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Room temperature plastic flow localization in a Mn-alloyed austenitic steel

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# Room Temperature Plastic Flow Localization in a Mn-Alloyed Austenitic Steel

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# Automotive Structural Steels (I)

*desired properties of automotive steel structures :*

*Lower weight* {  
*Lower fuel consumption*  
*Lower pollution emission (Euro 4 – 5 ...)*  
*Increase useful load (commercial vehicle)*  
*Lower cost*

*Increased safety* *Better crash energy absorption*



*Dent resistance of automotive body components*

# Automotive Structural Steels (II)

## ■ Current high-strength automotive steels:

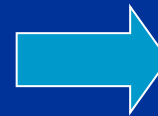
- HSLA (High Strength Low Alloy steel)
- Dual Phase
- TRIP (TRansformation Induced Plasticity)

## ■ Recently proposed:

- TWIP (TWinning Induced Plasticity)



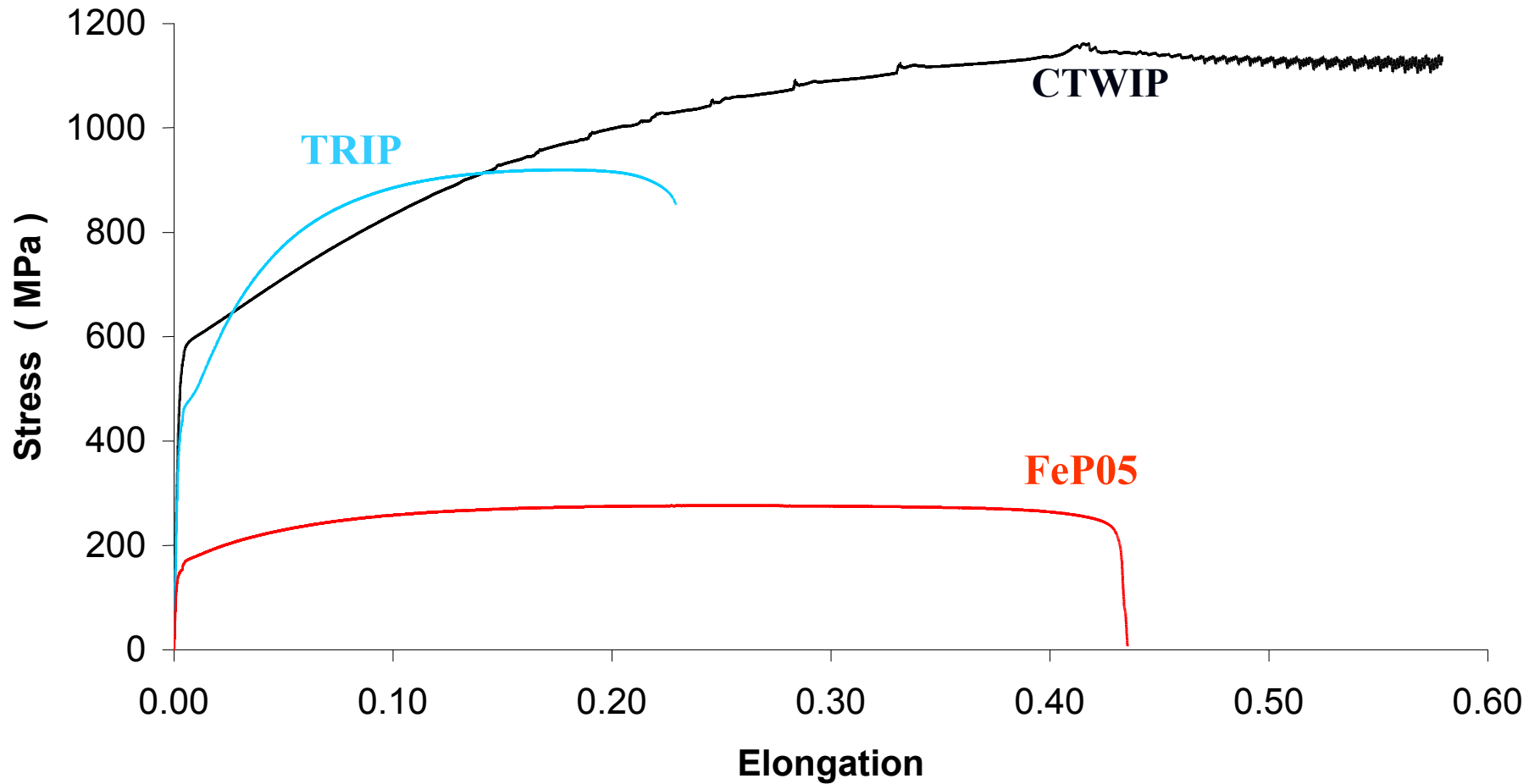
High strength  
High ductility  
High energy absorption



