

A Layered SAW Device Based on ZnO/LiTaO₃ for Liquid Media Sensing Applications

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Abstract – Surface Acoustic Wave (SAW) sensors comprising a zinc oxide guiding layer deposited on a 36°-YX lithium tantalate substrate were developed. They were found to have greater mass sensitivity than other LiTaO₃ based SAW sensors, such as the SiO₂/LiTaO₃ configuration. In this paper, the fabrication of the ZnO/LiTaO₃ sensor is described and micro-characterisation of the deposited films is presented. Sensitivity of these devices to surface mass and dielectric perturbations is then presented, followed by an analysis of temperature stability.

I. INTRODUCTION

90° rotated ST-quartz and 36°-YX LiTaO₃ substrates are the most commonly utilised piezoelectric materials which allow the propagation of shear waves. As a result, they are suitable for use in liquid sensing applications. By depositing a wave guiding layer onto such substrates, mass sensitivity can be increased as the acoustic waves are more confined onto the surface.

Layered SAW sensors for liquid media applications using SiO₂ on 90° rotated ST-quartz have been intensively studied (eg. Kovacs et al [1] and Du et al [2]). SiO₂ on 36° YX-LiTaO₃ layered structure is another SAW structure that offers potential for liquid sensing applications [3, 4]. However, such devices have relatively lower sensitivity than devices based on ST cut quartz.

Adding a piezoelectric guiding layer generally increases the mass sensitivity. It has been shown that replacing the SiO₂ layer with ZnO, which is a piezoelectric material, results in considerable improvements in mass sensitivity [5]. In this paper, a ZnO/36° YX-LiTaO₃ structure is introduced for sensing applications.

Shoji et al. [6, 7] showed that deposition of ZnO layer on LiNbO₃ or LiTaO₃ results in an improved electromechanical coupling coefficient (K^2), whilst Lim and Shindo [8] studied the defects in ZnO deposited on LiTaO₃ by electron cyclotron resonance-assisted molecular-beam epitaxy (ECR-assisted MBE). In this paper, it will be shown that the deposition of ZnO on LiTaO₃ can be used in the fabrication of a liquid media sensor with improved mass sensitivity.

II. SENSOR FABRICATION

The sensor consisted of a two-port resonator with 38 input and output Inter Digital Transducer (IDT) finger pairs, 160 reflectors on each side, 700µm aperture width and a periodicity of 40µm. A 2-port resonator structure was chosen over a delay line as its higher phase slope increases oscillation stability. The IDTs and reflectors were formed by patterning a 300nm Au layer. The Au layer was deposited upon 300nm Ni/300nm Ti for improved adhesion to the substrate. Devices were fabricated with ZnO layer thickness of 1.5µm and 2.6µm, deposited by an RF magnetron sputterer. Sputtering gas was 40% O₂ in Ar at 1×10^{-2} Torr, substrate temperature was 260°C, which resulted in a deposition rate of ~0.4µm/hour. For comparison, transducers with 3µm SiO₂ were also fabricated.

III. MATERIAL ANALYSIS

ZnO films were micro-characterised using Scanning Electron Microscopy (SEM) and X-Ray Diffraction (XRD). Figure 1 shows the SEM micrograph of the film at the edge of an IDT finger. It can be seen that grain structure is quite different on the metallised and non-metallised regions.

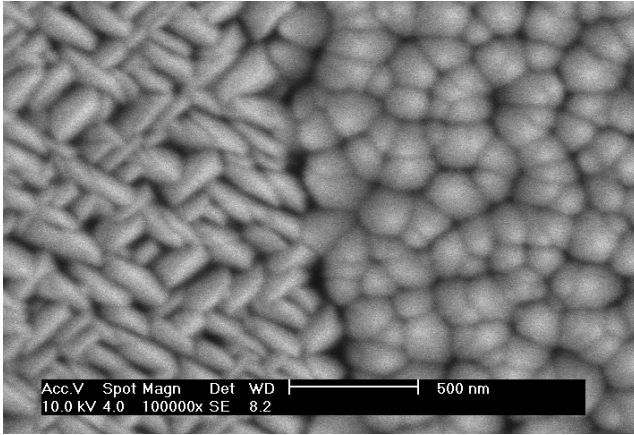


Figure 1: Micrograph ZnO on LiTaO₃ (left) and Au (right)

It has previously been reported that ZnO deposited by ECR-assisted MBE grows on LiTaO₃ with *c*-axis alignment parallel to the surface [6]. To confirm that the same relative orientation of thin film and substrate had been achieved with deposition conditions described in section II, a sample with no metal layer was subjected to XRD analysis. The results are presented in Figure 2. The strong (110) peak indicates that the *c*-axis lies in the plane of the substrate. A smaller (102) peak is also present, but is dominated by the (110) peak. Diffraction angles for crystal orientations have been taken from [6], [10], [11].

