

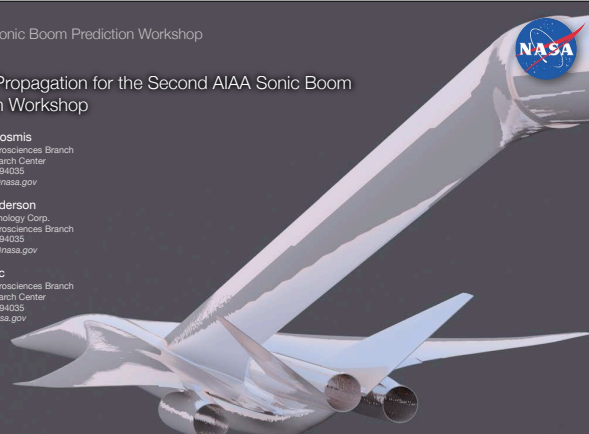
2nd AIAA Sonic Boom Prediction Workshop

sBOOM Propagation for the Second AIAA Sonic Boom Prediction Workshop

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7-8 Jan 2017, Grapevine TX, USA

Outline

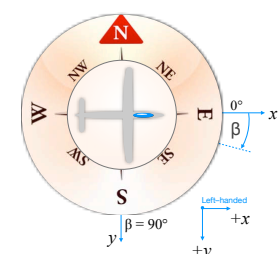
- Intro - codes, conventions and studies
  - Wind Convention
  - Mesh refinement
  - Accuracy requirements
- "Axibody" - Body of revolution
- "LM 1021" - Wind tunnel model of full configuration from 2014 boom workshop
- Summary

Introduction

- Propagation using sBOOM (v2.5)\* for all cases
  - Augmented Burgers' eq.
  - Finite-difference with space-operator splitting
  - Most runs under 1 min on laptop
- Loudness metrics computed with LCASB†
- Applied current "best practices"
- Mesh refinement study done for both geometries using std. atm.
- Ran all required & optional cases

\* Rallabhandi, S. "Advanced Sonic Boom Prediction Using the Augmented Burgers Equation" *J. of Aircraft* 48:1245-1253, 2011.  
† Shepard & Sullivan, "Loudness Code for Asymmetric Sonic Booms (LCASB)", NASA TP 3134, 1991

Wind Convention



- sBOOM uses left-handed coordinate system for wind
- $\beta$  = heading,
  - $\beta = 0^\circ$  A/C pointed East
  - Clockwise =  $+\beta$
- sBOOM wind tables are in meters vs m/s
- x and y inputs are wind components ("blows toward")

$(x, y) = (1, 0)$  is tail wind if heading is East  
 $(x, y) = (0, 1)$  is tail wind if heading is South  
 $(x, y) = (1, 1)$  is tail wind if heading is South-East

Net result is that sign on y-component of wind in the workshop wind-specification needs to be flipped.  $(W_x, W_y)_{sBOOM} = (W_x, -W_y)_{workshop}$

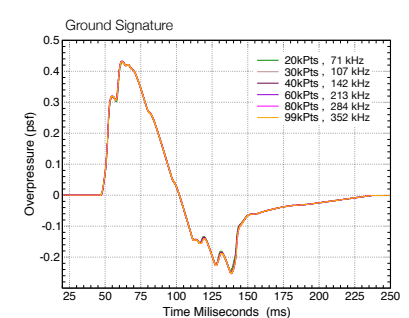
Mesh Convergence

Sensitivity of noise output to mesh refinement

- Propagation code is solving augmented Burgers' via finite difference
- Need to make sure we're getting mesh converged result
- Mesh convergence is case dependent
  - Do for each case, assume std atmosphere
- Dissipation due to truncation error directly impacts accuracy, resolution requirements are driven by need to minimize error in propagation
  - Initial signal typically has < 2 k pts
  - Propagation typically requires 20-50 kpts

Mesh Convergence

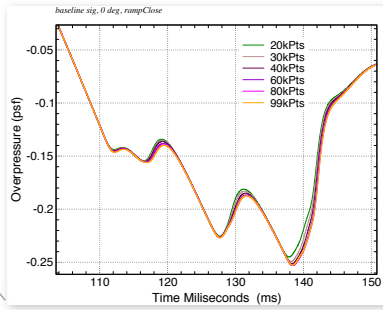
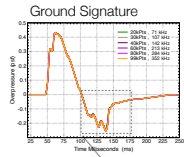
Sensitivity of noise output to refinement of the propagation mesh





## Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh

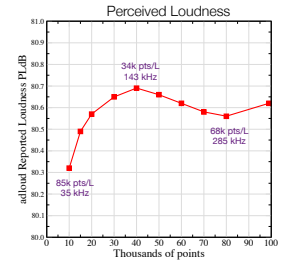
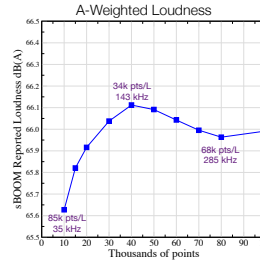


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## Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh



- Both dB(A) and PLdB show similar behavior
- Lower than 35 kHz, noise outputs drops quickly
- However, mesh convergence not convincing, even at higher frequencies

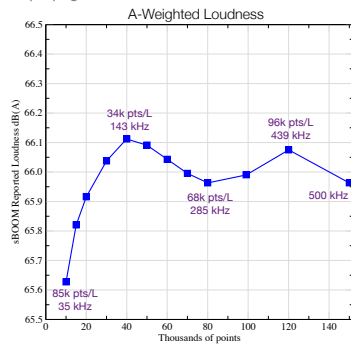
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## Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh

- Ran up to 500 kHz
- Mesh convergence still not convincing
- At 500 kHz, oversampling original signal by nearly 100:1
- Possibility of aliasing due to oversampling



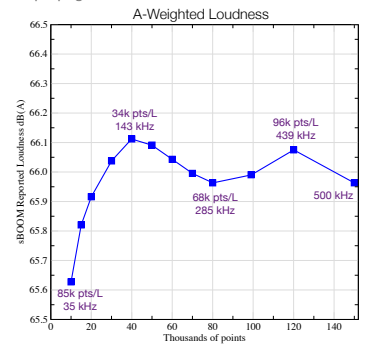
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## Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh

- Slow mesh convergence not surprising
- Signal is non-smooth, and integrated loudness outputs are very sensitive
- Oversampling introduces higher frequencies which may effect loudness output

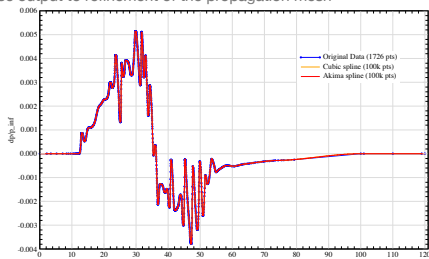


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## Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh



- Spline data at high resolution with Akima spline
- Pass high-resolution data from splined signal into sBOOM to avoid aliasing high-frequencies

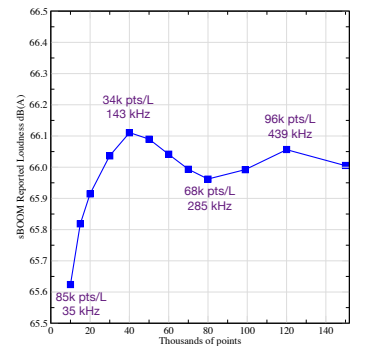
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## Mesh Convergence

Spline data to avoid aliasing

- Somewhat better mesh behavior at high frequencies, but...
- Mesh convergence still not really convincing
- Need to investigate more
- Used un-splined data sampled at 107 kHz (30 kpts) for runs

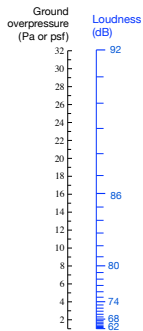


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### Caveats on Accuracy Requirements

Decibels are logarithmic units!

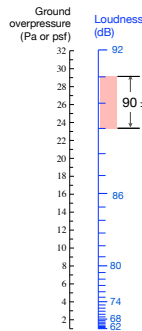


Double the loudness → -10 dB more sensed loudness level (psycho acoustic)  
 Double the sound pressure level → 6 dB more measured sound pressure level



### Caveats on Accuracy Requirements

Decibels are logarithmic units!



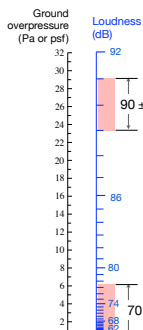
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- We propagate pressure signals to the ground  
 ↳ Propagation error has units of pressure
- e.g.
  - If error of ±2 Pa on a 90 dB signal is less than ± 1 dB
  - The same error on a 70 dB signal may be ± 6 dB
- Propagation accuracy requirements increase logarithmically as signals get quieter!
- Sampling frequency for a 90 dB signal is likely to be insufficient for a 70 dB signal



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### Axibody

Shaped axisymmetric body of revolution



Conditions:

