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Multi-Node Modeling of Cryogenic Tank Pressurization System using Generalized Fluid System Simulation Program

Alak Bandyopadhyay

*Department of Electrical Engineering and Computer Science, Alabama
A & M University, Normal, AL 35762*

&

Alok K. Majumdar, Andre C. Leclair and Juan G. Valenzuela

*Propulsion System Department, NASA Marshall Space Center,
Huntsville, AL 35812*



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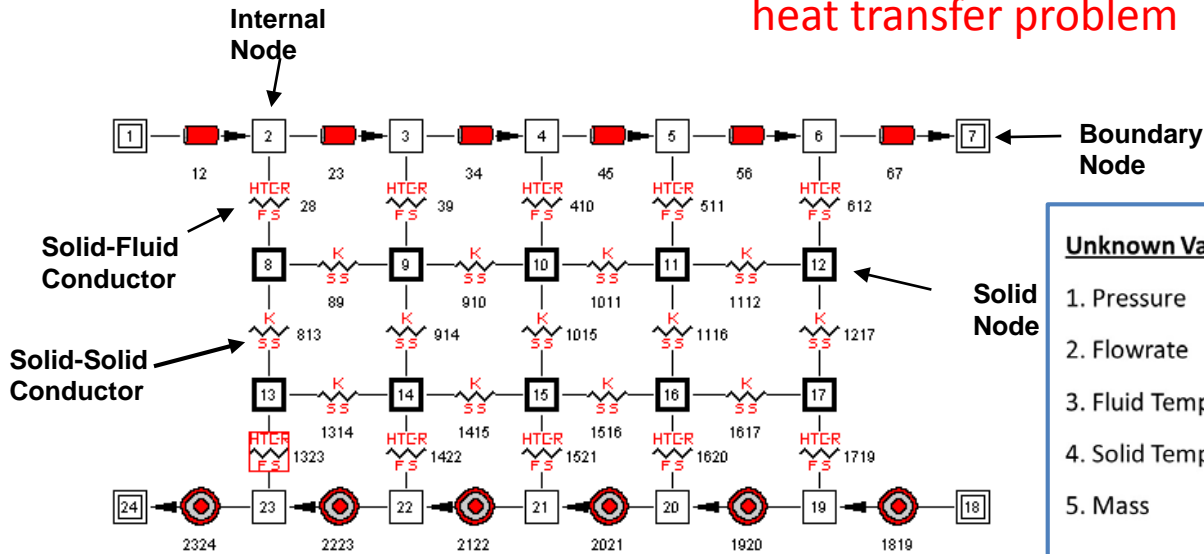
Purpose & Objective

- Historically, Cryogenic Tank Pressurization is either modeled by a single node using Fluid System Code (GFSSP & ROCETS) or by high fidelity Navier-Stokes code (FLUENT or CFX).
- Use of multi-node modeling using Fluid System code has not been explored. The main purpose of this paper is to describe a multi-node system modeling of cryogenic tank pressurization in GFSSP
- In recent years, a test program has been conducted at NASA/MSFC to measure boil-off of cryogenic liquid propellant in a flight tank to support United Launch Alliance's IVF (Inter Vehicular Fluid) program where boil-off propellants are used to pressurize the tank
- The model results have been compared with test data

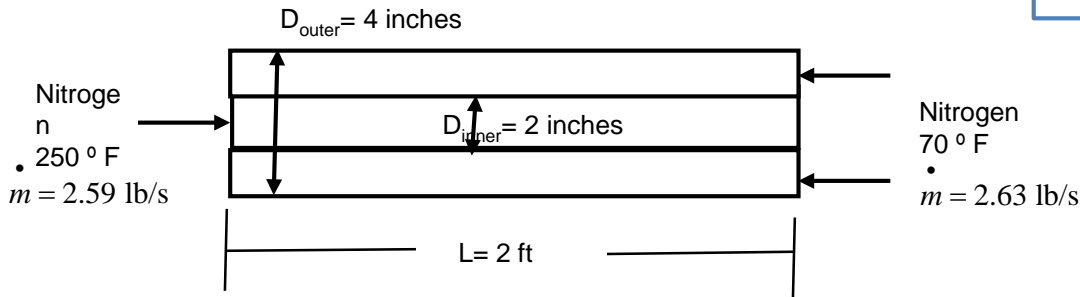


GFSSP(Generalized Fluid System Simulation Program)

Example of Heat Exchanger Model to define Network elements of a conjugate heat transfer problem



