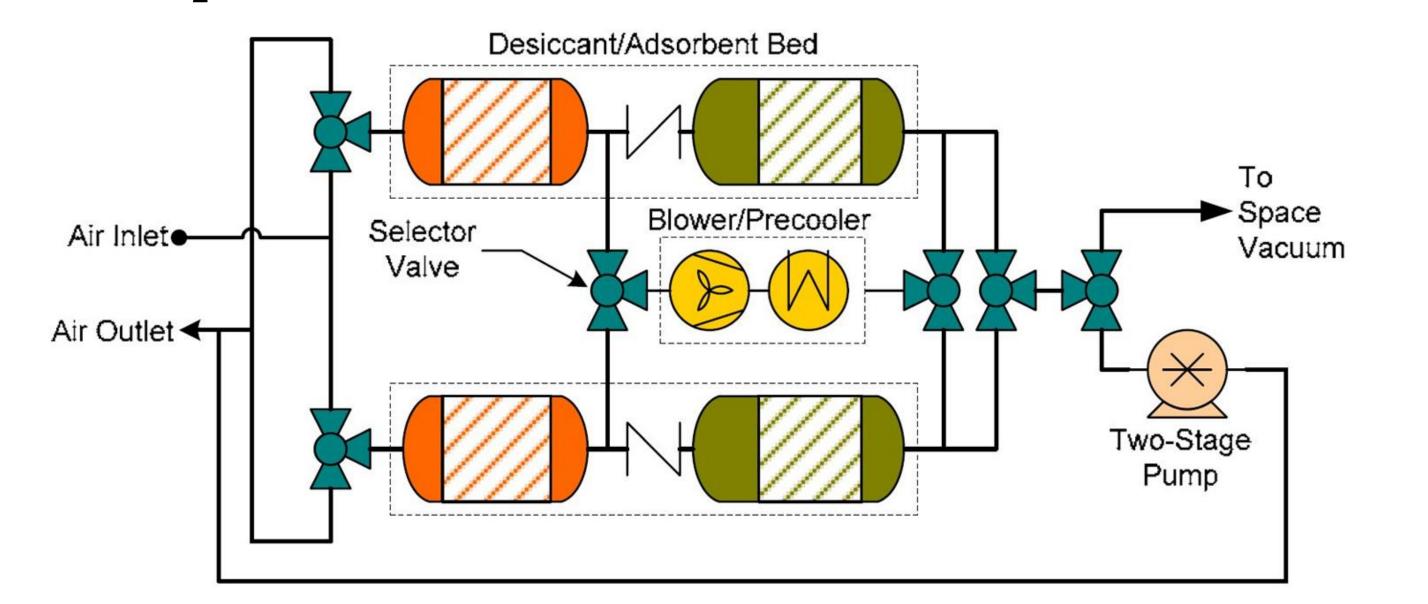
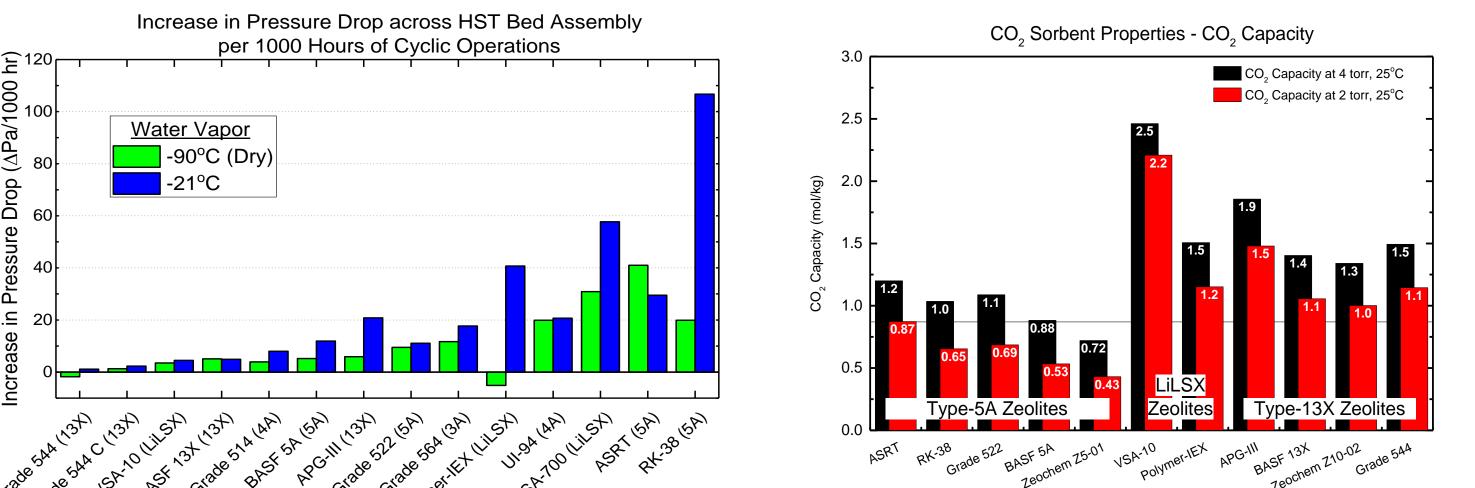


