

5th IAA Planetary Defense Conference – PDC 2017
15-19 May 2017, Tokyo, Japan

IAA-PDC-17-06-P07

USING INFORMATION FROM RENDEZVOUS MISSIONS FOR
BEST-CASE APPRAISALS OF IMPACT DAMAGE TO PLANET
EARTH CAUSED BY NATURAL OBJECTS

James O. Arnold⁽¹⁾, Paul W. Chodas⁽²⁾,
Stephan Ulamec⁽³⁾, Donovan L. Mathias⁽⁴⁾ and Craig D. Burkhard⁽⁵⁾

- (1) NASA Ames Research Center, N-229, Moffett Field CA 94035,
James.O.Arnold@NASA.Gov
- (2) NASA JPL, 4800 Oak Grove Drive, Pasadena CA 91011
Paul.W.Chodas@JPL.NASA.Gov
- (3) DLR RB-MUSC, German Aerospace Center, Linder Höhe, 51147 Cologne
Germany Stephan.Ulamec@dlr.de
- (4) NASA Ames Research Center, N-258, Moffett Field CA 94035
Donovan.Mathias@NASA.Gov
- (5) NASA Ames Research Center, N-229, Moffett Field CA 94035
Craig.D.Burkhard@NASA.Gov

Keywords: Asteroid Impact Appraisals, Mitigation Decisions, Rendezvous Missions, Characterization.

ABSTRACT

The Asteroid Threat Assessment Project (ATAP), a part of NASA's Planetary Defense Coordination Office (PDCO) has the responsibility to appraise the range of surface damage by potential asteroid impacts on land or water. If a threat is realized, the project will provide appraisals to officials empowered to make decisions about potential mitigation actions. This paper describes a scenario for assessment of surface damage when characterization of an asteroid had been accomplished by a rendezvous mission that would be conducted by the international planetary defense community. It is shown that the combination of data from ground and in-situ measurements on an asteroid provides knowledge that can be used to pin-point its impact location and predict the level of devastation it would cause. The hypothetical asteroid 2017 PDC with a size range of 160 to 290 m in diameter to be discussed at the PDC 2017 is used as an example. In order of importance for appraising potential damage, information required is: (1) where will the surface impact occur? (2) what is the mass, shape and size of the asteroid and what is its entry state (speed and entry angle) at the 100 km atmospheric pierce point? And (3) is the asteroid a monolith or a "rubble pile"? If it is a rubble pile, what is its structure and heterogeneity from the surface and throughout its interior? Item (1) is of first order importance to determine levels of devastation (loss of life and infrastructure damage) because it varies strongly on the impact location. Items (2) and (3) are used as inputs for ATAP's simulations to define the level of surface hazards: winds, overpressure, thermal exposure; all created by the deposition of energy during the object's atmospheric

flight, and/or cratering. Topics presented in this paper include: (i) the devastation predicted by 2017 PDC's impact on land based on initial observations using ATAP's risk assessment capability, (ii) how information corresponding to items (1) to (3) could be obtained from a rendezvous mission, and (iii) how information from a rendezvous mission could be used, along with that from ground observations and data from the literature to provide input for a new risk analysis capability that is emerging from ATAP's research. It is concluded that this approach would result in the creation of an appraisal of the threat from 2017 PDC with the least uncertainty possible, herein called the best-case.

INTRODUCTION

NASA's Planetary Defense Coordination Office (PDCO) [1] sponsors the Asteroid Threat Assessment Project (ATAP) to appraise devastation of the Earth's surface that could arise from impacts of any Near-Earth Object (NEO). The ATAP's function is exemplified herein by describing an assessment of damage caused by the impact of the hypothetical asteroid 2017 PDC, based on initial knowledge of the atmospheric impact corridor and its intrinsic magnitude of 21.9 +/- 0.4 (see <https://cneos.jpl.nasa.gov/pd/cs/pdc17/>). The predicted location of the impact is uncertain and the range of estimated devastation is large, owing to imprecise knowledge in 2017 PDC's orbit and its physical characteristics. This initial assessment is based on ATAP's Probabilistic Asteroid Risk Assessment (PAIR) capability [2, 3]. The discussion goes on to describe how the ATAP could reduce the uncertainty in their risk assessment of the threat as more information about 2017 PDC becomes available, including that from a rendezvous mission conducted by the international planetary defense community (assuming time to impact is sufficient). To meet this objective, it is pointed out how data from a rendezvous mission could be obtained, and how it would be used in an emerging model within the PAIR capability being described at PDC 2017 [4]. It is shown that information from a rendezvous mission, combined with that from ground observations and data from the literature could provide input to ATAP's PAIR capability enabling delivery of assessments with the lowest uncertainty possible (best-case) to decision makers empowered to implement planetary defense mitigation actions.

