



Guidance, Navigation, and Control for NASA Lunar Pallet Lander

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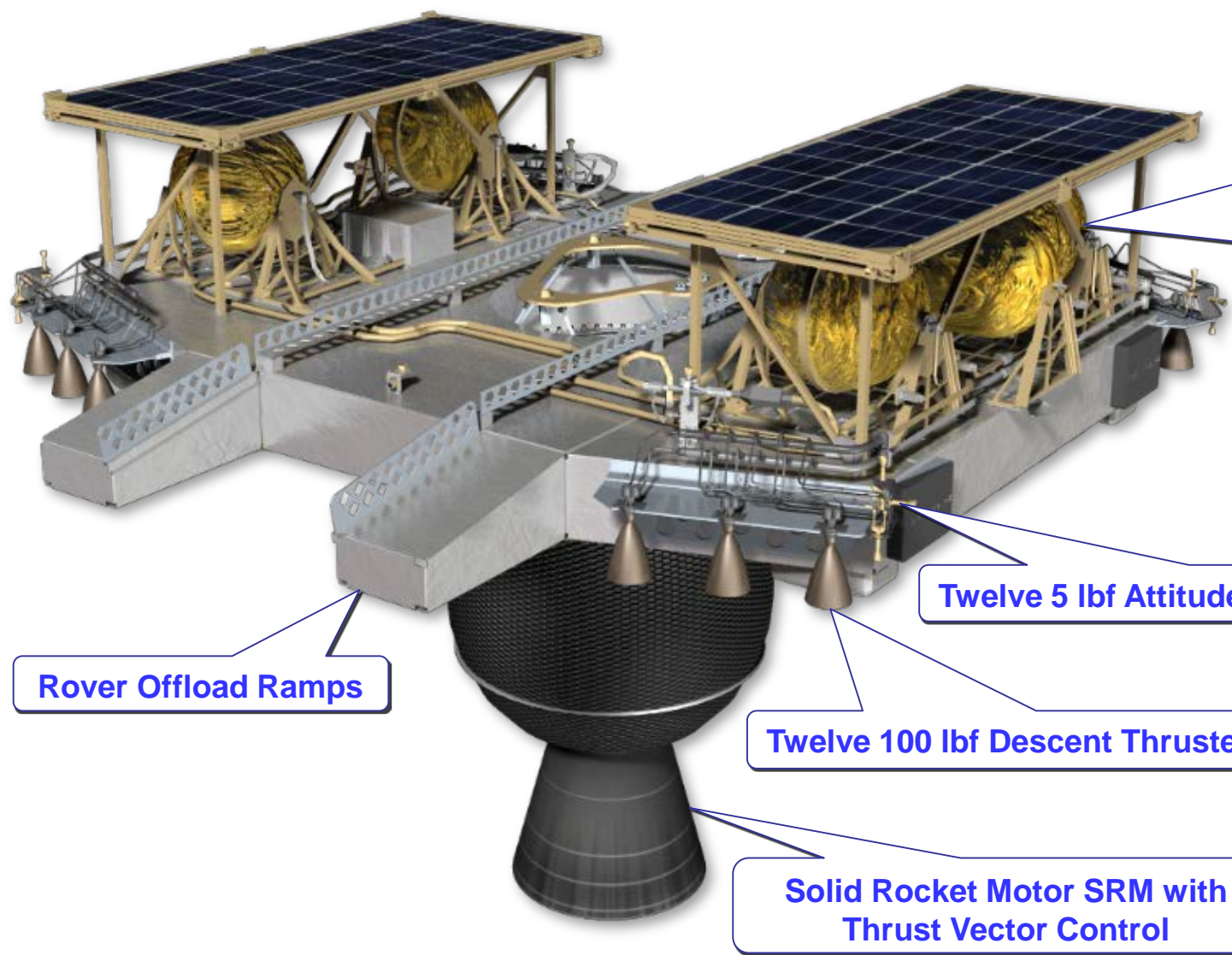
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Breckenridge, CO



- Mission Concept
- Mission Requirements and Navigation Sensor Selection
- Vehicle Guidance Navigation and Control Overview
- Simulation Architecture
- Vehicle Landing Performance
- Future Work and Next Steps

Lunar Pallet Lander



**Hypergolic Bipropellant:
Monomethyl hydrazine and
25% Nitric Oxide
or MON25**

Rover Offload Ramps

Twelve 5 lbf Attitude Thrusters (On/Off)

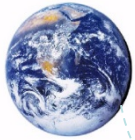
Twelve 100 lbf Descent Thrusters (On/Off)

**Solid Rocket Motor SRM with
Thrust Vector Control**

Mission Overview



Launch Vehicle provided
Trans-Lunar Injection



Trajectory Corrections,
GNC Cal Maneuver Burns

Lunar Transit
~4 days

Separation initiates
the power-up
sequence

Powered Descent by Star 48BV
Burnout altitude = 9.6 km

Coast
~ 0.5 minutes

SRM Lunar Impact
TBD downrange

Descent Initiation by Lander

Descent
~ 3 minutes

Vertical Descent by Lander

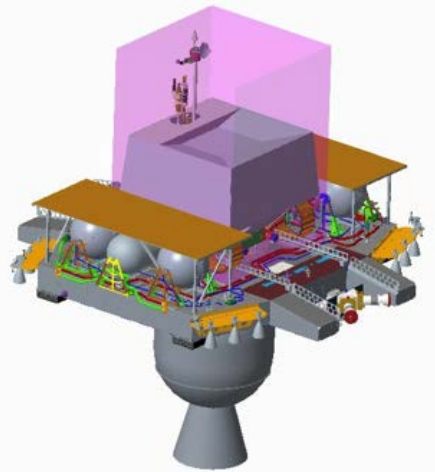
Terrain Relative
Navigation
(no hazard avoidance)

Powered Operation for the
remainder of the lunar
day

Moon

Site A: -85 N 108.64 W elevation -510m
Landing: 6/15/2022 12:00 (UTC)

