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DIGITAL BEAMFORMING BASED RFI MITIGATION FOR SYNTHETIC APERTURE RADAR

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Motivation



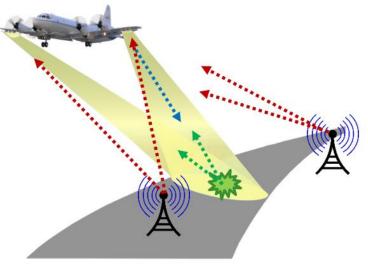
What is the problem?

Definition Radio Frequency Interference:

Radio frequency interference is the conduction or radiation of radio frequency energy that causes an electronic or electrical device to produce noise that typically interferes with the function of an adjacent device.

SAR transmits signal and measures:

- signal reflection from ground targets (wanted)
- signals of other RF instruments (unwanted)



Frequency spectrum is limited resource and shared with other users

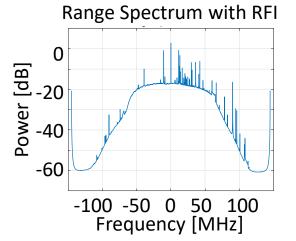


Motivation



What has been done so far?

Notching:



- + Fast processing
- Loss of SAR signal
- Distortion of Impulse Response Function (IRF)

- Coherent Subtraction:
 - 1. Modelling of RFI based on <u>a priori</u> information
 - 2. Coherent subtraction from data
- Filtering:
 - e.g. Adaptive Least Mean Square Filter

- + No distortions
- + SAR signal preserved
- Depends on model and RFI
- + No distortions
- + SAR signal preserved
- Depends on filter parameters and on SAR-RFI-Ratio

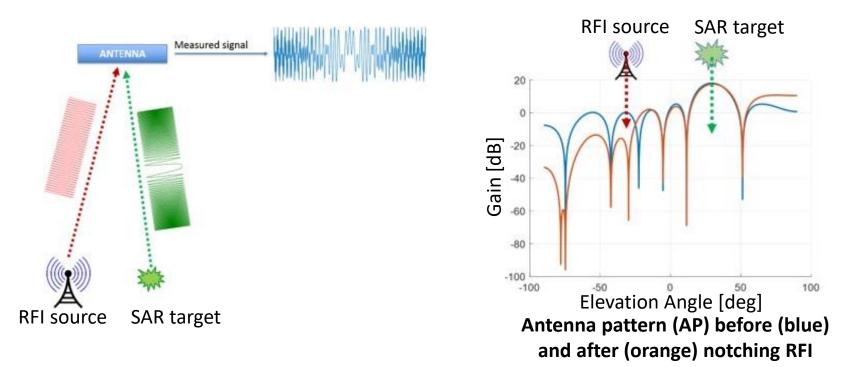
Can we use Digital Beamforming to suppress RFI?



Digital Beamforming



The idea



- SAR and RFI signal overlap at antenna → indistinguishable after antenna
- Spatial filtering of interferences with antenna pattern before overlapping
- Direction of RFI estimated from data after receive \rightarrow digital beamforming

What are the limitations and assumptions?



Digital Beamforming



Limitations and assumptions

Limitations

- An array with N active channels can only notch up to N-1 directions
- RFI from the same angular direction as the instantaneous SAR signal can not be separated and remains in image (conventional filtering necessary, e.g. blanking out)

Assumptions

Received signal is neither saturated nor at non-linear operating point

How can we automatically notch RFI? How many RFI sources can we notch for given N? How well can we notch RFI inside the swath?



