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Milton S. Mery
Lehigh University

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A COMPUTER PROGRAM TO
CALCULATE SONIC VELOCITIES IN
TWO PHASE VAPOR-LIQUID SYSTEMS

by

MILTON S. MERY

A COMPUTER PROGRAM TO CALCULATE
SONIC VELOCITIES
IN TWO PHASE VAPOR-LIQUID SYSTEMS

by

Milton S. Mery

A THESIS

Presented to the Chemical Engineering
Department of Lehigh University
in Candidacy for the Degree
of Master of Science

Lehigh University
Bethlehem, Pennsylvania
1963

CERTIFICATE OF APPROVAL

This thesis is accepted and approved in partial
fulfillment of the requirements for the degree of
Master of Science in Chemical Engineering

Professor in Charge

Head of the Department

Date

ACKNOWLEDGEMENT

The author wishes to express his appreciation to Dr. Leonard A. Wenzel and Dr. Alan S. Foust for their assistance and guidance in the development of this report.

Appreciation is also acknowledged to The Patterson-Kelley Co., Inc. for the use of their computer.

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ABSTRACT

A Computer program was developed to calculate sonic velocity in the two phase region for a pure fluid using the Royal Mc Bee LGP 30 Digital Computer. This program was used to calculate sonic velocities for ten pressures at all qualities in increments of 10 per cent for Freon 12 and Freon 22. Figs 3 and 4 are plots of this data.

The purpose of this study is to investigate sonic velocity in two phase systems in order to determine whether a sonic choke exists at any intermediate qualities. For the range of pressures for which velocities were calculated no choke was found to be exhibited.

If a choke region does occur for the Freon 12 or Freon 22 systems, it appears from the shape of the isobars that it would exist at lower pressures than those investigated.

INTRODUCTION

It has been proposed that a limiting sonic velocity, or choke effect, may occur at some intermediate quality for a two phase vapor-liquid mixture (3). If a sonic choke does exist at some quality other than the expected saturated vapor condition, this information would be of significance in the design of many systems where the flow of two phase mixtures is encountered.

The purpose of this report is to present a general computer program for the calculation of sonic velocities within the two phase region from saturated vapor and liquid properties. It is also the specific purpose of this report to develop a sonic velocity curve for the two phase Freon 22 system. A similar curve for Freon 12 was also obtained for comparison with the earlier work of Vaillancourt (8).

THEORETICAL BACKGROUND

It is a well established fact that the limiting velocity for a fluid in flow through a duct of uniform cross section is the velocity of sound. This can be shown from thermodynamic principals by examining a Mollier diagram for a high velocity vapor.

Considering the pressure-enthalpy diagram in Fig. 1, assume that a superheated vapor at high pressure is flowing through a uniform duct at low velocity (point 1). As the vapor expands adiabatically, the change in enthalpy is described by the equation

$$dH = - \frac{U dU}{g_c}$$

$$\text{or } \Delta H = - \frac{(U_2^2 - U_1^2)}{2 g_c} = -\Delta KE$$

Initially, at low velocity, the change in enthalpy will be very small for a moderate change in pressure. However, as the pressure decreases and the volume increases, the increase in velocity becomes more rapid for a given change in pressure. Finally as the pressure becomes very low, a small pressure decrement results in a very large increment in volume, velocity and kinetic energy, so that the enthalpy drops rapidly (point 3).

The path of a typical adiabatic expansion is shown in Fig. 1 by the broken line. At point 2 the curve passes through a maximum value of entropy and the entropy decreases through the balance of the expansion process. Since there is no work done and no heat transfer, it is obvious that the minimum change possible in entropy is zero and therefore a maximum velocity is reached when the differential change in entropy becomes zero.

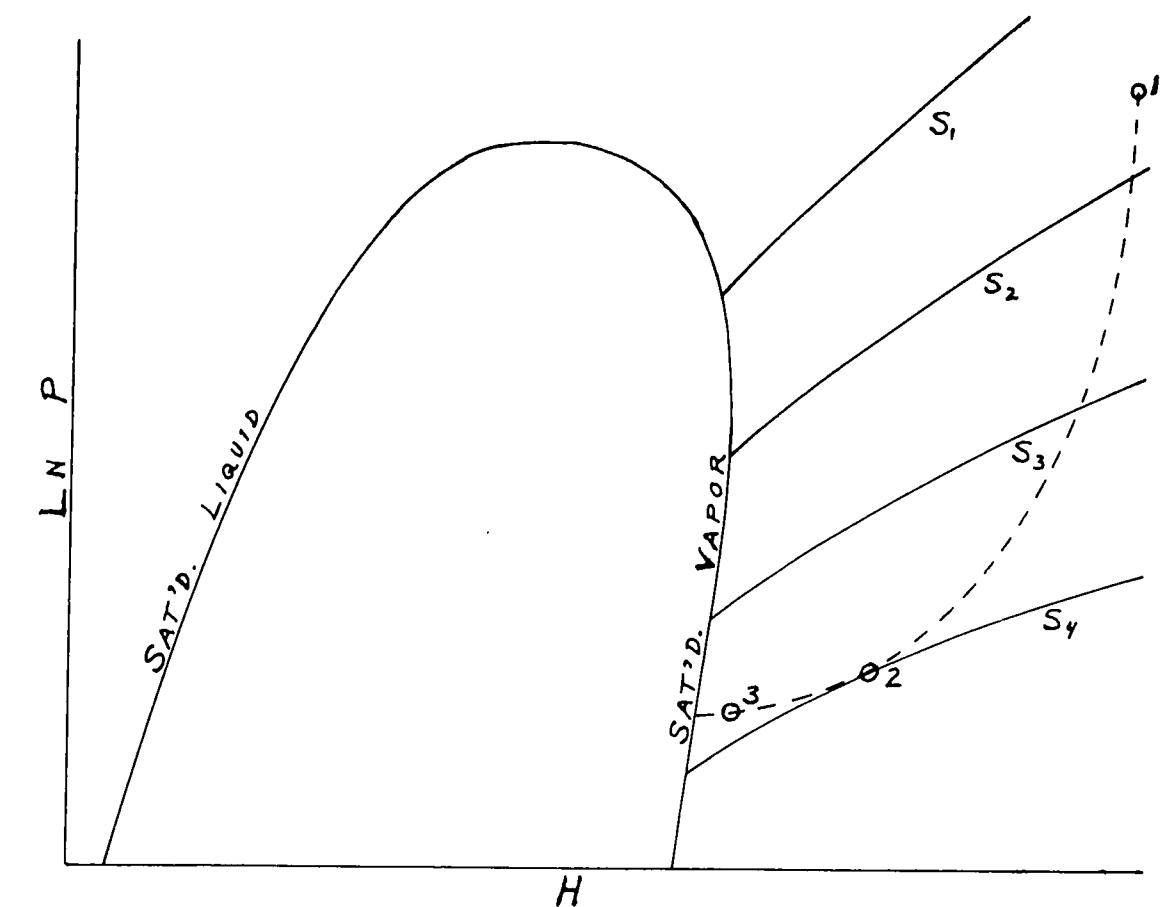


Figure 1 Mollier Diagram

By definition:

$$dH = dE + d(PV) = dE + PdV + VdP$$

But in the limit as the change in entropy approaches zero, a reversible process is being approached and $PdV = dW = 0$.

Since dE is zero for an ideal gas and $dH = -\frac{UdU}{g_c}$,

$$-\frac{UdU}{g_c} = VdP \quad (1)$$

Since the gas is flowing at a constant mass flow rate through a constant cross section,

$$dG = 0 = d\left(\frac{U}{V}\right)$$

$$\text{or } 0 = \frac{VdU - UdV}{V^2}$$

$$\text{or } dU = \frac{UdV}{V} \quad (2)$$

Substituting equation 2 into equation 1 we obtain,

$$-\frac{U^2}{g_c V} \frac{dV}{V} = V dP$$

Rearranging, and recalling that this applies only for the condition of constant entropy, which also is the necessary condition for maximum velocity, we have,

$$U_{Max}^2 = -g_c V^2 \left(\frac{\partial P}{\partial V} \right)_S$$

$$\text{or } G_{Max} = \sqrt{-g_c \left(\frac{\partial P}{\partial V} \right)_S}$$

This is the common equation for sonic velocity in fluid flow.

It applies strictly only to ideal gasses, since there was assumed to be no energy change for the adiabatic expansion. A second order term has been cited in the literature, however this has been assumed negligible (7).

This same equation is considered to hold true for liquids, where the isentropic compressibility of the fluid is very high and sonic velocities of the order of 5000 ft/sec. or 300,000 lbs./ft.²/sec. are considered typical (1 & 7). Since this is far above practical operating velocities, there has been very little interest in this region.

The two phase region has also lacked investigation in the past, since the assumption that the liquid volume is negligible compared to the vapor volume for most qualities of vapor leads people to assume that maximum velocity can be approximated by considering only the vapor velocities.

Since little work has been done on two phase fluids, and since there has been some reason to predict unexpectedly low maximum velocities

in this region, a study of the sonic velocities of vapor-liquid mixtures might prove profitable at this time.

COMPUTER PROGRAM

Discussion

A program was developed for the Royal McBee LGP-30 digital computer to calculate the velocity of sound for a vapor-liquid mixture. The program requires as input five values of saturated liquid and vapor enthalpy, entropy and specific volume with the corresponding pressures. Any number of pressures up to ten for which it is required to calculate sonic velocities may also be read in as input.

From the input data coefficients are calculated for a fourth order polynomial to solve for the saturated liquid and vapor properties at any pressure. A semi-log polynomial is used for the liquid properties and log-log for vapor properties.

After calculating the coefficients, headings are printed and the first isobar for which velocities are to be obtained is generated. The specific volume and entropy of saturated liquid and vapor are calculated for the isobar (P) and also for .975 times this pressure (P_1) and 1.025 times this pressure (P_2).

Setting the quality equal to zero, the entropy is calculated using the equation:

$$S_Q = Q S_V + (1-Q) S_L$$

at P . The quality at P_1 for which the mixture has the same entropy, S_Q , is obtained by rearranging the above equation to

$$Q_1 = \frac{S_Q - S_{L1}}{S_{V1} - S_{L1}}$$

From this value the specific volume for the mixture at P_1 is calculated from

$$V_{Q1} = Q_1 V_{V1} + (1-Q_1)V_{L1}$$

The same equations are repeated for P_2 except that at 0% and 100% quality the specific volume is calculated for P , since Q_2 would become negative and greater than 100% respectively

Since two values of pressure and the corresponding values of specific volume are now available, the equation

$$G_{Max} = \sqrt{-g_c \left(\frac{\partial P}{\partial V} \right)_s}$$

may be used in difference form

$$G_{Max} \approx 68.07 \sqrt{-\left(\frac{P_2 - P_1}{V_2 - V_1} \right)_s}$$

to calculate the sonic velocity at P and Q . The average mixture properties and the fictitious linear velocity, V_{max} , are calculated and the data are printed out.

The quality is increased by 10% and the calculations repeated for this new point. When the 100% quality point is completed, this procedure is repeated for the next isobar. When the last results are printed out for the last isobar, the computer will stop at break point 16, at which point one additional isobar may be entered. The computer always finishes at break point 16 so that an additional isobar may be read in at any time.

Reasonably accurate results have been obtained using this program to develop sonic velocity curves for Freon 12 and Freon 22. The critical step in this program is in obtaining constants for the

polynomial for the physical properties.

For this purpose the Curve Fit Subroutine on page 68 of the appendix was written. It is important to note that this is not a true curve fit, but so titled for lack of a more descriptive term. This routine solves for the coefficients of a fourth order polynomial and therefore requires smoothed data. The routine also has the obvious limitation that if care is not used in the choice of data points, excessive fluctuation will occur in the resulting polynomial.

In order to check the choice of data points, a subroutine is included in the main program to calculate the coefficients and from these to calculate properties at any pressure to compare with published data. A description of this routine is given beginning on page 104 of the appendix.

DESCRIPTION OF PROGRAM

Function:

To compute the sonic velocity of a mixture of saturated vapor and liquid for various pressures and vapor qualities. (a)

Input:

5 reference pressures followed by the corresponding values of saturated liquid and vapor enthalpy in sequence in locations 6100 through 6114 followed by an exit code. 5 reference pressures followed by the corresponding values of saturated liquid and vapor entropy in 6115 through 6129 followed by an exit code. 5 reference pressures followed by the corresponding values of saturated liquid and vapor specific volume in 6130 through 6144 and up to 10 pressures starting in 6146 for which it is required to calculate sonic velocities. An exit code at this point completes the input data. (See sample data load sheets, pgs. 118 to 121).

Operation:

Halt and transfer to 4200 with data tape in reader. Depress break point 4 if there is no error on the data tape. Depress break point 8 when ready for print out. When the calculations and print out are completed the computer stops at break point 16. At this point an additional pressure may be entered in 6146. An exit code will result in computing sonic velocities at this pressure.

(a) See pgs. 104 to 106 of Appendix for the function of the routine for checking the curve fit of the data points.

Output:

P, Q, H, V, S, G_{max} and V_{max} for 0% to 100% quality at increments of 10% for each pressure read into 6146 to 6155. These values will also be printed out for each additional pressure read into 6146.

Storage:

Locations 4200 through 5454

Temporary storage in 5900 through 6162

Program Stops:

4434 - No pressures read into 6146 to 6155

4029 - Constant or Y value for polynomial too large to hold
at q : 12.

Subroutines:

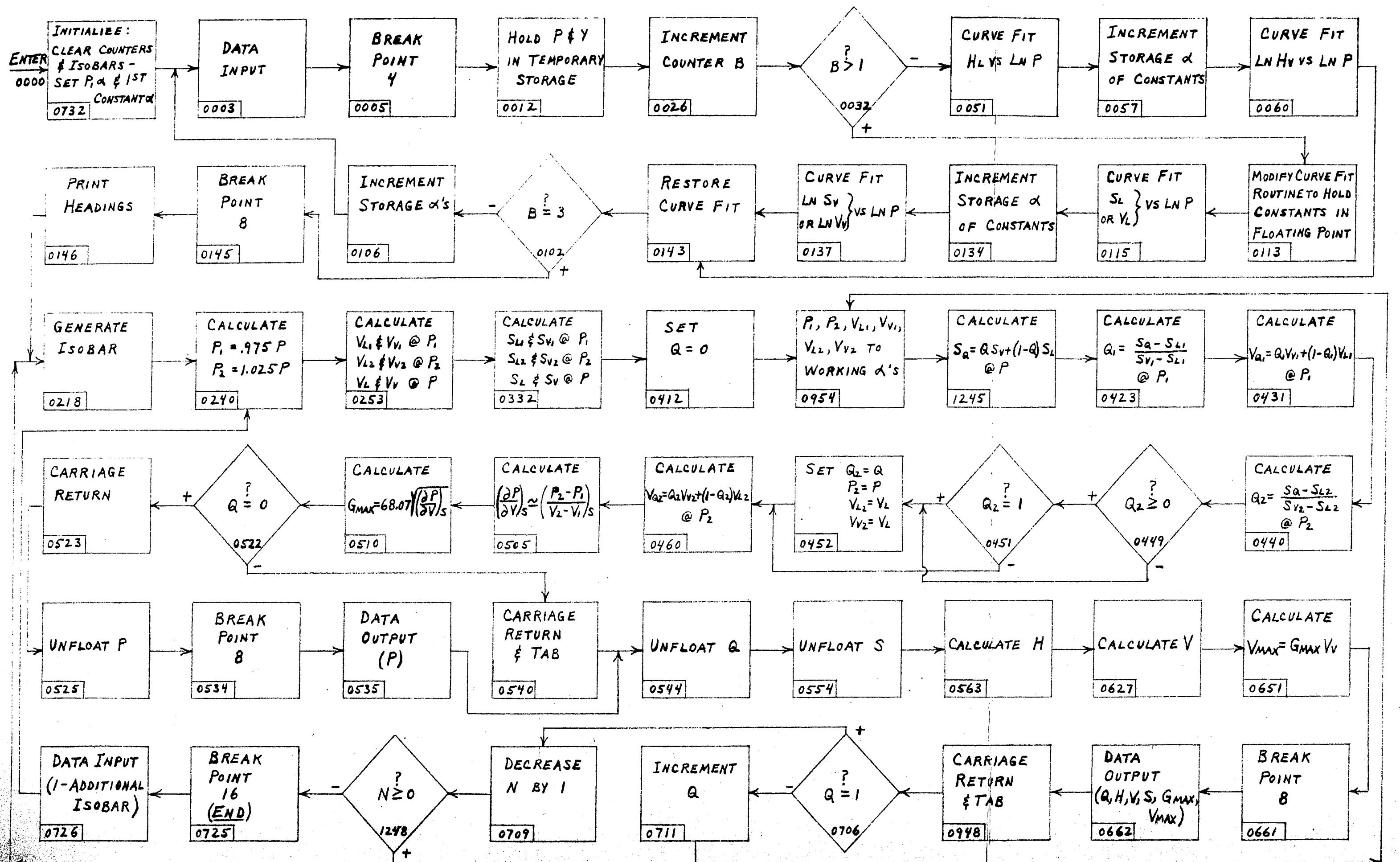
Data Input Routine #3	(11.2)	0300 to 0563
Data Out put Routine #2	(12.1A)	0600 to 0850
Extended Range Floating Point		
Interpretive Routine	(24.1)	0900 to 1963
Curve Fit		2000 to 3316
Data Output Driver		3332 to 3363
Logarithm	(18.2)	3419 to 3463
Exponential	(17.2)	3500 to 3663
Alphanumeric	(19.0)	3700 to 3757
Float and Unfloat	(25.1)	3800 to 4143
Decimal Memory Print Out	(21.0)	5500 to 5863

Time:

Approximately two hours for first print-out.

Approximately twenty minutes for each additional isobar.

