# OPTICAL TELESCOPE ASSEMBLY COST ESTIMATING MODEL 

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## INTRODUCTION

Parametric cost models can be used by designers and project managers to compare cost between major architectural cost drivers and allow high-level design trades; enable cost-benefit analysis for technology development investment; and, provide a basis for estimating total project cost between related concepts. The NASA Marshall Space Flight Center has developed a 5parameter cost model that explains $93 \%$ (Adjusted R2) of the cost variation in a database of 46 total ground and space telescope assemblies. This model can be used to estimate the most probably cost for the Habitable Exoplanet Telescope Assembly.

## DISCLAIMERS

Parametric cost models cannot predict the cost of a future system. They are backward looking. They describe how historical system costs vary as a function of cost estimating relations (CERs) - the most important factors that drive cost. The only forward prediction that a cost model can make is to provide guidance as to how the cost of a potential future system might scale relative to an existing historical system. Furthermore, a parametric cost model is only as good as its database. The fundamental challenge of cost modeling is developing a parametric model that includes the most important CERs. To do this requires a database with sufficient samples and data diversity to yield statistically meaningful results, and engineering judgment to interpret the results. Finally, cost models are statistical. They only provide an estimate of the most likely or $50 \%$ probable cost $+/-$ an uncertainty.

## DEFINITIONS

The MSFC multivariable model estimates the most likely cost for ONLY an Optical Telescope Assembly (OTA). Where an OTA is defined as the subsystem which collects electromagnetic radiation and focuses it (focal) or concentrates it (afocal) into the science instruments. An OTA consists of the primary mirror, secondary mirror, auxiliary optics and support structure (such as optical bench or truss structure, primary support structure, secondary support structure or spiders, straylight baffles, mechanisms for adjusting the optical components, electronics or power systems for operating these mechanisms, etc.). An OTA does not include science instruments or spacecraft

## DATABASE

The MSFC OTA database contains information on 46 different cost programmatic and engineering parameters for 35 space missions with normal incidence optical telescopes or antenna; and 26 ground telescopes or radio antenna. The database consists of both conventional imaging telescopes and non-imaging systems such as spectroscopic missions, LIDAR or radio antenna.

The cost model is developed by regressing over 18 combinations of 8 cost estimating relations (CERs) for 46 OTAs ( 26 Space and 20 Ground). Four CERs were identified as key: Aperture Diameter, Wavelength of Diffraction Limited Performance, Operating Temperature and Year of Development.

| SPACE TELESCOPES |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| rev. 1.001 .18 | $\begin{gathered} \hline \text { Effective } \\ \text { Diameter } \\ {[\mathrm{m}]} \end{gathered}$ | $\begin{gathered} \text { Dififacion } \\ \text { infin } \\ \text { Limin } \\ \text { in } \end{gathered}$ | $\begin{gathered} \hline \text { Operating } \\ \text { Temperature } \\ {[K]} \end{gathered}$ |  |
| Imagios |  |  |  |  |
| ${ }_{\text {ata }}^{\text {ATA }}$ | 2.40 0.00 | 0.78 | ${ }_{\substack{283 \\ 283}}$ | ${ }_{\substack{1992 \\ 1096}}^{\text {cen }}$ |
| Com 1.1 | ${ }^{1.10}$ | ${ }_{0}^{0.65}$ | ${ }_{283}^{283}$ | ${ }_{2097}$ |
| Hesschel | 3.50 | 88.00 | ${ }_{80}$ | 2201 |
|  | ${ }_{\substack{240 \\ 0.5 \\ 0.0}}$ | 0.50 <br> 8.80 <br> 80 | ${ }^{294}$ | ${ }_{\substack{1997 \\ 1077}}^{107}$ |
| INST | ${ }_{6} 6.20$ | ${ }^{\text {200 }}$ | 50 | ${ }_{2006}$ |
| Kepler | ${ }_{1}^{1.40}{ }_{0}$ | 1.00 <br> 05 | ${ }^{213}$ | $\underset{\substack{2001 \\ 1096}}{ }$ |
| MROO HiRISE | $\stackrel{0.50}{0.50}$ | O.35 0.40 0.20 |  |  |
| 000.2/ / CP | 0.61 | ${ }^{1.50}$ | ${ }_{300}^{30}$ |  |
| $0 \mathrm{OAO}, 3 / \mathrm{PEP}$ | 0.80 | 240 | ${ }_{28,5}$ |  |
| Palank | 1.70 | ${ }^{300.00}$ | ${ }^{40}$ | 2001 |
| Propictar | 2.40 | 0.60 | ${ }^{300}$ | 2012 |
| Spiuer | ${ }_{0}^{0.85}$ | 6.50 | ${ }^{5.5}$ |  |
| WIRE | 0.30 | ${ }^{24.00}$ | 12 | ${ }^{1995}$ |
| WMSE | +, |  | ${ }_{60}^{17}$ | ${ }_{\substack{2002 \\ 1096}}^{\substack{20}}$ |
| ${ }_{\text {Normaming }}$ |  |  |  |  |
| ${ }_{\text {chers }}^{\text {Cowlder }}$ | $\frac{3.97}{1.85}$ | 1950.00 <br> 13000 <br> 1000 | ${ }_{\substack{263 \\ 200}}^{\substack{20}}$ | ${ }_{\text {cose }}^{\substack{1984 \\ 2000}}$ |
| ${ }_{\text {catlex }}$ | ${ }_{0}^{0.50}$ | ${ }_{8000}$ | ${ }^{273}$ |  |
| ICESat | ${ }^{1.00}$ | ${ }^{8.00}$ | ${ }^{283}$ | ${ }^{1998}$ |
| Mo MOLA | ${ }_{0} 0.50$ | 3.500 | ${ }_{223}^{283}$ | ${ }_{1986}^{1936}$ |
| $\mathrm{OAO}_{\text {O/ } / \text { / GPP }}$ | 0.97 | 5.00 | ${ }^{289}$ |  |
| swas | ${ }^{0.68}$ | ${ }_{28,00}^{200}$ | ${ }_{10} 10$ | 193 |


