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A study of the Van Orden star

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Abstract

The purpose of the present study was to determine the variations in the star phoric behavior, using the Van Orden Star and a controlled stimulus to accomodation.

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INTRODUCTION

This present study is one of a series utalizing the Van Orden Star. More precisely it is a supplement to a previous work, conducted at the University₁, which attempted to determine the phoric behavior with varying stimuli to accomodation. In the study under consideration, however, the induced prismatic effects have been compensated for.

PURPOSE

The purpose of the present study was to determine the variations in the star phoric behavior, using the Van Orden Star and a controlled stimulus to accomodation.

PROCEEDURE

All the following data was obtained by using a wide base stereoscope, the dimensions of which were $18" \ge 24"$, to maintain a constant working angle of twenty degrees at the varying test distances.(see diagram 1). A head rest was attached to a stationary aluminum rod, along which the head rest could be moved to the desired testing distance. A septum 7.5" $\ge 4.5"$ was attached to the head rest to maintain dissociation. A trial frame was also used, in which varying amounts of prism and lenses could be inserted while retaining the individual P.D. of the person under test, thus eliminating induced prismatic effects.

The pencils used were of the same color and length in order to preclude any ahnd favoring other than that of natural hand dominancy.

L. A Study of the Van Orden Star - Edward Craig, Borbert King- a t thesis for Doctor's degree- Pacific University Library The testing was conducted at two distances, 8# and 16". At the 8" distance a total of fifty stars were drawn by each subject. These were divided into five series of ten stars; each series beingcomposed of five stars drawn with no stimulus to accomodation, which preceeded five stars drawn with varying stimuli to accomodation. These varying stimuli were five one diopter increases in the stimulus to accomodation.

The proceedure was repeated for the 16" test distance where fourty stars were drawn. Here, however, there were only four one diopter increases in the stimulus to accomodation.

A total of ten subjects were used in the study, ranging between 20 and 32 years of age, all of whom were wearing their distance prescriptions during the testing proceedures. There was no fixed time in which a series had to be completed, or the number of series completed in each session; however, once a series was begun, it had to be completed at that session.

The amount of prism necessary to gain dissociation was recorded for each subject and used in the computation of the seperation of the star points. Since each lens was individually centered, there were no residual prismatic effects which had to be taken into consideration. An average seperation was computed for each set of five findings; the prism used to obtain the dissociation was then used to calculate the real seperation of the star points. The mean was then calculated from the data.

RESULTS

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Graphs were then drawn. The first had as its abscissae the stimulus to accomodation, and, as its ordinate, convergence in prism diopters. On this both the 8" and the 16" test distances were plotted. The second and the third graph were plotted with their abscissae as no stimulus to accomodation, after a previous stimulus to accomodation; and their ordinates as convergence in prism diopters.

The mean for the 8" and 16" testing distance, with no previous stimulus to accomodation was taken as the base line. The differance between the means and the base line, for each subsequent return to no stimulus to accomodation, after a previous stimulus were plotted.

> 1. the effect of minus spheres on the star seperation a. the mean for each diopter of stimulus to accomodation was calculated for the group of ten subjects.

b. this was done for both the 8" and the 16" testing distance.

c. the calculated means were as follows

testing distance	stimulus	mean
÷	-1.00	14.0
	-2.00	15.9
8#	-3.00	19.3
	-4.00	22.9
	-5.00	24.9
	-1.00	12.6
16"	-2.00	14.5
	-3.00	18.6
	-4.00	20.9

d. for the 8" test distance a minus one to minus two
diopter stimulus to accomodation produced a slope of 1/3
- with a minus two to a minus four diopter

stimulus the slope was 1/2.

- with a minus four to a minus five diopter stimulus the slope was again 1/3.

e. for the 16" testing distance a minus one to a minus two diopter stimulus to accomodation produced a slope of 1/3.

- with a minus two to a minus three diopter stimulus the slope was 1/2.

- with a minus three to a minus four diopter stimulus the slope was 1/3.

2. The effect of practice on the star seperation after a previous practice with minus lenses.

a. the means were taken and the first mean was taken as the base line.

b. the differance between the subsequent means were as follows:

<u>distance</u>	<u>stimulus</u> no stimulus	differances	a <u>ctual mean</u> 13.7
8"	-1.00 -2.00 -3.00 -4.00	.6 B.I. 1.4 B.I. .2 B.I. .5 B.I.	13.1 12.3 13.5 13.2
16"	no stimulus -1.00 -2.00 -3.00	.6B.0. 1.0B.0. 1.6B.0.	9.8 10.4 10.8 11.4

CONCLUSION

1. The effect of minus spheres on the star seperation;

a. it was found that the ACA ratio for the first one

diopter stimulus to accomodation differed from the ACA ratio of the middle range of accomodation.

b. The amount of convergence that was elicited at the beginning of accomodation was smaller than the amount of convergence for the middle range of accomodation.
c. The ACA ratio for the first diopter of accomodation was found to be the same as the last diopter of accomodation.

d. the ACA ratio, rather than being a constant relationship, varies for the range of accomodation being utalized.

e. the above results should be checked by determining the confidence level.

