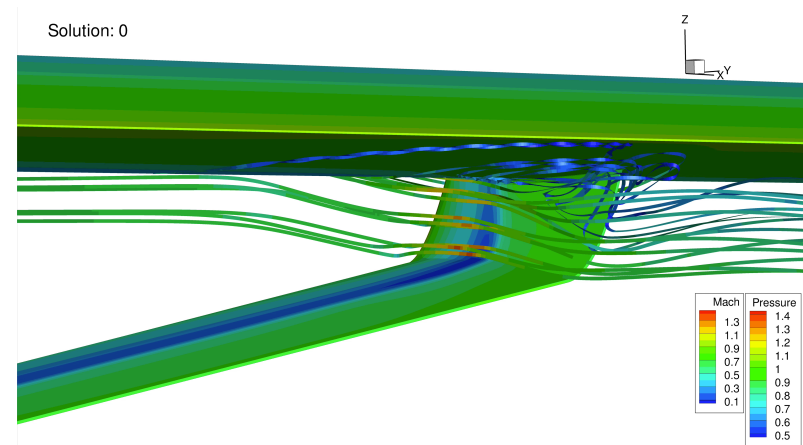




NASA Ames Research Center Contributions to the PADRI workshop

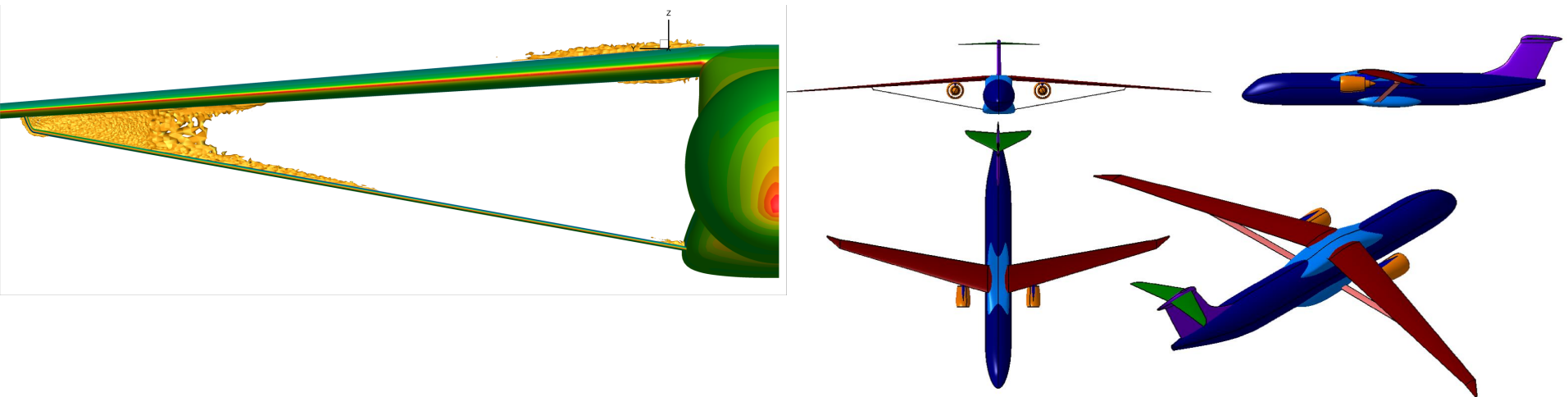
Gaetan Kenway
Jeffery Housman
Cetin Kiris

Computational Aerosciences Branch
NASA Ames Research Center



November 29, 2017

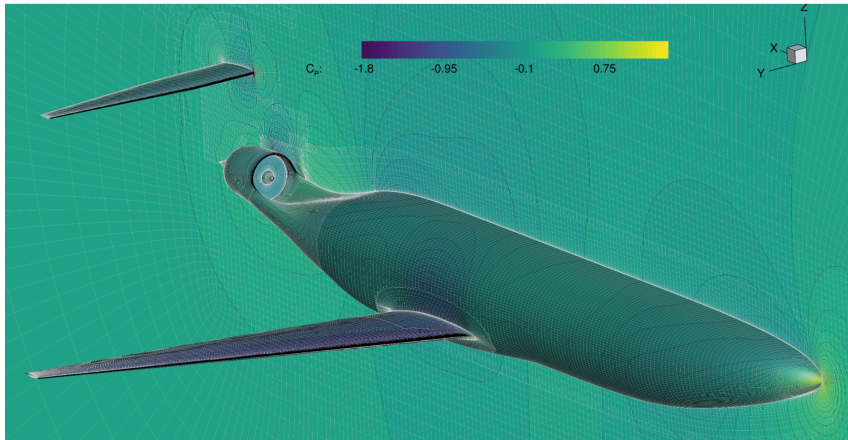
- PADRI: A common platform for validation of aircraft drag reduction technologies
- Generic strut-braced wing configuration
- Slightly swept wing for low cruise Mach number (0.72)
- Simplified geometry without engines, empennage or flap-track fairings
- Significant wave-drag and flow separation at strut-wing intersection
- Focus of this workshop is to redesign the junction



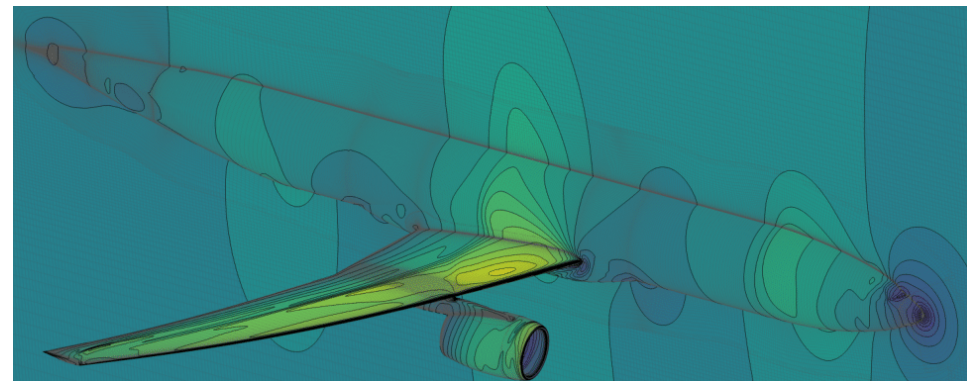
<h2>Python user script</h2> <p>Setup up the problem: objective function, constraints, design variables, optimizer and solver options</p>			
Optimizer interface <i>pyOptSparse</i> Common interface to various optimization software		Aerostructural solver <i>AeroStruct</i> Coupled solution methods and coupled derivative evaluation	
Geometry modeler <i>DVGeometry/GeoMACH</i> Defines and manipulates geometry, evaluates derivatives		Flow solver <i>ADflow</i> Governing and adjoint equations	Structural solver <i>TACS</i> Governing and adjoint equations
SNOPT	Other optimizers		

- Underlying solvers are parallelized and compiled
- All communication done through memory
- Easy-to-use Python scripting interface
- Only using aerodynamic design capacity for PADRI

- Automatic-Differentiation Flow Solver
- Second order finite volume RANS
- Standard SA turbulence model
- Point-matched multiblock and overset grids
- Multiple solvers: Runge Kutta (RK), DDADI, approximate Newton Krylov (ANK) and Newton Krylov (NK) algorithms
- DADI, ANK and NK used for optimization
- Extremely fast convergence for small design changes

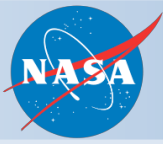


MIT D8 Double Bubble

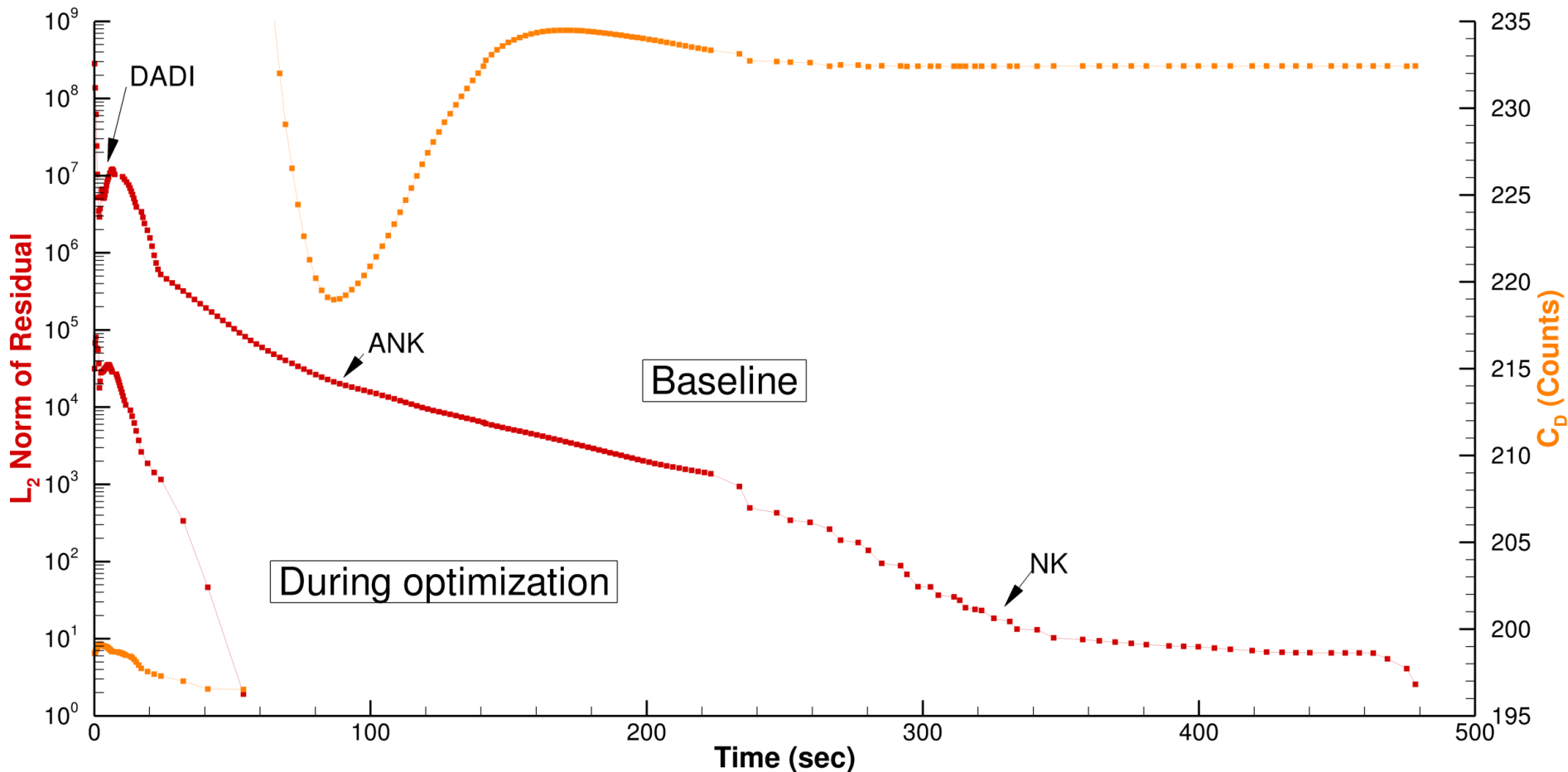


Common Research Model (DPW6)

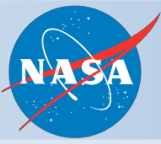
ADFlow Solver Convergence



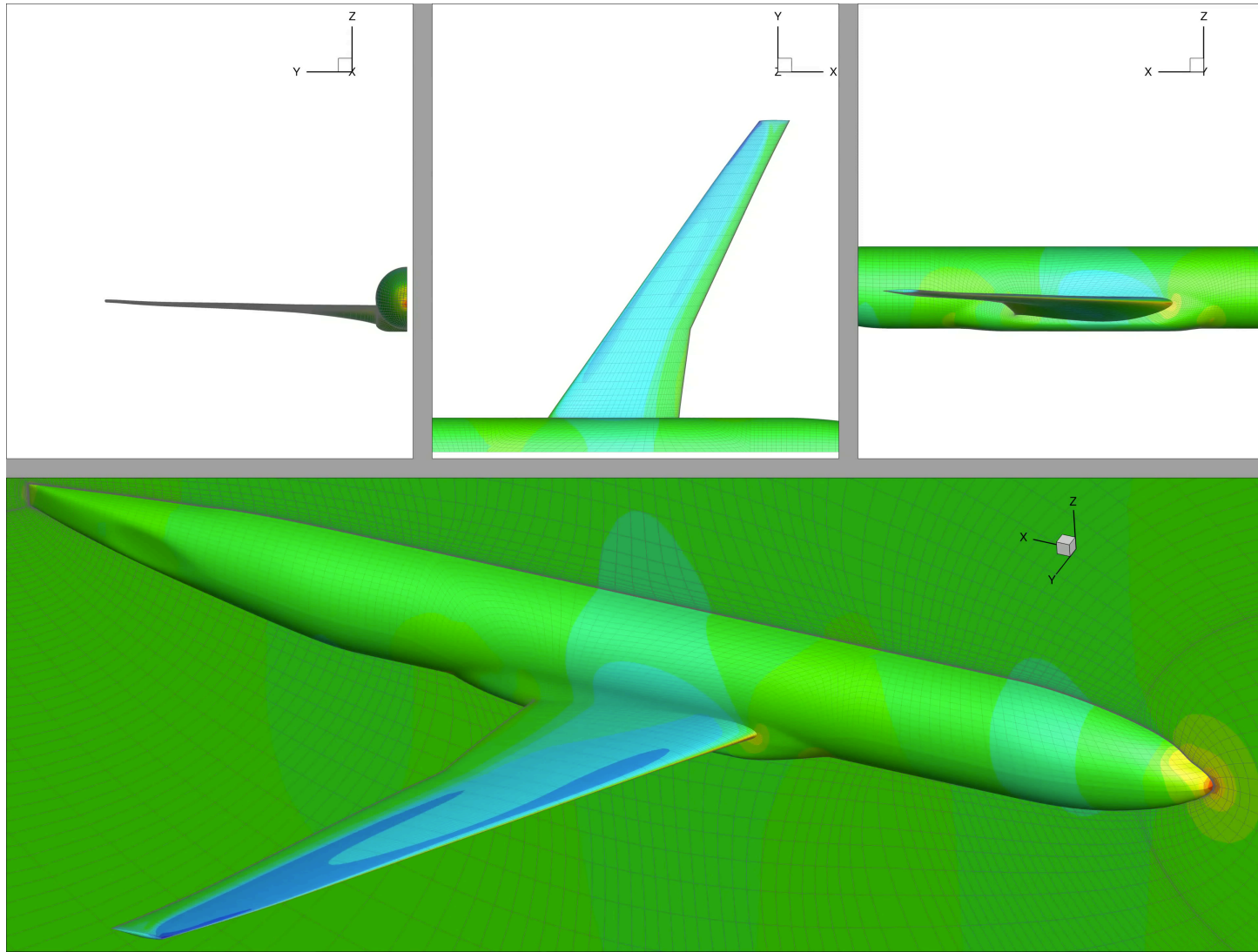
- Combination of three algorithms: Diagonalized Alternating Direction Implicit (DADI), Approximate Newton-Krylov (ANK) and Newton Krylov (NK)
- Newton-Krylov fully couples flow and turbulence variables



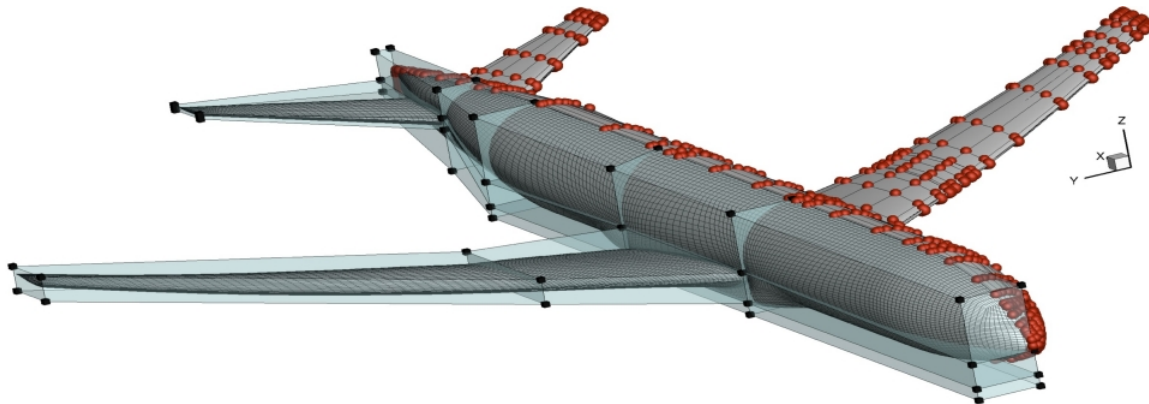
Mesh Deformation



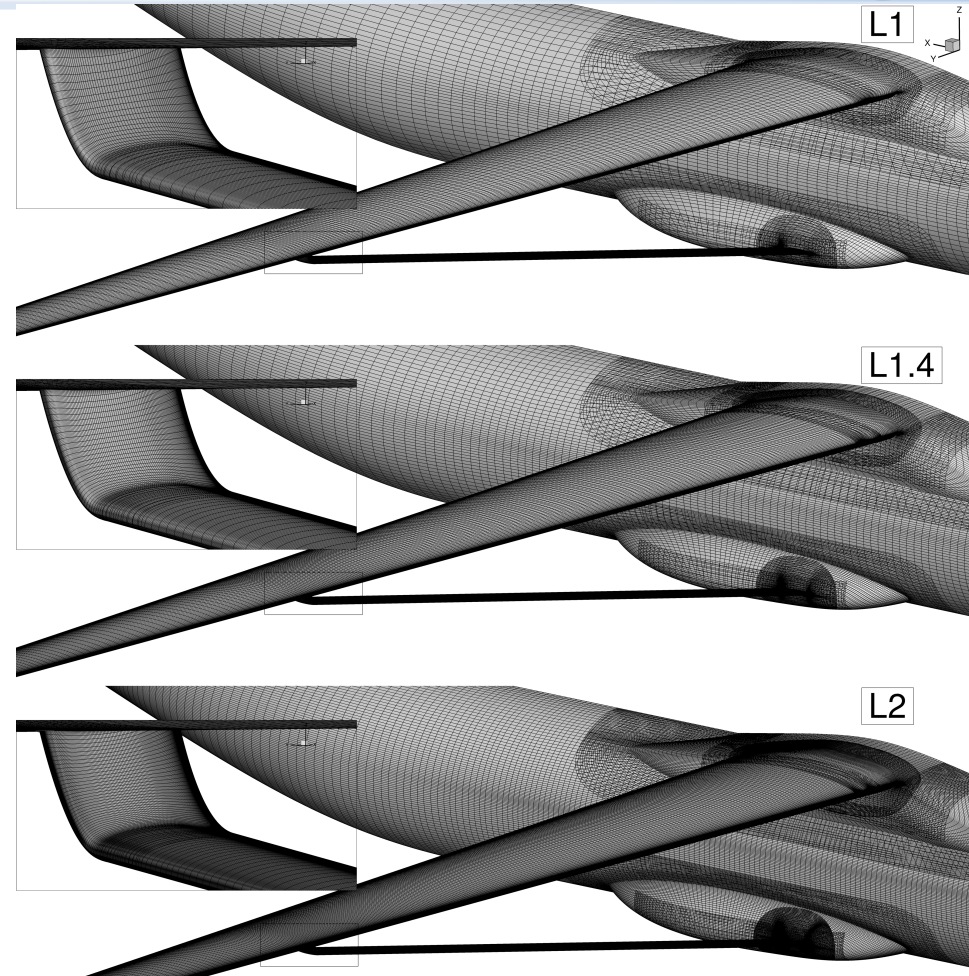
- Inverse-distance weighting method
- Parallel, fast and highly robust for large deformations



- Free-form deformation (FFD) volume approach
- Parametrize the change in geometry
- Embed discrete geometry into trivariate B-spline volumes
- Point-inversion algorithm to find u-v-w coordinates
- Control point motion smoothly controls the underlying geometry
- Sub-FFD approach for localized control

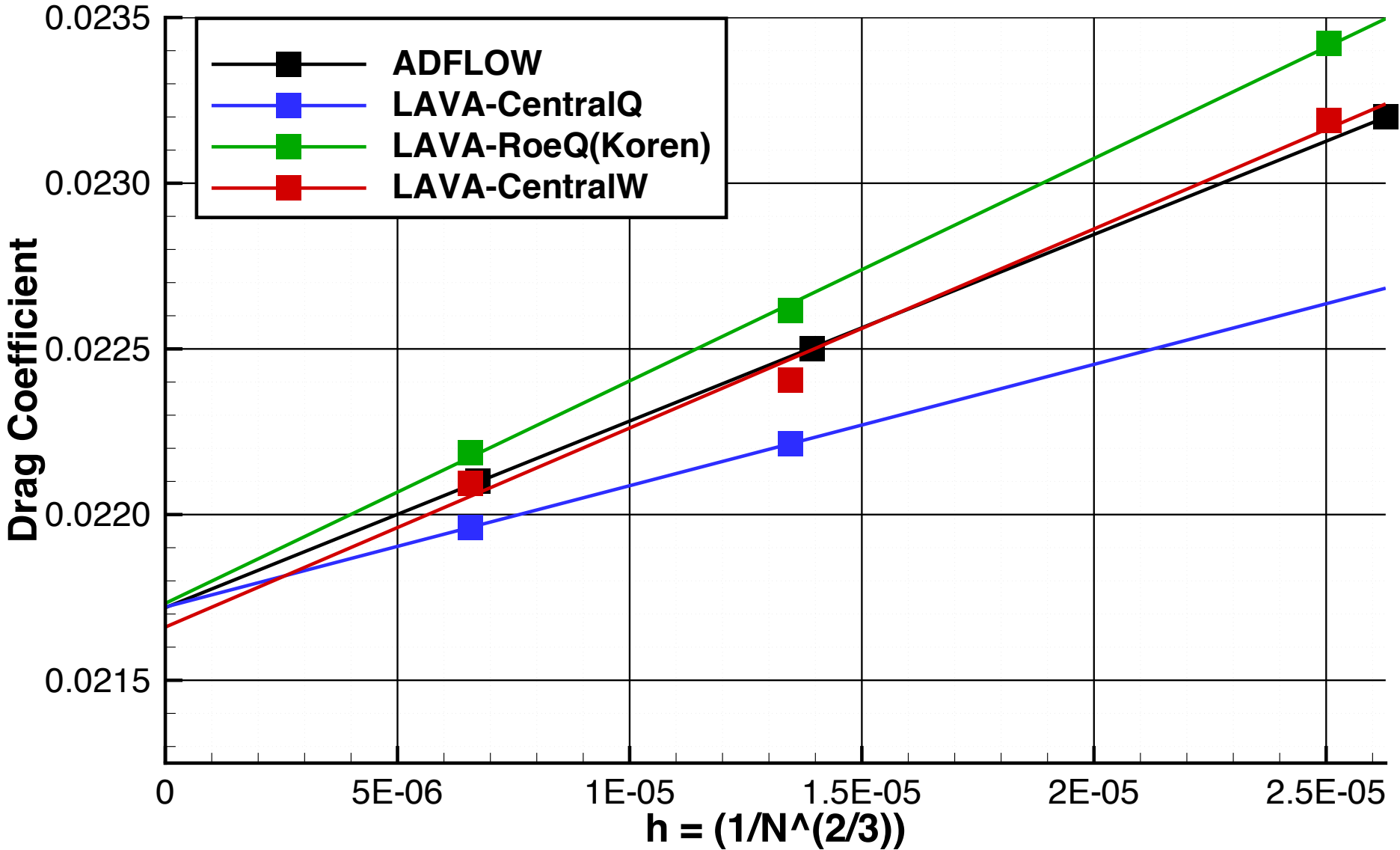
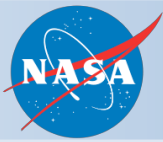


- Surface patches generated with Pointwise
- Chimera Grid Tools (CGT) for volumetric extrusion
- Hyperbolic mesh extrusion
- Consistent refinement between levels

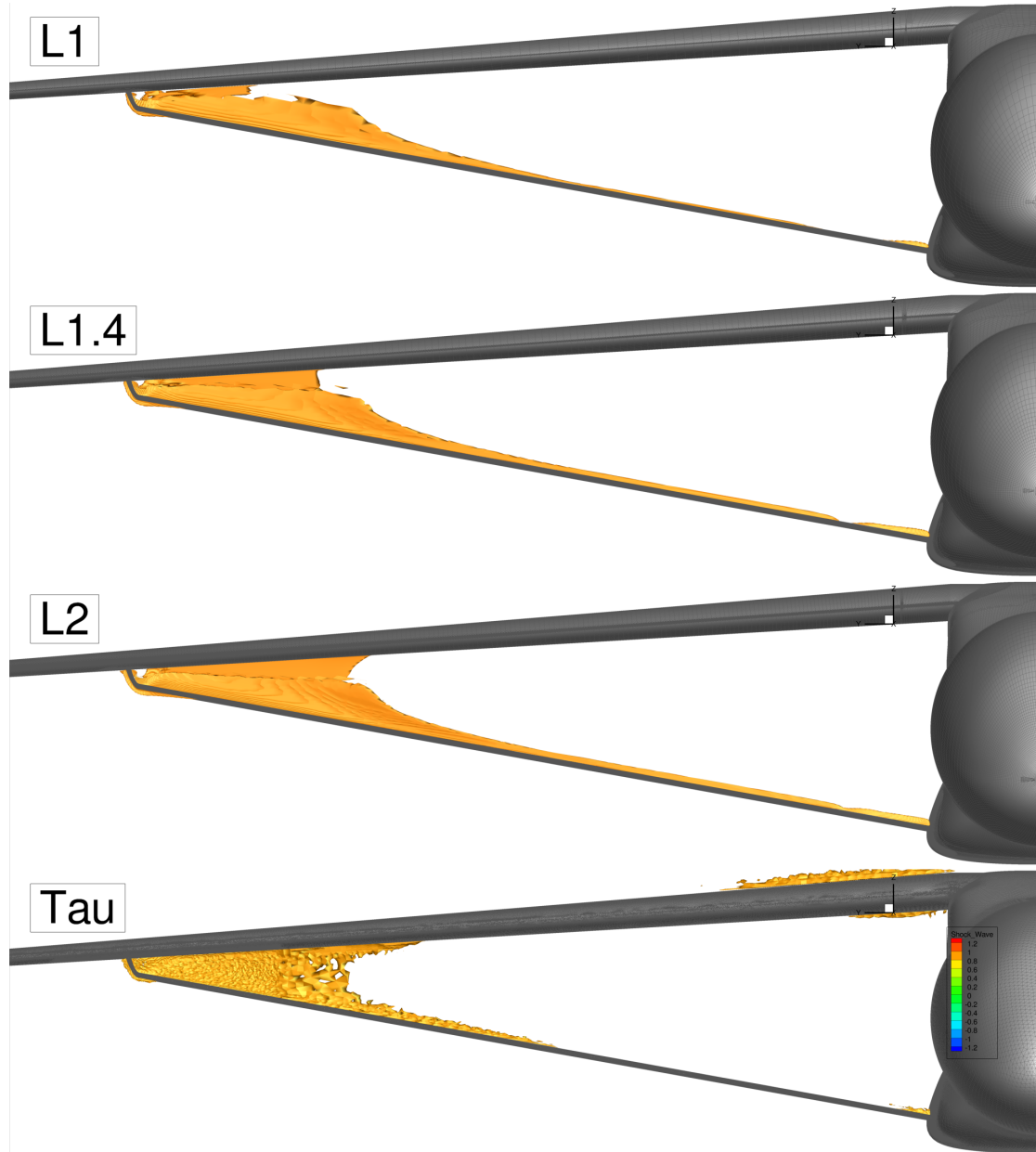
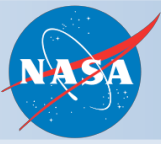


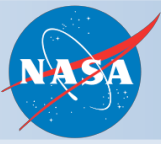
Mesh	# Wing Chordwise	# Wing Spanwise	# Truss Chordwise	# Truss Spanwise	Total Cells	Drag (counts)
L1	64	202	96	110	7.4 M	232.42
L1.4	88	282	134	154	19.2 M	224.61
L2	126	404	192	220	57.3 M	220.87

