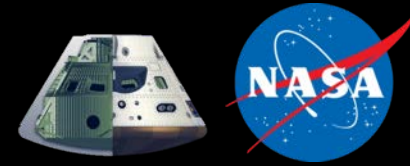


CHARACTERIZATION OF THERMAL PROTECTION SYSTEMS

An Analysis of Optical & Thermal Properties

Brian Cole, Clemson University (AMA)
Jay Feldman, NASA ARC (MEDLI2)
Matthew Gasch, NASA ARC (PICA-D & HEEET)

NASA ARC Annual Research Symposium
Moffett Field, CA August 8th, 2019



Background

- Background & Objectives

Materials Introduction

- Various Ablative Thermal Protection Systems (TPS)

Optical Properties

- Infrared, Ultra-Violet, & Visible Radiation Spectra
- Emissivity & Absorptivity Calculations

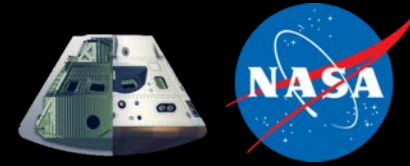
Thermal Properties

- Specific Heat & Thermal Conductivity

Summary

- Research Accomplishments & Contribution Towards Mars 2020

Background & Objectives



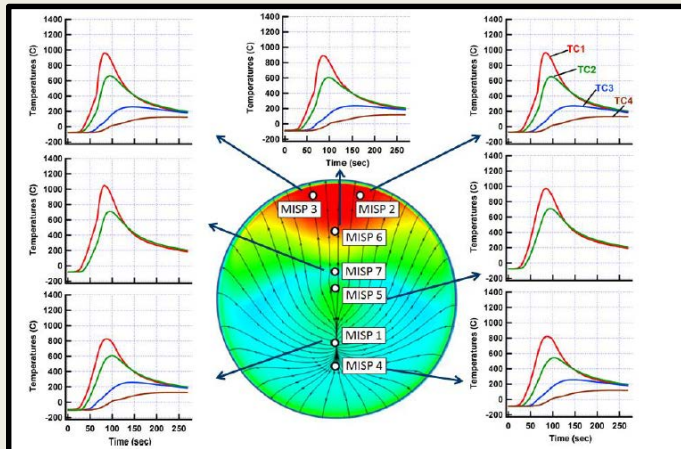
We Aim To Measure Physical Properties:

MEDLI Example

Improve Thermal Response Models



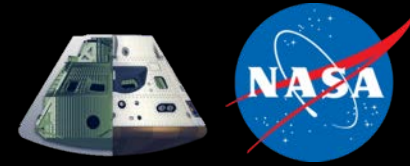
Reconstruct Flight Environments



Design TPS For Future Missions

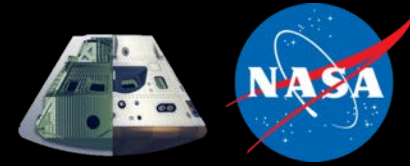


Background & Objectives



- **Objective:** Characterize Properties of TPS Materials
 - Optical properties
 - Thermal properties
- This allows us to develop Thermal Response Models for TPS
- The models enable design of TPS for Flight Missions and analysis of flight data to understand Aerothermal Environments experienced on the mission
- Comparing pre-flight predictions with actual flight data can allow us to reduce TPS margins and improve designs
 - **MEDLI** and **MEDLI2** are examples of this to be discussed

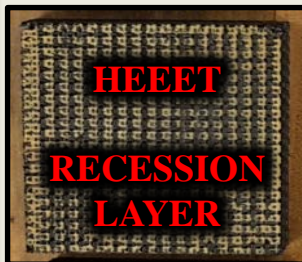
Materials Studied



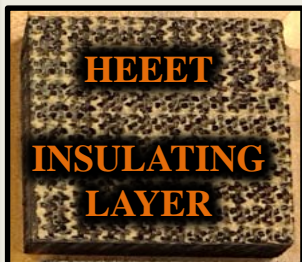
TPS Materials



Low Density Ablative
Sustainable Material
Made in USA



High Density
3D Woven Material
Opens Doors For
Venus & Saturn



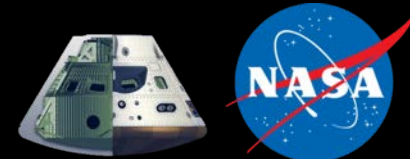
Lower Density
3D Woven Material
Lower Thermal Conductivity



Thermal Control Coatings

AZ 93	\$440.00 per pint Standard White Inorganic Coating
AZ 2100	\$1800.00 per pint Electrically Conductive
AZ W	\$7200.00 per pint Very Low Solar Absorbance

Optical Properties Overview

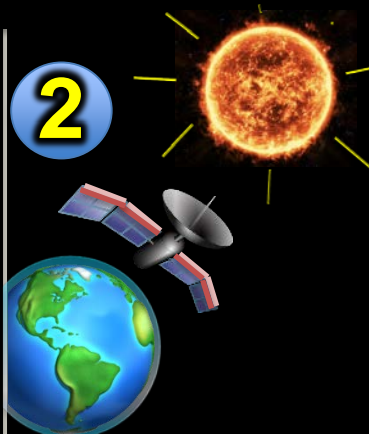


1

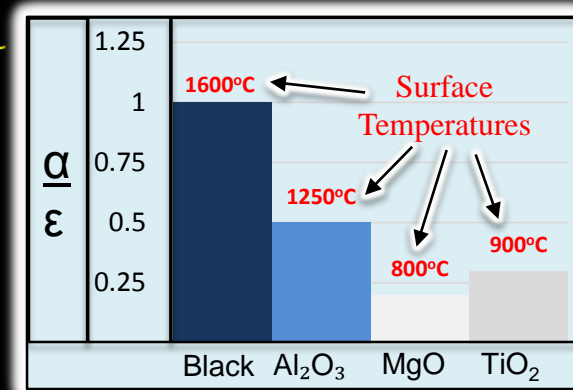


On Entry, Radiative Emission Is a Primary Cooling Method for TPS

2



On Orbit, Re-Emitting Solar Rays Reduces The Equilibrium Surface Temperature



FTIR (Fourier Transform Infrared Spectroscopy)
UV-Vis (Ultra-Violet & Visible Light Spectroscopy)