Flight Phase	Delta-V (m/s)
After separation from ELV	
+440-N descent thruster	25 (TCMs)
+22 N ACS thruster (10%)	2.5
SRM Operation	
+SRM operation	2390 (Braking Burn)
+22-N ACS thruster (25% Duty)	0.24
Vertical Descent by Lander	
+440-N descent thruster	411 (Liquid Descent)
+22-N ACS thruster (10%)	41
+440-N descent thruster (redirect budget)	21



Lander Notes:

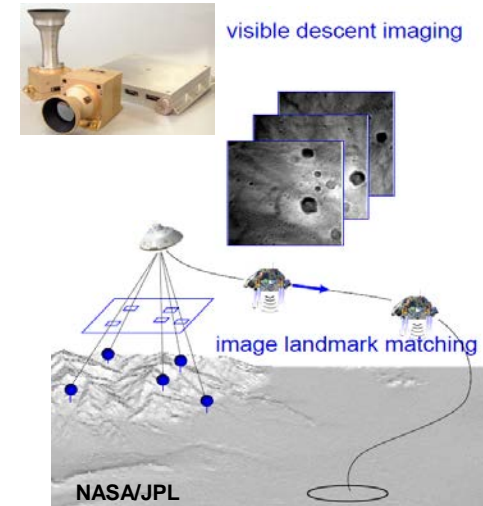
- 37.6 kg Flight Performance Reserve of usable propellant load is added at the end
- TVC assumed SRM
- Altitudes above average lunar radius

Driving Requirements & Sensor Selection



- **Touchdown position and velocity requirements drive GNC sensor selection**
- **Precision landing requirement of 100 meters**
 - To achieve the above precision landing, good measurement of position and velocity are needed:
 - Terrain Relative Navigation (TRN) position sensor is used, which takes images of lunar surface during descent and updates lander location within $< \sim 10\text{m}$ accuracy
 - Navigation Doppler Lidar (NDL) altimeter and velocity sensor for high accuracy altitude and 3-axis velocity measurements with $\sim 0.17\text{ cm/s}$ velocity error
- **Touchdown requirements of 2m/s maximum vertical & horizontal velocities**
 - To meet this requirement, analysis shows that the NDL and a medium grade IMU suffice

Terrain Relative Navigation



NASA- Navigation Doppler Lidar



Candidate sensor

Attitude and Attitude Rate Requirements:

- **Max vertical attitude at touchdown of 5 deg**
- **Max angular rate at touchdown of 2 deg/s**
- **Max attitude error at touchdown +/-10 deg**
 - Sun pointing or Communications pointing
- **Sun pointing during cruise +/-10 deg**

- The above requirements can be met with medium grade IMU, Star Trackers, and Sun Sensors



Candidate sensor:
Northrup Grumman LN200S IMU
~.07 deg/sqrthr angle random walk



Candidate sensor:
2-NST Blue Canyon Star Tracker
Cross-boresight Accuracy 6 arcsec, 1-sigma
Around-boresight Accuracy 40 arcsec, 1-sigma

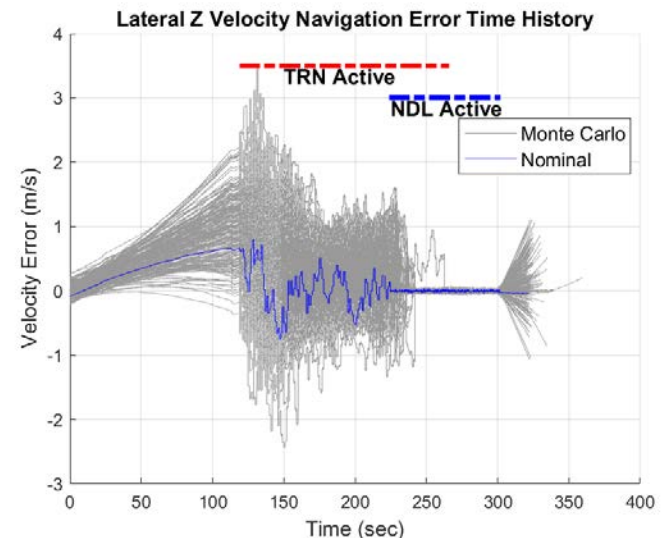
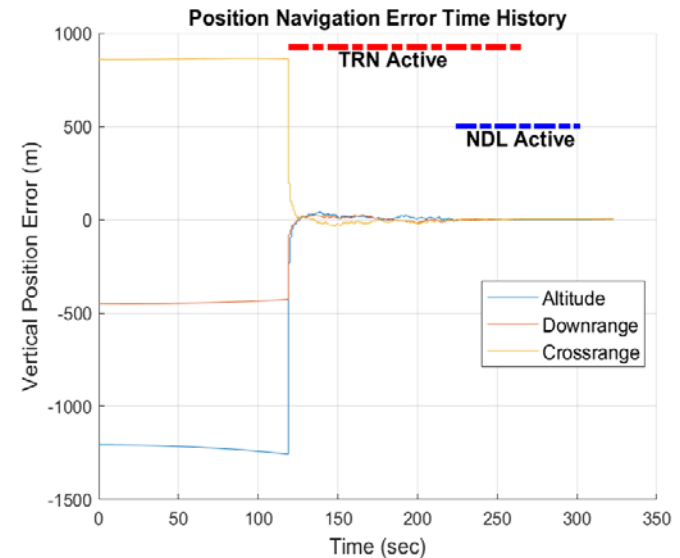


Candidate sensor:
6xNewSpace Fine Digital Sun Sensor
.1deg accuracy with 140deg FOV

Precision Landing Requirement



- Precision landing has never been attempted in space
 - For this mission precision landing means landing within 100 meters (3σ) of a prescribed target
 - Mars 2020 will employ *autonomous* TRN for the first time (primarily for hazard avoidance)
- Previous lunar missions targeted large, flat areas which are largely devoid of hazards
 - Most science missions, however, want to land near craters and outcrops
- Without lunar GPS, precision landing requires **Terrain Relative Navigation (TRN)**
- TRN measures position by correlating images taken by an on-board camera with stored imagery of the lunar/planetary surface
- Combining TRN with NDL significantly improves the Navigation knowledge to achieve precision and soft landing