Baseline Configuration Grid Convergence



Baseline Solutions (Shock Sensor)





- Single point drag minimization ($CL=0.417$)
- Design Variables: FFD Shape position + angle of attack
- Flight condition: $M=0.72$, altitude=30,000 ft, $\alpha=1.0$

- **Case 1**

- Nominal design problem

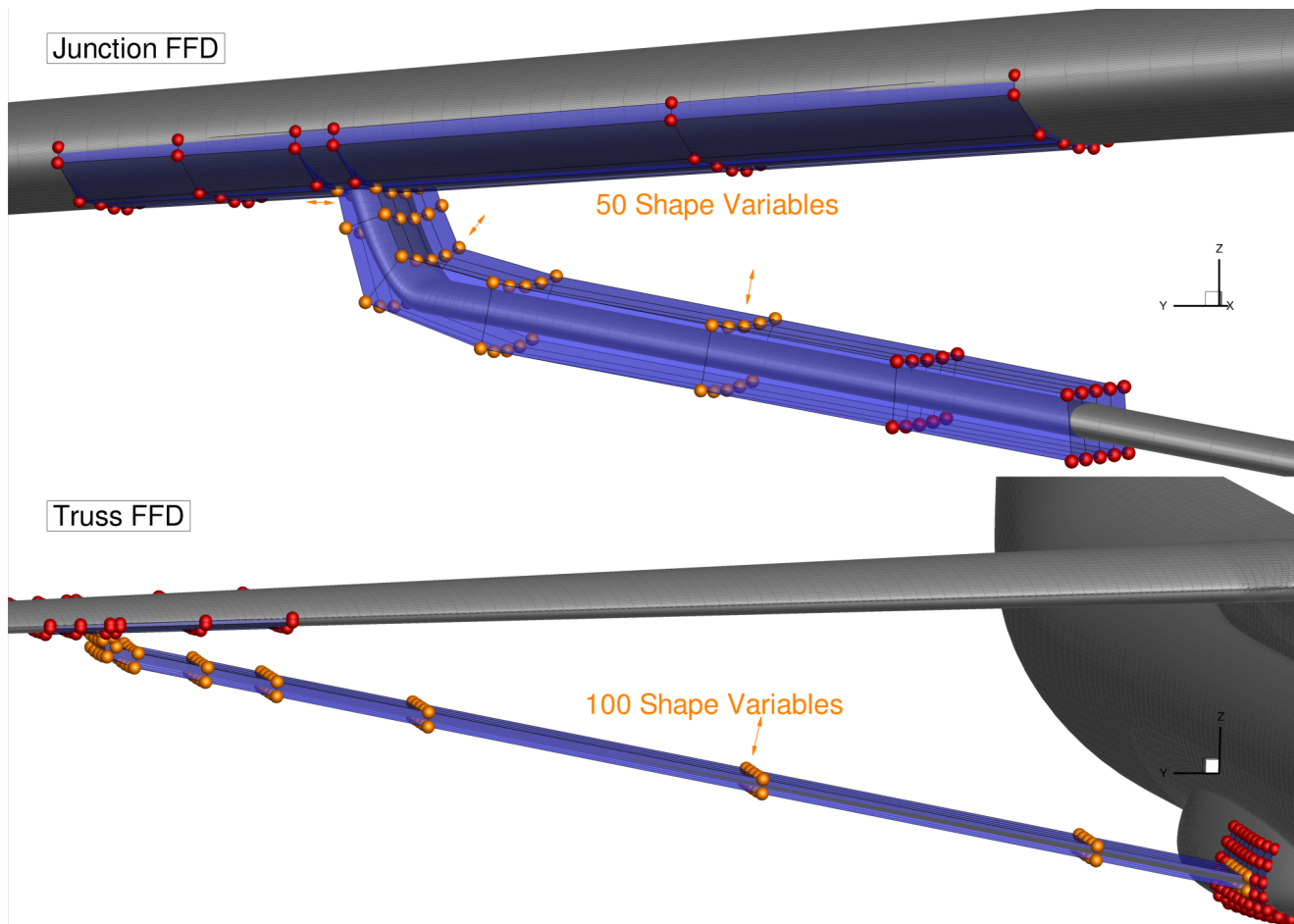
- **Case 2**

- Nominal design problem + fixed trailing edge

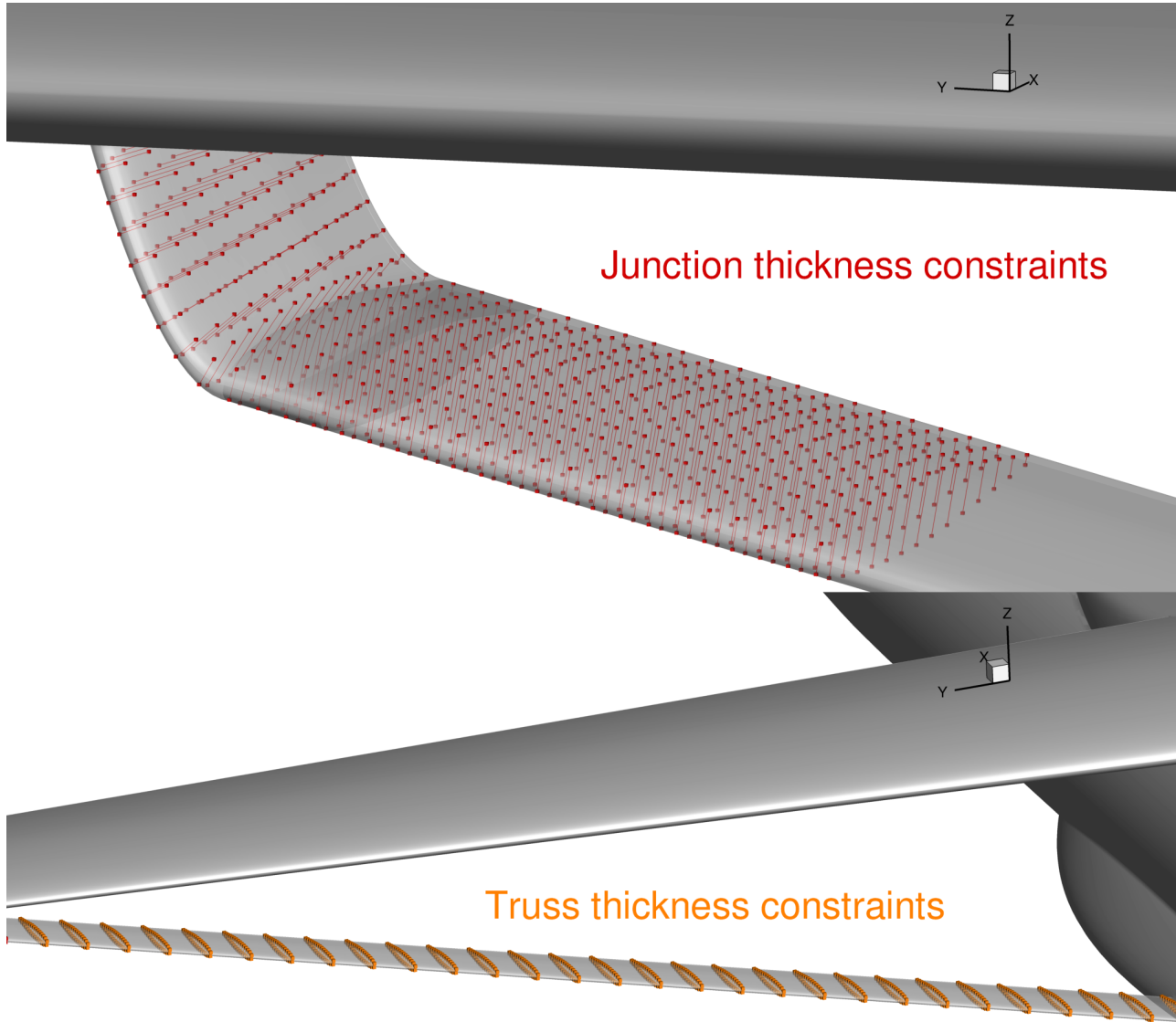
- **Case 3**

- Full truss redesign

- Only truss is modified
- Follows workshop guidelines for design region (Case 1 and 2)
- Orange control point spheres are modified



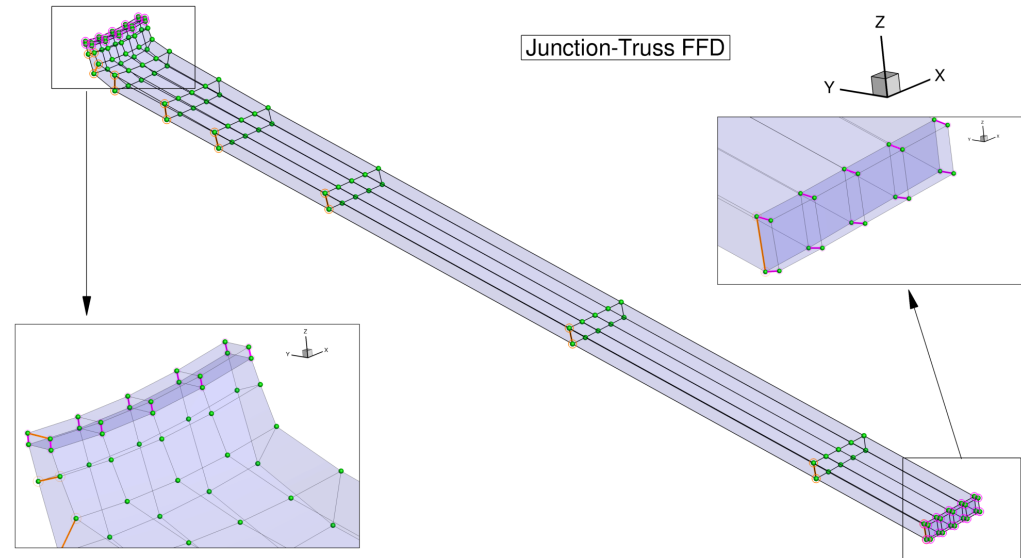
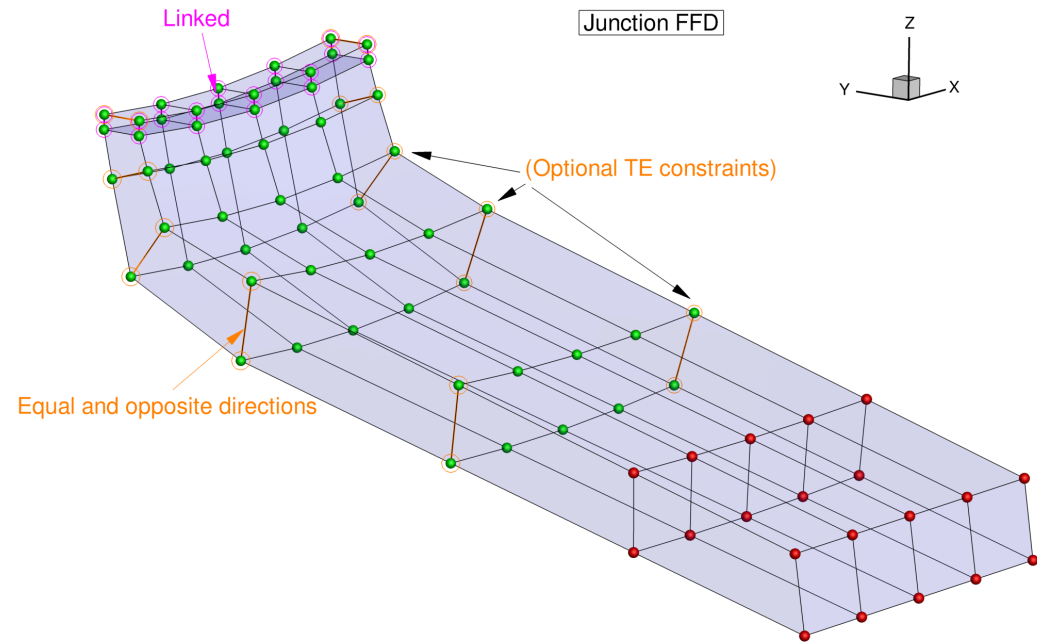
- Explicit “toothpick” thickness constraints



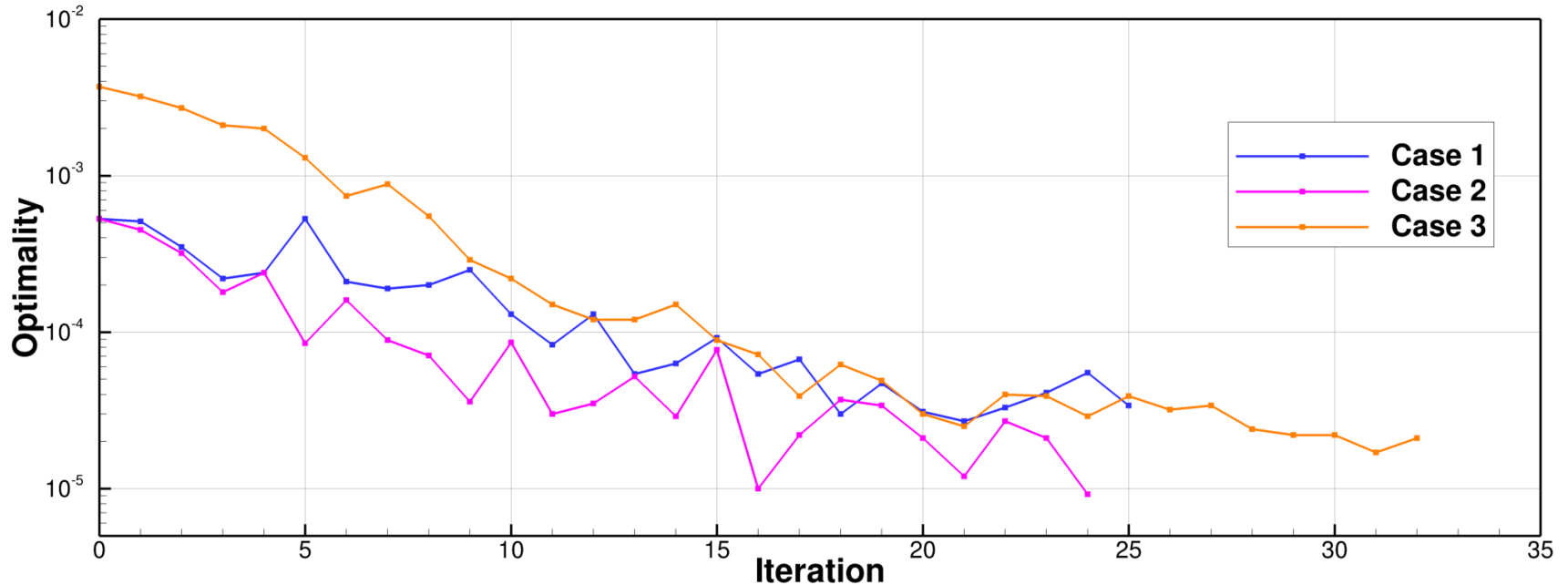
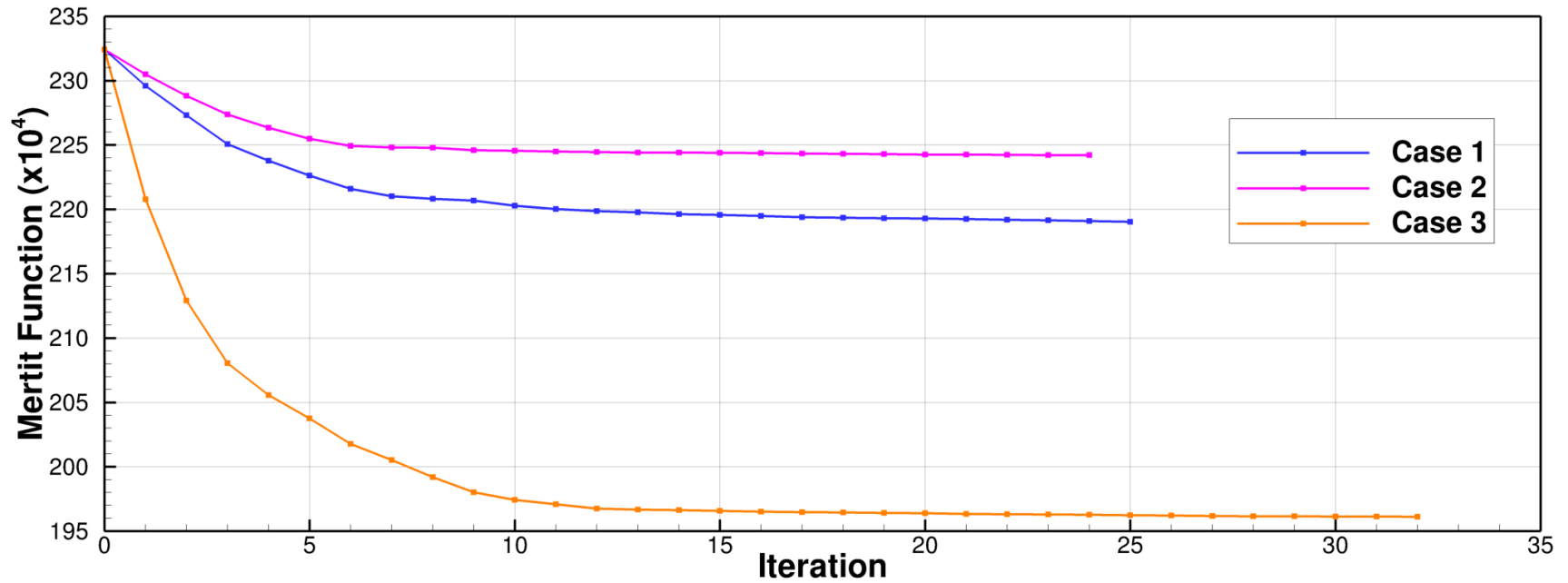
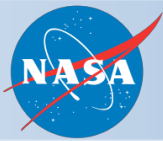
Optimization Constraints



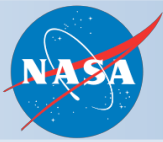
- Linear constraints enforce fixed leading and (optionally) trailing edge
- These constraints are enforced exactly by the optimizer



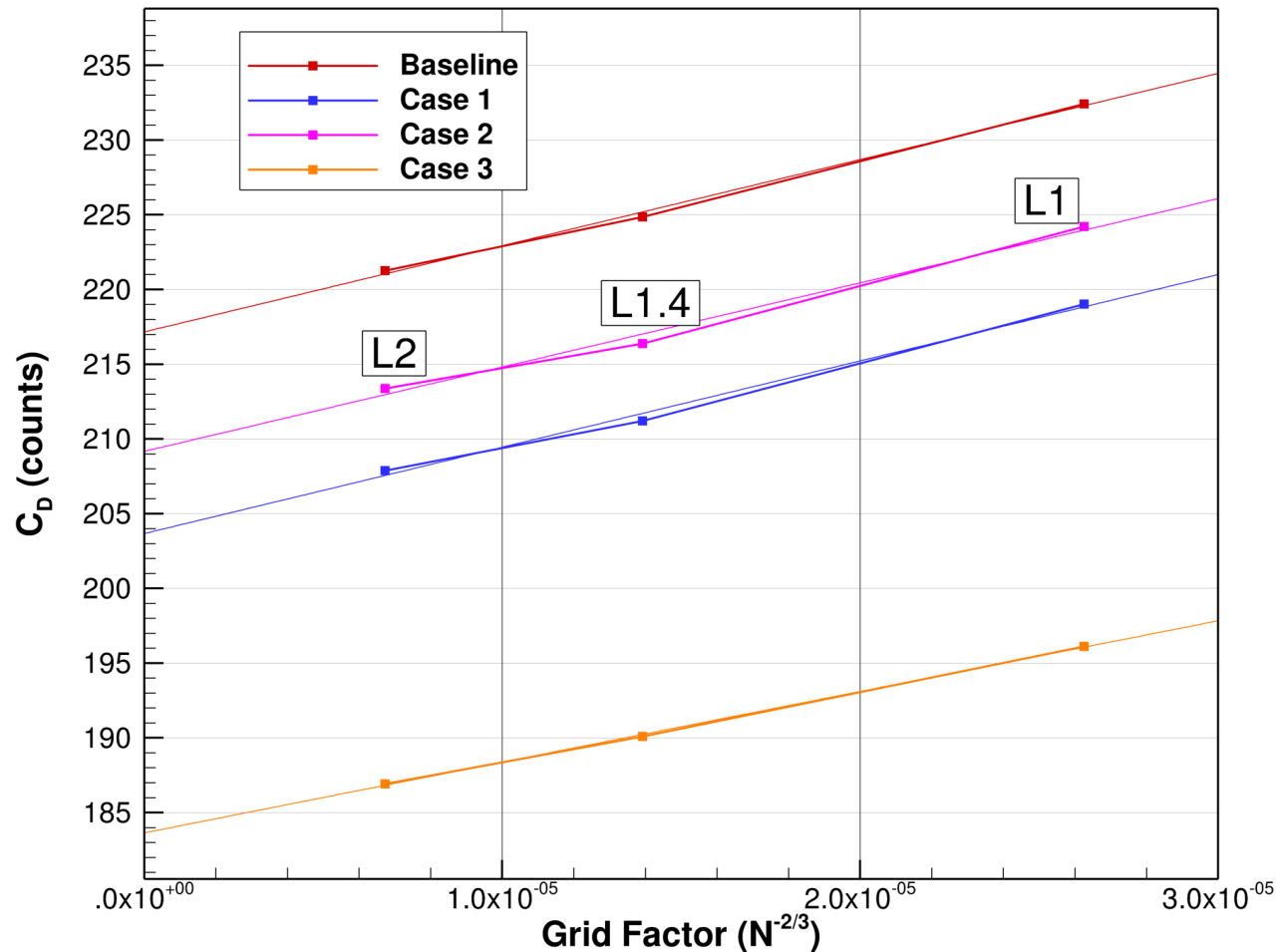
Optimization Convergence History



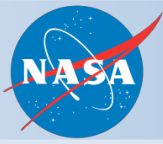
Grid Convergence Study



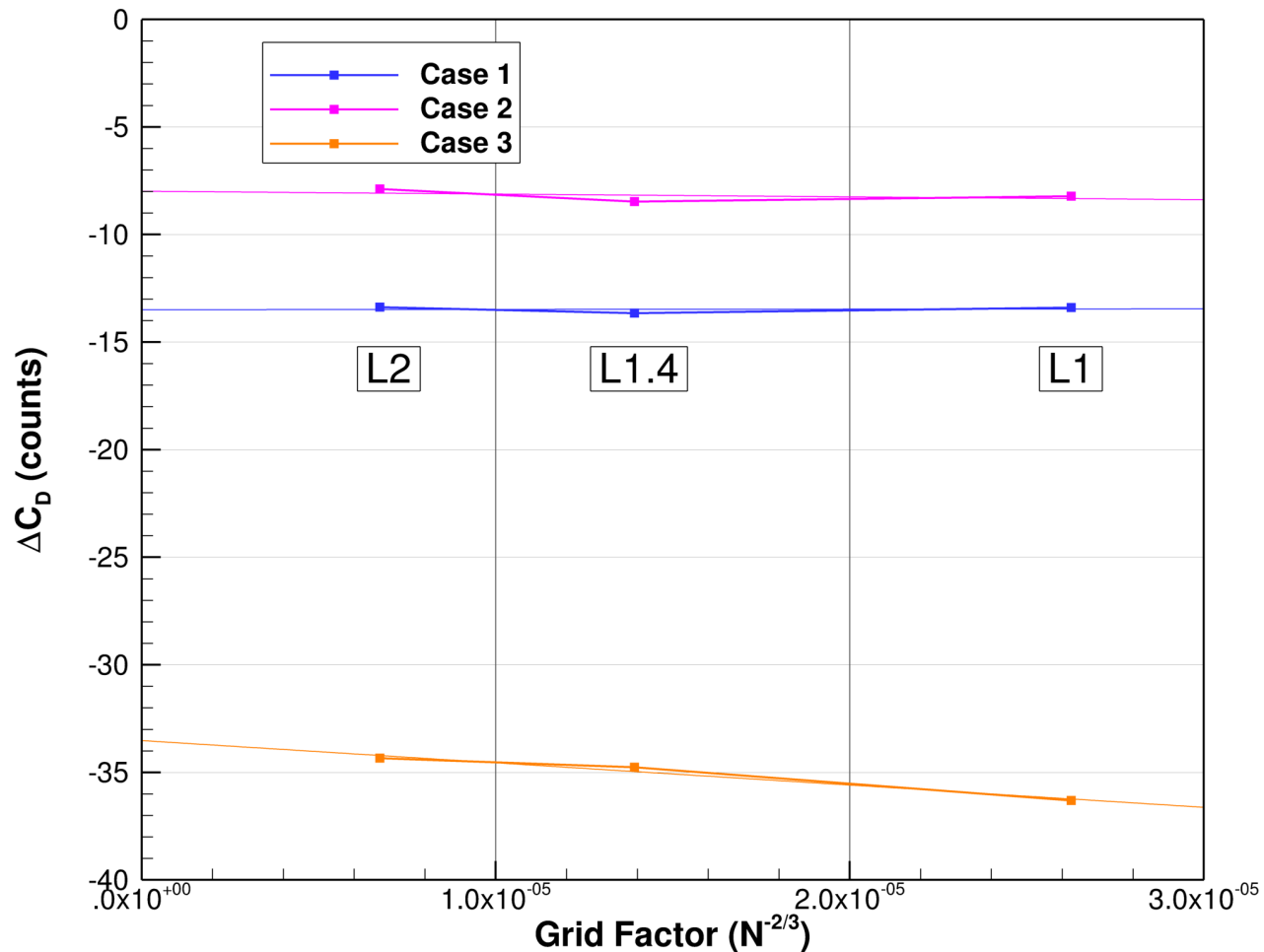
- Optimized L1 shape analyzed using finer meshes



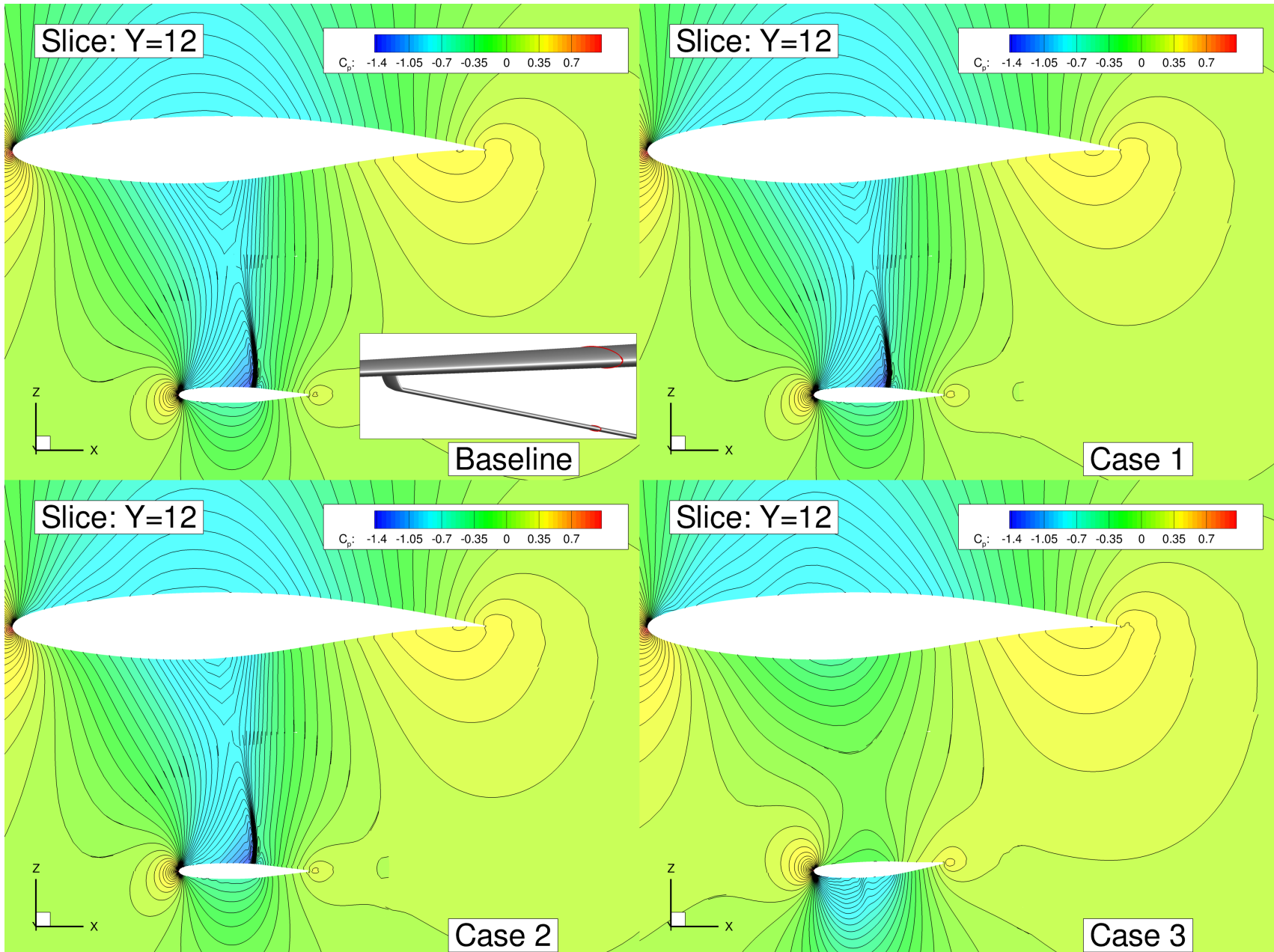
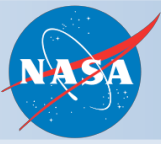
Grid Convergence Study



