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Approach Towards Energy Efficient Power Amplifier for 4G Communications

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Abstract—The biggest challenge for future 4G systems is the need to limit the energy consumptions of battery-powered and base station devices, with the aim to prolong their operational time and avoid active cooling in the base station. The green wireless communications requires research in areas such as energy efficient RF front end, MAC protocol, networking, deployment, operation, and also the integration of base station with renewable power supply. In this paper, the design concept of energy efficient RF front end is considered in terms of RF power amplifiers at which it represents the workhorse of modern wireless communication systems and inherently nonlinear. The approach of output power back off is to amplify the signal at the linear region to avoid distortion, but this approach suffers from significant reduction in efficiency and power output. To boost the efficiency at wide range of output power and keep the same margin for signal with high crest factor, the load modulation technique with new offset line are employed to operate over the frequency range of 3.4GHz to 3.6GHz band. The performances of load modulation power amplifier are compared with balanced amplifier. The results of 42dBm output power and 62% power added efficiency are achieved.

Index Terms— Balanced amplifier; load modulation RF power amplifier; OFDM; 4G

I. INTRODUCTION

The approach towards energy conservation and CO₂ reduction in 4G communications will require a lot of effort form physical layer to upper layers. As of today information and communication technology accounted for 3% and 2% global power consumption and global CO₂ emissions respectively. Corporate social responsibility for international efforts against climate change, targets set to reduce carbon emissions and environmental impacts of networks. Therefore, there’s need at both terminal and base station, to take a more holistic approach for improving or achieving green communications, right from radio operation, functionality, up to the implementation. 4G devices should be reconfigurable for multi-standard radios; that will scan the available spectrum and change its network parameters (frequency, bandwidth, modulation) for maximum data transfer, highly integrated, power efficient, and low cost. The 4G networks will provide mobility and connectivity at all the time, putting the priority of data over voice; as a result of this it needs higher modulation scheme to accommodate data. However, 4G adopts Orthogonal Frequency Division Multiplexing (OFDM), with modulations from QPSK to 64-QAM, and has crest factor around 9dB-12dB. This wideband digital modulation scheme offers high data rates and resilience to multipath effects. However, the scheme is critically dependent on linearity in the hardware system due to its inherently high crest factor and also affects the RF power amplifier efficiency. To support the proposed data services, the base station and the user terminal itself must be able to handle higher data rates. Achieving high efficiency and good linearity simultaneously in power amplifier design are the most challenging task.

The 4G offers a higher data rate but unfortunately at the expense of more power consumption. The transmitted power of base station increase exponentially as the data rate increase, from the baseband unit, the radio and the feeder network, the radio consumes more than 75% energy of the base station’s energy need and 60% consumed by power amplifier alone. The power amplifier consumes the highest power at the base station and converts more than 50% of what it consumed into heat as a waste. This paper explores the energy efficient power amplifier. The efficiency and the output power of the load modulation power amplifier have been achieved and the results show significant improvement over balanced RF power amplifier.

II. CONVENTIONAL BALANCED AND LOAD MODULATION CIRCUIT ARCHITECTURE

The conventional balance and load modulation amplifiers exploit the Freescale N-Channel Enhancement-Mode Lateral MOSFET MRF7S38010HR3 transistor. The balanced amplifier was first proposed to improve efficiency of 3G base station, is designed to work over a given dynamic range where the amplifier should behave linearly. Conventional balanced amplifier was commercially successful 2G/3G base station amplifiers. However, there are some problems that limit the balanced amplifier for use as power amplifier for 4G communications. Balanced amplifier can be realized by combining two class AB amplifiers as shown in Figure 1. The splitter divides the input signal equally with 90 degree phase-shift, after the input matching circuitry the signals are fed to the transistors’ gates. With the proper biasing of VGS both class AB amplifiers are set to conduct in the positive cycles, the signals from the drain of the transistors are also
90 degree in phase and feed into the combiner and at the output, combiner combines the signals un-phase-shift, and full sine wave. While load modulation can be realized by combining carrier class AB and peaking class C amplifiers as shown in Figure 2. The splitter divides the input signal into two equal magnitude but 90 degree phase difference. At the output a microstrip quarter wave impedance inverter combines the signals. The concept of load modulation technique has been fully explained by the present authors of their previous work in [2]. Load modulation power amplifier improves the efficiency and the linearity by complementing the saturation class AB amplifier with the turn on characteristic of class C amplifier.