FIGURE 2

SONIC VELOCITY - BLOCK DIAGRAM

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SONIC VELOCITY

PROGRAM INPUT CODES	LOCATION	INSTRUCTION		CONTENTS OF ADDRESS	NOTES
		OPERATION	ADDRESS		
0004200					
		0000	U0730		INITIALIZE
		01	B0914	α OP "α" FOR H _L VS LN P (0750)	
		02	H0850		
		03	XR0308	DATA	(0112)
		04	XU0300	} INPUT	
		05	XZ0400		
		06	B0849	P ₁ α	
		07	Y0012	α	
		08	B0913	P ₁ TEMP. α	
		09	Y0013		
		10	A0905	10 @ 29	
		11	Y0014	α	
		12	BL J	P's & Y's @ 12	(0043)
		13	HL J		
		14	HL J		
		15	B0825	α COUNTER A	
		16	A0900	1 @ 29	
		17	H0825	COUNTER A	
		18	S0904	5 @ 29	
		19	T0034	α	
		20	S0904	5 @ 29	
		21	T0044		
		22	S0900	1 @ 29	
		23	T0047	α	
		24	S0903	4 @ 29	
		25	T0034		
		26	XG6300		
		27	C0825	α COUNTER A	
		28	B0826	COUNTER B	
		29	A0900	1 @ 29	
		30	H0826	COUNTER B	OURCE 100
		31	S0904	2 @ 29	LJ M100 L100

P-16

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 CARRIAGE PICTURE

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SONIC VELOCITY

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SONIC VELOCITY

PROGRAM INPUT CODES	LOCATION	INSTRUCTION		STOP CODE	CONTENTS OF ADDRESS	NOTES
		OPERATION	ADDRESS			
		X				
	0 1 3 2	X E 0 0 0 0				
	3 3	X U 2 8 3 8				
	3 4	B 0 8 5 0	"a" &			(0121)
	3 5	A 0 9 0 4	X 5 @ 29			
	3 6	H 0 8 5 0	"a" &			
	3 7	B 0 9 0 0	1 @ 29			
	3 8	X H 3 3 0 3	FLAG			
	3 9	B 0 8 3 9	X P,			CURVE FIT
	4 0	B 0 8 5 0	"a"			LN Sv OR LN Vv
	4 1	X R 2 8 5 5				VS LN P
	4 2	X U 2 0 0 0				
	4 3	B 0 1 3 2	X E 0 0 0 0			
	4 4	U 0 9 3 6				
	4 5	X Z 0 8 0 0	B, P, 8			(0108)
	4 6	X R 3 7 0 0				ALPHANUMERIC
	4 7	X U 3 7 0 0	X			
0 0 0 0 0 3 4	4 8 2 0 1 0 4 2 0 6	CR, UC, P, SPACE				
	4 9 4 J 4 2 7 F 2 2	(, P, S, I				
	5 0 7 2 0 4 3 0 7 4	A), TAB, G				
	5 1 0 6 4 J 2 J 0 6	X SPACE, (, %, SPACE				
	5 2 3 A 0 0 7 2 4 2	V, LC, A, P				
	5 3 4 6 1 F 1 0 0 4	O, R, UC,)				
	5 4 3 0 6 2 0 6 4 J	TAB, H, SPACE, (
	5 5 0 F 5 F 5 2 0 8	X B, T, U, LC				
	5 6 2 6 1 0 0 J 0 8	/, UC, L, LC				
	5 7 0 F 1 0 0 4 3 0	B, UC,), TAB				
	5 8 3 A 0 6 4 J 6 F	V, SPACE, C, C				
	5 9 0 8 5 2 0 6 1 0	X Lc, U, SPACE, UC				
	6 0 5 4 0 0 5 F 2 6	F, LC, T, /				
	6 1 1 0 0 J 0 8 0 F	UC, L, LC, S				
	6 2 1 0 0 V 3 0 7 F	UC,), TAB, S				
	6 3 0 6 4 J 0 F 5 F	X SPACE, (, B, T				
		X CARRIAGE RETURN				

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SONIC VELOCITY

CONDITIONAL STOP CODE

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A small graphic icon representing a carriage return, consisting of a square with a diagonal cross.

CARRIAGE RETURN

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SONIC VELOCITY

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A small graphic element consisting of a square with a diagonal cross through it, representing a carriage return or end-of-line character.

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1		2		3		4		5		6		7		8		9		10		11		12		13		14		15		16		17		18		19		20		21		22		23		24		25		26		27		28		29		30		31		32		33		34		35		36		37		38		39		40		41		42		43		44		45		46		47		48		49		50		51		52		53		54		55		56		57		58		59		60		61		62		63		64		65		66		67		68		69		70		71		72		73		74		75		76		77		78		79		80		81		82		83		84		85		86		87		88		89		90		91		92		93		94		95		96		97		98		99		100	
1		2		3		4		5		6		7		8		9		10		11		12		13		14		15		16		17		18		19		20		21		22		23		24		25		26		27		28		29		30		31		32		33		34		35		36		37		38		39		40		41		42		43		44		45		46		47		48		49		50		51		52		53		54		55		56		57		58		59		60		61		62		63		64		65		66		67		68		69		70		71		72		73		74		75		76		77		78		79		80		81		82		83		84		85		86		87		88		89		90		91		92		93		94		95		96		97		98		99		100	
1		2		3		4		5		6		7		8		9		10		11		12		13		14		15		16		17		18		19		20		21		22		23		24		25		26		27		28		29		30		31		32		33		34		35		36		37		38		39		40		41		42		43		44		45		46		47		48		49		50		51		52		53		54		55		56		57		58		59		60		61		62		63		64		65		66		67		68		69		70		71		72		73		74		75		76		77		78		79		80		81		82		83		84		85		86		87		88		89		90		91		92		93		94		95		96		97		98		99		100	
1		2		3		4		5		6		7		8		9		10		11		12		13		14		15		16		17		18		19		20		21		22		23		24		25		26		27		28		29		30		31		32		33		34		35		36		37		38																																																																																																																													

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SONIC VELOCITY

INPUT CODES	S O R T	LOCATION	INSTRUCTION		STOP	CONTENTS OF ADDRESS	NOTES
			OPERATION	ADDRESS			
.	.						
.	X						
0 5	3 2		X E 0 0 1 2				
3 3			X H 6 1 5 6			P @ 12	
3 4			X E 0 8 0 0			B.P. 8	
3 5			X B 6 1 5 6		X	P @ 12	
3 6			X R 0 6 0 5				
3 7			X U 0 6 0 0				{ DATA
3 8			X E 0 1 1 2				OUTPUT
3 9			V 0 5 4 4		X		
4 0			X P 1 6 0 0				} C.R.
4 1			X E 0 0 0 0				
4 2			X P 2 4 0 0				} TAB
4 3			X E 0 0 0 0		X		
4 4			X R 0 9 0 0				} ERFP
4 5			X U 0 9 0 0				
4 6			8 0 X B 5 9 6 2			Q	
4 7			X E 0 0 0 0		X		
4 8			X R 3 8 5 1				
4 9			X U 4 0 0 8				
5 0			X E 0 9 0 0				
5 1			X E 0 0 0 1		X		
5 2			M 0 9 3 3			100 @ 11	
5 3			X H 6 1 5 7			Q @ 12	
5 4			X R 0 9 0 0				} ERFP
5 5			X U 0 9 0 0		X		
5 6			8 0 X B 6 0 0 0			S _a	
5 7			X E 0 0 0 0				
5 8			X R 3 8 5 1				
5 9			X U 4 0 0 8		X		
6 0			X E 0 9 0 0				
6 1			X E 0 0 1 2				
6 2			X H 6 1 6 0			S @ 12	
6 3			X B 6 1 5 6		X	P @ 12	

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SONIC VELOCITY

INPUT CODES	STOP	LOCATION	INSTRUCTION		STOP	CONTENTS OF ADDRESS	NOTES
			OPERATION	ADDRESS			
0 6 0 0		X C 6 2 6 2					SET FLAG @ 0
0 1		X C 3 3 0 3					
0 2		U 0 6 0 3					
0 3		X B 5 9 0 0			X	"a"	
0 4		X R 3 2 3 1					SOLN OF POLY
0 5		X U 3 1 3 2					
0 6		H 0 8 5 9				H L @ 12	
0 7		X B 6 1 5 6			X	P @ 12	
0 8		X C 6 2 6 2					
0 9		B 0 9 0 0				I @ 29	
1 0		X C 3 3 0 3				FLAG	
1 1		X B 5 9 0 5			X	"a"	
1 2		X R 3 2 3 1					SOLN OF POLY
1 3		X U 3 1 3 2					
1 4		H 0 8 6 0				H v @ 12	
1 5		X B 6 1 5 7			X	Q @ 12	
1 6		D 0 9 3 3				100 @ 11	
1 7		H 0 8 6 1				Q @ 1	
1 8		M 0 8 6 0				H v @ 12	
1 9		D 0 9 3 0			X	I @ 1	
2 0		H 0 8 5 1			X	Q H v @ 12	
2 1		B 0 9 3 0				I @ 1	
2 2		S 0 8 6 1			X	Q @ 1	
2 3		M 0 8 5 9			X	H L @ 12	
2 4		D 0 9 3 0				I @ 1	
2 5		A 0 8 5 1			X	Q H v @ 12	
2 6		X H 6 1 5 8				H @ 12	
2 7		X B 6 1 5 6			X	P @ 12	
2 8		X C 6 2 6 2					SET FLAG @ 0
2 9		X C 3 3 0 3					
3 0		X B 5 9 2 0			X	"a"	
3 1		X R 3 2 3 1			X		SOLN OF POLY

CARRIAGE RETURN

= CONDITIONAL STOP CODE

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CARRIAGE RETURN

PROGRAM NO.		PROGRAM PREPARED BY:		PROGRAM CHECKED BY:	
1	2	3	4	5	6
SONIC VELOCITY					
SOLN OF POLY					
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LGP-30 CODING SHEET

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SONIC VELOCITY

INPUT CODES	STOP	LOCATION	INSTRUCTION		STOP	CONTENTS OF ADDRESS	NOTES
			OPERATION	ADDRESS			
			XU0600				
		0 1	XZ0412				
		0 2	XZ0214				
		0 3	U0948		X		
		0 4	D0933	100@11 (Q@1)			(0953)
		0 5	S0930	1@1			
		0 6	T0711				
		0 7	XP1600		X	C.R	
		0 8	XZ0000				
		0 9	XB5930	N@29			
		1 0	U0719				
		1 1	A0935		X	1.1@1	(0706)
		1 2	XR3816				
		1 3	XU3800				FLOAT NEW Q
		1 4	XZ0900				
		1 5	XZ0001		X		
		1 6	XR0900				ERFP
		1 7	XU0900				
		1 8	U0413				
		1 9	S0900		X	1@29	(0710)
		2 0	XH5930	N@29			
		2 1	U1247				
		2 2	A0909		X	6145	(1250)
		2 3	Y0225		X		
		2 4	U0225				
		2 5	XZ1600	B.P. 16			(1248)
		2 6	XR0308				DATA
		2 7	XU0300		X	INPUT	! ADDITIONAL ISOBAR
		2 8	XB6146				
		2 9	U0226				
		3 0	XG6300				(0000)
		3 1	G0825		X	COUNTER A	

= CONDITIONAL STOP CODE

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CARRIAGE RETURN

CARRIAGE RETURN

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SONIC VELOCITY

INPUT CODES	LOCATION	INSTRUCTION		STOP	CONTENTS OF ADDRESS	NOTES
		OPERATION	ADDRESS			
		X				
0 8 0 0	B 0 8 2 8				COUNTER D	
0 1	A 0 9 0 0				1@ 29	
0 2	H 0 8 2 8				COUNTER D	
0 3	S 0 9 0 4				X 5@ 29	
0 4	T 0 8 1 0					
0 5	B 0 9 1 6				X U 3 2 1 3	
0 6	X H 3 2 4 9					
0 7	B 0 9 1 7				X V 0 8 1 7	MODIFIED
0 8	X H 3 2 2 6					SOLN OF POLY
0 9	U 0 9 4 1					
1 0	B 0 7 6 1					(0804)
1 1	A 0 9 0 1				X 2@ 29	
1 2	Y 0 7 6 1					
1 3	B 0 7 6 2					
1 4	A 0 9 0 1				X 2@ 29	
1 5	Y 0 7 6 2				X	
1 6	U 0 7 5 9					
1 7	B 0 9 1 8				X U 3 2 3 9	(X 3 2 2 6)
1 8	X H 3 2 4 9					
1 9	B 0 9 1 9				X R 3 8 5 1	
2 0	X C 3 2 2 6					
2 1	C 0 8 2 8				COUNTER D	
2 2	X R 0 9 0 0				{ ERFP	
2 3	X U 0 9 0 0				X	
2 4	U []				EXIT	
2 5	[]				COUNTER A	
2 6	[]				COUNTER B	
2 7	[]				X COUNTER C	
2 8	[]				COUNTER D	
2 9	[]				P ₁ @ 12	
3 0	[]				P ₂ @ 12	
3 1	[]				X P ₁ @ 12	

= CONDITIONAL STOP CODE

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CARRIAGE RETURN

X CARRIAGE RETURN

PROGRAM NO.		PROGRAM PREPARED BY:		PROGRAM CHECKED BY:	
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P.E. P.I.		TICKET NO. 00000000000000000000000000000000		NAME OF THE PERSON		ADDRESS		PHONE NUMBER		E-MAIL ID	
P.P. FORM		NAME		MATERIAL TESTED		TESTS PERFORMED		TEST RESULTS		REMARKS	
12		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
P.P. FORM		NAME		MATERIAL TESTED		TESTS PERFORMED		TEST RESULTS		REMARKS	
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41		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
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43		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
44		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
45		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
46		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
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52		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
53		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
54		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
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63		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
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72		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
73		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
74		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
75		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
76		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
77		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
78		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
79		SRI LAKSHMI		COTTON		PHYSICAL TEST		OK		<input checked="" type="checkbox"/>	
80		SRI LAKSHMI		COTTON		PHYSICAL TEST					

LGP-30 CODING SHEET

PAGE OF
21 / 29DATE
4/26/63TRACK
52

SONIC VELOCITY

M INPUT-CODES	STOP	LOCATION	INSTRUCTION OPERATION ADDRESS	STOP	CONTENTS OF ADDRESS	NOTES
	X					
1 0 0 0			B 1 2 3 2		U 1 0 1 3	
0 1			X H Z 8 3 7			
0 2			B 1 2 3 3		X U 3 6 1 3	
0 3			X H 3 2 4 9	X		
0 4			U 1 0 0 6			
0 5						
0 6			X R 0 3 0 8			{ DATA
0 7			X U 0 3 0 0	X		} INPUT
0 8			B 1 2 0 5			
0 9			B 1 0 3 1			{ CURVE
1 0			X R 2 8 5 5			FIT }
1 1			X U 2 0 0 0	X		
1 2			U 1 0 2 5			
1 3			X E 0 0 0 0			(X2837)
1 4			X B 2 8 4 2			
1 5			S 1 0 3 7	X	Z 1 2 2 5	
1 6			M 0 9 3 0		Z @ 2	
1 7			D 0 9 3 1		I @ 2	
1 8			A 1 0 3 9		X Z 1 2 1 5	
1 9			Y 1 0 2 2	X		
2 0			X R 0 9 0 0			{ ERFP
2 1			X U 0 9 0 0			
2 2			8 0 0 H []			CONSTANTS
2 3			X E 0 0 0 0	X		
2 4			X U 2 8 3 8			
2 5			X Z 0 8 0 0		B.P. 8	(1012)
2 6			B 1 2 0 5			
2 7			X R 0 6 0 5	X		{ DATA (P's)
2 8			X U 0 6 0 0			
2 9			X Z 0 5 1 2			OUTPUT
3 0			X P 1 6 0 0			
3 1			Z 1 2 2 5	X		C.R. CONSTANT

= CONDITIONAL STOP CODE

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CARRIAGE RETURN

38 1.5		7750 AM 9/26/82	
EPA 23		MON 1000 1000 1000 1000	
1	2	3	4
5	6	7	8
9	10	11	12
13	14	15	16
17	18	19	20
21	22	23	24
25	26	27	28
29	30	31	32
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213	214	215	216
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221	222	223	224
225	226	227	228
229	230	231	232
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661	662	663	664
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677	678	679	680
681	682	683	684
685	686	687	688
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693	694	695	696
697	698	699	700
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705	706	707	708
709	710	711	712
713	714	715	716
717	718	719	720
721	722	723	724
725	726	727	728
729	730	731	732
733	734	735	736
737	738	739	740
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749	750	751	752
753	754	755	756
757	758	759	760
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765	766	767	768
769	770	771	772
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777	778	779	780
781	782	783	784
785	786	787	788
789	790	791	792
793	794	795	796
797	798	799	800
801	802	803	804
805	806	807	808
809	810	811	812
813	814	815	816
817	818	819	820
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825	826	827	828
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833	834	835	836
837	838	839	840
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845	846	847	848
849	850	851	852
853	854	855	856
857	858	859	860
861	862	863	864
865	866	867	868
869	870	871	872
873	874	875	876
877	878	879	880
881	882	883	884
885	886	887	888
889	890	891	892
893	894	895	896
897	898	899	900
901	902	903	904
905	906	907	908
909	910	911	912
913	914	915	916
917	918	919	920
921	922	923	924
925	926	927	928
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933	934	935	936
937	938	939	940
941	942	943	944
945	946	947	948
949	950	951	952
953	954	955	956
957	958	959	960
961	962	963	964
965	966	967	968
969	970	971	972
973	974	975	976
977	978	979	980
981	982	983	984
985	986	987	988
989	990	991	992
993	994	995	996
997	998	999	1000

				PAGE 24 / 29
PROGRAM NO.	PROGRAM PREPARED BY:		PROGRAM CHECKED BY:	DATE 4/26/63
SONIC VELOCITY				TRACK 53
INPUT CODES	LOCATION	INSTRUCTION	OUTPUT CODES	NOTES
		OPERATION ADDRESS		
1 1	3 2	X H 3 2 4 9		
	3 3	U 1 1 3 5		
	3 4	OPEN		
	3 5	X R 0 3 0 8	☒ } DATA	
	3 6	X U 0 3 0 0	} OUTPUT	
	3 7	B 1 2 3 3	X U 3 6 1 3	
	3 8	X H 3 2 4 9		
	3 9	U 1 0 5 0	☒	
	4 0	B 1 1 0 9		(1114)
	4 1	U 1 2 3 6		
	4 2	B 1 1 4 5		(1238)
	4 3	A 0 9 0 0	☒ 1@29	
	4 4	Y 1 1 4 5		
	4 5	B []	P	
	4 6	X R 3 8 1 6	} FLOAT	
	4 7	X U 3 8 0 0	☒ }	
	4 8	X Z 0 9 0 0		
	4 9	X Z 0 0 1 2		
	5 0	X U 3 2 0 9		
	5 1	OPEN	☒	
	5 2	OPEN		
	5 3	OPEN		
	5 4	B 1 0 6 3		(1106)
	5 5	A 0 9 0 1	☒ 2@29	
	5 6	Y 1 0 6 3		
	5 7	B 1 1 0 0		
	5 8	A 0 9 0 1	2@29	
	5 9	Y 1 1 0 0	☒	
	6 0	U 1 0 6 1		
	6 1	X R 3 8 1 6	} FLOAT	(1238)
	6 2	X U 3 8 0 0	} FLOAT	
	6 3	X Z 0 9 0 0	☒	