INITIAL RISK ASSESSMENT OF 2017 PDC

The hypothetical asteroid 2017 PDC was "discovered" on March 6, 2017. As of March 7, 2017, the most likely date of impact for 2017 PDC was reported by the JPL Center for Near Earth Object Studies (CNEOS) to be on July 21, 2027, approximately ten years in the future. Shortly after it was discovered, the impact probability of 2017 PDC was estimated by the CNEOS to be 1 in 40,000, and that it would occur somewhere along the very long surface impact corridor shown by red dots on Figure 1.

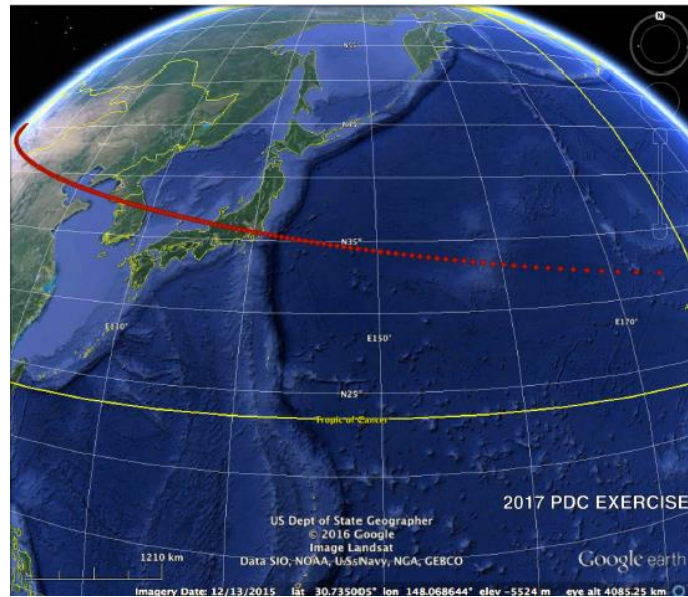


Figure 1. Initial impact corridor for the hypothetical asteroid 2017 PDC as of May 15, 2017. As of this date, the probability of the asteroid's impact was predicted to be 1 in 100.

Based on the apparent visual magnitude, 2017 PDC's absolute (intrinsic) magnitude was estimated by the CNEOS to be 21.9 +/- 0.4. Since its albedo (reflectivity) is unknown, the asteroid's mean size, using ATAP's analysis, could range from 160 to 290 m. For additional details, visit <https://cneos.jpl.nasa.gov/pd/cs/pdc17/>. ATAP personnel secured all that would be known as of May 15, 2017 about 2017 PDC's impact on July 21, 2027 from the CNEOS. Specifically, 2017 PDC's absolute magnitude, predicted speed and entry angle at the atmospheric pierce points (at 100 km altitude) and the predicted impact corridor as it was known on May 15, 2017.

The assessment of devastation along the May 15 impact corridor of 2017 PDC is shown in Figure 2. These results are based on an application of ATAP's PAIR capability [3]. The plot shows the overall "Affected Population", a metric that accounts for different fractions of the population and infrastructure within four over pressure ranges down to 68 mbar (1 psi), as defined in Table 1 and described in reference [3]. This assessment assumes the asteroid is of a spherical shape varying in size from 160 to 290 m with an unknown composition. Owing to lack of information, 2017 PDC's density, porosity and materials strength are unknown, so Monte Carlo sampling of characteristics for stony and carbonaceous classes for the ensemble of asteroids was used in the PAIR analysis. This approach is similar to that used for the recent Science Definition Team (SDT) analysis [3]. The entry angle for 2017 PDC relative to the local horizontal gets as high as 47.7 degrees at the mid-corridor. The entry speed at the Atlantic end of the corridor is 17.48 km/s, and at the Pacific end it is slightly lower at 16.92 km/s.

As shown in the Figure 2, devastation along the impact corridor depends strongly on location. The mean location of the blast is plotted in latitude and longitude coordinates in the figure. The mean value of Affected Population at that location is

identified by color. As can be seen from Figure 2, corresponding to the impact corridor over land, mean values of the Affected Population span 4 orders of magnitude from 10^4 to 10^7 . The variation in the magnitude of Affected Population about the mean is large, ~ two orders of magnitude, owing to the range of diameters (160 to 290 m) deduced from variation of the albedo and density (1.1 to 2.4 g/cc) selected from the ensemble of asteroid properties following the methodology used in Reference [3]. Not shown is the minimum level of Affected Population on land ~ 10^3 predicted to occur in Northern China, (Gobi Desert), while the maximum is at Japan, slightly over 10^7 . Two areas with low values of affected population in Kazakhstan and China (with predicted minima of ~ 10^3) might be considered by decision makers as places where “taking the hit” on land would be acceptable (given there is ample time for civil defense measures). The predicted devastation for 2017 PDC along the rest of the corridor on land is quite sobering, and illustrates the challenge decision makers would face for a real threat posed by asteroid of size similar to that of 2017 PDC, initially not knowing where the strike would happen on land.

