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David L. Klement Pacific University

Donald R. Turner Pacific University

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Abstract Blur effects on clock-dial cylinder determination

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BLUR EFFECTS ON CLOCK-DIAL CYLINDER DETERMINATION

David L. Klement

and

Donald R. Turner

Submitted in partial fulfillment of the requirements for the degree Doctorate of Optometry.

May 10, 1974

Approved by

Advisor

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INTRODUCTION

The aim of this study is to determine how the cylindrical power and axis determination using the Clock Dial test is affected by different amounts of blur. The cylinder axis and power determined by the use of the Jackson Cross Cylinder provide the reference values for our comparisons.

Standard methods for determining the pretest blur lens include: a) reducing the fogging lens until the 20/40 acuity line can barely be identified; similarly, b) reducing the fogging lens until the 20/30 acuity line can first be distinguished; or c) if a sunburst or clock dial is used, the stopping place is the point where any of the lines appears maximally distinct and/or black. Hebbard* also suggests beginning with a $\pm.75$ diopter sphere placed over the static retinoscopic correction, provided that this reduces the acuity to 20/25 or less.

HYPOTHESIS

It would be expected that a pretest blur of +.50 diopter relative to criterion c) above, would give the most accurate clock dial finding for a patient's cylindrical power and axis determination. Other amounts of blur should make the patient's discrimination more difficult, and would therefore cause the results to be less accurate. (See page 4 for further remarks.)

PROCEDURE

We designated our fogging lenses relative to a control lens which we determined by the following procedure. We started with the subject's habitual lenses in the phorometer. At this point we performed a 20/40 blur, an astigmatic clock dial, a red-green

*Borish, I.M., Clinical Refraction, 3rd Edition, Professional Press, Inc., Chicago, Illinois, 1970, p. 729.

biochrome test, and a Jackson Cross Cylinder Test (J.C.C.) for refinement of axis and power. For the J.C.C., in particular, we extrapolated to the nearest .12 diopter of power and to the nearest 1 degree in axis. Our final control lens consisted of the J.C.C. cylinder (in minus cylinder form) reduced by .50 diopter to induce a standard astigmatic interval in a known meridian. Combined with this induced astigmatism was a sphere which we determined by using the T-chart on an AO projector slide. Here we added +.75 diopter sphere. Reducing the plus sphere in .25 diopter steps, we instructed the patient to report when the darker lines stopped becoming darker. We now increased the plus sphere until the patient first noticed the same lines become just slightly blurred, or less dark. The sphere of the control lens is .25 diopter more minus than this sphere, and is combined with the cylinder previously mentioned. It is relative to the control lens that the different amounts of blur were chosen.

Varying amounts of blur from +.25 diopter to +1.00 diopter were then added, and the effects on the clock dial findings were compared. For each amount of blur the cylinder power was tested on the T-chart with Alines of the T parallel and perpendicular to cylinder the cylinder axis of the control lens. With changing Alens power, the blacker lines change by 90°, and the midpoint of this range was taken as the cylinder power. With the control cylinder restored, the cylinder axis was independently established for each standard blur by changing the orientation of the T-chart until first one set of lines was reported darker, and then the other set was reported darker. The recorded cylinder axis was 45° from the midpoint of this range.

2

SAMPLE

All twenty subjects for this investigation were members of the Pacific University faculty and student body, representing a total population of forty eyes. The spherical refractive errors ranged from -8.25D to +5.00D with eight eyes being hyperopic and the rest myopic, while the cylinder power ranged from -.12D to -3.50D.

RESULTS

For analysis of the data, several statistical tests were performed:

- the mean of the differences between the J.C.C. cylinder power and the respective cylinder power recorded for each blur.
- the mean of the differences between the J.C.C. cylinder axis and the respective cylinder axis recorded for each blur.
- the standard deviation of these same differences for both power and axis.
- 4. the variance of these differences for both power and axis.
- 5. Pearson's product-moment correlation coefficient between each J.C.C. and each blur value for both power and axis.
- Pearson's product-moment correlation coefficient between each J.C.C. and its respective original clock-dial measurement for both power and axis.
- 7. Student's t value for significance of differences

between the means of the data points correlated for both power and axis, and the means of the J.C.C.