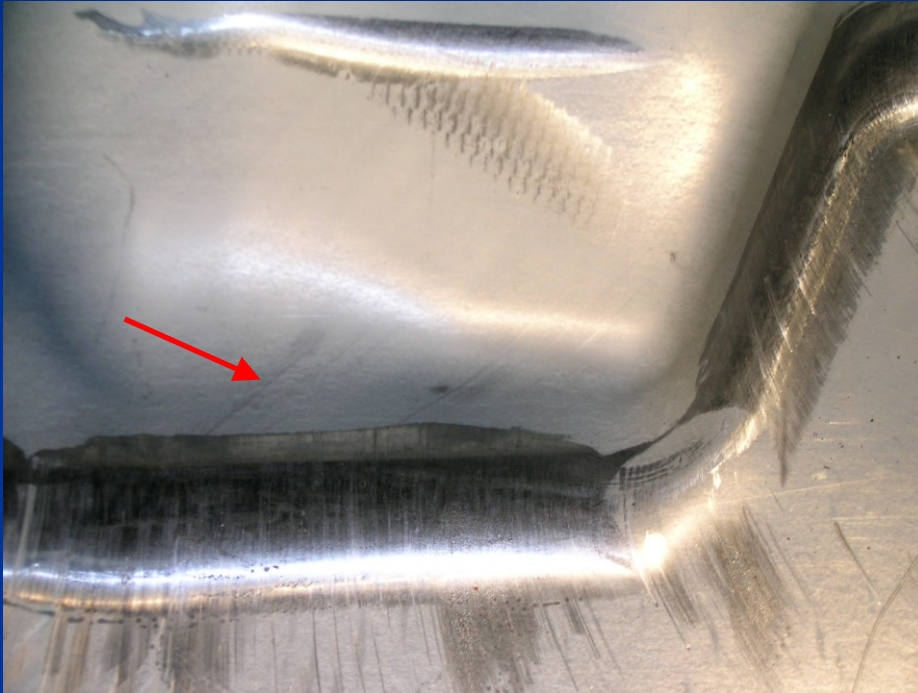
Examined here:  
medium-C TWIP steel  
**(CTWIP)**