# Virtual Design of a Four-Bed Molecular Sieve for Exploration T. J. Giesy, R. F. Coker, B. F. O'Connor, J. C. Knox<sup>1</sup> 1. NASA Marshall Space Flight Center, Huntsville, AL, USA

**Introduction:** Aboard the International Space Station, CO<sub>2</sub> is removed from the cabin atmosphere by a four-bed molecular sieve (4BMS) process called the Carbon Dioxide Removal Assembly (CDRA).<sup>1</sup> This 4BMS process operates by passing the  $CO_2$ -laden air through a desiccant bed to remove any humidity and then passing the dried air through a sorbent bed to remove the CO<sub>2</sub>. While one pair of beds is in use, the other pair is thermally regenerated to allow for continuous  $CO_2$  removal.



**Results**: Six new process configurations were studied, including configurations with four new CO<sub>2</sub> sorbents. Candidate sorbents were identified based on their CO<sub>2</sub> adsorption capacity and on their resistance to dusting (Fig. 5 & 6).<sup>3</sup>



**Figure 1**. Carbon Dioxide Removal Assembly (CDRA) process schematic.

Though CDRA has effectively removed  $CO_2$  throughout its lifetime, it has also experienced technical issues that have made maintaining the system difficult. One major issue is that the  $CO_2$  sorbent has been observed to break down, producing dust which impedes gas flow in the system and can damage system components such as valves. It is also likely that the beds are oversized, increasing the system mass and power requirement unnecessarily. Accordingly, design changes to address these issues are being pursued for implementation in a next-generation 4BMS process. These changes include a new bed geometry, a new sorbent, revised heater design, and revised valve design. As changes in bed geometry (especially length) and in the type of sorbent used lend themselves well to investigation by simulation, COMSOL modeling is being used to help guide the design of the new 4BMS process.

**Computational Methods**: A 1-D plug flow model is used, with each bed being represented by a separate domain.<sup>2</sup>

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#### Figure 5. Sorbent dusting comparison.

CO<sub>2</sub> Sorbents Figure 6. Sorbent CO<sub>2</sub> capacities.

For each configuration, the zeolite layer of the desiccant bed was reduced by 45%, and the sorbent bed size was reduced by 30-60%. For two of the sorbents (544 13X and APG III), two different flow rates were investigated. Each configuration uses a half-cycle time of 80 minutes. All six configurations exceed the daily CO<sub>2</sub> removal target for a four-person crew (4.16 kg).