DISCUSSION AND CONCLUSIONS

Comparing the differences of the means of the blur lenses with the mean of the J.C.C for power and axis, certain trends can be seen. The large difference between means for the +1.00 blur lens power indicates that with this much fog the power discrimination becomes very difficult for the patient to make. Because the patient is looking through so much plus, he prefers, on the average, an extra .25 diopter of minus cylinder. Likewise, the large difference between means for the +.25 blur lens axis indicates that with this little fog, the axis discrimination becomes very difficult for the patient to make. Because he is looking through so little plus, and all the lines are so much clearer, it is hard for him to determine when the change in darkness occurs. Consequently, the +.50 or +.75 blur lenses would be preferred for use in the clock dial test because the errors are minimum for both cylinder power and axis determination. This is in general agreement with our hypothesis and with Hebbard's recommendation for lens control.

The correlation coefficients are all quite high, which shows that the differences between the J.C.C. and the dock dial findings are relatively constant. The t-test for significance indicates the difficulty previously mentioned for determining cylinder power through a +1.00 blur and cylinder axis through a +.25 blur. A difference of this magnitude would only occur if due to chance 2% of the time with +1.00 blur, and 14% of the time with +.25

*It is likely that accommodative fluctuations influence judgements excessively when inadequate blur is used.

blur. There is no significant difference between either the standard deviations or the variances.

There are probably many sources of error in this investigation, as there are in any experiment. However, the three major sources are (1) inaccuracies in the equipment; (2) relatively small sample population; and (3) patient and examiner bias.

Table 1. CYLINDER POWER DIFFERENCE FROM J.C.C.

	Mean of Differences	Standard Deviation	Variance
+.25 blur	.14 Diopter	. 17	2.92 × 10-2
+.50 blur	.19 Diopter	• 20	.04
+.75 blur	.18 Diopter	. 17	.03
+1.00 blur	.18 Diopter	.20	4.07 × 10-2

Table 2. CYLINDER AXIS DIFFERENCE FROM J.C.C.

	Mean of Differences	Standard Daviation	Variance	
+.25 blur	18.58 Degrees	19.35	374.46	
+.50 blur	20.55 Degrees	20.32	412.98	
+.75 blur	15.50 Degrees	21.73	472.35	
+1.00 blur	16.82 Degraes	21.20	449.26	

Tabla 3.

CORRELATION WITH J.C.C. FOR CYLINDER POWER AND AXIS.

	POWER		AXIS		
	Difference of Means	Correlation Coefficient	Difference of Means	Correlation Coefficient	
+.25 blur	.04 D	.97	6.47°	.90	
+.50 blur	.04 D	.97	2.85°	. 88	
+.75 blur	.93 0	•96	4.15°	.76	
+1.00 blur	.26 D	.69	1.52°	. 89	
Briginal C.D.	.01 D	•96	2.00°	.94	

Table 4. t-TEST FOR SIGNIFICANCE OF DIFFERENCES BETWEEN THE MEANS OF THE DATA POINTS CORRELATED FOR BOTH POWER AND AXIS, AND THE MEANS OF THE J.C.C.

	<u>Þouer</u>			AXIS		
	t-value	probability	t-value	ριο	bability	
*.25 blur	1.28	• 20	1.52		•14	
+.50 blur	1.28	•20	.59		,55	
+.75 blur	.90	.38	68		.50	
+1.00 blur	-2.25	.02	.34		.73	
Griginal C.D.	.34	.75	.65		.51	

M.J.