# Automotive Structural Steels (III)

*typical tensile curves*



# Deep drawing



Localized deformation bands

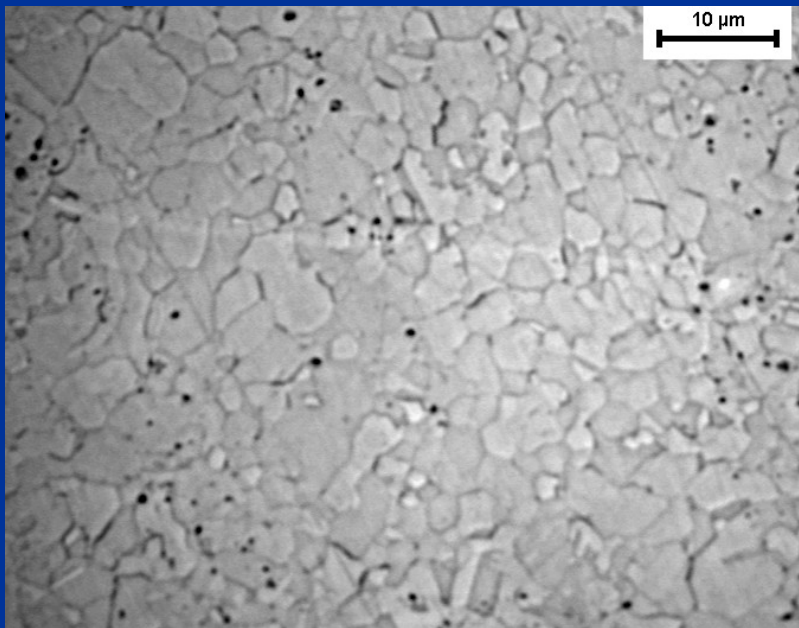
Aesthetic defect

# Examined CTWIP steel

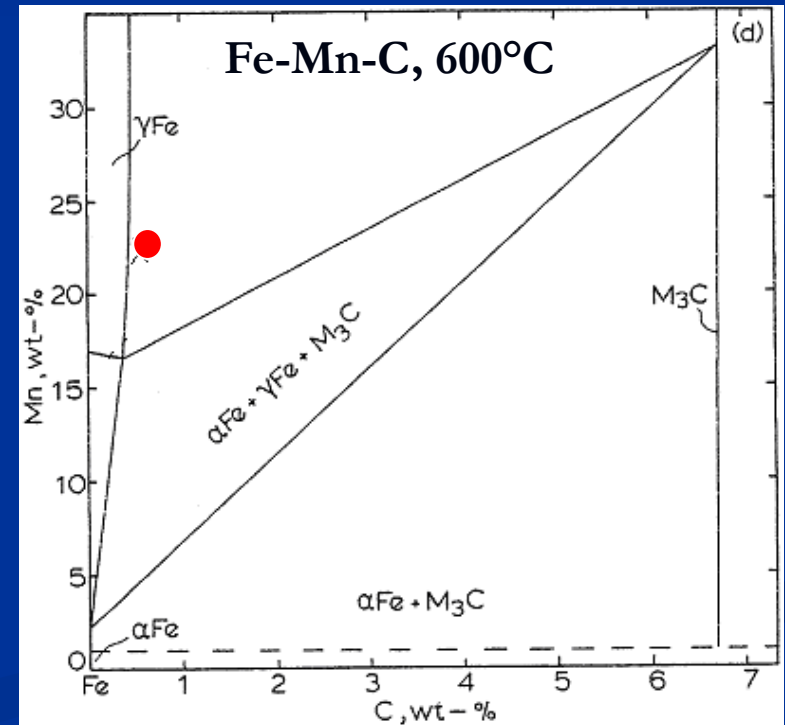
<i>steel</i>	<b>C</b>	<b>Mn</b>	<b>Ni</b>	<b>Si</b>	<b>Cr</b>	<b>P</b>	<b>S</b>	<b>V</b>	<b>Al</b>
CTWIP	<b>0.48</b>	<b>23.5</b>	<b>0.05</b>	<b>0.16</b>	<b>0.13</b>	<b>0.025</b>	<b>&lt;0.001</b>	<b>0.22</b>	<b>&lt;0.001</b>