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4/26/63
TRACK
54

SONIC VELOCITY

INPUT CODES	STOP	LOCATION	INSTRUCTION		STOP	CONTENTS OF ADDRESS	NOTES
			OPERATION	ADDRESS			
	X						
		1200	XZ001Z				
		01	XR0900				
		02	XU0900				
		03	80XH6Z6Z		X		
		04	U1063				
		05	[]	J		P ₁ @ 12	
		06	[]	J		P ₂ @ 12	
		07	[]	J	X	P ₃ @ 12	
		08	[]	J		P ₄ @ 12	
		09	[]	J		P ₅ @ 12	
		10	[]	J		Y ₁ @ 12	
		11	[]	J	X	Y ₂ @ 12	
		12	[]	J		Y ₃ @ 12	
		13	[]	J		Y ₄ @ 12	
		14	[]	J		Y ₅ @ 12	
		15	[]	J	X	a	
		16	[]	J		b	
		17	[]	J		c	
		18	[]	J		d	
		19	[]	J	X	e	
		20	[]	J		a @ 12	
		21	[]	J		b @ 12	
		22	[]	J	X	c @ 12	
		23	[]	J		d @ 12	
		24	[]	J	X	e @ 12	
		25	[]	J		COUNTER 1	
		26	[]	J	X	COUNTER 2	
		27	[]	J			
		28	[]	J			
		29	[]	J			
		30	[]	J			
		31	[]	J			

* = CONDITIONAL STOP CODE

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CARRIAGE RETURN

PAGE	OF
26	/29
DATE	
4/26/63	
TRACK	
54	

No. _____ Date _____ Assignment _____

Sonic Velocity

Track 59

sec -		Quantity	Q
00	a		12
01	b		12
02	c	H _L VS LN P	12
03	d		12
04	e		12
05	a		12
06	b		12
07	c	LN H _V VS LN P	12
08	d		12
09	e		12
10	a		12
11	b		12
12	c	S _L VS LN P	12
13	d		12
14	e		12
15	a		12
16	b		12
17	c	LN S _V VS LN P	12
18	d		12
19	e		12
20	a		12
21	b		12
22	c	V _L VS LN P	12
23	d		12
24	e		12
25	a		12
26	b		12
27	c	LN V _V VS LN P	12
28	d		12
29	e		12
30		N	25
31			

Sec- tor	Quantity	Q
32	P	
33		
34	P_1	
35		
36	P_2	
37		
38	V_{L1}	
39		
40	V_{L2}	
41		
42	V_{V1}	
43		
44	V_{V2}	
45		
46	V_L	
47		
48	V_V	
49		
50	S_{L1}	
51		
52	S_{L2}	
53		
54	S_{V1}	
55		
56	S_{V2}	
57		
58	S_L	
59		
60	S_V	
61		
62	Q	
63		

SOME VARIOUS

— 9 —

Sonic Velocity

Track 60

	<u>Quantity</u>	Q
1	S_a	
2	Q_1	
3	Q_2	
4	V_{e_1}	
5	V_{e_2}	
6	G_{MAX}	
7	P_1	
8	P_2	
9	V_{L_1}	
0	V_{L_2}	
1	V_{V_1}	
2	V_{V_2}	
3	a	
4	b	
5	c	
6	s	
7	d	

Sec - tor	Quantity	Q
32	[e])
33	[])
34	[a])
35	[])
36	[b])
37	[])
38	[c])
39	[])
40	[d])
41	[])
42	[e])
43	[])
44	[a])
45	[])
46	[b])
47	[])
48	[c])
49	[])
50	[d])
51	[])
52	[e])
53	[])
54	[a])
55	[])
56	[b])
57	[])
58	[c])
59	[])
60	[d])
61	[])
62	[e])
63	[])

LN *Sv*
vs
LN *P*

V_L
vs
 $\ln P$

LN V_r
VS
LN P

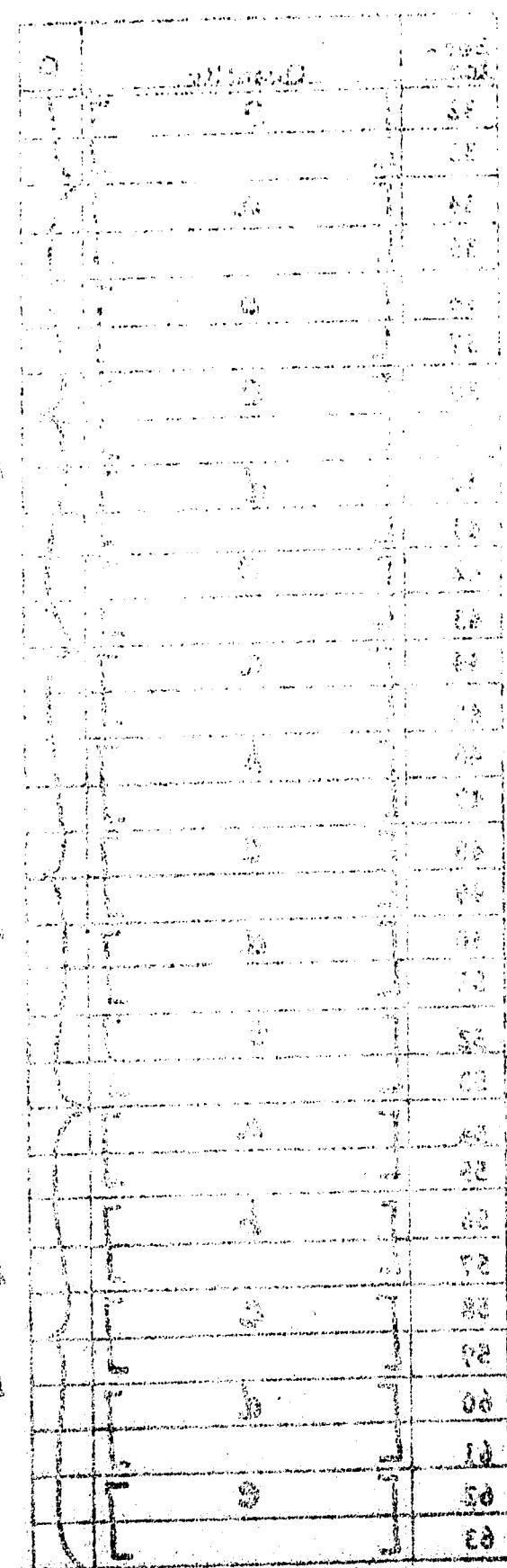
P.S. to B.S. 84

Information Averaged from

No. 6

AEROCAR 21402

90° start



No. _____ Data Storage Assignment

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SONIC VELOCITY

Track 61

INPUT & OUTPUT DATA

Sec- or	Quantity	Q
00	P_1	12
01	P_2	12
02	P_3	12
03	P_4	12
04	P_5	12
05	H_{L1}	12
06	H_{L2}	12
07	H_{L3}	12
08	H_{L4}	12
09	H_{L5}	12
10	H_{V1}	12
11	H_{V2}	12
12	H_{V3}	12
13	H_{V4}	12
14	H_{V5}	12
15	P_1	12
16	P_2	12
17	P_3	12
18	P_4	12
19	P_5	12
20	S_{L1}	12
21	S_{L2}	12
22	S_{L3}	12
23	S_{L4}	12
24	S_{L5}	12
25	S_{V1}	12
26	S_{V2}	12
27	S_{V3}	12
28	S_{V4}	12
29	S_{V5}	12
30	P_1	12
31	P_2	12

Sec- tor	Quantity	Q
32	P_3	12
33	P_4	12
34	P_5	12
35	V_{L1}	12
36	V_{L2}	12
37	V_{L3}	12
38	V_{L4}	12
39	V_{L5}	12
40	V_{V1}	12
41	V_{V2}	12
42	V_{V3}	12
43	V_{V4}	12
44	V_{V5}	12
45	XZ0000	
46	ISOBAR # 1	12
47	" 2	12
48	" 3	12
49	" 4	12
50	" 5	12
51	" 6	12
52	" 7	12
53	" 8	12
54	" 9	12
55	" 10	12
56	P (LB/SQ IN)	12
57	Q (%)	12
58	H (BTU/LB)	12
59	V (CU FT/LB)	12
60	S (BTU/LB-°F)	12
61	G _{MAX} (LB/SQ FT-SEC)	12
62	V _{MAX} (FT/SEC)	12
63		

OUTPUT

13 cont

ATAC TURTO & TURK

Q	quality	-392
S1	0.1	SE
S1	0.2	EE
S1	0.3	DE
S1	0.4	CE
S1	0.5	BE
S1	0.6	AE
S1	0.7	BE
S1	0.8	CE
S1	0.9	DE
S1	1.0	EE
S1	1.1	SE
S1	1.2	EE
S1	1.3	DE
S1	1.4	CE
S1	1.5	BE
S1	1.6	AE
S1	1.7	BE
S1	1.8	CE
S1	1.9	DE
S1	2.0	EE
S1	2.1	SE
S1	2.2	EE
S1	2.3	DE
S1	2.4	CE
S1	2.5	BE
S1	2.6	AE
S1	2.7	BE
S1	2.8	CE
S1	2.9	DE
S1	3.0	EE
S1	3.1	SE
S1	3.2	EE
S1	3.3	DE
S1	3.4	CE
S1	3.5	BE
S1	3.6	AE
S1	3.7	BE
S1	3.8	CE
S1	3.9	DE
S1	4.0	EE
S1	4.1	SE
S1	4.2	EE
S1	4.3	DE
S1	4.4	CE
S1	4.5	BE
S1	4.6	AE
S1	4.7	BE
S1	4.8	CE
S1	4.9	DE
S1	5.0	EE
S1	5.1	SE
S1	5.2	EE
S1	5.3	DE
S1	5.4	CE
S1	5.5	BE
S1	5.6	AE
S1	5.7	BE
S1	5.8	CE
S1	5.9	DE
S1	6.0	EE
S1	6.1	SE
S1	6.2	EE
S1	6.3	DE
S1	6.4	CE
S1	6.5	BE
S1	6.6	AE
S1	6.7	BE
S1	6.8	CE
S1	6.9	DE
S1	7.0	EE
S1	7.1	SE
S1	7.2	EE
S1	7.3	DE
S1	7.4	CE
S1	7.5	BE
S1	7.6	AE
S1	7.7	BE
S1	7.8	CE
S1	7.9	DE
S1	8.0	EE
S1	8.1	SE
S1	8.2	EE
S1	8.3	DE
S1	8.4	CE
S1	8.5	BE
S1	8.6	AE
S1	8.7	BE
S1	8.8	CE
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S1	10.6	AE
S1	10.7	BE
S1	10.8	CE
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S1	11.1	SE
S1	11.2	EE
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S1	11.4	CE
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S1	11.8	CE
S1	11.9	DE
S1	12.0	EE
S1	12.1	SE
S1	12.2	EE
S1	12.3	DE
S1	12.4	CE
S1	12.5	BE
S1	12.6	AE
S1	12.7	BE
S1	12.8	CE
S1	12.9	DE
S1	13.0	EE
S1	13.1	SE
S1	13.2	EE
S1	13.3	DE
S1	13.4	CE
S1	13.5	BE
S1	13.6	AE
S1	13.7	BE
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S1	13.9	DE
S1	14.0	EE
S1	14.1	SE
S1	14.2	EE
S1	14.3	DE
S1	14.4	CE
S1	14.5	BE
S1	14.6	AE
S1	14.7	BE
S1	14.8	CE
S1	14.9	DE
S1	15.0	EE
S1	15.1	SE
S1	15.2	EE
S1	15.3	DE
S1	15.4	CE
S1	15.5	BE
S1	15.6	AE
S1	15.7	BE
S1	15.8	CE
S1	15.9	DE
S1	16.0	EE
S1	16.1	SE
S1	16.2	EE
S1	16.3	DE
S1	16.4	CE
S1	16.5	BE
S1	16.6	AE
S1	16.7	BE
S1	16.8	CE
S1	16.9	DE
S1	17.0	EE
S1	17.1	SE
S1	17.2	EE
S1	17.3	DE
S1	17.4	CE
S1	17.5	BE
S1	17.6	AE
S1	17.7	BE
S1	17.8	CE
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S1	18.0	EE
S1	18.1	SE
S1	18.2	EE
S1	18.3	DE
S1	18.4	CE
S1	18.5	BE
S1	18.6	AE
S1	18.7	BE
S1	18.8	CE
S1	18.9	DE
S1	19.0	EE
S1	19.1	SE
S1	19.2	EE
S1	19.3	DE
S1	19.4	CE
S1	19.5	BE
S1	19.6	AE
S1	19.7	BE
S1	19.8	CE
S1	19.9	DE
S1	20.0	EE
S1	20.1	SE
S1	20.2	EE
S1	20.3	DE
S1	20.4	CE
S1	20.5	BE
S1	20.6	AE
S1	20.7	BE
S1	20.8	CE
S1	20.9	DE
S1	21.0	EE
S1	21.1	SE
S1	21.2	EE
S1	21.3	DE
S1	21.4	CE
S1	21.5	BE
S1	21.6	AE
S1	21.7	BE
S1	21.8	CE
S1	21.9	DE
S1	22.0	EE
S1	22.1	SE
S1	22.2	EE
S1	22.3	DE
S1	22.4	CE
S1	22.5	BE
S1	22.6	AE
S1	22.7	BE
S1	22.8	CE
S1	22.9	DE
S1	23.0	EE
S1	23.1	SE
S1	23.2	EE
S1	23.3	DE
S1	23.4	CE
S1	23.5	BE
S1	23.6	AE
S1	23.7	BE
S1	23.8	CE
S1	23.9	DE
S1	24.0	EE
S1	24.1	SE
S1	24.2	EE
S1	24.3	DE
S1	24.4	CE
S1	24.5	BE
S1	24.6	AE
S1	24.7	BE
S1	24.8	CE
S1	24.9	DE
S1	25.0	EE
S1	25.1	SE
S1	25.2	EE
S1	25.3	DE
S1	25.4	CE
S1	25.5	BE
S1	25.6	AE
S1	25.7	BE
S1	25.8	CE
S1	25.9	DE
S1	26.0	EE
S1	26.1	SE
S1	26.2	EE
S1	26.3	DE
S1	26.4	CE
S1	26.5	BE
S1	26.6	AE
S1	26.7	BE
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S1	26.9	DE
S1	27.0	EE
S1	27.1	SE
S1	27.2	EE
S1	27.3	DE
S1	27.4	CE
S1	27.5	BE
S1	27.6	AE
S1	27.7	BE
S1	27.8	CE
S1	27.9	DE
S1	28.0	EE
S1	28.1	SE
S1	28.2	EE
S1	28.3	DE
S1	28.4	CE
S1	28.5	BE
S1	28.6	AE
S1	28.7	BE
S1	28.8	CE
S1	28.9	DE
S1	29.0	EE
S1	29.1	SE
S1	29.2	EE
S1	29.3	DE
S1	29.4	CE
S1	29.5	BE
S1	29.6	AE
S1	29.7	

P (PSIA)	Q (% Vapor)	H (BTU/Lb)	V (Cu Ft/Lb)	S (BTU/Lb-deg F)	G max (Lb/Sq Ft-Sec)	V max (Ft/Sec)
225.00000	0.00000	41.56118	.01379	.08083	3860.082	673.4776
	10.00000	46.40607	.02985	.08890	3614.185	630.5753
	20.00000	51.25097	.04592	.09696	3374.145	588.6950
	30.00000	56.09586	.06199	.10502	3176.349	554.1850
	40.00000	60.94076	.07806	.11309	3009.702	525.1097
	50.00000	65.78565	.09413	.12115	2866.802	500.1776
	60.00000	70.63055	.11019	.12922	2742.497	478.4899
	70.00000	75.47544	.12626	.13728	2633.076	459.3988
	80.00000	80.32034	.14233	.14534	2535.786	442.4245
	90.00000	85.16523	.15839	.15341	2448.5410	427.2027
	100.00000	90.01013	.17447	.16147	2341.4272	408.5143
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150.00000	0.00000	33.43080	.01292	.06726	2848.216	767.1808
	10.00000	38.86436	.03855	.07681	2606.863	702.1713
	20.00000	44.29793	.06419	.08636	2394.4169	644.9478
	30.00000	49.73150	.08984	.09591	2226.6676	599.7637
	40.00000	55.16506	.11548	.10546	2089.8614	562.9143
	50.00000	60.59863	.14113	.11501	1975.5231	532.1167
	60.00000	66.03220	.16677	.12456	1878.1073	505.8773
	70.00000	71.46576	.19241	.13411	1793.8133	483.1723
	80.00000	76.89933	.21806	.14366	1719.9373	463.2735
	90.00000	82.33290	.24371	.15321	1654.4962	445.6466
	100.00000	87.76647	.26935	.16276	1577.2843	424.8492

100.00000	.00000	26.51649	.01228	.05504	2094.6424	852.6863
10.00000	32.40196	.05175	.06593	1873.3811	762.6153	
20.00000	38.28743	.09123	.07682	1694.5167	689.8032	
30.00000	44.17290	.13071	.08770	1558.7157	634.5214	
40.00000	50.05837	.17019	.09859	1451.0765	590.7037	
50.00000	55.94384	.20967	.10948	1363.0427	554.8669	
60.00000	61.82931	.24915	.12037	1289.3046	524.8497	
70.00000	67.71478	.28863	.13126	1226.3697	499.2301	
80.00000	73.60025	.32811	.14214	1171.8339	477.0297	
90.00000	79.48572	.36759	.15303	1123.9813	457.5499	
100.00000	85.37119	.40707	.16392	1068.9876	435.1631	

100.00000	.00000	26.51649	.01228	.05504	2094.6424	852.6863
10.00000	32.40196	.05175	.06593	1873.3811	762.6153	
20.00000	38.28743	.09123	.07682	1694.5167	689.8032	
30.00000	44.17290	.13071	.08770	1558.7157	634.5214	
40.00000	50.05837	.17019	.09859	1451.0765	590.7037	
50.00000	55.94384	.20967	.10948	1363.0427	554.8669	
60.00000	61.82931	.24915	.12037	1289.3046	524.8497	
70.00000	67.71478	.28863	.13126	1226.3697	499.2301	
80.00000	73.60025	.32811	.14214	1171.8339	477.0297	
90.00000	79.48572	.36759	.15303	1123.9813	457.5499	
100.00000	85.37119	.40707	.16392	1068.9876	435.1631	
60.00000	.00000	19.16436	.01170	.04120	1412.7614	947.8668
10.00000	25.48073	.07761	.05362	1226.6358	822.9892	
20.00000	31.79710	.14354	.06604	1089.6186	731.0599	
30.00000	38.11347	.20947	.07846	990.1835	664.3457	
40.00000	44.42984	.27539	.09089	913.7919	613.0922	
50.00000	50.74621	.34132	.10331	852.7287	572.1230	
60.00000	57.06258	.40723	.11573	802.4701	538.4028	
70.00000	63.37895	.47315	.12815	760.1647	510.0188	
80.00000	69.69533	.53908	.14057	723.9142	485.6972	
90.00000	76.01170	.60500	.15299	692.3997	464.5531	
100.00000	82.32807	.67093	.16542	656.9770	440.7869	

