

Numerical Analysis of Carbon Fiber Reinforced Plastic (CFRP) Shear Walls and Steel Strips under Cyclic Loads Using Finite Element Method

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Abstract—Reinforced concrete shear walls are the main elements of resistance against lateral loads in reinforced concrete structures. These walls should not only provide sufficient resistance but also provide sufficient ductility in order to avoid brittle fracture, particularly under strong seismic loads. However, many reinforced concrete shear walls need to be stabilized and reinforced due to various reasons such as changes in requirements of seismic regulations, weaknesses in design and execution, passage of time, damaging environmental factors, patch of rebar in plastic hinges and in some cases failures and weaknesses caused by previous earthquakes or explosion loads. Recently, Fiber Reinforced Polymer (FRP) components have been extensively and successfully used in seismic improvement. This study reinforces FRP reinforced concrete shear walls and steel strips. CFRP and steel strips are evaluated by different yield and ultimate strength. Numerical and experimental studies are done on walls with scale 1/2. These walls are exposed to cyclic loading. Hysteresis curves of force, drift and strain of FRP strips are reviewed in order to compare results of numerical work and laboratory results. Both numerical and laboratory results show that CFRP and steel strips increase resistance, capacity and ductility of the structure.

Keywords—numerical analysis; shear wall; FRP; lateral load; ABAQUS

I. INTRODUCTION

Polymer coatings used to improve concrete structures were first developed in 1980 in Europe and Japan. In Europe, FRP systems were used as an alternative to steel plates. Connection of steel plates to tensile part of concrete members by epoxy resins is a common durable method to enhance bending strength of these members. Steel plates are corroded and their corrosion leads to the collapse of steel plates with concrete. Moreover, they are difficult to install, because they are installed by heavy machinery. Thus, scientists tended to replace steel coatings by FRP materials. With almost 20% of the weight of steel coatings, FRP is approximately 8 to 10 times more resistant than steel. One of the problems with system structural calculations is the difficulty of computer modeling in the form of finite element. Moreover, variation in effective parameters on behavior of these structures challenges

laboratory methods due to high cost and time. Numerical methods also require a correct understanding of non-linear behavior of reinforced concrete and FRP [1]. This study develops suitable structural models and models non-linear behavior of concrete, reinforcement and FRP.

II. PROBLEM DESCRIPTION

A. Concrete Damage Plasticity

The most important step in numerical modeling of reinforced concrete structures is the determination of concrete's nonlinear behavior. In the finite element software ABAQUS, nonlinear behavior of brittle materials can be defined through three models: 1) smeared cracking, 2) brittle cracking and 3) concrete damage plasticity [2]. Concrete damage model is the only model which can be used in both static and dynamic analysis. In this model, it is assumed that tensile cracking and compressive crushing are two main aspects of concrete failure mechanism. In modeling brittle material cracking under cyclic loading (alternating tension and compression), stiffness recovery is allowed during reciprocating loads [3]. In plastic damage model, elimination of elements and cracking are not allowed during analysis due to the lack of failure criterion, however, this model is able to predict location and direction of cracks.

B. Interpretation of Moment - Curvature Curve for Reinforced Concrete Shear Wall Section

Unlike the simplicity in design and construction of reinforced concrete shear walls, the real response of these elements is rather complex. Overall behavior of walls is influenced by bending, shear and axial responses. Wall sections are against compressive axial forces caused by gravity loads and their own weight. Axial pressure acting on the wall is estimated at 20% of product of concrete compressive strength, f'_c , in A_g (gross concrete cross section) [4]. Authors in [4] described the moment-curvature relationship in walls of high-rise buildings against a unidirectional load. When bending moment is applied on the wall section, initial response of the wall is linear elastic with initial flexural stiffness. Cracking

occurs when moment exceeds initial elasticity and flexural stiffness is reduced by growth of the first crack and start of additional cracks. Slope of this phase results from approximately parallel response of flexural stiffness of the cracked and deformed section. Further increase in the applied moment leads to the weakening of steel and the section's capacity. It is thus considered essential to use non-linear analysis and theories of plasticity to simulate behavior of reinforced concrete shear wall.

Uniaxial stress-strain relationship of concrete under pressure and tension is an important parameter in importing concrete damage plasticity model to the software. To do this, the Hognestad curve is used. Equations (1) and (2) are used to import compressive stress of concrete versus compressive strain to the software. In these equations, ϵ_0 is the corresponding strain to maximum stress. For specimens of which ϵ_0 is unknown, this study uses the value 0.002, which is a rational value for conventional concretes [5]. In (2), f_c'' is maximum stress in concrete element. The k_s factor can be considered as portrayed in Table I [5] for concretes with cylindrical compressive strength. Descending branch of the modified Hognestad curve is linear which extends from ϵ_0, f_c'' to $\epsilon_u, 0.85f_c''$. ϵ_u corresponds to ultimate corresponding strain to compressive failure of concrete, which has been reported from 0.003 to higher than 0.005. This study considers 0.0038.