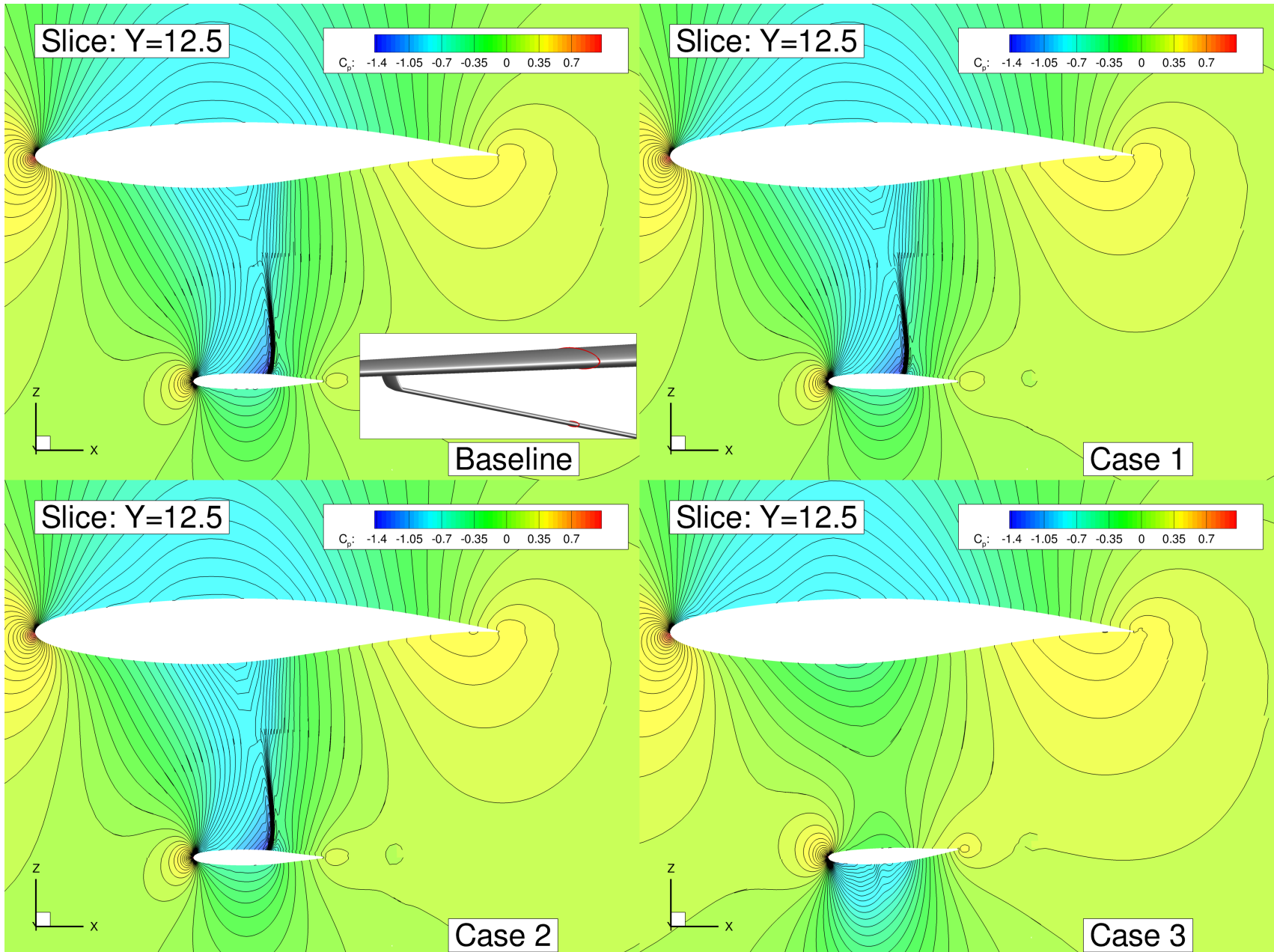
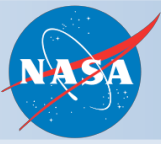
- Nearly constant drag deltas
- L1 mesh capturing the critical flow features



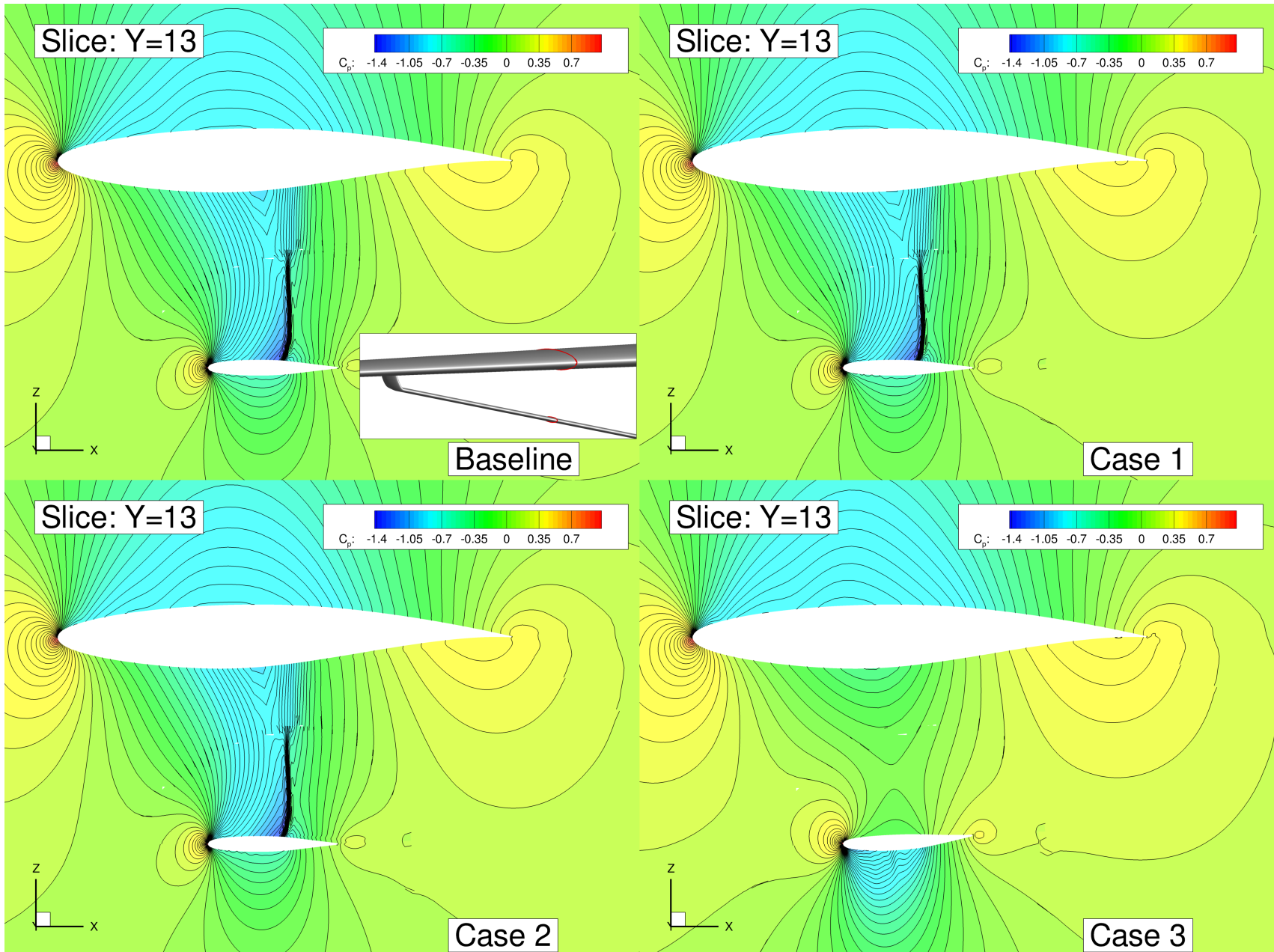
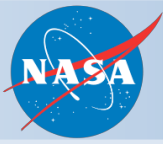
2D Slices of Junction Region



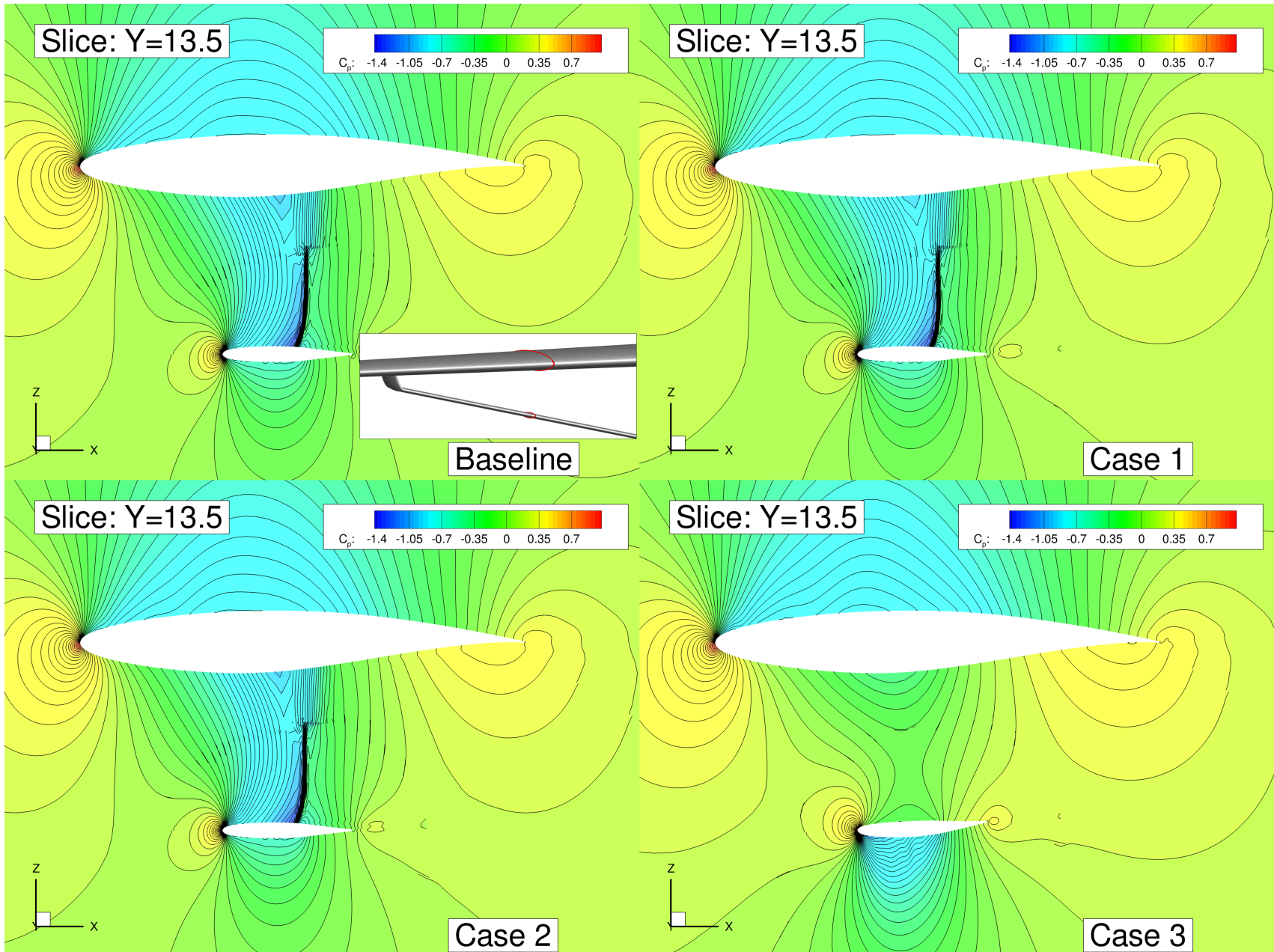
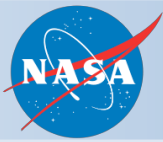
2D Slices of Junction Region



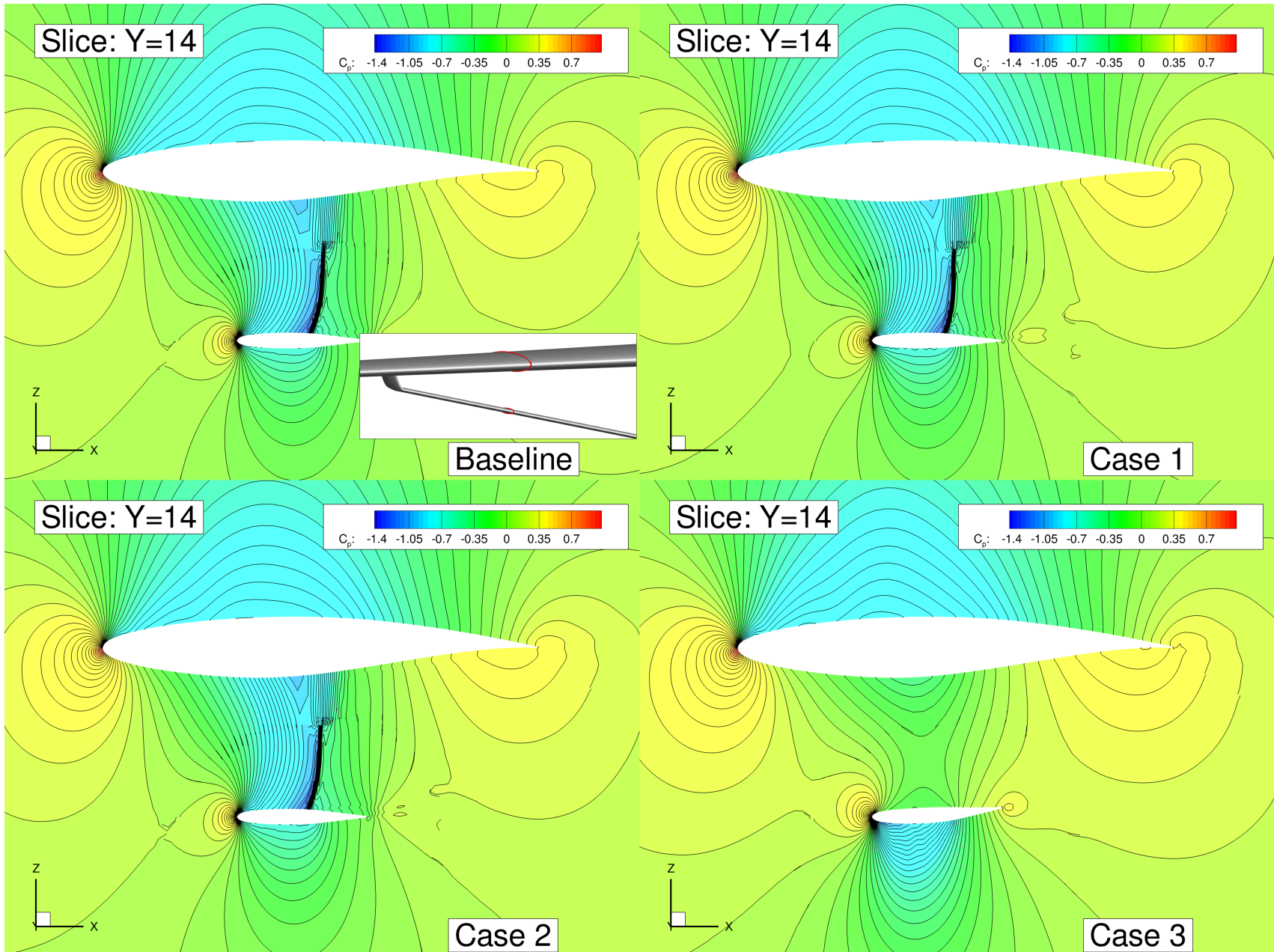
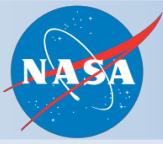
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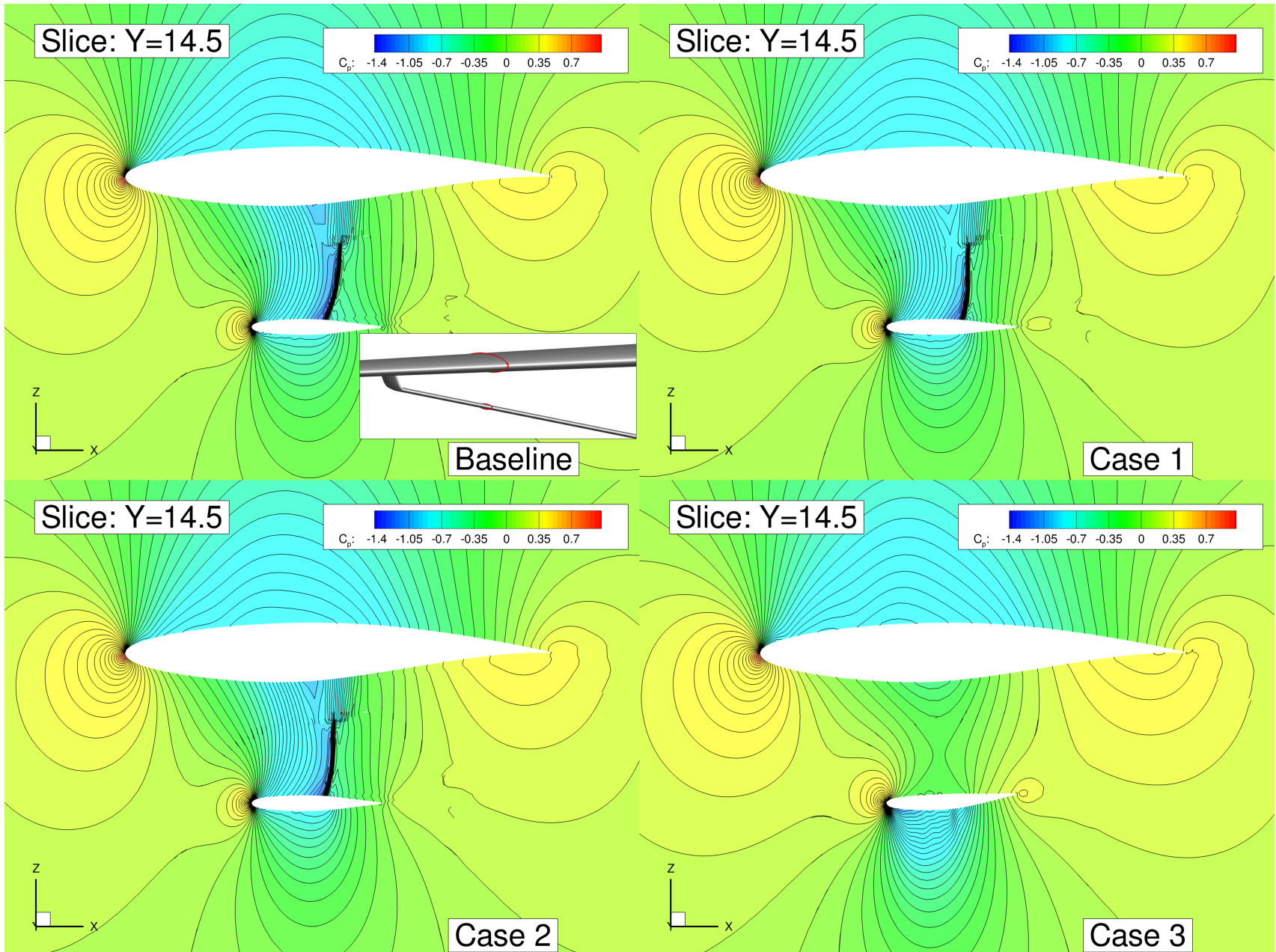
2D Slices of Junction Region