45.00000	.00000	15.54924	.01146	.03401	1127.2291	995.5271
10.00000		22.06073	.09862	.04725	962.3046	849.8719
20.00000		28.57222	.18579	.06048	846.6413	747.7224
30.00000		35.08371	.27296	.07372	764.6533	675.3136
40.00000		41.59520	.36014	.08695	702.6413	620.5469
50.00000		48.10670	.44730	.10018	653.6213	577.2542
60.00000		54.61819	.53447	.11342	613.6103	541.9180
70.00000		61.12968	.62164	.12665	580.1489	512.3661
80.00000		67.64117	.70882	.13989	551.6253	487.1751
90.00000		74.15266	.79598	.15312	526.9334	465.3682
100.00000		80.66415	.88316	.16635	499.4296	441.0778
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30.00000	.00000	10.95418	.01118	.02449	815.6691	1056.3539
10.00000		17.70186	.13956	.03883	679.7745	880.3601
20.00000		24.44955	.26795	.05317	590.4457	764.6724
30.00000		31.19724	.39634	.06750	529.0532	685.1644
40.00000		37.94492	.52473	.08184	483.5334	626.2128
50.00000		44.69262	.65311	.09617	448.0471	580.2553
60.00000		51.44030	.78151	.11051	419.3784	543.1271
70.00000		58.18799	.90990	.12484	395.5912	512.3208
80.00000		64.93568	1.03828	.13918	375.4407	486.2245
90.00000		71.68337	1.16667	.15352	358.0858	463.7486
100.00000		78.43106	1.29507	.16785	338.9478	438.9634

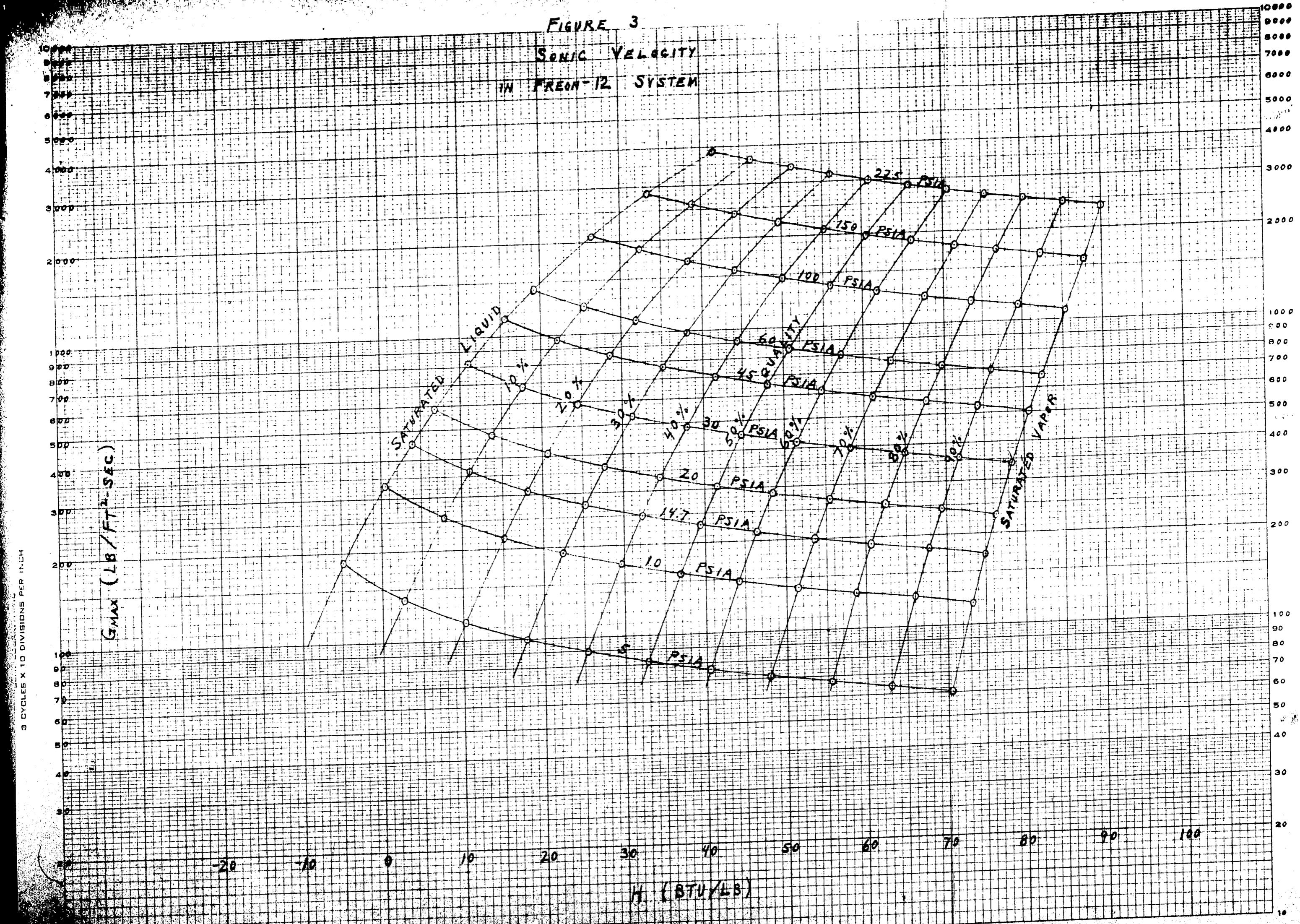
20.00000	.00000	6.82453	.01094	.01556	586.7008	1111.3096
10.00000	13.77807	.19926	.03096	477.2194	903.9336	
20.00000	20.73162	.38758	.04637	409.5513	775.7588	
30.00000	27.68517	.57590	.06178	364.3534	690.1465	
40.00000	34.63872	.76422	.07718	331.4305	627.7849	
50.00000	41.59226	.95255	.09259	306.0735	579.7546	
60.00000	48.54581	1.14086	.10799	285.7679	541.2924	
70.00000	55.49935	1.32919	.12340	269.0323	509.5923	
80.00000	62.45290	1.51750	.13881	254.9299	482.8800	
90.00000	69.40645	1.70583	.15421	242.8355	459.9712	
100.00000	76.36000	1.89416	.16962	229.6036	434.9078	

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14.70000	.00000	3.93755	.01077	.00910	455.2620	1150.4308
10.00000	11.03422	.26239	.02531	363.4705	918.4770	
20.00000	18.13091	.51401	.04151	309.2457	781.4528	
30.00000	25.22759	.76562	.05772	273.7528	691.7636	
40.00000	32.32428	1.01724	.07392	248.2135	627.2266	
50.00000	39.42096	1.26886	.09013	228.7043	57.9275	
60.00000	46.51764	1.52048	.10633	213.1734	538.6815	
70.00000	53.61433	1.77210	.12254	200.4298	506.4790	
80.00000	60.71101	2.02371	.13874	189.7286	479.4373	
90.00000	67.80769	2.27533	.15495	180.5766	456.3107	
100.00000	74.90438	2.52696	.17115	170.6151	431.1381	

10.00000	.00000	.57809	.01058	.00137	330.4629	1197.9930
10.00000		7.84246	.37203	.01857	257.6552	934.0506
20.00000		15.10685	.73350	.03576	216.9664	786.5457
30.00000		22.37124	1.09496	.05295	190.9616	692.2733
40.00000		29.63563	1.45642	.07015	172.5109	625.3858
50.00000		36.90002	1.81788	.08734	158.5470	574.7641
60.00000		44.16441	2.17934	.10454	147.5040	534.7308
70.00000		51.42879	2.54079	.12173	138.4875	502.0445
80.00000		58.69318	2.90226	.13892	130.9451	474.7018
90.00000		65.95757	3.26372	.15612	124.5144	451.3894
100.00000		73.22196	3.62518	.17331	117.5555	426.1619
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5.00000	.00000	-4.82829	.01028	-.01162	185.3602	1286.5730
10.00000		2.70676	.70333	.00732	138.1883	959.1560
20.00000		10.24182	1.39639	.02626	114.3329	793.5771
30.00000		17.77689	2.08946	.04520	99.6857	691.9115
40.00000		25.31194	2.78253	.06414	89.5272	621.4027
50.00000		32.84700	3.47559	.08307	81.9517	568.8212
60.00000		40.38205	4.16865	.10201	76.0223	527.6655
70.00000		47.91712	4.86172	.12095	71.2179	494.3189
80.00000		55.45217	5.55478	.13989	67.2227	466.5879
90.00000		62.98723	6.24784	.15883	63.8322	443.0550
100.00000		70.52229	6.94091	.17777	60.2008	417.8496

FIGURE 3
SONIC VELOCITY
IN FREON-12 SYSTEM



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TABLE 2

P (PSIA)	Q (% Vapor)	H (BTU/Lb)	V (Cu Ft/Lb)	S (BTU/Lb-deg F)	G max (Lb/Sq Ft-Sec)	V max (Ft/Sec)
225.00000	.00000	42.30810	.01415	.08507	3648.151	862.4993
	10.00000	49.38848	.03637	.09763	3362.615	794.9927
	20.00000	56.46888	.05859	.11020	3104.848	734.0510
	30.00000	63.54926	.08083	.12276	2898.516	685.2699
	40.00000	70.62965	.10305	.13533	2728.515	645.0780
	50.00000	77.71005	.12528	.14790	2585.298	611.2185
	60.00000	84.79044	.14750	.16046	2462.4975	582.1860
	70.00000	91.87083	.16973	.17303	2355.6831	556.9328
	80.00000	98.95121	.19196	.18559	2261.6621	534.7043
	90.00000	106.03160	.21419	.19816	2178.0691	514.9412
	100.00000	113.11200	.23642	.21072	2077.9104	491.2615
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150.00000	.00000	32.84031	.01338	.06817	2714.692	989.8249
	10.00000	40.73957	.04851	.08293	2428.7558	885.5674
	20.00000	48.63884	.08363	.09769	2197.7969	801.3557
	30.00000	56.53810	.11875	.11245	2022.2559	737.3503
	40.00000	64.43737	.15387	.12722	1883.0117	686.5795
	50.00000	72.33664	.18900	.14198	1769.0648	645.0324
	60.00000	80.23591	.22411	.15674	1673.5793	610.2167
	70.00000	88.13517	.25924	.17150	1592.0544	580.4913
	80.00000	96.03444	.29436	.18626	1521.3893	554.7255
	90.00000	103.93371	.32948	.20103	1459.3691	532.1118
	100.00000	111.83298	.36462	.21579	1387.9208	506.0605

(3814)

100.00000	.00000	24.88832	.01281	.05315	2010.2088	1106.8610
10.00000	33.39838	.06659	.06984	1745.6578	961.1940	
20.00000	41.90843	.12037	.08653	1551.1267	854.0812	
30.00000	50.41848	.17415	.10322	1409.8495	776.2912	
40.00000	58.92854	.22793	.11991	1301.2588	716.4990	
50.00000	67.43859	.28171	.13661	1214.4266	668.6875	
60.00000	75.94865	.33549	.15329	1142.9394	629.3252	
70.00000	84.45870	.38927	.16998	1082.7518	596.1847	
80.00000	92.96876	.44305	.18667	1031.1701	567.7828	
90.00000	101.47881	.49683	.20336	986.3211	543.0881	
100.00000	109.98887	.55061	.22005	935.9075	515.3293	
5						
60.00000	.00000	16.54166	.01228	.03644	1366.9255	1239.7134
10.00000	25.61727	.10174	.05530	1142.8738	1036.5129	
20.00000	34.69289	.19120	.07415	994.5816	902.0214	
30.00000	43.76852	.28067	.09300	892.2000	809.1679	
40.00000	52.84415	.37013	.11185	816.0692	740.1223	
50.00000	61.91977	.45960	.13070	756.6006	686.1880	
60.00000	70.99538	.54907	.14956	708.4866	642.5517	
70.00000	80.07101	.63853	.16841	668.5203	606.3049	
80.00000	89.14663	.72799	.18726	634.6344	575.5726	
90.00000	98.22225	.81746	.20612	605.4287	549.0848	
100.00000	107.29788	.90693	.22497	573.2498	519.9007	

45.00000	.00000	12.47868	.01203	.02792	1095.5099	1307.5195
10.00000	21.80544	.13017	.04790	896.4770	1069.9685	
20.00000	31.13222	.24833	.06788	771.7883	921.1493	
30.00000	40.45899	.36648	.08787	687.8832	821.0065	
40.00000	49.78577	.48462	.10785	626.4855	747.7268	
50.00000	59.11253	.60277	.12783	579.0512	691.1126	
60.00000	68.43932	.72093	.14782	540.9810	645.6749	
70.00000	77.76608	.83907	.16780	509.5508	608.1621	
80.00000	87.09286	.95721	.18778	483.0307	576.5096	
90.00000	96.41963	1.07536	.20777	460.2623	549.3350	
100.00000	105.74641	1.19352	.22775	435.3752	519.6316	
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30.00000	.00000	7.35094	.01174	.01678	797.2223	1394.7696
10.00000	16.97904	.18552	.03829	632.9835	1107.4279	
20.00000	26.60716	.35929	.05980	537.3440	940.1030	
30.00000	36.23528	.53307	.08131	475.0687	831.1501	
40.00000	45.86340	.70685	.10282	430.3968	752.9950	
50.00000	55.49151	.88063	.12433	396.3429	693.4164	
60.00000	65.11961	1.05441	.14585	369.2733	646.0571	
70.00000	74.74773	1.22819	.16736	347.0864	607.2404	
80.00000	84.37586	1.40196	.18887	328.4714	574.6728	
90.00000	94.00397	1.57575	.21038	312.5624	546.8394	
100.00000	103.63209	1.74953	.23189	295.3219	516.6766	

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230.0000

240.0000

250.0000

260.0000

270.0000

280.0000

290.0000

300.0000

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320.0000

330.0000

340.0000

350.0000

360.0000

370.0000

380.0000

390.0000

400.0000

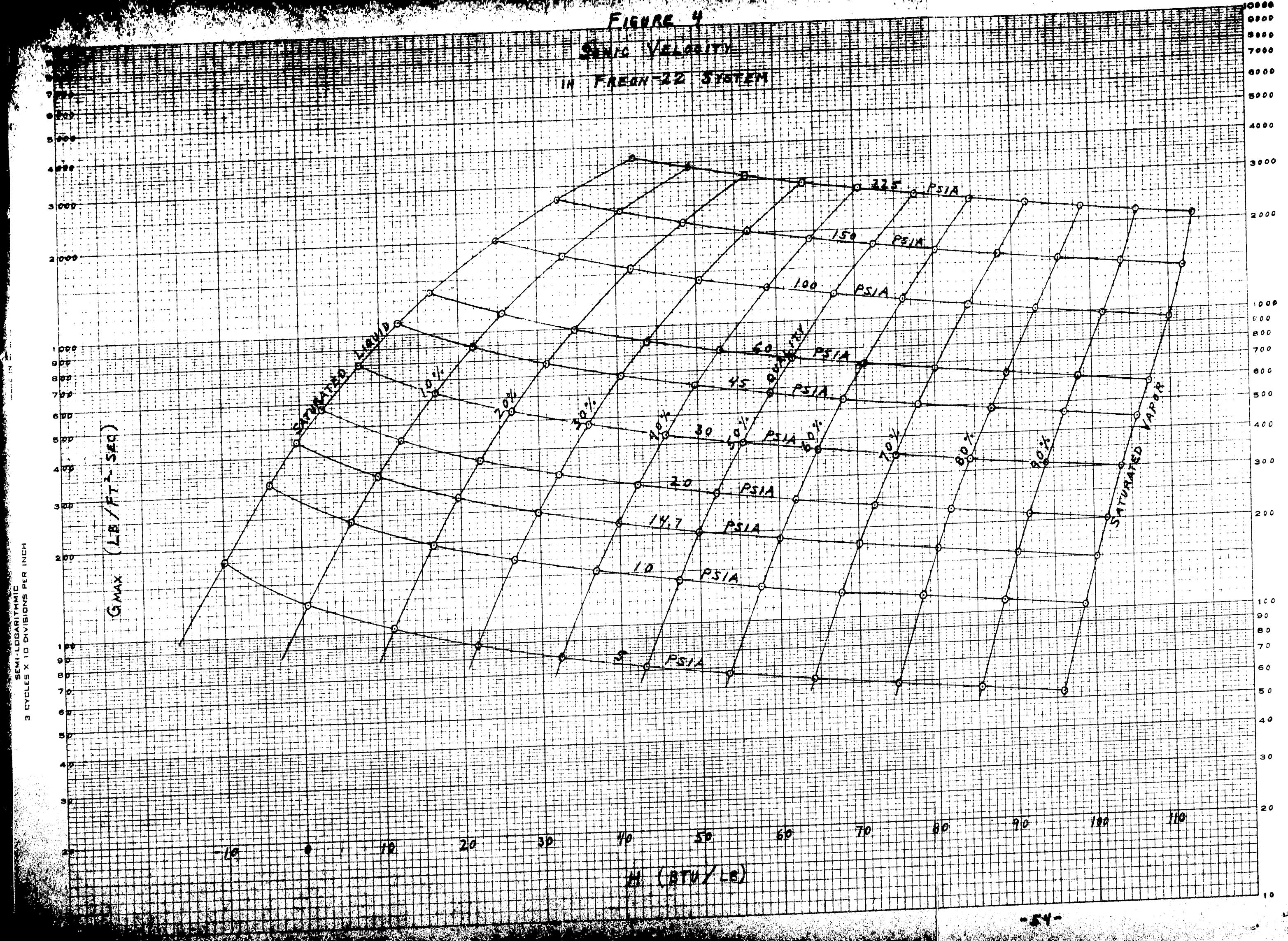
20.00000	.00000	2.77512	.01149	.00647	575.8634	1472.5610
10.00000	12.66433	.26604	.02947	443.8732	1135.0441	
20.00000	22.55354	.52061	.05246	372.0697	951.4329	
30.00000	32.44276	.77518	.07545	326.6582	835.3094	
40.00000	42.33198	1.02974	.09844	294.6329	753.4164	
50.00000	52.22119	1.28431	.12143	270.4914	691.6833	
60.00000	62.11041	1.53886	.14443	251.4528	642.9991	
70.00000	71.99963	1.79343	.16742	235.9405	603.3319	
80.00000	81.88884	2.04800	.19041	222.9850	570.2031	
90.00000	91.77806	2.30256	.21340	211.9533	541.9935	
100.00000	101.66728	2.55713	.23639	200.0751	511.6194	

14.70000	.00000	-.40502	.01132	-.00090	447.5835	1525.4569
10.00000	9.66421	.35100	.02319	337.5546	1150.4558	
20.00000	19.73343	.69068	.04729	280.5126	956.0450	
30.00000	29.80266	1.03037	.07138	245.1397	835.4868	
40.00000	39.87189	1.37006	.09548	220.4711	751.4110	
50.00000	49.94111	1.70975	.11957	202.0092	688.4891	
60.00000	60.01034	2.04944	.14366	187.5233	639.1180	
70.00000	70.07957	2.38913	.16776	175.7646	599.0419	
80.00000	80.14880	2.72881	.19185	165.9724	565.6681	
90.00000	90.21803	3.06850	.21595	157.6534	537.3152	
100.00000	100.28725	3.40820	.24004	148.7311	506.9062	

10.00000	.00000	-4.08073	.01112	-.00970	324.6660	1584.1892
10.00000		6.19467	.49795	.01575	238.5662	1164.0702
20.00000		16.47009	.98478	.04120	196.3472	958.0649
30.00000		26.74551	1.47161	.06665	170.7288	833.0617
40.00000		37.02092	1.95844	.09210	153.0769	746.9301
50.00000		47.29634	2.44527	.11755	139.9675	682.9634
60.00000		57.57175	2.93211	.14300	129.7361	633.0400
70.00000		67.84716	3.41893	.16845	121.4636	592.6747
80.00000		78.12258	3.90576	.19390	114.5953	559.1612
90.00000		88.39800	4.39259	.21935	108.7742	530.7575
100.00000		98.67342	4.87943	.24479	102.5568	500.4200

१

5.00000	.00000	-9.89189	.01090	-.02460	179.9204	1668.1387
10.00000	.68339	.93696	.00317	126.7759		1175.4077
20.00000	11.25867	1.86302	.03093	102.8727		953.7885
30.00000	21.83395	2.78908	.05869	88.8174		823.4736
40.00000	32.40924	3.71514	.08646	79.2952		735.1887
50.00000	42.98452	4.64121	.11422	72.2982		670.3155
60.00000	53.55980	5.56726	.14199	66.8770		620.0530
70.00000	64.13509	6.49333	.16975	62.5171		579.6294
80.00000	74.71037	7.41939	.19751	58.9119		546.2039
90.00000	85.28565	8.34544	.22528	55.8662		517.9654
100.00000	95.86094	9.27152	.25304	52.6341		487.9991



DISCUSSION OF RESULTS

Pages 122 to 127 of the Appendix are the computer print-out sheets used to check the accuracy of the program for the Freon 12 and Freon 22 systems investigated. They represent computer results for 5 saturation pressures very close to 5 of the 10 pressures listed in the "Results", but are values for which saturated liquid and vapor data are tabulated in Properties of Commonly Used Refrigerants (2). This choice of pressures was made to eliminate inter-polation of data for hand calculations.