The design comprises of step-by-step procedure for the optimum design of energy efficient power amplifier, the proposed additional of 90 degree offset lines at the output and input matching network for which will prevents power leakage at the output junction between the output impedance transformer and peaking Class C amplifier. The gate biases and the individually matchings of class AB and class C amplifiers are further optimized to achieve high efficiency, linearity and wideband characteristics. The peaking amplifier allows the load modulation amplifier to respond to the high input levels of short duration, by amplifying the signal peaks, and to dynamically change the load impedance of the main class AB amplifier.

III. DESIGN LAYOUT AND RESULTS

The conventional balanced and load modulation amplifiers are fabricated with RT 5880 substrates, H=0.5mm and relative permittivity of 2.2. Figure 3 and 4 shows the layout of conventional balanced amplifier and load modulation amplifier respectively. Figure 5 and 6 shows the simulated linear performance of the balance and load modulation amplifier respectively, the gain is flat in the range of 3.47 to 3.53 GHz with excellent input and output return losses.

The non-linear simulations and the comparisons of conventional balanced and load modulation amplifiers are performed. The bias conditions used in this experiment are shows in table 1, for balanced amplifier while in table 2; represent that of load modulation amplifier. The drain bias voltage VDS = 30V for both two transistors of balanced and their gate voltage is VGS = 3V. The drain bias voltage of load modulation amplifier is VDS = 30V for both carrier and the peak transistors, while their respective gate bias voltages are VGS (Carrier) = 3V and VGS (Peaking) = 2.2V. Figure 7 represent the comparison of the variation of the input power versus output power of both balanced and load amplifiers. It clearly shows that 42dBm output power is achieved at the linear region of both amplifiers. Figure 9 represent the transducer power gain versus output power. The load modulation has less gain compared to balanced amplifier; this is due to the fact that the peaking amplifier of load modulation is biased in Class C mode. Figure 10 shows the power added efficiency (PAE) versus output power of balanced and load modulation amplifier. From the graph one can be seen that the load modulation amplifier has a higher efficiency over the wide range of output power than conventional balanced amplifier. The PAE of 62% is obtained at 1dB compression point of 42dBm output power of load modulation amplifier while the PAE of 50% is obtained at 1dB compression point of 42dBm output power of conventional balanced amplifier.

The load modulation offers improved efficiency at the whole range of output power compared to conventional balanced amplifier. The heart of the load modulation is the load modulation output combiner and that is the fascinating part of the design, while the input behaves the same as a conventional balanced amplifier.

Table 1: Bias point setting for balanced amplifier

<table>
<thead>
<tr>
<th>Drain Voltage (V)</th>
<th>Class AB VGS (V)</th>
<th>Class AB2 VGS (V)</th>
</tr>
</thead>
<tbody>
<tr>
<td>30</td>
<td>3.0</td>
<td>3.0</td>
</tr>
</tbody>
</table>

Table 2: Bias point setting for load modulation

<table>
<thead>
<tr>
<th>Drain Voltage (V)</th>
<th>Carrier VGS (V)</th>
<th>Peaking VGS (V)</th>
</tr>
</thead>
<tbody>
<tr>
<td>30</td>
<td>3.0</td>
<td>2.2</td>
</tr>
</tbody>
</table>

Table 3: Performances of load modulation and balanced amplifiers

<table>
<thead>
<tr>
<th></th>
<th>Gain (dB)</th>
<th>PAE (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Balanced</td>
<td>19.5</td>
<td>50</td>
</tr>
<tr>
<td>Load Modulation</td>
<td>16.5</td>
<td>62</td>
</tr>
</tbody>
</table>
Figure 3. Design layout of Balance amplifier

Figure 4. Design layout of load modulation amplifier

Figure 5. Linear simulation of Balance amplifier

Figure 6. Linear simulation of load modulation amplifier

Figure 7. AM-AM responses

Figure 8. AM-PM responses

Figure 9. Transducer power gain

Figure 10. Power-Added Efficiency

IV. CONCLUSION

The performance comparisons between load modulation power amplifier and conventional balanced power amplifier are performed. The achieved results of the proposed design process have shown an excellent efficiency and power performances. The proper phasing of input signal splitter effectively contributed to the total efficiency of the system. The load modulation amplifier offers improved efficiency over wide range of output power compared to conventional balanced amplifier. The load modulation has less gain compared to balanced amplifier due the arrangement of lower biasing of Class C peaking transistor of load modulation. The operation of this design was strongly influenced by the coupling factor of the splitter, biasing of class AB and C amplifiers. Applying load modulation technique can significantly reduce the CO₂ emission and power consumption in the transceiver. The self-managing characteristic of the load modulation power amplifier has made its implementation more attractive.
ACKNOWLEDGMENT

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