- $M_\infty = 1.6$
- Altitude = 15849.6 m (52 kft)
- $Lref = 42.98m$  (141 ft)
- $r/L = 3.0$  at signal extraction
- Ground reflection factor = 1.9
- Heading East ( $\beta = 0^\circ$ )

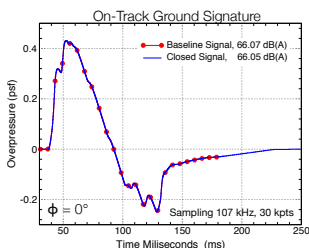
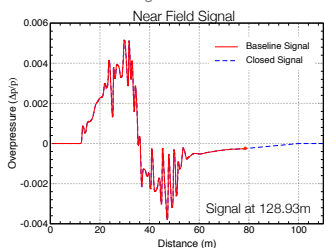
Cases:

- Required: Atm #3
- Optional #1: Std. Atm.
- Optional #2: Atm #4
- Optional #4: Std. Atm. with 70% humidity



### Axibody

Close near field signal

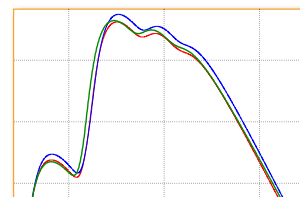
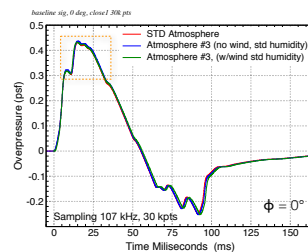


- Compared 2 different closures (both linear ramps) gave consistent results
- Closed signal using linear ramp to 0 at 100 m
- Ground signals & noise both virtually identical



### Axibody

Ground signature – Atmosphere #3 vs Standard Atmosphere

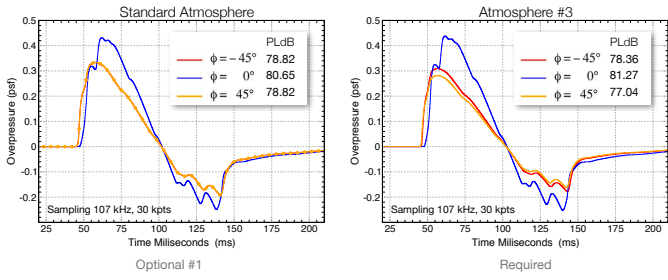


- Atmosphere 3 was required case
- ~0.6 PLdB louder than standard atmosphere



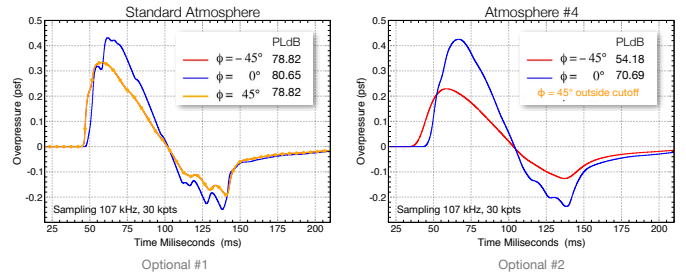
# Axibody

Ground signature – Standard Atm. vs Atmosphere 3,  $\phi = \{-45^\circ, 0^\circ, 45^\circ\}$



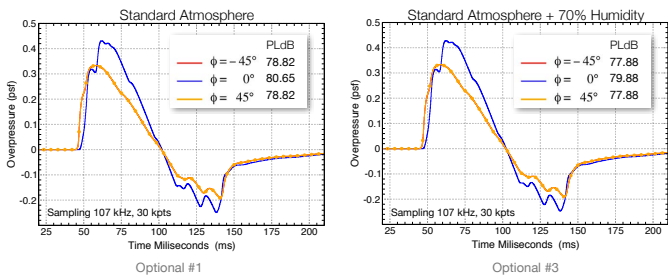
# Axibody

Ground signature – Standard Atm. vs Atmosphere 4,  $\phi = \{-45^\circ, 0^\circ, 45^\circ\}$