**C:** increases YS and UTS

**Mn:** stabilizes austenite, decreases SFE ( $\rightarrow$  twinning)



average grain size = 2.5  $\mu\text{m}$



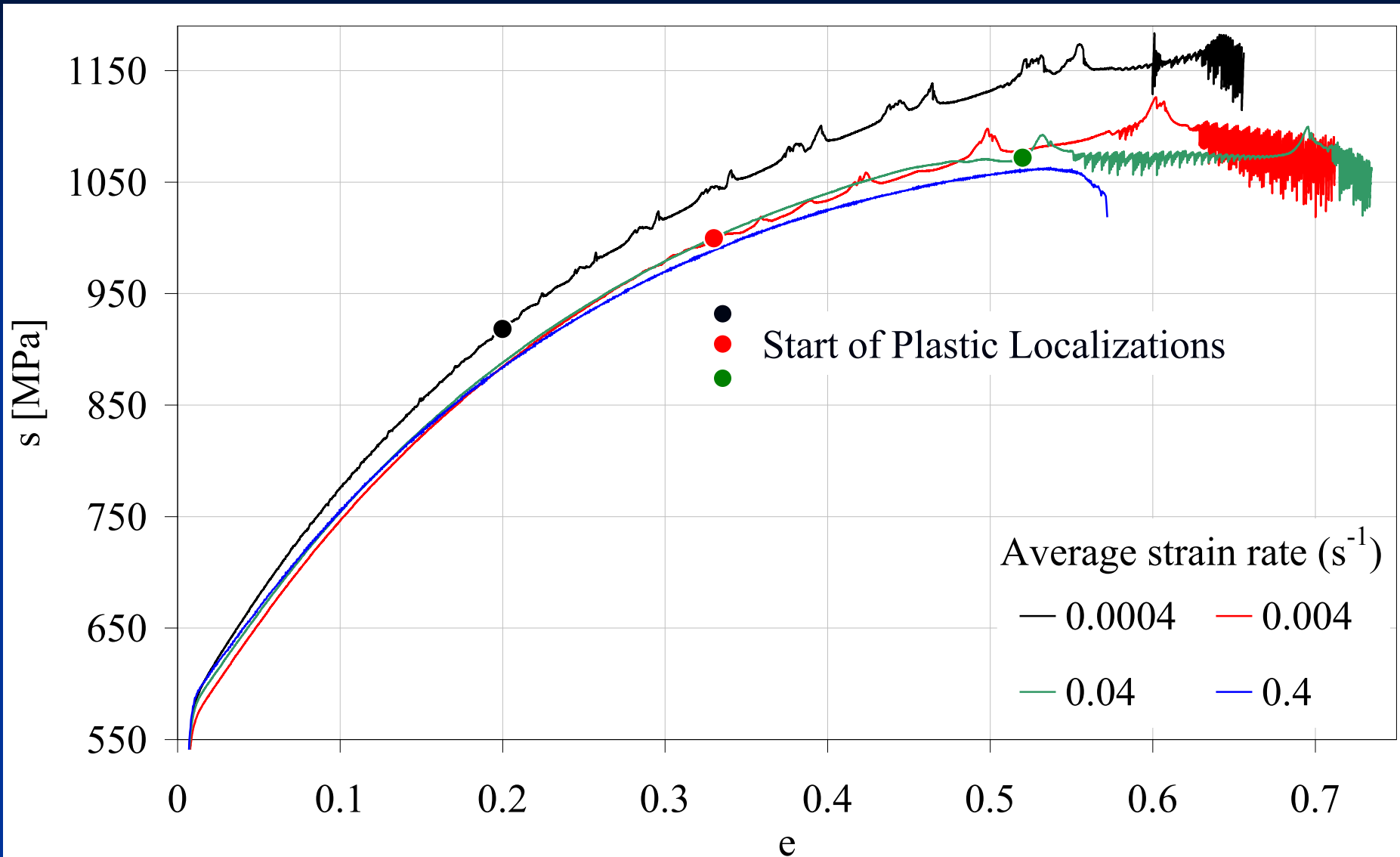
# Tensile test results

Cross-head speed	Strain rate (mean)	Yield strength	Tensile strength	Uniform elongation	Strain hardening exponent	$\epsilon_{PL}^*$
mm/s	s <sup>-1</sup>	MPa	MPa	%	-	-
0.06	0.0004	555	1180	65	0.35	0.2
0.5	0.004	540	1125	70	0.37	0.33
5	0.04	552	1100	72	0.37	0.52
40	0.4	557	1065	56	0.34	Not observed

$\epsilon_{PL}$ : strain at onset of Plastic Localization (PL)