Sonic velocity was calculated by hand for all 5 pressures at 0%, 50% and 100% quality by the same method and with the same equations used in the computer program, using the next higher tabulated pressure for P_2 and the next lower for P_1 . The results of these hand calculations and the equivalent computer values are listed in Tables 3 and 4 along with the percentage deviation of the computer values.

The maximum deviation for Freon 12 was found to be approximately 4% and for Freon 22 approximately 6.5%. Some of this deviation is due to the inherent error in using difference methods to approximate a derivative, since the differences are greater for the hand calculations and the accuracy of the differences is less than for the computer calculations.

However, the main reason for the deviation is the error in the physical properties resulting from the inaccuracy of the polynomials. Tables 5 and 6 show a comparison between published data and computer values for saturated liquid and vapor properties.

The maximum deviation in entropy or specific volume is 1.8%. Although the deviations are generally much smaller than this, the maximum velocity is a function of the slope of the entropy and volume

curves and is therefore affected by the oscillations of the polynomials, even though the equations may accurately reproduce the properties for a given point.

A comparison of the results from this report with those of Vaillancourt (8) for the Freon 12 system was of little value in determining the accuracy of the computer program. With the exception of the 14.7 psia isobar, a maximum difference of approximately 20% was found in the two methods. However, this discrepancy appears to be mostly a result of the use of different sources for physical properties. It would appear that Vaillancourt's 14.7 psia line is in error, although no attempt was made to determine the cause of the error.

The results presented in this report were obtained using a range of data points from 5 psia to 225 psia. The accuracy of the results could be improved by limiting each set of calculations to a smaller pressure range. For example, if the systems presented in this report had been divided into two or three ranges with well chosen data points better coefficients for the polynomials would have resulted. Better results could also be achieved by so selecting the data points that each isobar would fall on or near a data point.

However, the maximum errors recorded here for sonic velocity represent approximately the same reliability obtainable by graphical solutions. The results are also probably much better than the reproducibility of any experimental method for measuring sonic velocity. More important is the fact that the calculations assume equilibrium between two phases at very high velocity, which would certainly be far from accurate for the actual conditions.

From the above considerations it is concluded that the computer program presented in this report provides a method for calculating reliable theoretical data for a curve of sonic velocity versus enthalpy for one component, two phase systems. The reliability ceases in the region below 10% quality, since the change in compressibility is so great as to approach a discontinuity, and results in liquid velocities which are low by several orders of magnitude.

No sonic choke was found in the two phase region for the Freon 12 and Freon 22 systems studied. From the sonic velocity curves, Figs. 3 and 4, it can be seen that for all pressures the lowest velocity calculated occurs for saturated vapor.

However, considering typical approximations in engineering practice, some difficulties can be foreseen in designs based only on the vapor velocity. For example, a mixture of Freon 22 liquid and vapor at 225 psia and 50% quality might be assumed to be 90% vapor by volume. For the maximum vapor velocity being the velocity of sound in pure vapor, the overall maximum mass velocity would be two times 90% of the sonic velocity of the pure vapor, or

$$G_{\max} = 2 (0.9 \times 2078) = 3740 \text{#/ft}^2 \text{sec.}$$

However, from the computer results on page 49 it is seen that $G_{\max} = 2585 \text{#/ft}^2 \text{sec.}$ for 225 psia and 50% quality. Furthermore, assuming the phases are separate, the liquid velocity would be calculated to be 26.4 ft/sec., an entirely reasonable value.

Similarly at 5 psia and 50% quality for Freon 22, an overall maximum mass velocity of $104.2 \text{#/ft}^2 \text{sec.}$ would be calculated assuming 99% of the volume as a vapor. The resulting liquid velocity would be less than

1 ft/sec. However, the maximum mass velocity calculated by the computer is only $72.3 \text{#/ft}^2 \text{sec.}$

In order to reduce the possibility of errors of this type and to check for the existence of limiting sonic velocities within the two phase envelope, it is recommended that the Sonic Velocity program be used to develop sonic velocity curves for common fluids of various type - e.g., steam, inorganics, refrigerants and light hydrocarbons. If this study points to any significant value in these curves, the computer program should be rewritten to make use of a true curve fit routine, in order to make it applicable where the best kind of published physical data is not available.

At the time when this information is found to be of importance, it will also be necessary to find some physical means of verifying the results experimentally.

TABLE 3
COMPARISON OF RESULTS

FOR FREON 12

P(PSIA)	Q(%)	G_{max} (LB./FT ² SEC.)		DEVIATION (%)
		COMPUTER	CALCULATED	
224.00	0	3847	3857	-.26
	50	2855	2850	+.18
	100	2331	2311	+.87
60.364	0	1419	1458	-2.68
	50	857.5	862.5	-.58
	100	660.8	658.1	+.20
29.932	0	814.2	804.6	+1.19
	50	447.1	446.4	+.16
	100	338.2	335.4	+.83
14.564	0	451.8	433.2	+4.29
	50	226.7	222.6	+1.84
	100	169.1	167.4	+1.01
5.0516	0	186.9	184.5	+1.30
	50	82.75	83.10	-.42
	100	60.80	60.11	+1.15

TABLE 4
COMPARISON OF RESULTS

FOR FREON 22

P (PSIA)	Q (%)	G_{max} (LB./FT ² SEC.)		DEVIATION (%)
		COMPUTER	CALCULATED	
224.6	0	3643	3580	+1.76
	50	2581	2590	-.35
	100	2074	2050	+1.17
60.23	0	1371	1340	+2.31
	50	759	768	-1.17
	100	575	565	+1.77
29.94	0	796	770	+3.38
	50	396	396	.00
	100	295	287	+2.79
14.54	0	444	417	+6.47
	50	200	201	-.50
	100	147.2	141.8	+3.81
5.100	0	183.0	180	+1.67
	50	73.7	73.0	+.96
	100	53.6	52.2	+2.68

TABLE 5

FREON 12 PROPERTIES

P (PSIA)	H(BTU/LB)			V(CUFT/LB)			S(BTU/LB °F)		
	CALC.	ACTUAL	DEV. (%)	CALC.	ACTUAL	DEV. (%)	CALC.	ACTUAL	DEV. (%)
(SATURATED LIQUID)									
224.00	41.464	41.427	+.089	.01379	.013778	+.087	.08068	.080635	+.056
60.364	19.244	19.283	-.204	.01170	.011730	-.256	.04135	.041403	-.128
29.932	10.930	10.901	+.266	.01118	.011173	+.060	.02444	.024413	+.112
14.564	3.8533	3.8100	+1.14	.01077	.010764	+.056	.00891	.008864	+.520
5.0516	-4.7543	-4.6088	+3.16	.01028	.010337	-.552	-.01144	-.011259	+1.61
(SATURATED VAPOR)									
224.00	89.987	90.028	-.045	.17532	.17561	-.165	.16148	.16154	-.037
60.364	82.364	82.334	+.036	.66703	.66616	+.130	.16540	.16535	+.030
29.932	78.419	78.440	-.027	1.2978	1.2992	-.108	.16786	.16790	-.024
14.564	74.862	74.891	-.039	2.5490	2.5529	-.153	.17120	.17126	-.035
5.0516	70.560	70.471	+.126	6.8746	6.8412	+.488	.17770	.17753	+.096

TABLE 6

FREON 22 PROPERTIES

P (PSIA)	H(BTU/LB)			V(CUFT/LB)			S(BTU/LB °F)		
	CALC.	ACTUAL	DEV. (%)	CALC.	ACTUAL	DEV. (%)	CALC.	ACTUAL	DEV. (%)
(SATURATED LIQUID)									
224.6	42.26	42.32	-.142	.01415	.01408	+.497	.0850	.0851	-.128
60.23	16.60	16.52	+.484	.01228	.01229	-.081	.0366	.0364	+.55
29.94	7.33	7.43	-1.35	.01174	.01174	.000	.0167	.0170	-1.76
14.54	-.51	-.51	.000	.01131	.01133	-.088	-.0012	-.0012	.000
5.100	-9.74	-9.72	-.206	.01090	.01091	-.092	-.0242	-.0242	.000
(SATURATED VAPOR)									
224.6	113.11	113.16	-.044	.2369	.2370	-.042	.2108	.2107	+.047
60.23	107.32	107.33	-.009	.9036	.9032	+.044	.2249	.2249	.000
29.94	103.62	103.70	-.077	1.753	1.752	+.057	.2319	.2321	-.086
14.54	100.24	100.23	+.010	3.443	3.440	+.087	.2402	.2400	+.083
5.100	95.94	95.92	+.021	9.104	9.086	+.198	.2528	.2526	+.079

CONCLUSIONS

A computer program is presented in this report to calculate sonic velocities in two-phase flow for one component fluids. This program is considered to be a satisfactory tool for two-phase flow studies, if reasonable discretion is used in the choice of data points and pressure ranges. The results from this program are presented for the Freon 12 and Freon 22 systems in both tabulated and graphical form.

For the two systems studied, no sonic choke was found to exist in the two-phase region. However, from common engineering practices it can be seen that systems for handling two-phase fluids might be under-designed if pure vapor sonic velocity is considered the limiting criterion.

The author recommends continued work in this field in the following order:

1. The use of the program to develop velocity curves for other common fluids.
2. Verification of these calculated results with laboratory tests.
3. Revision of the program to incorporate a least squares curve fit routine, for use when less accurate physical properties are available.

Of course the necessity of each of these steps will depend on the previous step confirming the importance of this study.

NOMENCLATURE

- A_a - Determinant with dependent variables in first column.
- A_b - Determinant with dependent variables in second column.
- A_c - Determinant with dependent variables in third column.
- A_d - Determinant with dependent variables in fourth column.
- A_e - Determinant with dependent variables in fifth column.
- B - Determinant with all independent variables.
- E - Internal energy.
- G - Mass velocity.
- G_{max} - Sonic mass velocity - lb/sq.ft. sec.
- H - Enthalpy of vapor-liquid mixture above saturated liquid
@ -40°F., BTU/lb.
- H_L - Enthalpy of saturated liquid above saturated liquid
@ -40°F., BTU/lb.
- H_V - Enthalpy of saturated vapor above saturated liquid
@ -40°F., BTU/lb.
- P - Pressure, 1b/sq.in. Absolute.
- P₁ - .975 P, 1b/sq.in. Absolute.
- P₂ - 1.025 P, 1b/sq.in. Absolute.
- Q - Vapor quality, %
or Binary point
- S - Entropy of vapor-liquid mixture above saturated liquid
@ -40°F., BTU/lb. °F.
- S_L - Entropy of saturated liquid above saturated liquid
@ -40°F., BTU/lb. °F.

s_q - Entropy of vapor-liquid mixture at quality, Q, above saturated liquid @ -40°F., BTU/lb. °F.

s_v - Entropy of saturated vapor above saturated liquid, @ -40°F., BTU/lb. °F.

u - Linear velocity, ft./sec.

v - Volume of vapor-liquid mixture, Cu.Ft./lb.

v_L - Volume of saturated liquid, Cu.Ft./lb.

v_{max} - Fictitious sonic velocity - $G_{max} \times v_v$, Ft./sec.

v_v - Volume of saturated vapor, Cu.Ft./lb.

w - Work done on a system.

a - Zero order coefficient.

a_{mn} - Value of X or Y in row M, column N of determinant.

b - First order coefficient.

c - Second order coefficient.

d - Third order coefficient.

e - Fourth order coefficient.

x - Independent variable.

y - Dependent variable.

α - A particular computer location.

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4. Harvey, B.F. and Foust, A.S., Two-Phase One Dimensional Flow Equations and Their Application to Flow in Evaporator Tubes, Heat Transfer Symposium Series No. 5, Vol. 49.
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6. Schwepple, J.L. and Foust, A.S., Effect of Forced Circulation Rate on Boiling - Heat Transfer and Pressure Drop in a Short Vertical Tube, Heat Transfer Symposium Series No. 5, Vol. 49.
7. Shapiro, A.H., The Dynamics and Thermodynamics of Compressible Fluid Flow, Vol. 1, pp. 45-49, The Ronald Press Co., New York (1953).
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A P P E N D I X

CURVE FIT SUBROUTINE

Discussion

The Curve Fit Subroutine was developed to solve for the coefficients of a fourth order log-log or semi-log polynomial and solve for the dependent variable from these coefficients and any value of the independent variable.

The coefficients are calculated by substituting five values of X and the corresponding values of Y into the equation.

$$Y = a + 10^{-1}b(\ln x) + 10^{-2}c(\ln x)^2 + 10^{-3}d(\ln x)^3 + 10^{-4}e(\ln x)^4$$

or the similar log-log equation. The five resulting simultaneous equations are solved for the five coefficients by the use of determinants of the form.

$$\begin{vmatrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} \\ a_{21} & a_{22} & a_{23} & a_{24} & a_{25} \\ a_{31} & a_{32} & a_{33} & a_{34} & a_{35} \\ a_{41} & a_{42} & a_{43} & a_{44} & a_{45} \\ a_{51} & a_{52} & a_{53} & a_{54} & a_{55} \end{vmatrix}$$

where each column represents a power of $\ln x$ or the five Y values.

The subroutine evaluates these determinants by reducing each to twenty minor determinants of third order and substituting values of X and Y.

It should be noted that this is not a curve fit in the true sense. i.e. it is not a least squares curves fit. Therefore, it is not the purpose of this subroutine to obtain a smooth curve from scattered data points, but to calculate coefficients by inputting reliable smooth data. The necessity of having smooth data points should be kept in

mind when using this routine.

The evaluation of the dependent variable from given coefficients and a value of the independent variable is a straight forward substitution in the polynomial.

DESCRIPTION

Function:

- A. To compute the constants for the 4th order eqn:

$$Y := a + 10^{-1}b(\ln x) + 10^{-2}c(\ln x)^2 + 10^{-3}d(\ln x)^3 + 10^{-4}e(\ln x)^4$$

$$\text{or } \ln Y := a + 10^{-1}b(\ln x) + 10^{-2}c(\ln x)^2 + 10^{-3}d(\ln x)^3 + 10^{-4}e(\ln x)^4$$

- B. To calculate the value of Y for any value of X using one of the two above equations and the constants calculated in Function A.

Input:

- A. Five values of X and the corresponding values of Y in sequence @ q := 12.
 B. Any value of X @ q := 12.

Calling Sequence:

A. Solve for Constants			B. Solve for Y		
<u>Location</u>	<u>Order</u>	<u>Address</u>	<u>Location</u>	<u>Order</u>	<u>Address</u>
$\alpha - 2$	Z	$L(X_1)$			
$\alpha - 1$	B	$L("a")$			
α	R	2855	α	R	3231
$\alpha + 1$	U	2000	$\alpha + 1$	U	3132

For Function A the address portion of location " $\alpha - 2$ " must be the first location in the consecutive storage of 5 values of X and the corresponding values of Y. Instruction " $\alpha - 1$ " brings into the accumulator the first address for the desired storage of the constants.

For Function B the value of X for which Y is to be calculated must be stored in location 6262 @ q = 12.

For either function the flag in 3303 must be set at 0 for a semi-log function and at 1 @ 29 for a log-log function.

Output:

Function A: The constants a, b, c, d & e @ q = 12 in sequence beginning at the location established by " -1" of the calling sequence.

Function B: The value of Y in 6262 and in the accumulator @ q = 12.

Storage:

Locations 2000 to 3316

Temporary Storage - 6200 to 6263, 6300, 01, 02, 03, 04, 05, 28, 29, 33, 34, 35, 36, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 55, 56, 57, 58, 60, 61

Program Stops:

4029 - Constant or Y value too large to hold at q = 12.