Table 1: Affected Population percentages within different overpressure levels

Overpressure Range	Affected Population, Percent	Expected Damage
68 - 136 mbar 1 -2 psi	10	Window breakage
136 - 272 mbar 2 - 4 psi	30	Partial collapse of roofs/walls
272 - 680 mbar 4 - 10 psi	60	Partial building destruction
680+ mbar 10+ psi	100	Total building destruction and fatalities

Now consider the consequences of a strike on water by 2017 PDC along the corridor that stretches from Japan, far out into the Pacific. From results discussed at the Asteroid Generated Tsunami (AGT) Workshop [5] in August 2016, it was concluded for both airbursts and monolithic impacts from asteroids of size less than 250 m, that most damage to coastal populations is limited to impacts close to the shore, where direct blast damage is added to inundation. This result is based on the risk from the ensemble, but it should hold true for individual cases, for impacts far from shore. The risk from such near- shore impacts may be important when considering specific cases.

The initial risk assessment results depicted in Figure 2 vary widely because of the uncertainty in knowledge about the threat posed by the hypothetical asteroid 2017 PDC. The impact corridor is extremely long, and it remains long for years, even as more ground-based observations are made. The asteroid’s physical characteristics represent those from the ensemble, whereas the risk assessment should be based on those for 2017 PDC. ATAP would want decision makers have the best possible and timely information for their deliberations for taking potential mitigation actions. To meet this objective, the benefits to reduction of uncertainty in risk assessments that could be realized from a characterization mission to PDC 2017 are described below.

Options would be either a flyby or a rendezvous mission. It is important to note that a rendezvous mission provides the most powerful reduction of uncertainty for the impact location because the observations can be made over a long period of time, and dramatically improve knowledge of the orbit.



Figure 2. Prediction for Affected Population as a function of location for asteroid 2017 PDC, based on information available on May 15, 2017.

DATA FROM A RENDEZVOUS MISSION COULD PROVIDE IMPROVED RISK ASSESSMENTS

Since 2017 PDC's impact is ten years out, there is time for the international planetary defense community to conduct a rendezvous mission, possibly concurrently with, or followed by, a deflection mission similar to the Asteroid Impact and Deflection Assessment (AIDA) mission [6, 7].

Data obtained from a rendezvous mission to 2017 PDC, combined with ATAP's PAIR capability would enable the best-case assessment of risk because: (a) long term optical navigation data from the rendezvous spacecraft, combined with ground observations **could** allow significant improvement in knowledge of the asteroid's orbit. Use of the improved orbit would dramatically reduce the length of the impact corridor to probably less than 100 km, (b) in-situ optical measurements would provide information about 2017 PDC's shape, size, spin rate and spin orientation* as well as details of the surface regolith, and (c) the effective mass of the asteroid could be determined from the orbit of the rendezvous space craft while (d) radar tomography would enable determination of the structure of the asteroid [8], including boulders within the subsurface to depths of tens of meters and large fragments throughout the deep interior, answering the question: is 2017 PDC a heterogeneous "rubble pile", intact monolith or something in between?

With this information, it would be possible to precisely define the initial conditions of 2017 PDC at its pierce point into the Earth's atmosphere at 100 km: location, entry angle, speed and a rather complete description of its physical characteristics including the asteroid's interior structure and its orientation with respect to the objects flight path if it was a rubble pile.

**Given precise information of 2017 PDC's spin rate and spin axis from a rendezvous mission, modified JPL CNEOS software would enable the prediction of the orientation of the structural fragments within the asteroid with respect to its flight path at the 100 km pierce point to within a degree or so. The importance of having this information to simulate 2017 PDC's atmospheric entry and breakup is described below.*

HOW A RENDEZVOUS MISSION COULD DETERMINE THE INTERIOR STRUCTURE OF THE HYPOTHETICAL ASTEROID 2017 PDC

How? Radar sounding is the only technique capable of characterizing the internal structure and heterogeneity of an asteroid [8]. Performance is determined by the choice of the frequency and bandwidth of the transmitted radio signal: Frequency drives the penetration with lower attenuation at the lowest frequencies. Bandwidth drives resolution while the bandwidth is necessarily lower than the highest frequency. Estimated values of resolution quoted below assume a radar instrument as proposed for FANTINA (MarcoPoloR, AIDA/AIM-MASCOT2) [7]. The resolution of the monostatic radar (200 - 800 MHz) would be about 1 m. The resolution for the bistatic radar (30 - 70 MHz) would be in the range of 10 - 15 m. Density of fragments is deduced indirectly from a parameter called epsilon. See Figure 3 and the following discussion for a description of the instrumentation.