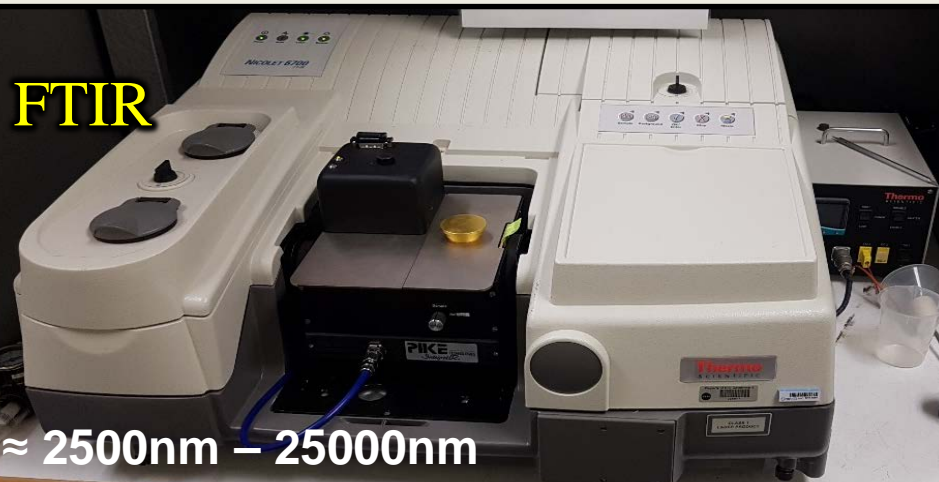
Calculate
Emissivity & Absorptivity

UV-VIS



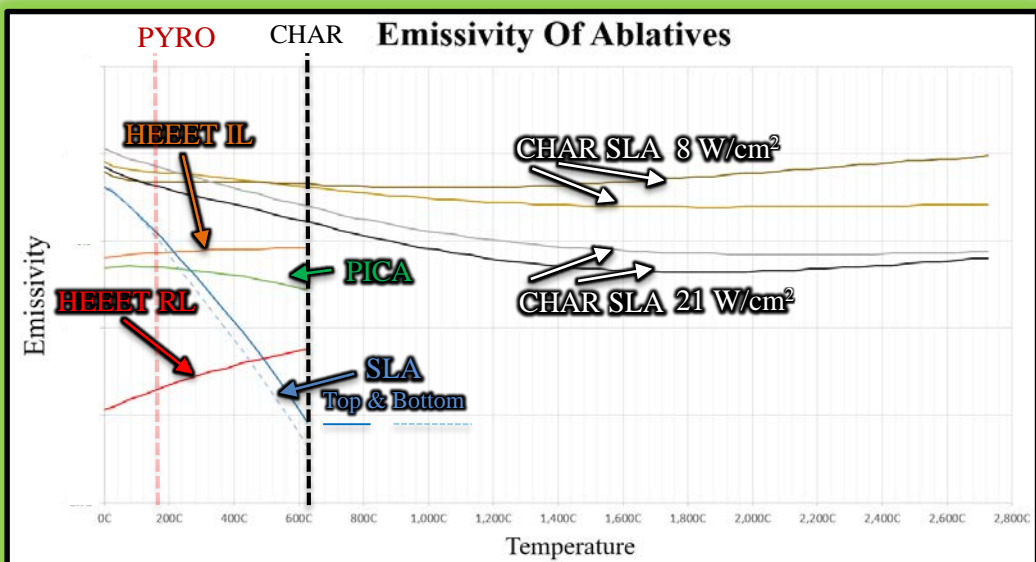
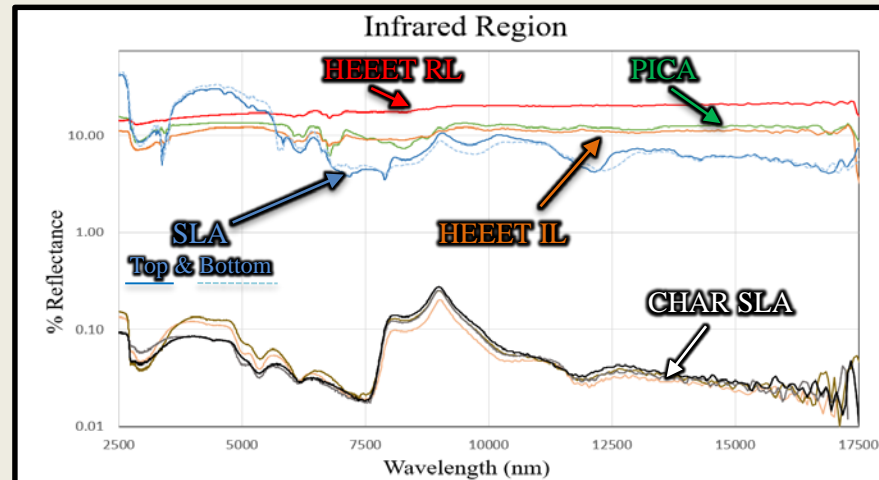
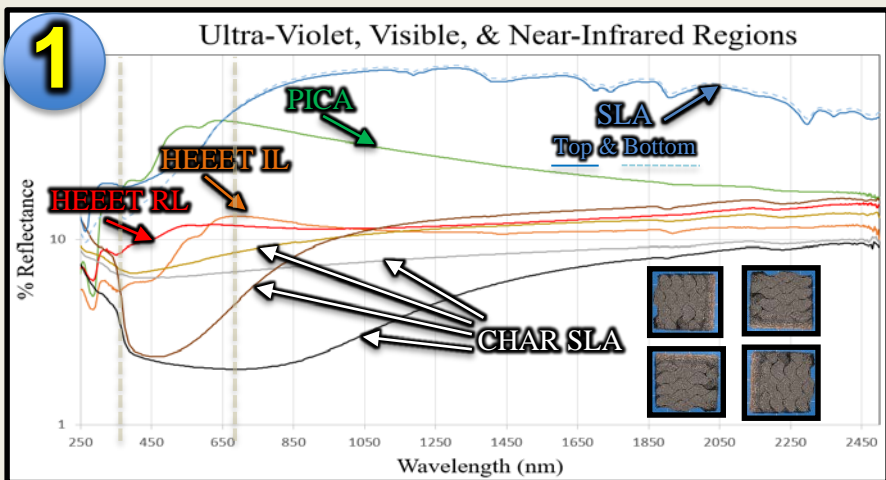
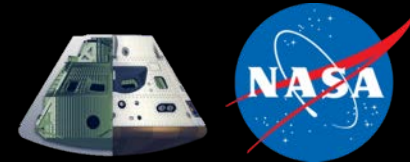
≈ 250nm – 2500nm