$$f_c = f_c'' \left[\frac{2\epsilon_c}{\epsilon_0} - \left(\frac{\epsilon_c}{\epsilon_0} \right)^2 \right] \tag{1}$$

$$f_c'' = k_s f_c' \tag{2}$$

TABLE I. k_s VALUES IN HOGNESTAD CURVE

f_c' (MPa)	15	20	25	30	>35
k_s	1	0.97	0.95	0.93	0.92

C. Stress-Strain Under Tension by Using ABAQUS-Suggested Equation

Concrete alone cannot tolerate tensile stresses and its tensile strength is low (7%-11% of compressive strength). Steel rebar is usually used to compensate these problems. Concrete tensile response begins with cracking and its expansion. Thus, concrete behavior cannot be evaluated by considering tensile strain. Instead, the crack should be evaluated. The concrete response under pressure is linear until it reaches its tensile strength which is associated with very fine cracks. The increase in loading decreases resistance and expands cracks to fracture under ultimate strain [6-7]. A straight line is usually used for softening part of tensile curve. Moreover, tensile strength and ultimate strain are calculated by following equations [8-10]:

$$f_t' = 0.33 \sqrt{f_c'} \tag{3}$$

$$\epsilon^* = 0.001 \tag{4}$$

In periodic loading, stiffness decreases and cracks after each cycle emerge. Unlike compressive cracks, these cracks are completely obvious and open [6]. The curves presented for the static scenario are in fact pushover curves of maximum stresses under periodic loading.

D. Damage Parameter

The slope of unloading curve is lower than the slope of the elastic curve in the softening part, which indicates damage. The reduced initial stiffness is shown by d_t and d_c (stiffness decline under tension, and d_c stiffness decline under pressure respectively). It is assumed that these two variables are functions of plastic strain, temperature and other field variables [3].

$$d_t = d_t(\epsilon_t^{pl}, \theta, f_t) \quad 0 \leq d_t \leq 1 \tag{5}$$

$$d_c = d_c(\epsilon_c^{pl}, \theta, f_c) \quad 0 \leq d_c \leq 1 \tag{6}$$

where, ϵ_t^{pl} and ϵ_c^{pl} are corresponding plastic strains under pressure and tension, θ is the temperature, and f_t, f_c is the field variable. In fact, concrete damage is determined by d_t and d_c in uniaxial stress-strain curves. These damage variables are expressed as follows:

$$E = (1 - d_{t,c}) E_0 \tag{7}$$

where E is the damaged module of elasticity, E_0 is undamaged module of elasticity. It is important to select properties of damage, because excessive damage values have unsuitable effect on convergence rate.

E. Behavior of Reinforcements

There are many stress-strain models in finite element software. This study uses a bilinear elastoplastic model for reinforcement. In ABAQUS, longitudinal and transverse reinforcements are modeled by two-node truss element T3D2 which is only able to tolerate axial force and acts separately from concrete.

F. Stiffness Recovery in ABAQUS

Stiffness recovery is an important discussion in the mechanical response of concrete in periodic loading. In ABAQUS, the user can directly import the stiffness recovery factors, w_t and w_c . In the majority of quasi-brittle materials such as concrete reflect improvement of compressive stiffness resulting from closure of cracks when loading shifts from tension to compression. On the other hand, tensile stiffness is not recovered by this shift after formation of microcracks under concrete crushing. This behavior which is related to $w_t=0$ and $w_c=1$ is default in ABAQUS.

III. SPECIMENS

A. Reinforced concrete shear walls specimens

Group A: Five specimens of CFRP reinforced concrete shear walls tested by authors in [11] at scale of 1/2 are modeled in different arrangements of CFRP in ABAQUS. All specimens are 1000 mm in length, 100 mm in width and 1500 mm in height. All specimens are exposed to cyclic loading with drift control. Group B: Three specimens of CFRP reinforced concrete shear walls tested in [12] are modeled in different arrangements of CFRP in ABAQUS. All specimens are 1200 mm in length, 80 mm in width and 1045 mm in height. All specimens are exposed to cyclic loading with drift control and 48 kN compressive axial force and two axial forces, one compressive and the other tensile, in a distance which forms couple on top of the wall, as shown in (8) and (9).

$$F_A = 24 + 1.115F_C \tag{8}$$

$$E = (1 - d_{t,c})E_0 \tag{9}$$

Group C: Four specimens of steel strip reinforced concrete shear walls tested in [13] at scale of 1/2 are modeled in different arrangements of steel strips in ABAQUS. All specimens are 1000 mm in length, 100 mm in width and 1500 mm in height. All specimens are exposed to cyclic loading with drift control

B. Specifications of materials

Group A: specimen 1 which is unreinforced is selected as reference specimen. Four other specimens are determined (Specimen 2, Specimen 3, Specimen 4 and Specimen 5). All four reinforced specimens have a layer reinforced by CFRP strips [11]. Group B: CW which is unreinforced is selected as reference specimen. Two other specimens are determined (RW1 and RW2). All two reinforced specimens have a layer reinforced by CFRP strips [2]. Group C: specimen 1 which is unreinforced is selected as reference. Three other specimens are determined (Specimen 2, Specimen 3 and Specimen 4). All three reinforced specimens have a layer reinforced by steel strips [13]. Table II shows 28-day resistance of concrete in all specimens. Table III shows yield and ultimate strength of rebar used in this experiment. Values of shear modulus (G) are given in Tables IV and V.