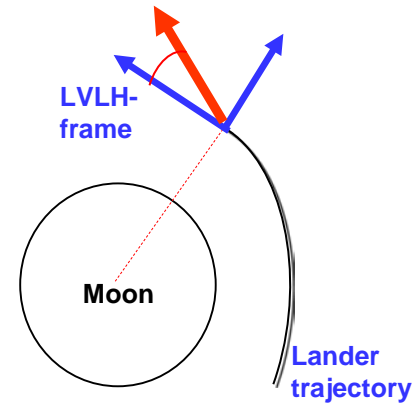


Guidance

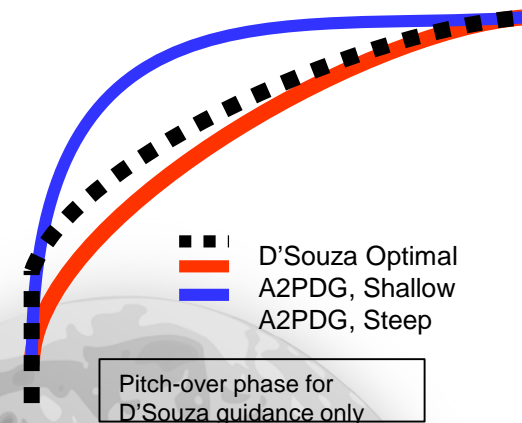


- SRM burn, uses a fixed pitch angle w.r.t. LVLH is used,
 - Based on a ***Moon Entry Descent Algorithm by Ellen M. Braden – NASA/JSC/EG5***
 - Employs a predictor-corrector, predicts vehicle location down to descent and landing
 - Uses an estimated SRM thrust profile based on PMBT
 - Attempts to ensure a good initial state for liquid burn
 - Can be ran during pre-SRM coast to calculate initial LVLH pitch angle
- Liquid Descent, several guidances are currently traded
 - Apollo (baseline), Tunable Apollo, and Quadratic guidances
 - With quadratic formulation of the commanded acceleration
$$a_c = c_0 + c_1 t_{go} + c_2 t_{go}^2$$
 - Differences lie in the commanded acceleration coefficients and the targets
 - All target a final position, velocity, and acceleration vector
 - By targeting acceleration, the desired final attitude of the vehicle can be specified
 - The Minimum Acceleration (D'Souza) guidance only targets the final position and velocity vectors
 - The final attitude of the vehicle cannot be specified
 - A pitch-over maneuver is needed for the vehicle to achieve the desired final attitude

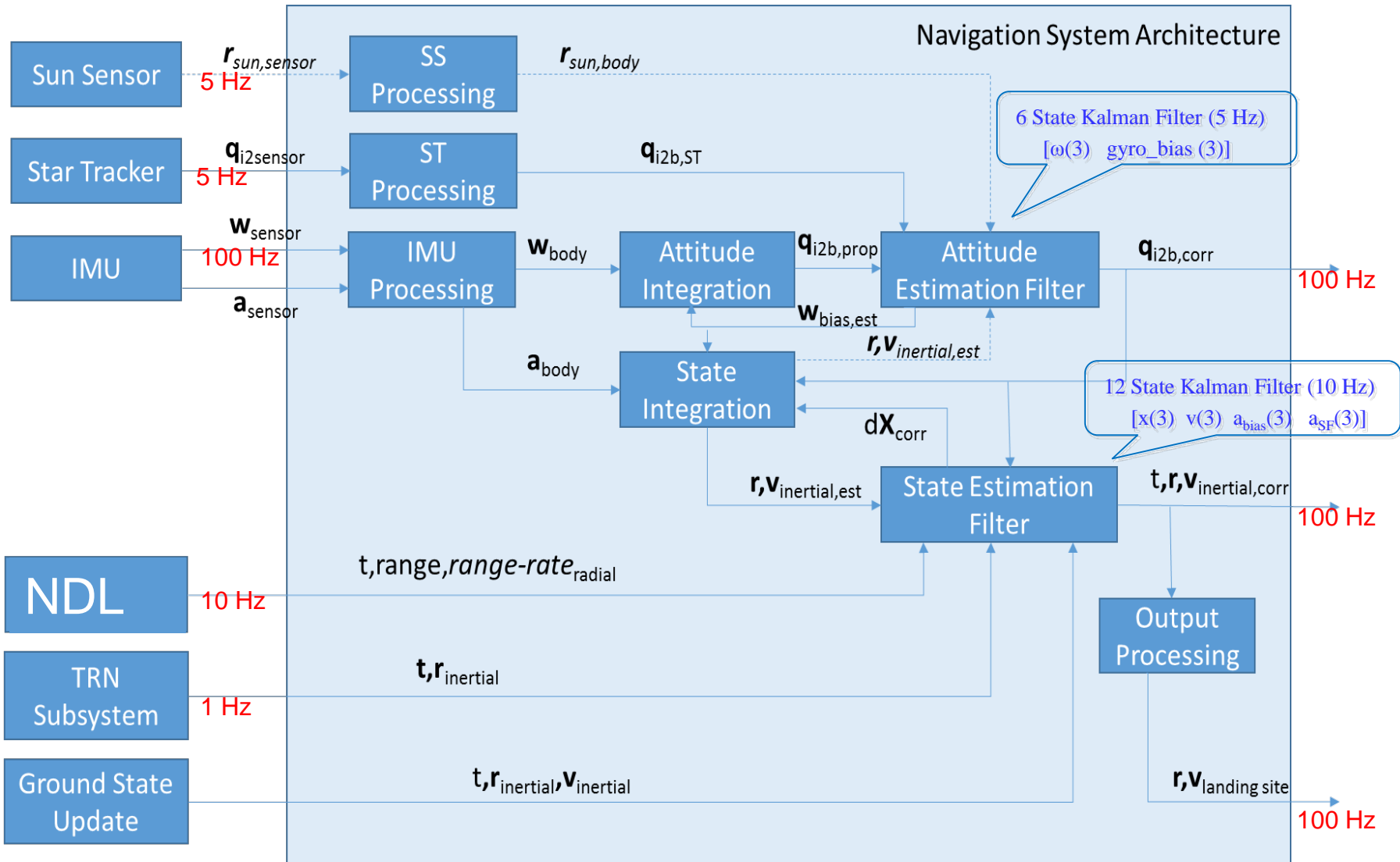
Solid Breaking Burn at Constant LVLH -Pitch