FTIR



≈ 2500nm – 25000nm

SLA Optical Properties



UV & VISIBLE REGIONS

- Char Consistent With Expectations (Absorbs Visible Light)

INFRARED REGION

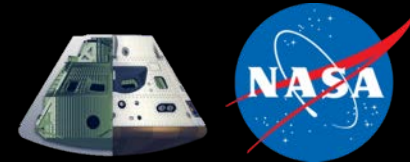
- Evidence of OH & CO Chemistry

EMISSIVITY (0°C -> 2700°C)

NOTE: SLA Fully Chars at 600°C

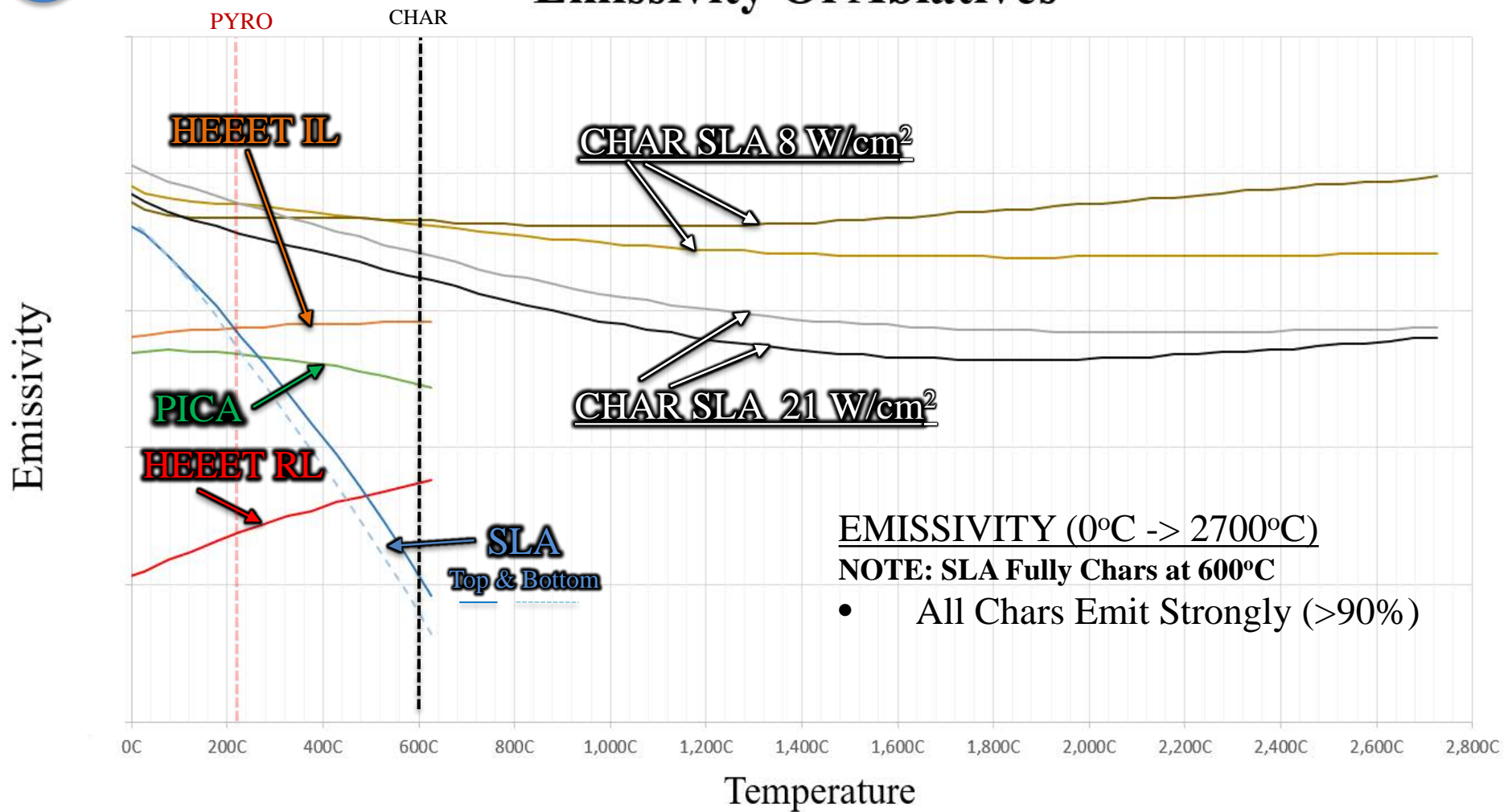
- All Chars Emit Strongly (>90%)