IV. RESULTS

A. Group A

Figure 1 shows the force-drift hysteresis curve of numerical analysis for Group A specimens under cyclic load [11]. Figure 3 shows the strain-force hysteresis curve of CFRP materials in numerical analysis for Group A Specimens under cyclic load. Table VI lists the experimental results and compares them to numerical results related to maximum strain. As shown, the numerical analysis is consistent with the experimental results.

TABLE II. SPECIFICATIONS OF SPECIMENS

Group A: Five specimens of CFRP reinforced concrete shear walls					
Specimen5	Specimen4	Specimen3	Specimen2	Specimen1	
15.6	15.9	15	15.7	15.5	$f'_c \frac{f'_s}{f'_s}(\text{MPa})$
A combination of mesh and horizontal and parallel strips at the top and bottom of specimen	A combination of X-shaped, horizontal and parallel strips at the top and bottom of specimen	An X-shaped layer	Horizontal and parallel strips	-	Fiber arrangement
Group B: Three specimens of CFRP reinforced concrete shear walls					
RW2	RW1	CW			
37	37	45			$f'_c \frac{f'_s}{f'_s}(\text{MPa})$
A crossed and a wrapping layer at the top and bottom of wall	A vertical C-shaped layer in side edges and a wrapping layer around the wall	-			Fiber arrangement
Group C: Four specimens of steel strip reinforced concrete shear walls					
Specimen 4	Specimen 3	Specimen 2	Specimen 1		
18.5	17.8	18.2	15.5		$f'_c \frac{f'_s}{f'_s}(\text{MPa})$
A combination of horizontal and vertical strips	Horizontal and parallel strips	A X-shaped layer	-		Arrangement of steel strips

TABLE III. SPECIFICATIONS OF REINFORCEMENTS

Group A: CFRP reinforced concrete shear walls		
Ultimate strength (MPa)	Yield strength (MPa)	Reinforcement diameter (mm)
420	325	6
522	430	10
515	428	12
520	425	16
Group B: CFRP reinforced concrete shear walls		
Ultimate strength (MPa)	Yield strength (MPa)	Reinforcement diameter (mm)
550	450	10
720	620	6
Group C: Steel strip reinforced concrete shear walls tested		
Ultimate strength (MPa)	Yield strength (MPa)	Reinforcement diameter (mm)