C.D.	pl -2.25	x 165	pl -2.25	x 180
R.G.	75 -2.2	5 x 165	25 -2.2	5 x 180
J.C.C.	75 -2.7	5 x 175	25 -2.5	0 x 180
CONTROL	pl -2.25	x 175	pl -2.00	x 180
	power	axis	power	axis
+.25 blur	-2.62	177	-2.62	2
+.50 blur	-2,62	1 80	-2.50	15
+.75 blur	-2.87	1 80	-2.25	7
+1.00 blur	-2.50	170	-2.37	5

G.W.

C.D.	-7.25 -1.25 x 180	-7.00 -2.50 x 15
R.G.	-8.25 -1.25 x 180	-7.75 -2.50 x 15
J.C.C.	-8.25 -1.25 x 175	-7.75 -3.00 x 5
CONTROL	-7.75 -1.25 x 175	-8.25 -2.50 x 5
	power axis	power axis
+.25 blur	-1.25 151	-3.00 175
+.50 blur	75 150	-3.00 170
+.75 blur	-1.25 150	-2.87 169
+1.00 blur	-1.25 150	-2.87 180

	0.D.	0.S.	
G.G.			
C.D.	- 2.50 - 1.25 x 168	-1.2575 x 30	
R.G.	-3.50 -1.25 x 168	-2.5075 x 30	
J.C.C.	-3.50 -1.25 x 165	-2.5075 x 175	
CONTROL	-3.2575 x 165	-2.5025 x 175	
	power axis	power axis	
+.25 blur	-1.25 180	-1.12 162	
+.50 blur	-1.87 5	-1.62 165	
+.75 blur	-1.87 173	-1.25 169	
+1.00 blur	-1.87 177	-1.75 165	

R.H.

C.D.	-1.75 -1.75 x 105	-2.00 -1.25 x 90
R.G.	-2.00 -1.75 x 105	-2.50 -1.25 x 90
J.C.C.	-2.00 -2.00 x 100	-2.50 -1.00 x 87
CONTROL	-1.50 -1.50 x 100	-2.2550 x 87
	power axis	power axis
+.25	-2.12 82	-1.12 75
+.50	-2.00 73	-1.00 35
+.75	-1.87 74	-1.25 86
+1.00	-2.25 72	-1.12 93

-1.50 x 180

-1.50 x 180

-1.75 x 172

-1.75 x 172

axis

1.65

157

163

173

W.C.

C.D.	-4.50 -1.0	00 x 180	-5.00
R.G.	-5.00 -1.0	00 x 180	-5.00
J.C.C.	-5.00 -1.0	00 x 175	5.00
CONTROL	-4.50 -1.0	00 x 175	-4.75
	power	axis	power
+.25 blur	87	5	-1.37
+.50 blur	-1.00	175	-1.50
+.75 blur	87	175	-1.62
+1.00 blur	75	150	-1.75

S.M.

C.D.	-4.00 -1.00 х бо	-3.7587 x 150
R.G.	-4.87 -1.00 x 60	-5.1287 x 150
J.C.C.	≟5.00 –.75 x 57	-5.25 -1.00 x 150
CONTROL	-4.0075 x 57	-4.25 -1.00 x 150
	power axis	power axis
+.25 blur	75 37	87 137
+.50 blur	75 35	87 130
+.75 blur	87 37	87 130
+1.00 blur	75 35	62 132

D.K.

C.D.	75 -2.75	5 x 180		-1.50	-3.75 x 180
R.G.	-1.62 -2.	75 x 180		-1.87	-3.75 x 180
J.C.C.	-1.50 -3.2	25 x 180	S • 5 1	-1.75	-3.50 x 180
CONTROL	-1.75 -2.7	75 x 180		-1.50	-3.00 x 180
	power	axis		power	axis
+.25 blur	-2.87	45		-3:37	60
+.50 blur	-3.00	61		-3.75	69
+.75 blur	-2.87	70		-3.50	70
+1.00 blur	-2.87	72		-3.62	70

D.S.