Deep interior of objects to size to ~290 m with resolution of fragments of 10 - 15 m. Measurement of the deep interior structure requires low-frequency radar to reduce the dielectric scattering losses and penetrate through the complete body. Radar wave penetration delay and received power are related to the composition and microporosity while small scale heterogeneities are related to scattering losses. Spatial variation of the signal and multiple paths provide information on the presence of heterogeneity (variations in composition) or porosity, layers, voids or large blocks. Partial coverage provides "cuts" of the body while dense coverage enables tomography. Two Instrument concepts for radar measurements are shown in Figure 3: (1) monostatic radar like MARSIS on board Mars Express ESA [9] that analyzes radar waves transmitted by the orbiter and received after reflection by the asteroid, its surface and internal structures. (2) bistatic radar like CONSERT on Philae and Rosetta ESA, DLR, CNES [10] that analyzes radar waves transmitted through the body between the lander and orbiter.

Regolith and Shallow Subsurface to ~ 10 m depth with ~ 1 m resolution.

These measurements can be achieved with a monostatic radar with a 200 - 800 MHz frequency range.

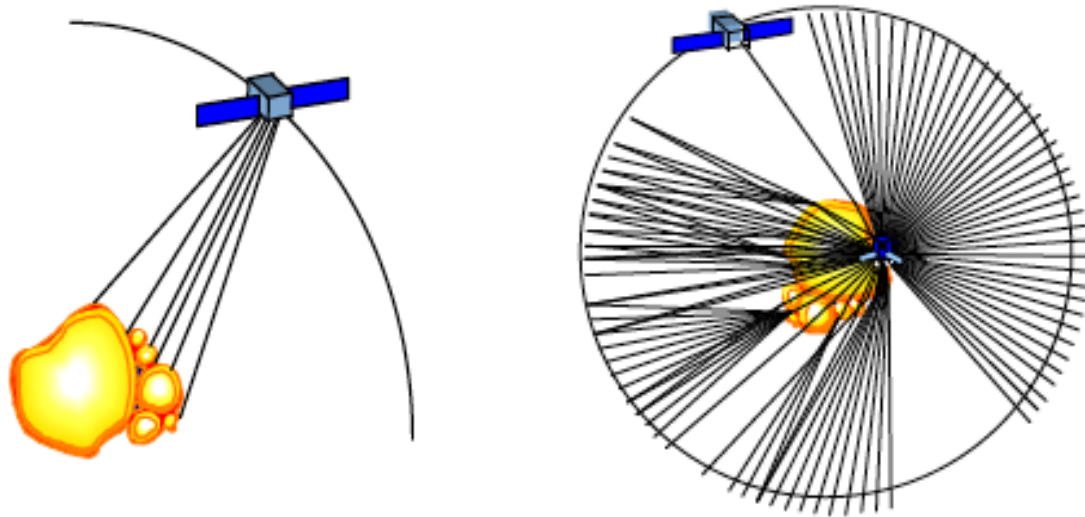


Figure 3. Radar sounding techniques to measure the sub and interior structure of asteroids: monostatic (left) and bistatic (right) [8].

The paper by Michel, *et al.*, [7] describes what could be learned from radar sounding to determine the structure of small asteroids. Plans for the ESA Asteroid Impact Mission (AIM) include the use of two radar instruments to collect direct information on the subsurface and interior structure of the ~160 m secondary in the Didymos binary asteroid system. The AIM mission was to be a part of the combined NASA-ESA AIDA mission [6]. High-frequency radar would sound the surface of the secondary (referred to as “Didymoon”) at depths to the first tens of meters at 1 m resolution to detect potential layering and embedded large rocks. A low frequency radar would be used to probe the deep interior of Didymoon to probe its structural homogeneity and to discriminate monolithic versus aggregate internal structure and to characterize the size distribution of constitutive blocks.