420	325	6
522	430	10
520	425	16

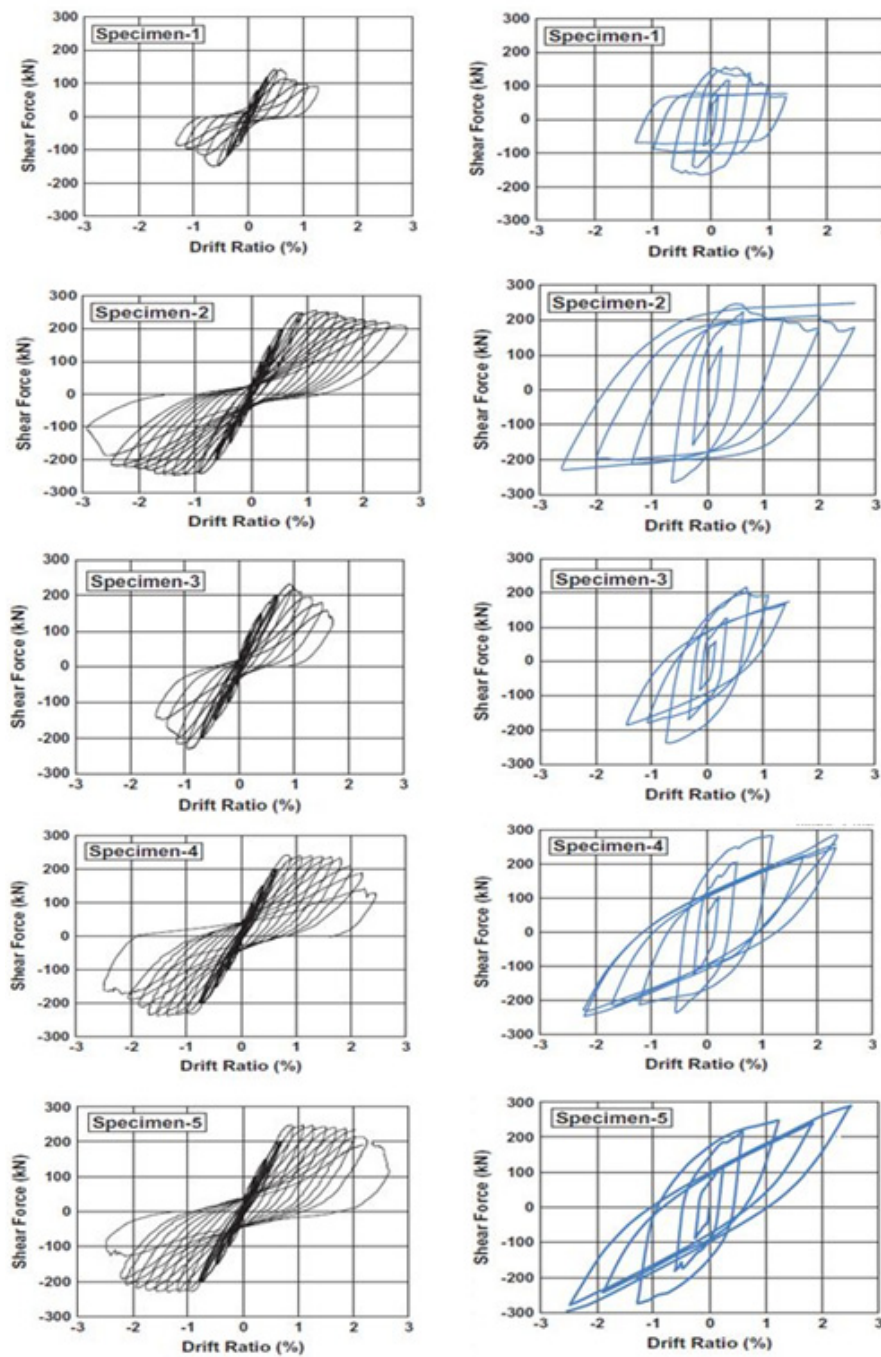


Fig. 1. Force-drift hysteresis curve under cyclic load, Group A, Specimens 1-5 a) experimental b) numerical

TABLE IV. SPECIFICATIONS OF CFRP

Group A: CFRP reinforced concrete shear walls				
Ultimate strain (%)	Ultimate tensile stress (MPa)	Modulus of elasticity (MPa)	Thickness (mm)	Fiber
1.7	4100	231000	0.12	CFRP
Group B: CFRP reinforced concrete shear walls				
Ultimate strain (%)	Ultimate tensile stress (MPa)	Modulus of elasticity (MPa)	Thickness (mm)	Fiber
1.6	3790	230	0.175	CFRP

Group C: Steel strip reinforced concrete shear walls		
Ultimate strength (MPa)	Yield strength (MPa)	Thickness (mm) Steel strips
470	340	2.5

TABLE V. INPUT PARAMETERS FOR MODELING FIBERS IN ABAQUS

Group A: CFRP reinforced concrete shear walls											
G_{23}	G_{13}	G_{12}	Nu_{23}	Nu_{13}	Nu_{12}	E_3	E_2	E_1	Thickness	Layer	Fiber
9625	9625	96250	0.2	0.2	0.2	23100	23100	231000	0.12	1	CFRP
Group B: CFRP reinforced concrete shear walls											
G_{23}	G_{13}	G_{12}	Nu_{23}	Nu_{13}	Nu_{12}	E_3	E_2	E_1	Thickness	Layer	Fiber
9583	9583	95833	0.2	0.2	0.2	23000	23000	230000	0.12	1	CFRP
Group C: Steel strip reinforced concrete shear walls											
Ultimate strength (MPa)	Yield strength (MPa)	Thickness (mm) Steel strips									
470	340	2.5									