CO <sub>2</sub> Sorbent	Flow Rate	% of Nominal	CO <sub>2</sub> Removal	CO <sub>2</sub> Efficiency
	(SCFM)	CDRA bed	Rate (kg/day)	
RK-38	24.25	70	4.21	0.81
VSA-10	24.25	40	4.32	0.84
544 13X	28	60	4.50	0.76
544 13X	26.75	60	4.47	0.79
APG III	28	55	5.14	0.86
APG III	24.25	55	4.26	0.82

## **Table 1**. A summary of the simulation results.

Using COMSOL, the behavior of a configuration can be explored in detail than is possible experimentally. Visualizing  $CO_2$ more concentration as a function of bed depth shows how close the bed is to breakthrough at the end of a half-cycle (Fig. 7). Plotting  $CO_2$ 

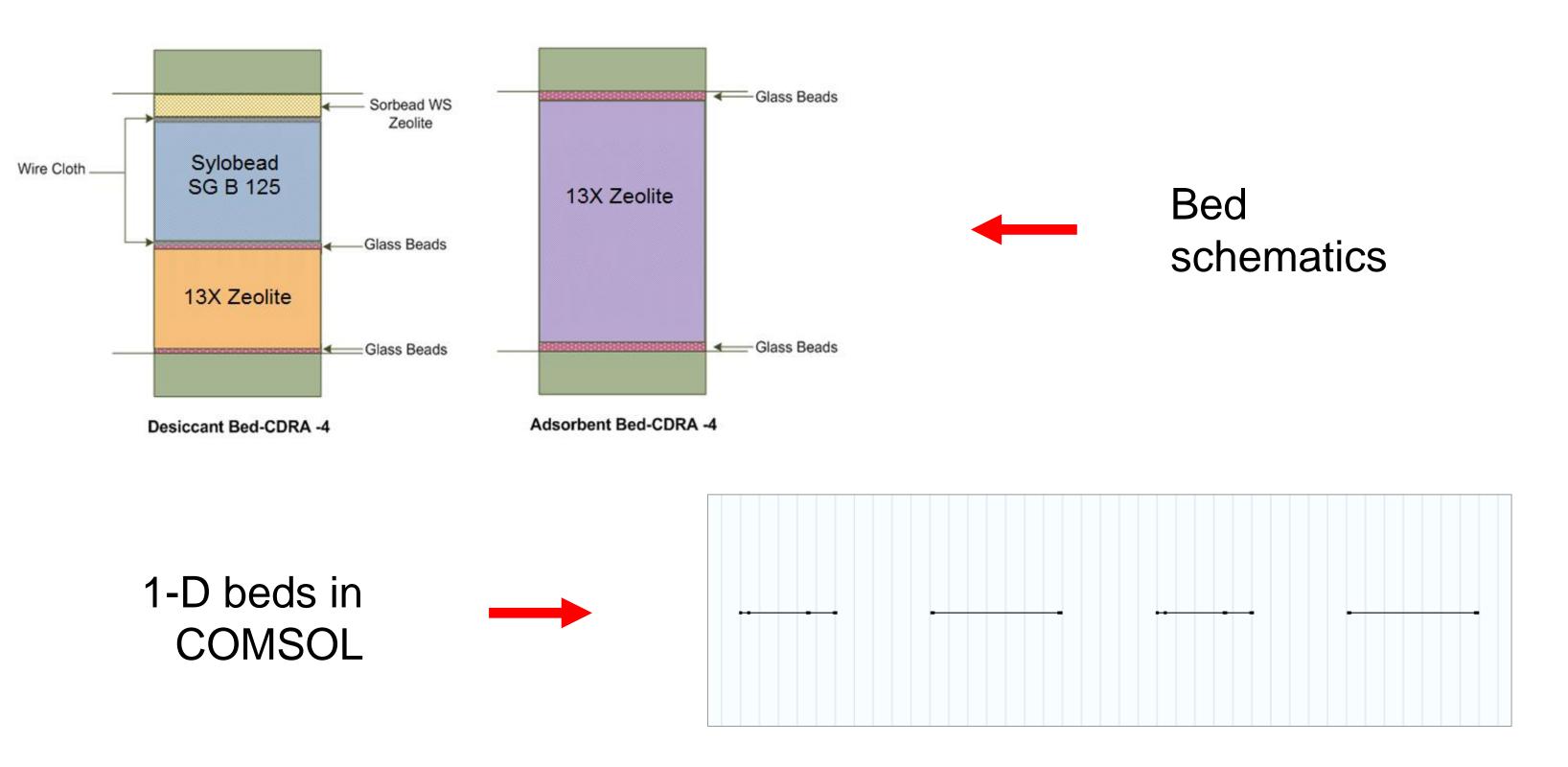
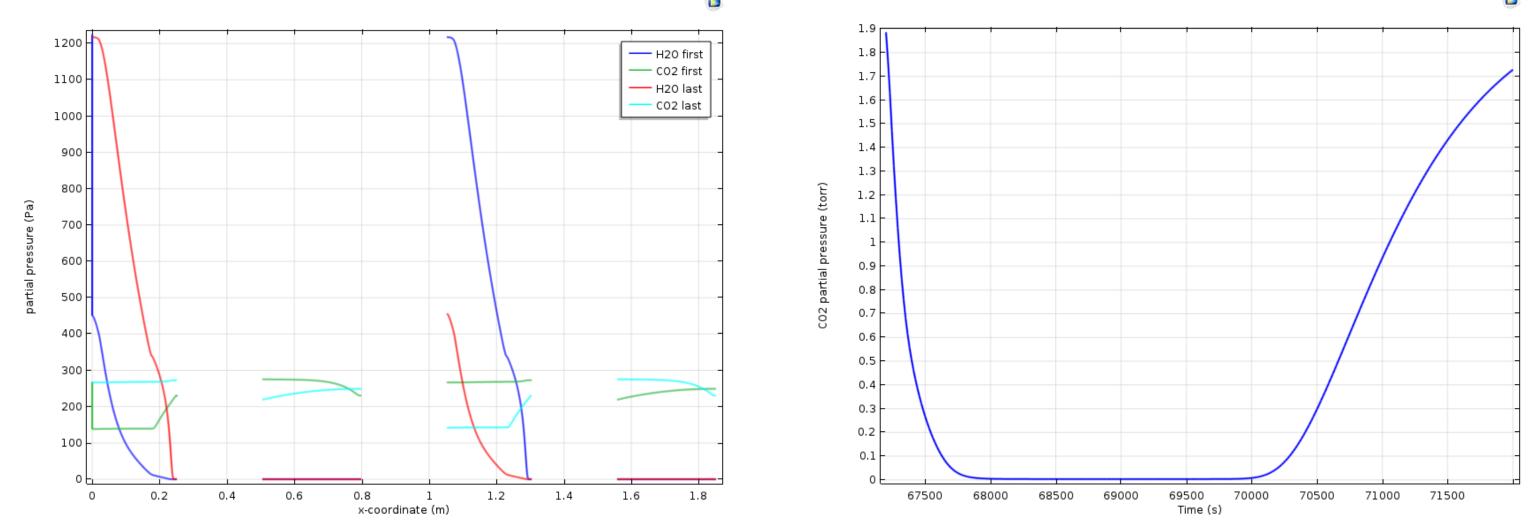