FRAGMENT CLOUD MODEL – RUBBLE PILE

An emerging ATAP model [4] being presented at PDC 2017 expands the current PAIR capability as it will include simulations of the entry and breakup of “rubble piles” - it is called the Fragment Cloud Model (FCM) Rubble Pile Model. Rubble piles are considered to be a heterogeneous ensemble of fragments varying in size, density and strength held together by gravity, or perhaps by other cohesive forces [11]. Figure 4, adopted from [4] depicts the FCM Rubble Pile approach. Time constraints do not permit a presentation of 2017 PDC’s entry and breakup, modeled as a rubble pile at this year’s conference. However, it is possible to describe how data from in-situ and ground observations, along with knowledge from the literature could be used as inputs to the new PAIR capability, and to describe how the approach could minimize uncertainty in the assessment of the risk created by the impact of 2017 PDC.

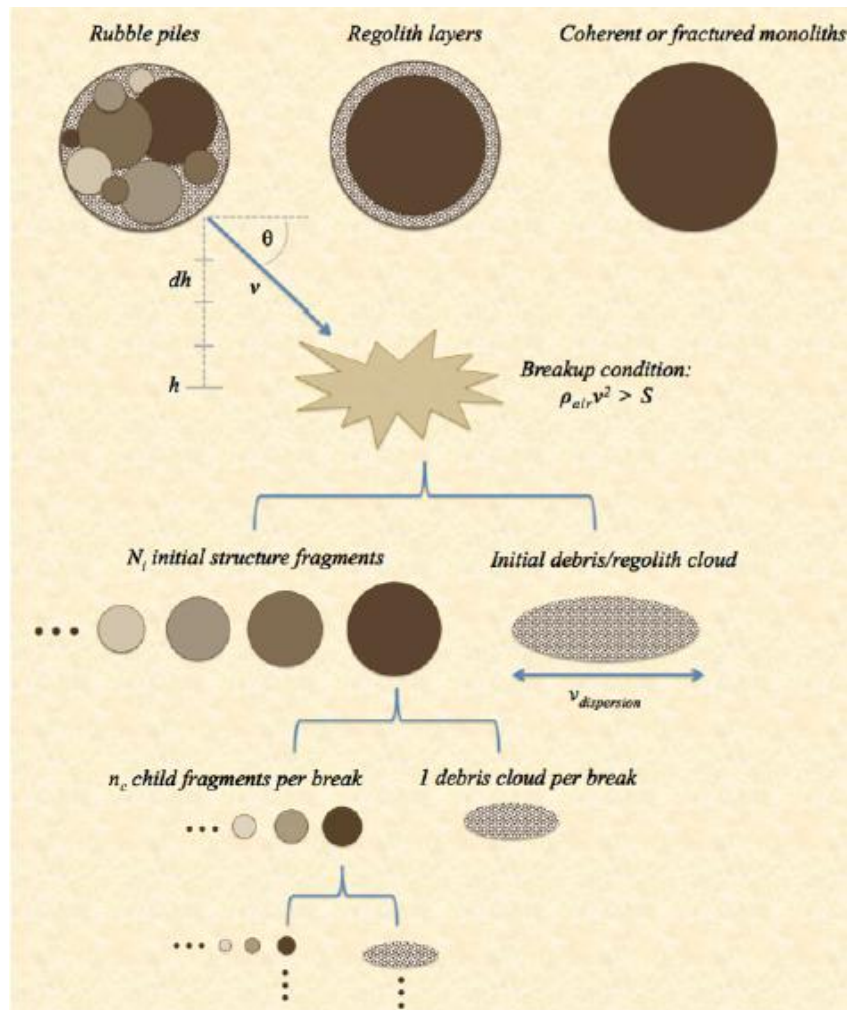


Figure 4. Schematic of the Fragment Cloud Model Rubble Pile Model. See [4] for more information.

Toward the Best-Case Assessment of 2017 PDC's Risk

Impact Location

Given data about 2017 PDC from a rendezvous mission, ground observations of the asteroid and general knowledge from the literature, the input for the PAIR assessment with respect to determining the location of the impact would be: (1) define the location of the pierce point at 100 km altitude and the initial entry velocity vector (speed v , entry angle (θ) and the heading). As discussed above, knowledge regarding the asteroid's orbit from the rendezvous mission, combined with data from ground observations will enable location of the atmospheric pierce point to within 100 km or less. (2) The PAIR capability would be exercised to simulate the entry and breakup of the asteroid, appropriate to one of the structural models shown in Figure 4. Solutions for the entry and breakup, specific to 2017 PDC from the atmospheric entry pierce point to the surface enables pin-pointing the location of the impact along the very long corridor shown in Figures 1 and 2. This answers the first order question, **where** will the devastation caused by 2017 PDC occur? Since the orbit is well known, the timing of the impact should be readily available.

Level of Devastation Created by 2017 PDC's Impact

The discussion here is limited to two of the four structural models depicted in Figure 4: The coherent monolith and the rubble pile.