Liquid Descent



Navigation Architecture



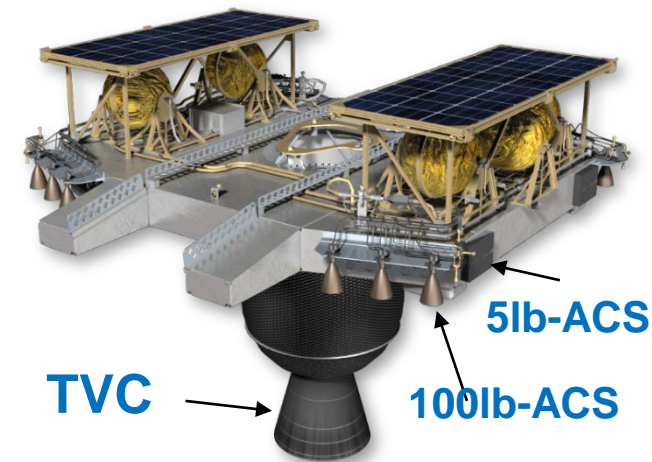
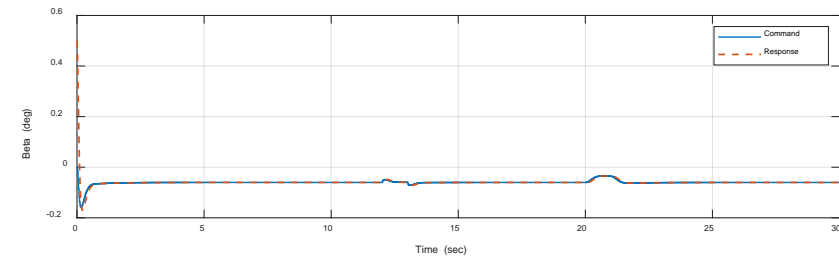
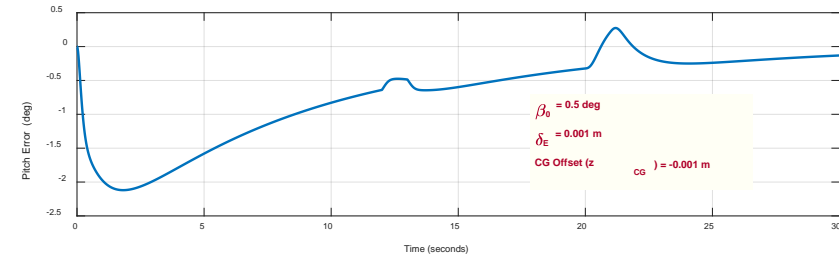
SRM - Control



- Control operates at 50Hz
- SRM stage uses thrust vector control
 - Proportional Integral Derivative (PID) linear control law
 - Roll control via the Attitude Control System (5lb-ACS)
 - SRM is sized for the specific mission/landing site

SRM Control Response

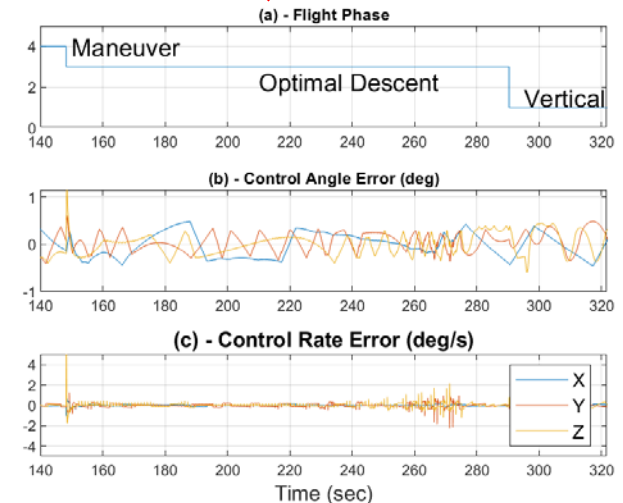
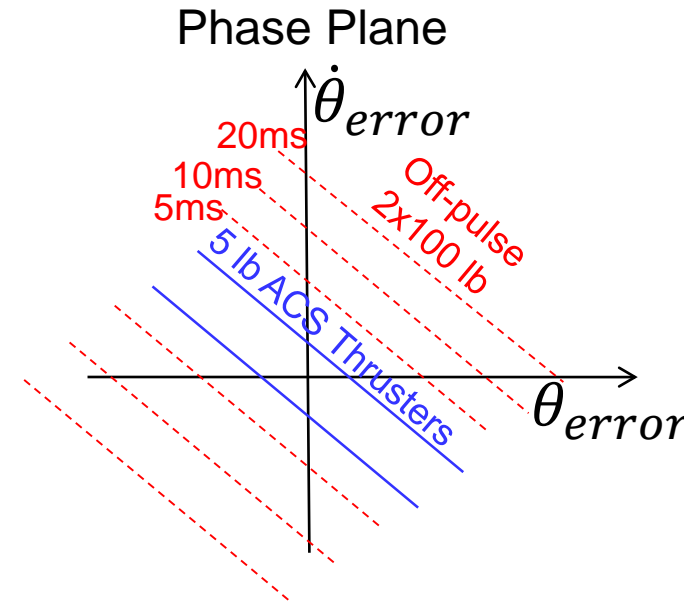
SRM Powered SC