Automatic RFI Notching



MVDR Beamformer

The Minimum Variance Distortionless Response (MVDR) Beamformer that maximizes SINR is subject to

$$w^H a(\theta_d) = 1$$

min $w^H R w$

w: steering weights $a(\theta)$: steering vector θ_d : desired signal direction R: Interference-Noise-Covariance (INC) Matrix

and has the optimal solution

$$w = \frac{R^{-1}a(\theta_d)}{a(\theta_d)^* R^{-1}a(\theta_d)}$$

Problem: we can only estimate sample covariance that contains SAR signal



Automatic RFI Notching



INC Estimation

The Capon Power Spectrum estimates the signal power arriving from a certain angular direction

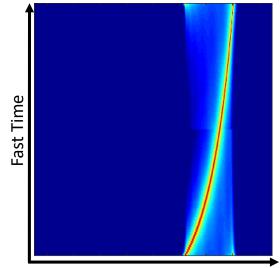
$$P(\theta) = \frac{1}{a^{H}(\theta) R_{S}^{-1} a(\theta)}$$

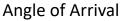
 R_s : Sample Covariance Matrix

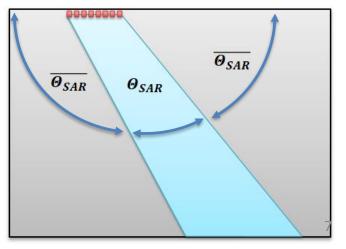
The INC in the presence of the SAR signal is estimated by integrating steering vector covariances weighted by the respective Capon Power Spectrum

$$R = \int_{\overline{\Theta_{SAR}}} \frac{a(\theta)a^{H}(\theta)}{a^{H}(\theta)R_{S}^{-1}a(\theta)} d\theta$$