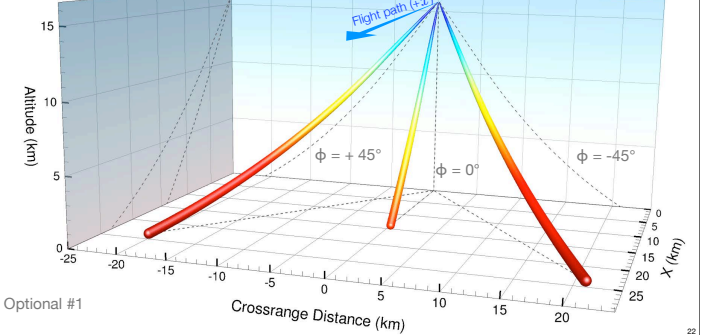
# Axibody

Ground signature – Standard Atm. vs Standard Atm. + 70% Relative Humidity



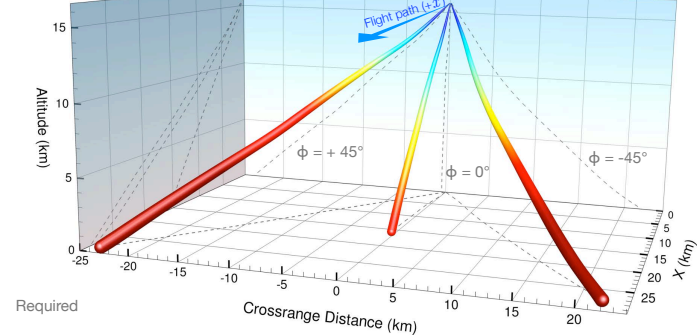
# Axibody

Raytubes, standard atmosphere Colored by raytube area



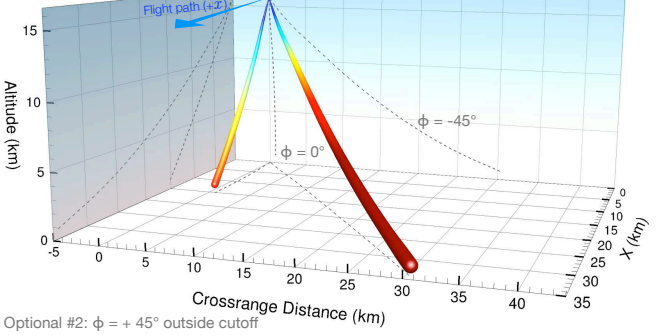