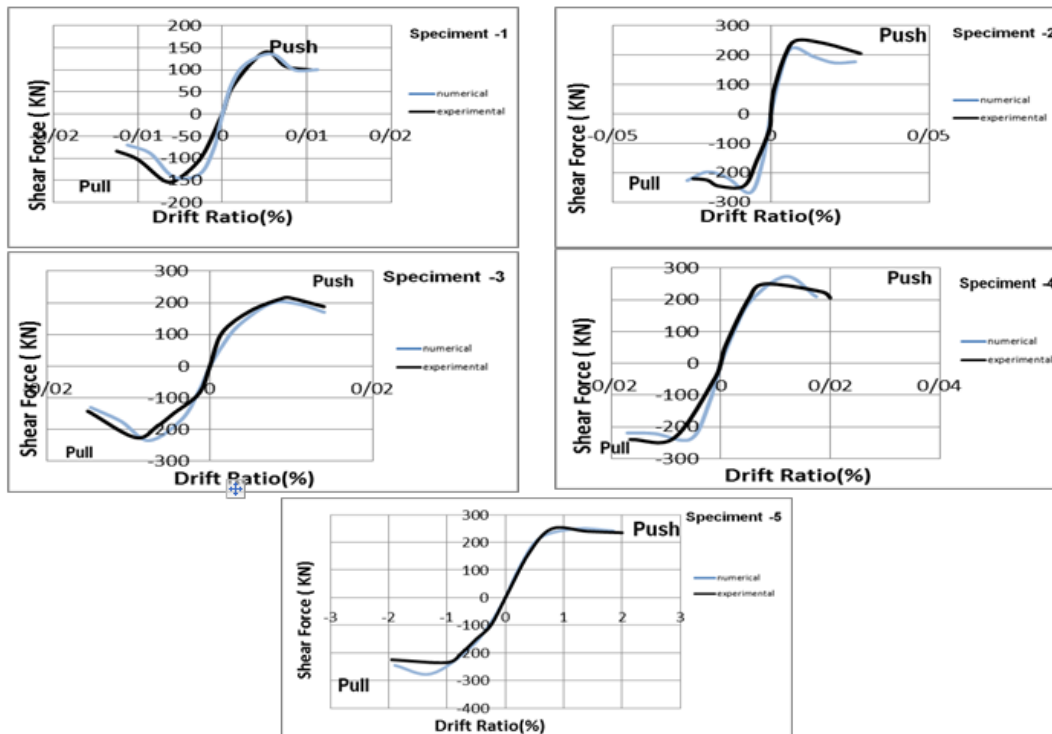


Fig. 2. Push comparison of hysteresis curves of experimental results and numerical analysis (Group A)

TABLE VI. GROUP A: COMPARISON OF MAXIMUM FORCE

Specimen	Exp		Num		Num/ Exp	
	Push (KN)	Pull (KN)	Push (KN)	Pull (KN)	Push (KN)	Pull (KN)
Specimen1	140	151.33	136.072	149.55	0.97	0.99
Specimen2	250	254.72	225.62	267.57	0.91	1.05
Specimen3	215	230.22	204.55	234.63	0.95	1.02
Specimen4	260	238	273.69	239	1.05	1
Specimen5	250	245	248.5	272.3	0.99	1.11

TABLE VII. GROUP A: MAXIMUM CFRP STRAIN

Specimen	Num	Exp	Num/Exp
Specimen1	-	-	-
Specimen2	0.0073	0.0075	0.97
Specimen3	0.0085	0.0095	0.89
Specimen4	0.0085	0.0088	0.97
Specimen5	0.008	0.0083	0.96

B. Group B

Figure 4 shows the force-drift hysteresis curve for Group B: CW, RW1 and RW2 under cyclic load [12] (Table VII). Figure 5 compares push of force-drift hysteresis curves of specimens under cyclic load resulting from experimental numerical analysis. Table VIII lists experimental results and compares them to numerical analysis related to maximum forced obtained in reciprocating cycles. As shown, the numerical analysis for Group B specimens is consistent with the experimental results. Figure 4 shows the strain-force hysteresis curve of CFRP materials in numerical analysis for RW1 and RW2 under cyclic load. Table IX compares the experimental and the numerical results which are shown to be consistent.