SLA Emissivity

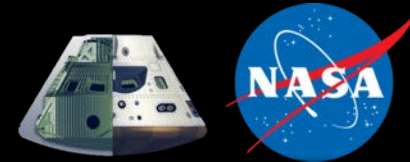


1

Emissivity Of Ablatives

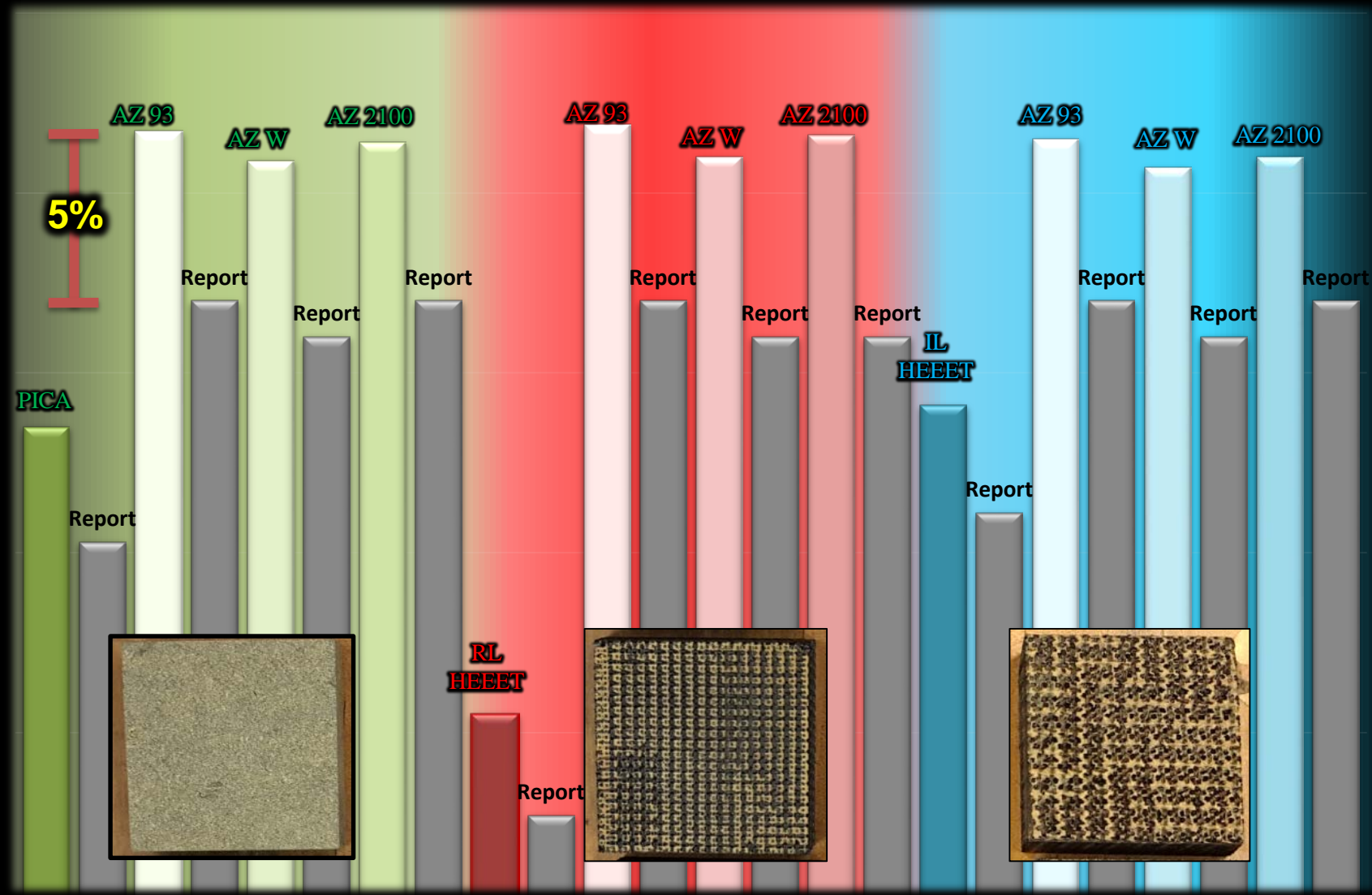


Thermal Control Coating Emissivity

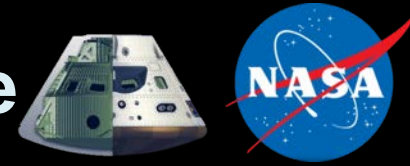


2

Emissivity at Room Temperature

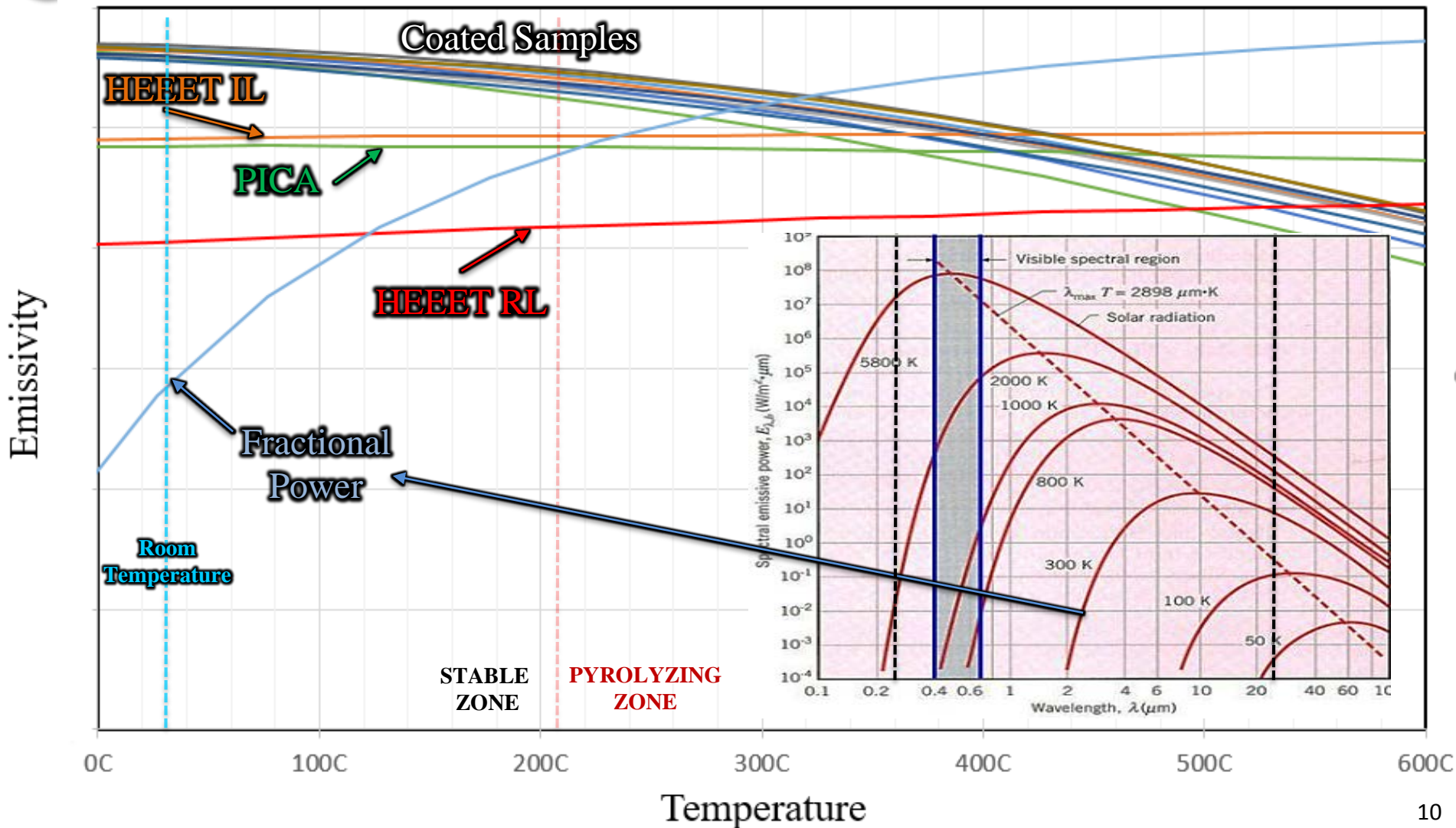