Pulsed Liquid Engine Control



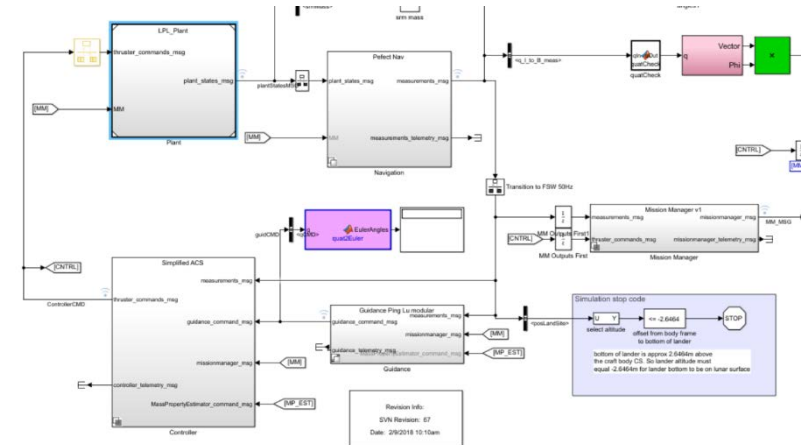
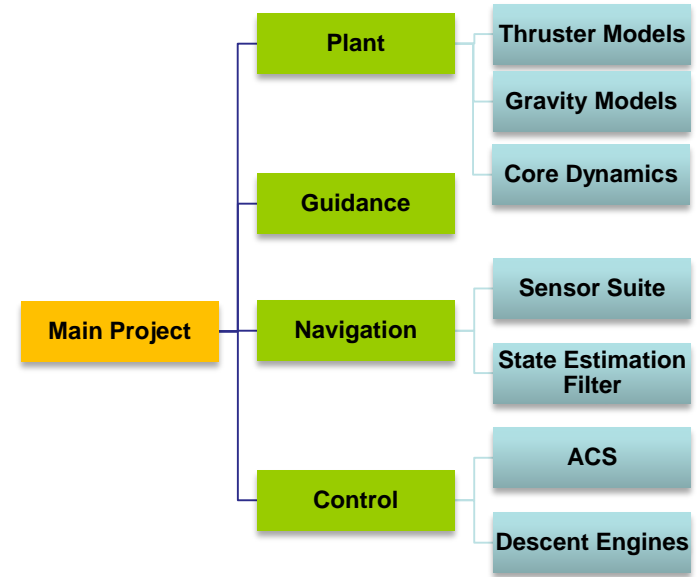
- Descent Engines (DE): 12 x 100 lb
 - Pulsed On/Off to minimize axial velocity error
 - “Water Hammer” effects:
 - All engines On/Off simultaneously causes high-pressure waves on propellant lines and valves
 - Mitigate through staggering the number of DE engines turned On/Off and at a given time
- Attitude Control System (ACS) Engines: 12 x 5 lb
 - Phase-Plane control: On/Off pulsing if attitude or rate error is outside “deadbands”
 - “Off-Pulsing” - Augment ACS control authority by turning Off pairs of DE engines:
 - To counter large torques e.g. due to C.G. offsets
 - Off-Pulsing requires fast-acting propulsion system/valves performance, ~5ms On/Off cycles
 - Off-Pulsing for 5, 10, or 20ms depending on magnitude of control error/disturbance torque



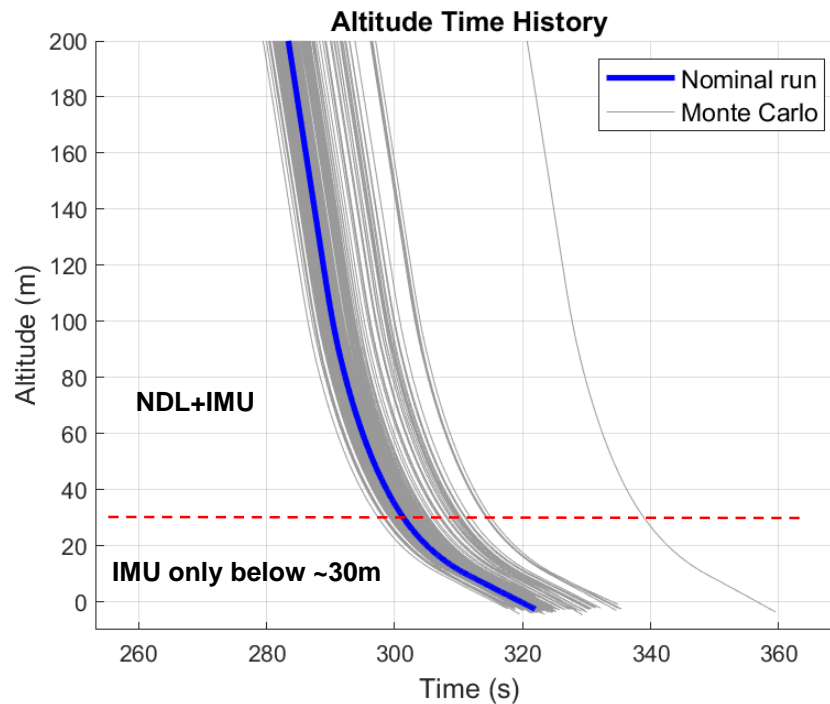
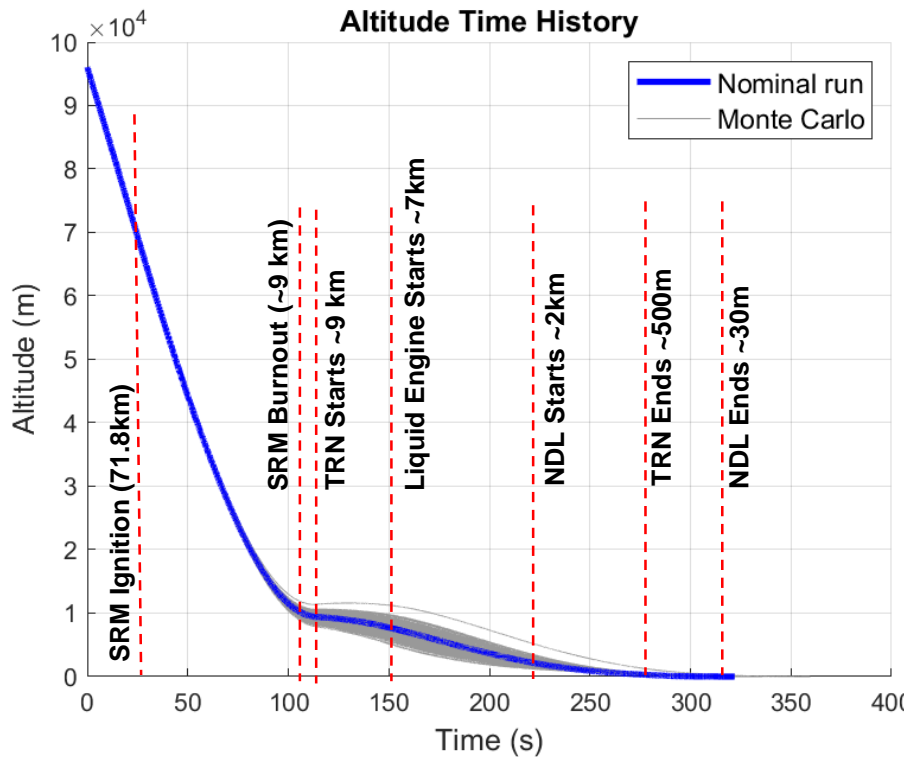
Generic LAnder Simulation in Simulink (GLASS)