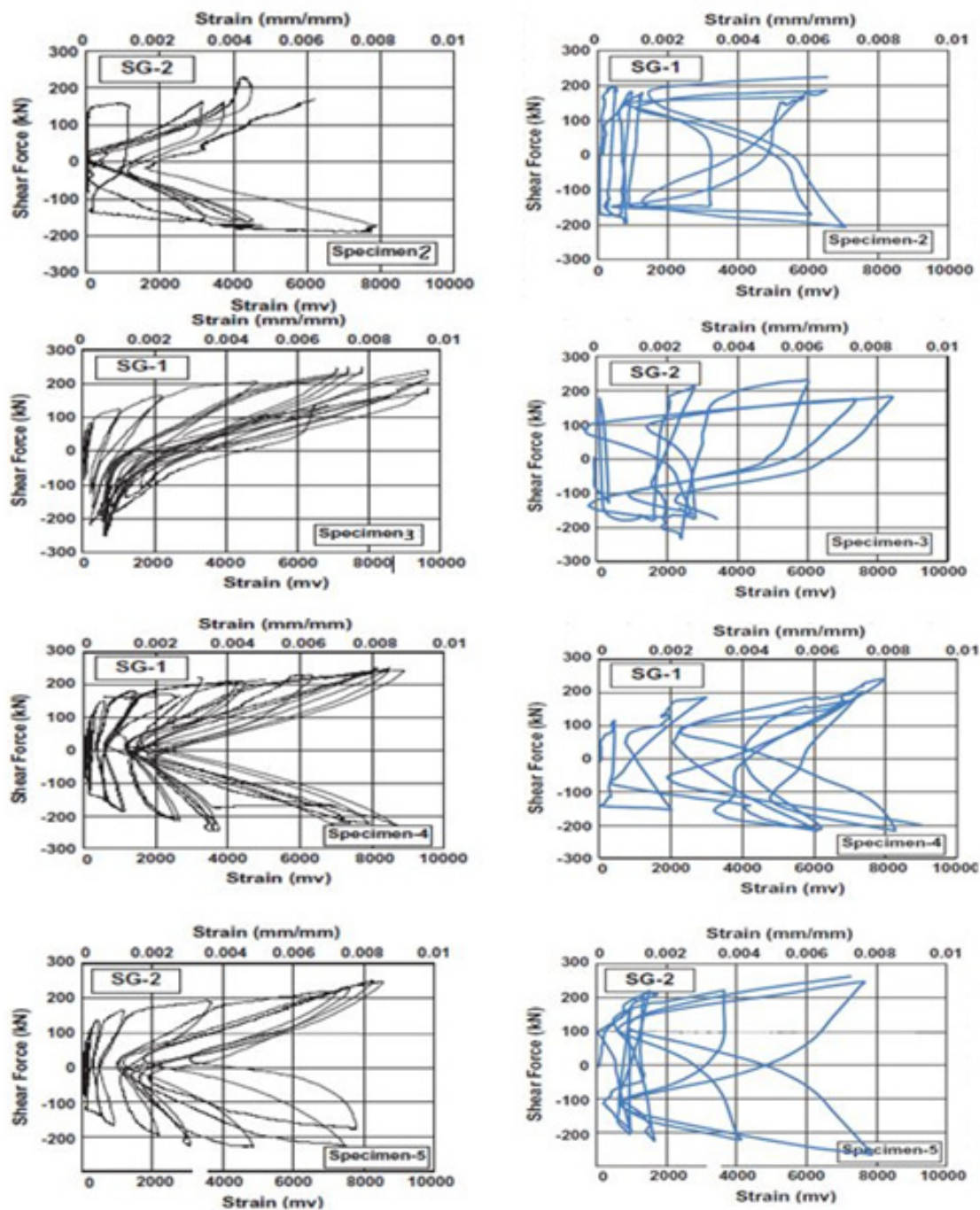


Fig. 3. Strain-force curve of CFRP in Group A, Spesimens 1-5 a) experimental b) numerical

TABLE VIII. GROUP B: COMPARISON OF MAXIMUM FORCE

Specimen	Exp		Num		Num/ Exp	
	Push (kN)	Pull (kN)	Push (kN)	Pull (kN)	Push (kN)	Pull (kN)
CW	60	60	62.53	64.52	1.04	1.075
RW1	110	110	117.53	111.63	1.06	1.01
RW2	94	90	107.82	100.33	1.14	1.11

TABLE IX. GROUP B: MAXIMUM CFRP STRAIN

Specimen	Num	Exp	Num/Exp
RW1	5300	5100	1.04
RW2	4000	4300	0.93

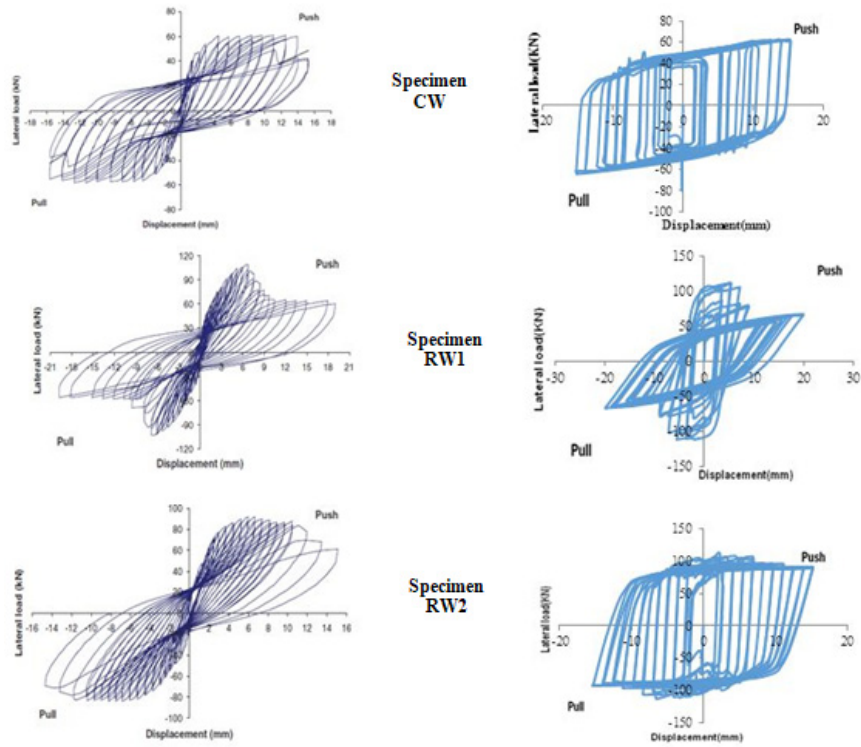


Fig. 4. Force-drift hysteresis curve under cyclic load, Group B, a) experimental b) numerical

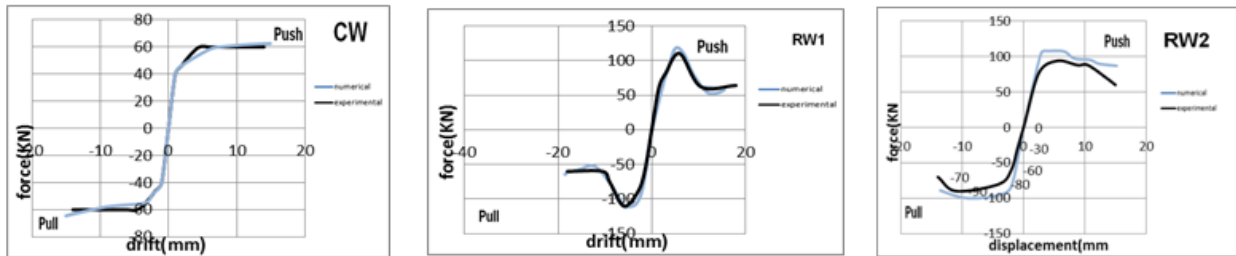


Fig. 5. Push comparison of hysteresis curves of experimental results and numerical analysis for Group B specimens.