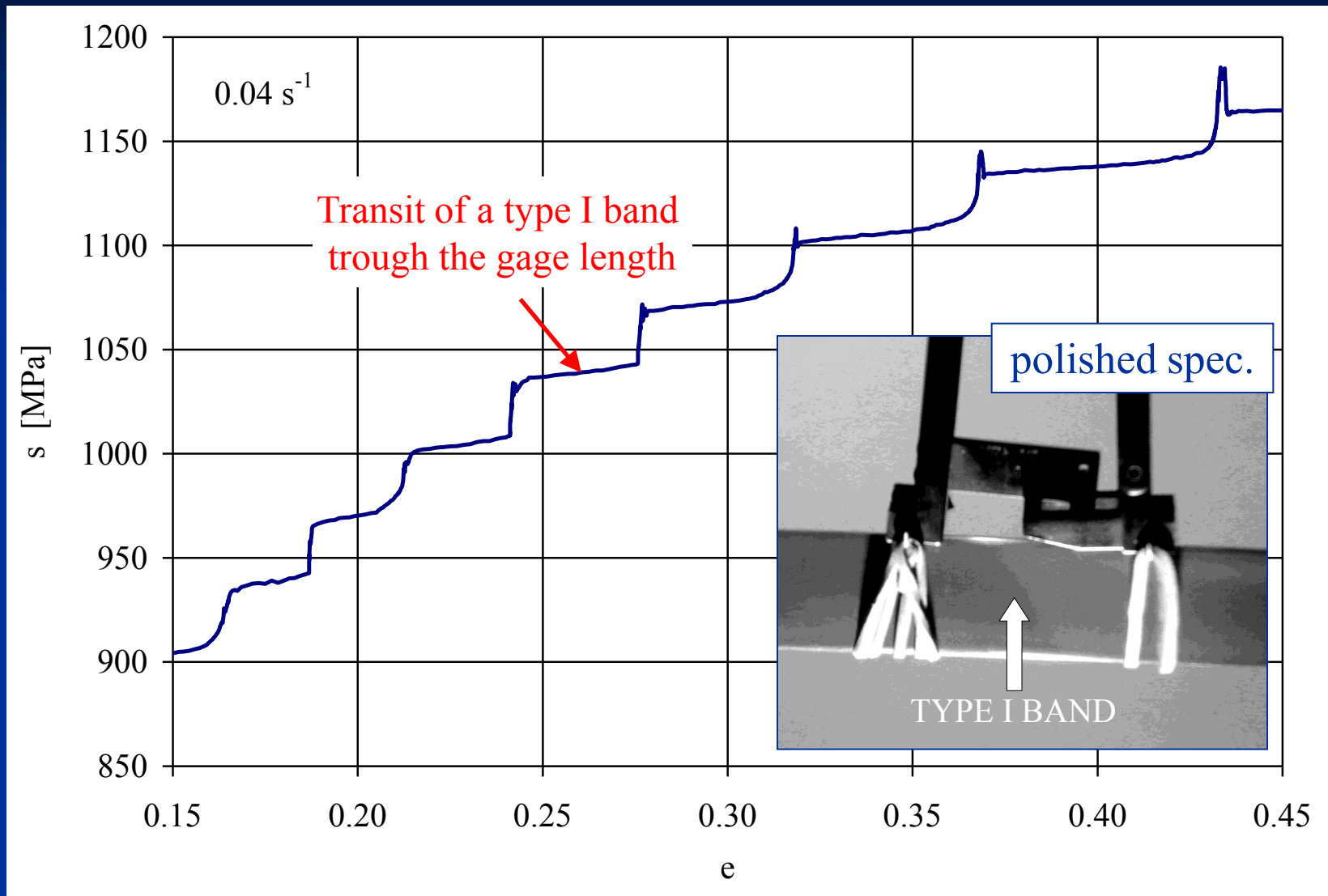


# Tensile Stress-Strain curves



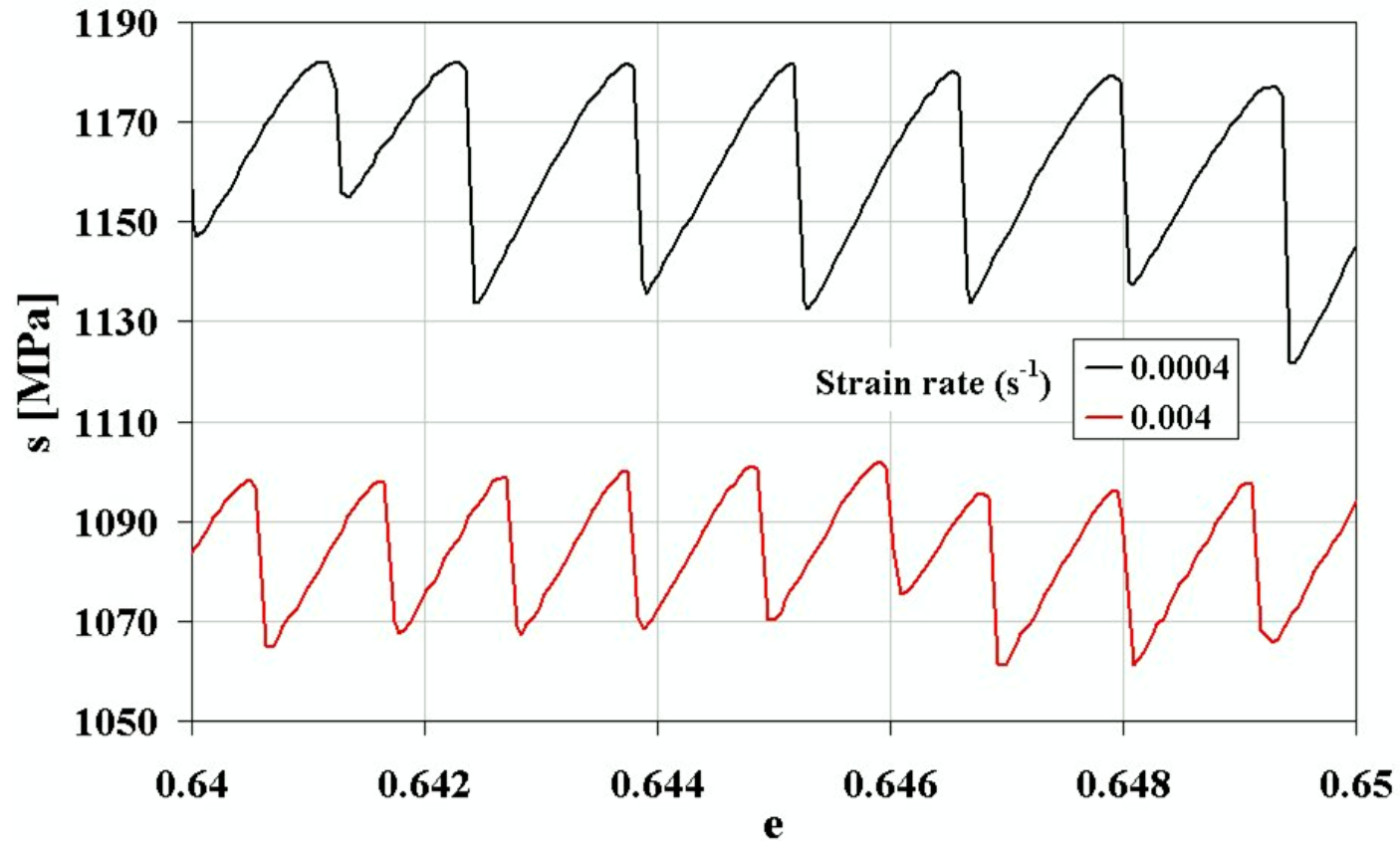
Strain calculated from the cross-head displacement