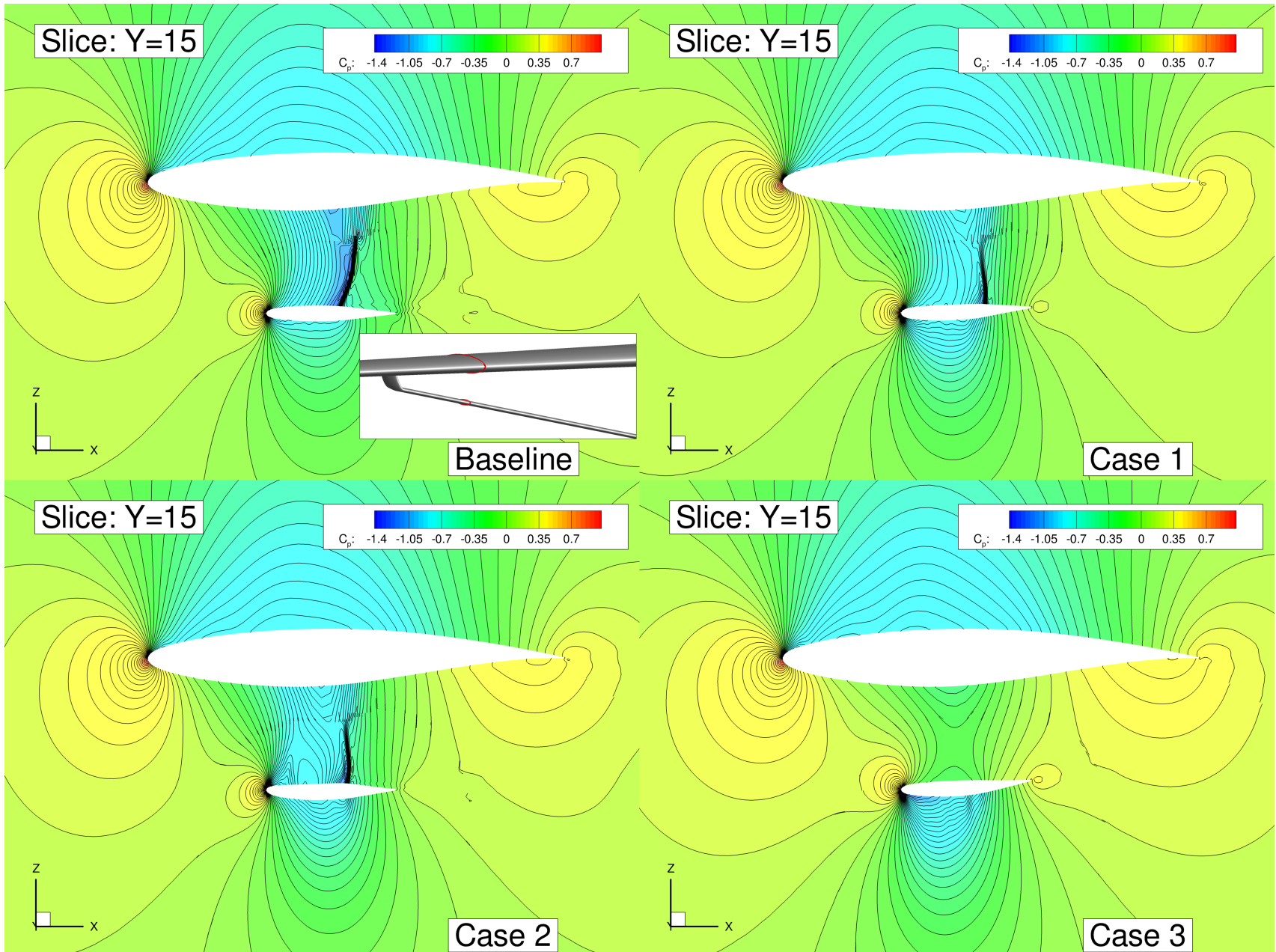
2D Slices of Junction Region



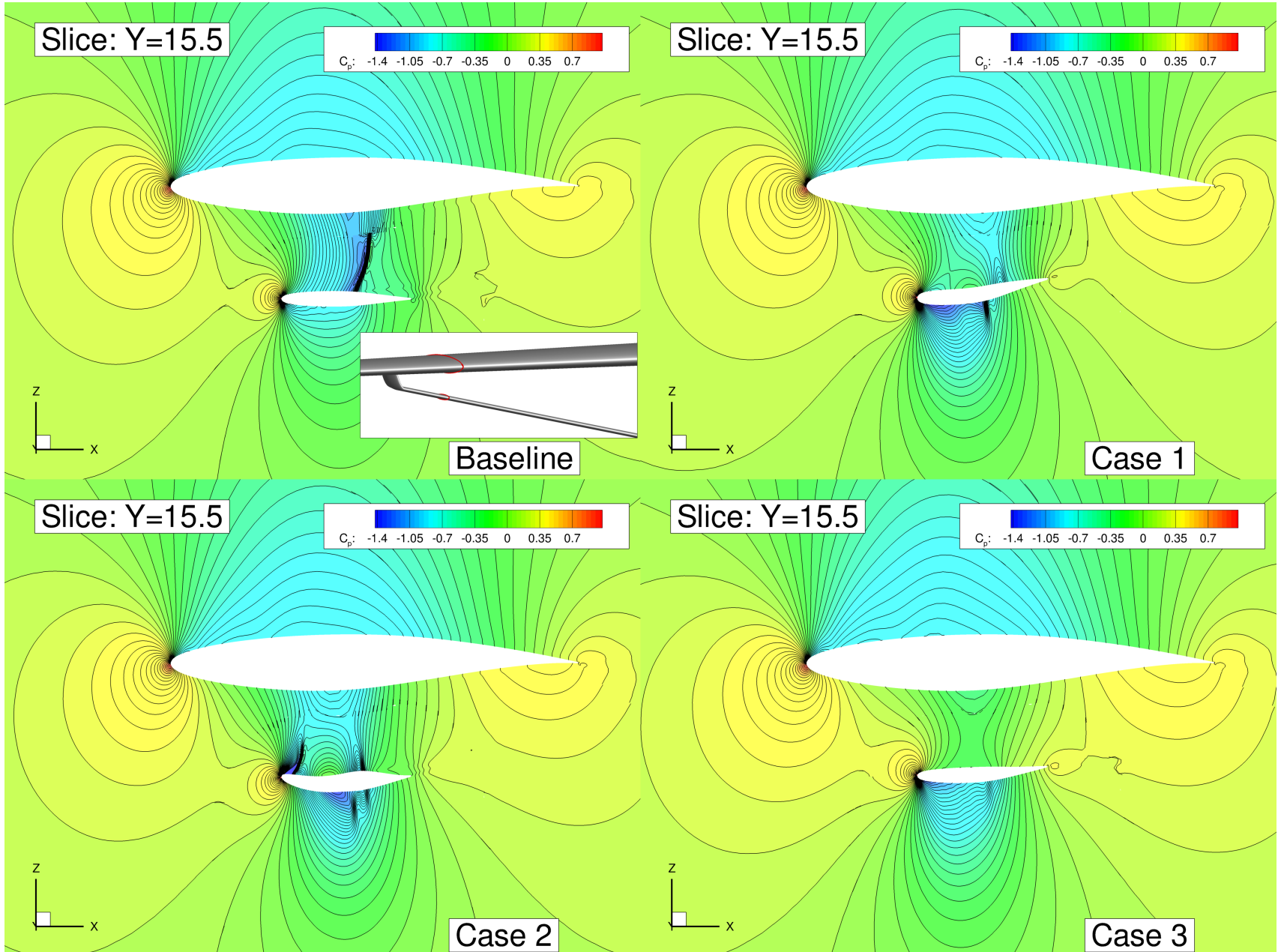
2D Slices of Junction Region



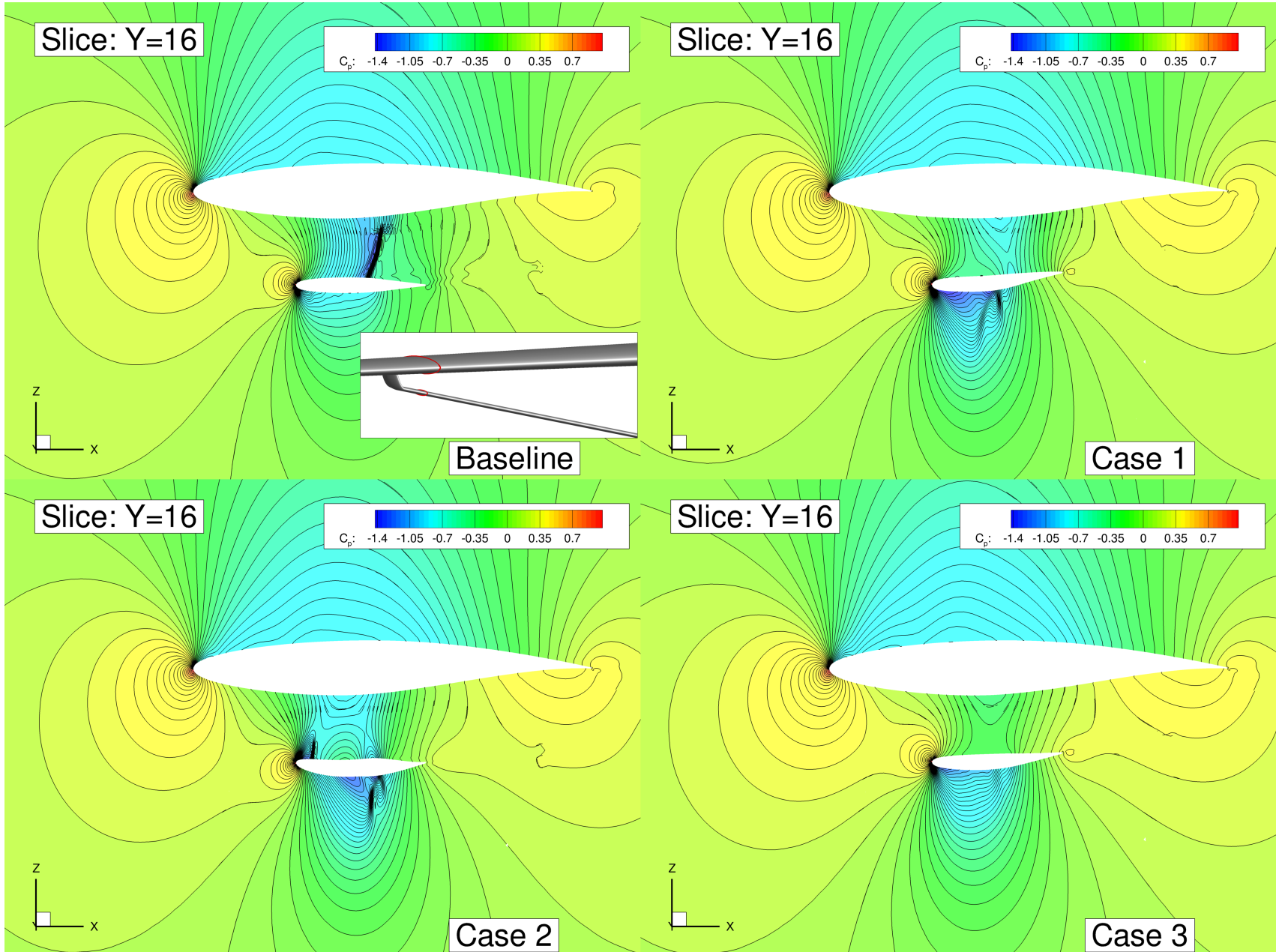
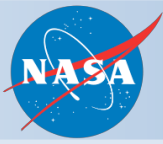
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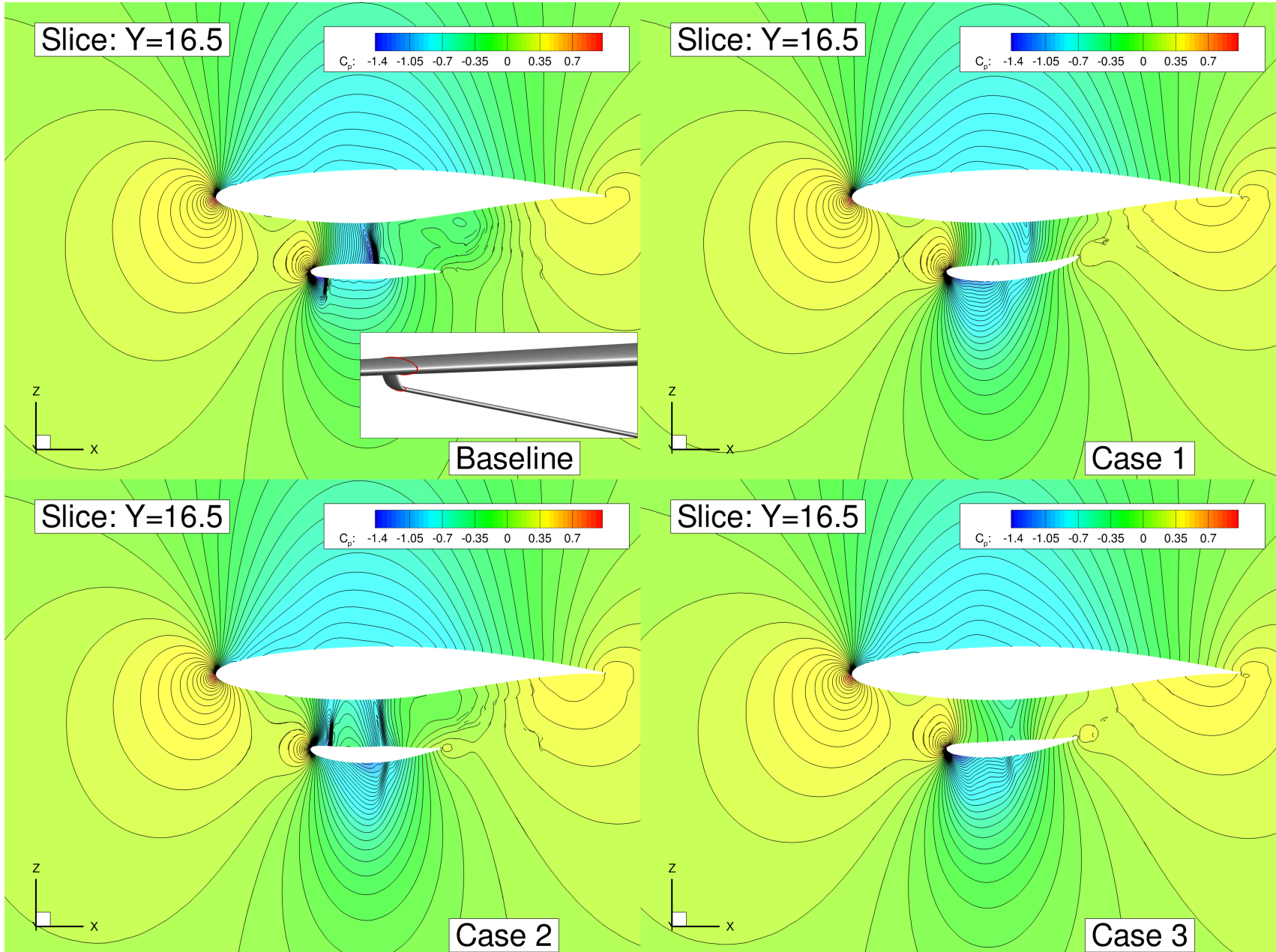
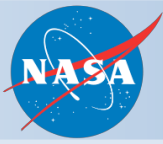
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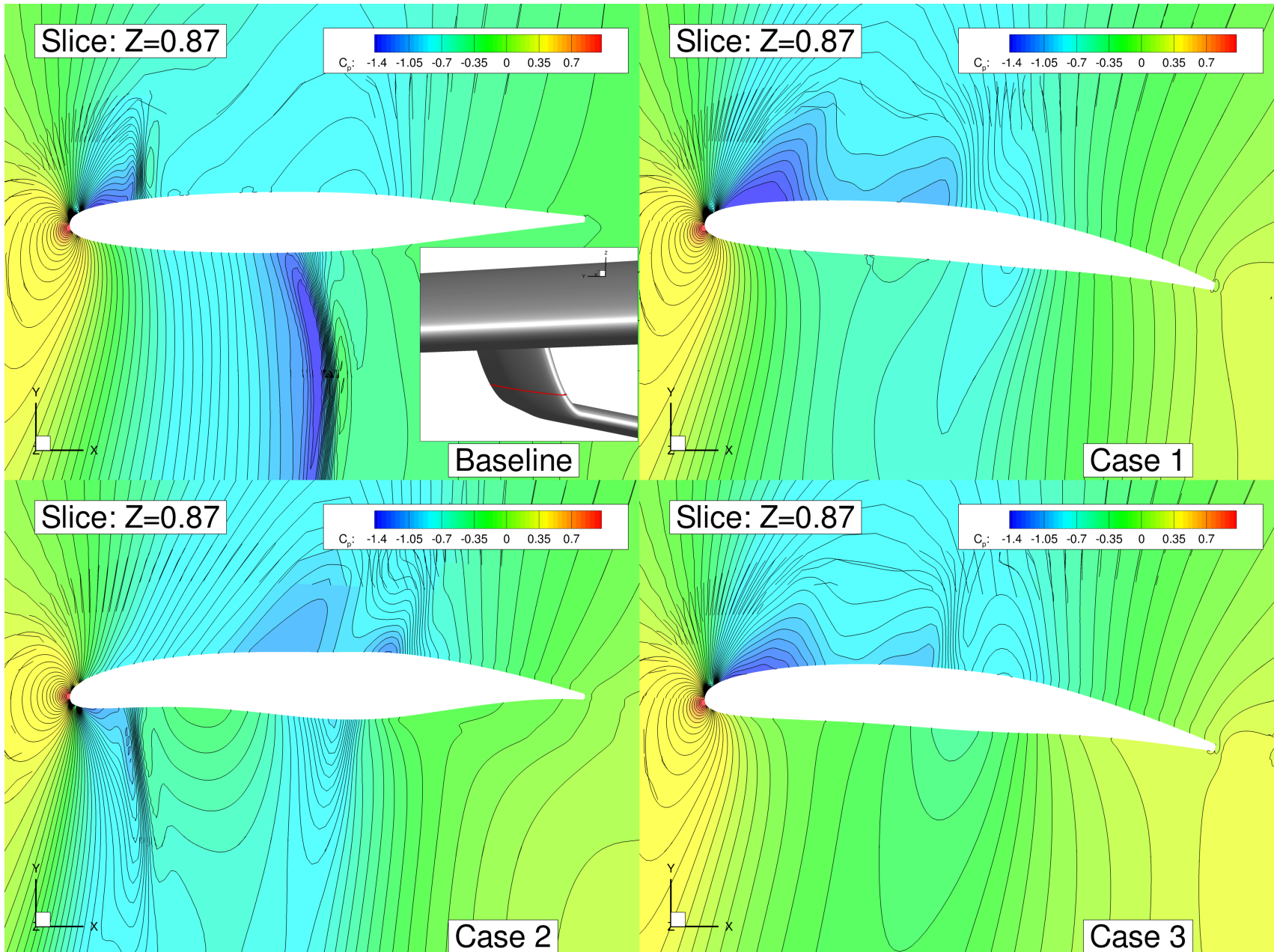
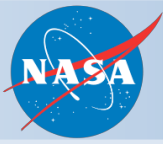
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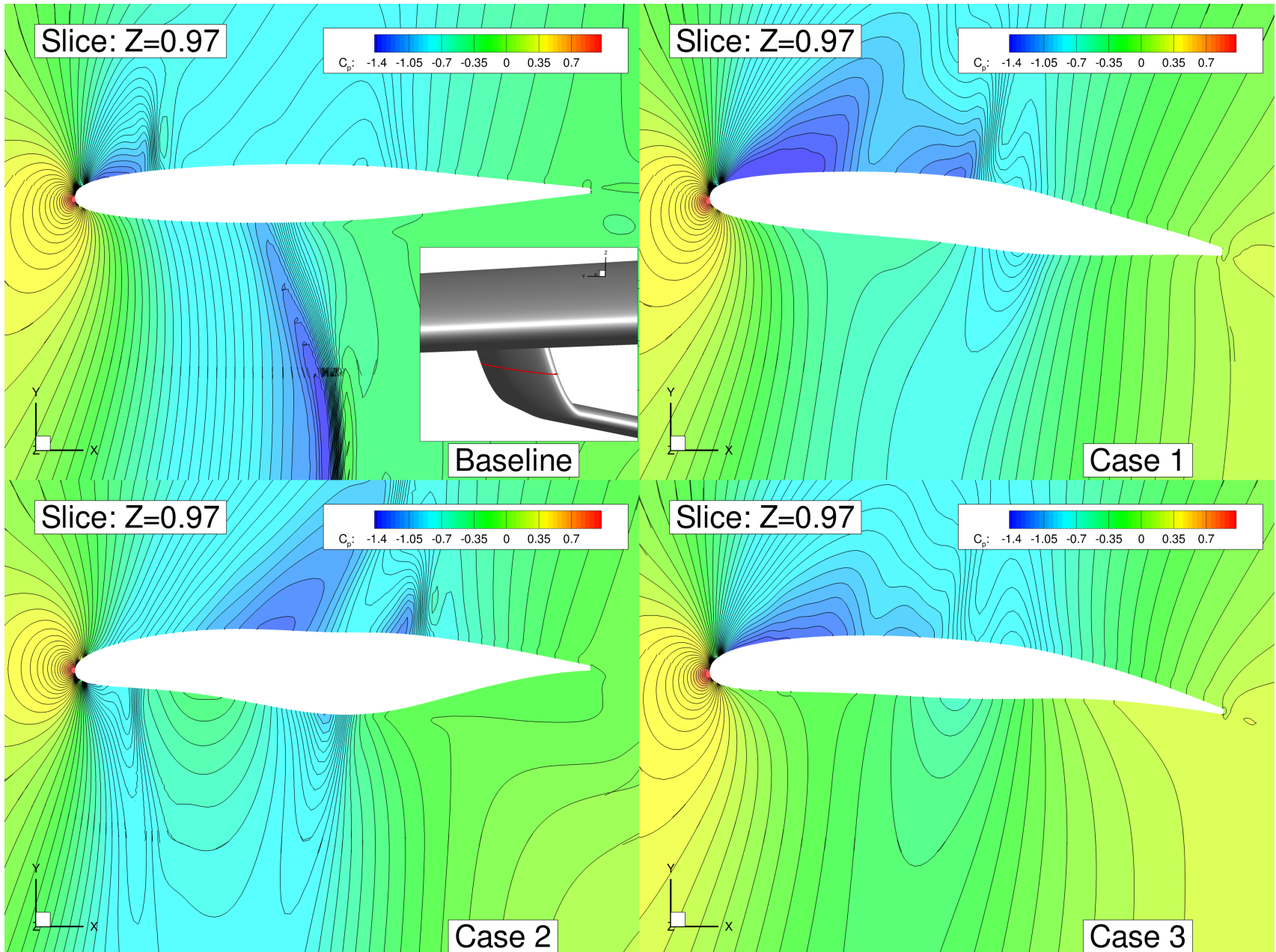
2D Slices of Junction Region