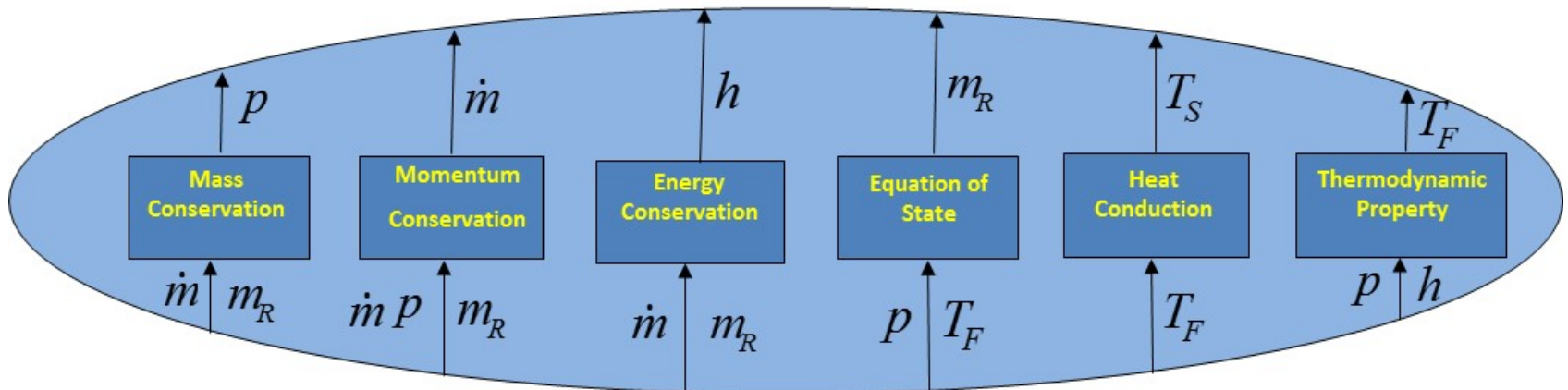
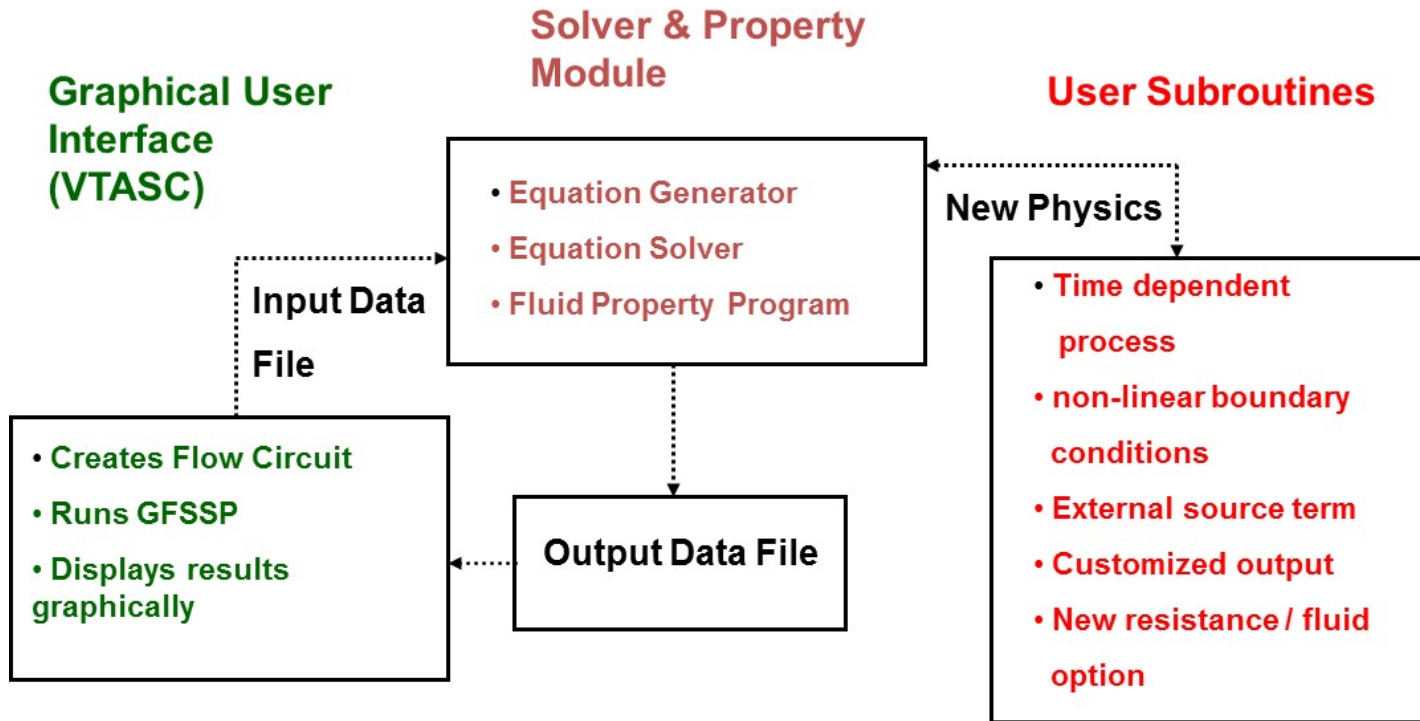
<u>Unknown Variables</u>	<u>Governing Equations to Solve</u>
1. Pressure	1. Mass Conservation Equation
2. Flowrate	2. Momentum Conservation Equation
3. Fluid Temperature	3. Energy Conservation Equation of Fluid
4. Solid Temperature	4. Energy Conservation Equation of Solid
5. Mass	5. Thermodynamic Equation of State



Thermodynamic and Thermo-physical properties are obtained from built-in GASP and GASPAK