| GROUND TELESCOPES |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| rev. 11.012018 | $\begin{gathered} \hline \text { Effective } \\ \text { Diameter } \\ {[\mathrm{m}]} \end{gathered}$ | $\begin{gathered} \text { Diffration } \\ \text { Linion } \\ \text { ind } \end{gathered}$ | $\begin{gathered} \text { Operating } \\ \text { Temperature } \\ {[\mathrm{K}]} \end{gathered}$ |  |
| јкт | 1.00 | 1.00 | 270.00 | 197 |
| Commercial |  | ${ }_{0}^{0.50}$ | 300.00 | ${ }_{2013}^{2013}$ |
| ${ }_{\text {Slafie }}^{\text {WITN }}$ | $\frac{3}{3.50}$ <br> 3.50 | ${ }_{\text {O }}^{0.93}$ | ${ }_{\text {27e.00 }}^{23}$ | ¢1989 |
| ${ }_{\text {AESOS }}^{\text {AEST }}$ |  | ${ }^{0.85}$ | 27300 27300 | ${ }^{19991}$ |
|  |  | $\stackrel{220}{200}$ | ${ }_{2}^{273.00}$ | - |
| Soak | ${ }_{4.20}^{4.20}$ | ${ }_{6}^{1.10}$ | ${ }_{\text {2 }}^{260.00}$ | ${ }_{1981}^{1981}$ |
| DKIIT | ${ }^{420}$ | ${ }_{0} 0.90$ | 30000 |  |
| T . Sm rephecen | ${ }^{6.50}$ | ${ }^{1.60}$ | 226200 |  |
| ${ }_{\text {Magelima }}^{\text {Comim }}$ | (6.00 ${ }_{\text {c. }}^{8.0}$ | (1.00 | 280,00 | (1994 |
| Stumar | ${ }_{8.30}$ | ${ }_{0}^{0.60}$ | ${ }_{2} 273.00$ | ${ }_{1988}^{1988}$ |
| ${ }_{\text {KECCK }}$ | 10.00 10 | ${ }^{1.00}$ | ${ }^{273.00}$ | ${ }_{1086}^{1986}$ |
| ${ }_{\text {Lem }}^{\text {LbT }}$ | ${ }^{11.88}$ | 0.65 | 273.00 |  |
| KECK-1/dil | ${ }^{14.14}$ | - | ${ }_{\text {27300 }}^{26000}$ | ${ }_{\text {l }}^{\substack{1986 \\ 198}}$ |
| Commercial Radio |  | 210000.00 | 300.00 | 2012 |
| SubMM Amay Dish | ${ }_{6}^{6.00}$ | ${ }^{300.00}$ | ${ }^{300.00}$ | ${ }^{1988}$ |
| Grecen Bank Rasio | 100.00 | ${ }_{650000}$ | ${ }^{300.00}$ | 1991 |