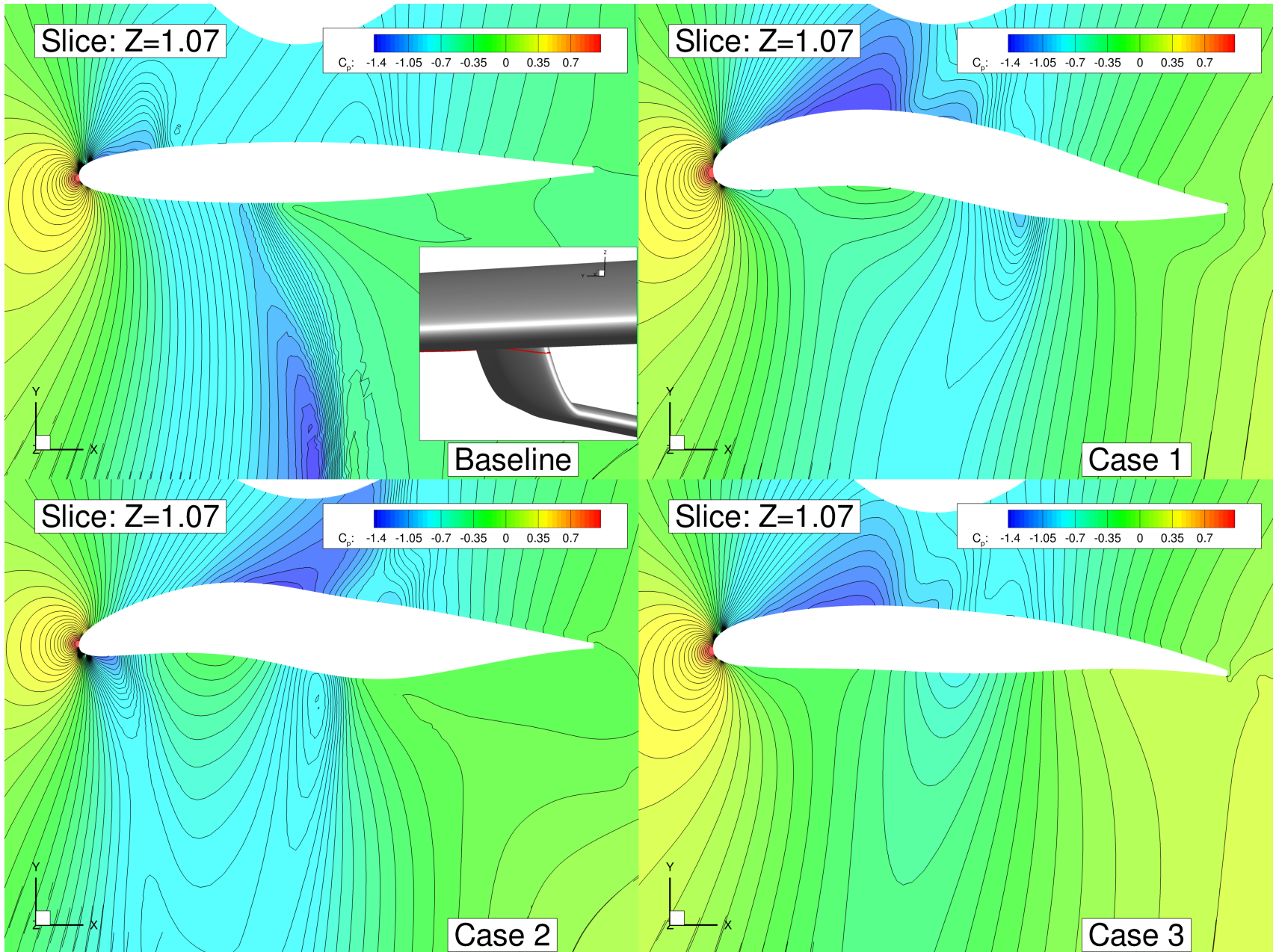
2D Slices of Junction Region



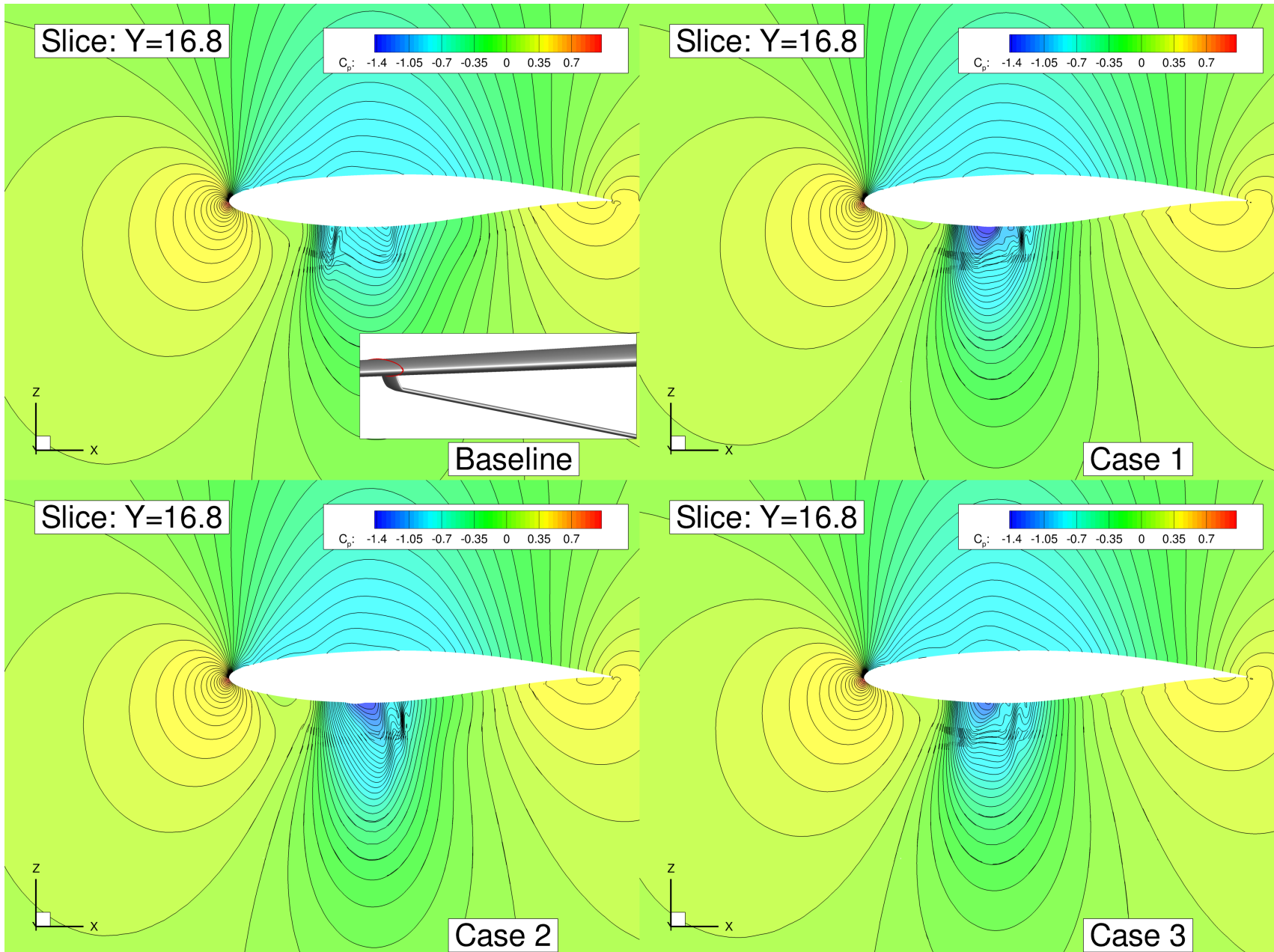
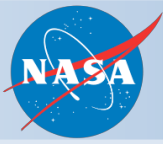
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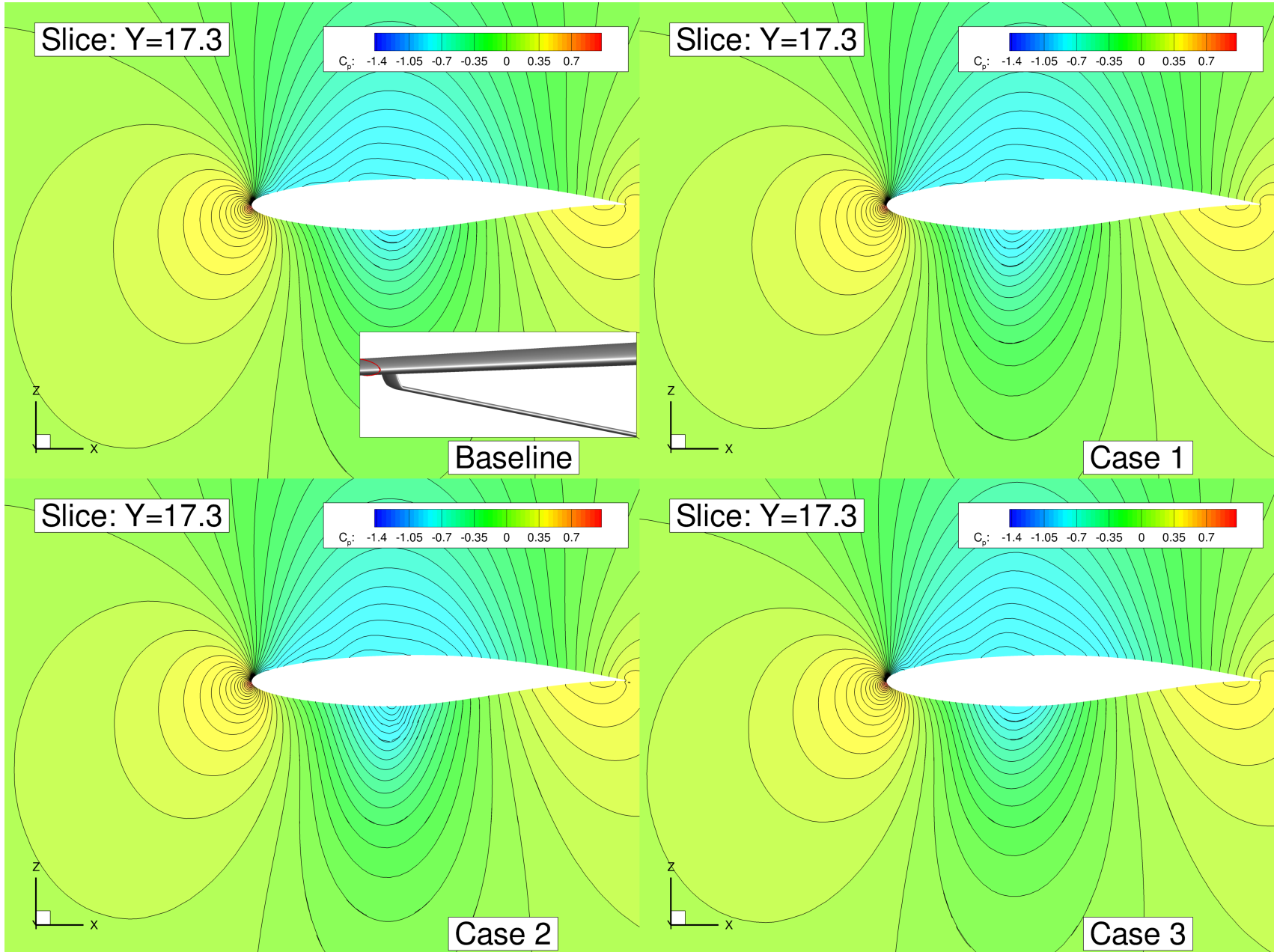
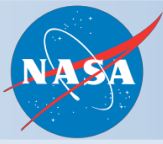
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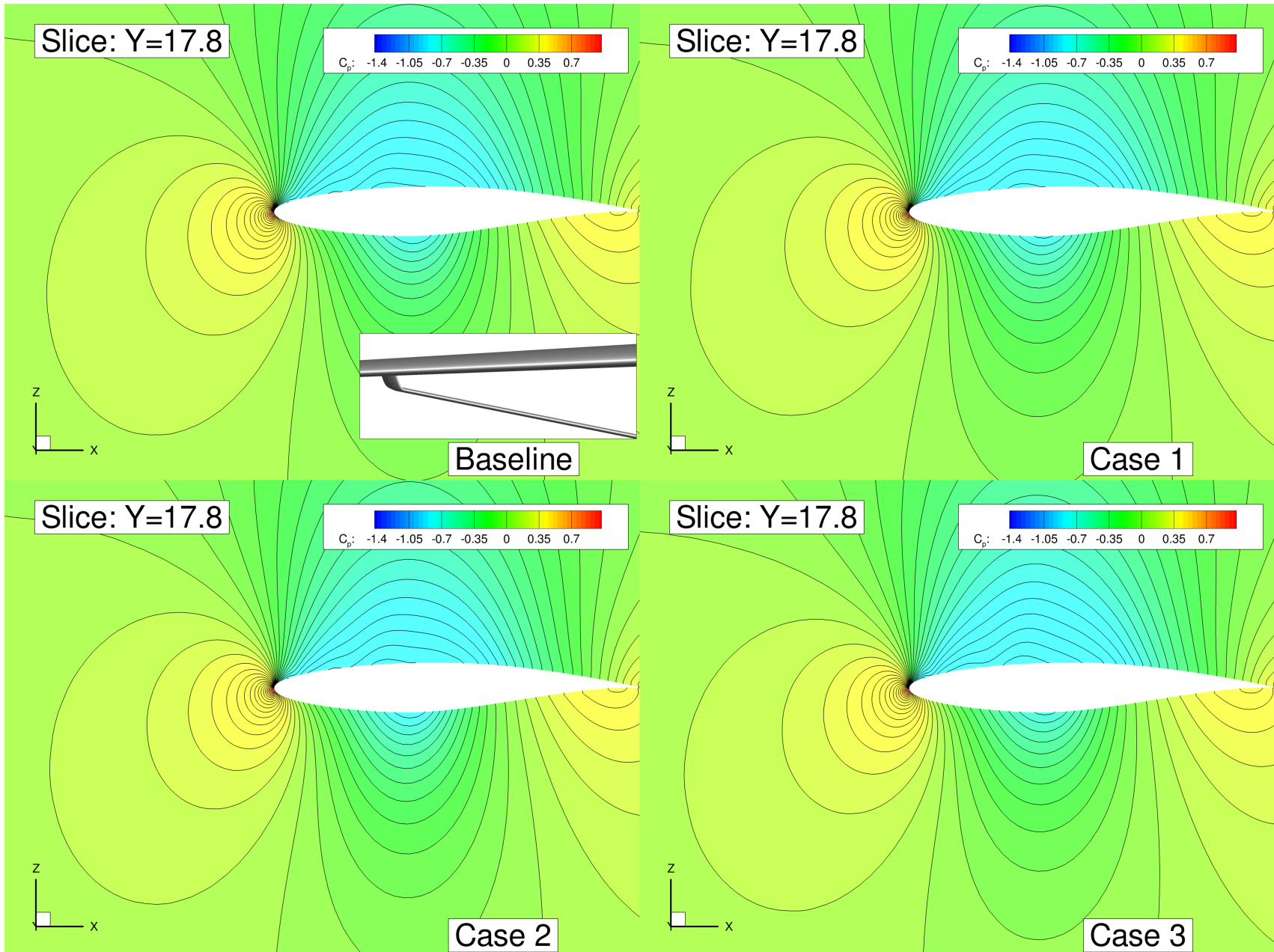
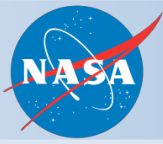
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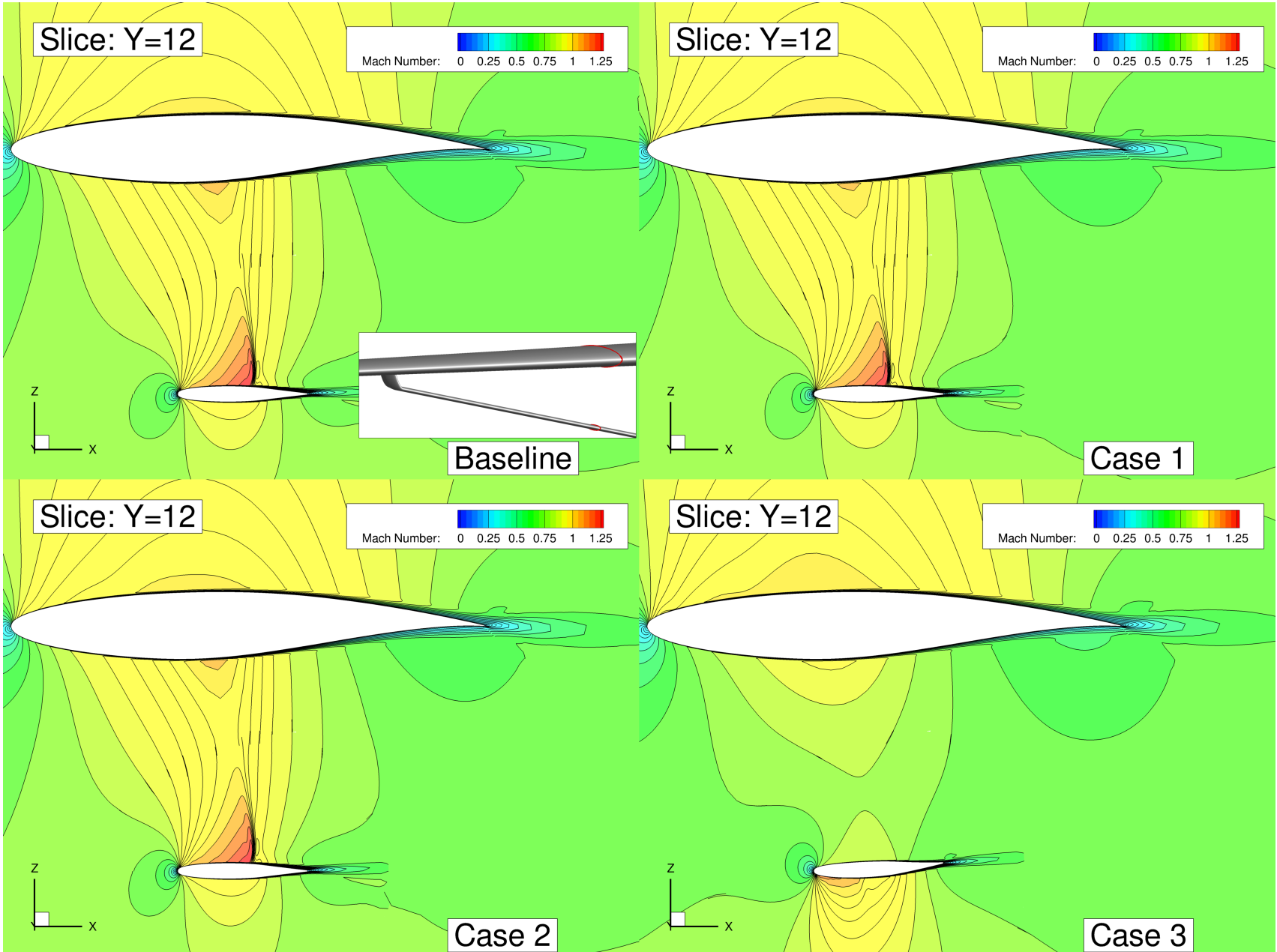
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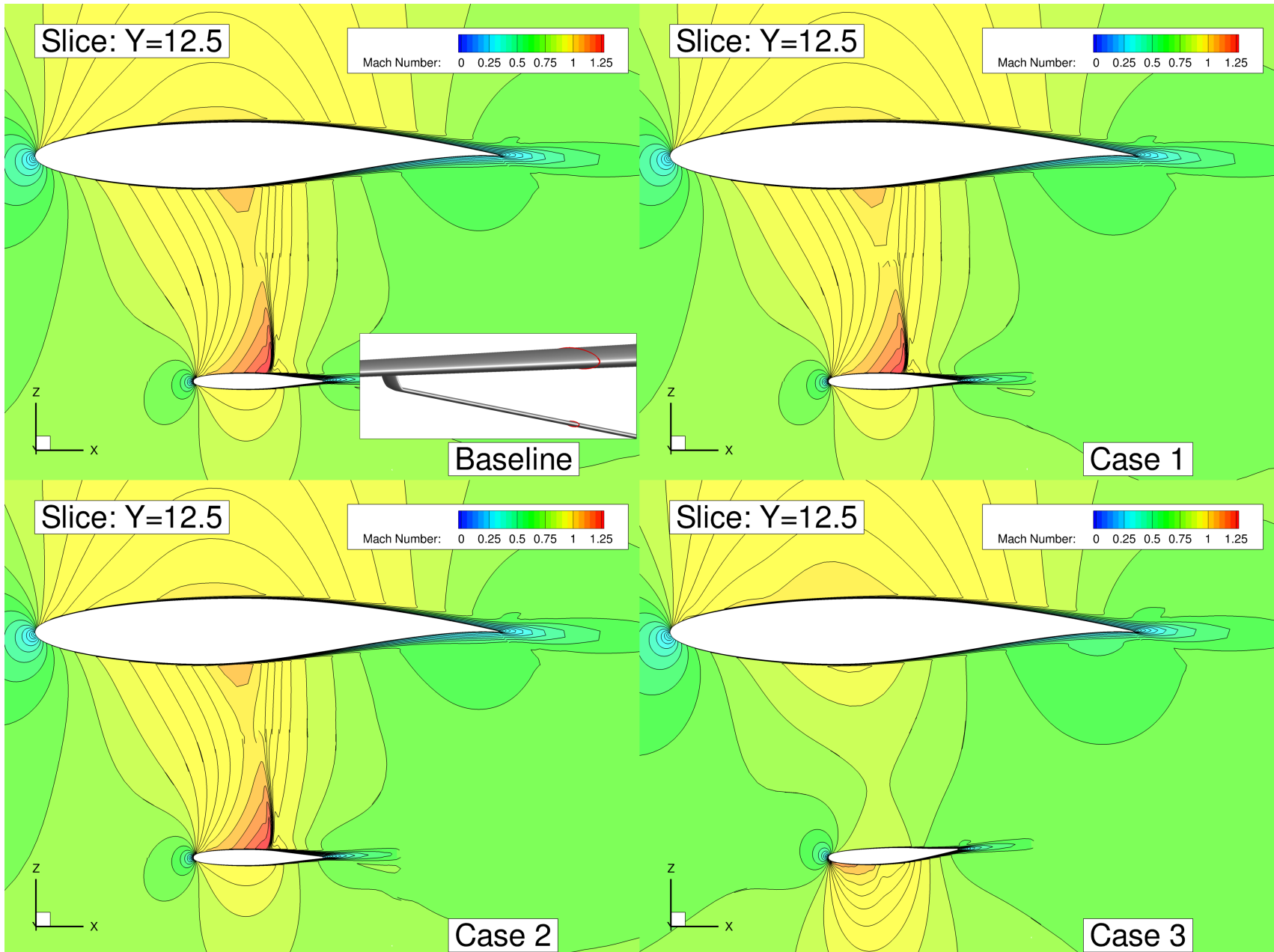
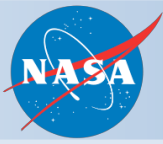
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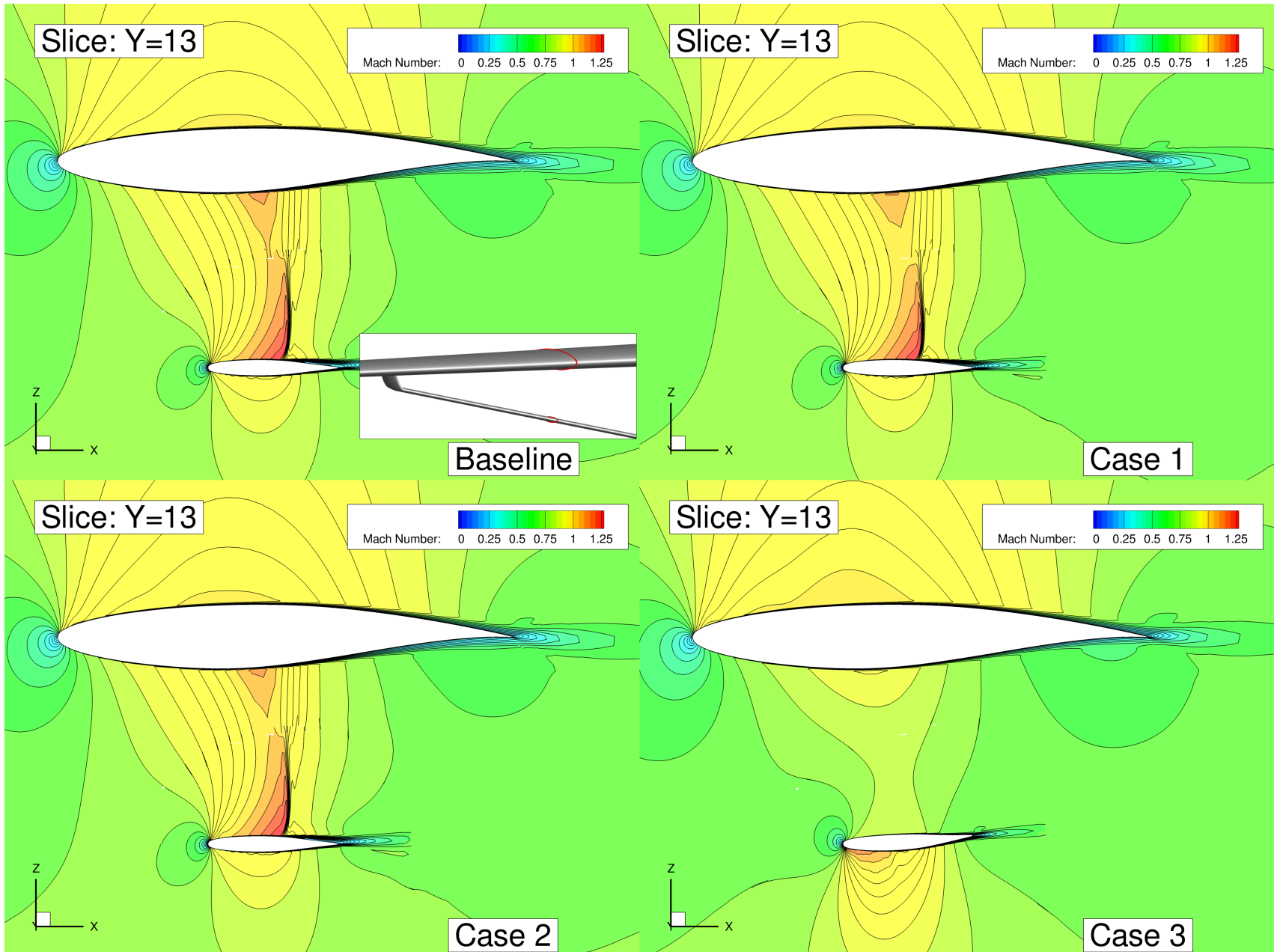
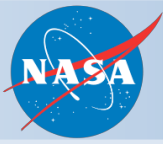
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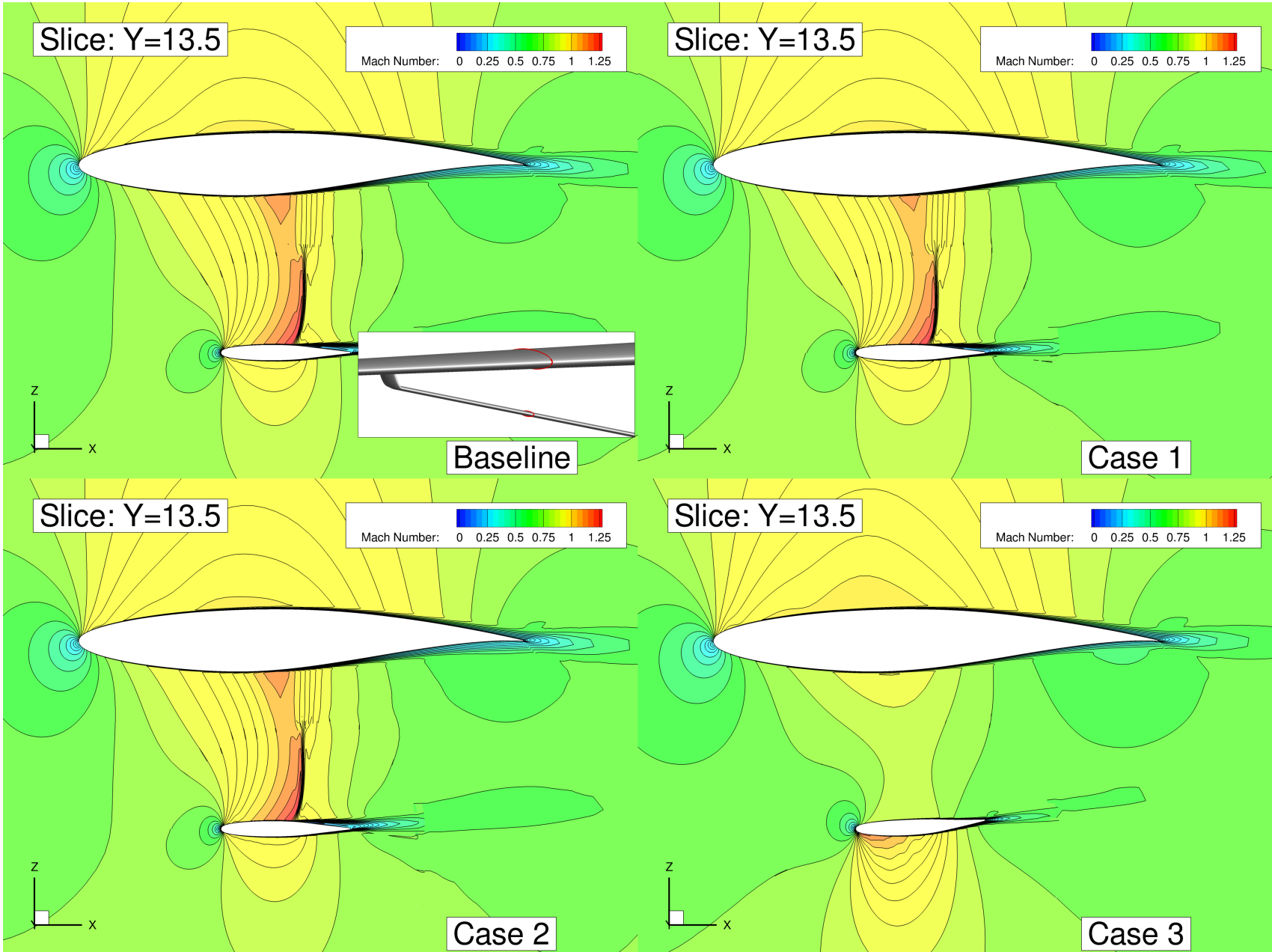
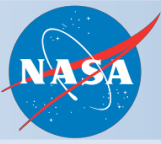
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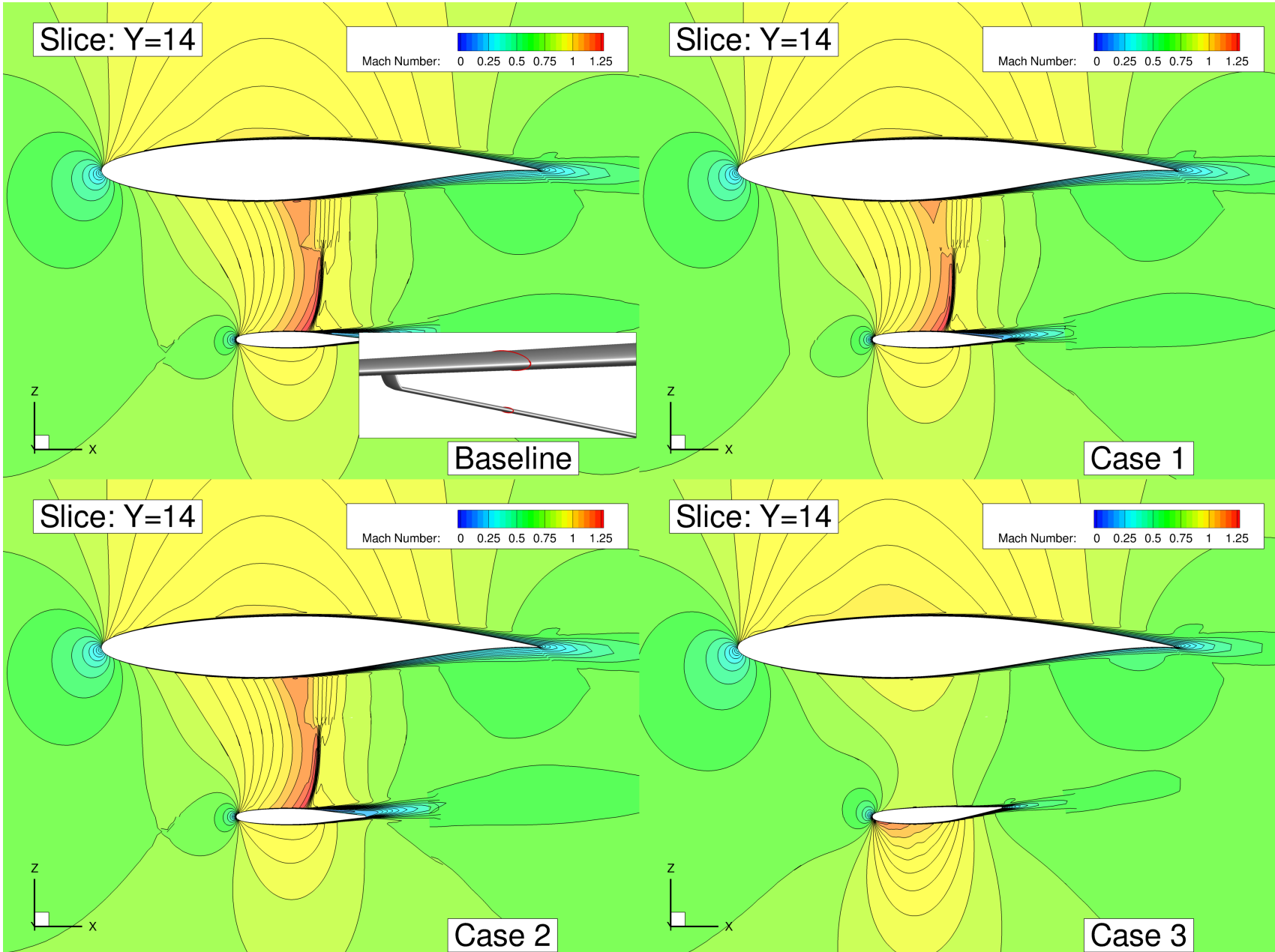
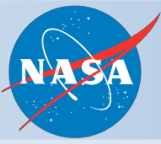
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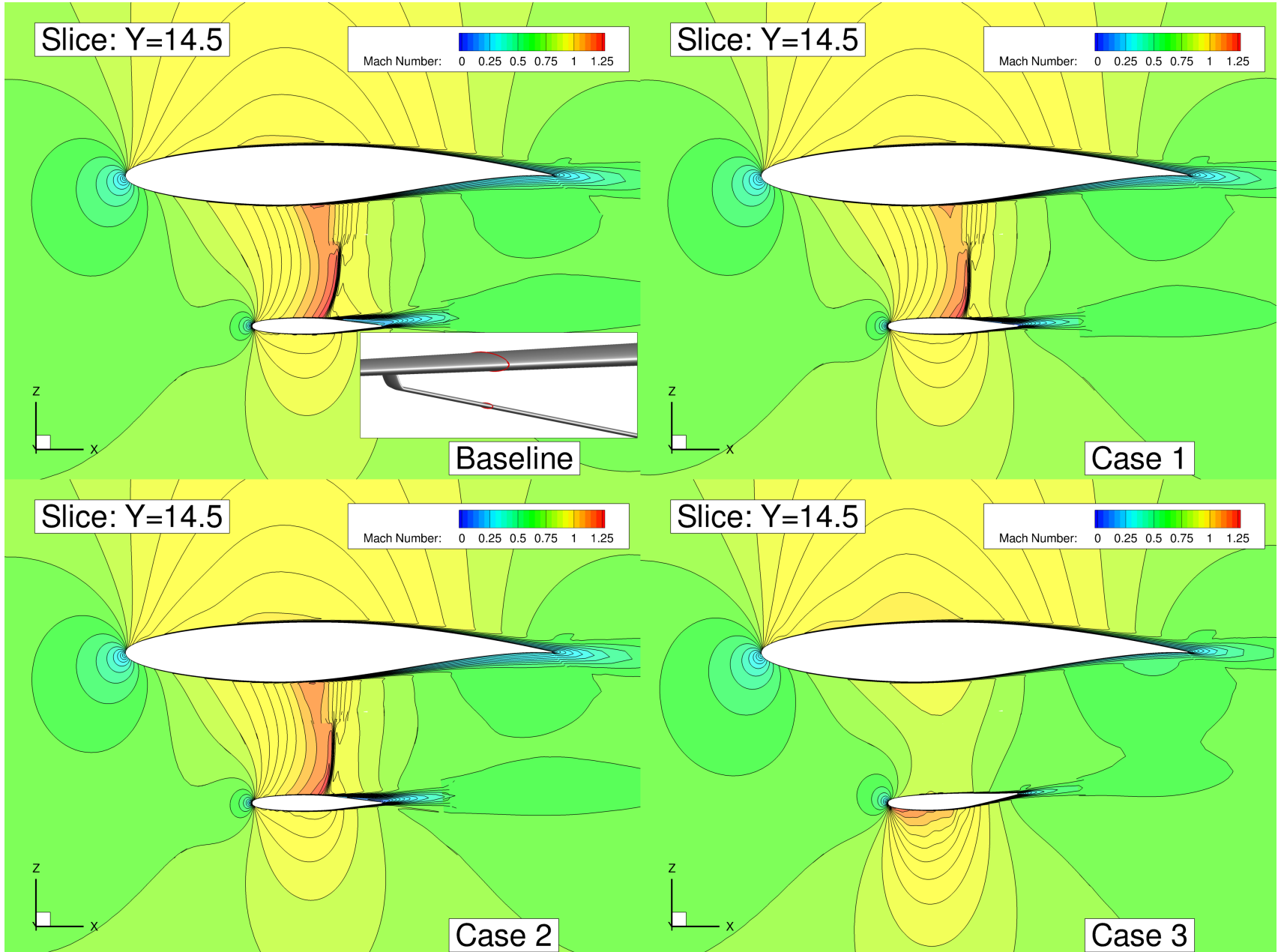
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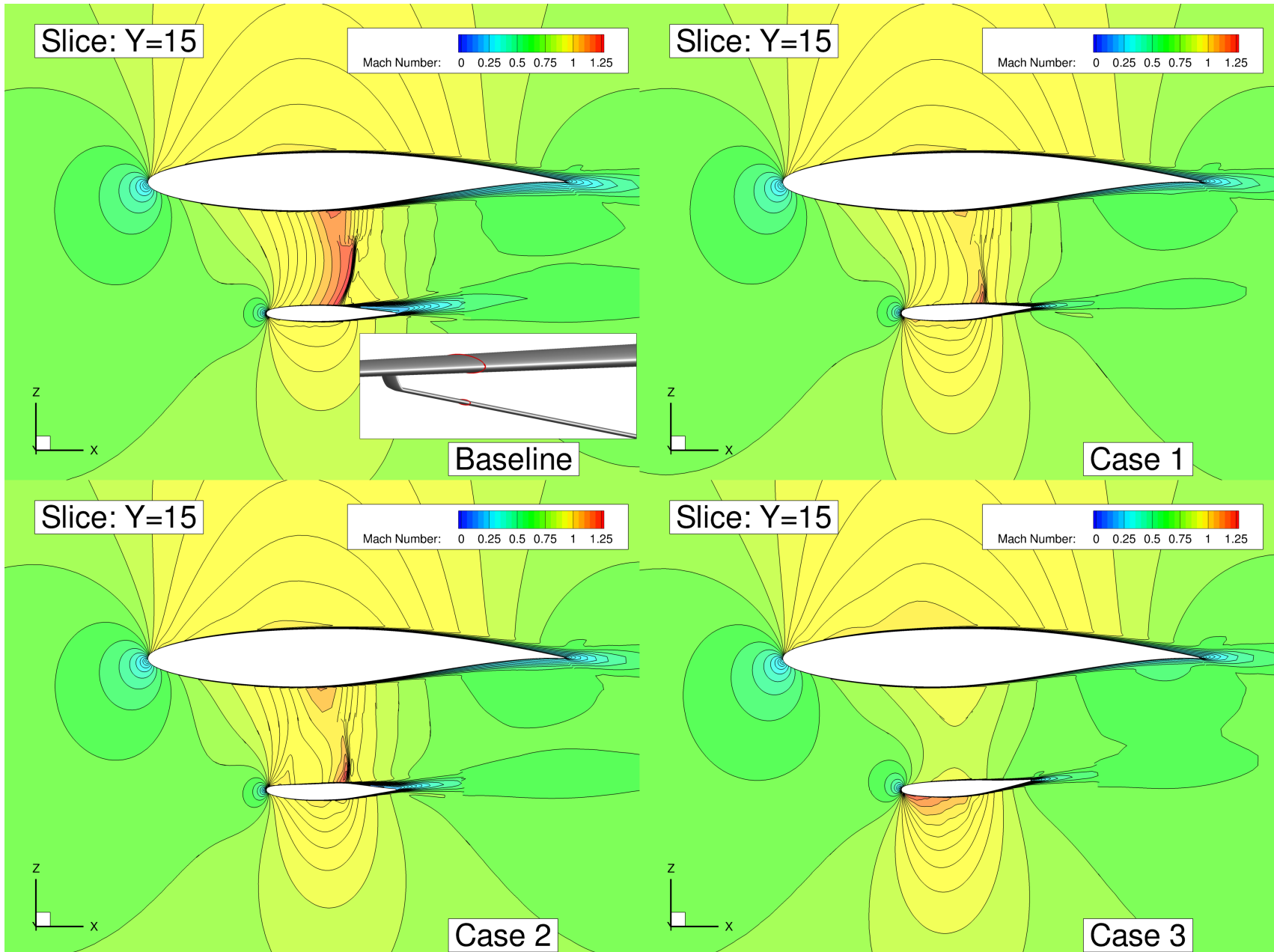
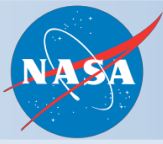
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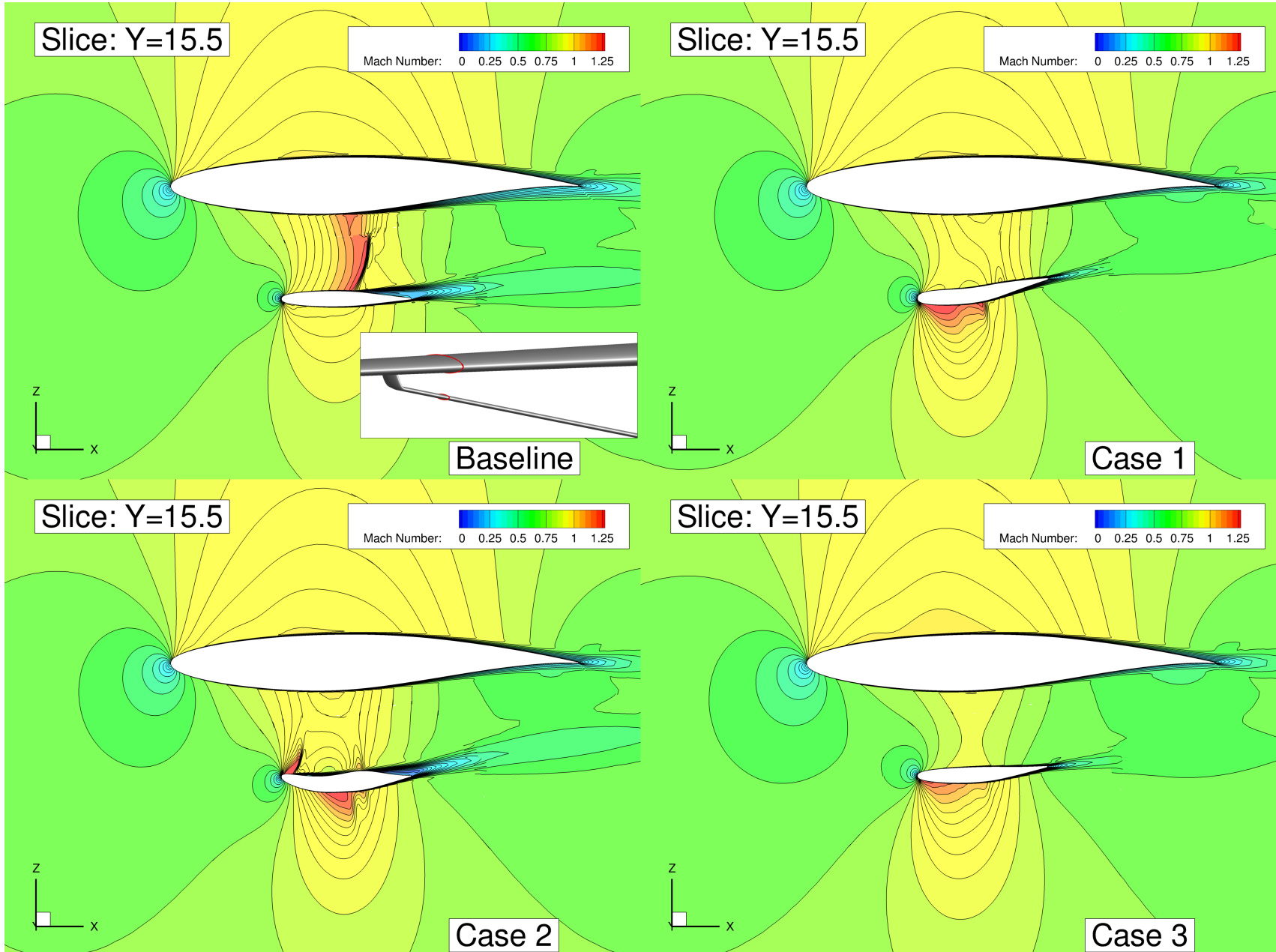
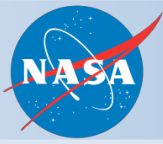
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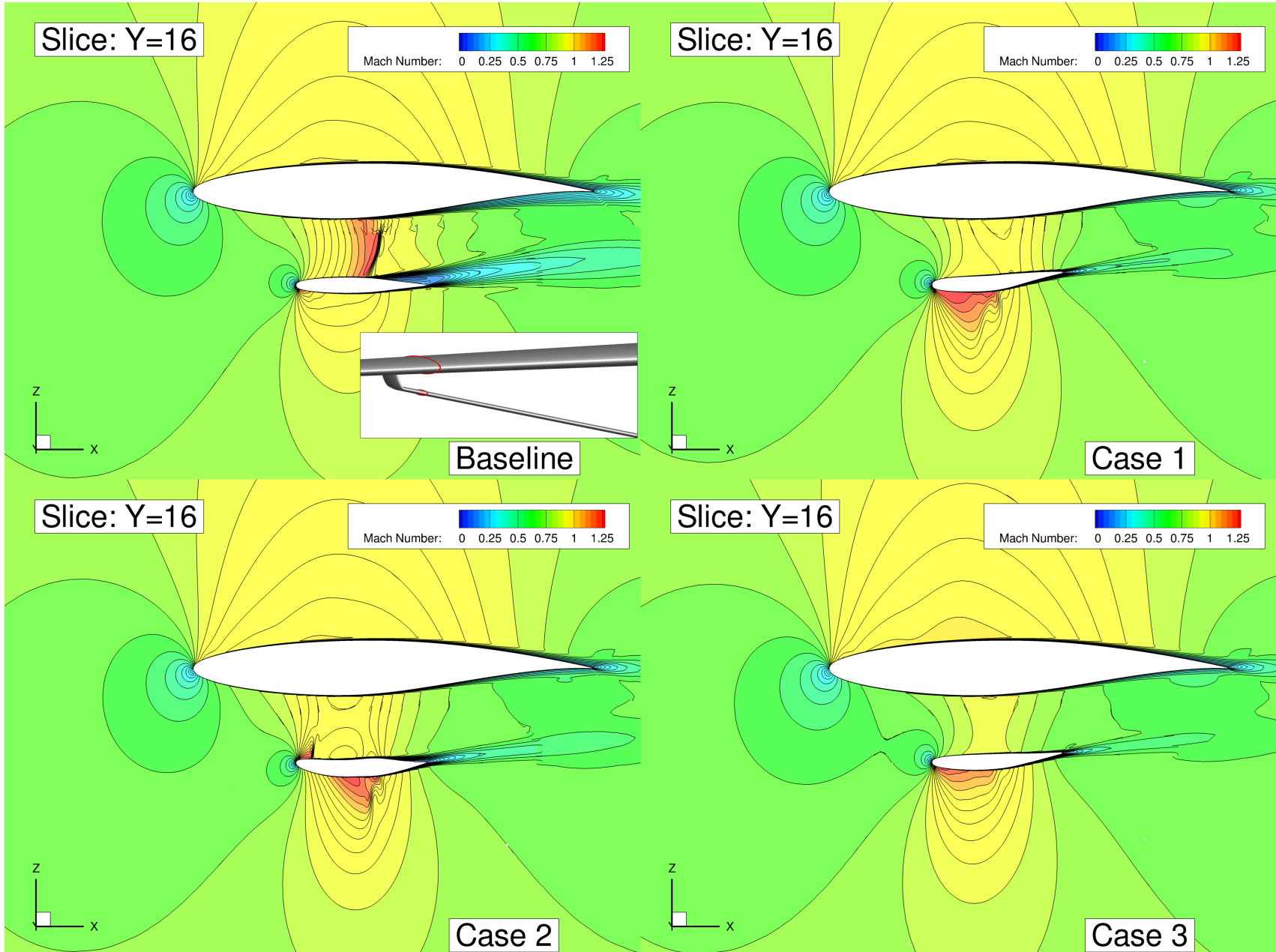
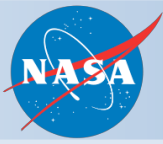
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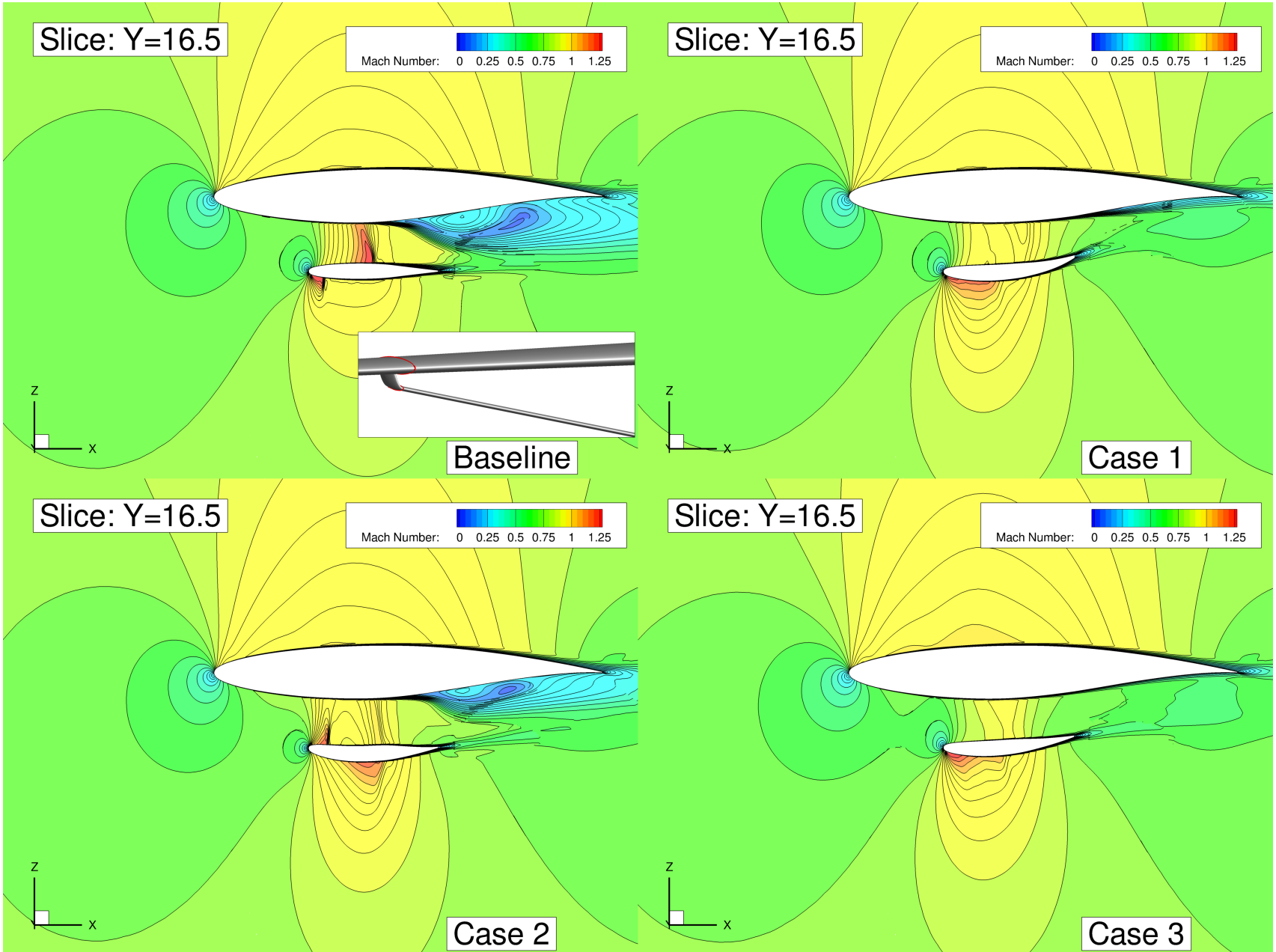
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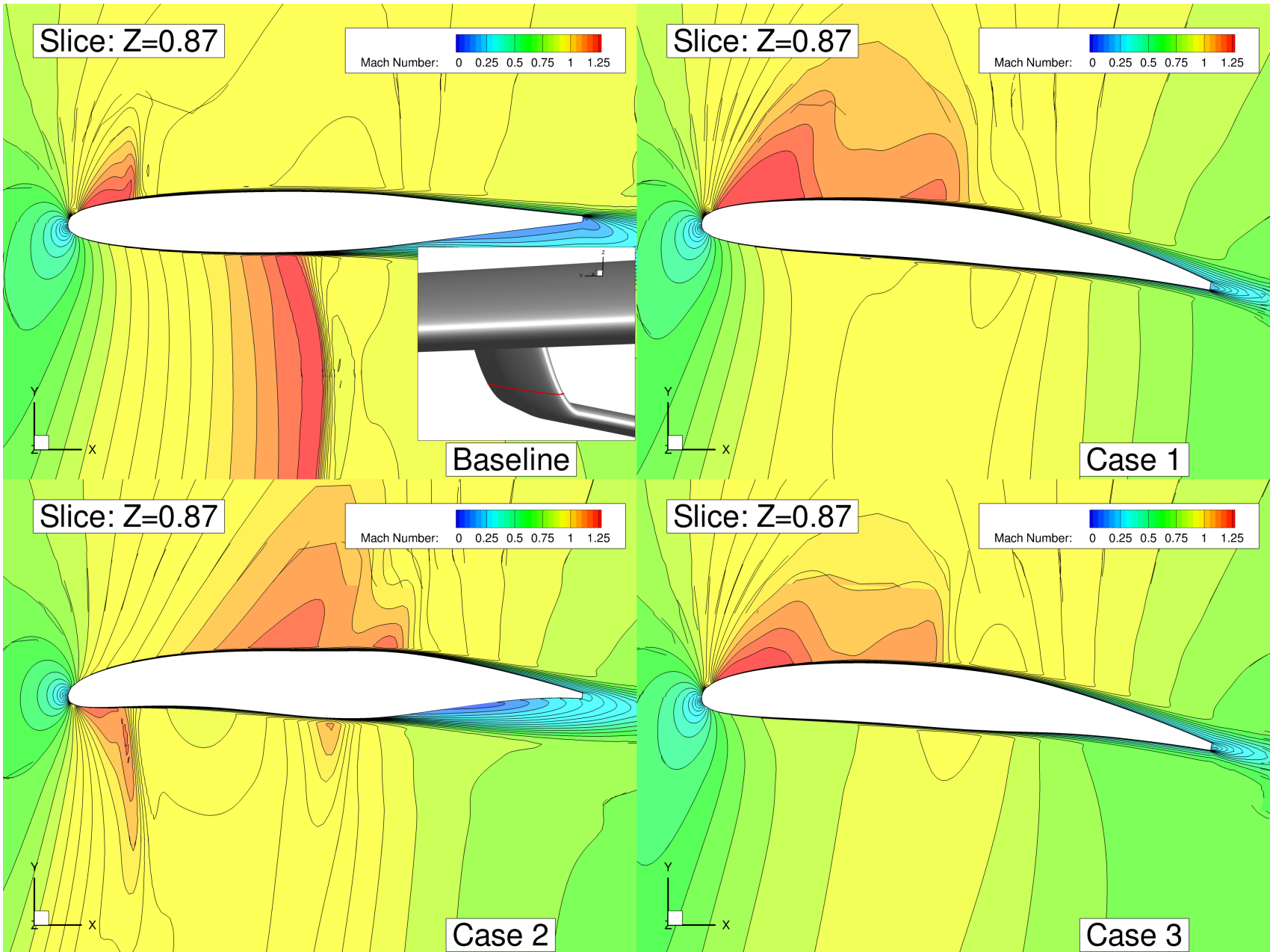
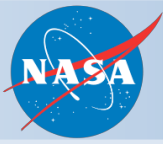
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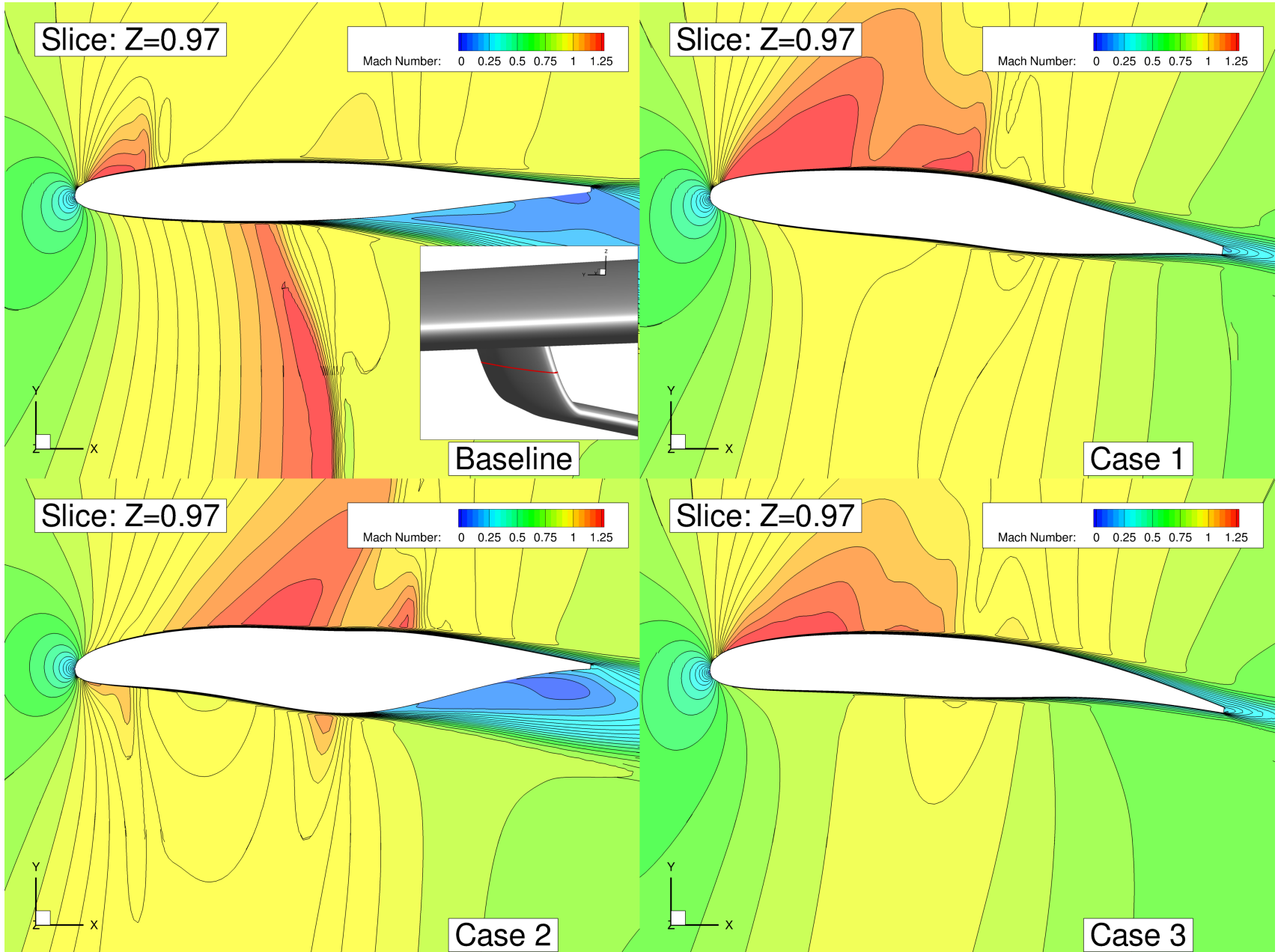
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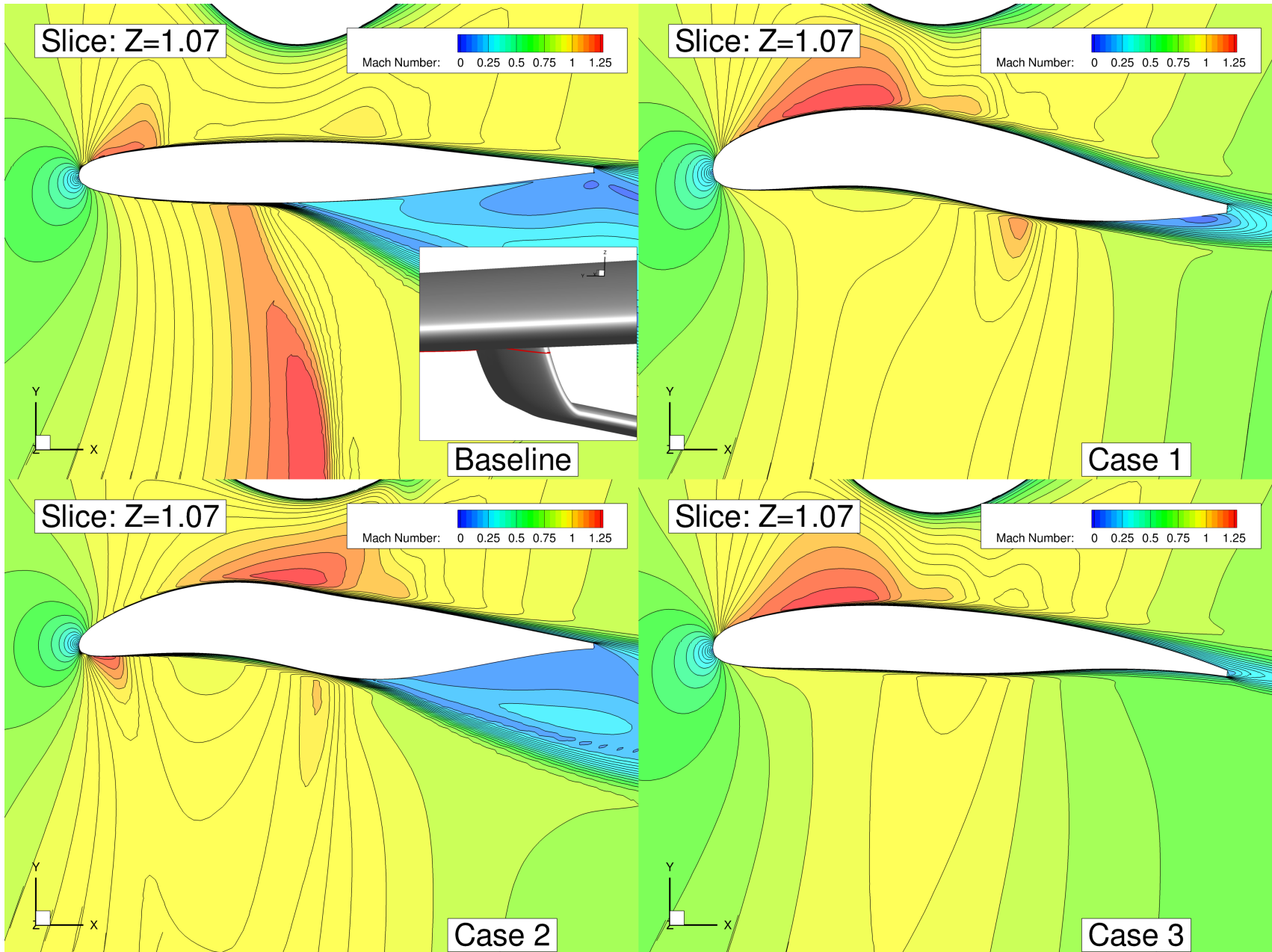
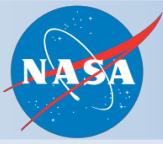
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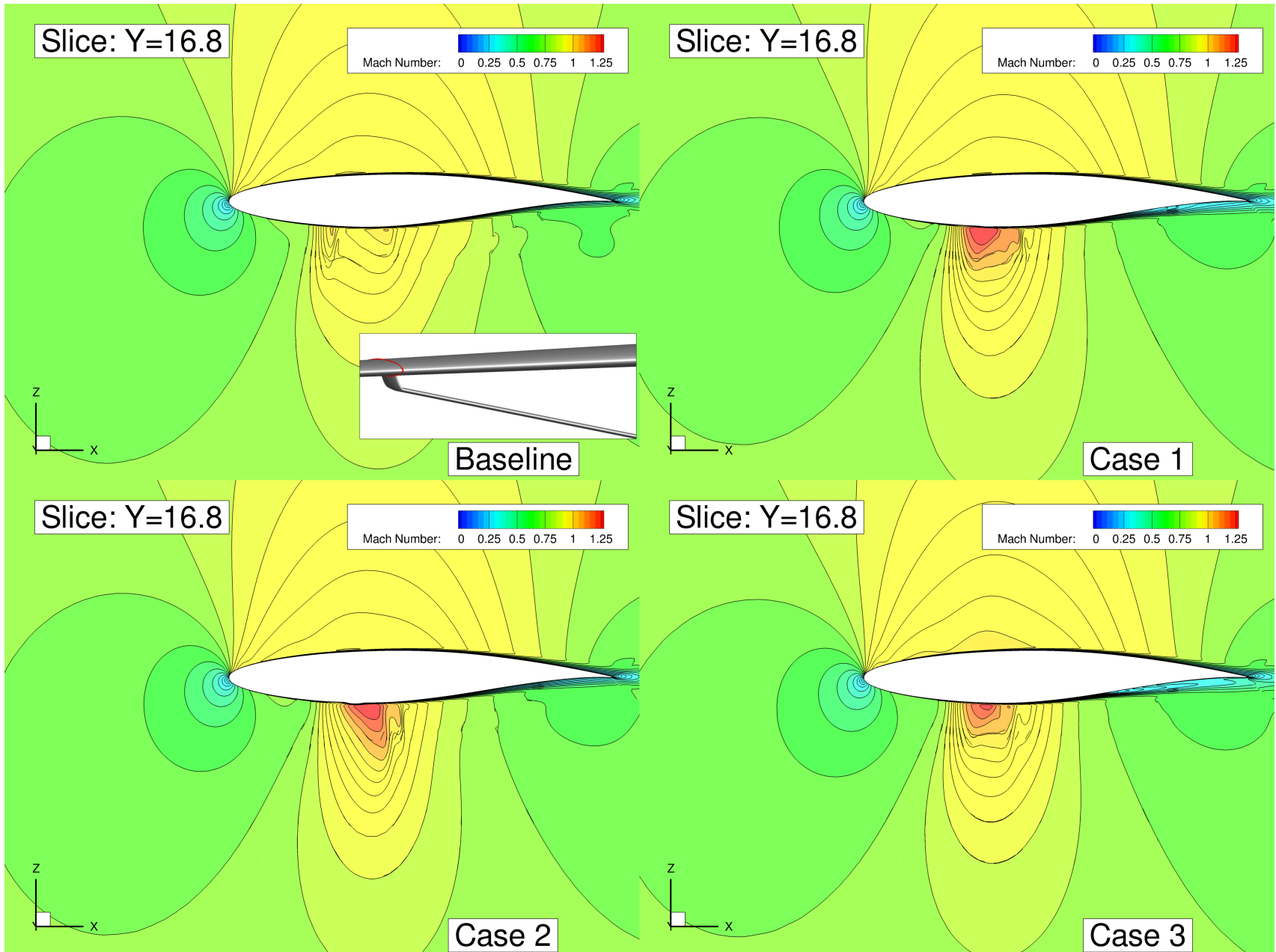
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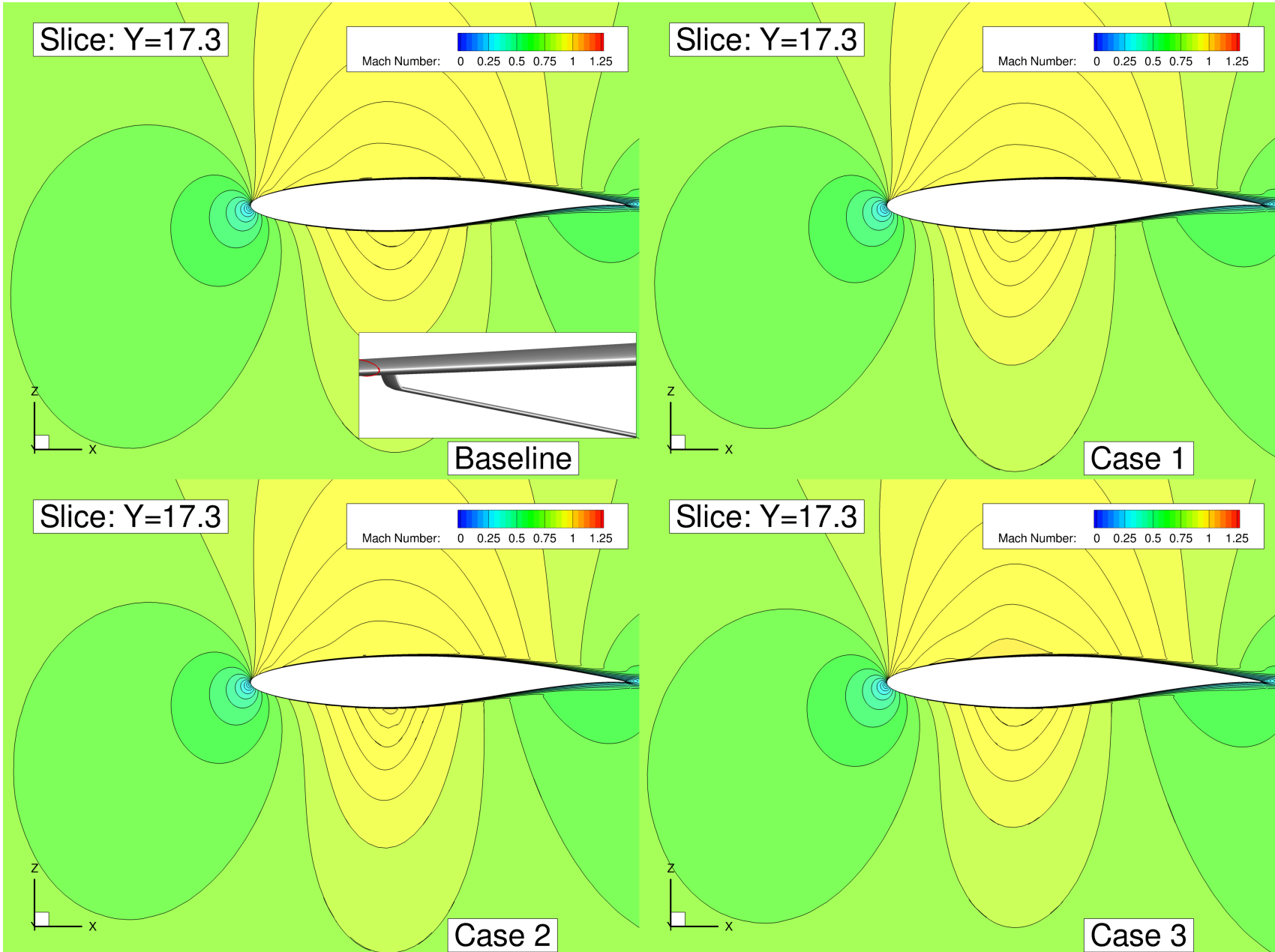
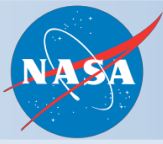
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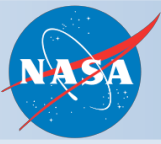
2D Slices of Junction Region