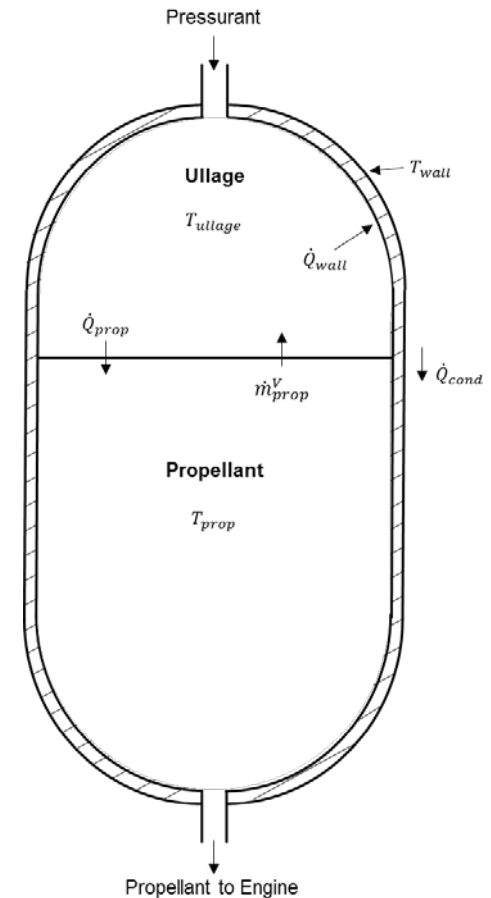
Program Structure & Numerical Scheme





Review of Tank Pressurization Model

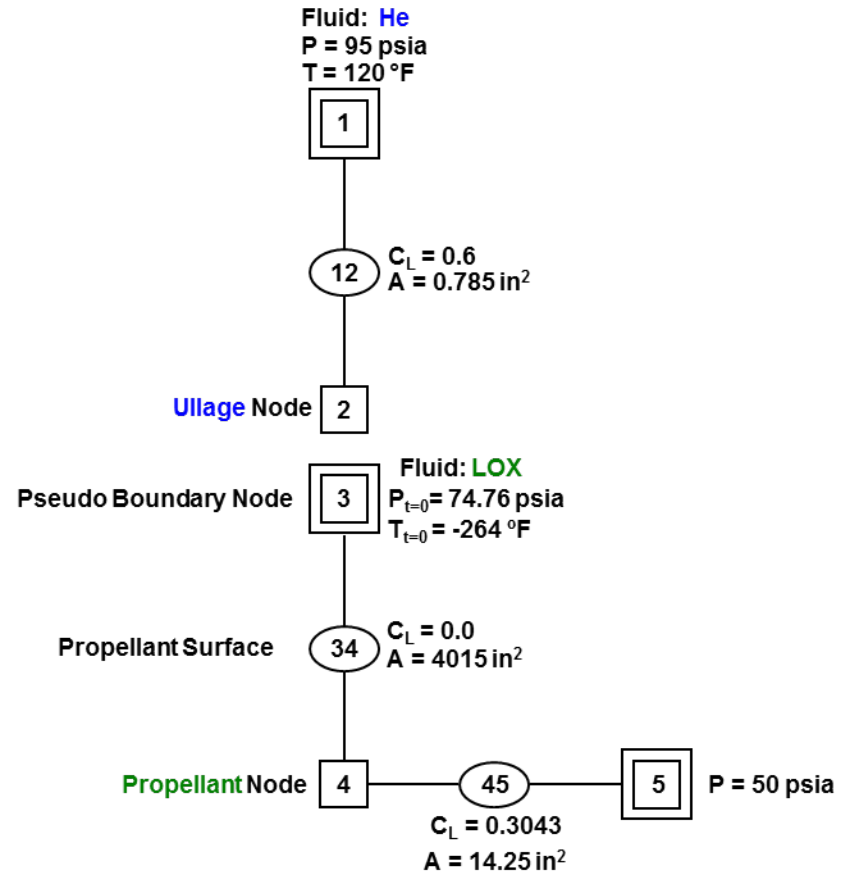
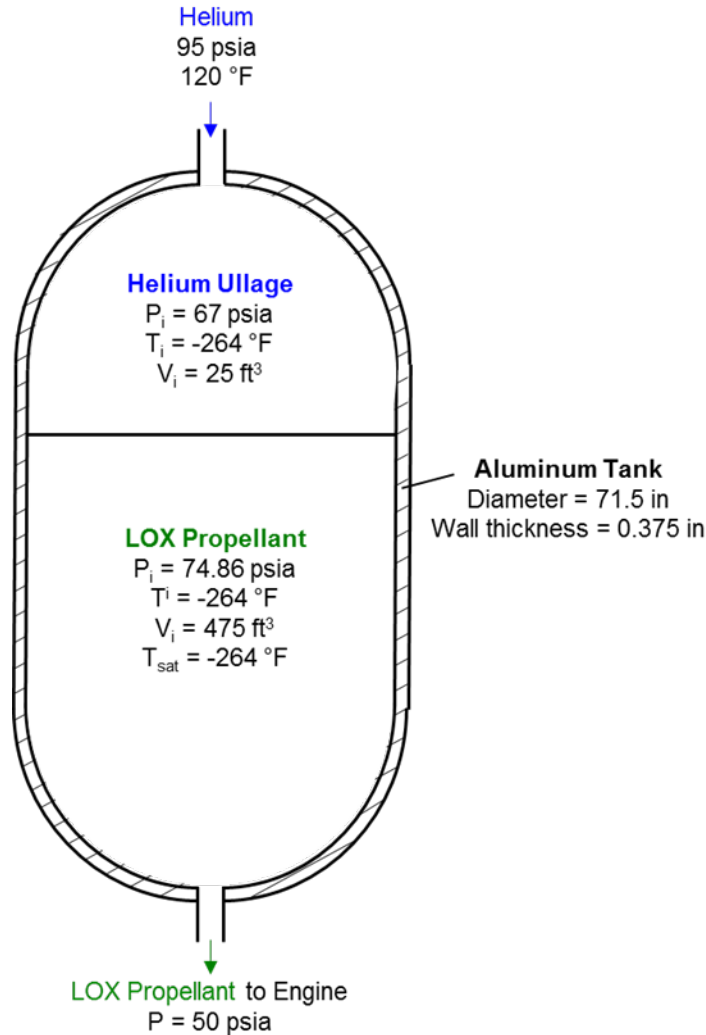
- In Liquid Propulsion System, accurate modeling of Cryogenic Tank Pressurization is needed to
 - a) Ensure safe operation of the turbo-pump
 - b) Estimate amount of pressurant requirement
 - c) Estimate boil-off of Liquid Propellant
- Cryogenic Tank Pressurization model must account for
 - a) Heat Transfer between ullage and wall
 - b) Heat Transfer between ullage and liquid propellant
 - c) Evaporative mass transfer between liquid propellant and ullage





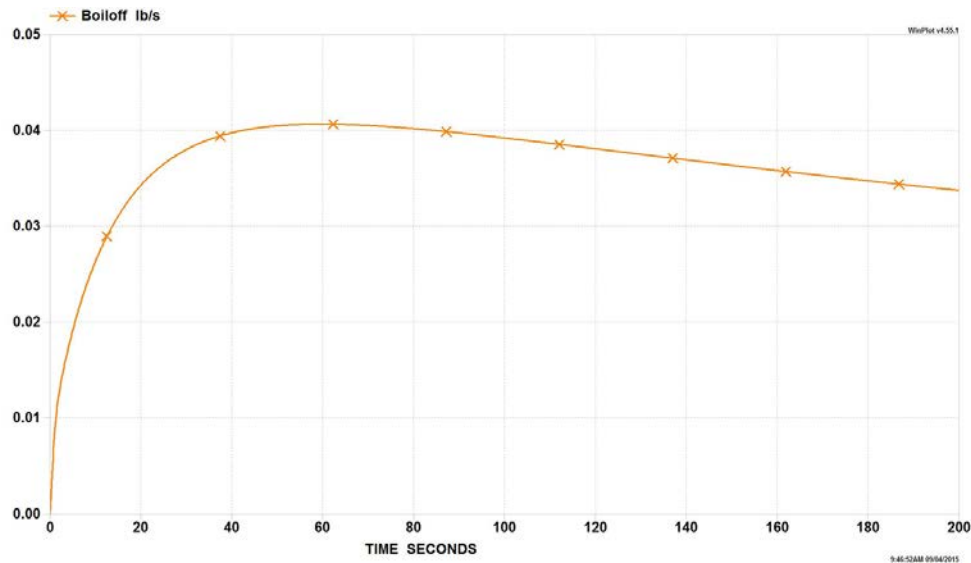
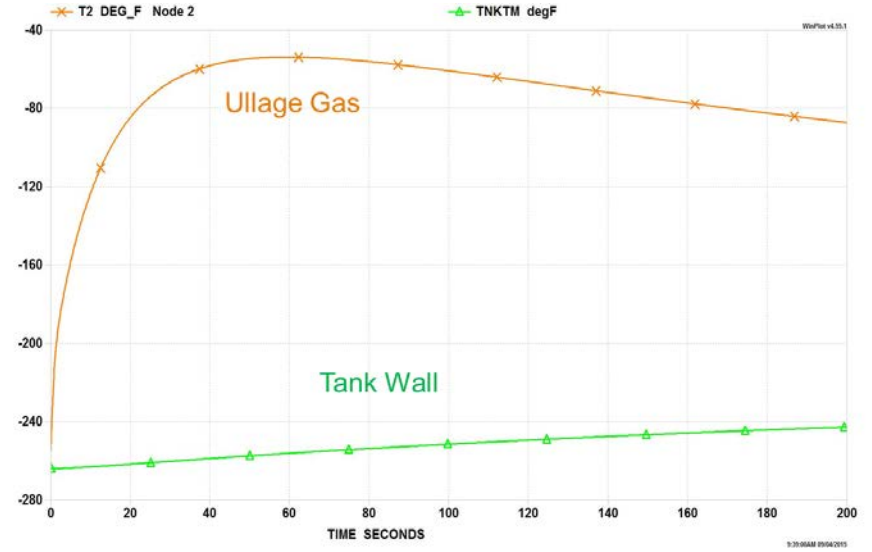
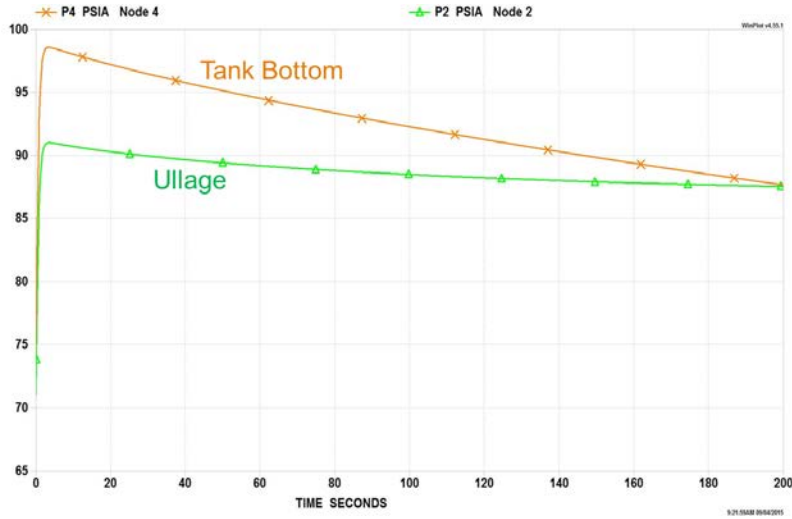
Review of Tank Pressurization Model