2. The effect of practice on the star seperation, after a previous stimulus to accomodation.

a. practice at the 16" test distance showed an after effect by posturing the star pattern in an increasing esophoric direction.

b. practice at the 8" test distance showed an after
 effect by the posturing of the star pattern in an
 exophoric direction.

c. the 8" testing distance showed an erratic effect on posturing, turning to a relative esophoric direction at the endpoint of accomodation.







APPENDIX

1.	Data	Moa sur	ed and Ca	alculated from	the Star	r Pattern S	eparation
	Obs.	PD	Dissocia Prism	at. Mean Sep. mm.	Lens	Diff. btw. Nean & PD.	Actual Sep.
	DH	65	16 BO	8* 66.4 65.8 67.2 64.8 65.2 58.6 58.6 54.6 54.6 68.2 47.2	5.00 4.00 5.00 5.00 2.00 5.00 1.00 5.00 planc	•7 •4 •1•1 •12 •12 •12 •12 •12 •12 •12 •12 •1	15.3 15.6 14.9 16.1 15.9 19.2 13.7 21.2 14.4 24.9
			12 B0 16 B0 12 B0 30 B0	16*67.8 60.4 68.2 44.8 60 54.6 63.4 91.2	2.50 2.50 0.50 2.50 2.50 2.50 2.50	•7 1•15 5•05 1•25 2•6 •4 6•55	11.3 13.15 11.2 17.05 13.25 18.6 12.4 23.45
	JB	67	12 80	85.8 84.6 87 80.2 89.5 78.6	5.00 4.00 5.00 3.00 5.00 2.00	9.25 8.8 10. 7.6 11.25 5.8	2.75 3.2 2.0 4.4 .75 5.2
			11 BO None 11 BO None 11 BO None 11 BO None	62.2 66.6 82.8 62.6 16"108.6 B0 102.4 63.2 86.8 65.6 77.4 63 74.7	5.00 1.00 5.00 plano 2.50 1.50 2.50 0.50 2.50 -0.50 2.50 -1.50	7.9 2.2 10.4 8.85 4.95 4.95 2.6 1.85	3.4 11.2 3.1 13.2 .6 2.25 BØ .95 BI 5.05 B0 .35 BI 7.4 B0 1. BI 8.15 B0
	RH I	62	6 BO	8" 31.8 36.2 37.4 28.2 42.2 26 45.8 33 45.8 34.4	5.00 4.00 5.00 3.00 5.00 5.00 1.00 5.00	15.1 12.9 12.3 16.9 9.9 18.0 8.1 14.5 8.1	21.1 18.9 18.3 22.9 15.9 24.0 14.1 20.5 14.1 25.8

12 B**D**

Obs.	PD	Dissociat. Prism	Mean Sep. mm.	Lens Diff. Btw. <u>Mean</u> & PD.	Actual Sep.
EH	62	12 B0 16'	80.4 66.2 76.0 68.2 67.8 47.1 75.0 40.4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7.4 10.95 8.5 10.55 10.55 15.7 8.75 17.4
LR	62	12 B0 8" 16'	64.2 62 64.8 67.4 58.8 63.4 50.4 45.4 77.8 77.8 77.8 77.8 77.8 77.8 77.8 77	5.00 1.1 4.00 0.0 5.00 2.0 3.00 1.4 5.00 2.7 2.00 1.6 5.00 7 1.00 5.8 5.00 1.7 planc 8.3 2.50 3.95 1.50 3.95 1.50 3.95 2.50 3.95 0.50 .5 2.50 3.45 .0.50 .25 2.50 3.5 -1.50 2.5	10.9 12.0 10.0 10.6 9.3 13.6 11.3 17.8 10.3 20.3 5 8.05 8.05 11.5 5 12.2 5 12.0 10.6 9.3 13.6 11.3 8.05 5 8.05 5 11.5 5 5 12.0 10.0 10.6 9.3 13.6 11.3 17.8 10.5 5 8.05 5 11.5 5 12.0 10.6 9.3 13.6 11.3 12.0 10.6 9.3 13.6 11.3 12.0 10.6 9.3 13.6 11.3 12.0 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 11.5 10.5 10
DD	66	12 B0 8* 16' 20 B0	63.6 64 67.2 53 65.4 47.8 37.2 37.2 28 73.4 51.8 73.4 51.8 73.4 51.8 73.4 51.8 73.4 51.8 73.4 51.8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 8 73.4 73.2 73.4 73.2 73.4 73.2 73.4 73.2 73.4 73.2 73.4 73.2 73.4 74.2 73.4 74.2 73.4 74.2 73.4 74.2 74.2 73.4 74.2 74.2 74.2 74.2 74.2 74.2 74.2 74	5.00 1.2 4.00 1.0 5.00 .6 3.00 6.5 5.00 3 2.00 9.1 5.00 .4 1.00 14.4 5.00 2.4 plano 19.0 2.50 1.85 1.50 3.55 2.50 1.35 2.50 1.35 -0.50 3.5 2.50 4.2 -1.50 4.7	13.2 13.0 11.4 18.5 12.3 21.1 22.4 26.4 14.4 31.0 10.15 10.15 10.55 10.45 10.65 19.5 11.8 24.7