Capon Power Spectrum of Range-Compressed SAR signal





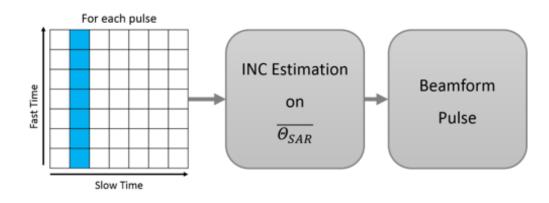




Adaptive Notching

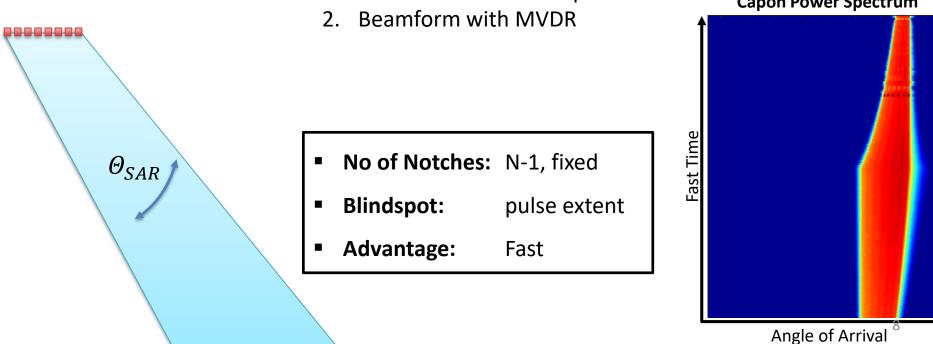


Pulse-Wise



1. Estimate INC for each pulse

Capon Power Spectrum

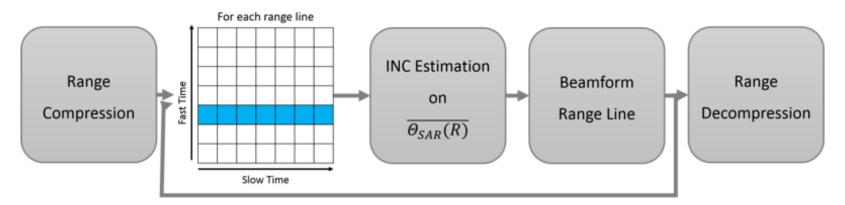


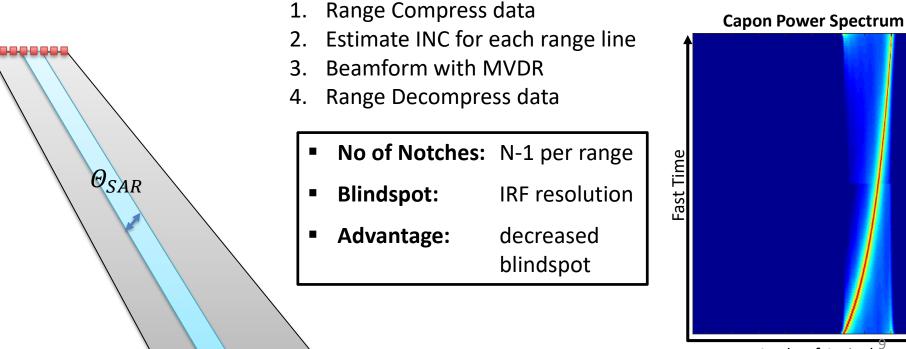


Adaptive Notching



Range-Dependent Time MVDR





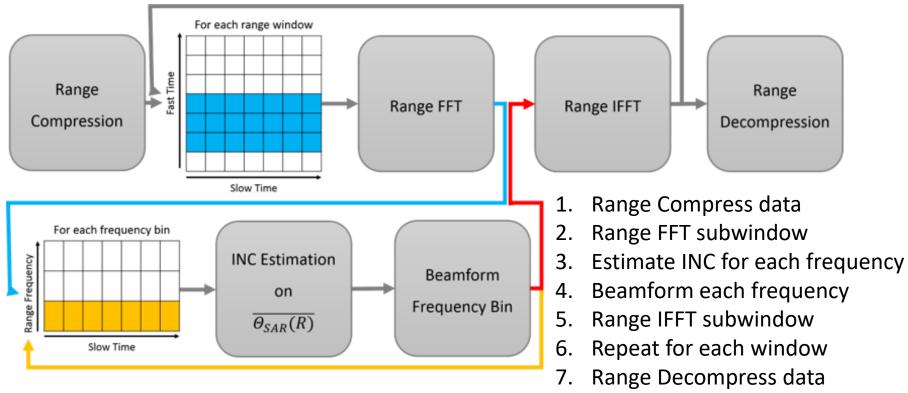
Angle of Arrival



Adaptive Notching



Range-Dependent Frequency MVDR



- **No of Notches:** N-1 per range and frequency bin
- Blindspot: IRF resolution of subwindow
- Advantage: frequency dependent notching can improve performance at cost of processing power



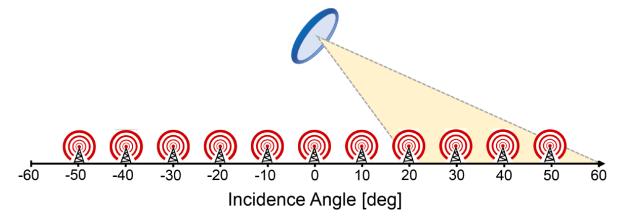
Simulations



Airborne SAR Parameters

Number of antenna elements N	2 - 64
Antenna element separation d	0.5 wavelength
Center frequency f	435 MHz
Sampling frequency	290 MHz
Pulse Bandwidth	120 MHz
Pulse Duration	20 microseconds
SAR Target locations	21 to 60 deg

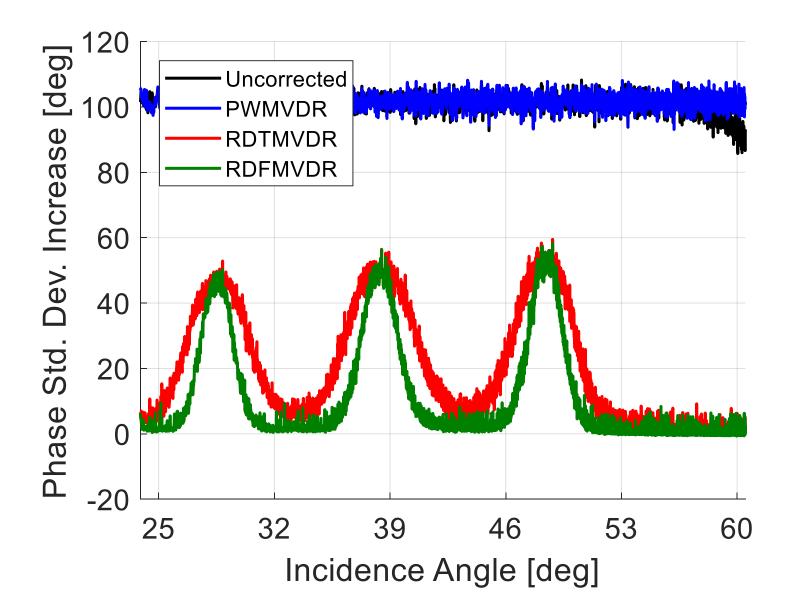
11 Interferers from -50deg to +50deg, 10 degree spacing, f=375MHz to 425MHz with 5MHz spacing