Zero Dimensional Model





Zero Dimensional Model Results





Zero Dimensional Model Validation

- Collapse Factor Correlation (Epstein)
 - Ratio of *actual* pressurant consumption to an *ideal* pressurant consumption which assumes **no** heat or mass transfer

$$\frac{w_p}{w_p^0} = \left\{ \left(\frac{T_0}{T_s} - 1 \right) [1 - \exp(-p_1 C^{p_2})] \times [1 - \exp(-p_3 S^{p_4})] + 1 \right\} \times \exp \left[-p_5 \left(\frac{1}{1+C} \right)^{p_6} \left(\frac{S}{1+S} \right)^{p_7} Q^{p_8} \right]$$

where:

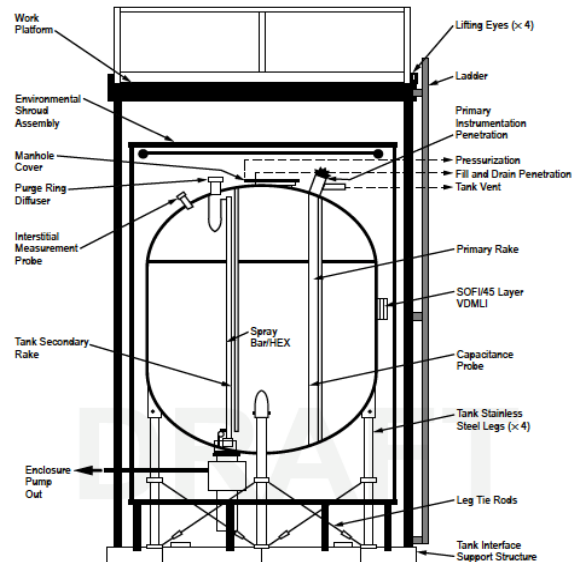
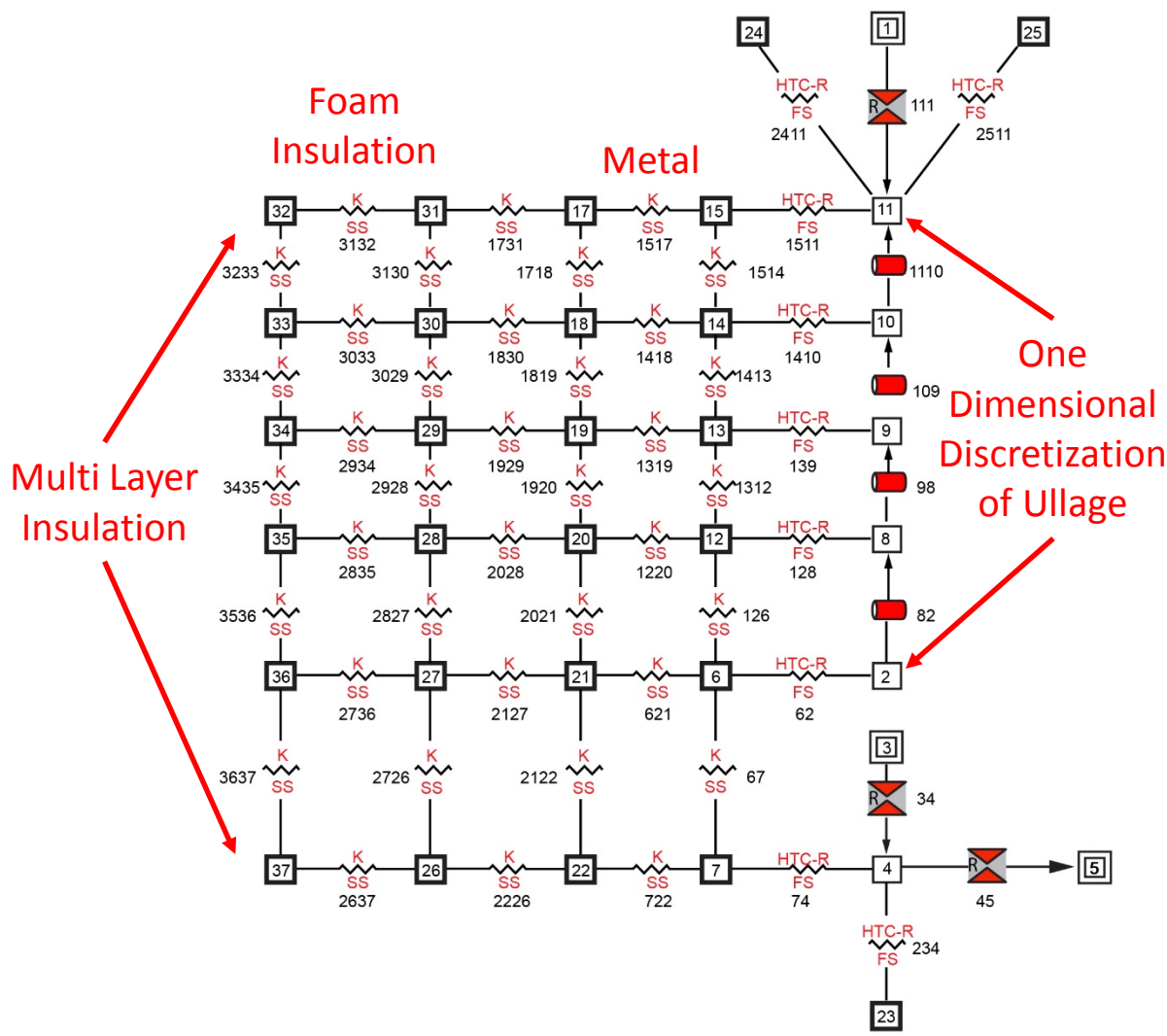
$$w_p^0 = \rho_G^0 \Delta V \quad C = \frac{(\rho c_p^0 t)_w T_s}{(\rho c_p)_G^0 D_{eq} T_0} \quad S = \frac{h_c \theta_T T_s}{(\rho c_p)_G^0 D_{eq} T_0} \quad Q = \frac{\dot{q} \theta_T}{(\rho c_p)_G^0 D_{eq} T_0}$$

- C ratio of wall to gas thermal capacitance
- $p_1 - p_8$ fitted constants (dependent on propellant)
- Q ratio of ambient heat input to effective thermal capacitance of gas
- S modified Stanton number
- T_0 pressurant inlet temperature
- T_s propellant saturation temperature at initial tank pressure

- Pressurization Model Validation
 - **GFSSP** Collapse Factor Prediction: **1.46**
 - Epstein Correlation Collapse Factor Prediction: **1.51**
 - **GFSSP** Prediction Discrepancy: **-3.3%**