Coherent Monolith

If the rendezvous mission established 2017 PDC to be a coherent monolith, the existing FCM capability within PAIR would suffice to model the asteroid's entry, breakup and surface damage as described in [2]. The FCM simulations would be based on the specific physical characteristics for 2017 PDC, i.e., size, mass and composition as determined from the rendezvous mission and ground data. Strength and porosity would be specified from the literature appropriate to 2017 PDC's composition. The uncertainty in the prediction of Affected Population will be greatly reduced compared to that in Figure 2, because the population density can be specified at the 100 km or less impact location, and the magnitude of the surface hazards can be better predicted because 2017 PDC's physical characteristics are well known, based on in-situ measurements and ground observations. Information on the level of Affected Population for the case where 2107 PDC is a coherent monolith will have a low level of uncertainty, very important for land impacts. Based on conclusions regarding tsunami created by asteroids of size <250 m [5], an impact in the Pacific far from shore would create low values of the Affected Population, and taking the hit there might be acceptable to decision makers. If the strike is on a populated coast line, detailed analysis specific to 2017 PDC such as those described at the 2016 AGT workshop [5] should be performed and provided to decision makers.

Rubble Pile

If the rendezvous mission determined 2017 PDC to be a rubble pile, the PAIR analysis would be more complicated. Referring to Figure 4, the PAIR assessment would start by defining the location, shape, size, density and materials strength S_i associated with the N_i initial structural fragments. As discussed above, regolith and boulders in the subsurface would be defined by monostatic radar measurement to depths of \sim tens of meters at a resolution of meter or so. Structure throughout the asteroid would be defined by bistatic measurements to within 10 - 15 m, and the density of the fragments could be specified as described above. Information from the literature would provide materials strength of the fragments, inferred from their size and density. The next step in the set up would be to orient the ensemble of fragments comprising 2017 PDC with respect to the initial flight path at the 100 km atmospheric pierce point. The importance of the orientation can be visualized by inspection of rubble pile cartoon in Figure 4. If the rubble pile 2017 PDC entered in an orientation rotated clockwise about 45 degrees in plane of Figure 4 from that shown, the largest, dark (dense) fragment would strike the atmosphere first and the subsequent break up probably would be much different than that for the orientation as shown, where two smaller, less dense fragments would strike the atmosphere first. The initial breakup of a rubble pile will result from aerodynamic forces that are created by shock heated gases flowing over, and between the fragments.

Given these inputs, the FCM Rubble Pile simulation would be run, with breakup of the initial configuration of the fragments and their "children" in accordance with the condition at the altitude h where the product of the free stream air density and the

velocity exceeds the materials strength, i.e., $\rho v^2 > S_i$. The variability of the strength with size of the “child” fragments (stronger at smaller sizes), that defines the altitude of the fracture of the “children” is accounted for by using the Weibull approach, as described in [2].

The question now is what information of significant importance, relevant to the level of devastation caused by 2017 PDC would come from FCM Rubble Pile simulations of its entry and breakup? The answer is that, similar to the FCM modeling, the simulation would provide details of the deposition of energy into the atmosphere along the entry trajectory. Subsequent propagation of the disturbance results in predicting surface hazards: overpressures, winds and thermal exposure. While simulations for the FCM Rubble Pile model are not yet available for 2017 PDC, analysis of existing FCM results can help understand the relation between level of hazards and the altitude of peak energy deposition that will be provided by the new PAIR capability. This understanding comes from Figure 5, and the associated discussion, adopted from [2] and another ATAP presentation [12] at PDC 2017. As pointed out by those authors, FCM simulations, and likewise FCM Rubble Pile simulations must account for the dispersal of fragments in order to produce realistic energy deposition profiles. They are quantified [12] by the empirical relation

$v_{disp} = \frac{\sqrt{C_{disp} \rho_A}}{\rho_m}$ where ρ_A air is the free stream air density and v_{disp} is the lateral spread velocity. Rubble pile asteroids will airburst, and C_{disp} strongly influences the altitude of the energy deposition as shown in Figure 5, adopted from [12] for a 50 m air bursting asteroid.