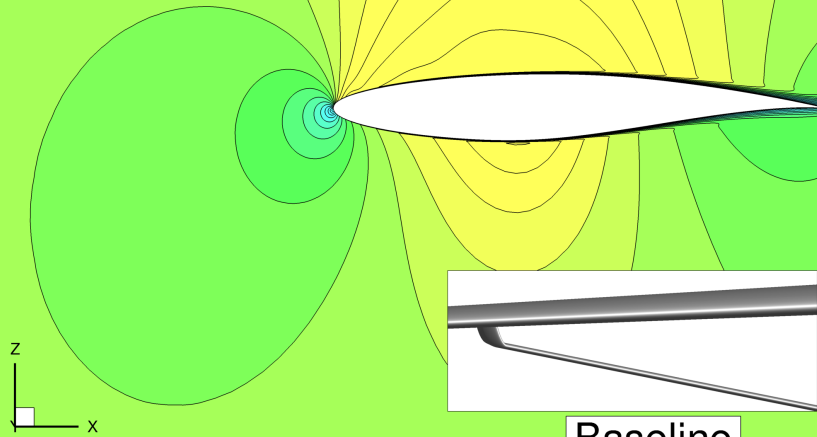
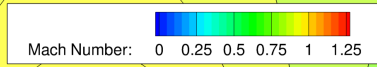
2D Slices of Junction Region