One Dimensional Self-Pressurization Model of Cryogenic Tank

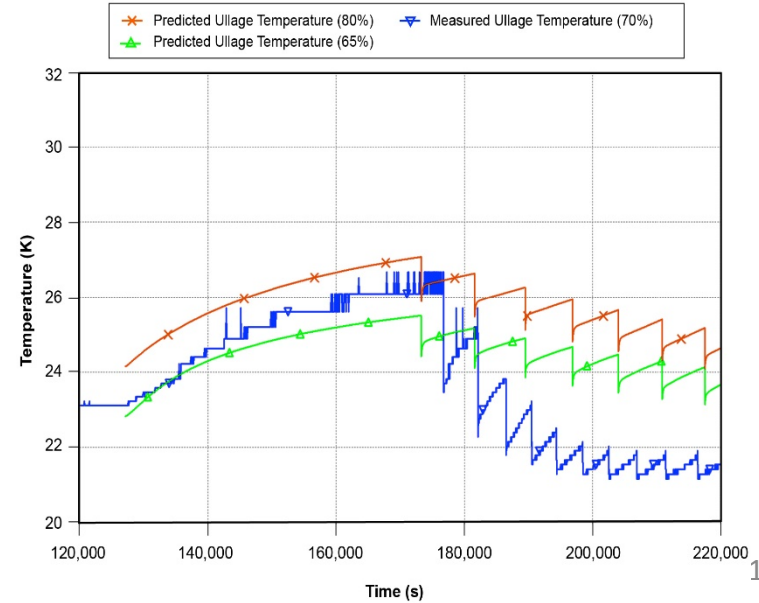
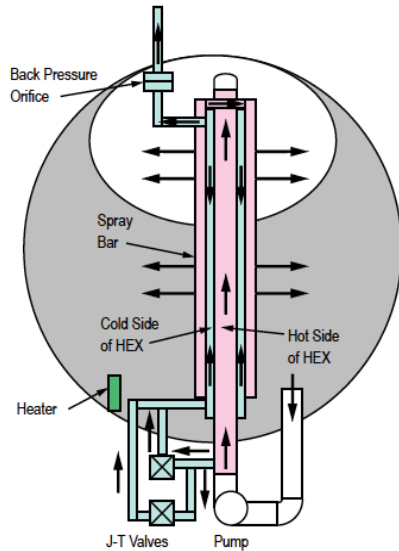
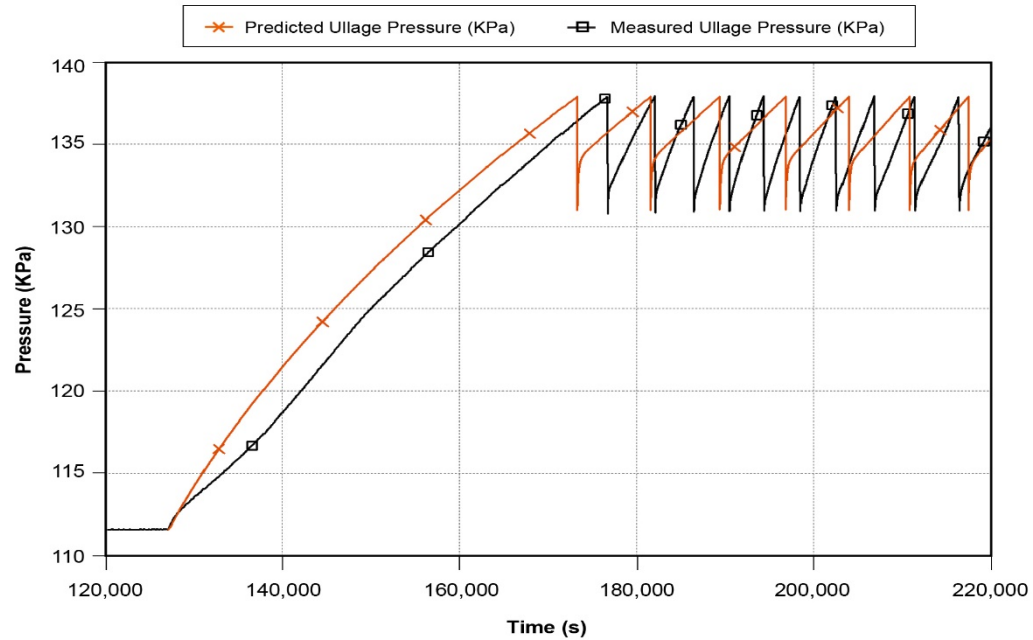