Emissivity as a Function of Temperature

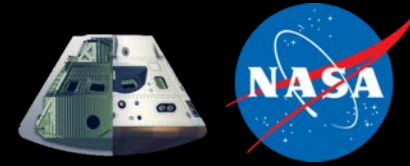


2

The Effect of Various White Coatings On The Emissivity



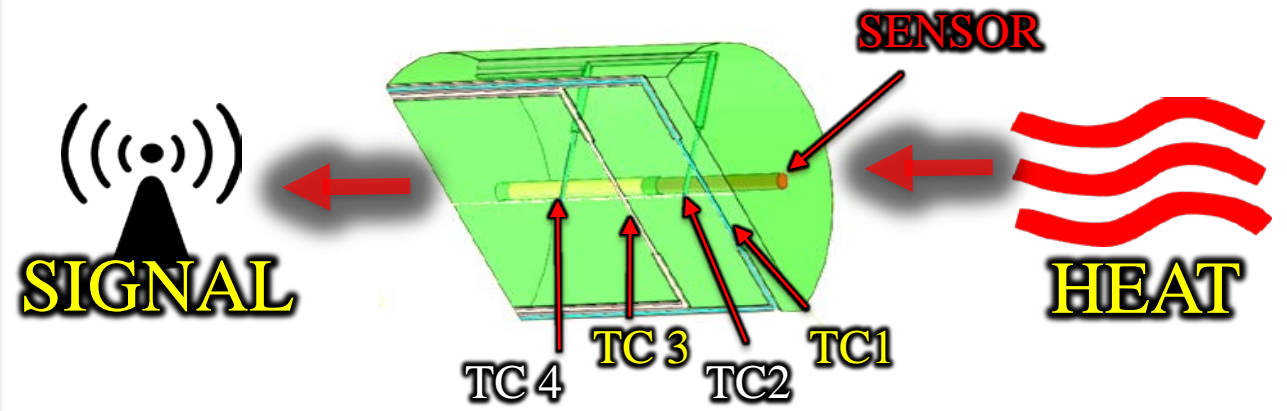
Thermal Properties Overview



- Mars Science Laboratory (MSL) launched in Nov **2011** & landed Curiosity Aug **2012**