C.D.	7550	x 120	256	2 x 135
R.G.	-1.505	50 x 120	-1.25	75 x 135
J.C.C.	-1.257	′5 x 160	-1.50	50 x 157
CONTROL	1.002	25 x 160	-1.25	
	power	axis	power	axis
+.25 blur	12	172	25	60
+.50 blur	25	170	37	56
+.75 blur	25	170	25	55
+1.00 blur	50	172	37	60

0.S.

J.R.

C.D.	2550	x 60	pl62 x	110
R.G.	7550	x 60	2562	x 110
J.C.C.	7575	x 60	2525	x 110
CONTROL	2525	x 110	2525	x 20
	power	axis	power	axis
+.25 blur	62	70	25	30
+.50 blur	62	117	~ ₅50	45
*.75 blur	62	124	50	47
+1.00 blur	50	80	25	35

D.V.

C.D.	+5.25 -1.	25 x 90	+5.25 -1.75	x90
R.G.	+4.75 -1.	25 x 90	+5.25 -1.75	x 90
J.C.C.	+4.757	5 x 97	+5.25 -1.75	x 82
CONTROL	+5.002	5 x 97	+5.00 -1.25	x 82
	power	axis	power ax	cis
+.25 blur	-1.00	110	-1.75 80)
+.50 blur	-1.00	110	-1.50 81	
+.75 blur	75	110	-1.50 80)
+1.00 blur	87	?	-1.25 70)

Patient J.A.

	3 D			05		
C.D.	-2.005	50 X 15	$C = d\delta$	-1.752	25 X 105	
R.G.	-3.005	50 X 15		-2.752	25 X 105	
J.C.C.	-3.003	37 X 15		-2.756	52 X 135	÷
Control	-2.75 spt	1		-2.252	25 % 135	
		rewor	axis		power	axis
+.25 blur	-2.50	12	X 180	-2.00	62	X 160
+.50 blur	-2.25	12	X 5	-1.75	37	X 150
+.75 blur	-2.00	25	X 15	-1.50	12	X 140
*1.00 blur	-1.75	37	8 X	-1.25	25	X 145

V ...

Patient L. C.	GD			25		
C.D.	-3.00 sph	3		-4.00 spl	r	
R.G.	-3.75 spt	ı		-4.75 spl	'n	
J.C.C.	-3.753	37 X 100		-4.75	12 X 15	
Control	-3.502	25 X 10		~4.25 =.	50 X 105	
		power	axis		power	axis
+.25 blur	-3.25	25	X-120	-4.25	sph	X 35
+.50 blur	-3.00	37	X 132	-4.00	12	X 37
+.75 blur	-2.75	37	X 128	-3.75	12	X 30
+1.00 blur	-2.50	50	X 118	-3.50	25	X 23

Patient C. H.

	0D			ØS		
C.D.	-2.25	50 X 90		-1.75	75 X 60	
R.G.	-3.25	50 X 90		-2.25	75 X 60	- N .,
J.C.C.	-3.25	75 X 145		-2.25	62 X 60	
Control	-3.25	25 X 140		-2.00 sp	ih	
		power	axis		power	axis
+.25 blur	-3.00	75	X 142	-1.75	25	X 60
+.50 blur	-2.75	-1.00	X 147	-1.50	25	X 65
#75 blur	-2.50	75	X 134	-1.25	25	X 62
+1.00 blur	-2.25	75	X 142	-1.00	50	X 63

1.1

Patient C. M.

	ΩD	ØS
C.D.	+1.0025 X 90	+1.00 sph
R.G.	2525 X 90	plano sph
J.C.C.	2512 X 90	plano12 X 90
Control	+.2550 X 180	+1.0050 X 180
	power axis	power axis
≁.25 blur	power axis *.5050 X 85	powsr axis
		¥ ¥
+.50 blur	≁.5050 X 85	+1.2512 × 85

Patient D. M.