# Axibody

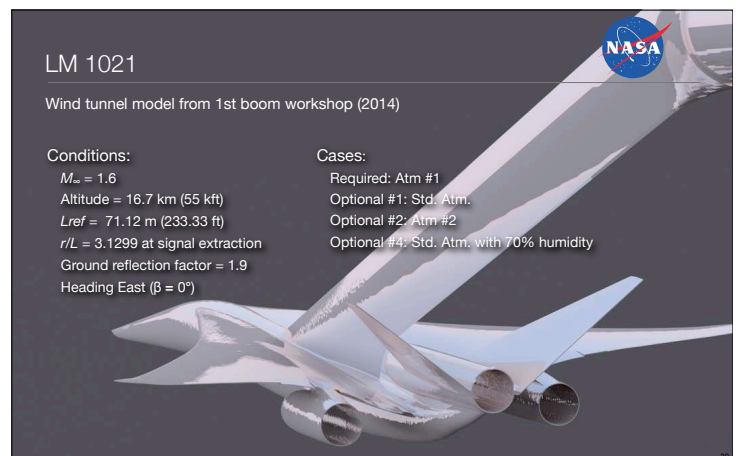
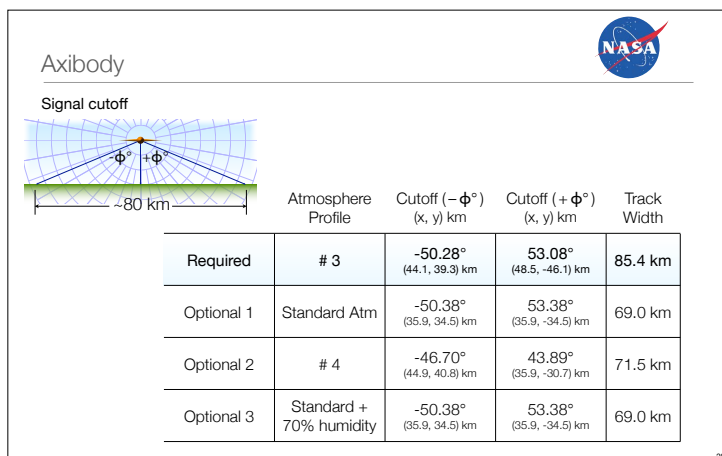
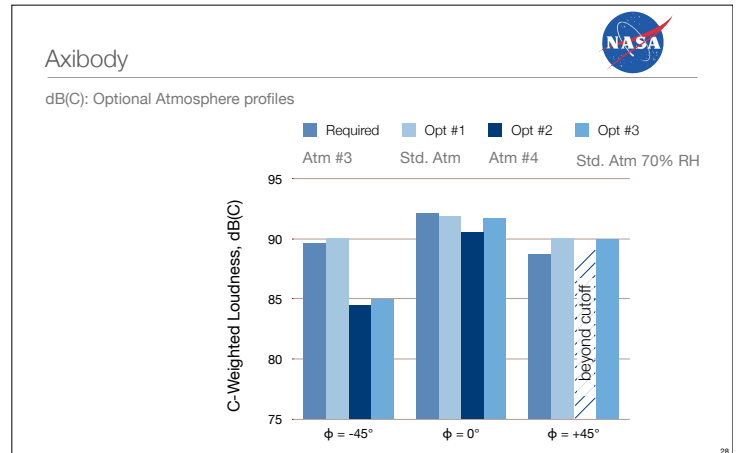
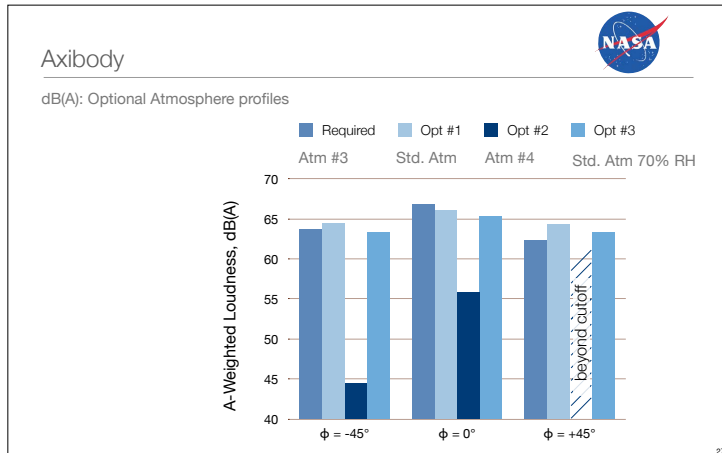
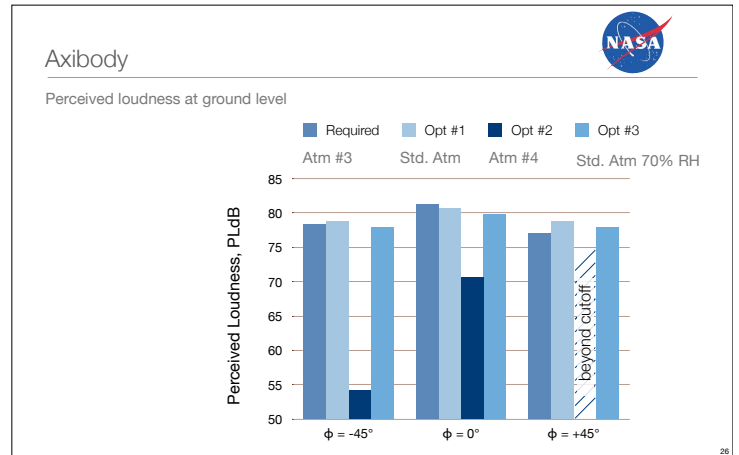
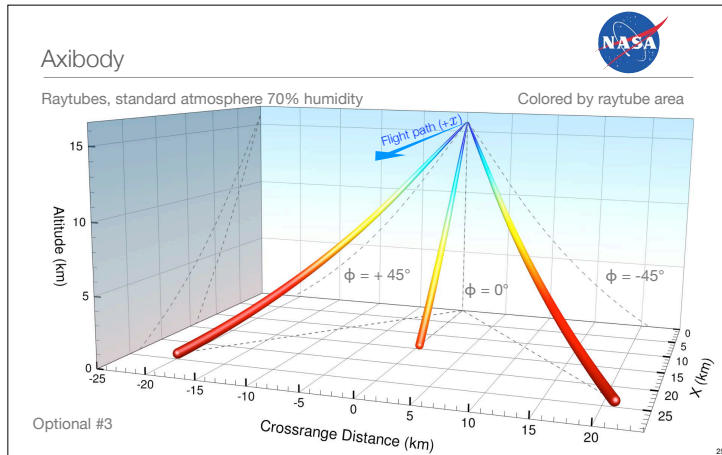
Raytubes, Atm #3 Colored by raytube area