Multi-Purpose Hydrogen Tank



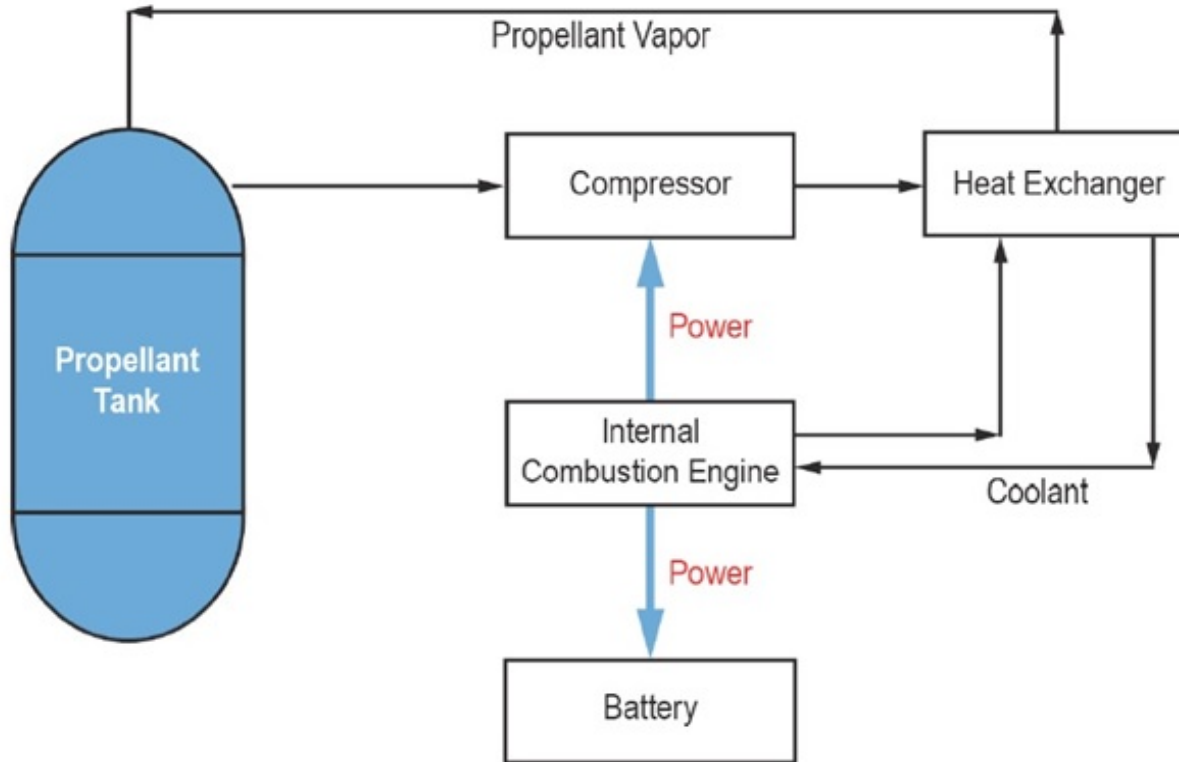


Results of Self-Pressurization Model





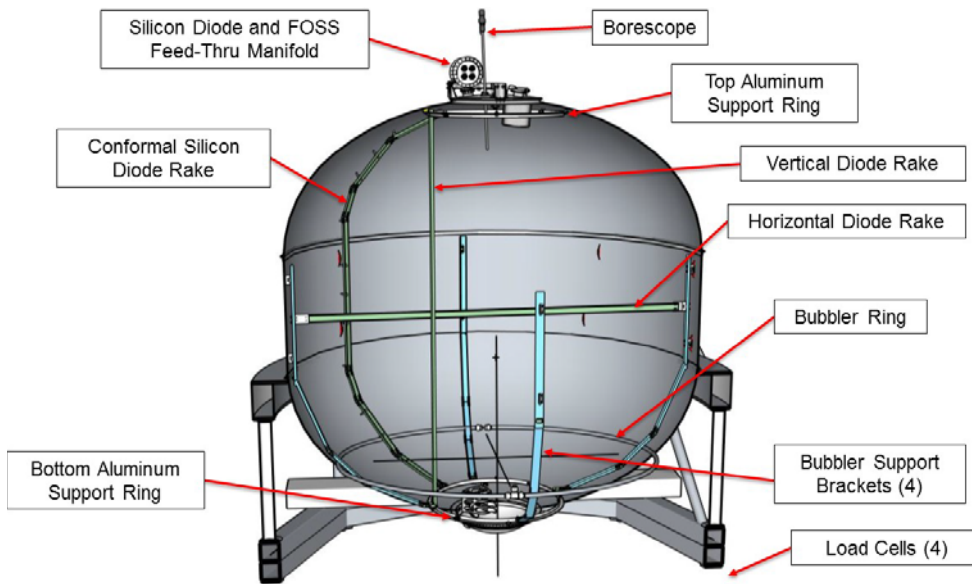
Integrated Vehicle Fluid System Overview





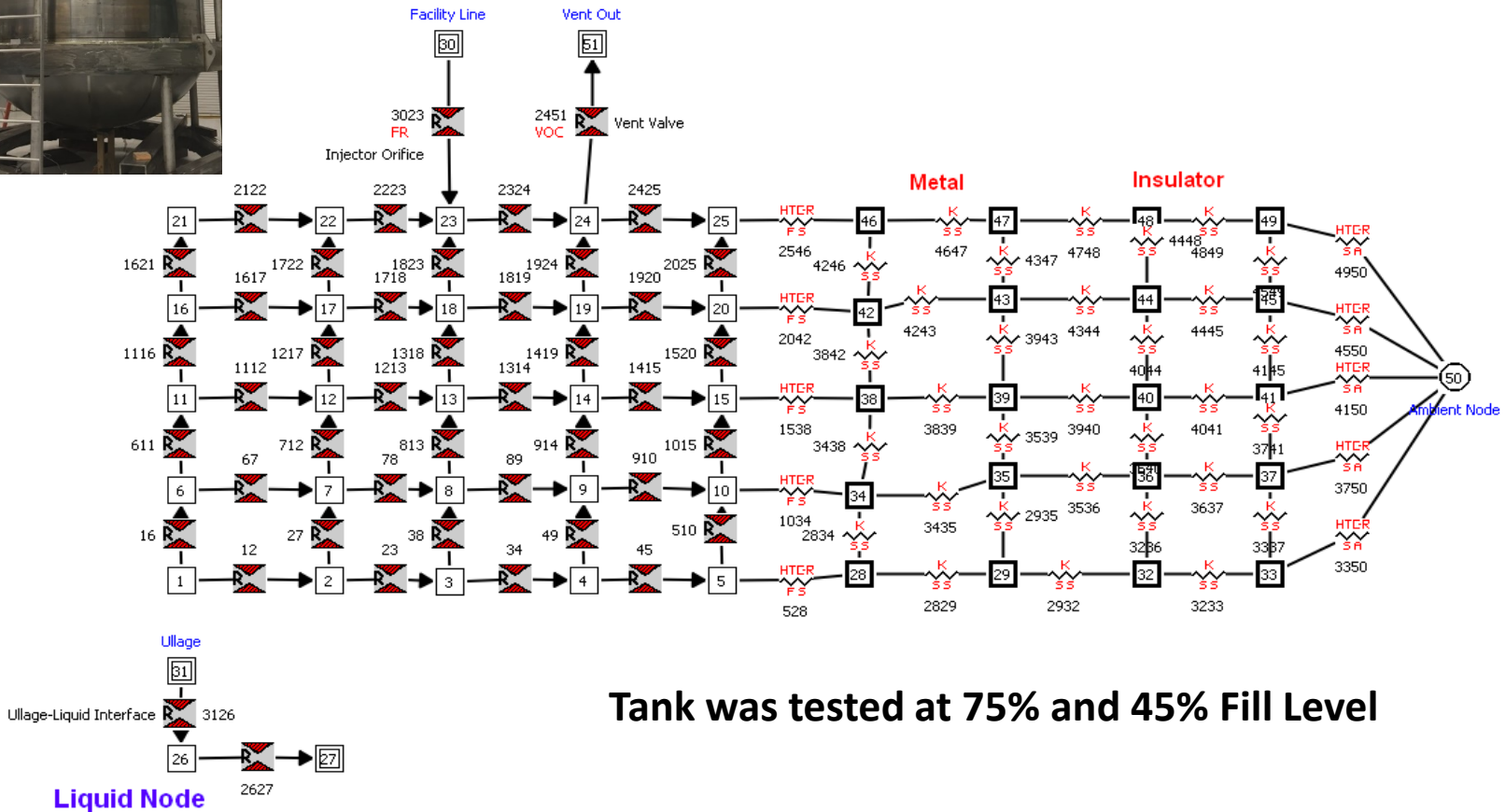
Test Program at MSFC

Flight Tank provided by ULA





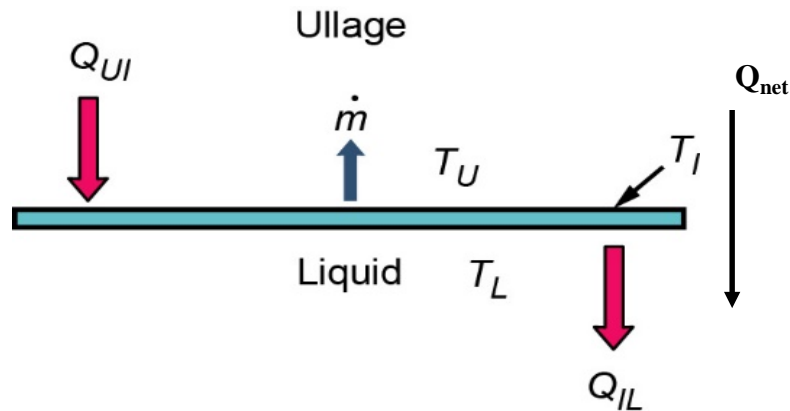
Two Dimensional Axisymmetric Model of Tank Pressurization