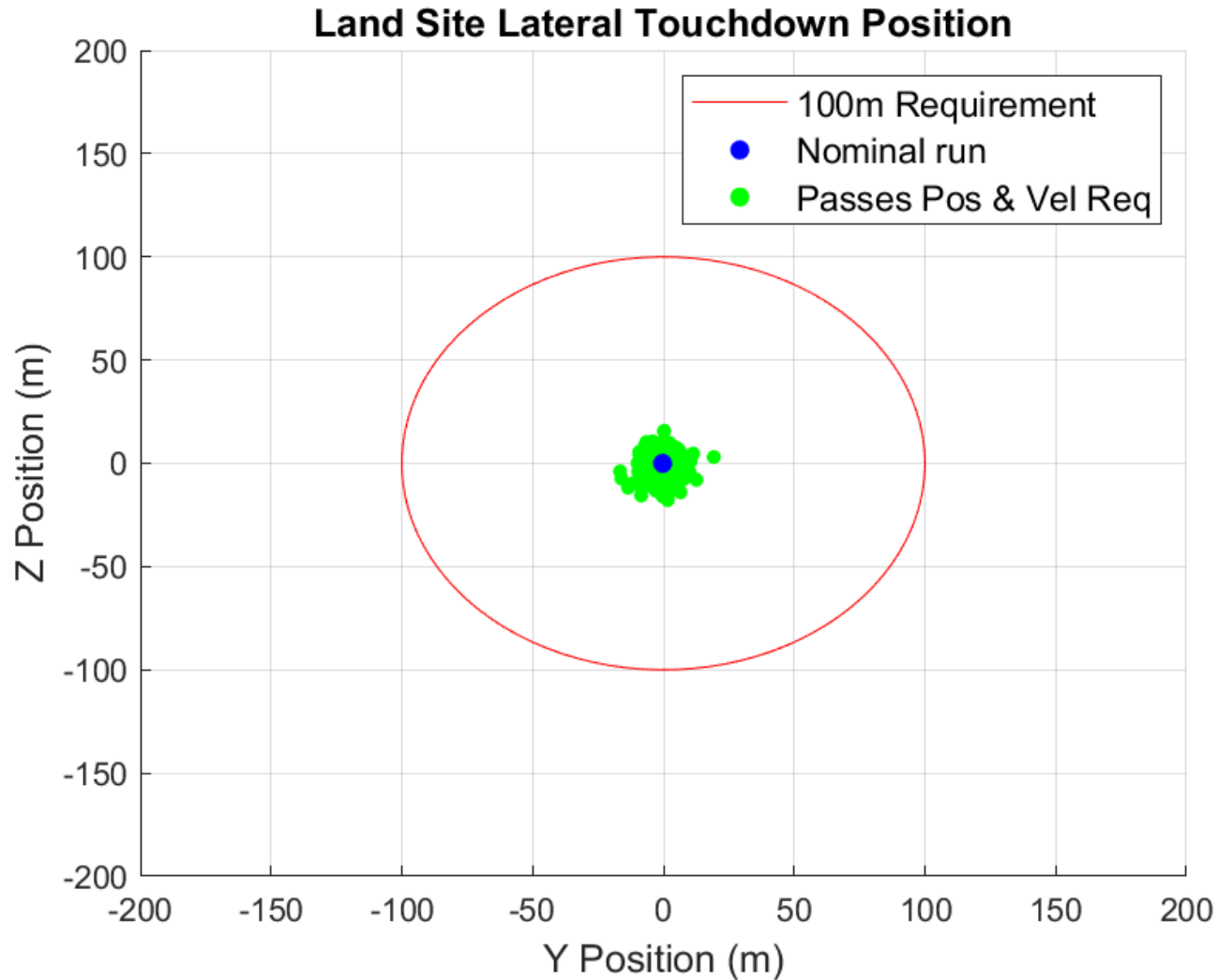
- Lunar Pallet Lander is modeled in the Generic LAnder Simulation in Simulink (GLASS) developed by MSFC
 - Uses Mathworks Simscape Multibody dynamics tool for spacecraft and planetary bodies
 - GLASS is used to develop and autocode GNC software in C language
 - Uses Simulink Projects for high modularity and version control capability
 - Highly focused on Model Based Design approach
 - Interfaces with Core Flight Software cFS
- Using GLASS a 200-Case Monte Carlo dispersed analyses has been conducted to evaluate the lander soft touchdown performance
- Dispersed mass properties, propulsion performance, and sensor error parameters