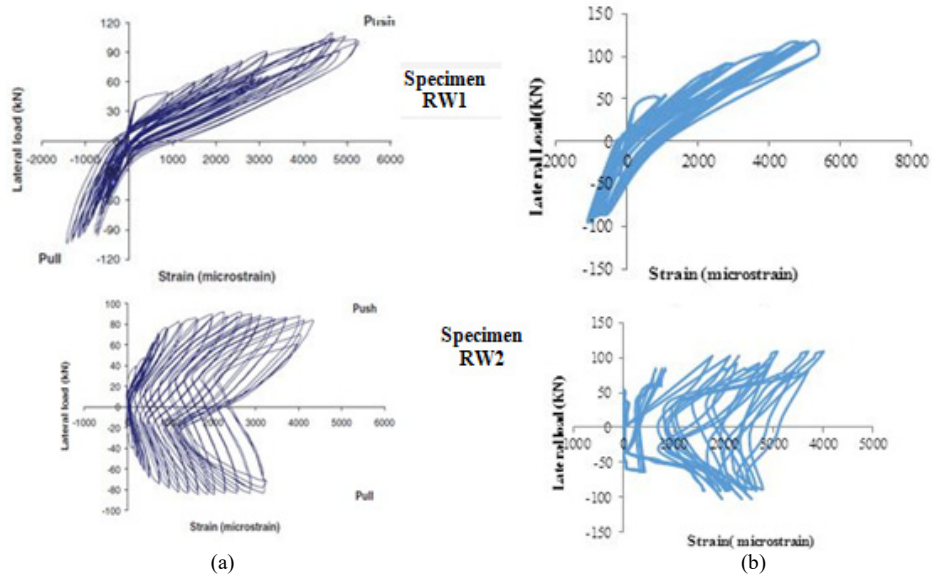


Fig. 6. Strain-force curve of CFRP in Group B, Specimens RW1 and RW2 a) experimental b) numerical

C. Group C

Figure 7 shows force-drift hysteresis curve for Group C specimens under cyclic load [13]. Figure 8 compares the experimental and numerical push of force-drift hysteresis curves. Table X lists the experimental results and compares them to numerical analysis related to maximum forced obtained in reciprocating cycles. As shown numerical analysis results are consistent with the experimental results.

TABLE X. COMPARISON OF MAXIMUM FORCE

Specimen	Exp		Num		Num/ Exp	
	Push (KN)	Pull (KN)	Push (KN)	Pull (KN)	Push (KN)	Pull (KN)
Specimen1	140	150	131.9	150	0.94	1
Specimen2	238	245	239.15	254.07	1.004	1.04
Specimen3	222	220	219.12	225.99	0.99	1.03
Specimen4	225	208	215.73	228.65	0.96	1.09