	20			0S		
C.D.	+.502	5 X 75		+.5075	5 X 75	
R.G.	752	5 X 7 5		5075	5 X 75	
J.C.C.	751	2 X 33		5062	X 92	
Control	plano	50 X 173	3	25 sph		
		powar	axis		bomet	axis
+.25 blur	+.25	37	X 67	plano	62	X 88
+.25 blur +.50 blur	+•25 +•50	. .37		plano +.25	62	
			X 65			X 101

Patient L. M.

	0.0				1	0S				
С.Э.	+1.0050	J X 45			+1.03	-1.0	00 X 105			
R.G.	+.2550	X 45			+1.00	-1.0	00 X 105			
J.C.C.	*.2512	X 180			÷1.00	91	7 X 105			
Control	2550	X 90			plano	75	5 X 105			
		power	10	xis			power	a	xis	
+.25 blur	plano	12	Х	145	+.25		87	χ	87	
+.50 blur	+.25	12	Х	170	+.50		97	Х	32	
+.75 blur	+.50	12	Х	178	+.75		37	Х	102	
+1.00 blur	+.75	37	Х	5	+1.00		87	X	97	

Patient S. R.

	00			<u>8</u> 5		
C.D.	+1.50	50 X 30		<1.50 -t	00 × 90	
R.G.	+ .75	+ .7550 X 30			1.00 X 90	
J.C.C.	+ .75	+ .7512 X 175			.97 X 100	
Control	+.255	ia x 85		*.502	25 X 100	
		power	axis		bomar	axis
+.25 blur	+.50	12	X 140	+.75	87	X 82
+.50 blur	+.75	12	X 155	+1.00	87	X 7?
♦.75 blur	÷1.99	12	X 173	+1.25	87	X 97
+1.00 blur	+1.25	37	X 130	+1.50	87	X 92

Patient N. R.

	JD			0s			
C.D.	+1.002	5 X 90		+1.007	5 X 90		
R.G.	2525	2525 X 90			plano75 X 90		
J.C.C.	2512	X 79		plano5	2 X 87		
Control	+.5050	X 168		+.25 sph			
		power	axis		zewar	axis	
+.25 blur	÷.75	37	X 62	+.50	62	X 83	
+.50 blur	+1.00	37	X 61	∻.75	87	X 96	
+.75 blur	+1.25	12	X 74	+1.00	37	X 94	
+1.00 blur	+1.50	12	X 81	+1.25	62	X 99	

Patient D. T.

100	5
51	11
Dee.	.

C.D.	-3.50 -1.00 X 30
R.G.	-4.75 -1.00 X 30
J.C.C,	-4.75 -1.12 X 15
Control	-4.25 -1.00 X 15
	power axis
+.25 blur	-4.00 -1.12 X 170
+.50 blur	-3.75 -1.12 × 180
+.75 blur	-3.50 -1.37 X 11
+1.00 blur	-3.25 -1.37 X 15

DS

-4.25 -1.25 X 152 -4.75 -1.25 X 152 -4.75 -1.12 X 155 -4.25 -1.00 X 155 power exis -4.00 -1.12 X 150 -3.75 -1.12 X 155 -3.50 -1.25 X 162 -3.25 -1.37 X 172

Patient F. Z.

	DD			DS .			
C.D.	-2.002	5 X 90		-1.505	0 X 60		
R.G.	-3.002	5 X 90		-2.0050 X 60			
J.C.C.	-3.0050	X 1 40		-2.3037 X 55			
Control	-3.80 sph			~1.7525 X 145			
		oower	axis		power	axis	
+.25 blur	-2.75	50	X 137	-1.50	sph	X 55	
+.50 blur	-2.50	75	X 142	-1.25	sph	X 60	
*.75 blur	-2.25	50	X 129	-1.00	sph	X 57	
+1.00 blur	-2.00	50	X 137	75	. 25	X 58	

0 5 Ľ