2D Slices of Junction Region

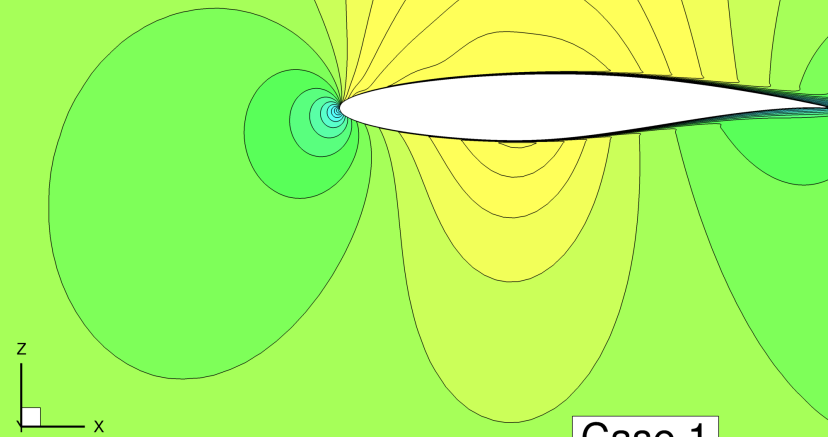
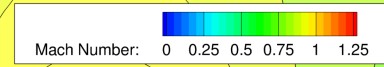


Slice: Y=17.8



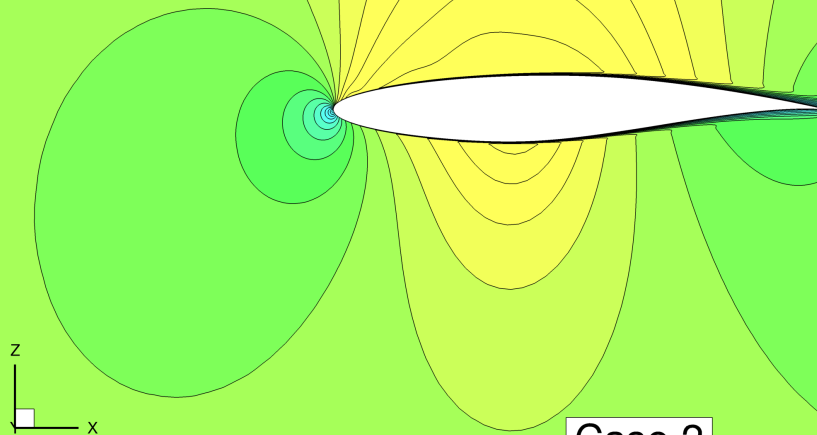
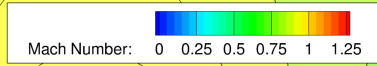
Baseline

Slice: Y=17.8



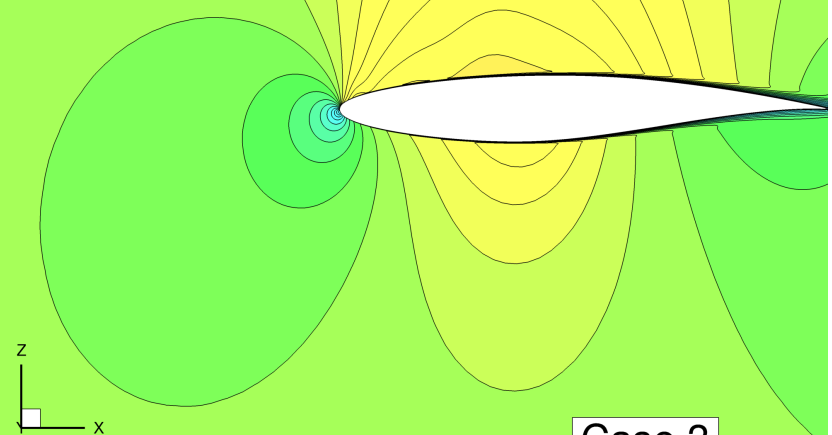
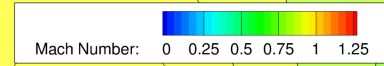
Case 1

Slice: Y=17.8



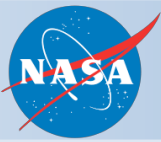
Case 2

Slice: Y=17.8

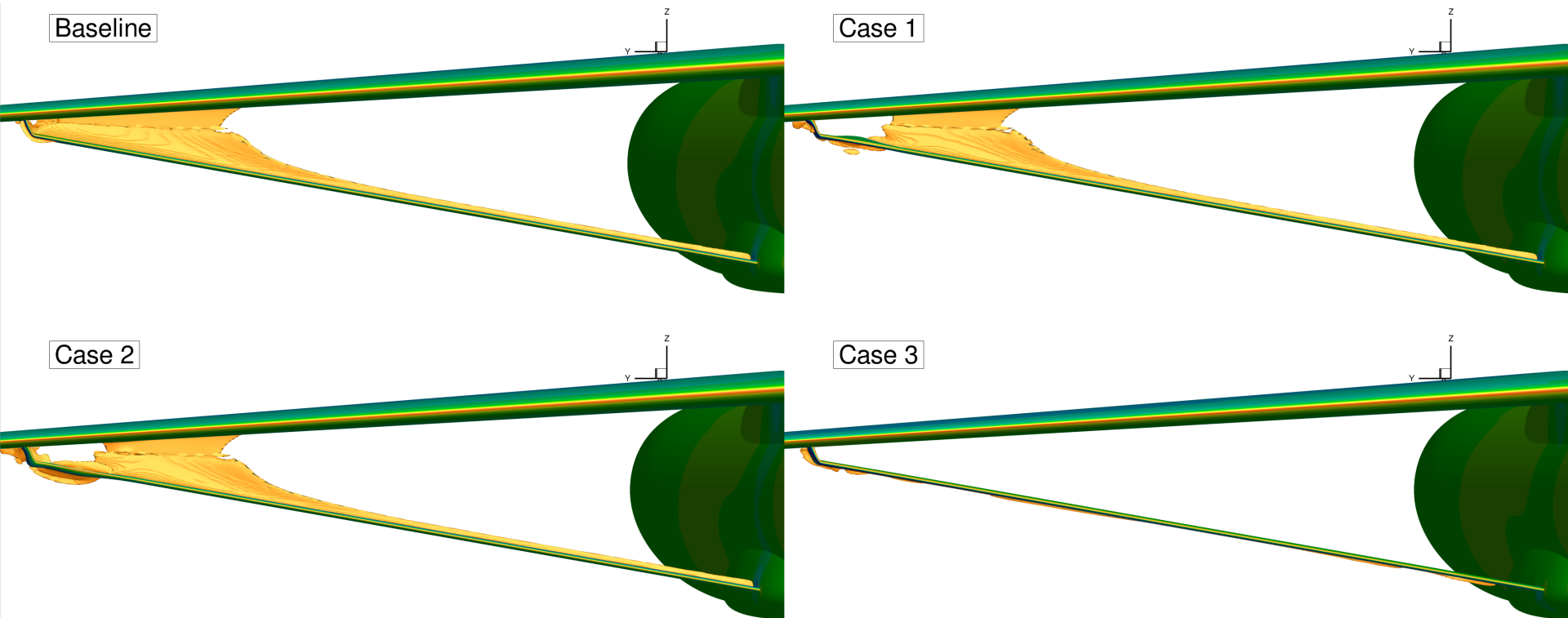


Case 3

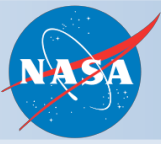
Shock Surface Visualization



- Case 1 successfully removes shock in design region
- Full truss redesign has weak shock on lower surface

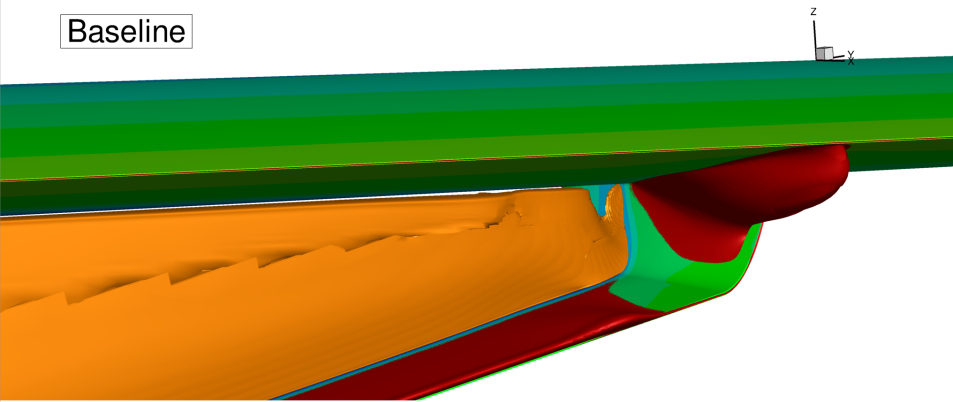


Separated Flow

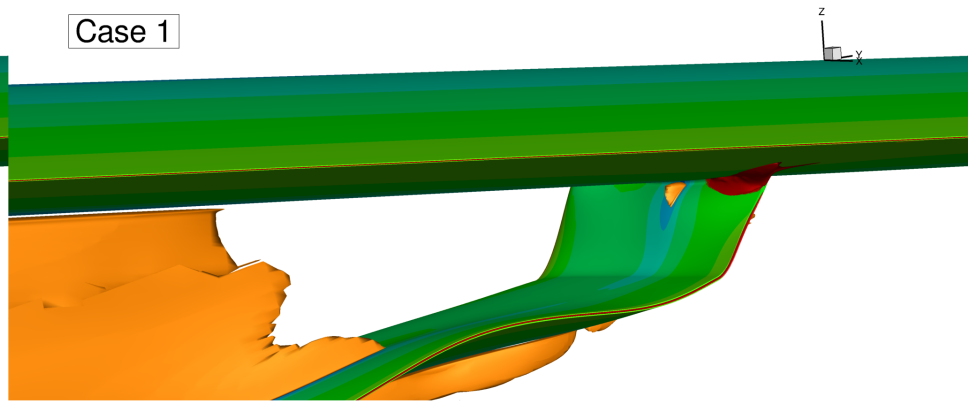


- All designs reduce the amount of separated flow at the strut-wing junction
- Red iso-contour at $V_x = -.0001$

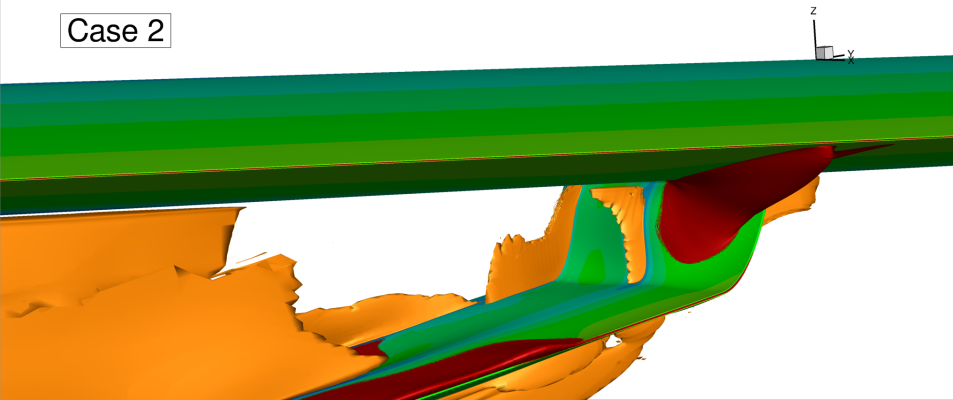
Baseline



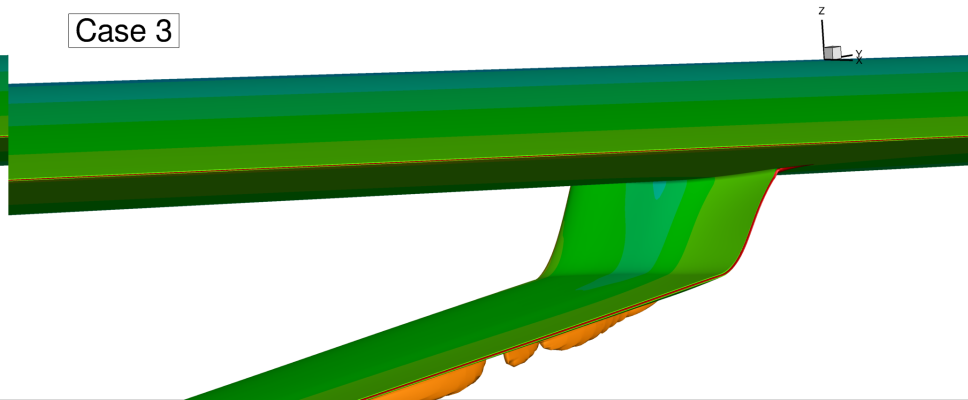
Case 1



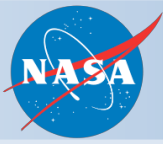
Case 2



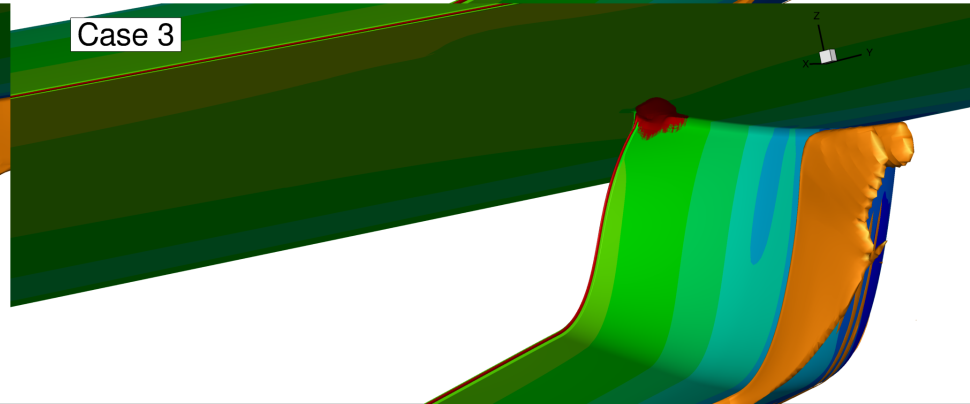
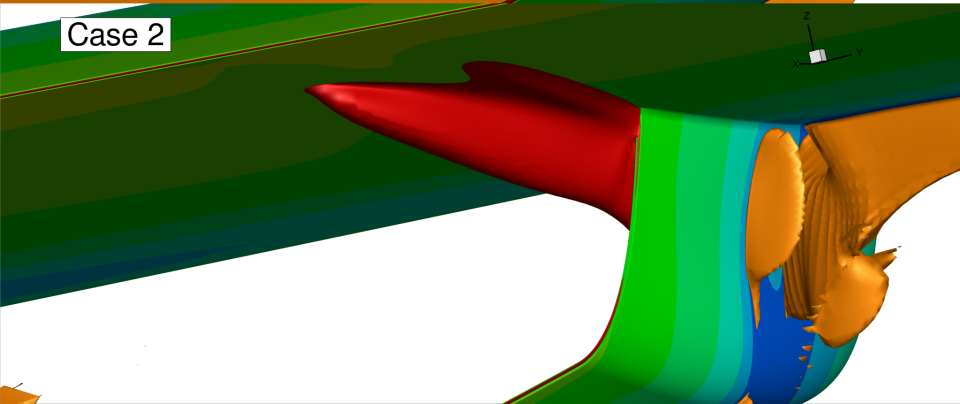
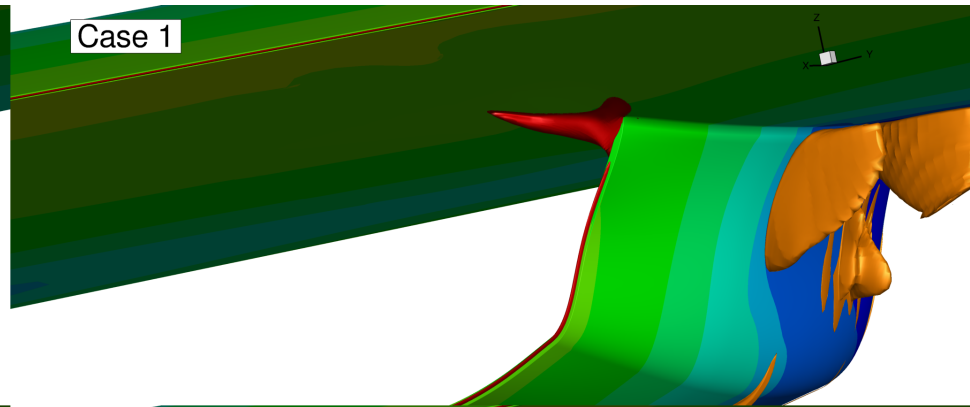
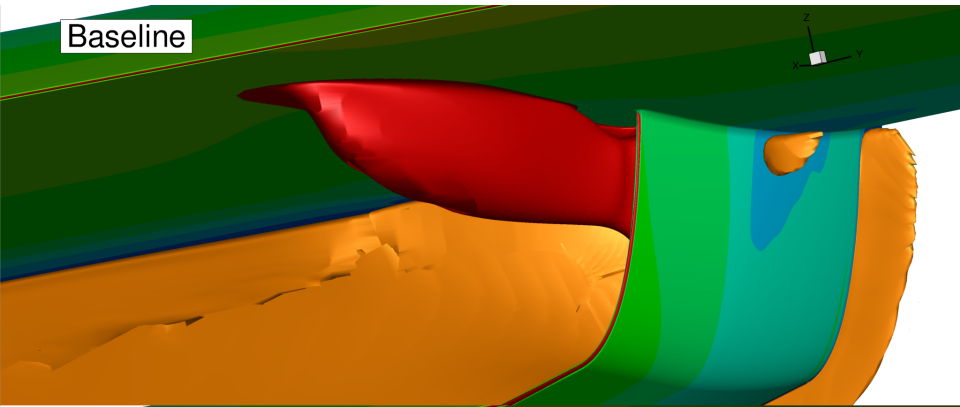
Case 3



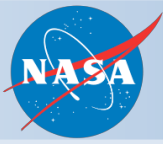
Separated Flow



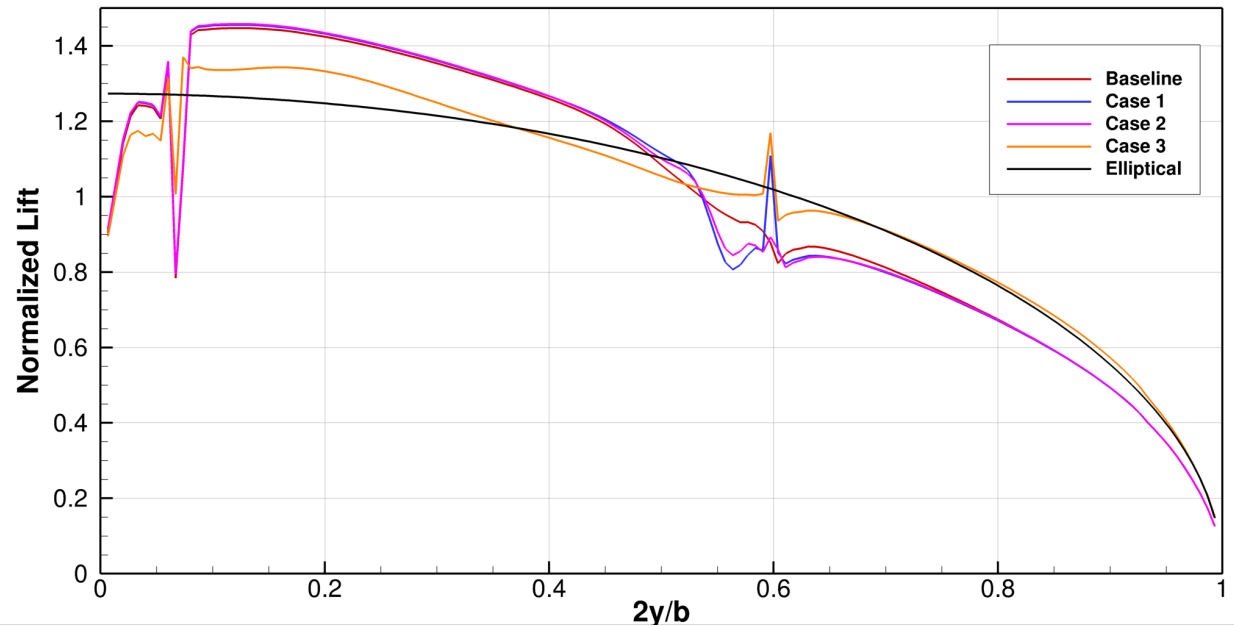
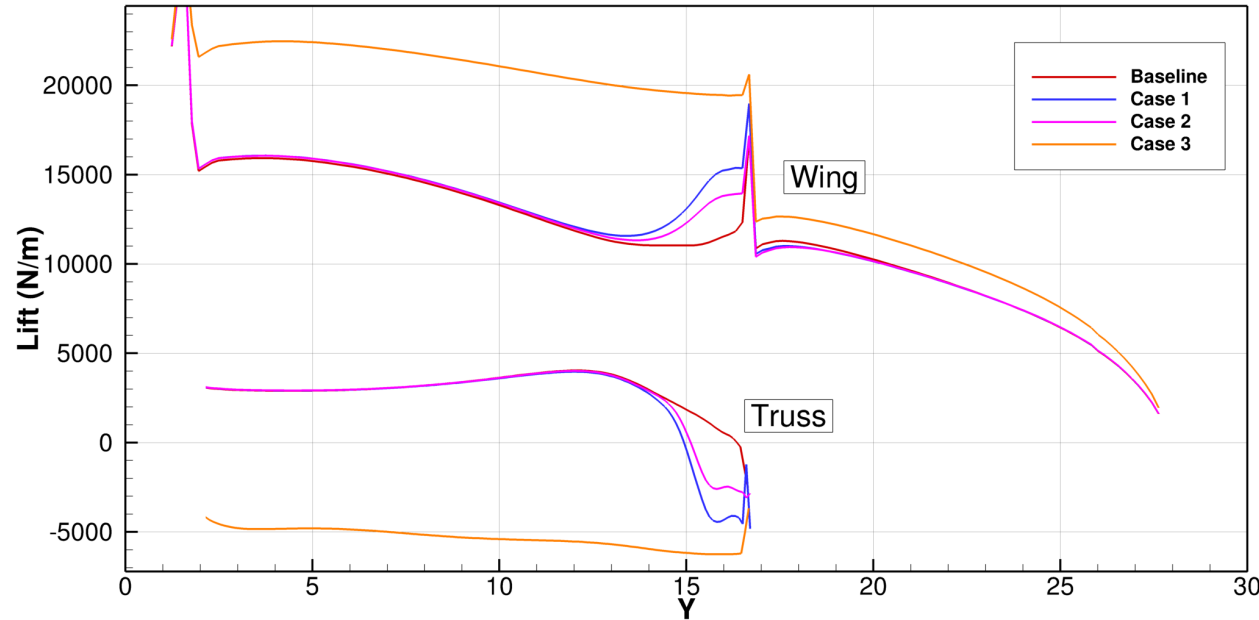
- All designs reduce the amount of separated flow at the strut-wing junction
- Red iso-contour at $V_x = -.0001$