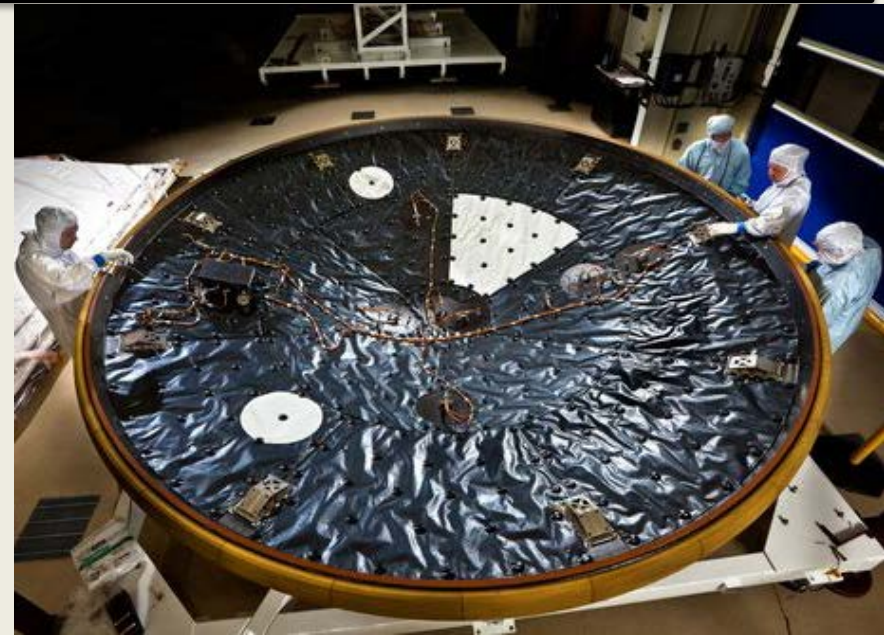
cp (Heat Capacity)
&
λ (Thermal Conductivity)

Allows Us To Infer
The In-Depth
Thermal Response

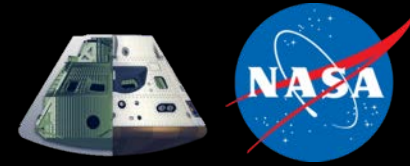


Example: Original MEDLI

- Improved Engineered Models for Future Missions
- Predicted T & P Response of TPS
- Improved Margins Allowing an Increased Payload



Solid State Heat Flow Meter Fox 50



Instrument Specifications

- Sample Size [2"-2.5" Diameter]
- Range [-10°C – 185°C]
- Accuracy [± 4%]
- Reproducibility [± 2%]

Methodology

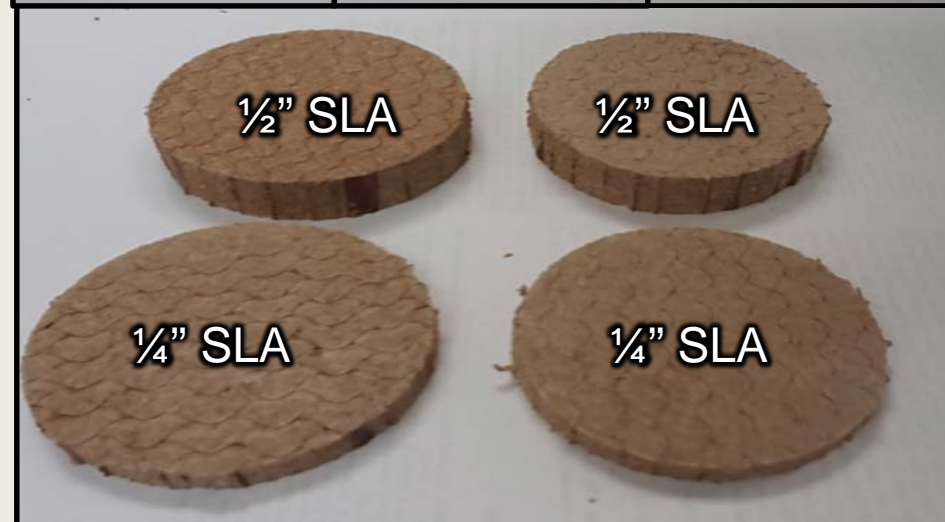
1. Obtain Contact Resistance of Rubber Matt
– Via two dx exp. with Perspex Standard
2. Measure λ of Standards & Samples
3. Correct λ by Rubber Matt Subtraction

Rubber Matt Subtraction Formula

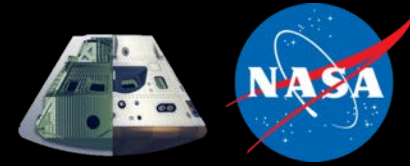
Assumptions

- 1) [$\lambda_T - \lambda_R$ is Negligible]
- 2) [$\lambda_R \cong \lambda_S$] \rightarrow [$\frac{\lambda_S}{\lambda_R} \cong 1$]
- 3) [$T_t \cong S_t - R_t$]