# Type I Plastic Localizations



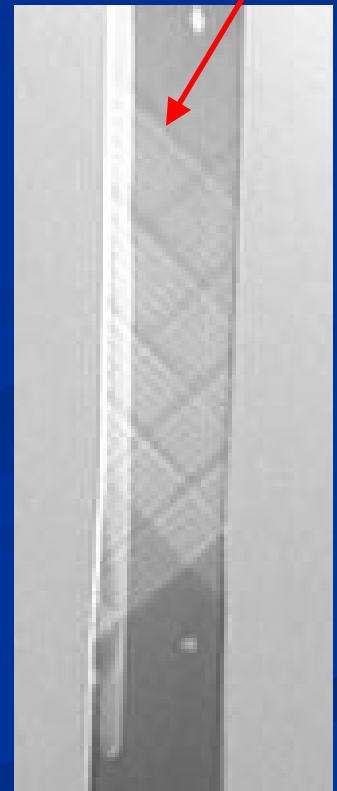
Strain calculated from the gage displacement

# Type II Plastic Localizations



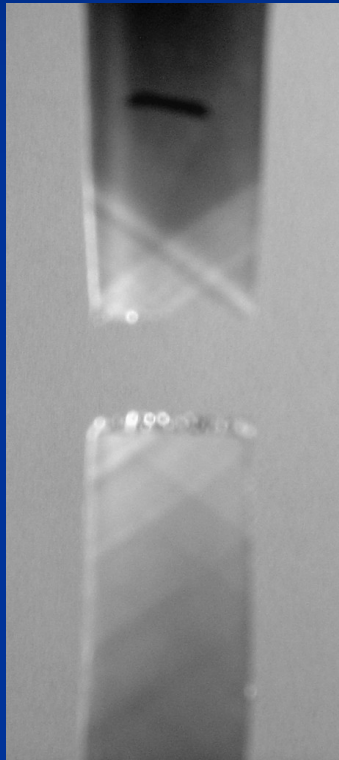
Strain calculated from the gage displacement