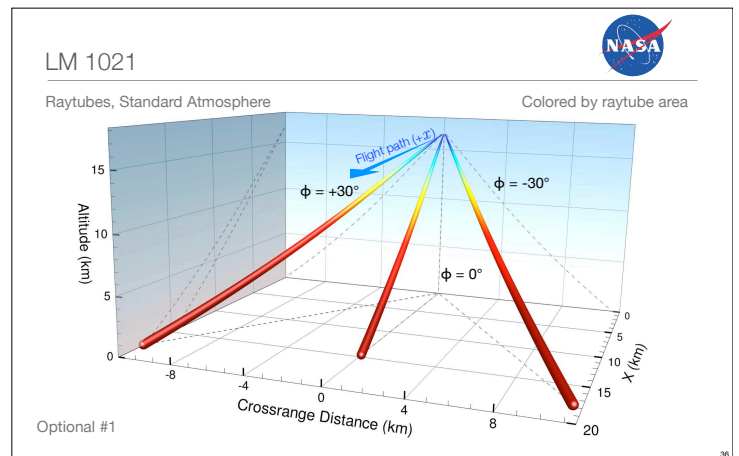
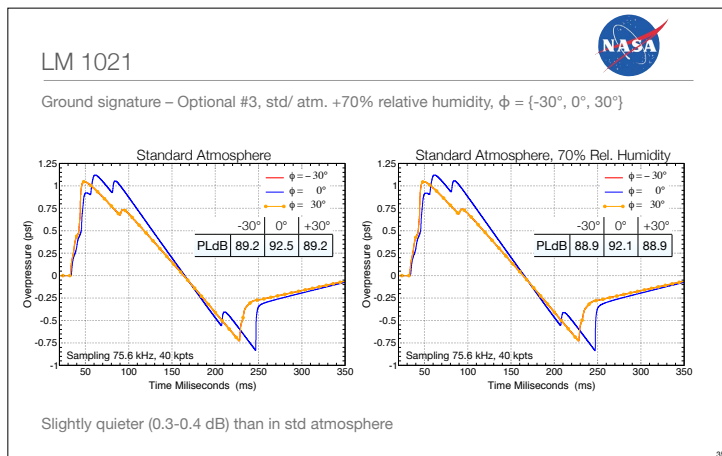
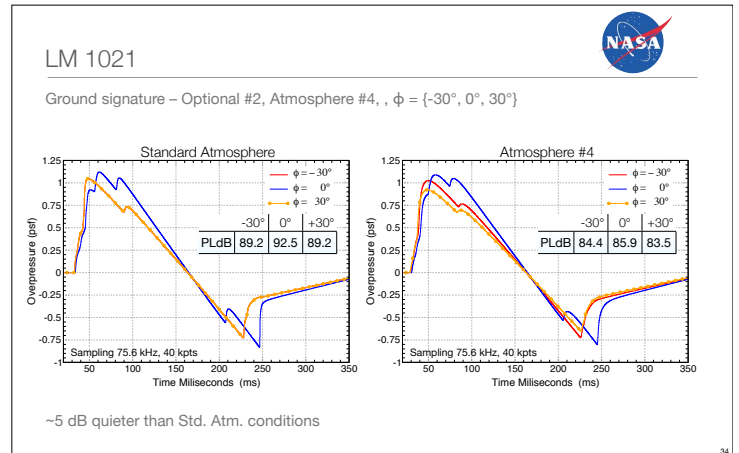
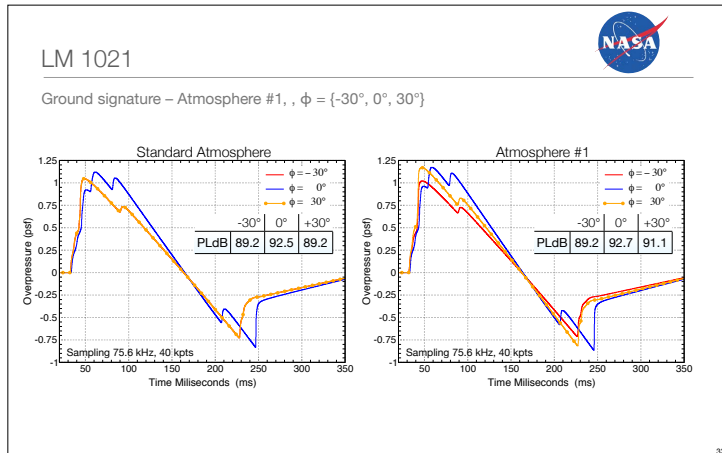
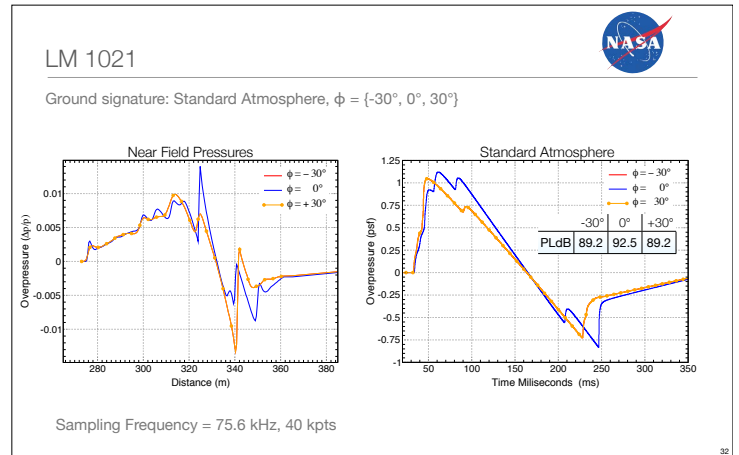
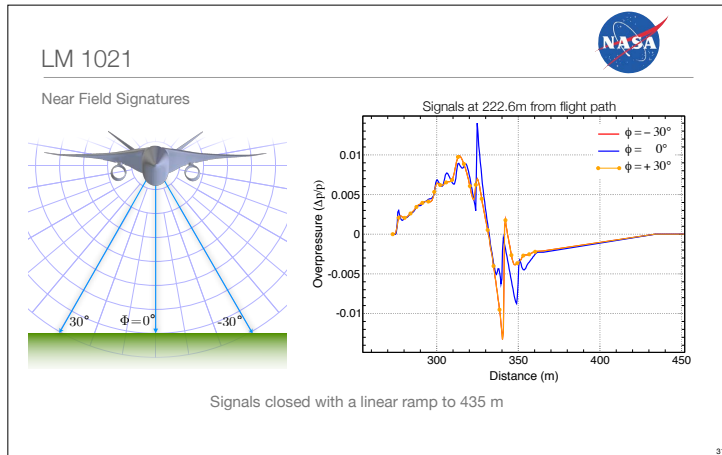