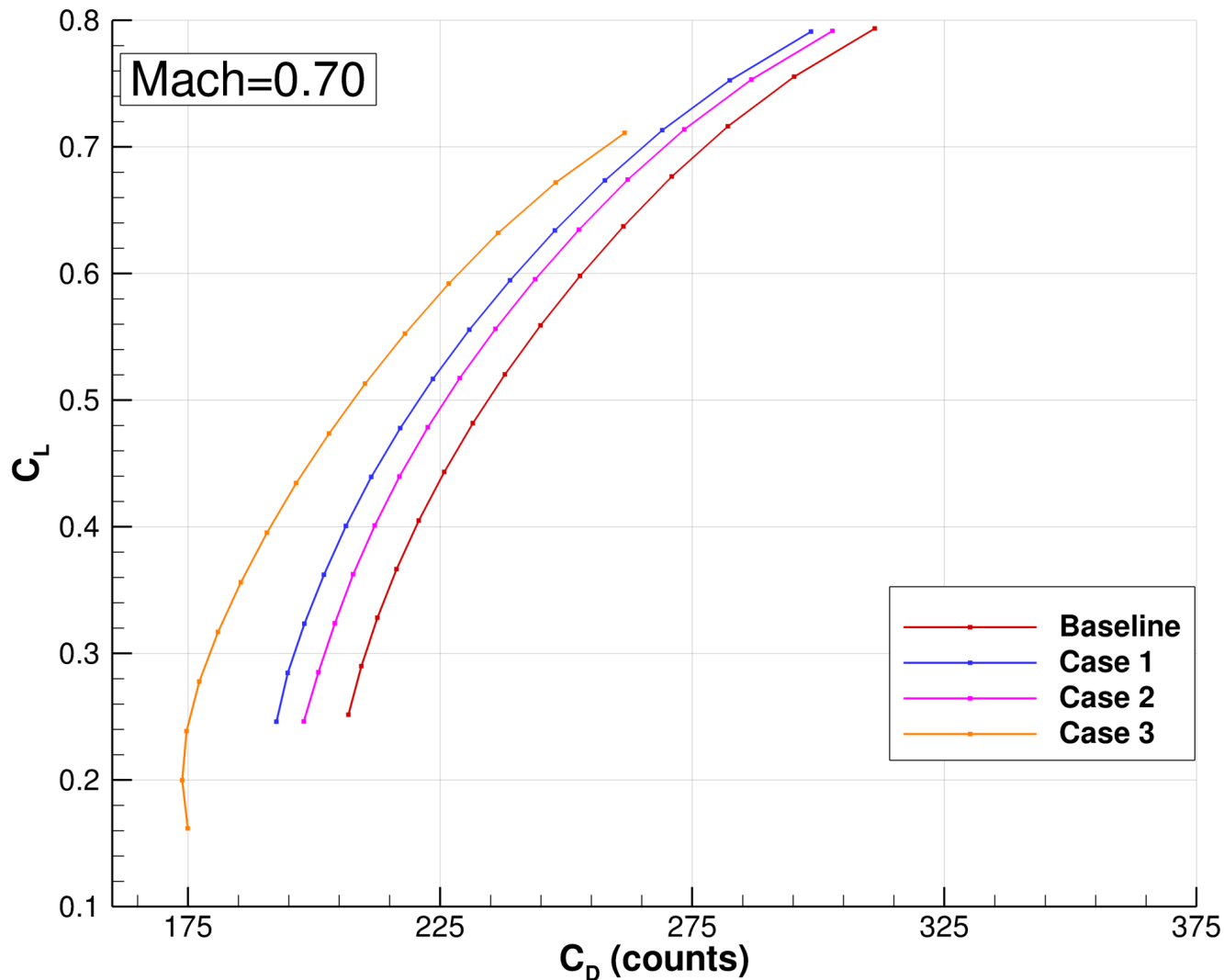
Lift Distributions



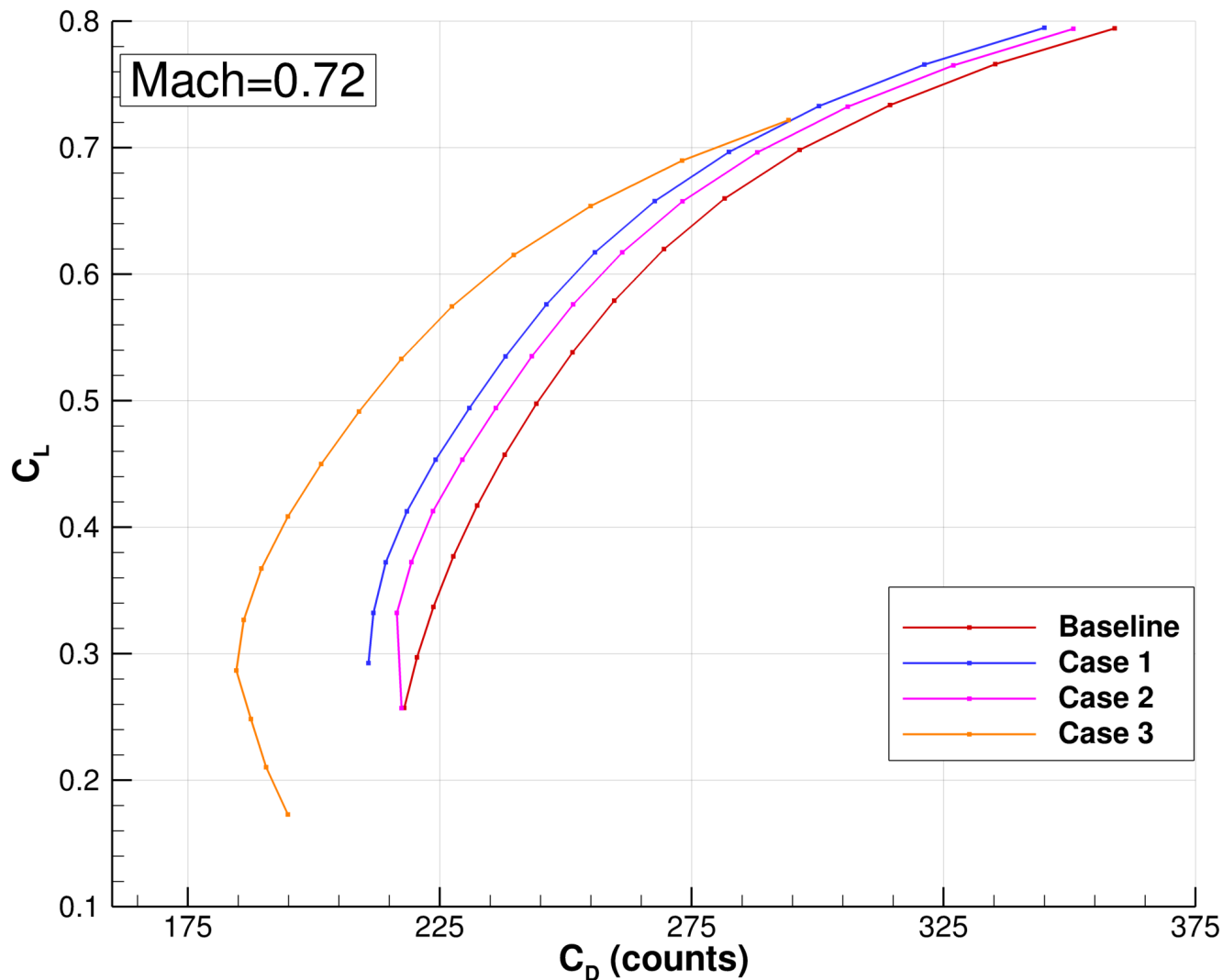
- All optimized designs reduce truss lift
- Nearly elliptical lift distribution and increased angle of attack for case 3
- Negative truss lift is optimal!



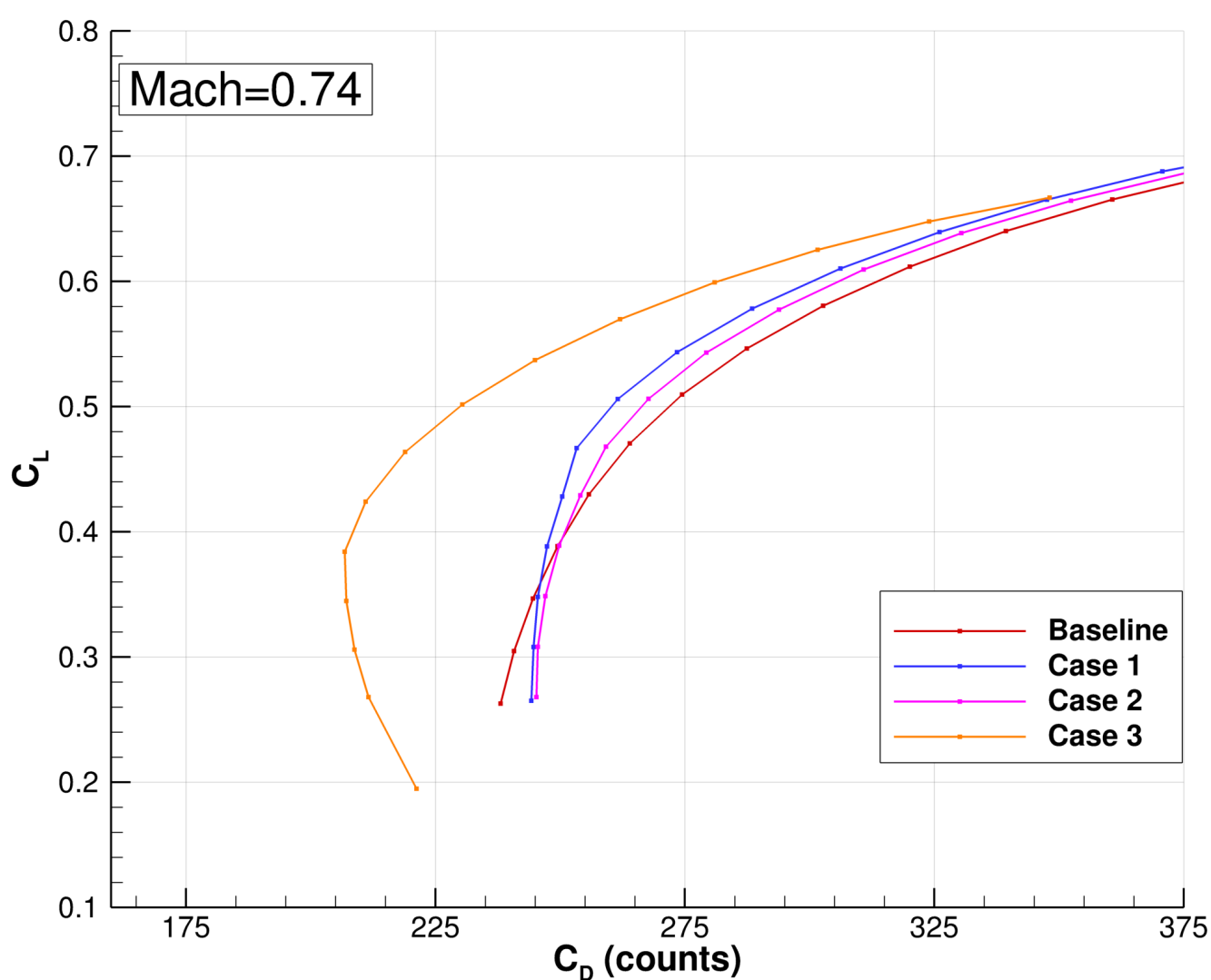
- Consistent improvement across Mach and angle of attacks



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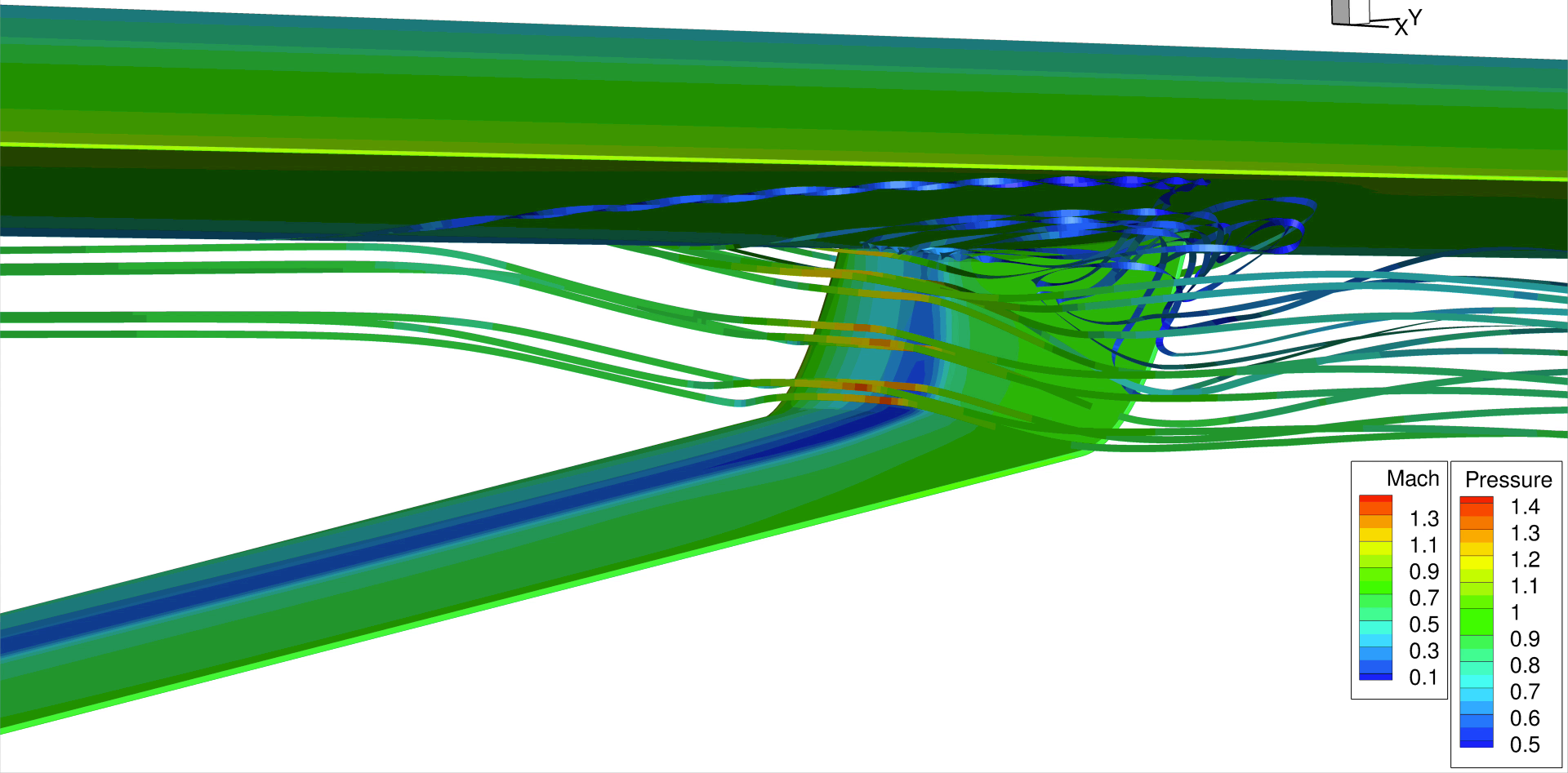
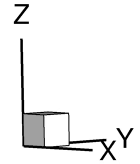
- Consistent improvement across Mach and angle of attacks



Optimization Case 1



Solution: 0

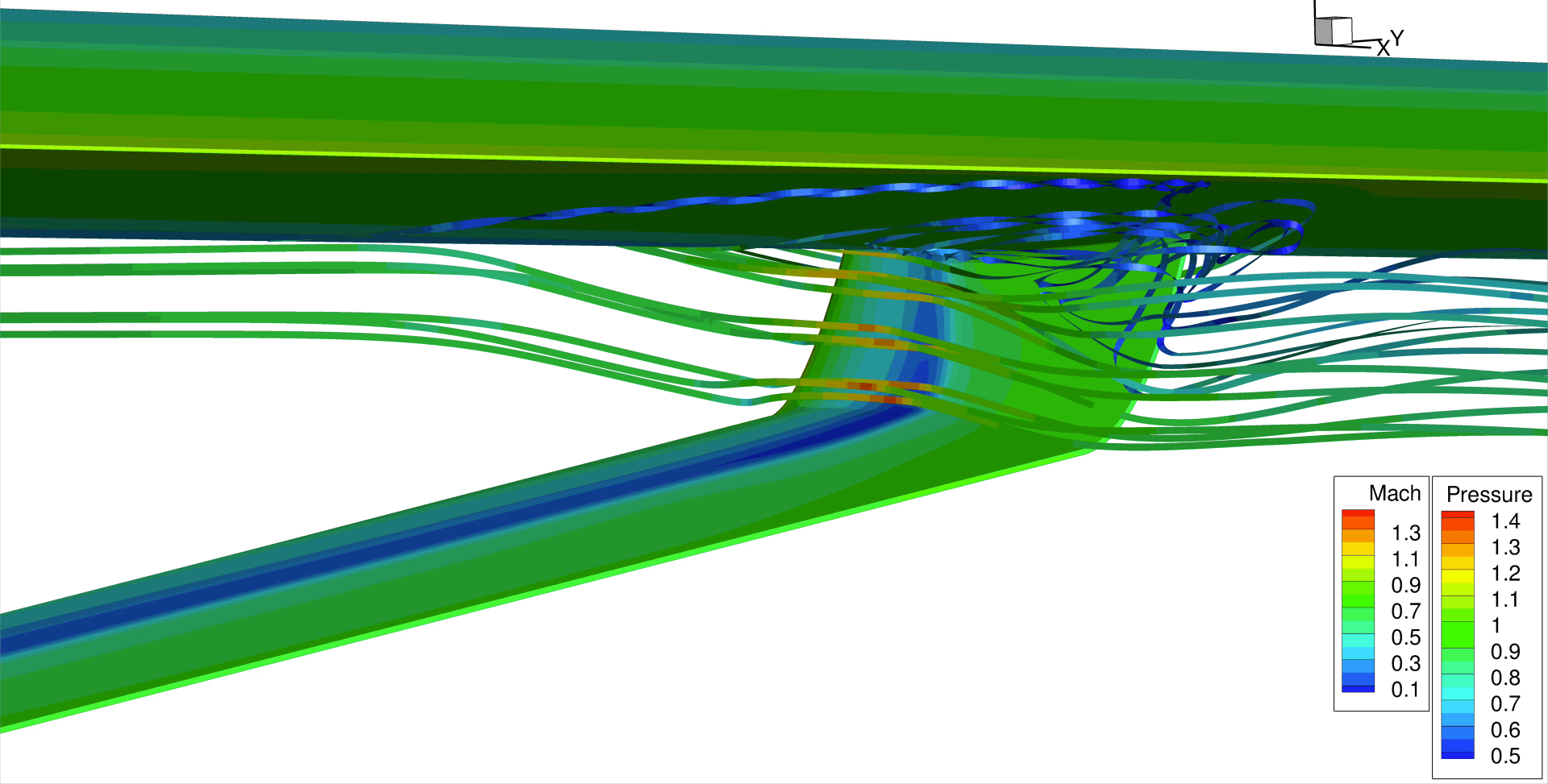
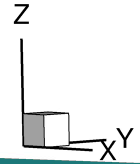


Pressure is shown on the surface. Stream ribbons are colored by Mach number.

Optimization Case 2



Solution: 0

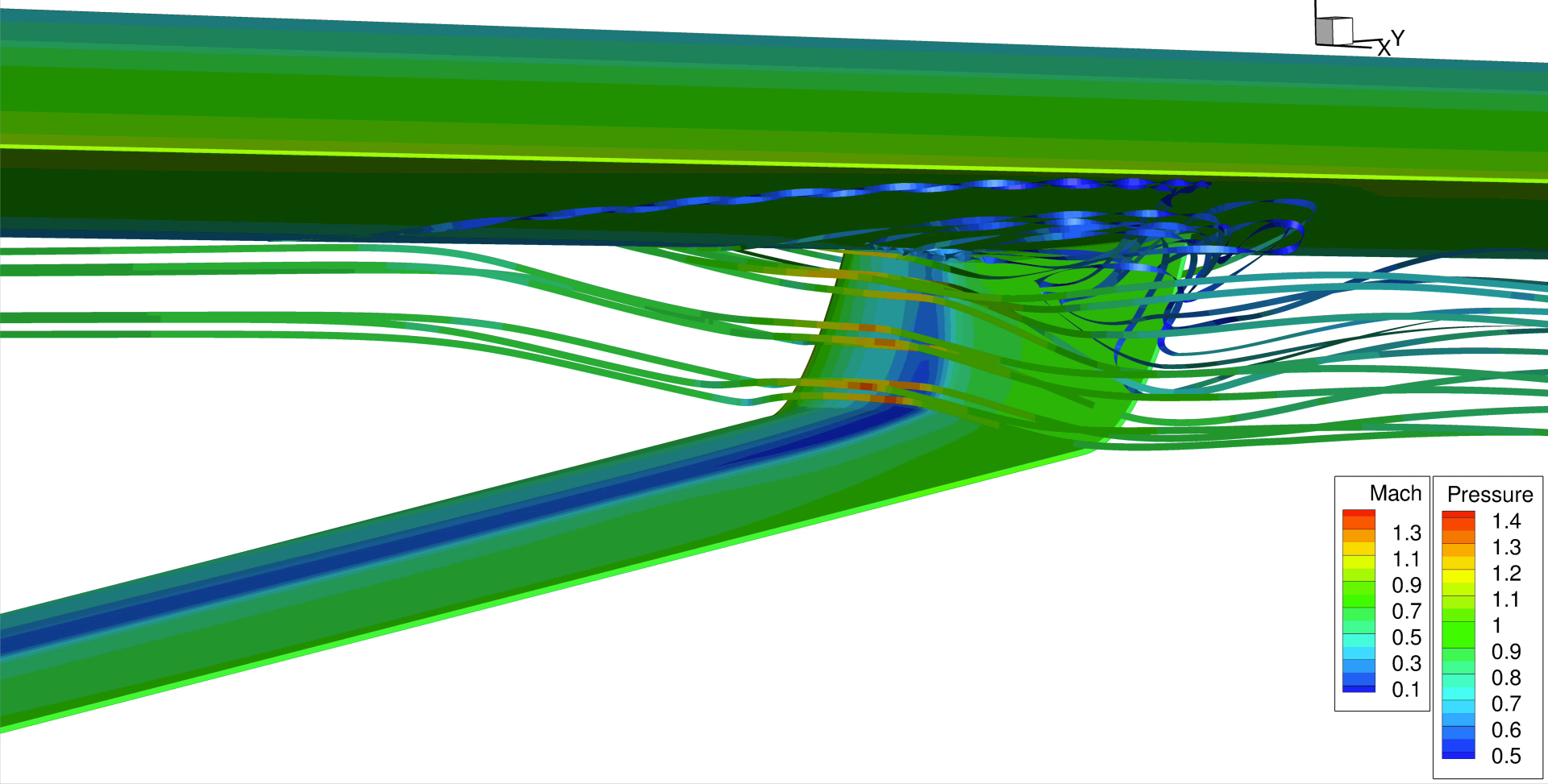


Pressure is shown on the surface. Stream ribbons are colored by Mach number.

Optimization Case 3

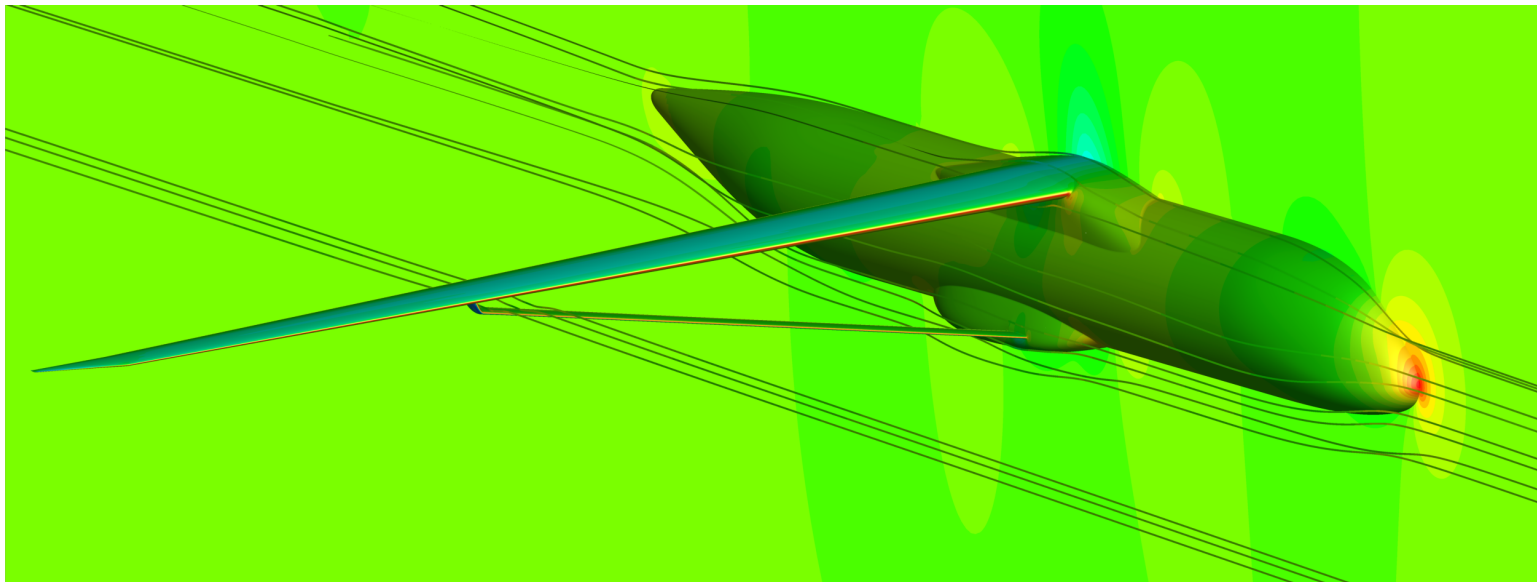


Solution: 0



Pressure is shown on the surface. Stream ribbons are colored by Mach number.

- Successfully redesigned truss-junction intersection
- Fast optimization turn-around times of under 2 hours
- 13.5 drag count reduction for Case 1
- 33.5 drag count reduction for Case 3
- In transonic flow, truss may have negative lift
- No cost associated with flow control device other than initial development costs
- Future work should include aero-structural trade-offs





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