Subroutines:

Data InputRoutine #3	(11.2)	0300 to 0563
Data Output Routine #2	(12.1A)	0600 to 0850

Extended Range Floating Point

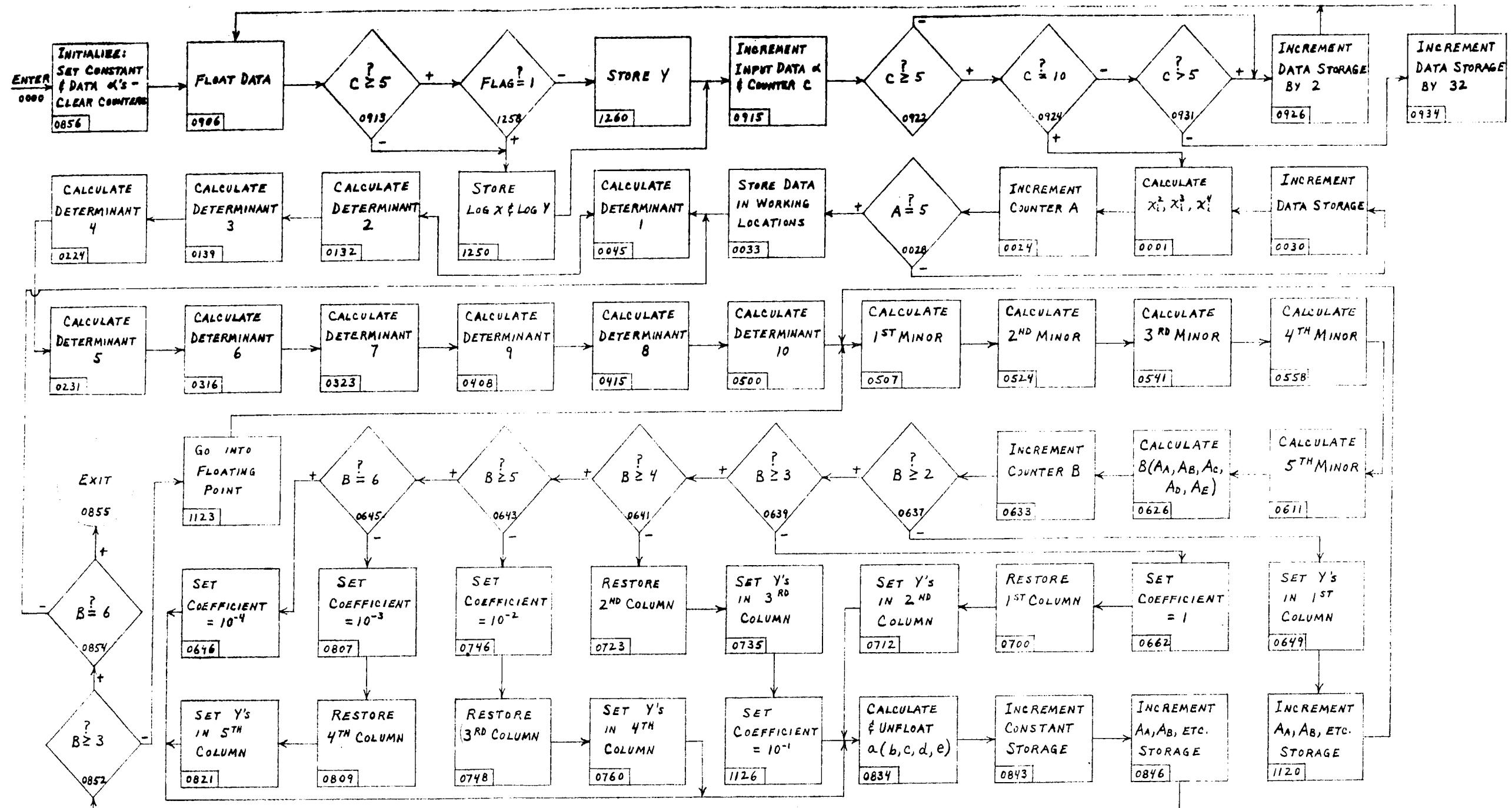
Interpretive Routine	(24.1)	0900 to 1963
Curve Fit		2000 to 3316
Data Output Driver		3332 to 3363
Logarithm	(18.2)	3419 to 3463
Exponential	(17.2)	3500 to 3663
Alphanumeric	(19.0)	3700 to 3757

Float & Unfloat	(25.1)	3800 to 4143
Decimal Memory Print Out	(21.0)	5500 to 5863

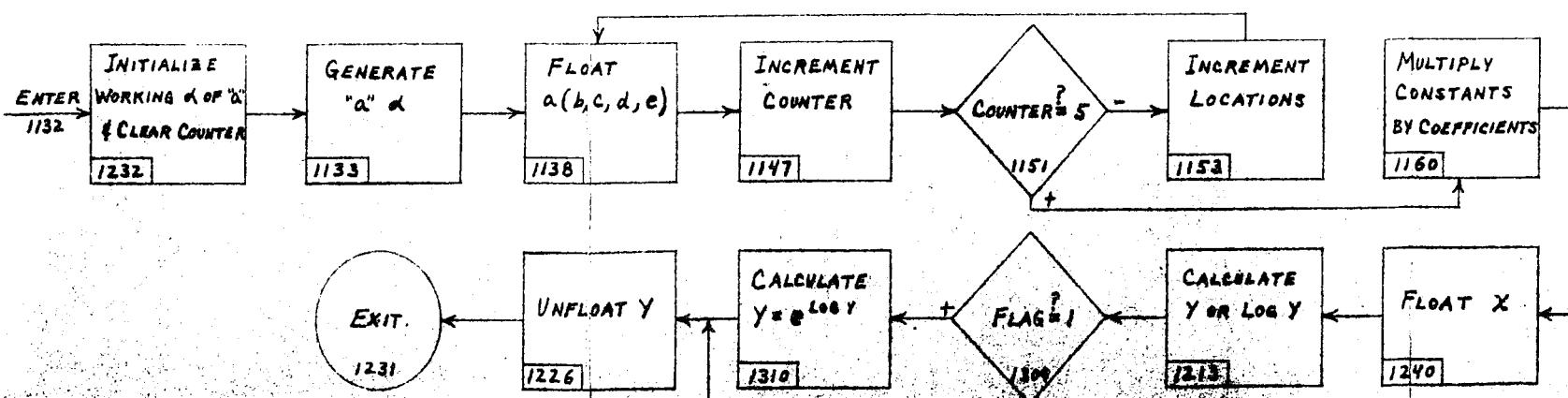
FIGURE 5

CURVE FIT SUBROUTINE - BLOCK DIAGRAM

(FUNCTION A)



(FUNCTION B)



LGP-30 CODING SHEET

PREPARED FOR:				PAGE	1 / 30	
JOB NO.	PROGRAM NO.	PROGRAM PREPARED BY:	PROGRAM CHECKED BY:	DATE:	5/1/68	
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PROGRAM INPUT CODES	LOCATION	INSTRUCTION		STOP	CONTENTS OF ADDRESS	NOTES
		OPERATION	ADDRESS			
10002000						
10002000	X					
	0,0,0	U0856	INITIALIZE \$ FLOAT DATA			
	0,1	B0725	X, A		(0925)	
	0,2	Y0014			(0032)	
	0,3	Y0015	X			
	0,4	Y0018				
	0,5	Y0021				
	0,6	A0956	10@29			
	0,7	Y0016	X			
	0,8	A0956	10@29			
	0,9	Y0019				
	1,0	A0956	10@29			
	1,1	Y0022	X			
	1,2	XR0900			ERFP	
	1,3	XU0900				
	1,4	B00P[]	X _i			
	1,5	B00ML[]	X _i			
	1,6	B00HL[]	X _i ²			
	1,7	XU0000				
	1,8	B00ML[]	X _i			
	1,9	B00HL[]	X _i ³			
	1,20	XU0000				
	1,21	B00ML[]	X _L			
	1,22	B00HL[]	X _L ²			
	1,23	XE0000	X			
	1,24	B0936	COUNTER A			
	1,25	A0951	1@29			
	1,26	H0936	COUNTER A			
	1,27	S0955	X			
	1,28	T0034				
	1,29	U0032				
	1,30	V0044	X _i , A		(0028)	
	1,31	W0032	X			
	1,32	Z0032	2@29			
FORMATTING: = CONDITIONAL STOP CODE				CARRIAGE RETURN: X		

LGP-30 CODING SHEET

CODE		CARRYAGE RETURN		CONDITIONAL STOP CODE	
NO.	PROGRAM NO.	PROGRAM PREPARED BY:	PROGRAM CHECKED BY:	DATE	TRACK
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OE 3	2112				
OE 4	2112				
OE 5	2112				
OE 6	2112				
OE 7	2112				
OE 8	2112				
OE 9	2112				
OE 10	2112				
OE 11	2112				
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LGP-30 CODING SHEET

LGP-30 CODING SHEET

GP-30 CODING SHEET

LGP-50 CODING SHEET

GE-P-30 CODING SHEET

LGP-30 CODING SHEET

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LGP-30 CODING SHEET

FEP-30 CODING SHEET

LGP-50 CODING SHEET

LGP-30 CODING SHEET

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LGP-30 CODING SHEET

PREPARED FOR

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100

CURVE FIT

PAGE	16	/	30
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TRACK	27		

LGP-30 CODING SHEET

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17 / 30DATE
5/1/63TRACK
28

JOB NO. PROGRAM NO. PROGRAM PREPARED BY: PROGRAM CHECKED BY:

PROBLEM: CURVE FIT

PROGRAM INPUT CODES	STOP	LOCATION	INSTRUCTION		STOP	CONTENTS OF ADDRESS	NOTES
			OPERATION	ADDRESS			
		X					
	0	0 0 0	8 0 0 B 1 0 5 4			y_3	
	1	0 1	8 0 X H 6 2 3 4			a_{34}	
	2	0 2	8 0 0 B 1 0 5 6			y_4	
	3	0 3	8 0 X H 6 2 3 6		X	a_{44}	
	4	0 4	8 0 0 B 1 0 5 8			y_5	
	5	0 5	8 0 X H 6 2 3 8			a_{54}	
	6	0 6	V 0 8 3 4				
	7	0 7	B 1 0 6 2		X	$\alpha \text{ of } 10^{-3}$	(0645)
	8	0 8	Y 0 8 3 6			A_0	
	9	0 9	X R 0 9 0 0			{ ERFP	
	10	1 0	X U 0 9 0 0				
	11	1 1	8 0 0 B 1 0 3 0		X	x_1^3	
	12	1 2	8 0 X H 6 2 3 0			a_{14}	
	13	1 3	8 0 0 B 1 0 3 2			x_2^3	
	14	1 4	8 0 X H 6 2 3 2			a_{24}	
	15	1 5	8 0 0 B 1 0 3 4		X	x_3^3	
	16	1 6	8 0 X H 6 2 3 4			a_{34}	
	17	1 7	8 0 0 B 1 0 3 6			x_4^3	
	18	1 8	8 0 X H 6 2 3 6			a_{44}	
	19	1 9	8 0 0 B 1 0 3 8		X	x_5^3	
	20	2 0	8 0 X H 6 2 3 8			a_{54}	
	21	2 1	8 0 0 B 1 0 5 0			y_1	
	22	2 2	8 0 X H 6 2 4 0			a_{15}	
	23	2 3	8 0 0 B 1 0 5 2		X	y_2	
	24	2 4	8 0 X H 6 2 4 2			a_{25}	
	25	2 5	8 0 0 B 1 0 5 4			y_3	
	26	2 6	8 0 X H 6 2 4 4			a_{35}	
	27	2 7	8 0 0 B 1 0 5 6		X	y_4	
	28	2 8	8 0 X H 6 2 4 6			a_{45}	
	29	2 9	8 0 0 B 1 0 5 8			y_5	
	30	3 0	8 0 X H 6 2 4 8			a_{55}	
	31	3 1	V 0 8 3 4		X		

* = CONDITIONAL STOP CODE

X = CARRIAGE RETURN

G-30 CODING SHEET

LGP-30 CODING SHEET

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5/1/63

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PROGRAM INPUT CODES		LOCATION	INSTRUCTION	CONTENTS OF ADDRESS	NOTES
STOP	OPERATION		ADDRESS		
		X			
		0 9 0 0	U 1 1 1 6		
		0 1	Y 1 2 5 3		(1119)
		0 2	X C 6 3 0 0		(1302)
		0 3	C 0 9 3 6	X COUNTER A	
		0 4	C 0 9 3 7	X COUNTER B	
		0 5	C 0 9 3 8	X COUNTER C	
		0 6	B []		(1302)
		0 7	X R 3 8 1 6	X	
		0 8	X U 3 8 0 0		
		0 9	X Z 0 9 0 0		
		1 0	X Z 0 0 1 2		
		1 1	B 0 9 3 8	X COUNTER C	
		1 2	S 0 9 5 5	5@29	
		1 3	T 1 2 5 0		
		1 4	U 1 2 5 6		
		1 5	B 0 9 0 6	X	(1255,1300)
		1 6	A 0 9 5 1	1@29	
		1 7	Y 0 9 0 6		
		1 8	B 0 9 3 8	X COUNTER C	
		1 9	A 0 9 5 1	X 1@29	
		2 0	H 0 9 3 8	X COUNTER C	
		2 1	S 0 9 5 5	5@29	
		2 2	T 0 9 2 6		
		2 3	S 0 9 5 5	X 5@29	
		2 4	T 0 9 3 0		
		2 5	U 0 0 0 1		(DATA COMPLETE)
		2 6	B 0 9 5 2	2@29	(0922,0932)
		2 7	A 1 2 5 3	X	(0935)
		2 8	Y 1 2 5 3		
		2 9	U 1 3 0 1		
		3 0	A 0 9 5 4	4@29	(0924)
		3 1	T 0 9 3 4	X	

FORMAT-10:

= CONDITIONAL STOP CODE

X CARRIAGE RETURN

LGP-30 CODING SHEET

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LGP-30 CODING SHEET

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JOB NO.	PROGRAM NO.	PROGRAM PREPARED BY:	PROGRAM CHECKED BY:	DATE 5/1/63
PROBLEM:				TRACK 30

CURVE FIT

PROGRAM INPUT CODES	L O C A T I O N S T O P	INSTRUCTION		L O C A T I O N S T O P	CONTENTS OF ADDRESS	NOTES
		OPERATION	ADDRESS			
10000010	1000	40000000		1		
	01	4				
	02	40000000		1		
	03	4				
	04	40000000		1		
	05	4				
	06	40000000		1		
	07	4				
	08	40000000		1		
	09	4				
	10	[]			x_1	
	11	[]			x_2	
	12	[]			x_3	
	13	[]			x_4	
	14	[]			x_5	
	15	[]				
	16	[]				
	17	[]				
	18	[]				
	19	[]				
	20	[]			x_1^2	
	21	[]			x_2^2	
	22	[]			x_3^2	
	23	[]			x_4^2	
	24	[]			x_5^2	
	25	[]				
	26	[]				
	27	[]				
	28	[]				
	29	[]				
	30	[]			x_1^3	
	31	[]				

FEP-30 CODING SHEET

LGP-30 CODING SHEET

TCP-30 CODING SHEET

LGP-30 CODING SHEET

LG-P-30 CODING SHEET

LGP-30 CODING SHEET

TGP-30 CODING SHEET

LGP-20 CODING SHEET

LGP-30 CODING SHEET

TO PAGE		30	
DATA		PROGRAMMING SHEET	
MACHINING		MACHINING	
OPERATION		OPERATION	
LOCATOR		LOCATOR	
CODES		CODES	
MATERIAL		MATERIAL	
TIME		TIME	
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LGP-30 CODING SHEET

OB 35	35	35	35
OB 36	36	36	36
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OB 236	236	236	236
OB 237	237	237	237</

TGP-30 CODING SHEET

Routine No.

Assignment

Circuit List (FUNCTION A)

Track 62

Sec-tor	Quantity	Q
00	a_{11}	
01		
02	a_{12}	
03		
04	a_{13}	
05		
06	a_{14}	
07		
08	a_{15}	
09		
10	a_{21}	
11		
12	a_{22}	
13		
14	a_{23}	
15		
16	a_{24}	
17		
18	a_{25}	
19		
20	a_{31}	
21		
22	a_{32}	
23		
24	a_{33}	
25		
26	a_{34}	
27		
28	PROB. a_{35}	
29		
30	a_{41}	
31		

Sec-tor	Quantity	Q
32	a_{42}	
33		
34	a_{43}	
35		
36	a_{44}	
37		
38	a_{45}	
39		
40	a_{51}	
41		
42	a_{52}	
43		
44	a_{53}	
45		
46	a_{54}	
47		
48	a_{55}	
49		
50	DETERMINANT 1	
51		
52	DETERMINANT 2	
53		
54	DETERMINANT 3	
55		
56	DETERMINANT 4	
57		
58	DETERMINANT 5	
59		
60	DETERMINANT 6	
61		
62	DETERMINANT 7	
63		



CONDITIONAL STOP CODE

-100-

FORM LP-10

OE to 85 P.M.

Debt and the American Dream

Лондонъ

Routine No.

Data Structure Analysis

Page 27 of 30

(A) MONTGOMERY T. R. BURGESS

maiden problems

CURVE & FIT

• 18 (1987)

Sec- tor	Quantity	Q
00	[DETERMINANT 8]	
01		
02	[DETERMINANT 9]	
03		
04	[DETERMINANT 10]	
05		
06		
07		
08		
09		
10		
11		
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14		
15		
16		
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18		
19		
20		
21		
22		
23		
24		
25		
26		
27		
28	[PRODUCT 4]	
29		
30		
31		

Sec- tor	Quantity	Q
32		
33	[PRODUCT 5]	
34		
35	[PRODUCT 6]	
36		
37		
38		
39		
40		
41		
42		
43	[PRODUCT 7]	
44		
45	[PRODUCT 8]	
46		
47	[PRODUCT 9]	
48		
49	[PRODUCT 10]	
50		
51	[PRODUCT 11]	
52		
53		
54		
55	[PRODUCT 12]	
56		
57	[PRODUCT 1]	
58		
59		
60	[PRODUCT 2]	
61		
62		
63		

CURVE FIT

model problem

CURVE FIT (FUNCTION B)

S. J. MONT

1. TOWER	10
2. TOWER	11
3. TOWER	12
4. TOWER	13
5. TOWER	14
6. TOWER	15
7. TOWER	16
8. TOWER	17
9. TOWER	18
10. TOWER	19
11. TOWER	20
12. TOWER	21
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18. TOWER	27
19. TOWER	28
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21. TOWER	30
22. TOWER	31
23. TOWER	32
24. TOWER	33
25. TOWER	34
26. TOWER	35
27. TOWER	36
28. TOWER	37
29. TOWER	38
30. TOWER	39
31. TOWER	40
32. TOWER	41
33. TOWER	42
34. TOWER	43
35. TOWER	44
36. TOWER	45
37. TOWER	46
38. TOWER	47
39. TOWER	48
40. TOWER	49
41. TOWER	50
42. TOWER	51
43. TOWER	52
44. TOWER	53
45. TOWER	54
46. TOWER	55
47. TOWER	56
48. TOWER	57
49. TOWER	58
50. TOWER	59
51. TOWER	60
52. TOWER	61
53. TOWER	62
54. TOWER	63

1. TOWER	10
2. TOWER	11
3. TOWER	12
4. TOWER	13
5. TOWER	14
6. TOWER	15
7. TOWER	16
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45. TOWER	54
46. TOWER	55
47. TOWER	56
48. TOWER	57
49. TOWER	58
50. TOWER	59
51. TOWER	60
52. TOWER	61
53. TOWER	62
54. TOWER	63

Track 62

Sector	Quantity	Q
00		
01		
02		
03		
04		
05		
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Sector	Quantity	Q
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48		
49		
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51		
52	[a]	
53		
54	[b OR 10^b]	
55		
56	[c OR 10^c]	
57		
58	[d OR 10^d]	
59		
60	[e OR 10^e]	
61		
62	[x]	
63		

FIXED
POINT
OR
FLOATING
POINT

08 to 09

(B) FUNCTION (CURVE FIT)

55 Start

Q	Y	Q	Y
	55		55
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	37		

followed by the word "constants", the input values of X on the fourth line and the calculated values of Y on the fifth line. At this point the computer stops at data input for function C. The constants are held in 5425 to 5429 at a q of 12. They are also held in 5415 through 5424 in Extended Range Floating Point Format #2.