crossed type II stationary bands

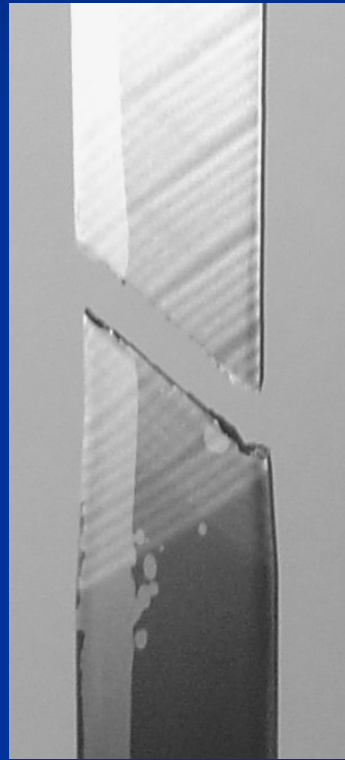


# Macroscopic Fracture Mode

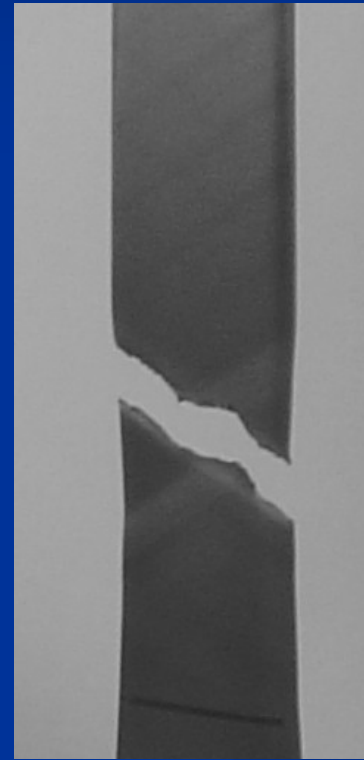
$0.0004 \text{ s}^{-1}$



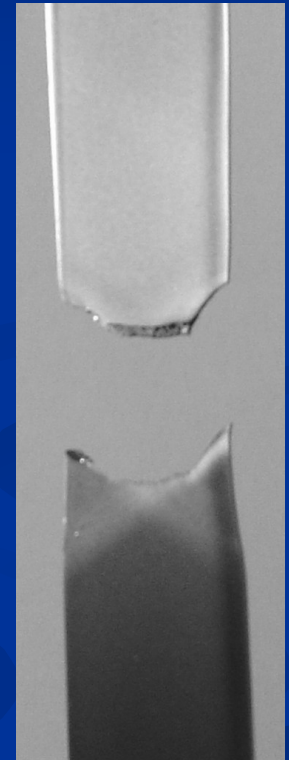
$0.004 \text{ s}^{-1}$



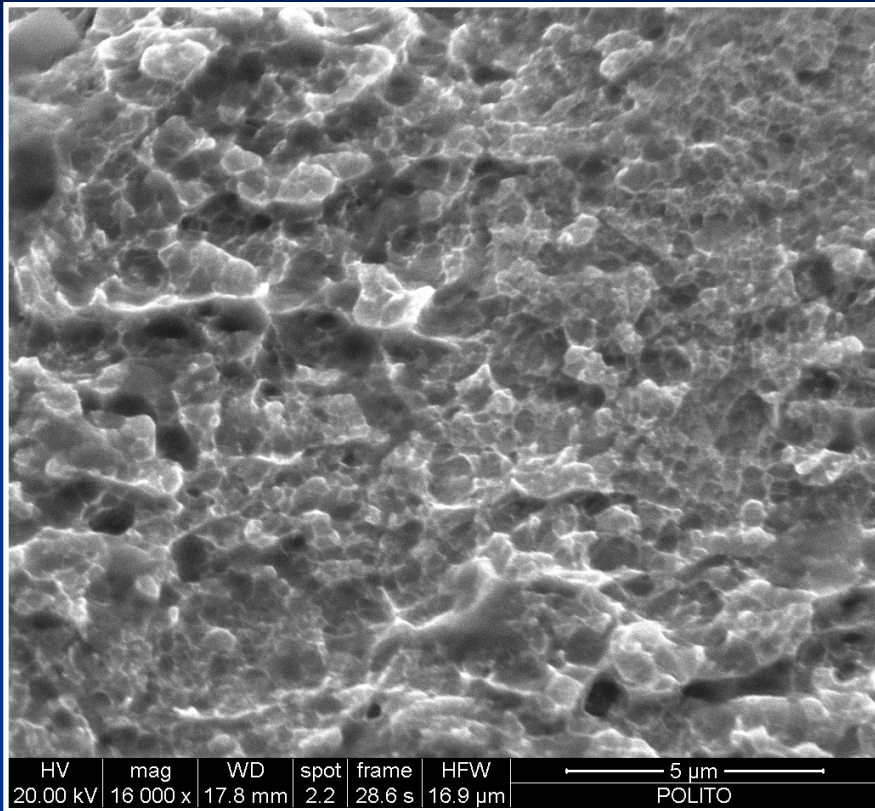
$0.04 \text{ s}^{-1}$



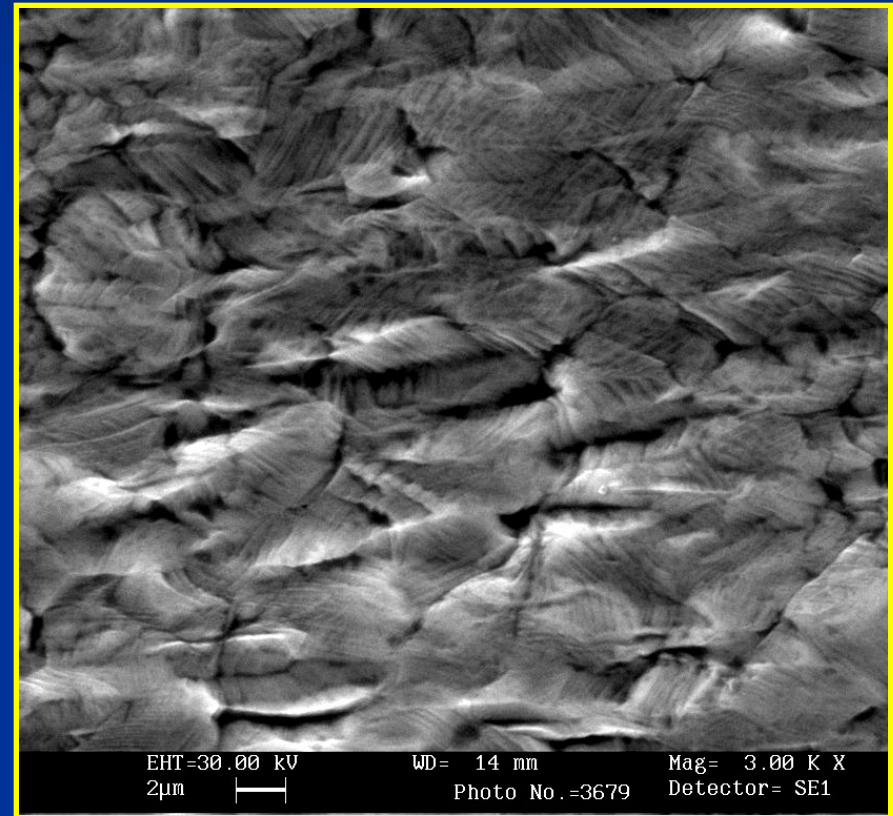
$0.4 \text{ s}^{-1}$



# SEM analyses

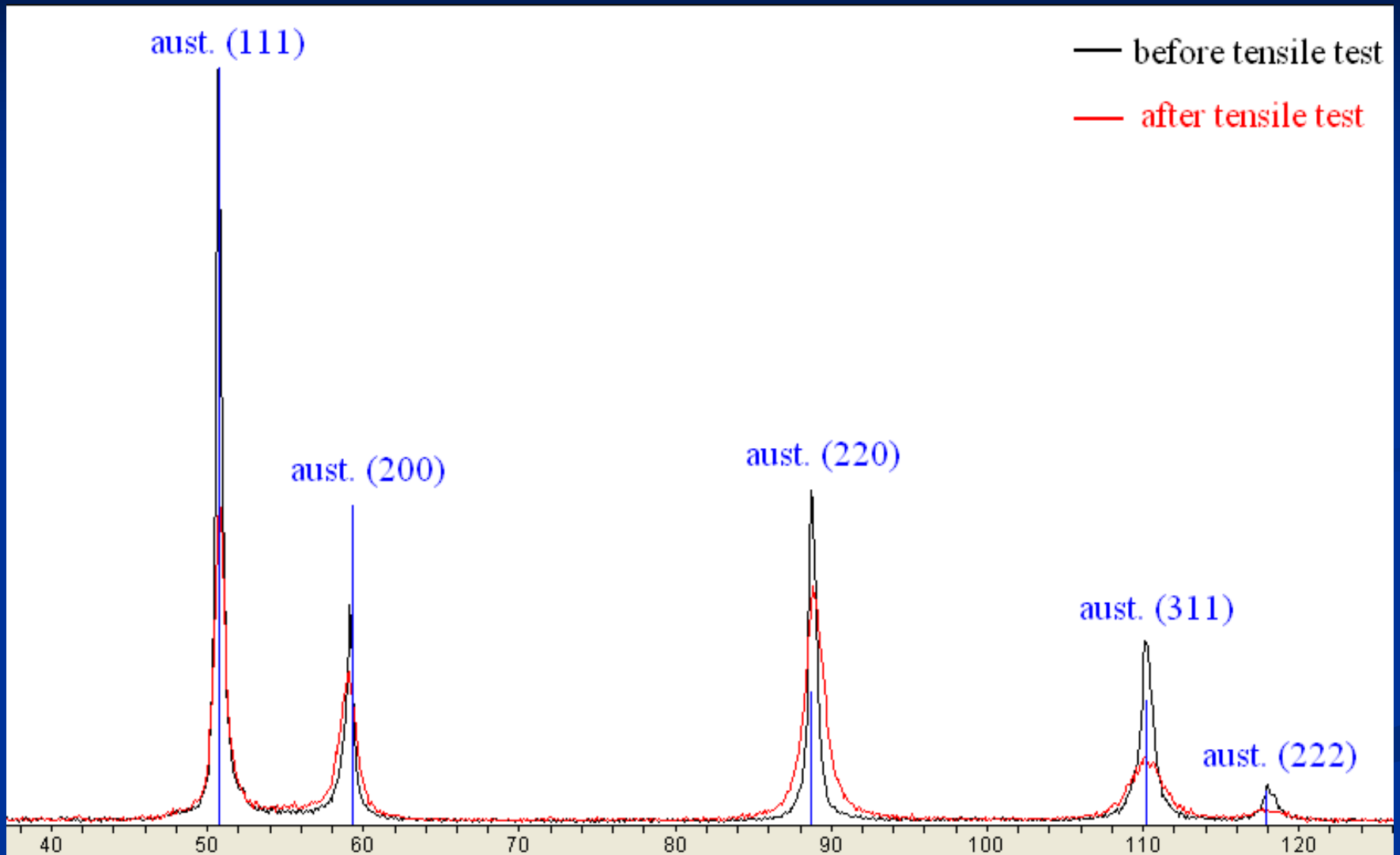


Fracture surface (microvoids)



Plastic deformation relief on the previously polished specimen surface

# X-Ray Diffraction



# Discussion - Portevin-Le Chatelier (PLC) Effect

- Plastic instabilities due to inhomogeneous plastic deformation
- occurring in limited strain-rate and temperature ranges
- due to a negative strain rate sensitivity
- in turn possibly due to Dynamic Strain Aging (DSA)

## Known band types:

- **A** : propagate continuously along the tensile axis
- **B** : oscillatory / intermittent propagation
- **C** : appear suddenly and do not propagate

# Conclusions

- The CTWIP steel exhibit a favorable combination of strength and ductility
- It also exhibit PLC effect at R.T. for strain rates less than  $0.4 \text{ s}^{-1}$
- Both type A and C (I and II herein) bands were observed
- This may arise from interactions between solute C atoms and mobile dislocations, yielding a negative strain rate sensitivity