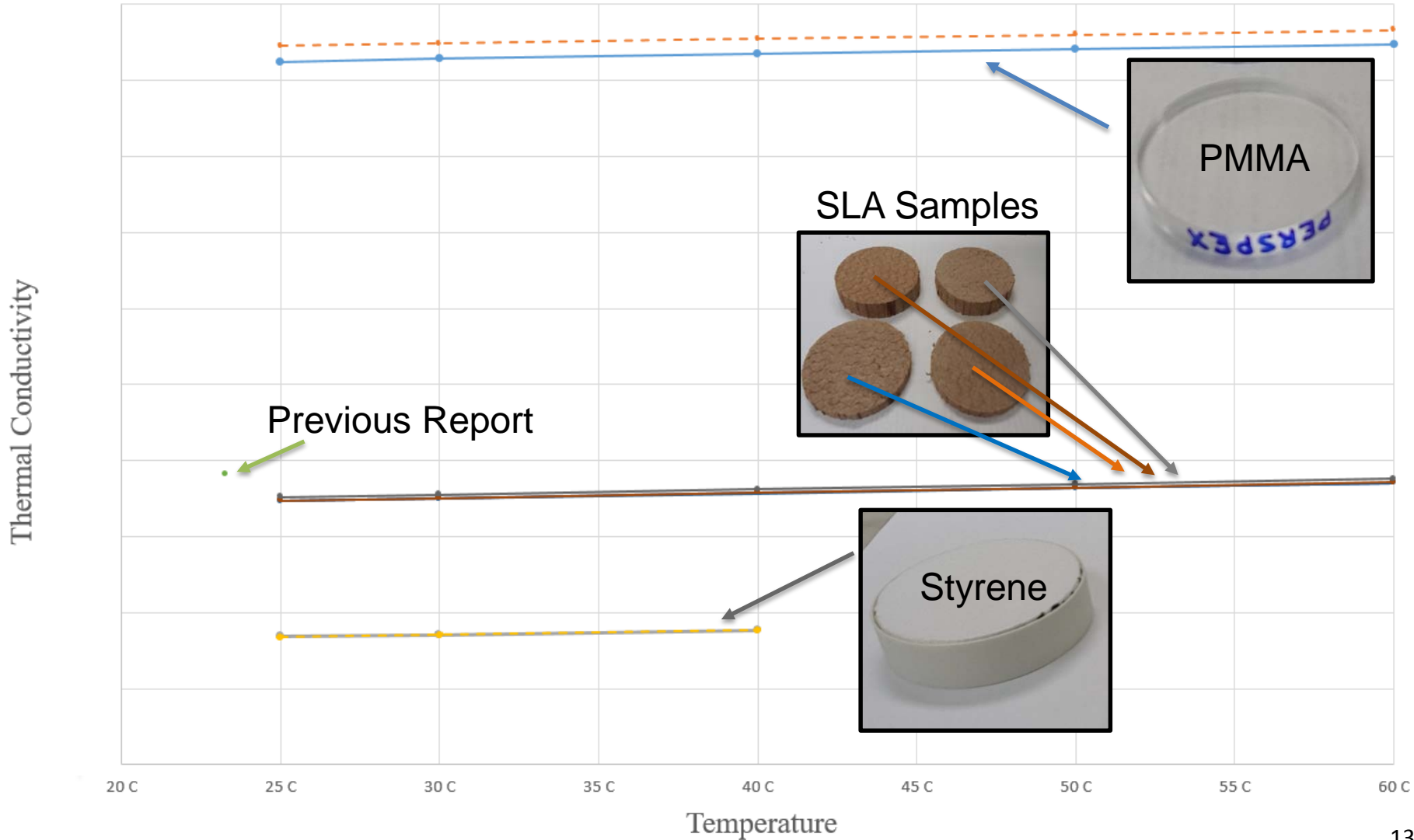
$$\frac{(T)_t - R_t}{\frac{(T)_t}{\lambda_T} - \frac{R_t}{\lambda_R}} = \lambda_S$$