# Axibody

Raytubes, atmosphere 4 Colored by raytube area



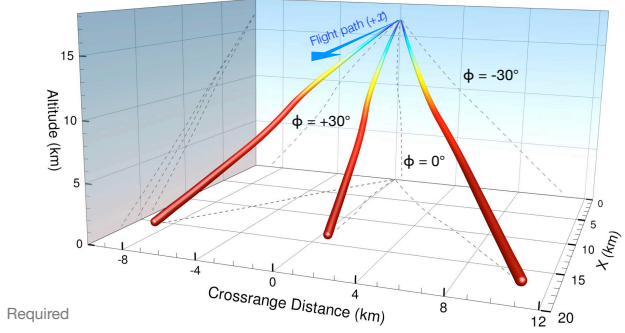






# LM 1021

Raytubes, Atmosphere #1

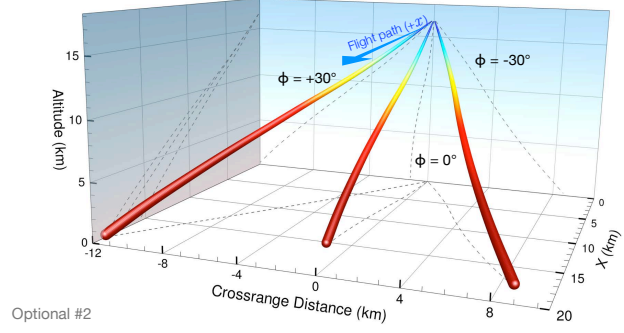


Required



# LM 1021

Raytubes, Atmosphere #2

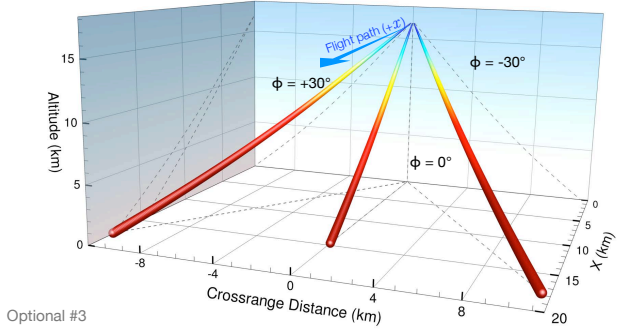


Optional #2



# LM 1021

Raytubes, Standard Atmosphere with 70% relative humidity

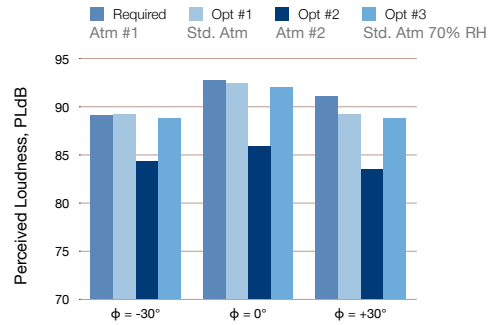


Optional #3



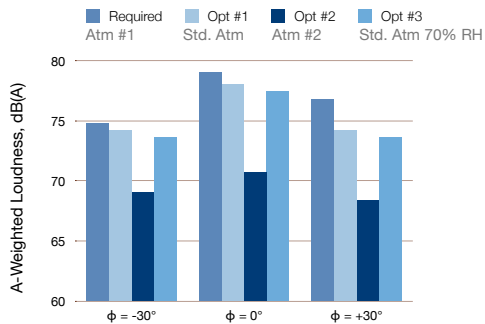
# LM 1021

Perceived loudness at ground level



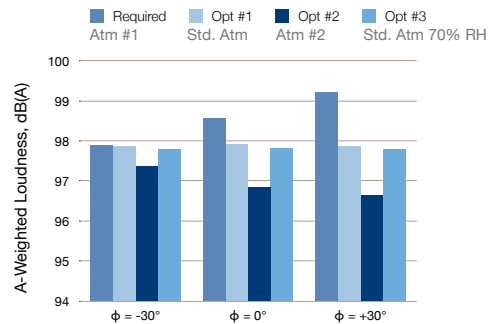
# LM 1021

A-Weighted Loudness at ground level



# LM 1021

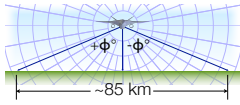
A-Weighted Loudness at ground level





# LM 1021

## Signal cutoff



	Atmosphere Profile	Cutoff ( $-\phi^\circ$ ) (x, y) km	Cutoff ( $+\phi^\circ$ ) (x, y) km	Track Width
Required	# 1	-57° (40.0, 42.3) km	74° (39.4, -44.6) km	86.9 km
Optional 1	Standard Atm	-50.38° (37.0, 35.6) km	50.38° (37.0, -35.6) km	71.2 km
Optional 2	# 2	-64.65° (43.9, 41.7) km	59.35° (67.0, -69.7) km	111.4 km
