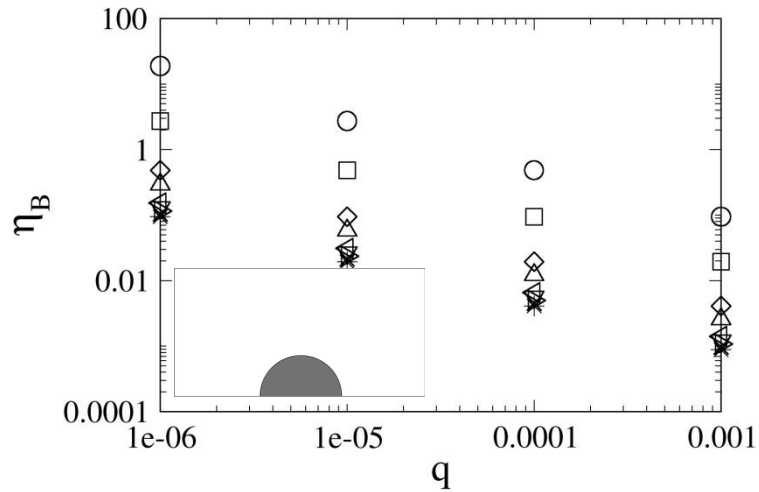
# RESULTS: PARTICLE DEPOSITION

## DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION



# RESULTS: PARTICLE DEPOSITION

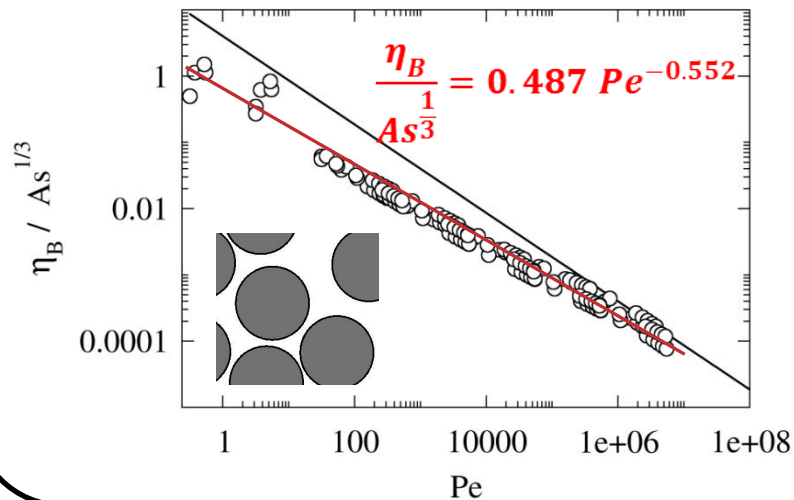
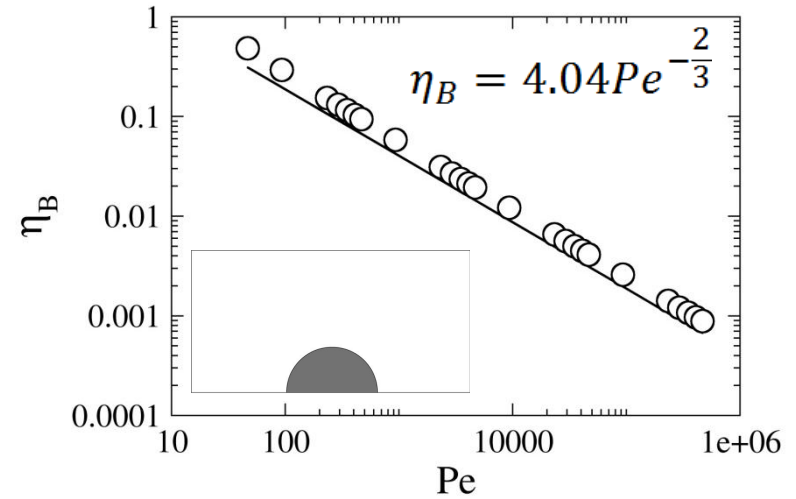
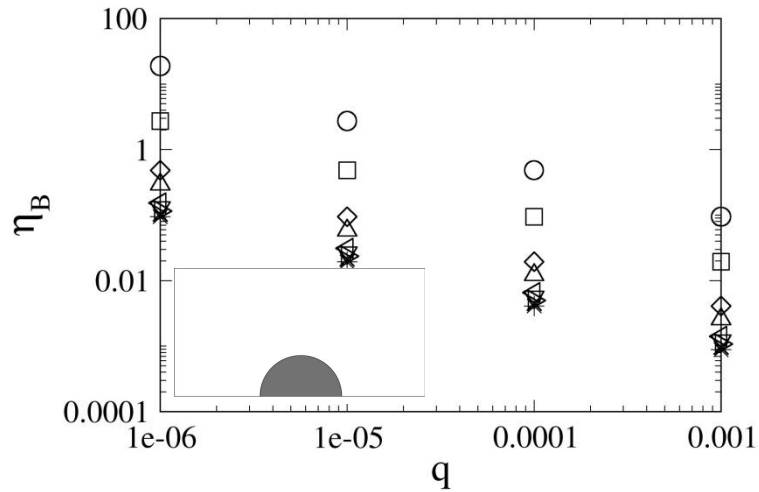
## DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION





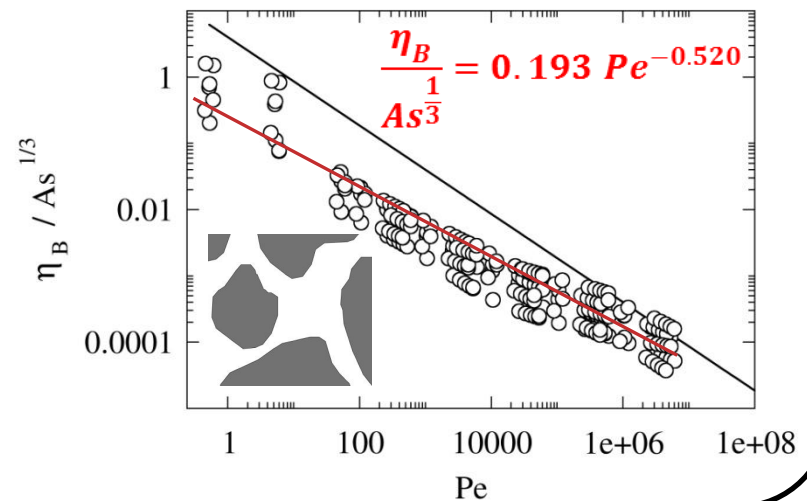
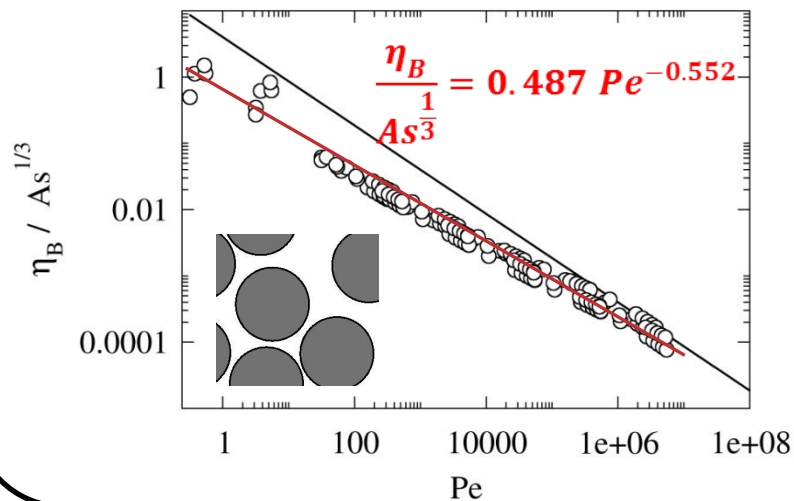
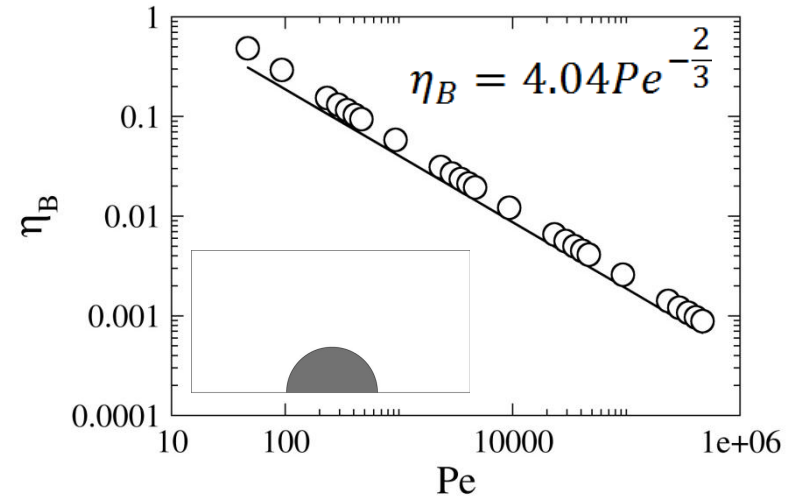
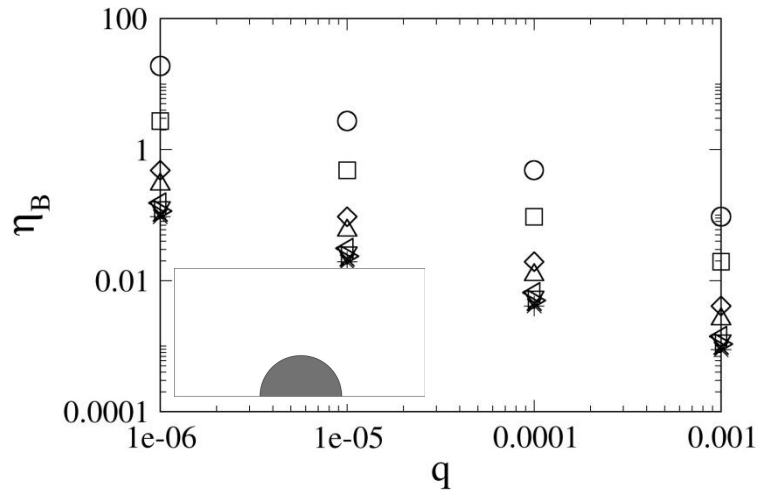
# RESULTS: PARTICLE DEPOSITION

## DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION



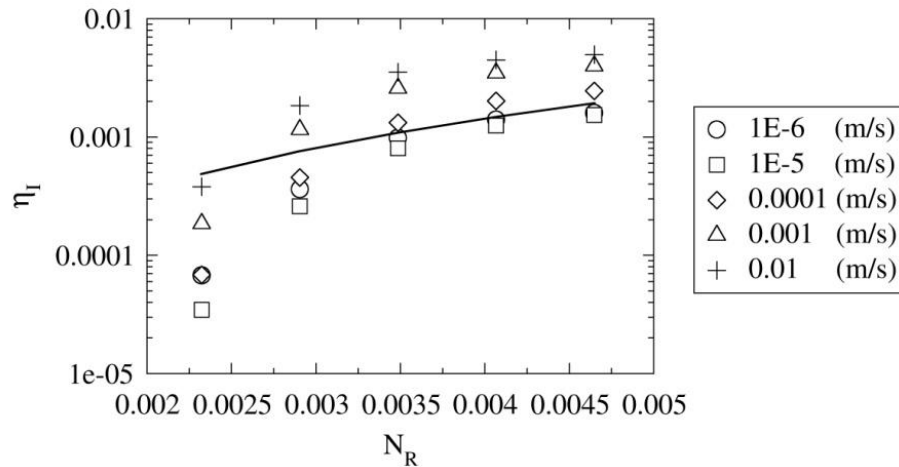
# RESULTS: PARTICLE DEPOSITION

## DEPOSITION EFFICIENCY: BROWNIAN DIFFUSION



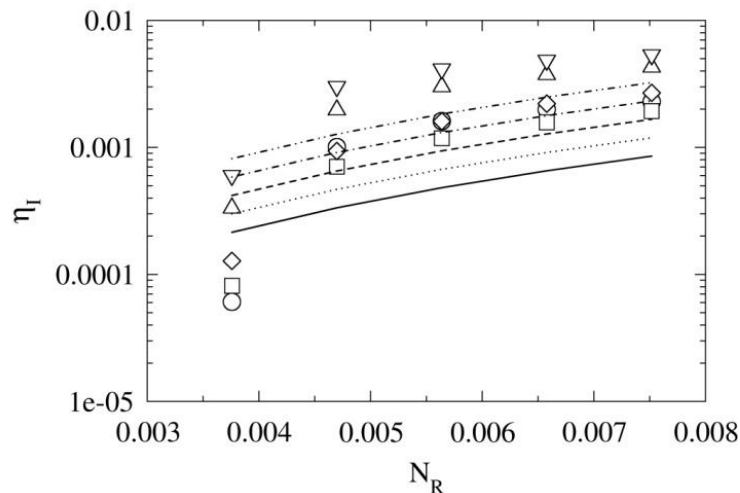
# RESULTS: PARTICLE DEPOSITION

## DEPOSITION EFFICIENCY: INTERCEPTION



Theoretical law:

$$\eta_I = \frac{3}{2} As N_R^2$$



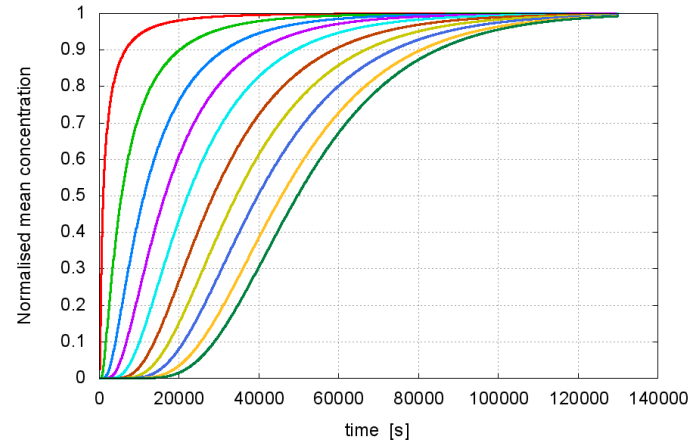
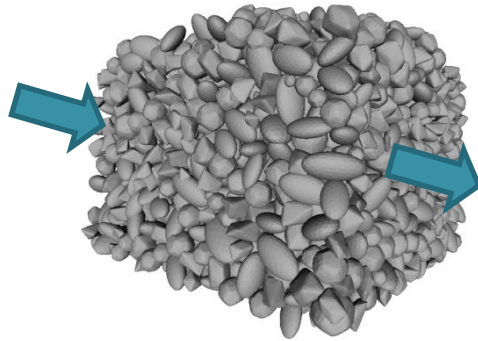
- Results appear in line with theoretical predictions but are strongly dispersed, with great variations at different  $q$
- A dependency of  $\eta$  on  $q$  can be proposed



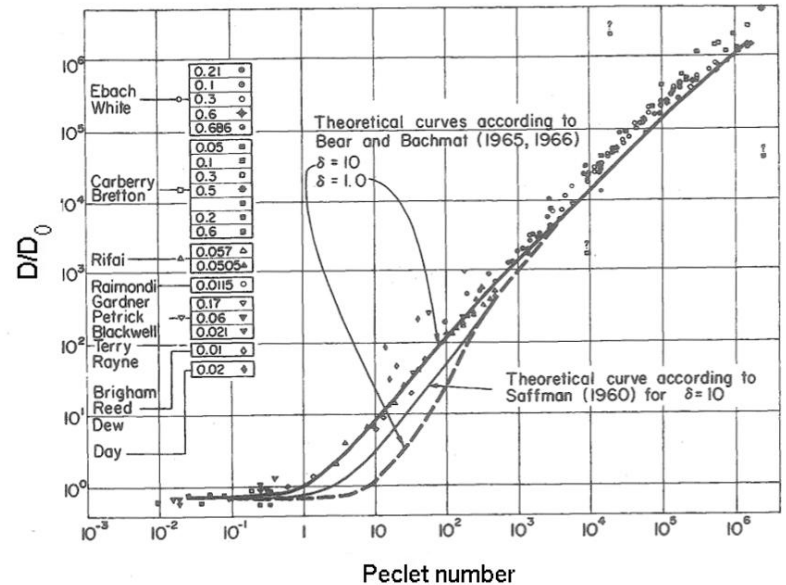
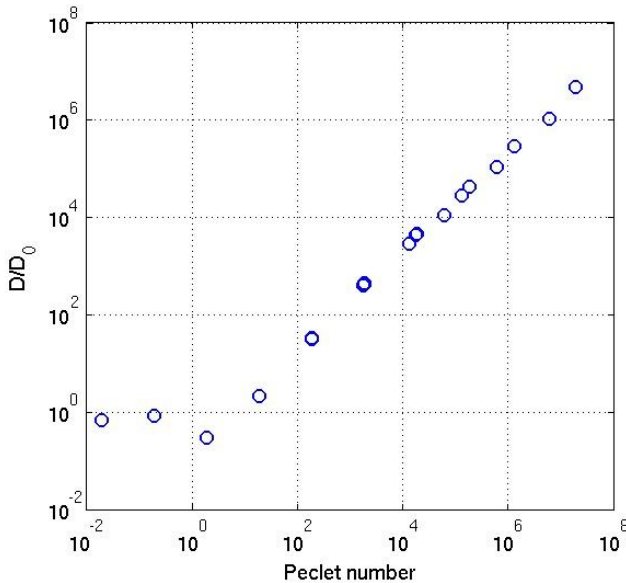
$$\eta_I = 3.377 As N_R^2 q^{0.145}$$

# CONCLUSIONS AND FUTURE WORK

## FULLY 3D PARTICLE TRANSPORT SIMULATIONS



Breakthrough curves fitting  $\longrightarrow$  Hydrodynamic dispersion  $D/D_0$  results



# CONCLUSIONS AND FUTURE WORK

## ACKNOWLEDGEMENTS

- AQUAREHAB (FP7, Grant Agreement no. 226565)
- PRIN Project 2008:  
“Disaggregazione, stabilizzazione e trasporto di ferro zerovalente nanoscopico”

*Thanks for your attention!*

*Any questions?*