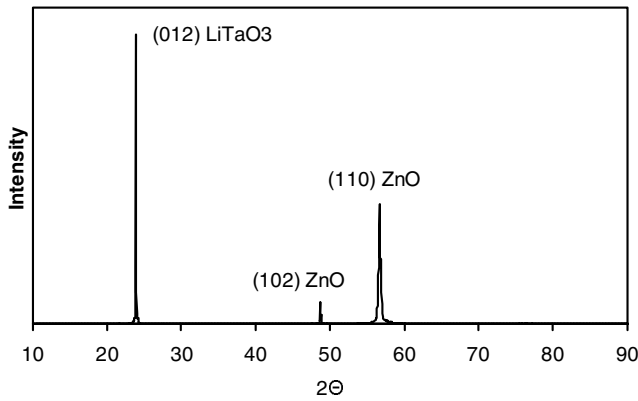


Figure 2: XRD pattern of ZnO on LiTaO₃

The orientation of ZnO on Au under similar sputtering conditions has previously been reported by the authors [2] as showing a strong (002) peak, and a grain formation similar to that on the right side of

Figure 1. This is indicative of strong surface-normal *c*-axis alignment.

IV. MASS SENSITIVITY ANALYSIS

To compare the mass sensitivity of the devices with SiO₂ and ZnO layers, a 0.4μm layer of the polymer APC (Poly(Bisphenol A carbonate)) was spin coated onto the surface of each SAW device. The frequency shift was measured on a network analyser, and taken as the change at the point of maximum phase slope. From [12], the change in velocity due to mass loading is known to be

$$\frac{\Delta V}{V} = \frac{V h v_2^2}{4P} \left(\rho - \frac{c_{44}}{V^2} \right), \quad (1)$$

where *V* is the SAW phase velocity, *h* is the thickness of the perturbing layer, ρ and *c*₄₄ are density and shear stiffness of the film respectively, *P* is the power flow per unit width, and *v*₂ is the particle velocity of the horizontally polarised shear wave. This equation was derived from perturbation theory, using the weak coupling assumption. This is invalid for a strong piezoelectric material such as LiTaO₃. However, it is assumed here that the qualitative results are still valid.

Table I: Frequency Response to Polymer Layer

Device	Frequency Shift
1.5μm ZnO	250kHz
2.6μm ZnO	500kHz
3μm SiO ₂	300kHz

Table I shows that a 2.6μm ZnO device is approximately 1.6 times as sensitive as a 3μm SiO₂ device. For comparison, the results of Hermann et al. [3] indicate a sensitivity of 0.5×10⁻⁸m²s/kg/Hz for a 36° YX-LiTaO₃ device with periodicity of 40μm and a 3μm SiO₂ layer. It was also noted that further sensitivity improvement could be gained by increasing the thickness of the SiO₂ layer, however further research needs to be undertaken to determine if this is also the case for a ZnO layer.

V. LIQUID SENSITIVITY ANALYSIS

SAW devices show frequency shift when exposed to different liquids. This is usually due to a combination of viscosity, conductivity and permittivity effects upon the wave propagation.

To assess the response of the SAW devices in liquid media, they were placed within a 6 μ l flow cell. To obtain maximum sensitivity, and to minimise the effects of variable gasket pressure or leakage, the flow cell covered the entire structure, including IDTs and reflectors. This has the disadvantage that input and output impedance will be affected, which has the potential to prevent oscillation [13].

A pump with a flow rate of 250 μ L/min supplied DI-water to the surface of the sensor. The sample was injected into a 500 μ L sample loop and switched into the flow path. Figure 3 shows the response of the three devices when exposed to methanol.

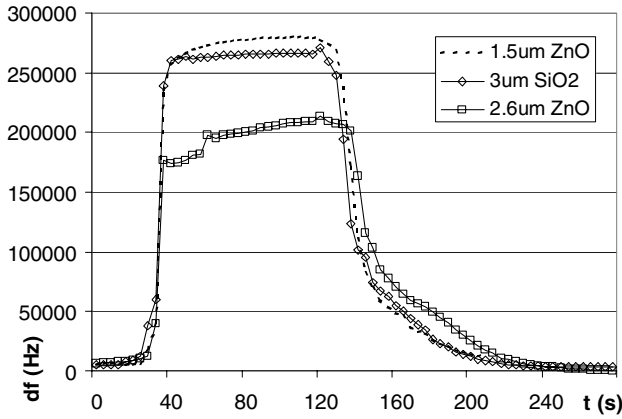


Figure 3: Responses to Methanol

The response is due to the lower dielectric constant and viscosity of methanol compared to water (see Table II). The perturbation relations [12] for velocity shift due to the electrical and mechanical properties of a liquid are respectively