N = 16, RFI-Noise-Ratio = 40 dB

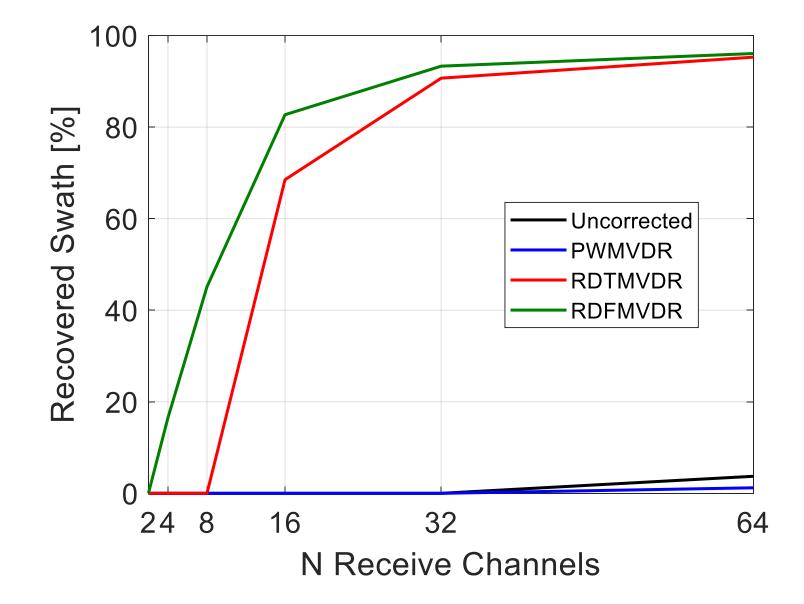






Percentage of Swath Recovered







About EcoSAR



- Two fully polarimetric, nadir-looking antennas (one per wing) for single-pass interferometry
- 32-channel (8 elements, 2 antennas, 2 polarizations)
- Beamforming architecture enables across-track scanning with customized Tx and Rx beams over a range of +-45 degrees.

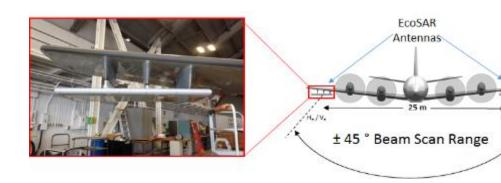


Center Frequency	435 MHz	Pulse Length	1 usec – 50 usec
Maximum Bandwidth	200 MHz	Array Peak Power	40 Watts
Polarization	HH, VV, VH,HV	PRF	100 Hz – 10 KHz
Polarization Isolation	> 30 dB	Swath	4 km – 8 km
NESZ	- 41 dB	Finest Range Resolution	0.75 m
Total Number of active Channels	32	Single Look Azimuth Resolution	0.5 m
Interferometric baseline	25 m	Vertical Accuracy	~ 1 m



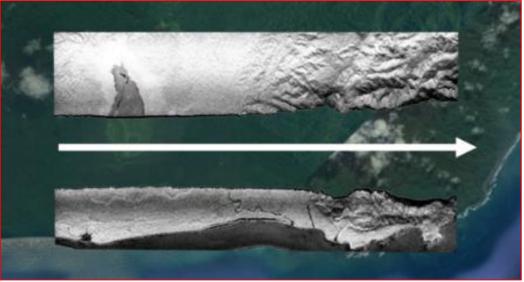
Application to measured EcoSAR data





Center Frequency	479MHz
Bandwidth	20MHz
Pulse Length	10usec
PRF	690Hz
Physical Baseline	25m
Polarization	НН
Antenna Elements	8
Antenna Spacing	29cm