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Obs.	PD	Dissociat. Prism	Mean Sep, mm.	Lens	Diff. Btw. Mean & PD	Actual Sep.
RG	66	8 BC 8#	70.8 66.6 73.0 55.0 70.0	5.00 4.00 5.00 3.00 5.00	2.4	5.6 7.7 4.5 13.5 6.
		12 BO	66.6 37.2 65.4	5.00 1.000 5.00	14.4	11.7 26.4 13.3
		6 B# 16*	27.0 80.4 64.6 77.4 45.4	2.50 1.50 2.50 0.50	3.6 •35 2.85 5.15	2.4 6.35 3.15 11.15
		16 B0 6 B0 16 B0	79.4 42.2 74.2 42.2	2.50 2.50 1.50	35.95 25.95 25.95	21.95 3.5 21.95
NG	64	6 BO 8"	30.2 28.6 27.8 27.8 21.8 21.8	5.00 4.00 5.00 3.90 5.00 2.00	16.9 19 17.7 18.1 18.1 21.5	22.9 25 23.7 24.1 24.1 27.5 26.1
		8 B0 6 B0 16	16.2 34. 2 10.2 *25.2	1.00 5.00 plano 2,50	23.9 14.9 26.9 9.7	31.9 20.9 32.9 15.7
		16 B0 20 B0	43 53.6 47.8	1.50	5.25	21.25 18.6 24.5
		30 80	65 66.2 84.8 52.4	2.50 -0.50 2.50 -1.50	•25 •55 4•2 2•9	19.75 29.45 25.8 32.9
DP	66	16 BO 8*	64.4 67.4 67.6 64.2	5.00 4.00 5.00 3.00	.8 .8	16.8 15.3 15.2 16.9
		12 BO	64 52.4 63.6 49.9 60.2	5.00 2.00 5.00 1000 5.00	1. 6.9 1.2 11.5 2.9	13 18.8 13.2 23.5 14.9
		16 80 16	73.2 69.2 67.2 77.2	2,50 1.50 2.50 0.60 2.50	2.5	13.6 14.2 15.2 15.7 13.2

Obs.	PD	Dissociat. Prism	Mean Sep. mm.	Lens	Diff. Btw. Mean & PD	Actual Sep.
DP	66	16 BO 16"	54.8	-0.50	2.8	18.8
			75.4	2.50	2.35	13.65
		30 30	102.2	-1.50	9.05	20.95
SG	60	6 BO 8"	46.4	5.00	6.8	12.8
			45.4	4.00	7.3	13.3
			48.4	5.00	5.8	11.8
			41.4	3.00	9.3	15.3
			45.4	5.00	7.3	13.3
			33.6	2.00	13.2	19.2
			47	5.00	6.5	12.5
			31	1.00	19.5	25.5
			49	5.000	5.5	11.5
		12 BO	36.1	plano	11.95	23.95
		8 BO 16	H 49	2.50	2.75	10.75
		12 BO	56	1.50	1.	13.
			66	2.50	1.5	10.5
		1. A	50.4	0.50	2.4	14.4
		16 BO	74.4	2.50	3.6	12.4
		12 BO	36.2	-0.50	5.25	17.95
		16 BO	75.2	2.50	3.8	12.2
			49.8	-1.50	2.55	18.55
KA	67	8 BO 8	1 52.4	5.00	2-3	15.3
			51	4.00	8.	16
			51.6	5.00	7.7	15.7
			49.4	3.00	8.8	16.5
			52.4	5.00	743	15.3
			36	2,00	15.5	23.2
			50.4	5.00	8.3	10.3
			34	1.000	10.9	24.9
			50.8	5.00	8.1	10.1
		12 80	27	plano	20.	32.
		10	* 44	2.50	2.75	17+77
		TO RO	44+2	1,20	2+7	201
			36 4	2.00	5-2	10.7
			30+0	0.90	1 75	37 75
			22 9	2.70	2012	2/ +/7
			55+0	0,70	0.3	38 AF
			2102	2.70	10 25	26.35
			6740	-1.570	10037	C.00.3/

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