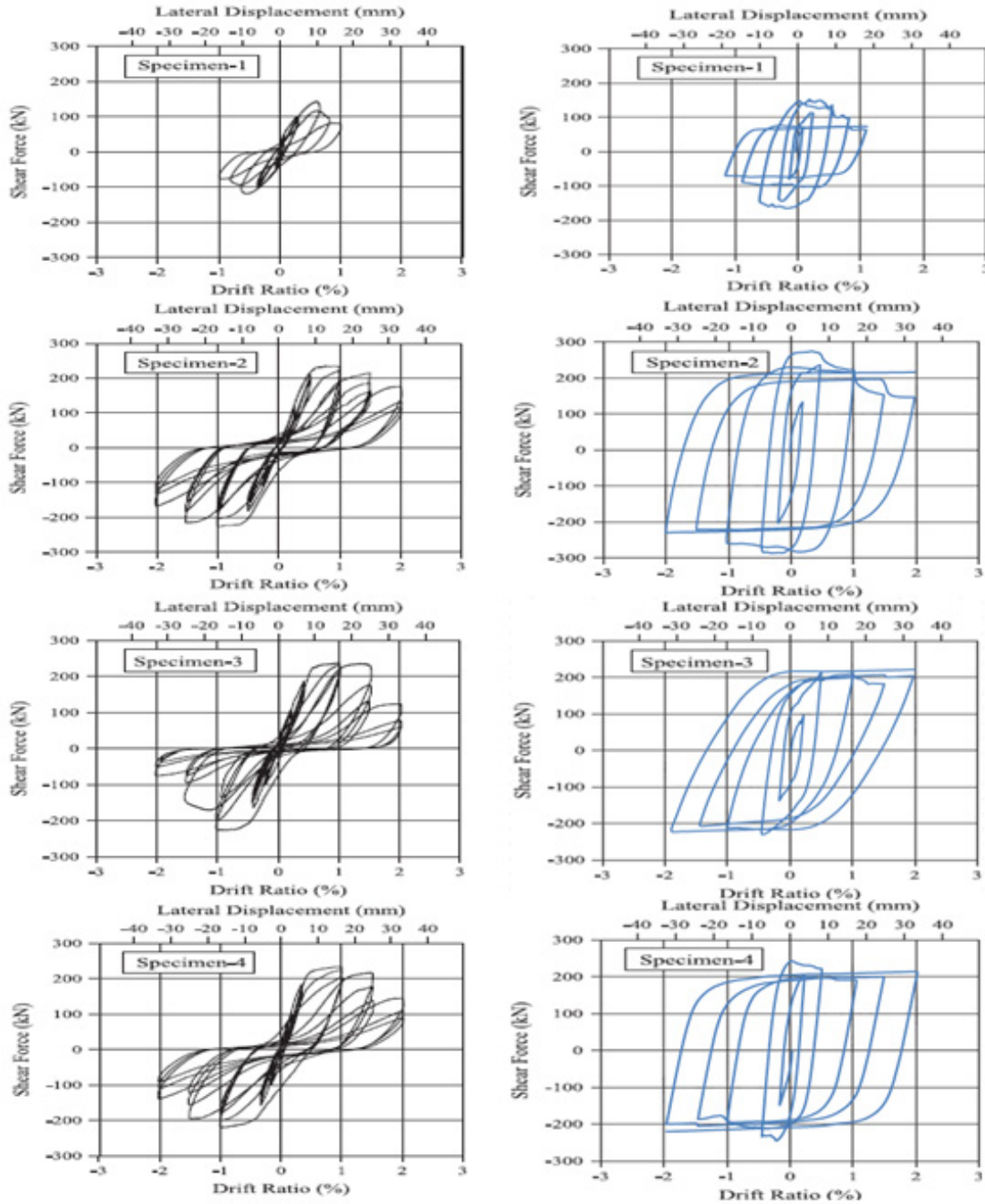


Fig. 7. Force-drift hysteresis curve under cyclic load, Group C – Specimens 1-4 a) experimental b) numerical

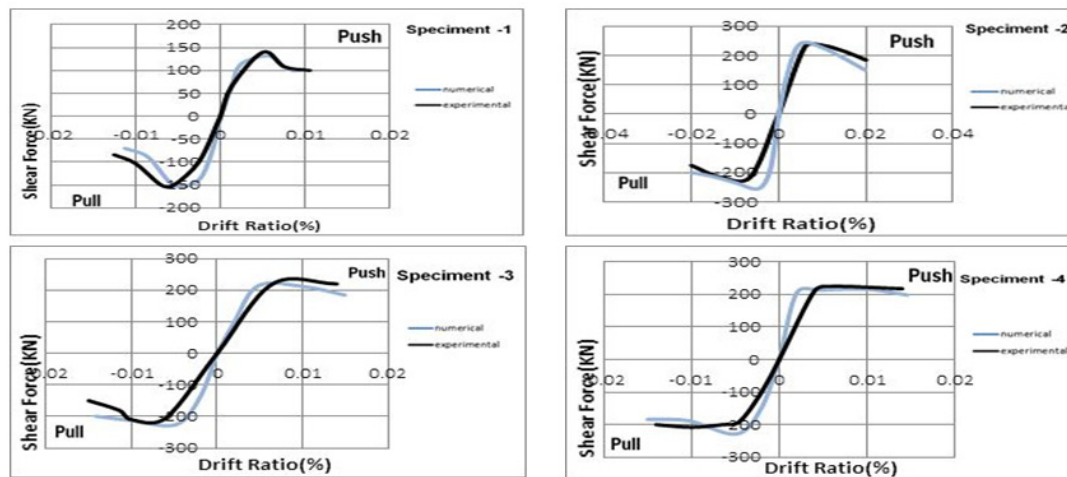


Fig. 8. Push comparison of hysteresis curves of experimental results and numerical analysis (Group C)

V. CONCLUSION

Close results of numerical analysis and experiments on specimens before and after FRP reinforcement indicate that numerical modeling can be used as a scientific and inexpensive tool for analyzing the cyclic behavior of unreinforced and FRP reinforced concrete shear walls. Both numerical and experimental results showed that reinforcement of reinforced concrete shear walls, which have shear weakness under seismic loads by FRP coating, is a suitable solution for increasing their resistance. Adjustment of reinforced strips was effective on cyclic behavior of reinforced shear walls and failure mode. To compensate shear weakness of reinforced concrete shear walls, it is better to use horizontal strips along transverse reinforcements on both sides of the wall. To compensate bending weakness of reinforced concrete shear walls, FRP plates are installed vertically along the height of shear wall parallel to longitudinal reinforcements. In general, results show that shear positions of fibers concentrated on edges increase bending and shear strength of the wall. Both numerical and experimental results show that FRP materials increase ultimate strength related to reinforced walls compared to unreinforced ones.

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