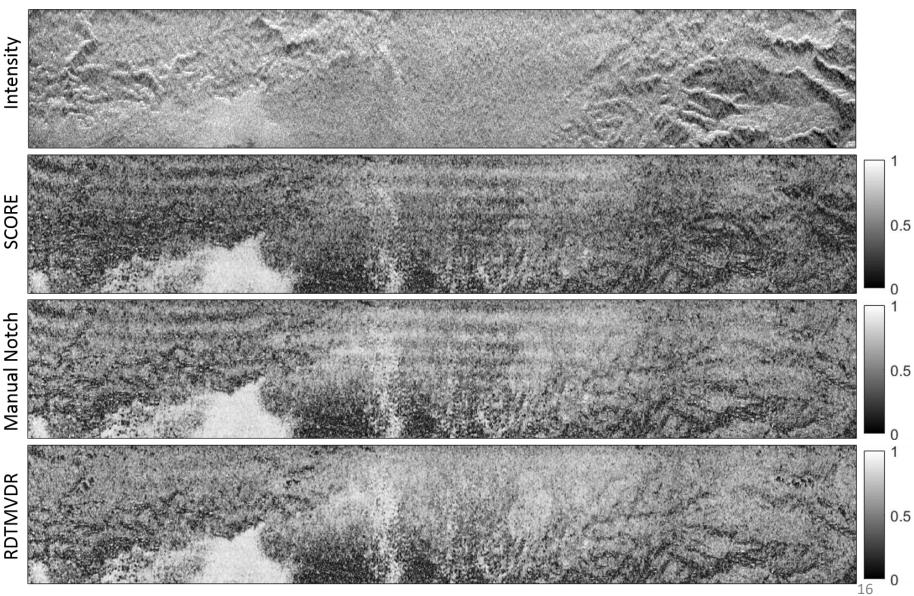




Application to measured EcoSAR data



Intensity and coherence images for different antenna patterns

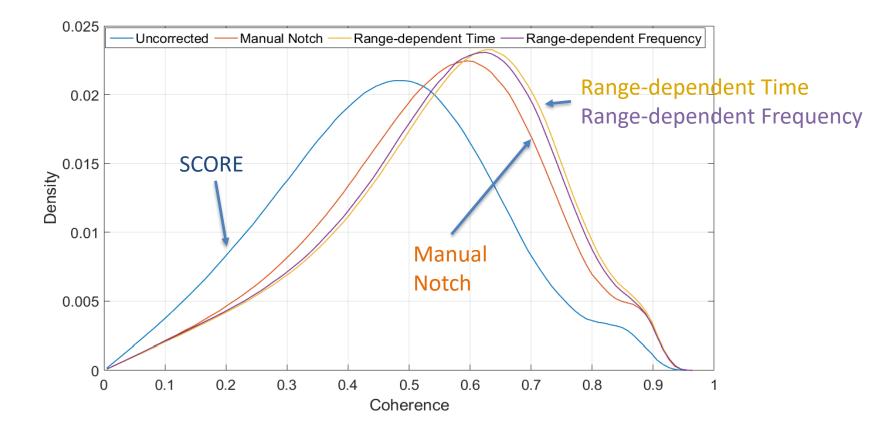


SCORE: Scan-on-Receive only, Manual Notch: Placement of wide notch at negative steering angle, RDTMVDR: Range-Dependent Time MVDR





Histogram peak shifts from 0.48 (uncorrected) to 0.62 (RDTMVDR)





Conclusion



- Spatial distribution of SAR signal that is inherent to imaging geometry can be used to notch RFI with DBF
- Range Dependent Frequency MVDR showed best performance in simulations (e.g. interferers in swath)
- Performance of Range Dependent Time MVDR similar for RFI Mitigation in EcoSAR data

Outlook

 Multiple azimuth channels can utilize spatial SAR signal distribution in range-doppler domain