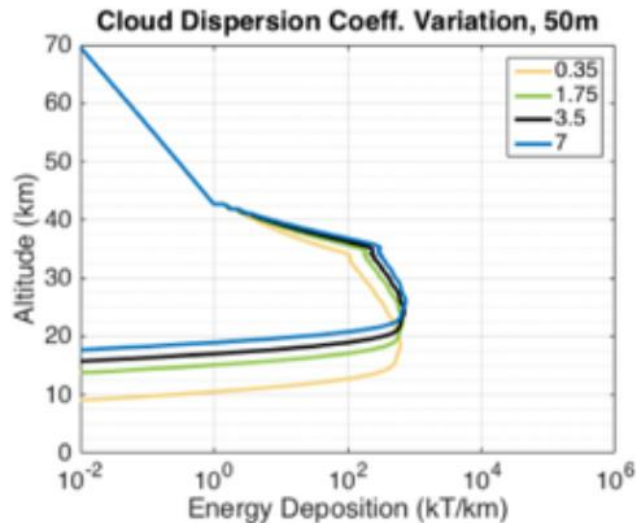


Figure 5. FCM model of the variation of the height of peak Energy Deposition for a 50 m air bursting asteroid as a function of altitude corresponding to values of the lateral dispersion coefficient C_{disp} ranging from 0.35 to 7. Figure adopted from [12].

As can be seen, the variation in the altitude of peak Energy Deposition is from about 25 to 18 km over a range of values for C_{disp} from 0.35 to 7, respectively. The variation in altitude is important in the resulting prediction of surface devastation. For example the area of overpressures roughly doubles [2,12] as the altitude of peak energy deposition is reduced from 25 to 18 km. At “ground zero” thermal radiation varies inversely with the square of altitude, h . From this example for a 50 m rubble

pile asteroid, it is seen that variation in the altitude of peak energy deposition can result in an increase by a factor of about two for both the area of surface overpressures and thermal exposure. Each of them would result in significant increases in the level of Affected Population. This information for a 50 m asteroid illustrates how important it is to know the details of its sub and interior structure, how the constitutive fragments break up and how the “children” disperse laterally. This knowledge is of great importance for determining the magnitude of hazards for land impacts at 2017 PDC’s pin-pointed location along the impact corridor. As stated above, structure and heterogeneities of asteroids like 2017 PDC can only be determined by radar sounding via a rendezvous mission [8].

It is noted that care should be undertaken for the assessment of Affected Population that could happen on land impacts. If 2017 PDC was a rubble pile, it could quickly evolve into several objects reacting to aerodynamic forces, flying independently with larger ones potentially creating dispersed surface craters. On the other hand, depending on the initial orientation, some of the fragments could be captured in the wake of the leading body, staying there until striking the surface. This would lead to a more compact area of cratering, possibly similar to that caused by a coherent monolith. Note that ATAP is conducting collaborative research with DLR Cologne on the subject of multi-body hypersonic aerodynamics relevant to this topic, and initial results [12] will be presented at PDC 2017. Dispersion of landed fragments of tens of km could be very important in evaluating levels of affected population along an impact corridor on land. For example, the largest meteorite from Chelyabinsk (~ 600 kg) fell in Lake Chebarkul, 78 km away from the damage that occurred within the city [13]. Damage by impacts could be very different for cases with and without crater dispersions at narrow boundaries between cities and unpopulated areas or at coast lines.

The conclusion made at the AGT workshop [5] regarding low risk for airburst and impacts for asteroids of 250 m or less on water will likely be true for those by 2017 PDC on the Pacific Ocean.

If a rendezvous mission could establish the orbit and physical characteristic of a threat like 2017 PDC to provide high confidence by the CNEOS that the strike would occur in the Pacific, far from populated coastlines and the ATAP predicted the resulting Affected Population to be minimal, it seems that decision makers would have sufficient information to evaluate if “taking the hit” in the Pacific Ocean could be a viable option for 2017 PDC across its ranges in size (160 – 290 m). ATAP would conduct extensive simulations for expected damage with their PAIR capability accounting for water depths and bathymetry in the relatively small (100 km or less) corridor length of the ocean strike. This work would include their own hydrocode simulations that would be compared to that from the FCM Rubble Pile based risk assessment and to those involving hydrocode based simulations by other groups from the DoE tri-labs.

The discussion of these risk assessments for 2017 PDC illustrates how information from a rendezvous mission could be combined with that from ground observation and data from the literature to provide best-case information for decision makers. Information with low levels of uncertainty in the level of Affected Population should

help in deciding whether to “take the hit” in the ocean far from shore, or in remote land areas versus implementing an in-space mitigation.

Finally, at the risk of stating the obvious, it is noted that if “taking the hit” is an accepted solution, it would eliminate the risk that deflection of 2017 PDC could make matters worse, owing to uncertainty in the outcome of the in-space mitigation.