Optional 3	Standard + 70% humidity	-50.38° (37.0, 35.6) km	50.38° (37.0, -35.6) km	71.2 km



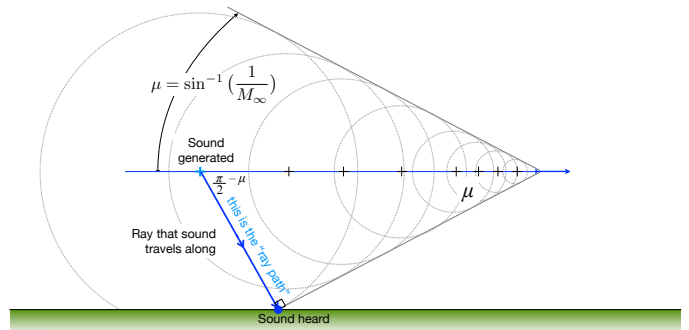
# Summary

- Applied sBOOM and LCASB for all required and optional cases
- Showed difficulty in obtaining mesh-converged loudness metrics
  - Noted issues due to oversampling
  - Noted that resolution requirements increase as signals get quieter
- Open questions & Opportunities
  - Impact of step-size on mesh convergence?
  - Splining of the input
  - Consider higher-order discretization to control truncation error at lower sampling rates
  - Automatic output-based adaptation of sBOOM propagation mesh for loudness functional

# Questions?



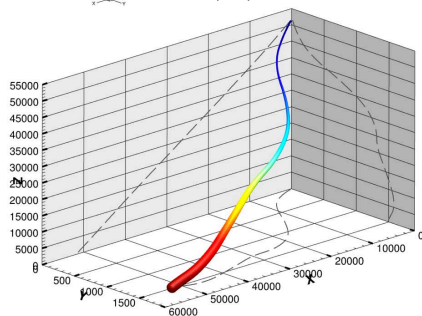
# understanding the ray path



# Effect of wind on raytube (sBOOM coords)



here is a cross-section of the raytube with the wind. tube is scaled by local raytube area



• %% sBOOM 2.5 -v -d reports:  
 - Ground intercept: For Azimuth: 0.000000  
 - Propagation time: 68.010707 (s)  
 - X = 51811.993216 (ft) Y = 1478.793091 (ft)