| COST MODEL |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OTA\$ $=\$ 20 \mathrm{M} 30^{(\mathrm{S} / \mathrm{G})} \mathbf{D}^{(1.7)} \lambda^{(-0.5)} \mathbf{T}^{(-0.25)} \mathbf{e}^{(0)}$ |  |  |  |  |  |  |
| Fit value | 19.0 | 30.4 | 1.69 | -0.47 | -0.24 | -0.0274 |
| SE | 1.6 | 6.0 | 0.09 | 0.03 | 0.07 | 0.006 |
| p-value | 5E-7 | 2E-18 | 2E-21 | 1E-20 | 0.002 | 4E-5 |
| Model explains 93\% (Adjusted R2) of the cost variation in the OTA database |  |  |  |  |  |  |
| where: |  |  |  |  |  |  |
| S/G = | $=1$ for Space Missions and 0 for Ground Telescopes. |  |  |  |  |  |
| $\mathrm{D}=$ | = Aperture Diameter |  |  |  |  |  |
| $\lambda=$ | = Wavelength of Diffraction Limited Performance (UV is more expensive) |  |  |  |  |  |
| $\mathrm{T}=$ | = Operating Temperature (Cryo is more expensive) |  |  |  |  |  |
| $\mathrm{Y}=$ | = Year of Development (Cost reduces by 50\% approx. every 25 years) |  |  |  |  |  |

NOTE:

- Model predicts ONLY the MOST PROBABLE or $50 \%$ cost.
- The prediction uncertainty is $45 \%$.
- Thus to get the $84 \%$ most probably cost, multiply by 1.45 X .


## Residual Analysis

The below graphic illustrates the residual error of the model. Each column shows cost versus CER. The top row is the 'raw' database date. Row two is after normalizing cost by diameter. Row three is after normalizing cost by wavelength. Row four is after including temperature and YOD normalization
And, row five is after invoking ground to space multiplier.


## OTA COST ESTIMATION EXAMPLE

OTA cost can be estimated via two methods: using the model directly or using model to compare relative cost with other OTAs (i.e. Hubble \& JWST).

For an OTA with:

- 4 m diameter
- $0.4 \mu \mathrm{~m}$ diffraction limit
- 270 K operating temperature
- 2025 year of development

Direct Model Method
OTA $\$(50 \%$ probable $)=\$ 430 \mathrm{M}$
$=\$ 20 \mathrm{M} \times 30 \times(4)^{(1.7)} \times(.4)^{(-0.5)} \times(270)^{(-0.25)} \times \mathrm{e}^{(-0.027)(2025-1960)}$
OTA\$ $(84 \%$ probable $)=\$ 620 \mathrm{M}$

## SUB-SYSTEM COST

Average cost breakdown for 14 missions is: payload $\sim 33 \%$, spacecraft $\sim 33 \%$, labor $\sim 25 \%$; (Instruments + Spacecraft $\sim 50 \%$ ).
Analysis based on Cost Analysis Data Requirements (CADRe) reports for 14 missions: CALIPSO, CLOUDSAT, GALEX ICESAT, JWST, Kepler, LANDSAT-7, Spitzer, STEREO, SWAS, TRACE WIRE, WISE and WMAP.

Relative Comparison Method
$\underset{\substack{\text { Total Cost }[\mathrm{FY17} \text { SM] } \\ \text { Dianeter }[\text { meter }]}}{\text { WDP }}$ $\underset{\text { WDIP [micrometer] }}{\text { Temperature }[\text { K }]}$ $\underset{\substack{\text { Temperature } \\ \text { exp } \\ \text { [K] } \\ \text { (KOD) }}}{ }$
 ${ }_{85 \%}^{50 \% \text { Prediciceded Cost } \operatorname{Cost}[\mathrm{FY17} 77 \mathrm{SM}]}$

Total Cost [FY17 SM]
Diameter [meter] WDIP [micrometer] Temperature $[\mathrm{K}]$
$\exp ($ YOD $)$ $\exp$ (YOD)
$50 \%$ Predicte 50\% Predicted Cost [FY17 SM]
$85 \%$ Predicted Cost [FY17 SM]


Average Mission WBS Distribution