CONCLUSION

Based on early information on the hypothetical strike of 2017 PDC provided by the JPL CNEOS, an initial risk assessment was presented using ATAPs risk assessment capability. Owing to lack of information, the initial assessment is of high uncertainty with respect to both the location and magnitude of the inflicted damage. A rendezvous mission would dramatically improve the prediction of the strike location as well as information regarding the physical characteristics of the hypothetical asteroid 2017 PDC. A brief discussion of the methodology to determine physical characteristics from an asteroid via a rendezvous mission was provided including definition of structure and heterogeneity in the subsurface to depths of tens of meters and that within its deep interior by radar mapping was provided. Also presented was a description of how ATAP’s PAIR capability will include emerging FCM Rubble Pile modeling, and how data from a rendezvous mission would be used for risk assessments of asteroids like 2017 PDC. Because of the benefits to reducing uncertainty in risk, it becomes clear that a rendezvous mission followed by, or concurrently with, a mitigation action should be considered by decision makers in the event that a real threat, similar to 2017 PDC materializes.

FUTURE WORK

Clearly, the emerging Fragment Cloud Model (FCM) Rubble Pile capability described herein will enable the Asteroid Threat Assessment Project’s (ATAP’s) capability to simulate entry and breakup of rubble pile asteroids and the subsequent hazards they produce at higher level of detail than currently possible. As was done for the development of the existing FCM capability, sensitivity studies with the new capability should be conducted to prioritize how the project should conduct inclusion of detailed physics based models into the PAIR capability, focus its ground testing and continue its measurements of meteorite properties. This study could also provide insight with respect to prioritizing measurements that should be taken during rendezvous missions. After sensitivity studies are mature, the information and conclusions made herein should be updated and documented in a submission to an appropriate journal. After the work is peer reviewed and published, it should be made available to those in the community that are (or will be) empowered to decide upon mitigation of actual threats of impact to the Earth by natural objects.

ACKNOWLEDGEMENTS

For support from the Planetary Defense Coordination Office - Lindley Johnson, Lorien Wheeler for her outstanding work on the PAIR predictions reported herein, and Ethiraj Venkatapathy and Dave Morrison for their critical review of this manuscript.

REFERENCES

- [1] www.lpi.usra.edu/sbag/meetings/jun2016/presentations/johnson-neo.pdf Jun 30
- [2] Wheeler, L. F., Register, P. J., and Mathias, D. L., "Fragment-Cloud Model for Asteroid Breakup and Atmospheric Energy Deposition", (Accepted, in press), doi:10.1016/j.icarus.2017.02.01
- [3] Mathias, D. L., Wheeler, L. F., Dotson, J. L., "A Probabilistic Asteroid Impact Risk Model: Assessment of Sub-300 m Impacts", *Icarus* 289C (2017) pp. 106-119, doi: 10.1016/j.icarus.2017.02.009.
- [4] Wheeler, L. F. and Mathias, D. L., 2017 "Modeling the atmospheric breakup of varied asteroid structures: inference for the Chelyabinsk meteor and risk assessment application: IAA 5th Planetary Defense Conference, 2017 Tokyo, Japan
- [5] Morrison, D. D, Venkatapathy, E., "Asteroid Generated Tsunami: "Summary of NASA/NOAA Workshop NASA/Technical Memorandum (NASA/TM-219463) January 2017". See details and presentation materials at <https://tsunami-workshop.arc.nasa.gov/>
- [6] A.F. Cheng, *et al.*, "Asteroid impact & deflection Assessment mission", *Acta Astron.*, Vol. 115, pp. 262-26.
- [7] Michel, P. *et al.*, "Science case for the Asteroid Impact Mission (AIM): a component of the Asteroid Impact & Deflection Assessment (AIDA) Mission", *Adv. in Space Res.*, Vol. 57, pp. 2529-2547, 2016.
- [8] Herique, A. *et al.*, "A Direct Observation of an Asteroid Structure from Deep Interior to Regolith: Why and How?" 4th IAA Planetary Defense Conference 13-17 April, Frascati, Rome Italy.
- [9] Picardi, G. *et al.*, 2005, "Radar soundings of the subsurface of Mars", *Science*, 310, 1925-1928
- [10] Kofman, W. *et al.*, 2007. "The Comet Nucleus Sounding Experiment by Radiowave Transmission (CONCERT). A short description of the instrument and of the commissioning stages". *Space Science Reviews*, Vol 128,
- [11] P. Sanchez, *et al.*, "The Strength of Regolith and Rubble Pile Asteroids", *Meteoritics and Planetary Science*, pp. 1-49, 2014.
- [12] Venkatapathy, E. *et al.*, "In Pursuit of Improving Airburst and Ground Damage Predictions: Recent Advances in Multi-Body Aerodynamic Testing and Computational Tools Validation", IAA 5th Planetary Defense Conference, 2017 Tokyo, Japan
- [13] Popova, O., *et al.*, "Chelyabinsk Airburst, Damage Assessment, Meteorite Recovery, and Characterization", *Science Express*, pp. 1-11, 2013