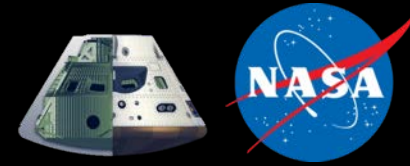
Thermal Conductivity of SLA



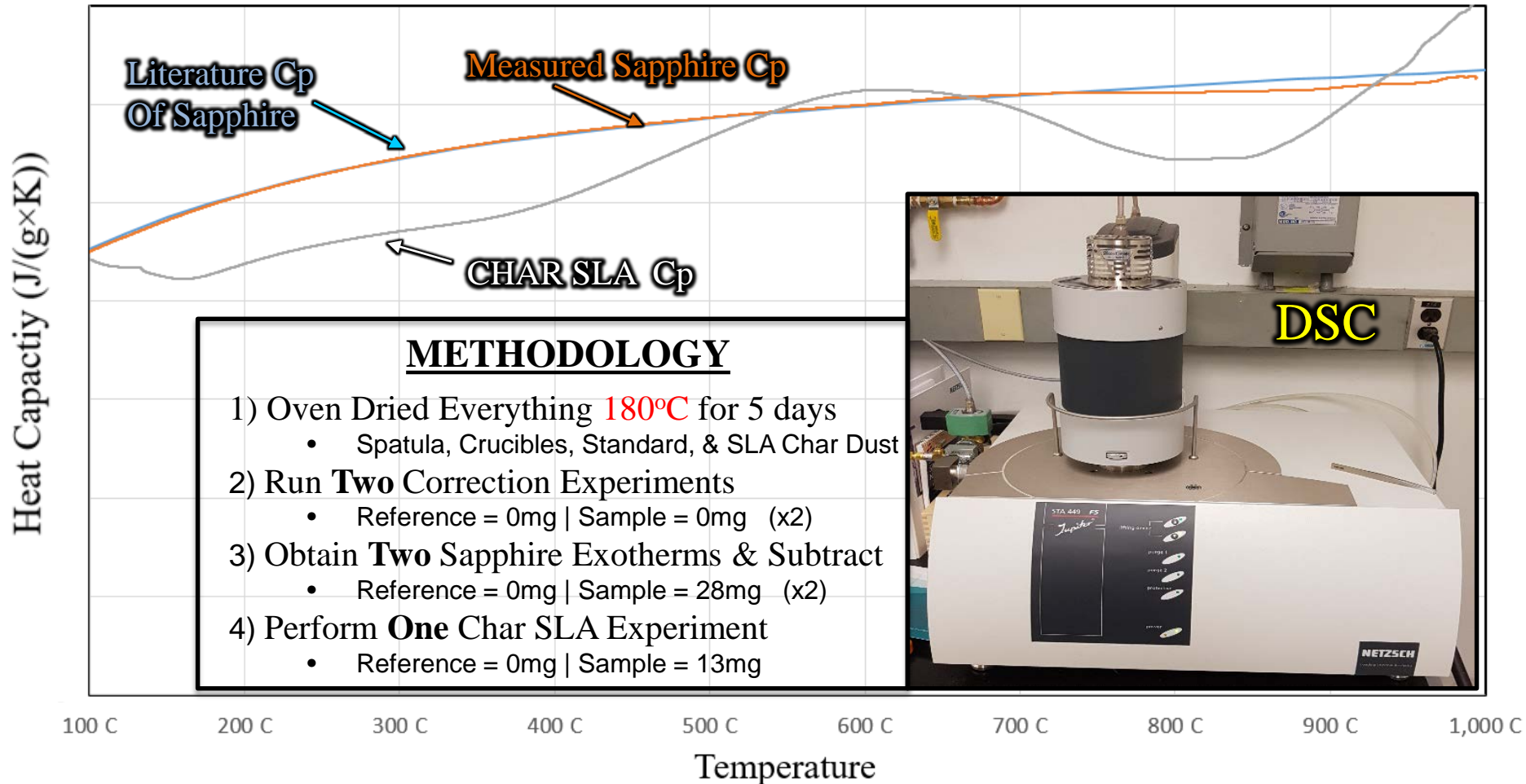
Thermal Conductivity of SLA



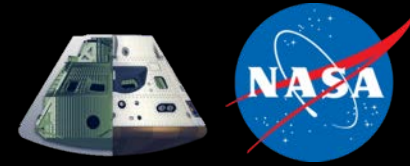
Heat Capacity by DSC



Specific Heat of SLA CHAR vs. Sapphire Standard

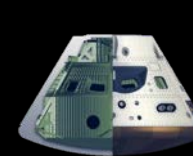


Summary



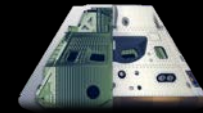
- Reviewed Various Ablative Materials
 - Purpose & Utility In NASA Missions
- Contributed Values For MEDLI2 Thermal Response Models and PICA-D and HEEET thermal response models
 - Optical Properties (Emissivity & Absorptivity)
 - Thermal Properties (Heat Capacity & Thermal Conductivity)
- Some of This Work is Not Complete and Highlights Questions To Investigate in The Future

Acknowledgments



Special Thanks To:

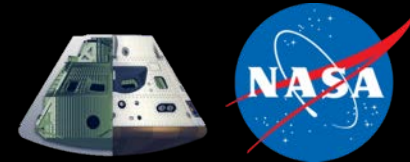
- Jay Feldman
- Greg Gonzales
- Matthew Gasch
- Susan White
- Mairead Stackpoole
- NASA AMES RESEARCH CENTER
- Tane Boghozian



Questions?



Solid State Heat Flow Meter Fox 50



Instrument Specifications

- Sample Size [2"-2.5" Diameter]
- Range [0°C – 190°C]
- Accuracy [± 4%]
- Reproducibility [± 2%]



$$\frac{\left(\frac{(T)_t - R_t}{\lambda_T} - \frac{R_t}{\lambda_R} \right)}{\left(\frac{(T)_t - R_t}{\lambda_S} - \frac{R_t}{\lambda_S} \right)} = \frac{\left(\frac{S_t - R_t}{\lambda_S} - \frac{R_t}{\lambda_S} \right)}{\left(\frac{S_t + R_t}{\lambda_S} - \frac{R_t}{\lambda_S} \right)} = \frac{\left(\frac{S_t}{\lambda_S} \right)}{\left(\frac{S_t}{\lambda_S} \right)} = \frac{1}{1} = \lambda_S$$

1. Obtain
2. Measure
3. Correct

Rubber Matt Subtraction Formula

- 1) $[\lambda_T - \lambda_R \text{ is Negligible}]$
- 2) $[\lambda_R \cong \lambda_S] \rightarrow \left[\frac{\lambda_S}{\lambda_R} \cong 1 \right]$
- 3) $[T_t \cong S_t - R_t]$

$$\frac{(T)_t - R_t}{\lambda_T} - \frac{R_t}{\lambda_R} = \lambda_S$$