- C. The 5 input values of X on the first line and the 5 calculated values of Y on the next line. At this point the computer stops at data input to repeat function C for 5 more values of X. The values of Y are held in 5410 to 5414 at a q of 12.

Storage:

Locations 5200 through 5441

No temporary storage.

Program Stops:

4029 - Constant or Y value too large to hold at q = 12.

Subroutines:

Data Input Routine #3	(11.2)	0300 to 0563
Data Output Routine #2	(12.1A)	0600 to 0850
Extended Range Floating Point		
Interpretive Routine	(24.1)	0900 to 1963
Curve Fit		2000 to 3316
Data Output Driver		3332 to 3363
Logarithm	(18.2)	3419 to 3463
Exponential	(17.2)	3500 to 3663
Alphanumeric	(19.0)	3700 to 3757

Float and Unfloat (25.1) 3800 to 4143

Decimal Memory Print Out (21.0) 5500 to 5863

Note:

This program is part of the major Sonic Velocity Program.

SONIC VELOCITY - HEX PUNCH

FORMS FILE - WILLOW GLEN, CALIF.

0005800
 03000763
 v1400300'104fj'k03g0'80098'40000'j05gj'g0354'
 w05f8'f0320'g0300'q0598'60074'90484'
 j3w08'903f8'70590'f0340'q3w08'j3w0j'
 903f0'703f4'f0360'303g0'f0328'80'
 q3w0j'2045j'w04kj'905j4'g0380'k3w04'
 w3w04'f0384'q05w4'704w8'j0478'f0394'
 78'1055j'905gj'f03fj'wwwwo0'f0000000'
 3j3j3j0'70520'q0578'j3w0j'70480'f03j0'
 q056j'203w0'10390'w0478'w3w0j'g0464'
 q044j'203q8'10570'20448'104w8'k0450'
 10538'k3w00'80050'40000'60574'70594'
 g0428'f0410'w04gj'g0494'q047j'305fj'
 f05g0'f0448'904g8'w04gj'g0300'q047j'
 305fj'f05g0'k3w0j'w3w0j'f0488'4j0'
 20000'53w00'703g0'k3kq0'f05q0'k3w10'
 105j0'20448'1044j'f049j'44f0'2'
 20000000'5wkjkj'50450'53w00'f045j'k3w08'
 f045j'w3w10'204f4'10300'f04g0'q0578'
 k03g0'f03w0'1wwwwoq'2'7wwwwoq'40000000'
 20000000'10000000'8000000'4000000'2000000'1000000'
 800000'400000'200000'100000'80000'40000'
 20000'10000'8000'4000'2000'1000'
 800'400'200'100'80'40'
 20'10'8'7wwwwoq'50000000'32000000'
 1w400000'13880000'j350000'7f12000'4j4g400'2wfwo80'
 lkjk650'70000000'1q1q1q0'1q01wq00'g2000000'534'
 f0488'8''q3w0j'j3w10'905w8'
 705wj'f059j'k0000000'2000000'4'q3w10'
 f05fj'300'4'f0424'j0478'90560'
 f05j8'12126146'f0454'wwwwo000'70590'q0478'
 j3w0j'90564'70568'f057j'105f8'q045j'
 k045j'800g0300'f03w8'1000000'1wwq0000'93880000'
 10614'w075j'2060j'130w8'207gj'1310j'
 907j4'w07fj'g0640'f0870'q07k4'907f0'
 706w8'q07q0'j0800'f07g0'q087j'j07k4'
 906w4'q07kj'206kj'106q4'f0628'107qj'
 r0680'81710'106j0'j0764'1081j'w0834'
 g081j'f0840'206k8'w0830'j0834'f06k0'
 q07qj'207qj'106w0'7072j'f07q8'80650'
 j0700'10774'60840'f06j4'3j00'80250'
 g0778'90770'j0774'f0740'j0700'1072j'
 50714'70738'f0858'j'q'4'
 8000000'j'2000000'4'7wwwwoq'
 50000000'32000000'1w400000'13880000'j350000'7f12000'
 4j4g400'2wfwo80'lkjk650'3q76j148'7wwwwoq'10000000'
 20000000'40000000'70808'906g8'q06gj'k06f4'
 w06wj'q0700'f0760'j'j'g0778'
 f06f4'4'7wwwwoq'1360k400'81808'1080j'
 q07gj'207gj'107k4'4'w0804'g07f4'
 j07k4'f0838'w0'10614'f0824'10000'
 207qj'10860'k0764'13kwj'f07j8'w3w7j'
 j0774'g0848'f0864'38'807j0'730'
 704'10774'j072j'w0714'q06q8'g065j'
 1076j'f0690'
 082kq504'

08001263
v1400800'714'100'2800'4'803j0'803j0'
f06j8'1j'f0778'q06qj'20614'f0614'
w0704'10'10800'f07g0'f'f06f4'
107k8'k0814'w0774'f07q8'q06q8'f0880'
g0664'10810'k0814'f07q4'10614'20878'
f310j'ww00'j072j'w08j0'g08j4'f08g8'
600'w06qj'g08g8'80310'j0700'1072j'
60840'j072j'40'f0884'1072j'f0814'
jjjjjjj'10700'f0894'k3w00'108qj'q08w8'
208w4'13w00'g08w4'w08wj'g2k78'q08wj'
f2k7j'4'2'10900'130kj'20fjj'
j3w44'710k4'q09gj'209j0'10kj4'f0920'
90fjj'w0jk0'f09j0'k3wf0'f0w70'j0f1j'
g1174'30f94'f0998'73w9j'j3wf0'f0f50'
k3wj'f0974'10fjj'912k0'w0jk4'g0950'
f0970'f0w78'10g00'q0fjj'20fk0'90w0j'
q112j'20fkj'f0f24'70qlj'w0jjj'f0ff8'
13w44'g0j20'f0958'3jwww850'3jwww850'3jwww850'
3jwww850'3jwww850'3jwww850'9j4'f09q8'f1000'
f0938'f115j'f0q60'f126j'f0w14'f0fgj'
f0j9j'f1334'f1234'f1360'f0f70'f0wg4'
f10g8'f0glj'g1w48'30f94'f0998'k3wk4'
w3wf0'71388'f0g2j'24'3wj'10fk0'
90jk4'q0k68'f0f38'10wwj'j0fq4'f0fk0'
40000'4'13wf0'f0dkj'13w18'j0flj'
f0jk8'3wwwwwq'10k0j'w122j'g0k08'f0jk8'
g0g44'109g0'g12qj'13w44'g12w4'f0q8j'
j3w18'j3w1j'10q58'f0w44'1384'ww00ww0'
20fkj'f0f34'q0flj'q1104'f12j4'20000000'
2'g224j'1096j'j0w70'f0w3j'
13gj0'j3w9j'j3wf0'13gj4'f0fq4'f0f88'
912g0'w1260'g11w4'w12f0'f0f88'10'
4'7135j'q0f98'20dk4'w0j68'g0kk4'
f0q8j'g213j'30f94'f0998'73w9j'j3wf0'
g0g3j'w13wj'g0q8j'109g0'g0gj0'w0fg8'
g0f50'f0gj0'4'j0flj'13w94'g0k28'
f0q30'24'2'10w34'q0900'f0q94'
3wwwwwq'q0gg8'6132j'k3w4j'w0fwj'q0flj'
f0g9j'40000000'3wwwwwq'j0flj'13w4j'g0kwj'
f0q3j'1024'w0f5j'f0j44'4000000'4'
13w18'w0flj'g0g04'q1108'20koj'w0j64'
g0f48'13w18'f1154'109fj'g0q8j'k3w98'
w09g8'f0jkj'900'q138j'61358'j3w94'
10flj'w0q9j'f0k54'23260'f0q8j'2000002'
10fjj'20fk0'q1180'f0ff0'f0q8j'
3wwwwwq'4'q10qj'711w0'j3wf0'10flj'
q0jwj'j0flj'f0jk8'k3w24'f0j80'1388'
13w8'j3w34'10flj'90f20'60f40'f0qkj'
k3q8'f10j4'j3w34'10flj'90f20'61208'
f0qkj'w0g64'g0ff8'10934'j0w70'f0w3j'
w0g78'q0q7j'g0k48'w0q84'f0j00'w0w00'
f1044'50'4'j'13wf0'j09f4'
j09f8'j09fj'j09g0'j09g4'j09g8'f0q8j'
400000'4'
02g06qfq'

13001763
v1400k00'w0k3j'fow64'109g4'71388'q3wf0'f0kq0'
lwwwwwq'q12fj'g0gg0'w0g98'q0kg8'g0kw8'
w0kj0'f0qj8'1gjf96'1wwwwwq'q09g4'f0j80'
woq84'f0jkj'j'jof1j'13w94'g0jg4'
f0q48'20'71294'q0k18'g0k00'w0k3j'
f0qw0'13w44'g1244'91230'w0k50'g0w04'
10fjj'q0q5j'f110j'13wk8'f11fj'j3w34'
10f1j'90f20'60q5j'f0qkj'3wwwq'3ww0'
3wwwq'3wwj'10900'90q78'f0j6j'1138j'
73wf0'q09f4'g0k1j'w1358'g0q0j'w0g98'
g0q2j'f0j40'w0kj0'q0j38'g0jg0'w0g78'
f0g80'k3w80'k3wf0'f0f54'1388'80000000'
lwwwwwq'13w7j'f121j'q11gj'w0jw8'g0qj4'
q1300'w0w94'g0g7j'q0gg8'w0qf0'g0gvj'
q138j'f0jkj'40000000'4'g10w0'q0ggj'
20j14'10qf8'q0900'f0j14'www0'1wwwwwq'
www000'1wwwwwq'f0f88'10900'q0j3j'20900'
f0900'4'20000000'24'8'k3w3j'
q3w40'20f44'f0q8j'6487qk50'2'q1300'
61320'k3w94'10f1j'w0k64'f0g54'q3w34'
j3qwj'109fj'f0k40'q0fg4'60fg8'k3wf0'
w0g50'f0w68'3wwwwwq'10fjj'f110j'3ww0'
34f253ko'w0qf4'g098j'10gfj'20f94'f0998'
q11w0'k3wf0'f1050'8'900'30r94'
f0998'13w9j'70w10'g0k6j'w13wj'g10jj'
w0q20'g0qqj'q129j'k3wf0'q10f4'q3w18'
j0f1j'f0jk8'j3w18'13wf0'f0g30'q0ww8'
g0jj4'w0w00'f0w2j'4000000'10f44'f0wf0'
2210j'f0q8j'40000000'73w58'f10k8'g2300'
11380'20j84'f0k7j'10f1j'g113j'w1324'
g1144'f0j30'91230'w0g50'g0kj8'w0j3j'
g105j'10900'90q80'f0kf4'3wwwwwq'f0f88'
g1068'10fjj'w0f44'g0q8j'w0g68'g0g6j'
f0q8j'900'1384'109g4'53w9j'g0w84'
w0qj0'g0q0j'w0w00'g0w28'q10qj'71lw0'
j3wf0'113w8'w3w18'q0f1j'f0f54'10900'
90f9j'f0j88'1000'f0q0j'10f1j'f1078'
j3w40'109g8'31kgj'flgwj'10g50'q0900'
20900'f116j'10f44'20900'f0q8j'18'
10900'q0j3j'210g4'f30q0'g2048'30j84'
f0k7j'k0f1j'f0jkj'k3w94'f092j'20000'
j3wf0'f10q0'10f1j'70q58'f0f54'40000000'
109g8'g12gj'w0qj0'g0q8j'f11j4'28'
1384'20j80'90kgj'q0k50'20qq0'20kj8'
2105j'20wqj'f0wj4'j'58g90j00'10'
1088'q12jj'g0j5j'10j80'f0wk8'j10f4'
f0q8j'j0f1j'f0f60'g0gqj'q0q9j'20wf0'
f0w98'f0900'109g0'g0gqj'f0q8j'
4'q13w8'20900'f0900'w3w58'g0q24'
111w0'f0wfj'k3w68'w3w6j'f0k1j'53w58'
q3wqj'j3w7j'f1190'40000000'g8ff3g2'10f1j'
90j3j'w0q5j'g120j'10q9j'q0f1j'f11q0'
j0f1j'109fj'70g94'f1210'40000000'q12f0'
f0f88'11138'
1kj23810'

18002263
v1401200'21f84'f1408'400'109g8'j3wk8'109f4'
q0wf8'j3w58'70g94'j3wqj'f0k9j'713w8'
j'gl0f8'q0g00'21378'f1378'20j80'
q0ggj'f1250'20qq0'10flj'f0qq0'62ggqwf'
200'j0w10'f128j'g11wj'q0g00'q0f44'
23w40'13w44'g0qfj'f1304'jj40f5r'10flj'
f1368'2000'200000'20000000'200'18'
713w0'3wwwwwq'3wj'78'68'
f0q8j'jofl1j'f0q8j'1wj'j'10w10'
j3wf0'110f4'j3wf8'109fj'f1264'13w44'
f1188'90q84'800g1188'f0q8j'400000'13w40'
912ko'w0jk4'g0qfj'10g50'f0qg0'
100'200'3k8q24j'10'g1070'
f133j'30f94'f0998'73w9j'j0w10'f1350'
13w18'f114j'2'80000000'g12k4'f1184'
j10f4'13wf8'jofl1j'f0jk8'13300'20f44'
f0q8j'7wwwwwq'40000000'20000000'10000000'8000000'
4000000'2000000'1000000'800000'400000'200000'
1000000'800000'40000'20000'10000'8000'
4000'2000'1000'800'400'200'
100'80'40'20'10'8'
4'2'f1jq0'11g64'21438'2143j'
21448'21454'qlkq0'21440'qlkq0'2144j'
qlkq0'21458'30900'f0900'80080000'80070000'
800j0000'f0000'80070000'800j0000'f0000'80070000'
800j0000'90000'11k90'qlkj'jlk90'wlkkj'
g1478'f1484'11438'qlkk0'f1408'11w20'
21494'qlqwj'21498'10000'j0000'11w24'
w1494'g14g4'11494'qlkj'f1488'30900'
f0900'80083q90'80073qj0'f0000'80073q60'800j3wq4'
80073q58'800j3wqj'80083q68'80073q98'f0000'80073qg0'
800j2110'80073qf8'800j3w70'80083q70'80073qg8'f0000'
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f0000'80073q60'800j3wfj'80073q58'800j3wg4'80083q68'
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 3207j'f1w80'j32w0'13kg4'53384'j32w4'
 732w0'53378'j32jj'13378'w32w4'732qj'
 53378'q32jj'j3kg8'13kg0'k3qw8'k210j'
 13g50'3207j'f1w80'j32q4'13kg0'k3qw8'
 13300'k210j'13g64'3207j'f1w80'j32q8'
 732w4'53378'j32jj'13378'w32w4'732q4'
 53378'q32jj'j3kgj'30900'f0900'80083j28'
 8073gj0'90000'326jj'f2820'900'38'
 j3kw8'800'13kg4'30614'f0600'430'
 238'f33j0'53384'w3378'g312j'81000'
 '13g78'f314j'q338j'32640'f2600'
 900'4'30900'f0900'f2q34'w3300'
 j3g78'f36gj'q3324'22j64'f2j64'1000'
 30320'f0300'13kg8'f2j68'k3w00'k3264'
 k3268'k326j'k3270'k3kg4'k3kg8'k3kgj'
 k3kj0'k3kj4'k3kj8'k3kjj'k3kk0'k3kk4'
 k3kj8'k3kj'1331j'j32j4'12g80'j1j94'
 f2f04'90000'13320'231w8'13260'w3308'
 231q4'12g20'231w4'30900'f0900'80013jf8'
 800k3qw0'90000'13270'q3300'j3270'w3310'
 g3228'13340'j20j4'13344'j2068'f33f4'
 131w4'q3304'231w4'131w8'q3304'231w8'
 f31qj'13348'j20j4'1334j'k2068'k3270'
 30900'f0900'f2q2j'!!!
 !!!
 !!!
 !!!
 !!!
 4f2j10'
 10'94w36300'wwwww8'46q08388'wwwwwj'1654'
 4f2j12'wvg0kk6f'2wqq334'40000000'!!!
 4'8'j'10'14'28'
 3j'3k00'3qk0'3kg4'3kkj'3g28'
 3j60'3274'3g00'f2g58'f2034'f3244'
 f209j'326jj'40000000'4'
 4199999f'4'7jjjj000'4411qg80'1j'
 40000000'20000000'2'6400000'100000'46666668'
 j1j94'f2g08'12,j98'22,j64'f2j58'30900'
 f0900'80013qw8'60000'800k3qw8'90000'f1ww0'
 81000'81800'13kg4'f3110'
 80013j30'800j3g88'80013j38'800j3g90'80013j40'800j3g98'
 80013j48'800j3g70'80013j50'f36f8'13680'j1j94'
 13684'j20j4'f3418'30320'f0300'
 13614'1347j'31jkj'f1400'f3464'90000'
 11jf8'w3494'73378'5337j'q349j'23458'
 30900'f0900'800j0000'90000'f1j98'800'
 13614'30614'f0600'530'81000'3664'
 13628'30614'f0600'530'81000'3664'
 81000'363j'13664'30614'f0600'530'
 32500'f2500'30106108'46327f5f'72325f7f'20207q00'
 1349j'234wj'13550'23500'13568'23524'
 k3w00'k3678'k367j'136f0'f369j'30900'
 f0900'80010000'
 1kgqj98'

53005463
v0803500'800k0000'90000'13678'q3300'j3678'w3310'
g35k8'3207j'f1ww0'j0000'1367j'q3300'
j367j'w3310'g35f0'13614'30614'f0600'
530'81000'3qk0'13628'30614'f0600'
530'81000'3628'81000'13688'
j1j94'1368j'j20j4'f358j''30320'
f0300'13684'j20j4'f34j8'13524'f3690'
135g4'q3300'235g4'10000'32640'f2600'
900'30'f2024'!!!
134wj'q3304'234wj'13500'q3304'23500'
f34wj'32640'f2600'900'30'30900'
f0900'800j3qw8'f34wj'!!!
!!!!!!
!!!!!!
!!!!!!
f3434'f213j'90000'f209j'q3300'23524'
f35f8'235g4'13614'f35w4'800j3gf8'80013j58'
800j3gg0'80083gw8'f2q3j'w3300'g3164'q3300'
f3158'13328'w326j'22j64'f2j58'w3q34'
f3g7j'f377j'f3770'376j8g44'1000'999999f'
7vkw3g64'50w08'
03918448'