$$\frac{\Delta V}{V} = \frac{K^2}{2} \frac{(\sigma'/\omega)^2 + \epsilon_0(\epsilon_r' - \epsilon_r)(\epsilon_r' \epsilon_0 + \epsilon_p^T)}{(\sigma'/\omega)^2 + (\epsilon_r' \epsilon_0 + \epsilon_p^T)^2} \quad (2)$$

$$\frac{\Delta V}{V} = \frac{V_{V_2}^2}{4\omega P} \left(\sqrt{\frac{\omega \eta' \rho_l'}{2}} + \sqrt{\frac{\omega \eta \rho_l}{2}} \right), \quad (3)$$

where σ is the conductivity, ϵ_r is the relative permittivity, η is the viscosity and ρ_l is the density of the liquid. Quantities denoted by ' indicate the perturbing liquid (methanol), while others indicate the water. It is most likely that the dominant effect is the change in dielectric constant, since this sensitivity is

proportional to K^2 . It has been shown that K^2 is higher for the 1.5 μ m ZnO device than the 2.6 μ m ZnO device [7].

Table II: Properties of Methanol and Water

	ϵ_r	η (mPa s)
Water	80	1
Methanol	33	0.58

This shows that with an appropriate choice of ZnO layer thickness, it is possible to increase the mass sensitivity, whilst reducing cross-sensitivity due to dielectric constant and viscosity change.

VI. TEMPERATURE COEFFICIENT

For dispersive SAW devices, including any with layered structure or reflectors, the magnitude of the temperature coefficient of delay (TCD) and temperature coefficient of frequency (TCF) are not identical. Instead, the relationship is [8]

$$TCF = -\frac{v_g}{V} TCD, \quad (4)$$

where v_g is the group velocity of the acoustic wave.

To measure TCF, the sensors were placed within an environmental chamber, with the remainder of the oscillator system being kept outside. Figure 4 shows a typical plot of fractional frequency deviation versus temperature for a device with 2.6 μ m ZnO layer. It can be seen that it is highly linear over a broad range of frequencies, and gives a TCF of -40ppm/K. It was observed that a change in cable lengths between the SAW and amplifier, or an adjustment of the phase shift network, which alters the oscillation frequency, could have a strong impact upon the TCF. Variation was observed over repeated measurement. Since the SAW devices were not hermetically sealed, it is possible that humidity variation caused some additional error.

Table III: TCF of SAW devices

Device	TCF (ppm/K)	Variation (ppm/K)
1.5 μ m ZnO	-22	± 6
2.6 μ m ZnO	-40	± 4
3 μ m SiO ₂	-25	± 4

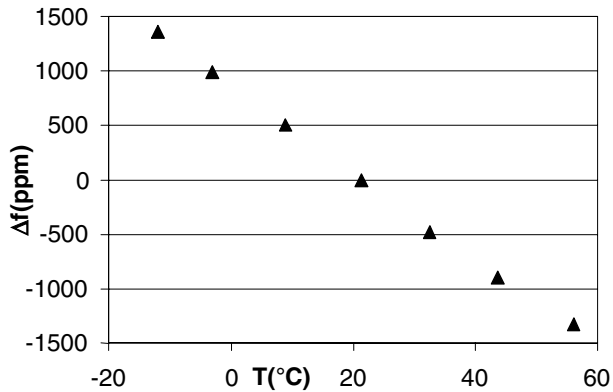


Figure 4: Frequency deviation vs. temperature for 2.6 μm ZnO device.

It can be seen that the TCF of the devices with ZnO layer is inferior to that of the SiO₂ devices. This is due to the opposite signs of the TCD of SiO₂ and 36° YX-LiTaO₃ having a cancelling effect.

VII. CONCLUSION AND FUTURE WORK

Mass sensitivity of the 36° YX-LiTaO₃ devices with 1.5 μm ZnO, 2.6 μm ZnO and 3 μm SiO₂ layers were compared. It was shown that mass sensitivity of the 2.6 μm ZnO device is 1.6 times that of the 3 μm SiO₂ device, however it suffers from a higher temperature sensitivity. The response to a change in liquid on the surface was measured, and it was found that the 1.5 μm ZnO and 3 μm SiO₂ devices had a similar response, which was about 1.3 times that of the 2.4 μm ZnO device.

For liquid sensing application, it is proposed to use an SiO₂ or polymer protective layer to ensure that ZnO does not react with any acidic materials within the liquid. Work will be carried out by the authors to model the behaviour of sensors based on ZnO/LiTaO₃, and to apply them to chemical and biochemical sensing applications.

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