Working Fluid: Nitrogen, Tank Height \approx 10 ft, Tank Dia \approx 10 ft



Heat and Mass Transfer Model at Liquid-Ullage Interface



$$Q_{UI} = h_{UI}A(T_U - T_I)$$

$$Q_{IL} = h_{IL}A(T_I - T_L)$$

Evaporative Mass Transfer:

$$\dot{m} = \frac{Q_{UI} - Q_{IL}}{h_{fg}}$$

Heat Transfer Coefficients using Natural Convection

$$h_{UI} = K_H C \frac{k_f}{L_s} \text{Ra}^n = h_{IL},$$

$$C = 0.27, n = 0.25, K_H = 0.5$$

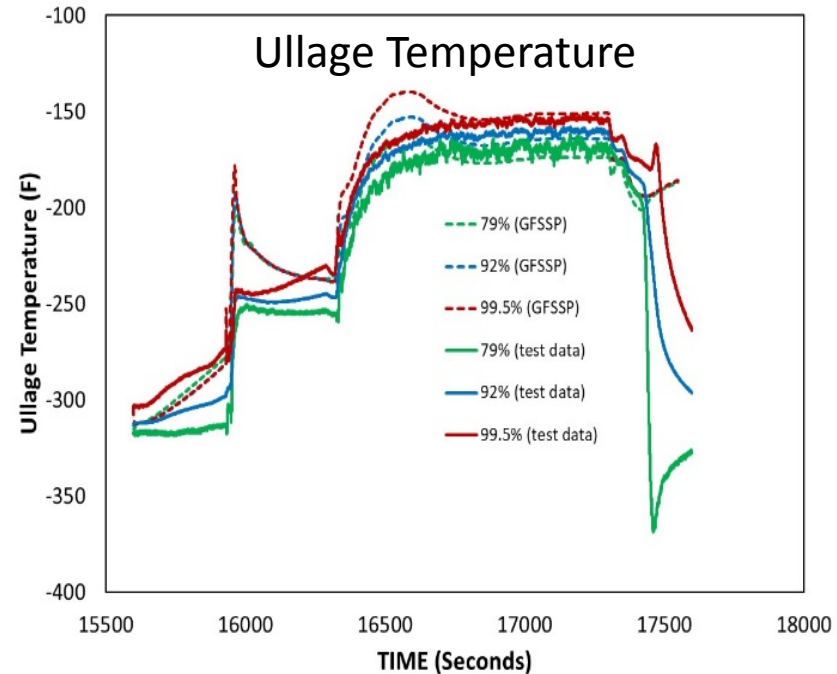
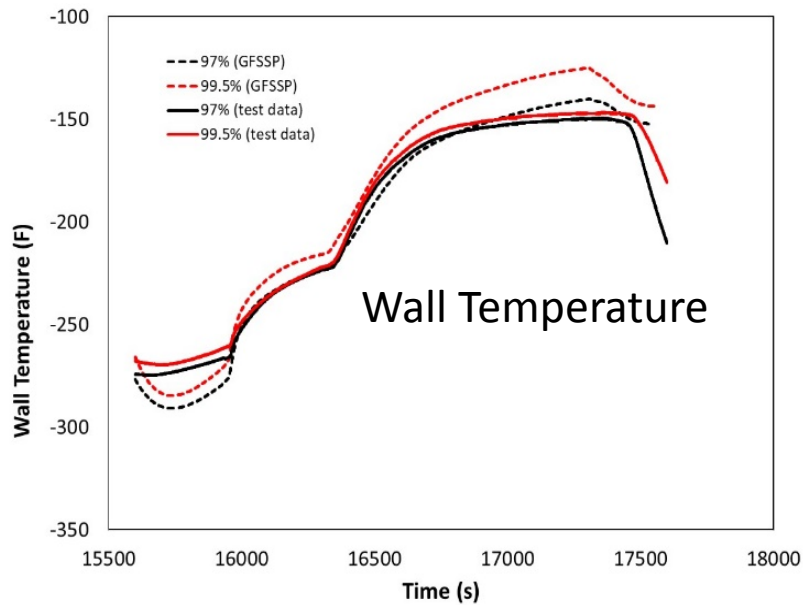
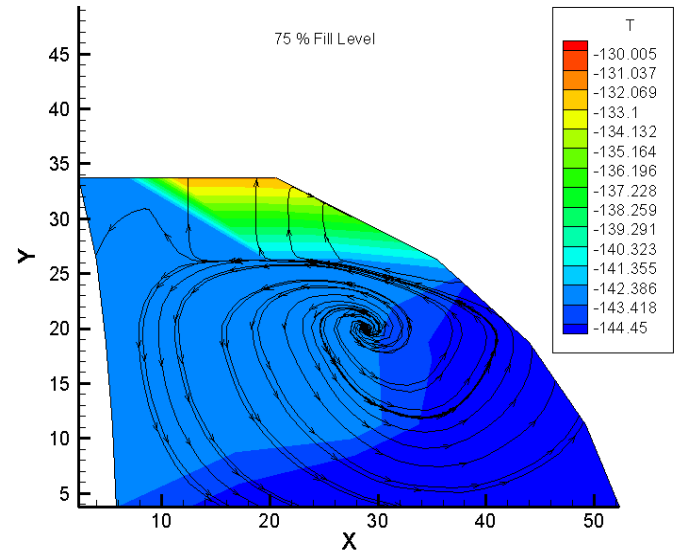
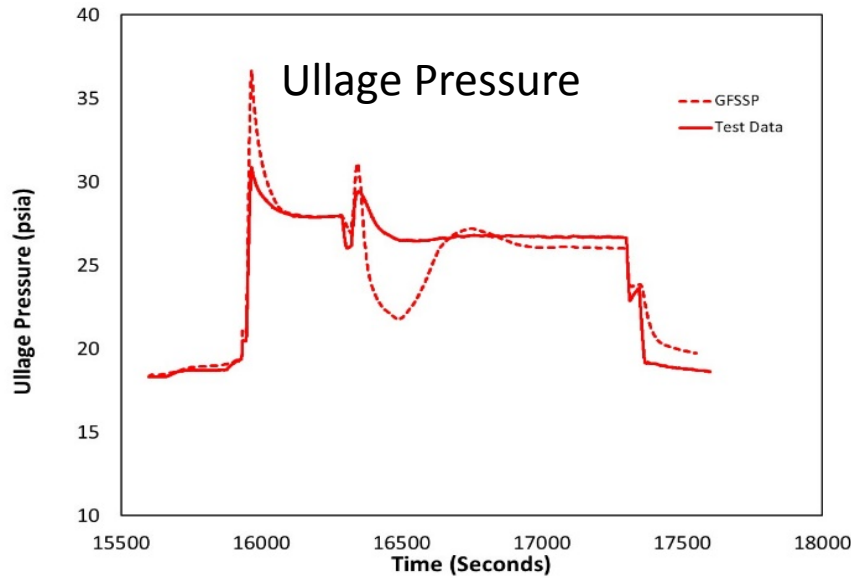
Net Heat Transfer Rate:

$$Q_{\text{net}} = \dot{m}[C_{P,l}(T_I - T_L) + h_{fg}]$$



Results for 75% Fill Level

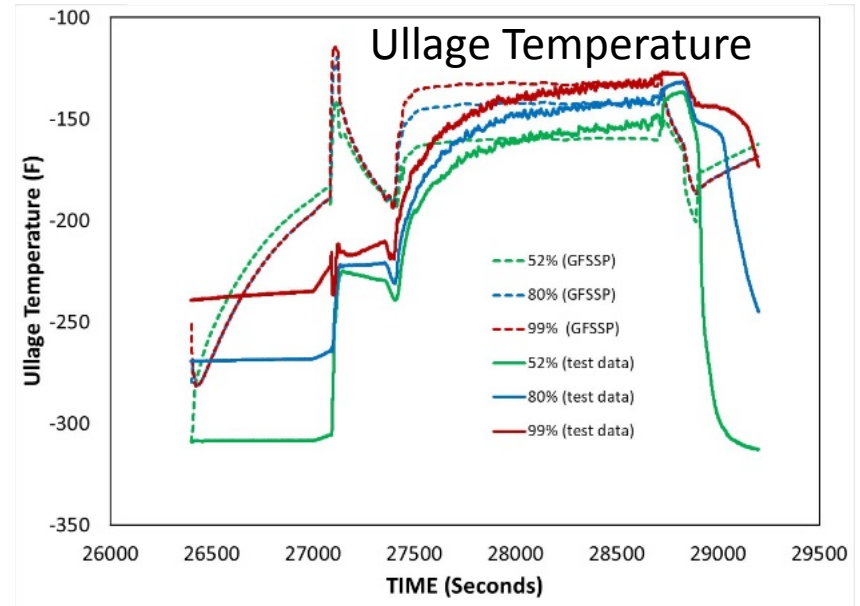
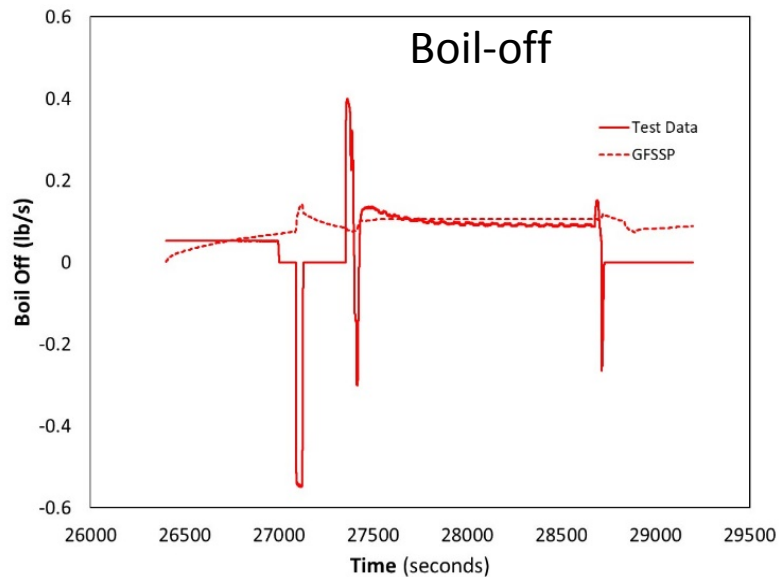
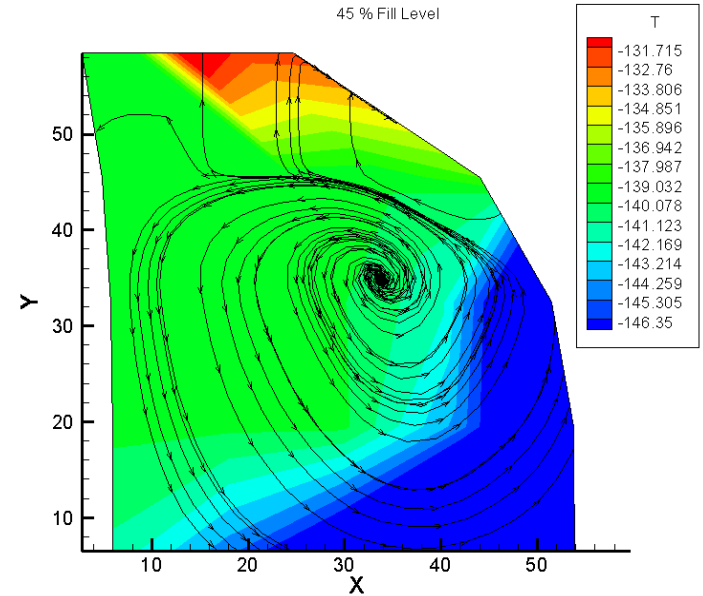
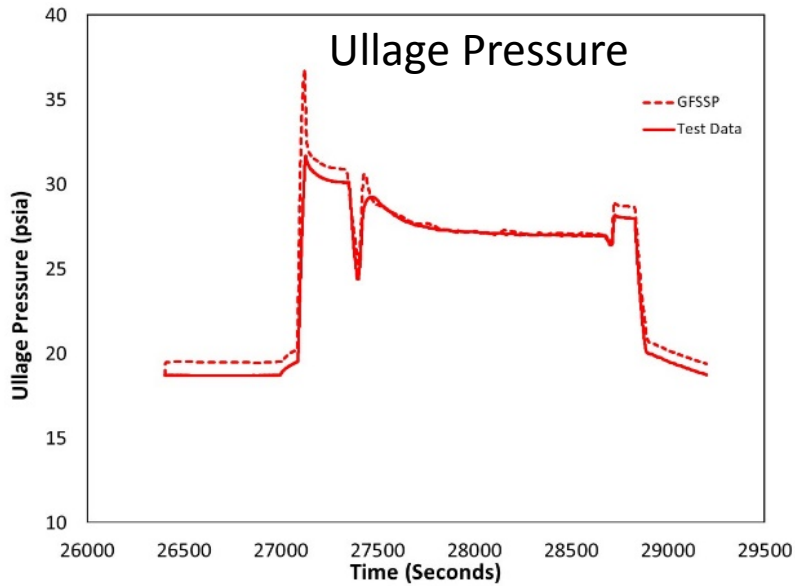
Temperature contour /stream traces





Results for 45% Fill Level

Temperature contour /stream traces





Conclusions

- This paper demonstrates the feasibility of system level modeling of tank pressurization using multiple nodes.
- The ullage of a flight tank has been modeled using 25 nodes and 40 branches where mass and energy conservation equations were solved at the nodes and momentum equations are solved at the branches.
- Gravity, heat and mass transfer at the liquid vapor interface, and heat transfer between solid and fluid are accounted for in the governing equations.
- The model results have been verified by comparing with test data.
- The advantage of using multiple nodes in a system level code is that it allows prediction of recirculation and stratification with a fraction of the computational cost of a high fidelity Navier-Stokes code.



Acknowledgement

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- The authors want to acknowledge Arthur Werkheiser of NASA/MSFC for their contribution
- More information about GFSSP is available at <https://www.nasa.gov/gfssp>
- GFSSP is available free of cost for US Government work from MSFC Tech Transfer Office <https://software.nasa.gov/software/MFS-33019-1>