Figure 2. The simulated beds.

Though only 1-D, the model includes the majority of the relevant physics, including Darcy's law for flow in porous media; separate heat transfer solutions for sorbent, gas, can, and insulation; and diffusion in the gas phase. Moreover, experimental adsorption rate and equilibrium data<sup>3</sup> (Fig. 3 & 4) are used as inputs to the model, as these factors are the major drivers of model behavior. For further model details, see Knox, et al.<sup>4</sup>

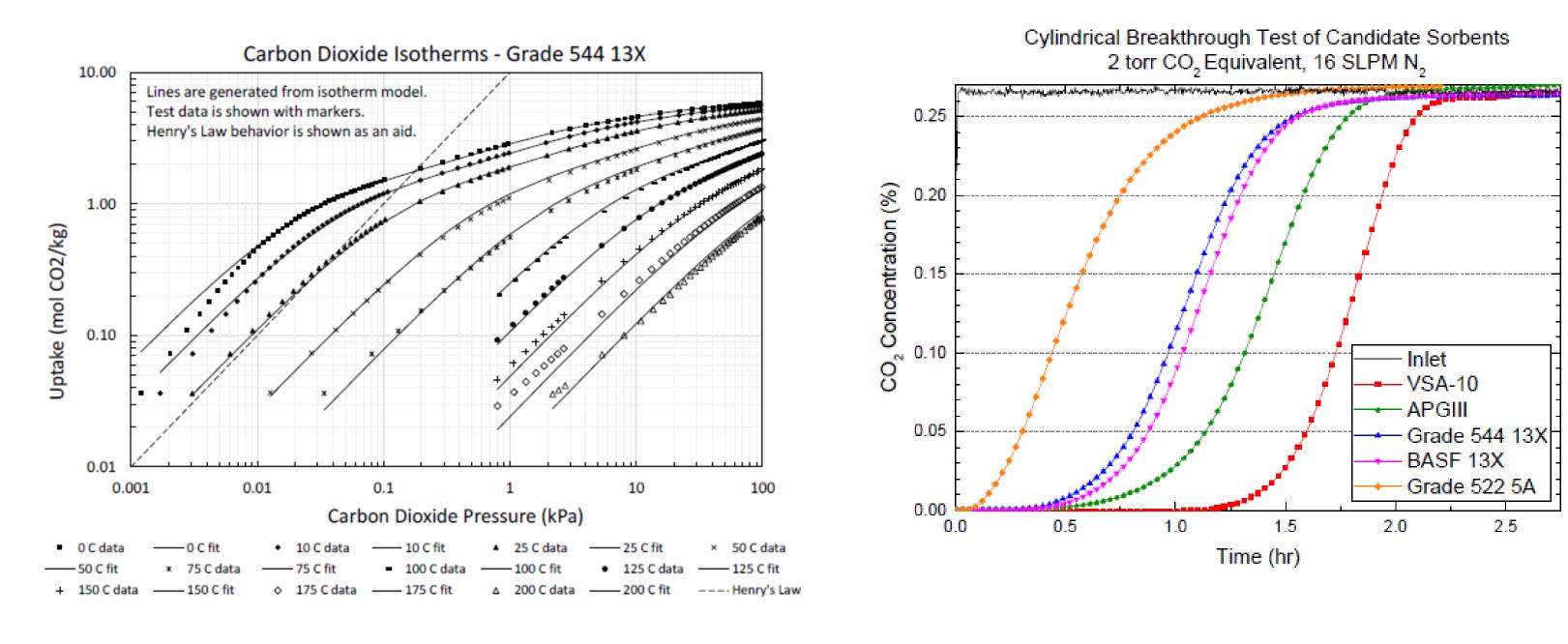
concentration as a function of time shows when breakthrough occurs during a half-cycle, and how much  $CO_2$  is exiting the sorbent bed (Fig. 8). This ability to visualize breakthrough is especially important since the six configurations studied all involve smaller bed sizes.



### **Figure 7**. Bed concentration profiles.

**Figure 8**. CO<sub>2</sub> outlet pp as f(t).

**Conclusions**: Six new configurations of a 4BMS process for CO<sub>2</sub> removal in space have been simulated. The configurations chosen focus on reducing the bed sizes and choosing a new sorbent for  $CO_2$  adsorption. This work shows that reductions in bed size and changes in sorbent are feasible while still yielding a 4BMS process for space that meets the minimum requirement of 4.16 kg/day CO<sub>2</sub> removal. Future studies will focus on 544 13X as the sorbent due to its acceptable performance and its superior resistance to dusting. Bed size, half-cycle time, and flow rate will be optimized.



**Figure 3**. Adsorption equilibrium data.

**Figure 4**. Adsorption breakthrough data.

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