LGP-30 DATA LOAD SHEET

RECEIVED
PAGE 1 / 2
JULY NO. PROGRAM NO. PROGRAM PREPARED BY: PROGRAM CHECKED BY: DATE
5/20/63
PROBLEM DATA INPUT NO.
SONIC VELOCITY OF FREON - 12 3

NOTES	P ± q	LOCATION	S ±	NUMBER	STOP CODE RET
P ₁	3 + 1 2 6 1 0 0 '			2 0 5 1 '	
P ₂				1 0 3 2 0 '	✗
P ₃				3 9 3 1 0 '	
P ₄				1 2 1 2 2 0 '	✗
P ₅				2 4 6 4 0 0 '	
H _{L1}			-	- 0 0 1 0 4 0 9 '	✗
H _{L2}				8 4 3 '	
H _{L3}				1 3 9 5 8 '	✗
H _{L4}				2 9 6 6 3 '	
H _{L5}				4 3 5 7 8 '	✗
H _{V1}				6 7 3 5 5 '	
H _{V2}				7 3 3 5 4 '	✗
H _{V3}				7 9 9 0 4 '	
H _{V4}				8 6 5 2 1 '	✗
H _{V5}				9 0 4 8 2 '	
				- 0 0 0 0 0 0 0 "	✗
P ₁	3 + 1 2 6 1 1 5 '			2 0 5 1 '	
P ₂				1 0 3 2 0 '	✗
P ₃				3 9 3 1 0 '	
P ₄				1 2 1 2 2 0 '	✗
P ₅				2 4 6 4 0 0 '	
S _{L1}	6 + 1 2 6 1 2 0 '	- 0 0 2 6 3 6 7 '			
S _{L2}		1 0 0 1 9 9 5 '			
S _{L3}		1 0 3 0 7 7 2 '			
S _{L4}		1 0 6 0 6 9 0 '			
S _{L5}		1 0 8 4 0 9 6 '			
S _{V1}		1 1 8 3 9 8 0 '			
S _{V2}		1 1 7 3 1 3 0 '			
S _{V3}		1 1 6 6 8 3 0 '			
S _{V4}		1 1 6 3 3 8 0 '			
S _{V5}		1 1 6 1 1 5 0 '			

05-p-130
-20-59-547
COMPUTER SYSTEMS

LGP-30 DATA LOAD SHEET

2 / 2

DATE 5/20/68

DATA INPUT NO

SONIC VELOCITY OF FREON - 12

NOTES	P ± q	LOCATION	STOP ± -	NUMBER	STOP CGO RET
				- 0 0 0 0 0 0 0	"
P ₁	3 + 1 2 6 1 3 0'			2 0 5 1 '	✗
P ₂				1 0 3 2 0 '	
P ₃				3 9 3 1 0 '	
P ₄				1 2 1 2 2 0 '	
P ₅				2 4 6 4 0 0 '	✗
				- 0 0 0 0 0 0 0	'
V _{L1}	6 + 1 2 6 1 3 5'			0 1 0 0 7 3 '	✗
V _{L2}				0 1 0 6 0 7 '	
V _{L3}				0 1 1 3 6 6 '	✗
V _{L4}				0 1 2 5 6 2 '	
V _{L5}				0 1 4 0 4 3 '	✗
				- 0 0 0 0 0 0 0	'
V _{V1}	5 + 1 2 6 1 4 0'			1 5 8 2 1 0 0	'
V _{V2}				3 5 1 9 8 0	'
V _{V3}				1 0 0 3 9 0	✗
V _{V4}				3 3 5 4 0	'
V _{V5}				1 5 7 7 4	'
				- 0 0 0 0 0 0 0	'
ISOBAR #1	1 + 1 2 6 1 4 6'			2 2 5 0	'
2				1 5 0 0	'
3				1 0 0 0	'
4				6 0 0	'
5				4 5 0	'
6				3 0 0	'
7				2 0 0	✗
8				1 4 7	'
9				1 0 0	✗
10				5 0	'
				- 0 0 0 0 0 0 0	"

05 p 59
-2514247
www Loc S 0003

-119-

$$e \geq q \geq 0$$

$$r \geq p \geq 85$$

$$eae \geq eae \geq 0000$$

**PUNCH A
STOP CODE AFTER
THE LAST NUMBER!**

NO

1978-08-05 08:00:00 1978-08-05 08:00:00

LGP-30 DATA LOAD SHEET

SONIC ACTIVE LINE 94 FEBRUARY - 19

PUNCH A
STOP CODE AFTER
THE LAST NUMBER
 NO YES

TGP-30 DATA LOAD SHEET

SOME FEATURES OF REGION - 15

PUNCH A
STOP CODE ALTEER
THE LAST NUMBER
NO

-211-

$$\begin{aligned} & q \geq 0 \\ & r \geq p \geq rs \\ & 0000 \leq \text{val} \leq 0000 \end{aligned}$$

LGP-30 DATA LOAD SHEET

FEDERAL BUREAU OF INVESTIGATION - U. S. DEPARTMENT OF JUSTICE	
PAGE	OF
1 / 2	
DATE	
5/20/63	
DATA INPUT NO.	
3	

SONIC VELOCITY OF FREON - 22

NOTES	P ± 4	LOCATION	S ±	NUMBER	STOP CGE RET
P ₁	3 + 1 2 6 1 0 0'			4 7 8 7 '	
P ₂				1 6 9 7 0 '	
P ₃				5 1 5 9 0 '	
P ₄				1 2 1 0 0 0 '	
P ₅				2 4 3 4 0 0 '	
H _{L1}			-	0 0 1 0 2 2 0 '	
H _{L2}				1 0 5 0 '	
H _{L3}				1 4 3 6 0 '	
H _{L4}				2 8 4 6 0 '	
H _{L5}				4 4 3 5 0 '	
H _{V1}				9 5 6 8 0 '	
H _{V2}				1 0 0 9 3 0 '	
H _{V3}				1 0 6 5 0 0 '	
H _{V4}				1 1 0 9 3 0 '	
H _{V5}				1 1 3 2 9 0 '	
			-	0 0 0 0 0 0 0 "	
P ₁	4 + 1 2 6 1 1 5'			4 7 8 7 0 '	
P ₂				1 6 9 7 0 0 '	
P ₃				5 1 5 9 0 0 '	
P ₄				1 2 1 0 0 0 0 '	
P ₅				2 4 3 4 0 0 0 '	
S _{L1}			-	0 0 0 0 2 5 5 '	
S _{L2}				0 0 2 5 '	
S _{L3}				0 3 1 9 '	
S _{L4}				0 6 0 0 '	
S _{L5}				0 8 8 6 '	
S _{V1}				2 5 3 5 '	
S _{V2}				2 3 8 3 '	
S _{V3}				2 2 6 4 '	
S _{V4}				2 1 8 1 '	
S _{V5}				2 0 9 6 '	
			-	0 0 0 0 0 0 0 "	

$$0 \leq p \leq 9 \\ -28 \leq q \leq 47 \\ 0000 \leq Loc \leq 0343$$

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**PUNCH A
STOP CODE AFTER
THE LAST NUMBER?**

GP-30 DATA LOAD SHEET

DATE	DATA	NUMBER	POINTAGE	P	Q	R	S	INFORMATION
2/26/83		1 6 8 7 4	1 0 0 1 9 5 1 7 8					1 6
		1 6 8 7 5						1 6
		1 6 8 7 6						1 6
		1 6 8 7 7						1 6
		1 6 8 7 8						1 6
		1 6 8 7 9						1 6
		1 6 8 8 0						1 6
		1 6 8 8 1						1 6
		1 6 8 8 2						1 6
		1 6 8 8 3						1 6
		1 6 8 8 4						1 6
		1 6 8 8 5						1 6
		1 6 8 8 6						1 6
		1 6 8 8 7						1 6
		1 6 8 8 8						1 6
		1 6 8 8 9						1 6
		1 6 8 9 0						1 6
		1 6 8 9 1						1 6
		1 6 8 9 2						1 6
		1 6 8 9 3						1 6
		1 6 8 9 4						1 6
		1 6 8 9 5						1 6
		1 6 8 9 6						1 6
		1 6 8 9 7						1 6
		1 6 8 9 8						1 6
		1 6 8 9 9						1 6
		1 6 8 9 0						1 6
		1 6 8 9 1						1 6
		1 6 8 9 2						1 6
		1 6 8 9 3						1 6
		1 6 8 9 4						1 6
		1 6 8 9 5						1 6
		1 6 8 9 6						1 6
		1 6 8 9 7						1 6
		1 6 8 9 8						1 6
		1 6 8 9 9						1 6
		1 6 8 9 0						1 6
		1 6 8 9 1						1 6
		1 6 8 9 2						1 6
		1 6 8 9 3						1 6
		1 6 8 9 4						1 6
		1 6 8 9 5						1 6
		1 6 8 9 6						1 6
		1 6 8 9 7						1 6
		1 6 8 9 8						1 6
		1 6 8 9 9						1 6
		1 6 8 9 0						1 6
		0 0 0 0 0 0 0						1 6

PUNCH A
STOP CODE AFTER
THE LAST NUMBER


- 05 -

$$\begin{aligned} & p \geq q \geq 0 \\ & \tau p \geq p \geq 0.5 \\ & 0.000 \geq \rho \geq 0.000 \end{aligned}$$

LGP-30 DATA LOAD SHEET

PREPARED FOR:								PAGE OF	
JOB NO.	PROGRAM NO.	PROGRAM PREPARED BY:		PROGRAM CHECKED BY:				DATE	
PROBLEM		SONIC VELOCITY OF FREON - 22						DATA INPUT NO	
NOTES	P	+/- Q	LOCATION	STOP	+/-	NUMBER	STOP	CGE	RET
P ₁	3	+ 1 2	6 1 3 0	'		4 7 8 7	'		
P ₂						1 6 ^ 9 7 0	'	X	
P ₃						5 1 ^ 5 9 0	'		
P ₄						1 2 1 ^ 0 0 0	'	X	
P ₅						2 4 3 ^ 4 0 0	'		
						- 0 0 0 0 0 0 0	'	X	
V _{L1}	5	+ 1 2	6 1 3 5	'		0 1 0 9 0	'		
V _{L2}						0 1 1 4 0	'	X	
V _{L3}						0 1 2 1 5	'		
V _{L4}						0 1 3 0 7	'	X	
V _{L5}						0 1 4 3 3	'		
V _{v1}						9 6 5 0 0 0	'	X	
V _{v2}						2 9 8 1 0 0	'		
V _{v3}						1 0 4 8 0 0	'	X	
V _{v4}						4 5 4 6 0	'		
V _{v5}						2 1 6 7 0	'	X	
						- 0 0 0 0 0 0 0	'		
ISOBAR # 1	1	+ 1 2	6 1 4 6	'		2 2 5 0	'	X	
2						1 5 0 0	'		
3						1 0 0 0	'	X	
4						6 0 0	'		
5						4 5 0	'	X	
6						3 0 0	'		
7						2 0 0	'	X	
8						1 4 7	'		
9						1 0 0	'		
10						5 0	"		
						- 0 0 0 0 0 0 0	"	X	

$$0 \leq p \leq 9$$

$$-28 \leq q \leq 47$$

$$0000 \leq Loc \leq 0363$$

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**PUNCH A
STOP CODE AFTER
THE LAST NUMBER!**

29.93200	.00000	10.92988	.01118	.02444	814.1785	1056.6747
	10.00000	17.67878	.13983	.03878	678.4410	880.5089
	20.00000	24.42769	.26850	.05313	589.2465	764.7486
	30.00000	31.17661	.39717	.06747	527.9564	685.2038
	40.00000	37.92552	.52583	.08181	482.5174	626.2312
	50.00000	44.67443	.65450	.09615	447.0966	580.2606
	60.00000	51.42334	.78317	.11049	418.4823	543.1238
	70.00000	58.17226	.91183	.12484	394.7412	512.3116
	80.00000	64.92117	1.04050	.13918	374.6305	486.2111
	90.00000	71.67008	1.16917	.15352	357.3103	463.7322
	100.00000	78.41900	1.29784	.16786	338.2113	438.9448

-123	14.56400	.00000	3.85333	.01077	.00891	451.7714	1151.5883
		10.00000	10.95419	.26459	.02514	360.4799	918.8817
		20.00000	18.05505	.51842	.04137	306.6230	781.5977
		30.00000	25.15592	.77225	.05760	271.3919	691.7918
		40.00000	32.25679	1.02608	.07383	246.0499	627.1937
		50.00000	39.35766	1.27991	.09005	226.6960	577.8596
		60.00000	46.45853	1.53372	.10629	211.2913	538.5924
		70.00000	53.55940	1.78755	.12251	198.6530	506.3766
		80.00000	60.66026	2.04138	.13874	188.0411	479.3264
		90.00000	67.76113	2.29521	.15497	178.9664	456.1944
		100.00000	74.86201	2.54904	.17120	169.0901	431.0192

5.05160	.00000	-4.75425	.01028	-.01144	186.9461	1285.1790
10.00000		2.77716	.69670	.00748	139.4678	958.7846
20.00000		10.30858	1.38313	.02639	115.4211	793.4733
30.00000		17.84000	2.06957	.04530	100.6479	691.9133
40.00000		25.37141	2.75599	.06422	90.3988	621.4553
50.00000		32.90283	3.44241	.08313	82.7541	568.9008
60.00000		40.43424	4.12885	.10204	76.7697	527.7604
70.00000		47.96565	4.81528	.12096	71.9203	494.4227
80.00000		55.49707	5.50170	.13987	67.8872	466.6970
90.00000		63.02849	6.18813	.15878	64.4644	443.1670
100.00000		70.55991	6.87457	.17770	60.7979	417.9607

TABLE 8

SONIC VELOCITY IN TWO PHASE FREON-22 SYSTEM

P (PSIA)	Q (% Vapor)	H (BTU/Lb)	V (Cu Ft/Lb)	S (BTU/Lb-deg F)	G max (Lb/Sq Ft-Sec)	V max (Ft/Sec)
224.60000	.00000	42.26272	.01415	.08499	3643.469	863.0804
	10.00000	49.34725	.03641	.09757	3357.857	795.4234
	20.00000	56.43179	.05869	.11014	3100.163	734.3798
	30.00000	63.51634	.08096	.12272	2893.941	685.5291
	40.00000	70.60087	.10323	.13530	2724.062	645.2873
	50.00000	77.68541	.12551	.14787	2580.968	611.3906
	60.00000	84.76995	.14778	.16045	2458.2875	582.3296
	70.00000	91.85449	.17005	.17302	2351.5877	557.0541
	80.00000	98.93903	.19232	.18560	2257.6750	534.8076
	90.00000	106.02357	.21460	.19817	2174.1840	515.0299
125	100.00000	113.10812	.23688	.21075	2074.1702	491.3382
	.00000	16.59846	.01228	.03656	1370.9253	1238.7776
	10.00000	25.67046	.10140	.05540	1146.5451	1036.0261
	20.00000	34.74248	.19054	.07423	997.9241	901.7311
	30.00000	43.81449	.27967	.09307	895.2792	808.9805
	40.00000	52.88650	.36880	.11191	818.9353	739.9956
	50.00000	61.95851	.45793	.13075	759.2910	686.1006
	60.00000	71.03053	.54707	.14958	711.0293	642.4910
	70.00000	80.10253	.63619	.16842	670.9367	606.2631
	80.00000	89.17455	.72533	.18726	636.9415	575.5448
	90.00000	98.24656	.81446	.20609	607.6399	549.0677
	100.00000	107.31857	.90360	.22493	575.3513	519.8914

29.94000	.00000	7.32710	.01174	.01672	795.9578	1395.1769
10.00000	16.95658	.18585	.03824	631.8858		1107.5870
20.00000	26.58607	.35996	.05976	536.3767		940.1760
30.00000	36.21556	.53406	.08128	474.1960		831.1839
40.00000	45.84506	.70817	.10280	429.5959		753.0076
50.00000	55.47454	.88228	.12432	395.5988		693.4165
60.00000	65.10402	1.05638	.14584	368.5755		646.0493
70.00000	74.73351	1.23049	.16736	346.4273		607.2274
80.00000	84.36300	1.40460	.18887	327.8452		574.6562
90.00000	93.99249	1.57871	.21039	311.9647		546.8203
100.00000	103.62198	1.75282	.23191	294.7557		516.6560
<hr/>						
14.54000	.00000	-51392	.01131	-.00116	443.5573	1527.2388
10.00000	9.56145	.35449	.02298	334.2642		1150.9250
20.00000	19.63683	.69768	.04711	277.6971		956.1555
30.00000	29.71220	1.04086	.07124	242.6418		835.4546
40.00000	39.78758	1.38404	.09538	218.2058		751.3106
50.00000	49.86296	1.72723	.11951	199.9189		688.3526
60.00000	59.93834	2.07041	.14364	185.5742		638.9615
70.00000	70.01372	2.41359	.16777	173.9315		598.8741
80.00000	80.08910	2.75678	.19191	164.2369		565.4940
90.00000	90.16447	3.09996	.21604	156.0014		537.1377
100.00000	100.23986	3.44315	.24017	147.1697		506.7289

१००•१००	३००•३००
२००•२००	४००•४००
३००•३००	५००•५००
४००•४००	६००•६००
५००•५००	७००•७००
६००•६००	८००•८००
७००•७००	९००•९००
८००•८००	१०००•१०००
९००•९००	११००•११००
१०००•१०००	१२००•१२००

३४२-३५६
३४२-३५०
३५१-३५७
३५१-३५८
३५१-३५९
३५१-३६०
३५१-३६१
३५१-३६२
३५१-३६३
३५१-३६४

5.10000	.00000	-9.74102	.01090	-.02419	185.0091	1666.1541
10.00000	.82748	.92023	.00351	129.0938		1175.2972
20.00000	11.39600	1.82955	.03122	104.7902		954.0321
30.00000	21.96452	2.73888	.05892	90.4884		823.8253
40.00000	32.53304	3.64822	.08662	80.7953		735.5777
50.00000	43.10154	4.55754	.11432	73.6709		670.7154
60.00000	53.67005	5.46687	.14202	68.1501		620.4528
70.00000	64.23857	6.37620	.16972	63.7094		580.0240
80.00000	74.80709	7.28553	.19743	60.0371		546.5910
90.00000	85.37560	8.19486	.22513	56.9345		518.3440
100.00000	95.94412	9.10420	.25283	53.6415		488.3632