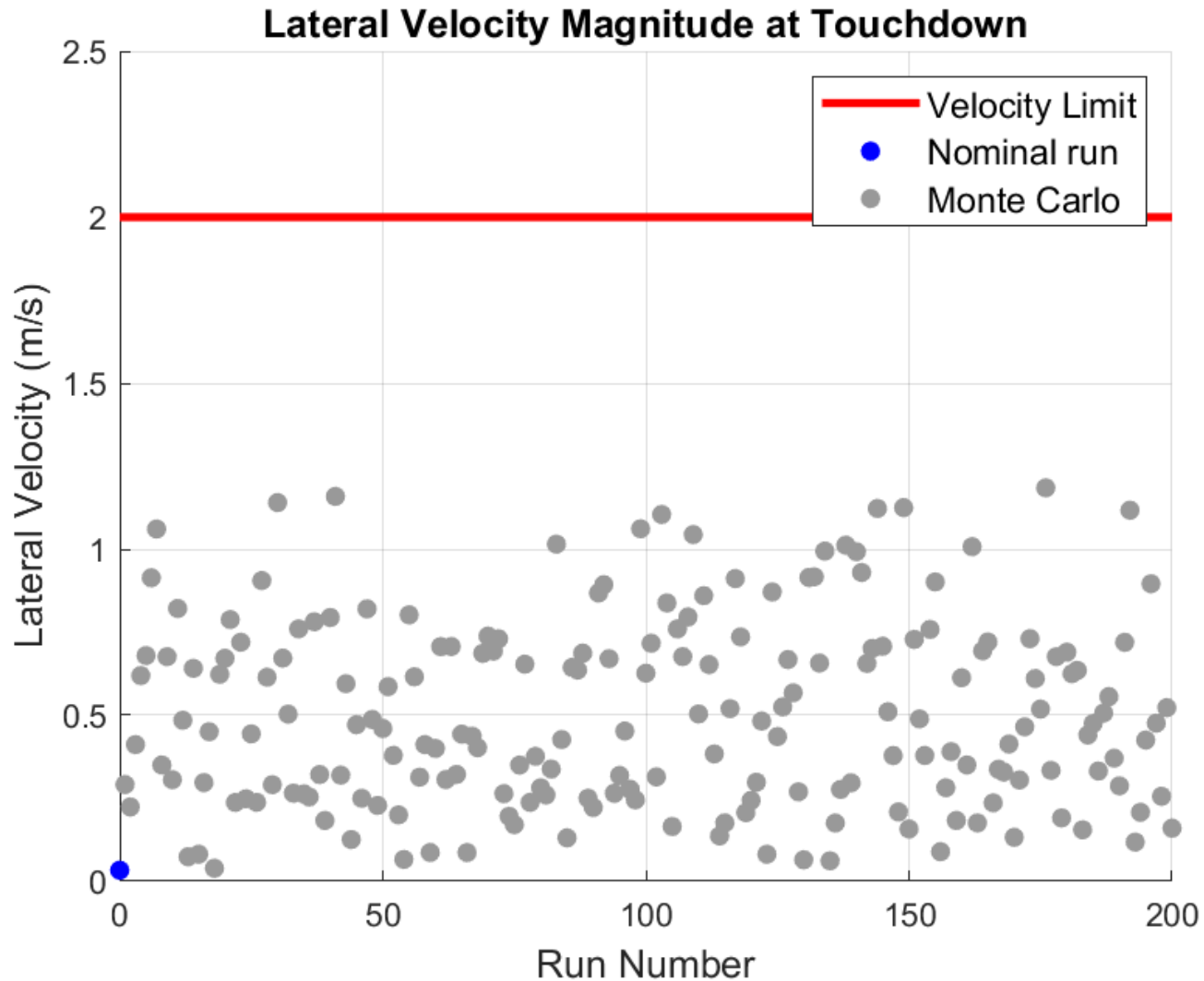
Monte Carlo Results: Altitude



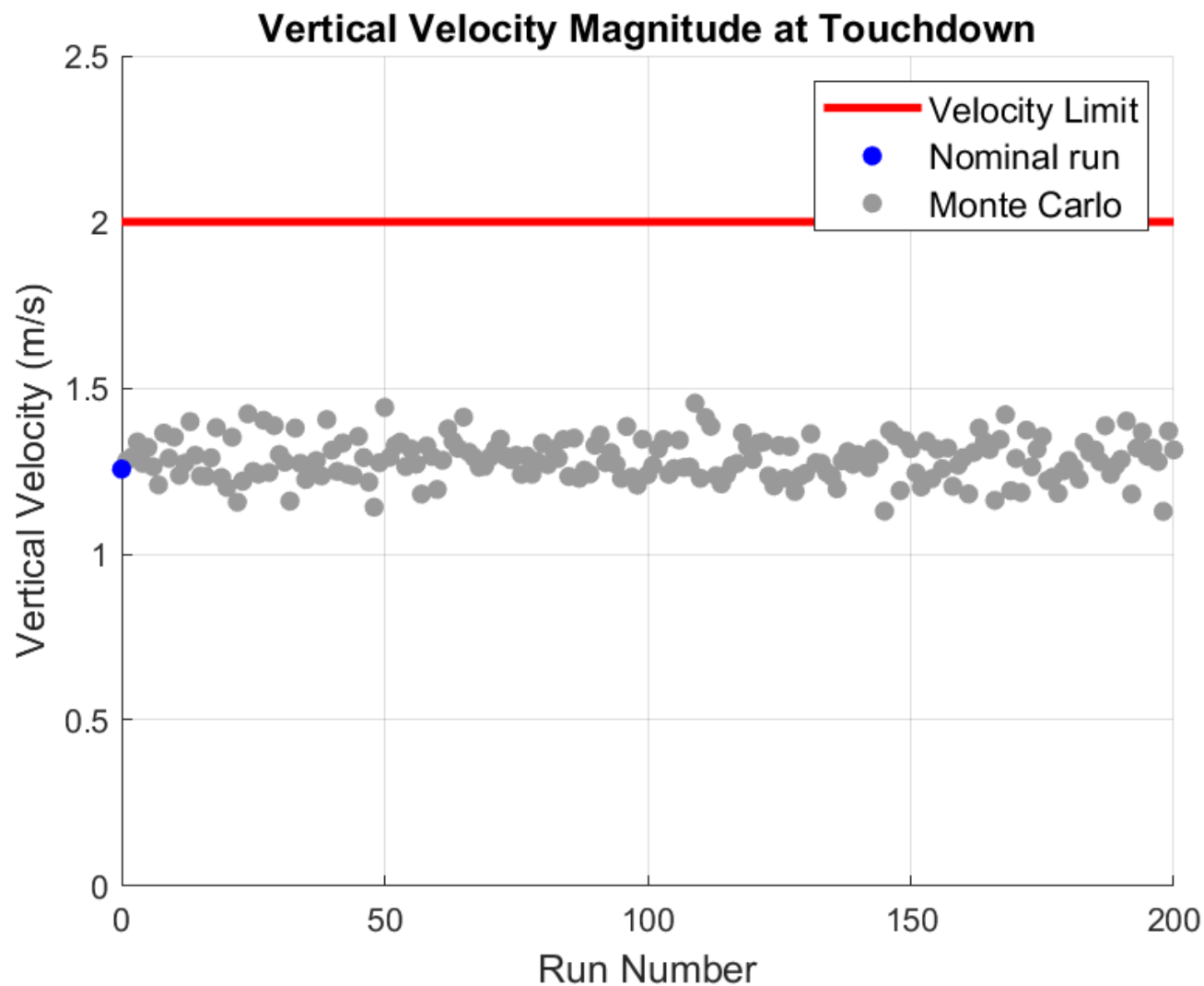
Lateral Position at Touchdown



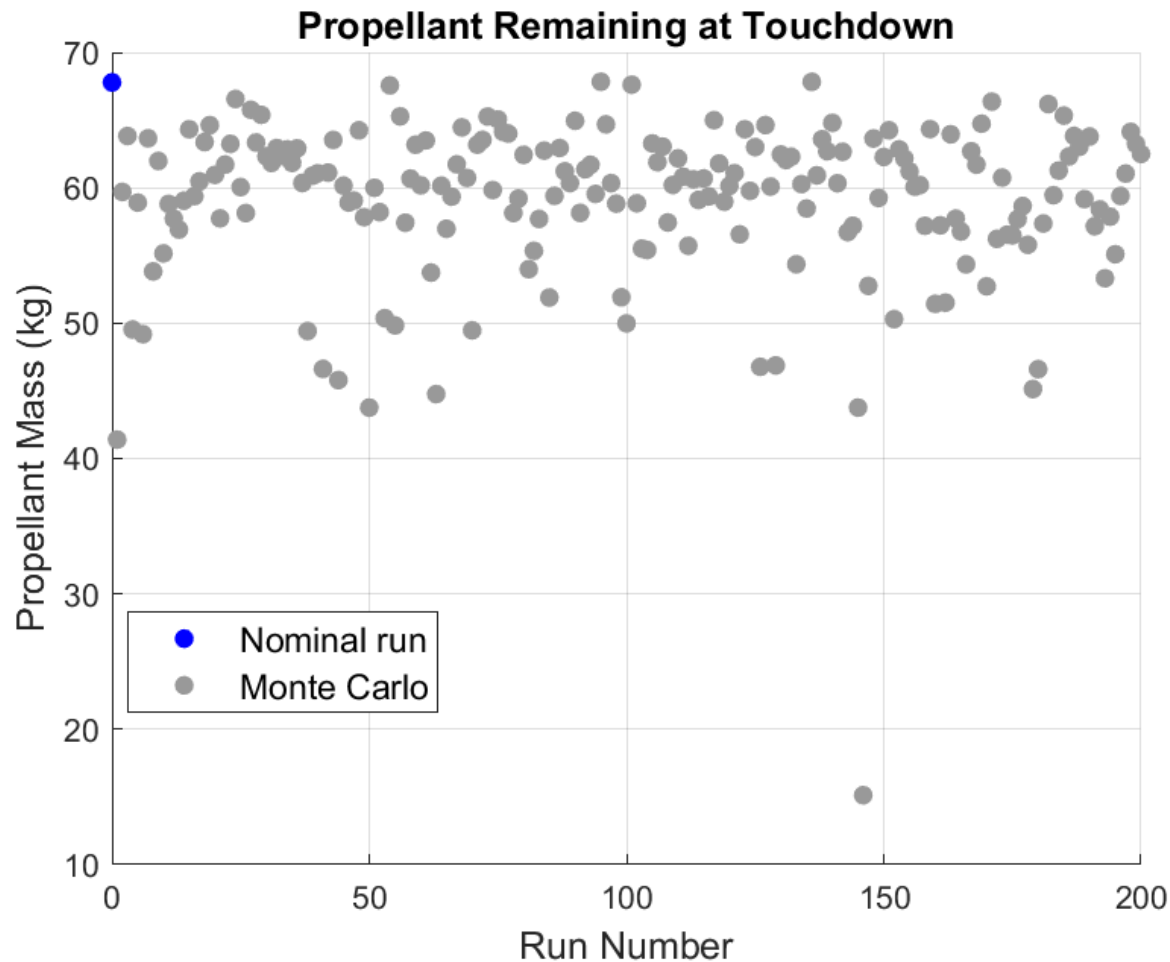
Lateral Velocity at Touchdown



Vertical Velocity at Touchdown



Usable Propellant Remaining



*26.9 kg of unusable propellant remaining onboard

Working towards PDR in the Spring:

- Finalize TRN sensor requirements
- Finalize Nav. trades including lunar “touchdown” detection sensor selection
- Analyze Plume Surface Interaction effects
- Finish evaluation of different Guidance algorithms
- Evaluate alternative control algorithms
- Incorporate vehicle flexible body dynamics and mature propulsion models
- Include SRM separation analysis/effects
- Include Launch vehicle performance into dispersed analysis
- Finalize system-level requirements



Thank you

Thanks to...

Co-Authors:

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And our partners at NASA/JSC and NASA/LaRC

Any questions?